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*Institute for
Ocean Technology*

CFD Predictions for Ocean Gliders

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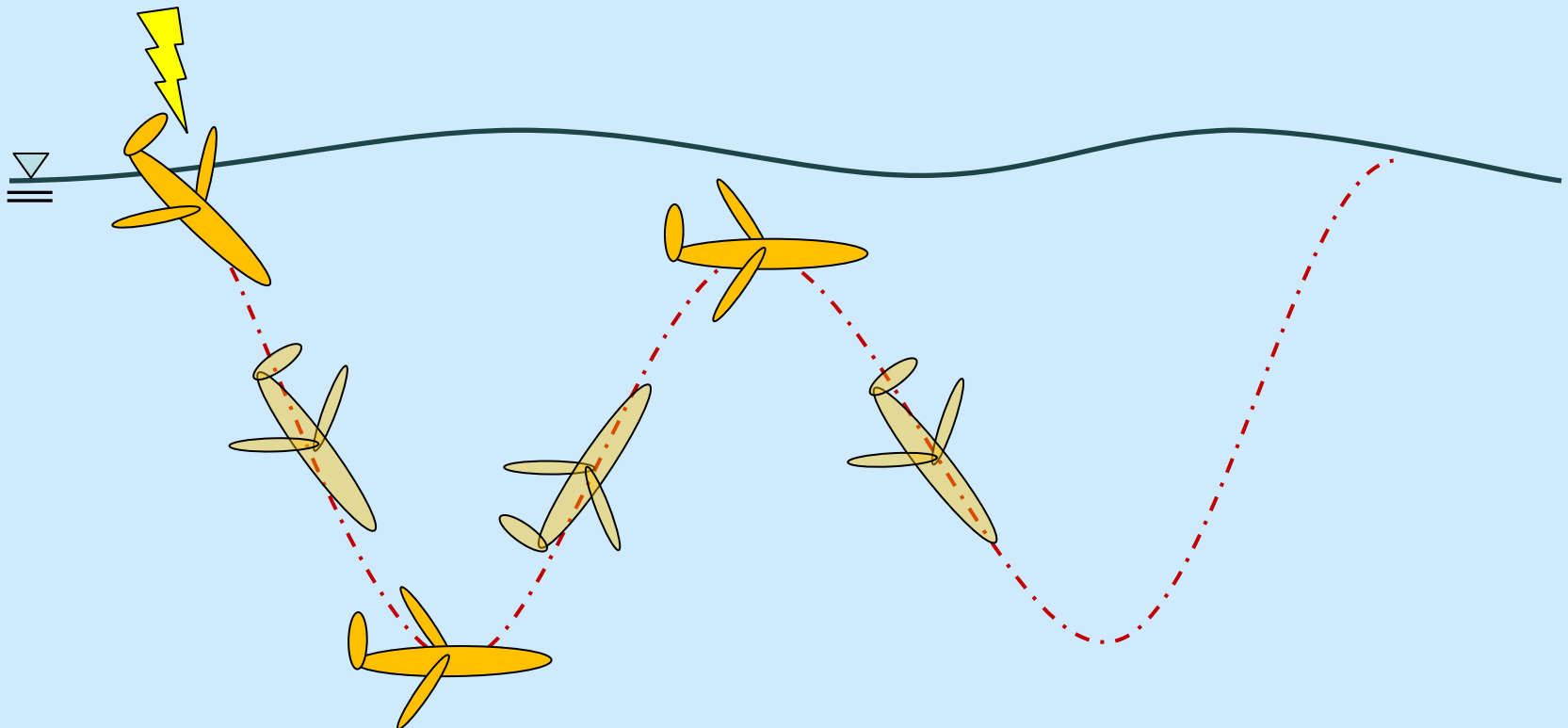
Canada

Outline

- Research background
 - Concept of acoustic survey using ocean glider
 - Roll of CFD analysis
- Numerical model for CFD analysis
 - Grid system
 - Turbulence mode
- Results
 - Velocity and pressure contour
 - Pressure & shear coefficient
 - Validation
- Summary & future work

Ocean glider

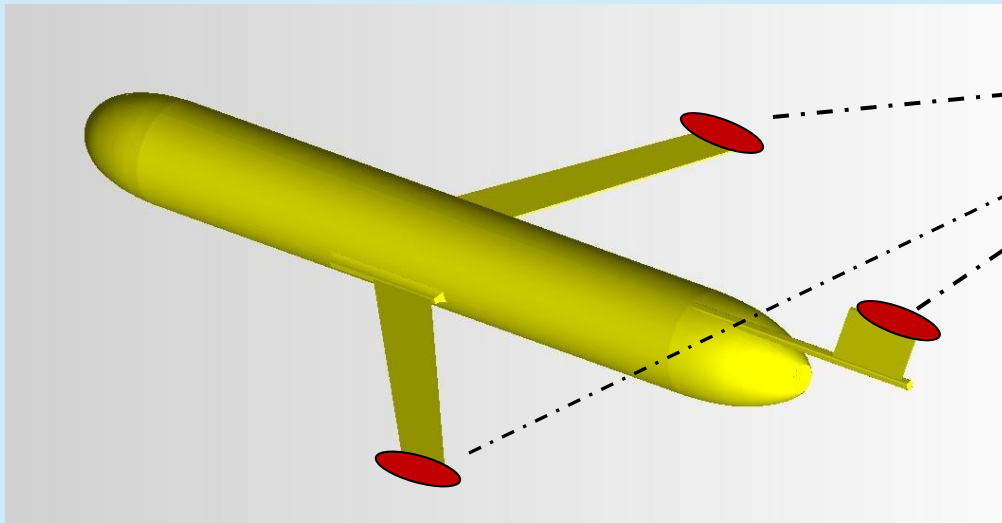
- Saw-tooth trajectory of ocean glider
→ **Long operation time & wide coverage**



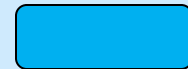
Acoustic survey using ocean glider

- Long operation time
- Low ambient noise due to no external propulsion device
- Long base line between hydro-phones

 Hydrophone

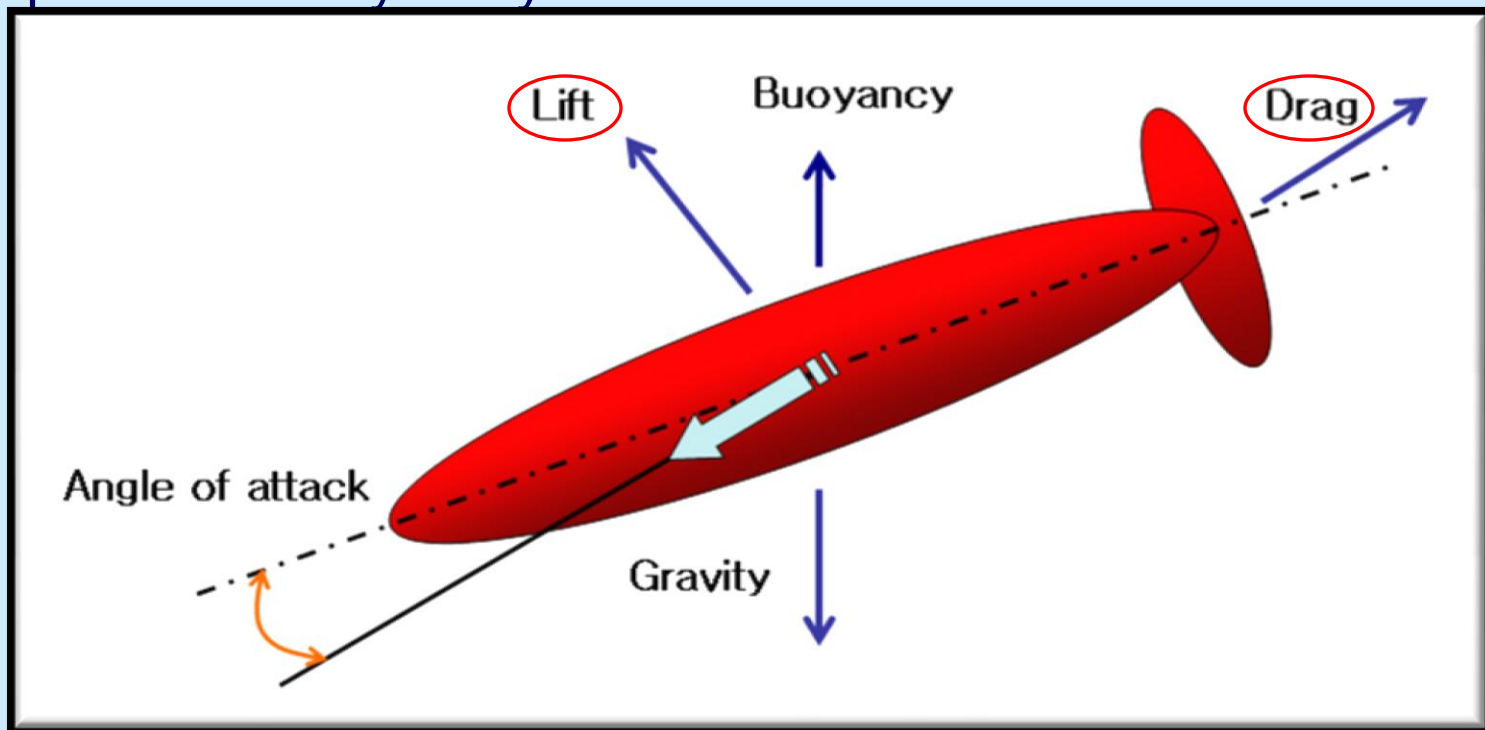


Sound source



Balancing problem

- Importance of hydrodynamic force



To change the hull for installing the hydrophones

➡ ***Needs for estimating hydrodynamic forces of the modified body***

Object of CFD analysis

At design stage,

to predict hydrodynamic forces such as drag and lift

- Optimum design of the buoyancy engine
- Accurate prediction of the operation time

to estimate the local flow around hydrophone

- Minimizing the ambient noise caused by violent flow

to predict maneuverability

- Radius of turning circle and the depth requirement for the mode change

In this study,

to examine CFD performance and prepare the hull modification

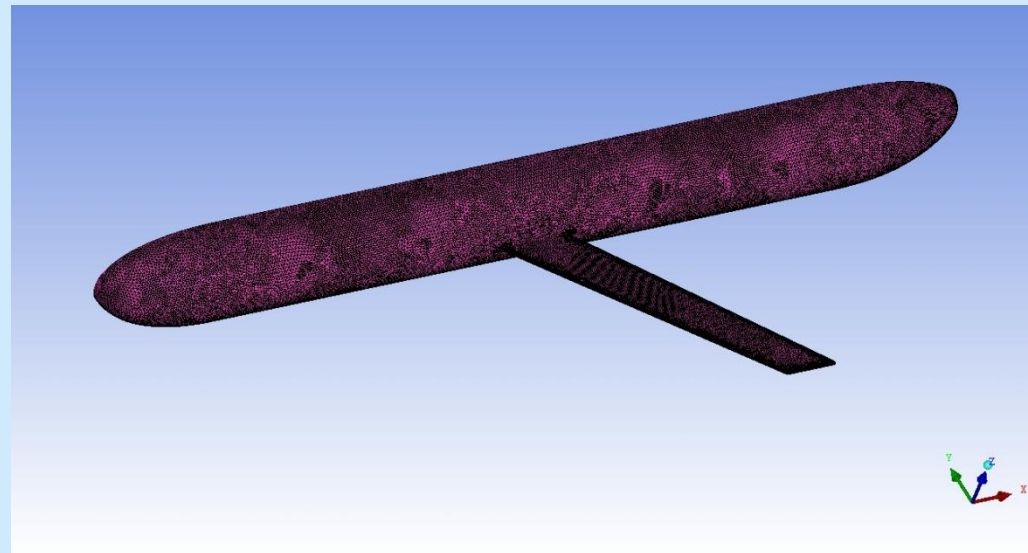
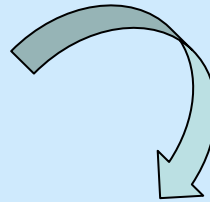
Geometric model

Slocum glider



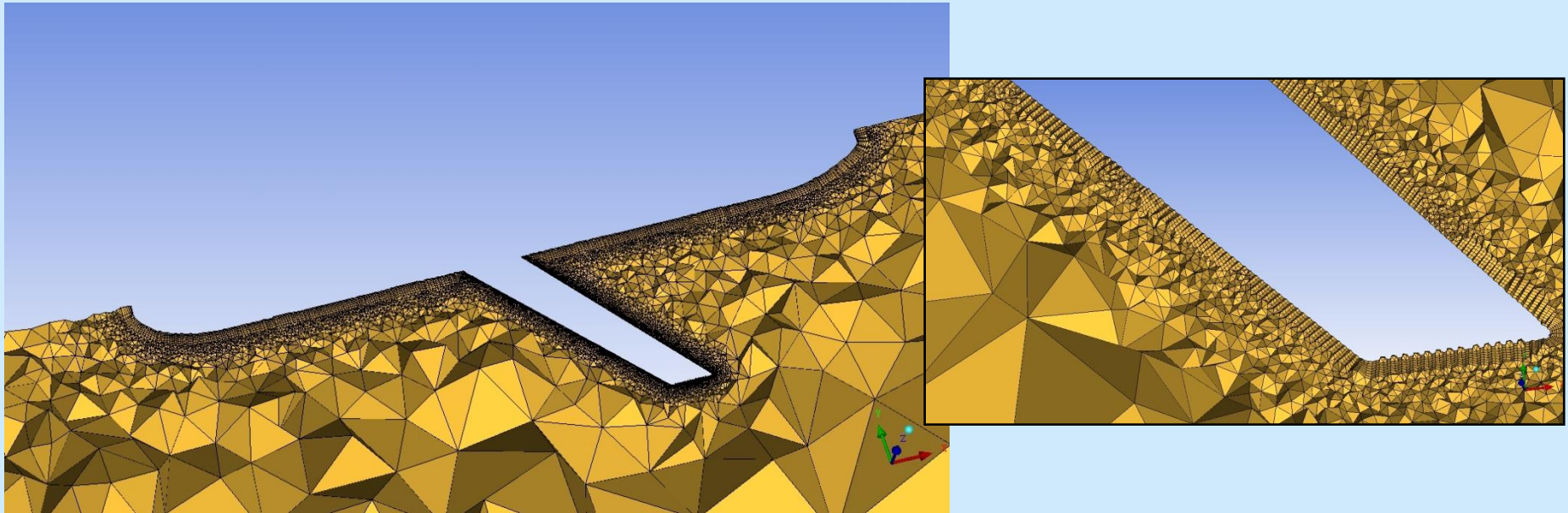
From www.webresearch.com

Simplified geometry
without tail wing and small
appendages



Grid system

- Hybrid grid system
 - Unstructured surface mesh
 - Prismatic layer
 - 7 layers with 2mm thickness of the first layer $\sim Y^+ < 10$
 - 1.8 million cells



Turbulence model

- Shear-stress transport (SST) k- ω model
 - Widely used model for streamlined aerodynamic and hydrodynamic bodies
- SST transition model
 - Developed for the laminar-turbulent transition
 - ***Reynolds number of ocean glider: $10^5 \sim 10^6$***
 - Cost effective method compared with LES* or DNS** considering transition flow

* *Large Eddy Simulation*

** *Direct Numerical Simulation*

Simulation case

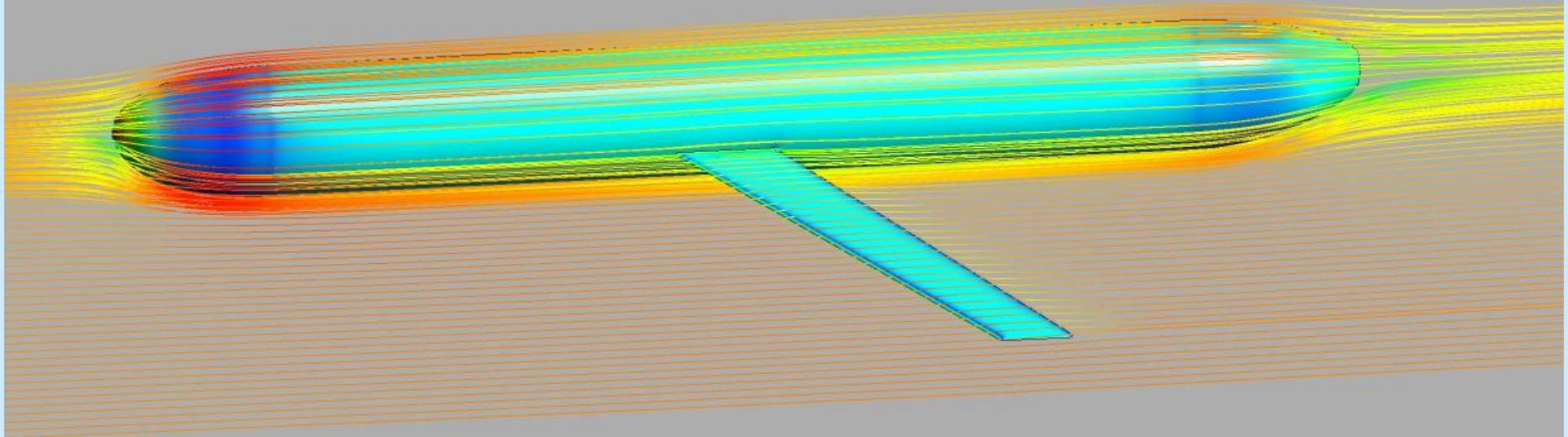
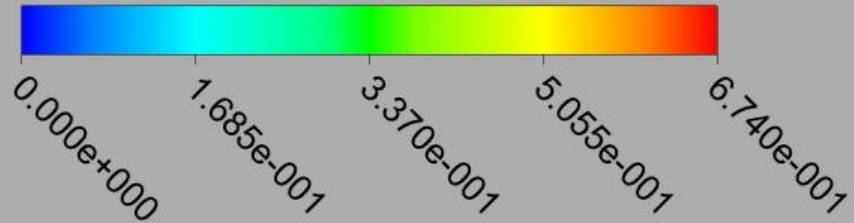
- Approaching velocity
 - 0.3 m/s and 0.5 m/s
- Turbulence model
 - SST- $k\omega$ model and transition model
- Zero angle of attack

0.3 m/s with SST-$k\omega$	0.3 m/s with transition
0.6 m/s with SST-$k\omega$	0.6 m/s with transition

Stream line

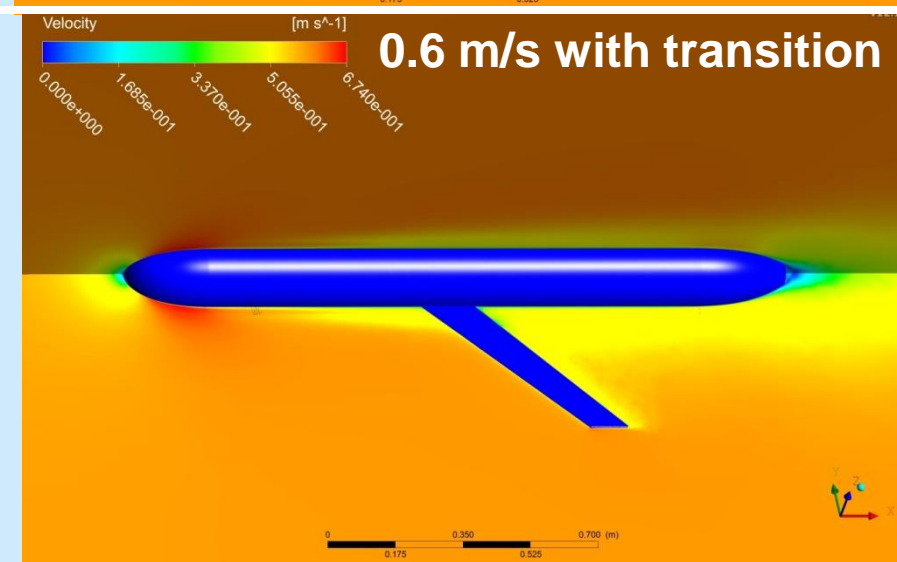
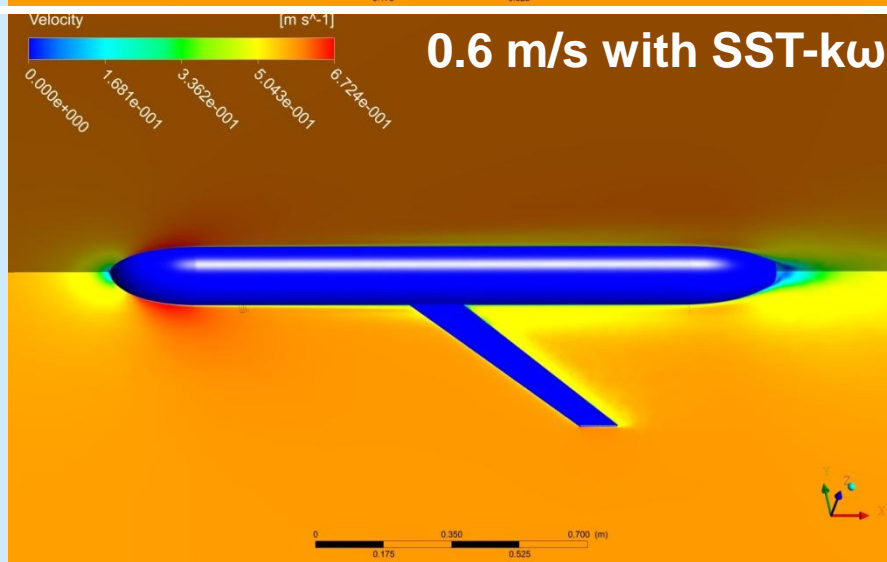
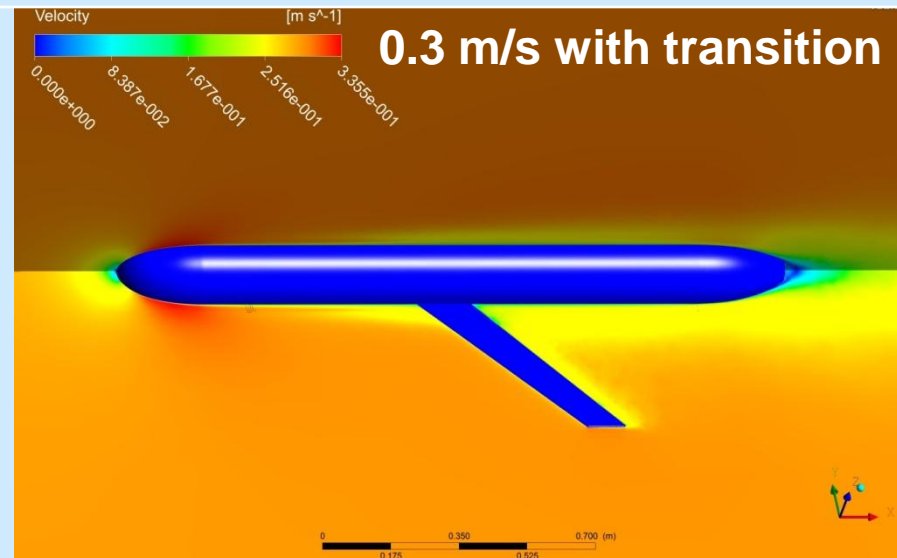
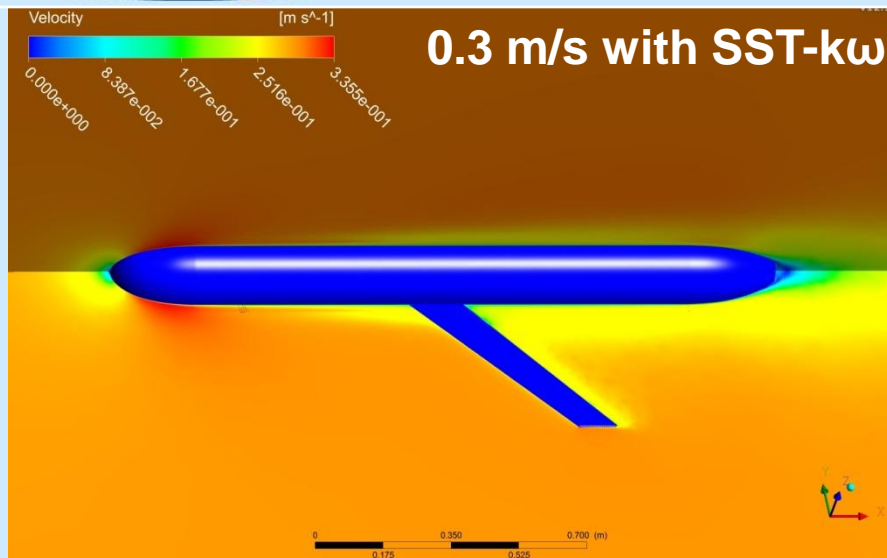
Velocity
Streamline 2

[m s⁻¹]

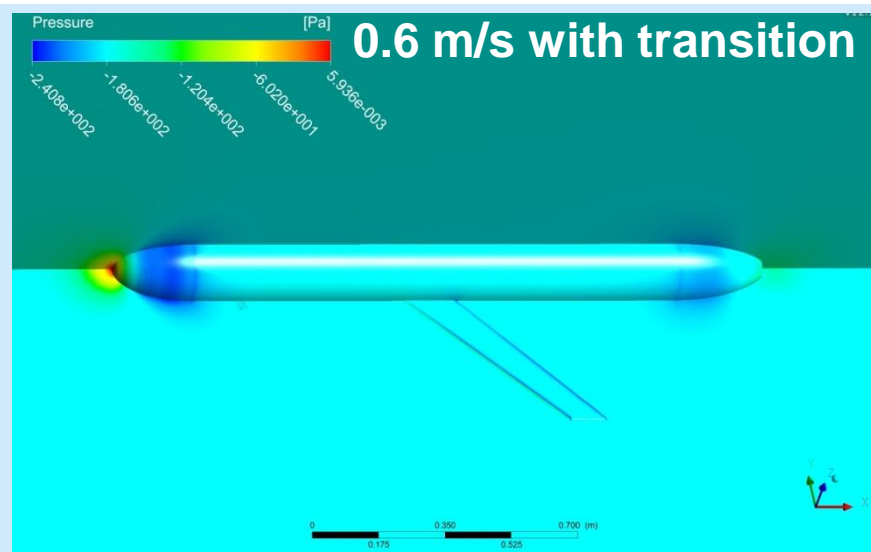
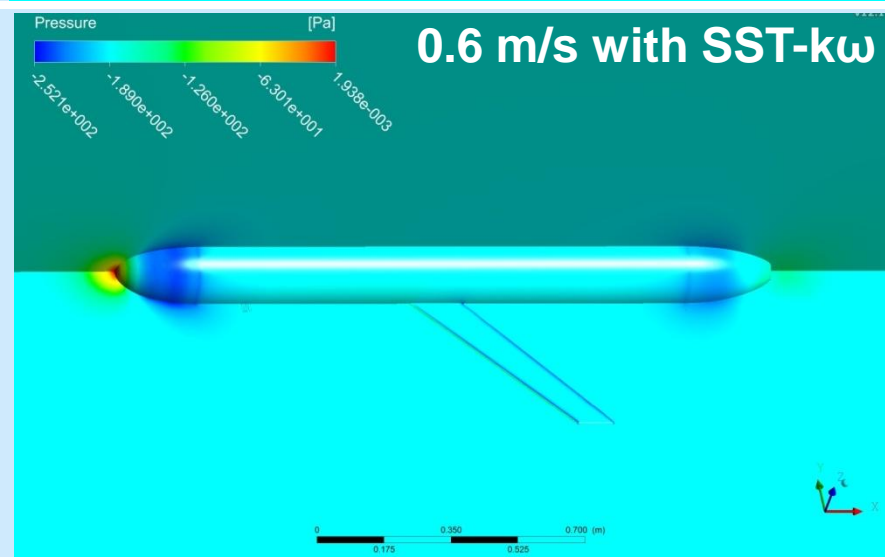
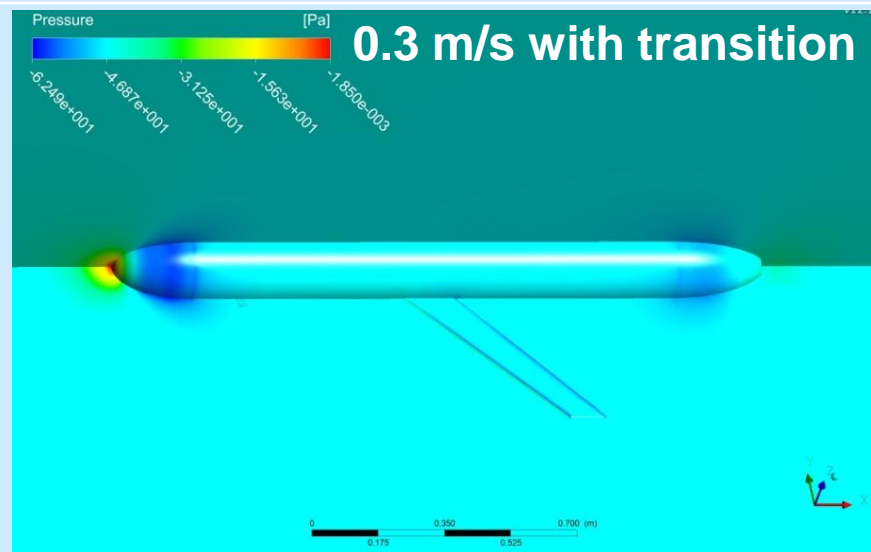
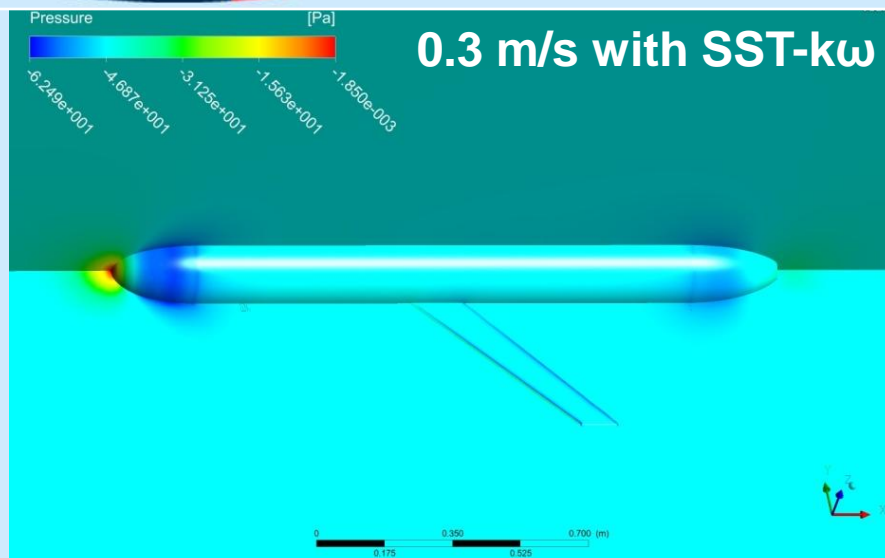


At 0.6 m/s of approaching speed with transition model

Velocity contour



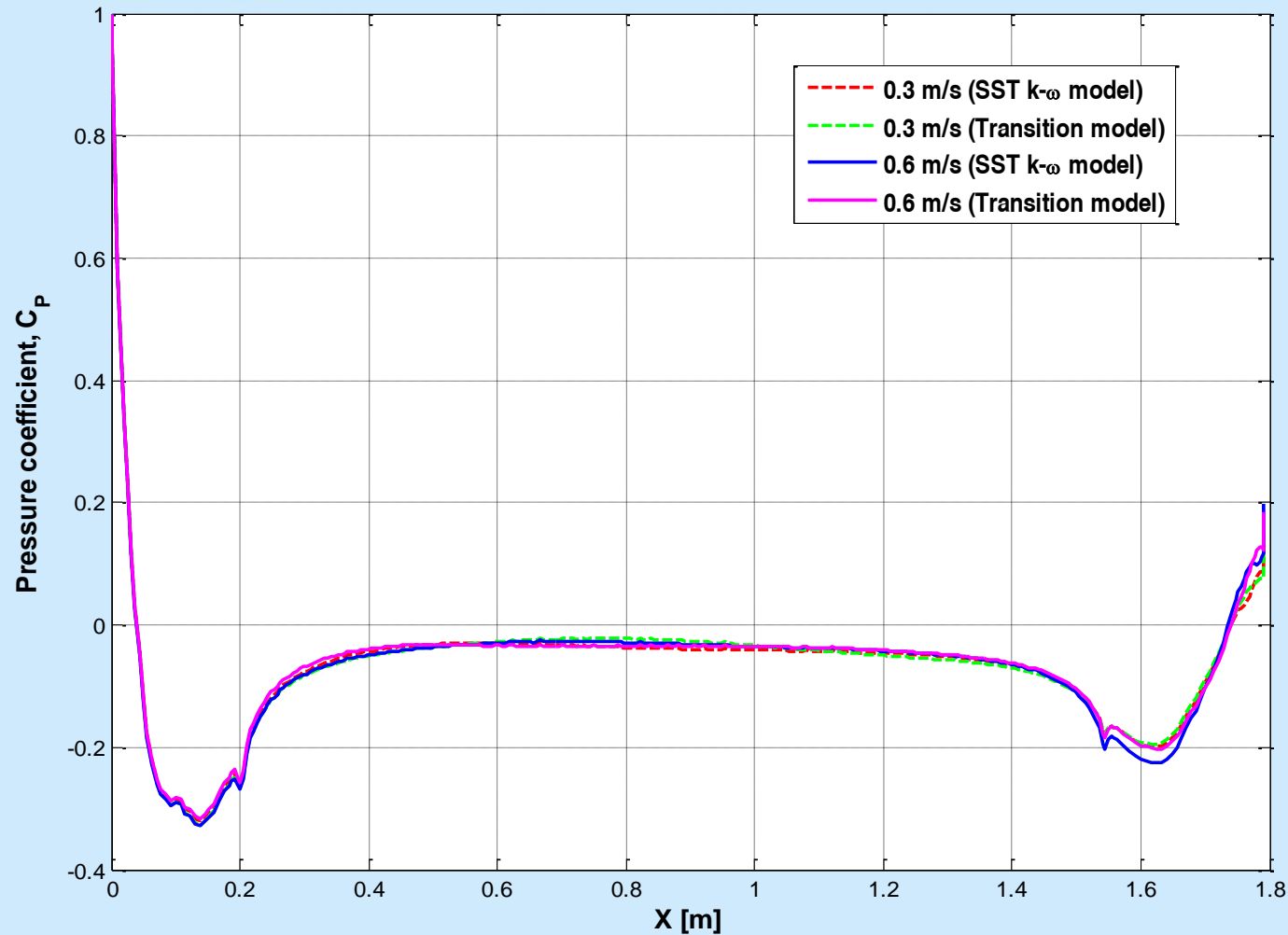
Pressure contour



Drag component

Velocity [m/s]	Drag component	SST k- ω model		Transition model	
		Force [N]	Portion [%]	Force [N]	Portion [%]
0.3	Pressure drag	0.18	37	0.18	33
	Viscous drag	0.32	63	0.35	67
	Total Drag	0.50	100	0.53	100
0.6	Pressure drag	0.68	38	0.70	39
	Viscous drag	1.12	62	1.11	61
	Total Drag	1.80	100	1.81	100

Pressure coefficient



$$C_p = \frac{P - P_\infty}{1/2 \rho V_\infty^2}$$

where,

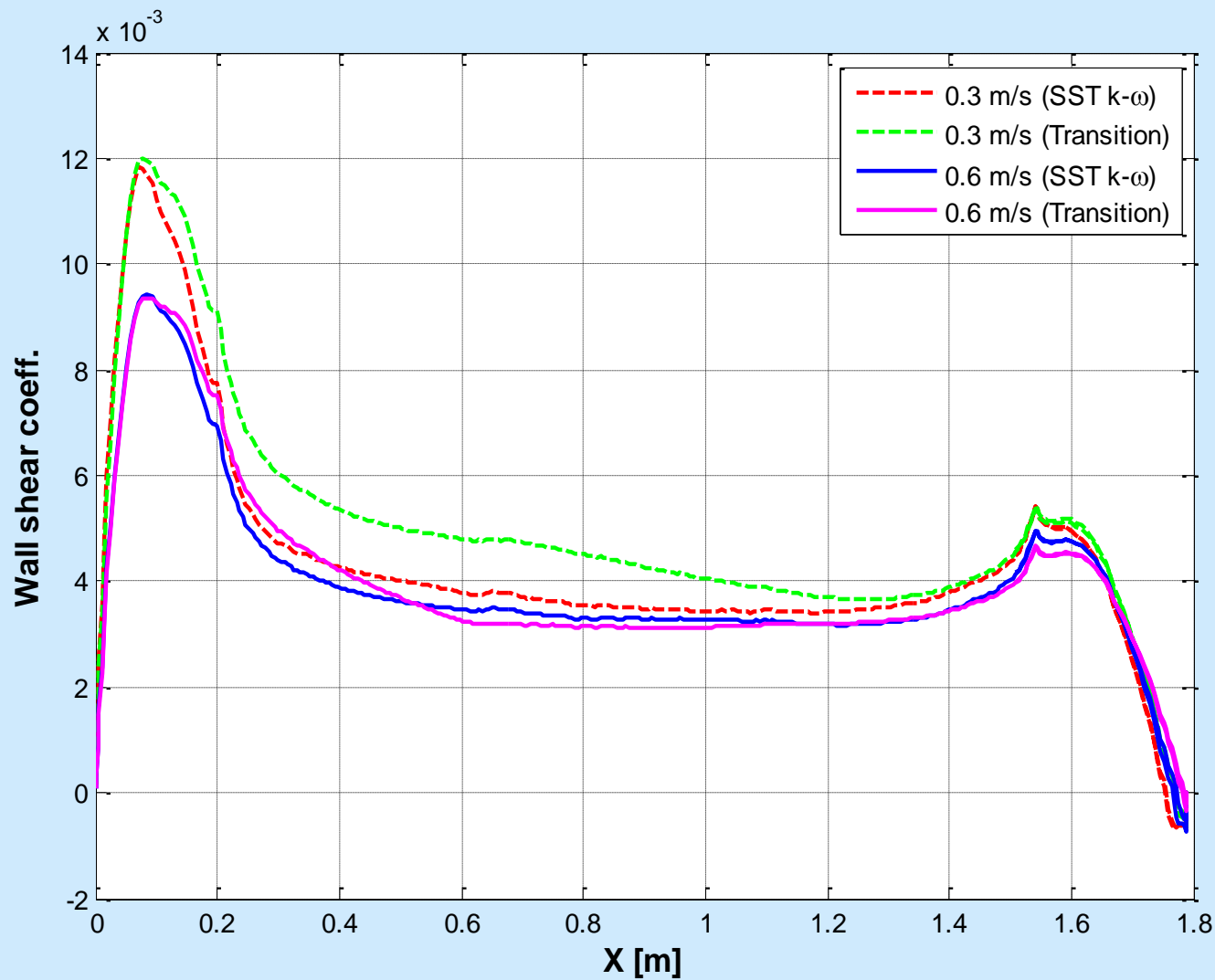
P : Pressure

P_∞ : Ambient pressure

ρ : Density

V_∞ : Ambient velocity

Shear coefficient



$$C_s = \frac{\tau_{shear}}{1/2 \rho V_\infty^2}$$

where,

τ_{shear} : Shear stress

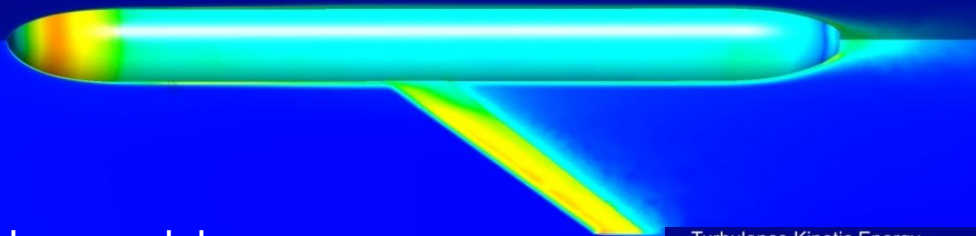
ρ : Density

V_∞ : Ambient velocity

Turbulence kinetic energy contour (0.3 m/s)

Turbulence Kinetic Energy [m² s⁻²]

9.208e-006 3.712e-004 7.332e-004 1.095e-003 1.457e-003



SST k- ω model

$$TKE = \frac{1}{2} \left(\overline{(u'_1)^2} + \overline{(u'_2)^2} + \overline{(u'_3)^2} \right)$$

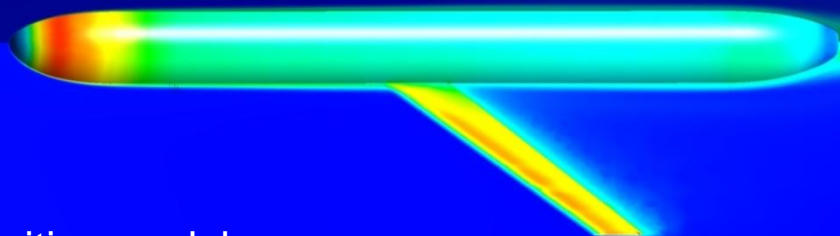
where,

u'_i : Turbulent velocity (fluctuation term)

i.e. $u_i = \overline{u_i}$ (mean value) + u'_i (fluctuation)

Turbulence Kinetic Energy [m² s⁻²]

4.978e-006 3.309e-004 6.569e-004 9.829e-004 1.309e-003

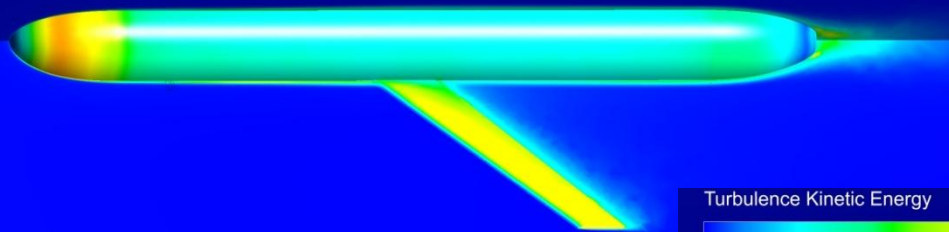


Transition model

Turbulence kinetic energy contour (0.6 m/s)

Turbulence Kinetic Energy [m² s⁻²]

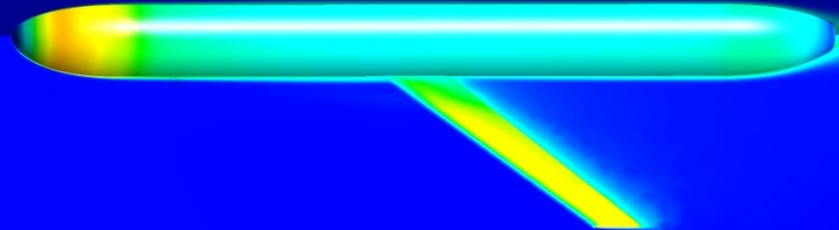
1.881e-005 1.173e-003 2.327e-003 3.481e-003 4.635e-003



SST k- ω model

Turbulence Kinetic Energy [m² s⁻²]

9.935e-006 1.132e-003 2.253e-003 3.375e-003 4.497e-003



Transition model

$$TKE = \frac{1}{2} \left(\overline{(u'_1)^2} + \overline{(u'_2)^2} + \overline{(u'_3)^2} \right)$$

where,

u'_i : Turbulent velocity (fluctuation term)

i.e. $u_i = \overline{u_i}(\text{mean value}) + u'_i(\text{fluctuation})$

Computation time

On a 2.1 GHz Pentium® Dual core CPU with 2Gb memory

Velocity (m/s)	SST k-ω model Time (sec)	Transition model Time (sec)
0.3	13,144	16,744
0.6	15,240	18,239

Validation

- Comparison with the experiment

Velocity (m/s)	CFD		Experiment* [N]
	SST k- ω model [N]	Transition model [N]	
0.3	0.50	0.53	0.50
0.6	1.80	1.81	1.75

*From B. Claus et al., JEME, 2010

Summary & future work

- Drag force is predicted by CFD method. The result is well agreed with the experimental result.
- Two turbulence model, SST- $k\omega$ and SST Transition model are examined. Both of two models give the similar result. However, at some region, the flow shows little different pattern.
- *Hydrodynamic forces will be estimated using the candidate hull shape for the hydrophone installation.*
- *More study and more validation is needed for the transition model.*



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Thanks for your attention!



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