# Entrained flow reactor (EFR)

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## 1 Introduction

This report provides an overview of the Entrained Flow Reactor (EFR) at NREL and associated computational modeling tasks. The reactor operates at fast pyrolysis conditions to thermochemically convert biomass into gaseous products.

The EFR is part of the Thermochemical Process Development Unit (TCPDU) at NREL which was originally designed for biomass gasification where the EFR was used as a thermal cracker. An overview of the TCPDU system is shown in Figure 1.

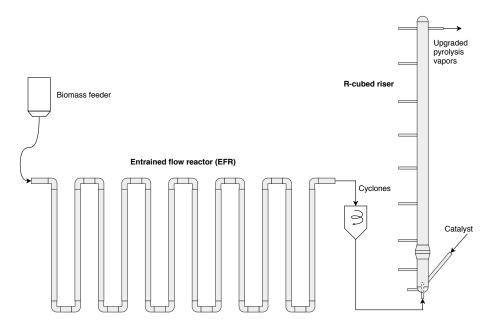


Figure 1: Overview of the main components of the NREL TCPDU system. Fast pyrolysis of biomass occurs in the entrained flow reactor. Catalytic vapor phase upgrading occurs in the R-cubed riser reactor.

## 2 Experimental setup

This section provides geometric dimensions and typical operating conditions for the entrained flow reactor. Characteristics for the Blend3 and forest residue feedstocks are also discussed.

#### 2.1 Entrained flow reactor

Fast pyrolysis in the TCPDU system occurs in the entrained flow reactor (EFR) which is comprised of a series of horizontal and vertical pipes connected with 90 degree elbows (see Figure 2). The EFR is essentially a pneumatic conveyor where biomass particles flow through a long pipe with several bends. Dimensions and material information about the EFR are provided in Figure 3 below. Operating conditions such as temperatures, pressures, and flow rates for the EFR are shown in Figure 4. Nitrogen gas at 500°C is generally used as the conveying medium for the solids.

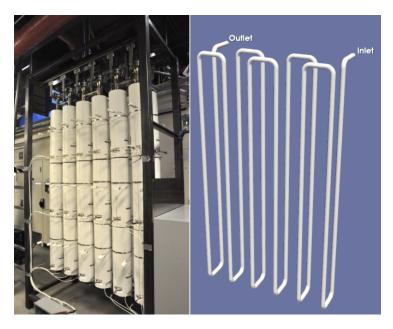


Figure 2: Left - picture of the EFR assembly with heat jackets, insulation, and thermocouples. Right - CAD representation of the EFR pipe assembly used for MFiX simulations.

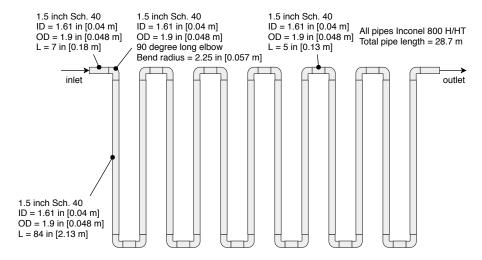


Figure 3: Geometry of the entrained flow reactor at NREL.

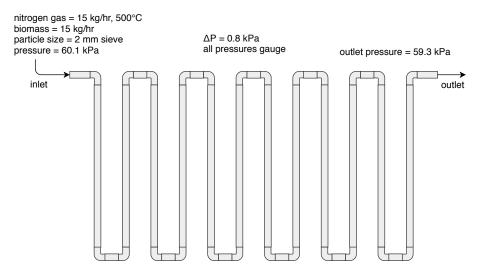


Figure 4: Typical operating conditions for the entrained flow reactor.

#### 2.2 Blend3 feedstock

General information about the Blend3 feedstock used in the entrained flow reactor is provided in Table 1. There is currently no information regarding identification of the feedstock or who performed the feedstock measurements and data preparation. Proximate and ultimate analysis data for the feedstock are presented in Tables 2 and 3. Only one set of analysis data is available therefore the uncertainty in the values is unknown.

Table 1: General information for the Blend3 feedstock.

Item	Description
Name	Blend3
ID	?
Contact	?

Table 2: Blend3 proximate analysis mass percent, as-received basis. Source [3].

Proximate	%ar	%ar	%ar
FC	16.92	?	?
VM	76.40	?	?
ash	0.64	?	?
moisture	6.04	?	?

Table 3: Blend3 ultimate analysis mass percent, as-received basis. Source [3].

Element	% ar	% ar	% ar
С	49.52	?	?
H	5.28	?	?
O	38.35	?	?
N	0.15	?	?
$\mathbf{S}$	0.02	?	?
ash	0.64	?	?
moisture	6.04	?	?

The chemical analysis of the Blend3 feedstock is presented in Table 4. Again, only one set of data is available so the uncertainty in the measurements is unknown. The chemical analysis measurements are used to determine the biomass composition which is needed for the kinetics model.

Table 4: Blend3 chemical analysis mass percent, dry basis. Source [7].

Chemical component	% dry	% dry	%dry
glucan	38.95	?	?
acetyl	1.59	?	?
arabinan	1.40	?	?
galactan	3.16	?	?
mannan	10.52	?	?
xylan	7.89	?	?
lignin	29.48	?	?
free fructose	0.07	?	?
free glucose	0.04	?	?
sucrose	0.04	?	?
water extractives	2.75	?	?
ethanol extractives	3.49	?	?
non-structural inorganics	0.22	?	?
structural inorganics	0.41	?	?

Table 5: Blend3 ash analysis as weight percent of ash. Source [3].

Metal oxide	wt. %	wt. %	wt. %
-SiO <sub>2</sub>	28.1	?	?
$Al_2O_3$	7.06	?	?
${ m TiO_2}$	0.34	?	?
CaO	21.8	?	?
$Na_2O$	0.71	?	?
$K_2O$	13.8	?	?
$P_2O_5$	5.47	?	?
$\mathrm{SO}_3$	1.23	?	?
Cl	0.09	?	?
$CO_2$	5.14	?	?

Table 6: Blend3 particle properties from pelletized crushed feedstock. The crushed feedstock is used in the entrained flow reactor.

Property	Value	Description	Source
$\rho$	$1{,}050~\rm kg/m^3$	particle density, daf basis	[6]
$\eta$	0.27	particle porosity	
k	$0.23~\mathrm{W/mK}$	thermal conductivity	

Table 7: Entrained flow reactor yields for Blend3 feedstock.

Yield	wt. %
total liquid	64.9
char	$13.9 \pm 0.1$
gas	$17.2 \pm 0.2$
mass balance	$96.9 \pm 1.5$
carbon balance	$93.0 \pm 1.0$

### 2.3 Forest residue feedstock

The forest residue feedstock is comprised of branches/twigs, cambium, needles, bark, and whitewood. This feedstock is used in the NREL fluidized bed reactor (FBR) for the purposes of the FCIC project. The FBR is operated at fast pyrolysis conditions for the thermochemical conversion of biomass. The reactor is sometimes referred to as the 2FBR.

Table 8: General information for the forest residue feedstock.

Item	Description
Name	forest residue
ID	?
Contact	?

Table 9: Bark ultimate analysis mass percent, dry ash-free basis. Source [1].

Element	% daf	% daf	% daf
С	48.27	?	?
H	5.72	?	?
N	0.52	?	?

Table 10: Branches/twigs ultimate analysis mass percent, dry ash-free basis. Source [1].

Element	% daf	% daf	% daf
С	49.69	?	?
Н	6.36	?	?
N	0.25	?	?

Table 11: Cambium ultimate analysis mass percent, dry ash-free basis. Source [1].

Element	% daf	% daf	% daf
С	48.52	?	?
Н	6.39	?	?
N	0.11	?	?

Table 12: Needles ultimate analysis mass percent, dry ash-free basis. Source [1].

Element	% daf	% daf	% daf
С	48.59	?	?
$\mathbf{H}$	5.92	?	?
N	1.22	?	?

Table 13: Whitewood ultimate analysis mass percent, dry ash-free basis. Source [1].

Element	% daf	% daf	% daf
С	48.27	?	?
${ m H}$	6.15	?	?
N	0.10	?	?

Table 14: Whitewood biomass composition mass percent, dry basis. Source [2].

Component	% dry
Cellulose	38.04
Hemicellulose	24.2

## 3 Model development

Details about the biomass pyrolysis kinetics and computational models developed for the entrained flow reactor are discussed in this section.

### 3.1 Pyrolysis kinetics

The kinetic reaction mechanisms presented by Debiagi et al. are used to model biomass pyrolysis in the entrained flow reactor. These reactions are shown below in Table 15.

Table 15: Kinetic reactions for biomass pyrolysis where A is the prefactor, E is the activation energy, and T is temperature. Source [4].

Item	Reaction	A (1/s)	E (cal/mol)
1	$CELL \rightarrow CELLA$	$1.5 \times 10^{14}$	47,000
2	CELLA $\rightarrow$ 0.40 CH2OHCHO + 0.03 CHOCHO + 0.17 CH3CHO + 0.25	$2.5 \times 10^{6}$	19,100
	C6H6O3 + 0.35 C2H5CHO + 0.20 CH3OH + 0.15 CH2O + 0.49 CO + 0.05		
	$G{CO} + 0.43 CO2 + 0.13 H2 + 0.93 H2O + 0.05 G{COH2} loose + 0.02$		
	$\text{HCOOH} + 0.05 \text{ CH2OHCH2CHO} + 0.05 \text{ CH4} + 0.1 \text{ G}\{\text{H2}\} + 0.66 \text{ CHAR}$		
3	$CELLA \rightarrow C6H10O5$	$3.3 \times T$	10,000
4	CELL $\rightarrow$ 4.45 H2O + 5.45 CHAR + 0.12 G{COH2} stiff + 0.18 G{COH2}	$9.0 \times 10^{7}$	31,000
	loose + $0.25 \text{ G}\{\text{CO}\} + 0.125 \text{ G}\{\text{H2}\} + 0.125 \text{ H2}$		
5	$GMSW \rightarrow 0.70 \ HCE1 + 0.30 \ HCE2$	$1.0 \times 10^{10}$	31,000
6	$XYHW \rightarrow 0.35 \text{ HCE1} + 0.65 \text{ HCE2}$	$1.25 \times 10^{11}$	31,400
7	$XYGR \rightarrow 0.12 \text{ HCE1} + 0.88 \text{ HCE2}$	$1.25 \times 10^{11}$	30,000
8	$\text{HCE1} \rightarrow 0.25 \text{ C5H8O4} + 0.25 \text{ C6H10O5} + 0.16 \text{ FURFURAL} + 0.13 \text{ C6H6O3}$	$16.0 \times T$	12,900
	+ 0.09  CO2 + 0.1  CH4 + 0.54  H2O + 0.06  CH2OHCH2CHO + 0.1  CHOCHO		
	+ 0.02  H2 + 0.1  CHAR		
9	$\text{HCE1} \rightarrow 0.4 \text{ H2O} + 0.39 \text{ CO2} + 0.05 \text{ HCOOH} + 0.49 \text{ CO} + 0.01 \text{ G{CO}}$	$3.0 \times 10^{-3} \times T$	3,600
	$+ 0.51 \text{ G}\{\text{CO2}\} + 0.05 \text{ G}\{\text{H2}\} + 0.4 \text{ CH2O} + 0.43 \text{ G}\{\text{COH2}\} \text{ loose} + 0.3$		
	$CH4 + 0.325 G\{CH4\} + 0.1 C2H4 + 0.075 G\{C2H4\} + 0.975 CHAR + 0.37$		
	$G{COH2} stiff + 0.1 H2 + 0.2 G{C2H6}$		

10	HCE2 → 0.3 CO + 0.5125 CO2 + 0.1895 CH4 + 0.5505 H2 + 0.056 H2O + 0.049 C2H5OH + 0.035 CH2OHCHO + 0.105 CH3CO2H + 0.0175 HCOOH + 0.145 FURFURAL + 0.05 G{CH4} + 0.105 G{CH3OH} + 0.1 G{C2H4} + 0.45 G{CO2} + 0.18 G{COH2} loose + 0.7125 CHAR + 0.21 G{H2} + 0.78 G{COH2} stiff + 0.2 G{C2H6}	$7.0\times10^9$	30,500
11	$LIGH \rightarrow LIGOH + 0.5 \text{ C2H5CHO} + 0.4 \text{ C2H4} + 0.2 \text{ CH2OHCHO} + 0.1 \text{ CO} + 0.1 \text{ C2H6}$	$6.7\times10^{12}$	37,500
12	$LIGO \rightarrow LIGOH + CO2$	$3.3 \times 10^{8}$	25,500
13	LIGC $\rightarrow$ 0.35 LIGCC + 0.1 VANILLIN + 0.1 C6H5OCH3 + 0.27 C2H4 + H2O + 0.17 G{COH2} loose + 0.4 G{COH2} stiff + 0.22 CH2O + 0.21 CO + 0.1 CO2 + 0.36 G{CH4} + 5.85 CHAR + 0.2 G{C2H6} + 0.1 G{H2}	$1.0 \times 10^{11}$	37,200
14	LIGCC $\rightarrow$ 0.25 VANILLIN + 0.15 CRESOL + 0.15 C6H5OCH3 + 0.35 CH2OHCHO + 0.7 H2O + 0.45 CH4 + 0.3 C2H4 + 0.7 H2 + 1.15 CO + 0.4 G{CO} + 6.80 CHAR + 0.4 C2H6	$1.0 \times 10^4$	24,800
15	LIGOH $\rightarrow$ 0.9 LIG + H2O + 0.1 CH4 + 0.6 CH3OH + 0.3 G{CH3OH} + 0.05 CO2 + 0.65 CO + 0.6 G{CO} + 0.05 HCOOH + 0.45 G{COH2} loose + 0.4 G{COH2} stiff + 0.25 G{CH4} + 0.1 G{C2H4} + 0.15 G{C2H6} + 4.25 CHAR + 0.025 C24H28O4 + 0.1 C2H3CHO	$1.5 \times 10^{8}$	30,000
16	LIG $\rightarrow$ VANILLIN + 0.1 C6H5OCH3 + 0.5 C2H4 + 0.6 CO + 0.3 CH3CHO + 0.1 CHAR	$4.0 \times T$	12,000
17	LIG $\rightarrow$ 0.6 H2O + 0.3 CO + 0.1 CO2 + 0.2 CH4 + 0.4 CH2O + 0.2 G{CO} + 0.4 G{CH4} + 0.5 G{C2H4} + 0.4 G{CH3OH} + 1.25 G{COH2} loose + 0.65 G{COH2} stiff + 6.1 CHAR + 0.1 G{H2}	$8.3 \times 10^{-2} \times T$	8,000
18	LIG $\rightarrow$ 0.6 H2O + 2.6 CO + 0.6 CH4 + 0.4 CH2O + 0.75 C2H4 + 0.4 CH3OH + 4.5 CHAR + 0.5 C2H6	$1.5\times10^9$	31,500
19	$TGL \rightarrow C2H3CHO + 2.5 MLINO + 0.5 U2ME12$	$7.0 \times 10^{12}$	45,700
20	$TANN \rightarrow 0.85 C6H5OH + 0.15 G\{C6H5OH\} + G\{CO\} + H2O + ITANN$	$2.0 \times 10^{1}$	10,000
21	ITANN $\rightarrow$ 5 CHAR + 2 CO + H2O + 0.55 G{COH2} loose + 0.45 G{COH2} stiff	$1.0 \times 10^{3}$	25,000
22	$G\{CO2\} \to CO2$	$1.0 \times 10^{6}$	24,500
23	$G(CO) \rightarrow CO$	$5.0 \times 10^{12}$	52,500
24	$G\{CH3OH\} \rightarrow CH3OH$	$2.0 \times 10^{12}$	50,000
25	$G{COH2}loose \rightarrow 0.2 CO + 0.2 H2 + 0.8 H2O + 0.8 CHAR$	$6.0 \times 10^{10}$	50,000
26	$G\{C2H6\} \rightarrow C2H6$	$1.0 \times 10^{11}$	52,000
27	$G(CH4) \rightarrow CH4$	$1.0 \times 10^{11}$	53,000
28	$G\{C2H4\} \rightarrow C2H4$	$1.0 \times 10^{11}$	54,000
29	$G\{C6H5OH\} \rightarrow C6H5OH$	$1.5 \times 10^{12}$	55,000
30	G{COH2}stiff $\rightarrow$ 0.8 CO + 0.8 H2 + 0.2 H2O + 0.2 CHAR	$1.0 \times 10^{9}$	59,000
31	$G\{H2\} \to H2$	$1.0 \times 10^{8}$	70,000
32	$ACQUA \rightarrow H2O$	$1.0 \times T$	8,000

Chemical species in the Debiagi et al. kinetic scheme for biomass pyrolysis are listed in Table 16. Species are grouped into solid, metaplastic, gas, and liquid phases.

Table 16: Chemical species in the Debiagi kinetics scheme for biomass pyrolysis. Source [4].

Item	Name	Formula	Phase	Description
1 2	CELL CELLA	$C_6H_{10}O_5$ $C_6H_{10}O_5$	solid solid	cellulose active cellulose
3	GMSW	$C_5H_8O_4$	solid	hemicellulose softwood

Name	4	XYHW	$C_5H_8O_4$	solid	hemicellulose hardwood
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9		-			
10					•
11		-			
12					
13 LIGO $C_{20}H_{22}O_{10}$ solid intermediate lignin intermediate light interplement interplement interplement light interplement interplement interplement interplement interplement interplement interpl					
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$					
15 TANN $C_{15}H_{12}O_{7}$ solid tannins $C_{15}H_{12}O_{7}$ solid triglycerides $C_{15}H_{12}O_{7}O_{7}$ solid triglycerides $C_{15}H_{12}O_{7}O_{7}O_{7}O_{7}O_{7}O_{7}O_{7}O_{7$					
16 TGL $C_{37}H_{100}O_7$ solid solid triglycerides char as pure carbon loose formaldehyde trapped carbon monoxide trapped methanol trapped methanol trapped methanol stiff formaldehyde trapped carbon monoxide trapped methanol trappe					<u>e</u>
17 CHAR C $C$ solid char as pure carbon loss formaldehyde $CCO^2$ metaplastic trapped carbon monoxide trapped carbon monoxide trapped carbon monoxide trapped carbon monoxide trapped methanol trapped methanol trapped ethylene $CCO^2$ metaplastic trapped methanol trapped methanol trapped methanol trapped phenol stiff formaldehyde $CCO^2$ metaplastic trapped methanol trapped phenol stiff formaldehyde $CCO^2$ metaplastic trapped phenol stiff formaldehyde $CCO^2$ metaplastic trapped trapped phenol stiff formaldehyde $CCO^2$ metaplastic trapped hydrogen metaplastic trapped hydrogen $CCO^2$ metaplastic trapped methanol $CCO^2$ metaplastic metaplastic metaplastic trapped methanol $CCO^2$ metaplastic metaplastic trapped methanol $CCO^2$ metaplastic metaplastic metaplastic $CCO^2$ metaplastic metaplastic $CCO^2$ metaplastic metaplastic $CCO^2$ metaplast					
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-		$C_{57}H_{100}O_{7}$		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	17	CHAR	$^{\mathrm{C}}$	solid	char as pure carbon
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	18	$G\{COH2\}$ loose	$CH_2O$	metaplastic	loose formaldehyde
21 $G\{CH3OH\}$ $CH_4O$ metaplastic trapped methanol trapped $G\{CH4\}$ $CH_4$ metaplastic trapped methane $G\{CH4\}$ $G\{CH4\}$ $G\{CH4\}$ metaplastic metaplastic trapped ethylene $G\{CGH5OH\}$ $G_{0}$ $G_{0}$ $G\{CH2\}$ stiff $G_{0}$	19		$CO_2$	metaplastic	trapped carbon dioxide
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	20	G{CO}	CO	metaplastic	trapped carbon monoxide
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	21	G{CH3OH}	$CH_4O$	metaplastic	trapped methanol
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	22	,	$CH_4$	-	
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$		C2H5CHO	$C_3H_6O$	•	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	37	C2H5OH	$C_2H_6O$	liquid	ethanol
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	38	C5H8O4	$C_5H_8O_4$	liquid	xylofuranose
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	39	C6H10O5	$C_6H_{10}O_5$	liquid	levoglucosan
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	40	C6H5OCH3	$C_7H_8O$	liquid	anisole
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	41	C6H5OH	$C_6H_6O$	liquid	phenol
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	42			_	hydroxymethylfurfural
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56 VANILLIN C <sub>8</sub> H <sub>8</sub> O <sub>3</sub> liquid vanillin				_	
10 0 0				_	
57 ACQUA H <sub>2</sub> O liquid water within biomass					
	57	ACQUA	$H_2O$	liquid	water within biomass

#### 3.2 Biomass characterization

Here.

#### 3.3 Batch reactor

The material balance for a typical chemical reactor is shown in Equation 1 where  $C_0$  is inlet concentration, C is outlet concentration, v is volumetric flow rate, r is the reaction rate, and V is the reactor volume.

$$accumulation = input - output + reaction$$

$$\frac{dC}{dt}V = vC_0 - vC + rV$$
(1)

A batch reactor was modeled to understand the time scales associated with the biomass pyrolysis kinetics. For the batch reactor, input and output is zero therefore only the accumulation and reaction terms remain in the material balance. For a constant volumne reactor the V terms cancel out; therefore, Equation 2 represents the material balance for a batch reactor model.

$$accumulation = 0 - 0 + reaction$$

$$\frac{dC}{dt} = r$$
(2)

#### 3.4 Sensitivity analysis

Here.

#### 4 Results and discussion

Characterization of the biomass along with batch reactor and sensitivity analysis results are discussed in this section.

#### 4.1 Blend3 biomass composition

Several approaches were investigated to characterize the Blend3 feedstock for use with the Debiagi pyrolysis kinetics. The first approach uses the characterization method discussed in the Debiagi et al. 2015 paper where carbon and hydrogen from ultimate analysis is used to determine the biomass composition [5]. To use this approach for the Blend3 feedstock, the mass fraction of C and H on a dry ash-free basis (last column in Table 17) is used for the biomass characterization procedure.

Table 17: Ultimate analysis bases calculated from the Blend3 feedstock asreceived data. Mass percent values are given for as-received (ar), dry, and dry ash-free (daf) basis.

Element	% ar	% dry	% daf	% daf
С	49.52	52.70	53.06	53.16
H	5.28	5.62	5.66	5.67
O	38.35	40.82	41.10	41.17
N	0.15	0.16	0.16	
$\mathbf{S}$	0.02	0.02	0.02	
ash	0.64	0.68		
moisture	6.04			

The Blend3 characterizaton was performed using a carbon mass fraction of 53.16%, hydrogen mass fraction of 5.67%, and splitting parameters  $\alpha=0.6$ ,  $\beta=0.8$ ,  $\gamma=0.8$ ,  $\delta=1.0$ , and  $\epsilon=1.0$  which do not account for extractives in the feedstock. Results from this characterization are shown in Figure 5 and the associated biomass composition is given in Table 18. While this approach is useful for limited feedstock data, its accuracy is questionable when compared to experimental measurements. For example, chemical analysis of the Blend3 feedstock provides a lignin composition of 29.48% (see Table 4) whereas the characterization method using ultimate analysis data estimates a total lignin composition greater than 59%.

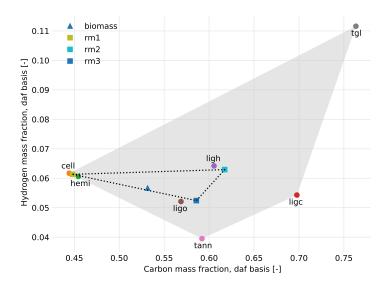


Figure 5: Characterization of the Blend3 feedstock using ultimate analysis data. Reference mixtures (rm) are labeled with square markers.

Table 18: Biomass composition estimated from the Blend3 ultimate analysis data. Values are mass basis.

Biomass composition	%daf
cellulose	26.38
hemicellulose	14.33
lignin-c	7.84
lignin-h	5.27
lignin-o	46.18
tann	0.00
tgl	0.00

To improve the Blend3 characterization based on ultimate analysis data, the splitting parameters were adjusted to account for extractives in the feedstock by using  $\alpha=0.56$ ,  $\beta=0.6$ ,  $\gamma=0.6$ ,  $\delta=0.78$ , and  $\epsilon=0.88$ . Also, since the uncertainty in the ultimate analysis data is unknown (see Table 3) the carbon mass fraction was adjusted to 51% and the hydrogen mass fraction to 6%. Results from these adjustments are presented in Figure 6 and Table 19.

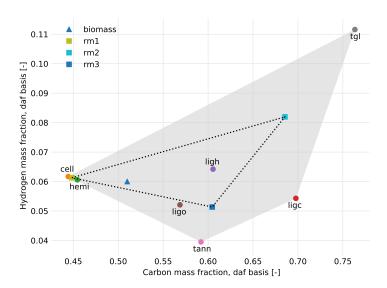


Figure 6: Characterization of the Blend3 feedstock using modified ultimate analysis data and adjusting the splitting parameters to account for extractives. Reference mixtures (rm) are labeled with square markers.

Table 19: Biomass composition estimated from the modified Blend3 ultimate analysis data. Values are mass basis.

Biomass composition	% daf
cellulose	39.24
hemicellulose	25.12
lignin-c	8.57
lignin-h	3.11
lignin-o	18.00
tann	2.95
tgl	3.01

## 4.2 Batch reactor conversion and yields

Here.

### 4.3 Sensitivity analysis

Results for the sensitivity analysis of the Debiagi kinetics using a batch reactor model are shown in Tables X.

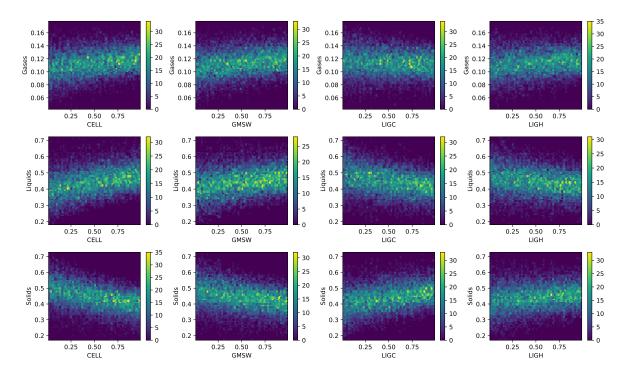


Figure 7: Batch reactor results for cellulose, hemicellulose (GMSW), carbon-rich lignin (LIGC), and hydrogen-rich lignin (LIGH) using 16,000 samples. Reaction time is 10 seconds at 773.15 K and 101,325 Pa. Colorbar represents bin count.

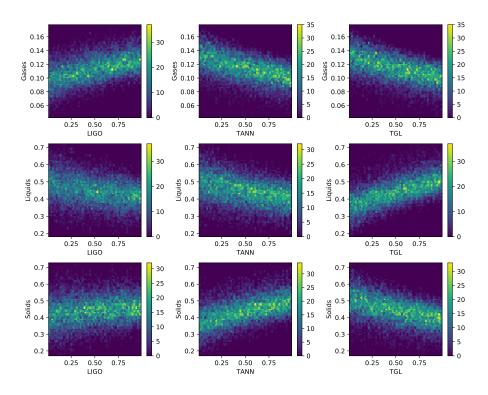


Figure 8: Batch reactor results for oxygen-rich lignin (LIGO), tannins (TANN), and triglycerides (TGL) using 16,000 samples. Reaction time is 10 seconds at 773.15 K and 101,325 Pa. Colorbar represents bin count.

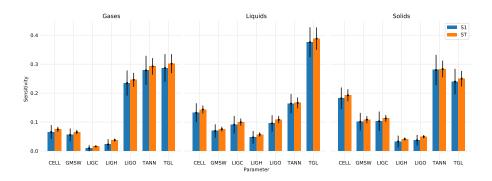


Figure 9: First-order (S1) and total-order (ST) Sobol indices for biomass composition with reactants grouped as gases, liquids, and solids using 16,000 samples.

## 5 Conclusions

Here.

# 6 Source code

The Python code used to develop the models and generate results discussed in this paper is available on GitHub at https://github.com/ccpcode/nrel-efr.

## A Appendix

### A.1 Sensitivity analysis

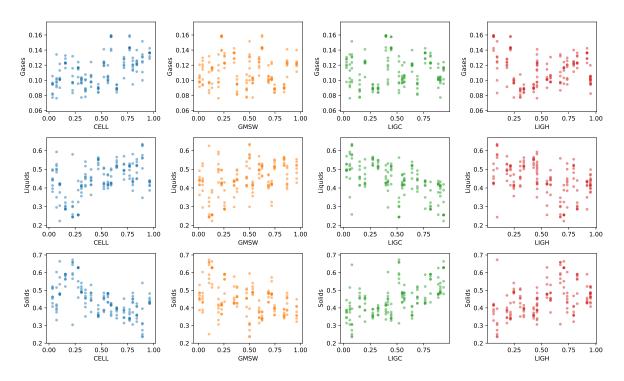


Figure 10: Batch reactor results for cellulose, hemicellulose (GMSW), carbon-rich lignin (LIGC), and hydrogen-rich lignin (LIGH) using 160 samples. Reaction time is 10 seconds at 773.15 K and 101,325 Pa.

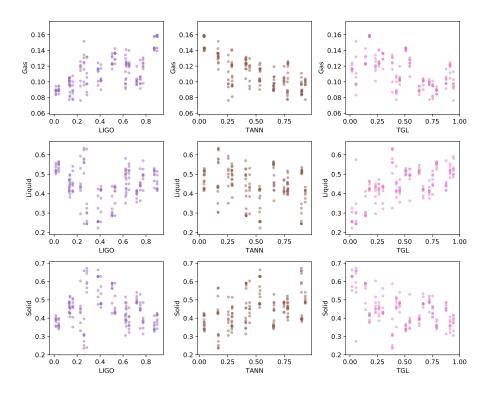


Figure 11: Batch reactor results for oxygen-rich lignin (LIGO), tannins (TANN), and triglycerides (TGL) using 160 samples. Reaction time is 10 seconds at  $773.15~\mathrm{K}$  and  $101,325~\mathrm{Pa}$ .

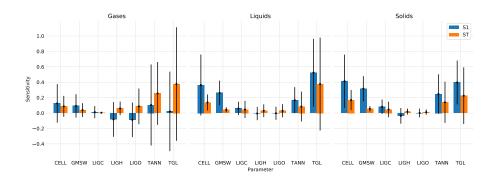


Figure 12: First-order (S1) and total-order (ST) Sobol indices for biomass composition with reactants grouped as gases, liquids, and solids using 160 samples.

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