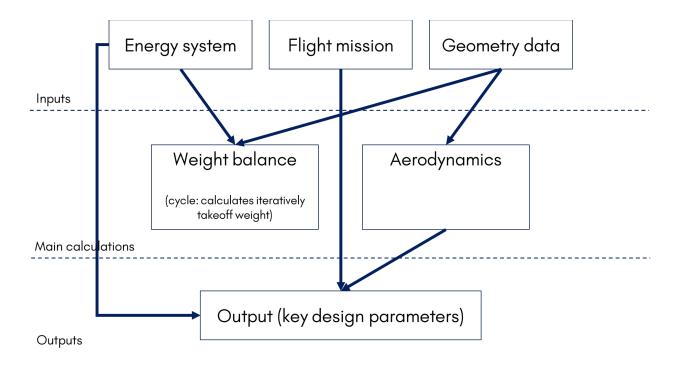


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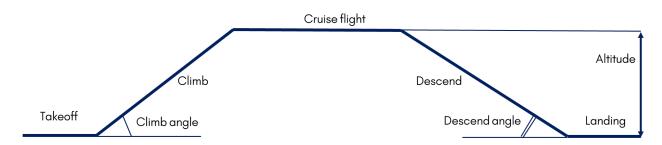
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1. MODEL STRUCTURE



Pic.1 Model structure

2. MISSION DESIGN



Pic.2 Flight plan

2.1 Takeoff

$$V_0$$
 – preliminary takeoff velocity $\left[\frac{m}{s}\right]$

$$V_{0 \ final} - final \ takeoff \ velocity \left[\frac{m}{s}\right]$$

$$V_{takeoff} = V_{0 \, final} * 0.7 - average \, takeoff \, velocity \left[\frac{m}{s}\right]$$

$$f_{friction_{to}} = 0.04 - friction coefficient$$

2.2 Climb

 θ_{climb} – climb angle [deg]

$$l_{climb} = \frac{H}{\sin\left(\theta_{climb} * \frac{\pi}{180}\right)} - climb \ diagonal \ distance[m]$$

$$d_{climb} = \frac{H}{tan\left(\theta_{climb} * \frac{\pi}{180}\right)} - climb \ horizontal \ distance[m]$$

2.3 Cruise flight

H-flight altitude [m]

 P_{hf} – Flight altitude pressure [Pa]

 ρ_{cruise} – Flight altitude air density [kg/m3]

 $V_{cruise} - Cruise speed [m/s]$

 M_{cruise} — Cruise Mach number

 $q_{cruise} = 0.5 * ro * V_{cruise}^2 - Cruise dynamic pressure [Pa]$

 $g = 9.81 - Gravitational\ acceleration\ [m/s2]$

 μ – kinematic viscosity parameter according to ISA – 76 $\left[\frac{m^2}{s}\right]$

2.4 Descend

 $\theta_{descend}$ – descend angle [deg]

$$l_{descend} = \frac{H}{sin\left(\theta_{descend} * \frac{\pi}{180}\right)} - descend \ diagonal \ distance[m]$$

$$d_{descend} = \frac{H}{tan\left(\theta_{descend} * \frac{\pi}{180}\right)} - descend \ horizontal \ distance[m]$$

2.5 Landing

$$V_{landing}$$
 – preliminary landing velocity $\left[\frac{m}{s}\right]$

$$V_{landing\ final} - final\ landing\ velocity\ [\frac{m}{s}]$$

 $f_{friction_{land}} = 0.3 - landing friction coefficient$

2.6 Load factors

 P_{cabin} – Cabin pressure (equal to pressure at 2000 m altitude) [Pa]

 P_{delta} – cabin pressure differential, [Pa]

n = 3 - Limit load factor

 $N_z = 1.5 * limit load factor (3 - 4 for normal category aircraft)$

- $ultimate\ load\ factor$

 $N_l = 1.5 * n_{landing \; gear} - ultimate \; landing \; load \; factor$

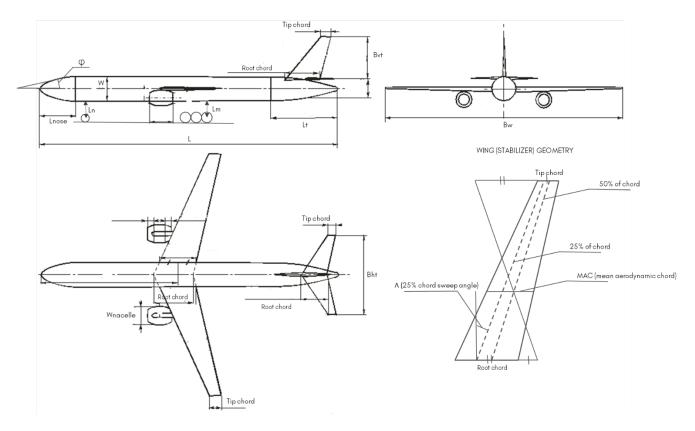
2.7 Payload

 N_p – number of personnel onboard (crew and passengers)

 $W_{payload} - Payload weight [kg]$

 P_{delta} — cabin pressure differential, [Pa]

3. GEOMETRY DATA



Pic.3 Aircraft and its geometry parameters

3.1 Fuselage (nacelle)

 $V_{pr}-volume\ of\ pressurized\ section,[m^3]$

 S_f – fuselage wetted area, $[m^2]$

 L_t – tail length, [m]

 L_{nose} – nose part length [m]

 $L-fuse lage\ structural\ length,[m]$

 $D-fuse lage\ structural\ depth,[m]$

W – total fuselage structural width, [m]

$$S_{fus} = W^2 * \frac{pi}{4} - crossectional area [m2]$$

$$r_{relative} = \frac{nose\ radius}{fuse lage\ radius} - nose\ relative\ radius$$

 φ – nose semipart angle [rad]

$$D_{fus} = sqrt\left(4 * \frac{S_{fus}}{pi}\right) - fuselage equivalent diametr[m]$$

$$AR_{fus} = \frac{L}{W} - fuselage \ aspect \ ratio$$

$$AR_{nose} = \frac{L_{nose}}{W} - nose \ part \ aspect \ ratio$$

$$AR_{aft} = \frac{L_t}{W} - rear \ part \ aspect \ ratio$$

3.2 Wing (or stabilizer or fin)

 $k_{A_{wind}}$

- airfoil type coefficient (supercritical (0.97) or conventional (0.88))

$$B_w$$
 – wing span, $[m]$

$$TR_w = \frac{tip\ chord}{root\ chord} - wing\ taper\ ratio$$

$$AR_w = \frac{B_w^2}{S_w} - wing \ aspect \ ratio$$

$$t/c - thickness - to - chord - ratio$$

 $S_w - trapezoidal wing area, [m^2]$

 $\Lambda-wing$ sweep at 25% MAC

$$mac = \frac{S_w}{B_w} - Mean \ aerodynamic \ chord \ [m]$$

 $S_{wf} = W * mac - wing area intersected with fuselage [m²]$

 $\frac{H_t}{H_t} = 0$ if tail is conventional, 1 if tail is T – shaped

 $\overline{mac_f} \approx 0.2 - flap \ chord \ related \ to \ wing MAC$

 $\overline{b_f} = [0 ... 1] - flap span related to winspan$

 $S_0 = [0 ... S_w] - propellerblown wing area, [m^2]$

 $TV_{ht} \approx 1.2 - horizontal stabilizer tail volume$

 $TV_{vt} \approx 0.1 - vertical stabilizer tail volume$

 LA_{ht} $= [0.4 * L \dots 0.6L]$

- distance between horizontal stabilizer and center of gravity,[m]

= [0.4 * L ... 0.6L]

distance between horizontal stabilizer and center of gravity, [m]

$$S_{ht} = \frac{TV_{ht} * mac_w * S_w}{LA_{ht}} - horizontal \ stabilizer \ area, [m^2]$$

$$S_{ht} = \frac{TV_{vt} * mac_w * S_w}{LA_{vt}} - verticalal stabilizer area, [m^2]$$

3.3 Landing gear

 W_l – landing design gross weight, [kg]

 L_m – extended lentgh of main landing gear, [m]

 L_n – extended lentgh of nose landing gear, [m]

4. ENERGY SYSTEM

Conventional propulsion (piston or turboprop engine)

$$PW \approx 150 - 350 - power - to - weight ratio, \left[\frac{Wt}{kg}\right]$$

$$SFC_{eng} = 0.408 - specific fuel consumption, \left[\frac{kg}{kW * h} \right]$$

 SFC_{ground}

 $= 2.2 * SFC_{eng}$

– specific fuel consupmtion before takeoff and after landing, $[\frac{kg}{kW*h}]$

 N_{en} – number of engines

 η_{eng} \sim 0.85 - electric engine efficiency

 N_t – number of fuel tanks

 W_{fw} – weight of fuel in wing, [kg]

 $W_{fuel} - fuel\ weight, [kg]$

 V_t – total fuel volume, $[m^3]$

 V_i – intergral tanks volume, $[m^3]$

 $P_{en \ max} = PW * W_{total} - engine \ takeoff \ power \ [kW]$

 $SW_{eng} \approx 0.2 - electric engine weight - to - power ratio, <math>\left[\frac{kg}{kW}\right]$

 $p_{elec} \approx 1.05 - electric$ systems power penalty coefficient

 $t_{ground} = 0.25 [h] - preparation + start + taxi in + taxi out time$

 $E_{ground} = 0.06 * P_{en \, max} * t_{ground} - energy \, required \, for \, preparation$ + $start + taxi \, in + taxi \, out, [Wh]$

5. PROPELLER

$$D_{prop} = \frac{B_w - W}{N_{en}} - \Delta_{prop} * N_{en} - propeller diameter$$

$$A_{prop} = \frac{\pi * D_{prop}^2}{4} - propeller disk area, [m^2]$$

 Δ_{prop} – distance between propellers

$$F_{prop} = \frac{4 * P_{en max}}{\pi * D_{prop}^2} - propeller loading, [\frac{Wt}{m^2}]$$

 $Thrust_{max} = 3.21 * P_{en max} * F_{prop}^{0.33} - maximum engine thrust, [N]$

$$B = \frac{2 * Thrust_{max}}{\rho * V_0^2 * A_{prop}} - loading factor first iteration$$

 η_{prop} – propeller efficiency (~0.8 for cruise flight and ~0.6 – 0.7 for takeoff and landing)

6. WEIGHT BALANCE

 W_{dg} – flight design gross weight (preliminary takeoff weight), [kg]

6.1 Propulsion system weight calculation

 $W_{installed\ engine\ (total)} = 2.421*W_{en}^{0.922}*N_{en} - installed\ engine\ weight, [kg]$

$$W_{en} = SW_{eng} * P_{en max} - engine weight, [kg]$$

6.2 Structures weight calculation

$$\begin{split} W_{structure} &= W_{fuselage} + W_{wing} + W_{ht} + W_{main\,landing\,gear} \\ &+ W_{nose\,landing\,gear} - structure\,weight, [kg] \end{split}$$

6.2.1 Fuselage weight calculation

$$W_{fuselage} = 0.23 * S_f^{1.086} * (N_z * W_{dg})^{0.177} * L_t^{-0.051} * (\frac{L}{D})^{-0.072} * q^{0.241} + W_{press} - fuselage weight, [kg]$$

$$W_{press} = 1.2926 * (V_{pr} * P_{delta})^{0.271}$$

$$- weight penalty due to pressurization, [kg]$$

6.2.2 Wing weight calculation

$$\begin{split} W_{wing} &= 0.13817 * S_w^{0.758} * W_{fw}^{0.0035} * \left(\frac{AR_w}{cos^2\Lambda}\right)^{0.6} * q^{0.006} * TR_w^{0.04} \\ &* \left(\frac{100t}{c}\right)^{-0.3} * \left(N_z * W_{dg}\right)^{0.49} - wing\ weight, [kg] \end{split}$$

 W_{fw} – weight of fuel in wing, [kg]

6.2.3 Empennage weight calculation

$$\begin{split} W_{ht} &= 0.01917 * \left(N_z * W_{dg}\right)^{0.414} * q^{0.168} * S_{ht}^{0.896} * \left(\frac{\frac{100t}{c}}{cos\Lambda_{ht}}\right)^{-0.12} \\ &* \left(\frac{AR_{ht}}{cos^2\Lambda_{ht}}\right)^{0.043} * TR_{ht}^{-0.02} - horizontal \ stabilizer \ weight \end{split}$$

$$\begin{split} W_{vt} &= 0.12 * \left(1 + 0.02 * \frac{H_t}{H_v}\right) * \left(N_z * W_{dg}\right)^{0.376} * q^{0.122} * S_{vt}^{0.873} \\ &* \left(\frac{100t}{c}\right)^{-0.49} * \left(\frac{AR_{vt}}{cos^2 \Lambda_{vt}}\right)^{0.357} * TR_{vt}^{0.039} \end{split}$$

 $-\ vertical\ stabilizer\ weight$

6.2.4 Landing gear weight calculation

W_{main landing gear}

$$= 0.12855 * (N_l * W_l)^{0.768} * (L_m)^{0.409}$$

- main landing gear weight, [kg]

 $W_{nose\ landing\ gear}$

$$= 0.242 * (N_l * W_l)^{0.566} * (L_n)^{0.845}$$

- nose landing gear weight, [kg]

6.3 Equipment weight calculation

$$\begin{split} W_{fuel\,system} &= 64.7374 * V_t^{0.726} * \left(\frac{1}{1 + V_i/V_t}\right)^{0.363} * N_t^{0.242} * N_{en}^{0.157} \\ &- fuel\,system\,weight, [kg] \end{split}$$

 $W_{flight\ controls}$

$$= 0.43613 * L^{1.536} * B_w^{0.371} * (N_z * W_{dg} * 10^{-4})^{0.8}$$

- flight controls weight, [kg]

$$W_{hydraulics} = 1.1734*K_h*W^{0.8}*M^{0.5} - hydraulics\ weight, [kg]$$

 $K_h - 0.05$ (low subsonic), 0.11 (medium subsonic), 0.12 (high subsonic) - hydraulics weight coefficient

$$W_{electrical} = 8.533 * (W_{fuel \, system} + W_{avionics})^{0.51} - electrical \, system \, weight, [kg]$$

$$W_{avionics} = 2*W_{uav}^{0.933} - avionics\ weight, [kg]$$

 W_{uav} – uninstalled avionics weight (350 – 650 kg), [kg]

$$W_{air\ conditioning\ and\ anti-ice} = 0.2074*W_{dg}^{0.52}*N_p^{0.68}*W_{avionics}^{0.17}*M^{0.08}$$

$$W_{furnishings} = 0.0582 * W_{dg} - 29.48 - furnishings weight, [kg]$$

$$W_{equipment} = W_{fuel\ system} + W_{flight\ controls} + W_{hydraulics} + W_{electrical} + W_{avionics} + W_{uav} + W_{air\ conditioning\ and\ anti-ice} + W_{furnishings} - equipment\ weight, [kg]$$

 $W_{total} = W_{fuel} + W_{structure} + W_{equipment} - final total takeoff weight, [kg]$

7. AERODYNAMICS

7.1 Polar coefficient and lift coefficient

$$e = \frac{1}{1 + 0.025 * AR_w} - Oswald \ coefficient$$

$$A = \frac{1}{pi * AR_w * e} - polar coefficient$$

$$C_{Lcruise} = 0.71 * sqrt(pi * AR_w * C_{D0}) - optimal \ lift \ coefficient$$

7.2 Drag coefficient

$$C_D = C_{D0} + A * C_L^2 - drag \ coeff cient$$

 $K_{int} \sim 0.2 - 0.25 - interference coefficient (depends on position of wing)$ $v_{\mu} = -0.04 * M^2 - 0.03 * M + 1 - flow compressibility coefficient$

7.2.1 Fuselage (nacelle) drag

$$Re_{fus} = V_{cruise} * \frac{L}{\mu} - Reynolds number$$

$$C_{f_{fus}} = 0.0454 * Re_{fus}^{-0.189} - flat \ plate \ friction \ coefficient$$

$$v_{lambda_{fus}} = 1.7564 * AR_{fus}^{-0.225} - fuselage shape coefficient$$

$$\begin{aligned} \textit{C}_{D0_{fus_{friction}}} = \ 2 * \textit{C}_{f_{fus}} * \textit{v}_{\mu} * \textit{v}_{lambda_{fus}} * \frac{\textit{S}_{f}}{2 * \textit{S}_{fus}} \\ - \textit{friction drag coefficient} \end{aligned}$$

$$C_{D0_{par}} = (1.0699 * M^3 - 2.2393 * M^2 + 1.6016 * M - 0.3859) - 0.01 * (AR_{nose} - 2) - parabolic nose drag coefficient$$

$$delta_{C_{D_{dump}}} = 1.6667 * M^3 - 2.1786 * M^2 + 0.8512 * M - 0.0386 - dumping coefficient$$

$$\begin{split} \mathcal{C}_{D0_{nose}} &= \ \mathcal{C}_{D0_{par}} \\ &* \left(1 - r_{relative}^2 * \left(cos(\varphi) \right)^2 \right. \\ &* \left(3.1 - 1.4 * r_{relative} * cos(\varphi) - 0.7 * r_{relative}^2 * \left(cos(\varphi) \right)^2 \right) \right) \\ &+ delta_{\mathcal{C}_{D_{dumn}}} * \ r_{relative}^2 - nose \ drag \ coefficient \end{split}$$

$$C_{D0_{aft}} = (0.5455 * M^2 - 0.6764 * M + 0.2698) - 0.013 * (AR_{aft} - 2) - aft \ part \ drag \ coefficient$$

$$C_{D0_{fus_{pressure}}} = C_{D0_{nose}} + C_{D0_{aft}} - pressure drag coefficient$$

$$C_{D0_{fuselage}} = C_{D0_{fus_{friction}}} + C_{D0_{fus_{pressure}}} - fuselage drag coefficient$$

7.2.2 Wing (or stabilizer or fin) drag

$$K1 = 2 - \frac{S_{with_{eng}}}{S_w} - wing - nacelles interference coefficient$$

$$v_{c_{wing}} = 1 + 1.5 * t/c - airfoil thickness coefficient$$

$$Re_{wing} = V_{cruise} * \frac{mac}{\mu} - Reynolds number$$

$$C_{f_{wing}} = 0.0454 * Re_{wing}$$
. $^{-0.189}$ – flat plate friction coefficient

$$C_{D0_{form_{wing}}} = 0.925 * K1.* C_{f_{wing}} * \nu_{\mu} * \nu_{c_{wing}} - form \ drag \ coefficient$$

$$M_{DD_{wing}} = \frac{k_{A_{wing}} - W_{total} * \frac{\frac{g}{q_{cruise} * S_w}}{10 * (cos(\Lambda))^2} - \frac{t/c}{cos(\Lambda)}}{cos(\Lambda)}$$

- drag divergence Mach number

$$M_{cr_{wing}} = M_{DD_{wing}} - 0.108 - critical Mach number$$

$$C_{D0_{wave_{wing}}} = 20 * (M - M_{cr_{wing}}).^4 - wave drag coefficient$$

$$C_{D0_{prime_{wing}}} = C_{D0_{form_{wing}}} + C_{D0_{wave_{wing}}} - clean wing drag coefficient$$

$$C_{D0_{wing}} = C_{D0_{prime_{wing}}} + K_{int} \cdot * C_{D0_{form_{wing}}} \cdot * \frac{S_{wf}}{S_w} - wing \ drag \ coefficient$$

7.2.3 Zero drag coefficient

$$\begin{split} C_{D0} = \ 1 * \left(C_{D0_{fuselage}} . * \frac{S_{fus}}{S_w} + \ C_{D0_{wing}} + \ C_{D0_{ht1}} * \frac{S_{ht1}}{S_w} + \ C_{D0_{ht2}} * \frac{S_{ht2}}{S_w} + \ C_{D0_{vt}} \\ * \frac{S_{vt}}{S_w} + \ n_{eng} * C_{D0_{nacelle}} * \frac{S_{nac}}{S_w} \right) - zero \ drag \ coefficient \end{split}$$

7.3 Lift coefficient

 $\alpha_{takeoff} = [0 ... 3] - takeoff angle of attack, [deg]$

 $\alpha_{landing} = [3 ... 8] - landing angle of attack, [deg]$

$$C_L^{\alpha} = 2 * \pi^2 * \frac{AR_w * cos\Lambda_w}{180 * (2 + AR_w)} - lift coefficient derivative, [\frac{1}{deg}]$$

 $C_{L \max airfoil} = [1.6 ... 1.8] - airfoil maximum lift coefficient$

$$C_{L \max 0} = 0.5 * k_{\eta} * C_{L \max airfoil} * (1 + cos\Lambda_{w})$$

aircraft default maximum lift coefficient

$$k_{\eta} = -0.2135 * TR_w^2 + 0.2398 * TR_w + 0.8737 - taper - ratio coefficient$$

$$\Delta C_{L\,flap} = k_{\delta} * \overline{mac_f} * \overline{b_f} * \frac{mac}{S_w} * C_L^{\alpha} * 57.3 * cos \Lambda_w$$

additional flap lift coefficient

 k_{δ} – flap coefficient (see table below)

Flap type	k_{δ}
Conventional (takeoff)	<mark>0.34</mark>
Conventional (landing)	<mark>0.52</mark>
Fowler flap (takeoff)	<mark>0.7</mark>
Fowler (landing)	<mark>1.33</mark>
Double-slotted Fowler flap (takeoff)	<mark>0.79</mark>
Double-slotted Fowler flap (landing)	<mark>1.49</mark>

C_{L max without prop}

 $= C_{L \max 0} + \Delta C_{L flap}$

- maximum aircraft lift coefficient excluding propeller effect

 $C_{L max final} = C_{L max without prop} - aircraft lift coefficient first iteration$

 $V_{\max takeoff}$

 $= V_0 - maximum takeoff lift coefficient velocity first iteration, <math>\left[\frac{m}{s}\right]$

 $V_{\max landing}$

 $=V_{landing}$

- maximum landing lift coefficient velocity first iteration, $\left[\frac{m}{s}\right]$

 $B_{takeoff} = B$ - takeoff loading factor first iteration

 $B_{landing}$ – landing loading factor first iteration

Takeoff lift coefficient loop

$$Lift_{\max 0} = 0.68 * C_{L \max final} * \frac{(\rho * V_{max})^2}{2} * S_w -$$

$$maximum \ takeoff \ lift \ force, [N]$$

$$Drag_{max\ 0} = (C_{D0} + A * C_{L\ max\ final}^{2}) * \frac{(\rho * V_{max\ takeoff})^{2}}{2} * S_{w}$$
$$- maximum\ takeoff\ drag\ force, [N]$$

$$\begin{split} \theta_{eff} &= arctg(\frac{Lift_{\text{max}\,0}}{Thrust_{max} - Drag_{max\,0}}) \\ &- effective \ flow \ deflection \ angle, [deg] \end{split}$$

$$C_{\mu} = B * \frac{A_{prop}}{S_0} - propeller coefficient$$

 ΔC_L^{α}

$$= \pi * \frac{1.152 * \sqrt{C_{\mu}} + 1.106 * C_{\mu} + 0.051 * C_{\mu} * \sqrt{C_{\mu}}}{180}$$

– derivative of a lift coefficient increment by the angle of attack, $\left[\frac{1}{deg}\right]$

 ΔC_L^{θ}

$$= \pi * \frac{-0.19356 * C_{\mu}^{2} + 2.87645 * C_{\mu} + 6.2 * \overline{b_{f}}}{180}$$

– derivative of a lift coefficient increment by the angle of a flow deflection, $[rac{1}{deg}]$

$$\Delta C_{L \, prop} = \left(\Delta C_{L}^{\theta} * sin\theta_{eff} + \Delta C_{L}^{\alpha} * \alpha_{takeoff} - N_{en} * B * \frac{A_{prop}}{S_{0}} * sin\theta_{eff}\right) * \frac{S_{0}}{S_{w}}$$

$$* \left(1 + \frac{t}{c}\right) * \frac{C_{L}^{\alpha}}{2 * \pi} + N_{en} * B * \frac{A_{prop}}{S_{w}} * sin\theta_{eff}$$

$$- additional \, lift \, coefficient \, caused \, py \, propeller$$

C_{L max final takeoff}

 $= C_{L max without prop} + \Delta C_{L prop}$

– final aircraft takeoff maximum lift coefficient

$$V_{\max takeoff} = \sqrt{\frac{2 * W_{total}}{0.68 * C_{L \max final \ takeoff} * \rho * S_{w}}}$$

final takeoff maximum lift coefficient velocity

$$B_{takeoff} = \frac{2*Thrust_{max}}{\rho*V_{\max takeoff}^2*A_{prop}} - final \ takeoff \ loading \ factor$$

Landing lift coefficient loop

$$Lift_{\max landing} = 0.68 * C_{L \max final} * \frac{(\rho * V_{\max landing})^{2}}{2} * S_{w} - \max landing lift force, [N]$$

Drag_{max landing}

$$= (C_{D0} + A * C_{L \max final}^{2}) * \frac{(\rho * V_{\max landing})^{2}}{2} * S_{w}$$

$$- \max landing drag force, [N]$$

$$heta_{eff} = arctg(\frac{Lift_{max\,landing}}{Thrust_{max} - Drag_{max\,landing}})$$

$$- effective flow deflection angle, [deg]$$

$$C_{\mu} = B * \frac{A_{prop}}{S_0} - propeller coefficient$$

 ΔC_L^{α}

$$= \pi * \frac{1.152 * \sqrt{C_{\mu}} + 1.106 * C_{\mu} + 0.051 * C_{\mu} * \sqrt{C_{\mu}}}{180}$$

- derivative of a lift coefficient increment by the angle of attack, [$rac{1}{deg}$

 ΔC_L^{θ}

$$= \pi * \frac{-0.19356 * C_{\mu}^{2} + 2.87645 * C_{\mu} + 6.2 * \overline{b_{f}}}{180}$$

– derivative of a lift coefficient increment by the angle of a flow deflection, $[\frac{1}{deg}]$

$$\Delta C_{L \, prop} = \left(\Delta C_{L}^{\theta} * sin\theta_{eff} + \Delta C_{L}^{\alpha} * \alpha_{takeoff} - N_{en} * B * \frac{A_{prop}}{S_{0}} * sin\theta_{eff} \right) * \frac{S_{0}}{S_{w}}$$

$$* \left(1 + \frac{t}{c} \right) * \frac{C_{L}^{\alpha}}{2 * \pi} + N_{en} * B * \frac{A_{prop}}{S_{w}} * sin\theta_{eff}$$

$$- additional \, lift \, coefficient \, caused \, py \, propeller$$

C_{L max final landing}

 $= C_{L \max without prop} + \Delta C_{L prop}$

final aircraft landing maximum lift coefficient

$$V_{\text{max landing}} = \sqrt{\frac{2 * W_{total}}{0.68 * C_{L max final} * \rho * S_{w}}}$$

- final landing maximum lift coefficient velocity, $\left[\frac{m}{s}\right]$

$$B_{landing} = \frac{2*Thrust_{max}}{\rho * V_{\max landing}^2 * A_{prop}} - final \ landing \ loading \ factor$$

8. OUTPUTS

8.1 Takeoff

$$F_{takeoff} = f_{friction_{to}}$$

$$* (W_{total} * g - C_{L max final takeoff} * V_{takeoff}^{2} * 0.5 * \rho * S_{w})$$

$$- Friction force, [N]$$

$$a_{takeoff} = g * \frac{\frac{Thrust_{prop} - Drag_{max\ 0} - F_{takeoff}}{W_{total}}}{10} - Acceleration\ [m/s2]$$

$$L_{takeoff} = V_{takeoff}^2 * \frac{0.5}{a_{takeoff}} - Takeoff \ distance \ [m]$$

$$W_{fuel_{takeoff}} = SFC_{eng} * 0.001 * 0.000277 * Thrust_{prop} * \frac{L_{takeoff}}{\eta_{eng} * \eta_{prop}} * p_{elec}$$

- Takeoff consumed fuel [kg]

8.2 Landing

 $Cd_{landing} = C_{D0} + A * C_{L max final landing}^2 - Landing drag coefficient$

$$a_{landing} = g * \left(2 * \frac{f_{friction_{land}}}{3} + \frac{1}{3} * \frac{Cd_{landing}}{C_{L max final landing}}\right)$$

- Acceleration, [m/s2]

$$L_{landing} = V_{\max landing}^2 * \frac{0.5}{a_{landing}} - Landing distance, [m]$$

$$W_{fuel_{landing}} = SFC_{eng} * 0.001 * 0.000277 * 0.06 * Thrust_{prop} * \frac{L_{landing}}{\eta_{eng} * \eta_{prop}}$$

$$*p_{elec}$$
 – Landing consumed fuel, [kg]

8.3 Climb

$$W_{fuel_{climb}} = W_{total}$$

$$-\exp\left(log(W_{total}) - SFC_{eng}*0.001*\frac{0.000277}{\eta_{eng}*\eta_{prop}}*g*p_{elec}\right)$$

$$*\left(\frac{cos(phi_{climb})}{15} + sin(phi_{climb})\right) * l_{climb}\right)$$

Climb consumed fuel weight [kg]

8.4 Descend

$$\begin{split} W_{fuel_{descend}} &= W_{total} \\ &- exp \left(log(W_{total}) - SFC_{eng} * 0.001 * \frac{0.000277}{\eta_{eng} * \eta_{prop}} * p_{elec} * g \right) \\ &* \left(\frac{cos(phi_{descend})}{15} - sin(phi_{descend}) \right) * l_{descend} \right) \\ &- Descend \ consumed \ fuel \ weight \ [kg] \end{split}$$

8.5 Cruise flight

$$L_{D_{cruise}} = g * (W_{total} - m_{fuel_{cruise}}) * q_{cruise}$$

$$* \frac{S_{w}}{C_{D0} * q_{cruise}^{2} * S_{w}^{2} + A * g^{2} * (W_{total} - m_{fuel_{cruise}}).^{2}}$$

$$- Cruise \ lift - to - drag \ ratio$$

$$m_{fuel \ cruise} = W_{fuel} - W_{fuel_{takeoff}} - W_{fuel_{landing}} - W_{fuel_{climb}} - W_{fuel_{descend}} - \frac{SFC_{ground}*0.001}{E_{ground}} - cruise \ fuel \ mass, [kg]$$

$$fL_{cruise} = \eta_{eng} * \eta_{prop} * p_{elec} * L/D_{cruise}./(SFC_{eng} * 0.001 * 0.000277$$

$$* (W_{total} - m_{fuel \ cruise}) * g)$$

$$L_{cruise} = \int_{0}^{m_{fuel \ cruise}} fL_{cruise} * dm_{fuel_{cruise}} - Cruise \ flight \ distance$$

$$Flight_{distance} = L_{cruise} + d_{climb} + d_{descend} - Total \ flight \ distance$$

9. EXAMPLE

Reference case - Piaggio Avanti P.180 aircraft



Pic.4 Piaggio P.180 Avanti

Parameter	P.180	Math.model	Error
Takeoff weight [kg]	5489	5615	2.3%
Flight distance [km]	2592	2321	10.45%
Takeoff distance [m]	972	1066	9.7%
Landing distance [m]	1000	979	2.1%