B-field of a horizontal bar magnet

C := 1 coefficient to linearly scale everything as needed.

$$a := 250$$
 $b := 50$ $R := \frac{b}{2}$

a = length of bar magnet in arbritrary units b=width of bar magnet

R = radius of bar magnet

The following are elliptic integrals for x and y components of the B-field. Magnet is oriented horizontally along the x-direction. These integrals have no analytical solution. The field is scaled so the B at the center of an infinitely long bar magnet is 1. The field at the center of a finite-length magnet is a little less than 1.

$$Bx(x,y) := \frac{C \cdot R}{4 \cdot \pi} \cdot \int_{-\frac{a}{2}}^{\frac{a}{2}} \int_{0}^{2 \cdot \pi} \frac{(R - y \cdot \sin(\text{phi}))}{\left[R^2 + y^2 - 2 \cdot y \cdot R \cdot \sin(\text{phi}) + (x - xp)^2\right]^{\frac{3}{2}}} d\text{phi dxp}$$

$$By(x,y) := \frac{C \cdot R}{4 \cdot \pi} \cdot \int_{-\frac{a}{2}}^{\frac{a}{2}} \int_{0}^{2 \cdot \pi} \frac{(x - xp) \cdot \sin(phi)}{\left[R^2 + y^2 - 2 \cdot y \cdot R \cdot \sin(phi) + (x - xp)^2\right]^{\frac{3}{2}}} dphi dxp$$

Check: B at middle of right edge of magnet should be about 1/2 of B-field at center.

Bx(0,0) = 0.980581 Bx
$$\left(\frac{a}{2},0\right)$$
 = 0.4975
$$\frac{Bx\left(\frac{a}{2},0\right)}{Bx(0,0)}$$
 = 0.50737

$$B_{mag}(x,y) := \sqrt{Bx(x,y)^2 + By(x,y)^2}$$
 Magnitude of B-field (unused)

$$B(y,z) := \begin{pmatrix} Bx(y,z) \\ By(y,z) \end{pmatrix}$$
 Actual B-field

Following line scales B so that it does not appear to fall off with distance too rapidly. THIS ASSUMES THAT B=1 at CENTER OF MAGNET. (This is unused in this mathcad file).

n := 4 n is a number between 1(no rescaling) and, say, 5 (big rescaling)

$$B_dir(x,y) := \begin{bmatrix} \frac{Bx(x,y)}{B_mag(x,y)} \\ \left(\frac{By(x,y)}{B_mag(x,y)}\right) \end{bmatrix} \qquad Bscaled(x,y) := \begin{bmatrix} \sqrt[n]{B_mag(x,y)} \cdot \frac{Bx(x,y)}{B_mag(x,y)} \cdot \frac{By(x,y)}{B_mag(x,y)} \\ \left(\sqrt[n]{B_mag(x,y)} \cdot \frac{By(x,y)}{B_mag(x,y)}\right) \end{bmatrix}$$

Compute field interior to magnet:

$$b = 50$$
 $a = 250$ $a = 2$

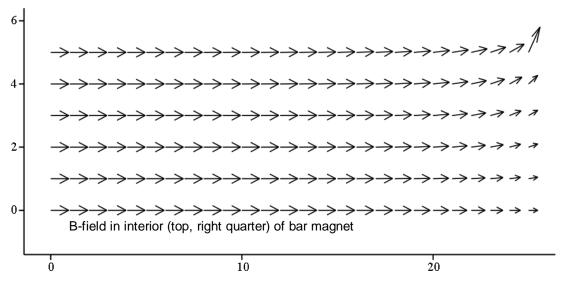
$$i := 0.. \frac{\text{xrange}}{\text{xdel}}$$
 $j := 0.. \frac{\text{yrange}}{\text{ydel}}$

gridOffset := 0.1 Offset is so that none of the points fall exactly on the edge of the magnet, where the integrals do not converge.

$$\begin{array}{ll} xind_i \coloneqq i \cdot xdel - gridOffset & yind_j \coloneqq j \cdot ydel - gridOffset \\ \\ M_{i\,,\,j} \coloneqq B \Big(xind_i\,, yind_j \Big) & iMax \coloneqq \frac{xrange}{xdel} \quad jMax \coloneqq \frac{yrange}{ydel} \\ \\ BX_int_{i\,,\,j} \coloneqq \Big(M_{i\,,\,j} \Big)_0 & iMax = 25 & jMax = 5 \\ \\ BY_int_{i\,,\,j} \coloneqq \Big(M_{i\,,\,j} \Big)_1 & iMax = 25 & jMax = 5 \end{array}$$

$$BXrounded_int_{i,j} := round(BX_int_{i,j}, 6)$$

$$BYrounded_int_{i,j} := round(BY_int_{i,j}, 6)$$



(BX_int, BY_int)

Compute field outside magnet, nearby with dense grid

$$xrange := 2a$$
 $yrange := 8 \cdot b$ $xdel := 5$ $ydel := 5$

$$i := 0.. \frac{xrange}{xdel} \qquad \qquad j := 0.. \frac{yrange}{ydel} \qquad \qquad xrange = 500$$

$$iMax := \frac{xrange}{xdel}$$
 $iMax := \frac{yrange}{ydel}$ $yrange = 400$

$$iMax = 100$$
 $jMax = 80$

<u>gridOffset</u> := 0.1 Offset is so that none of the points fall exactly on the edge of the magnet, where the integrals do not converge.

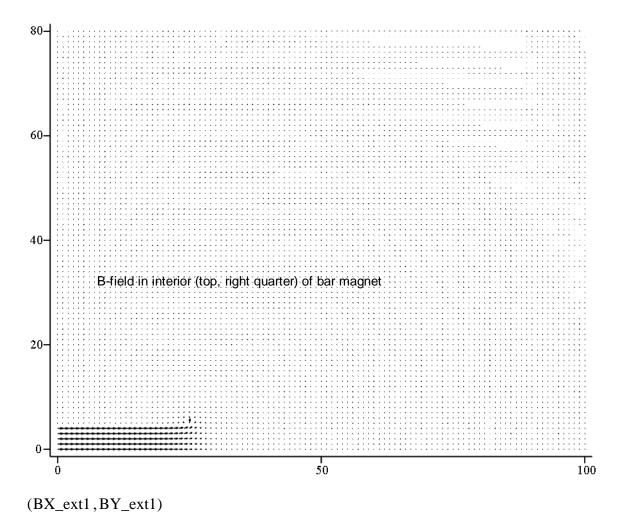
$$xind_i := i \cdot xdel + gridOffset \qquad \quad yind_j := j \cdot ydel + gridOffset$$

$$M_{i,j} := B(xind_i, yind_j)$$

$$BX_{ext1_{i,j}} := (M_{i,j})_0 \quad BY_{ext1_{i,j}} := (M_{i,j})_1$$

 $BXrounded_ext1_{i,j} := round\big(BX_ext1_{i,j}, 6\big)$

 $BYrounded_ext1_{i,j} := round(BY_ext1_{i,j}, 6)$



Compute B-field far away, with sparse grid.

$$\begin{aligned} & \underset{i}{\text{xrange}} := 10 \cdot \text{a} & \underset{\text{yrange}}{\text{yrange}} := 24 \cdot \text{b} & \underset{\text{xdel}}{\text{xdel}} := 20 & \underset{\text{ydel}}{\text{ydel}} := 20 \\ & \text{i} := 0 ... \frac{\text{xrange}}{\text{xdel}} & \text{j} := 0 ... \frac{\text{yrange}}{\text{ydel}} & \text{xrange} = 2.5 \times 10^3 \\ & \text{yrange} = 1.2 \times 10^3 \end{aligned}$$

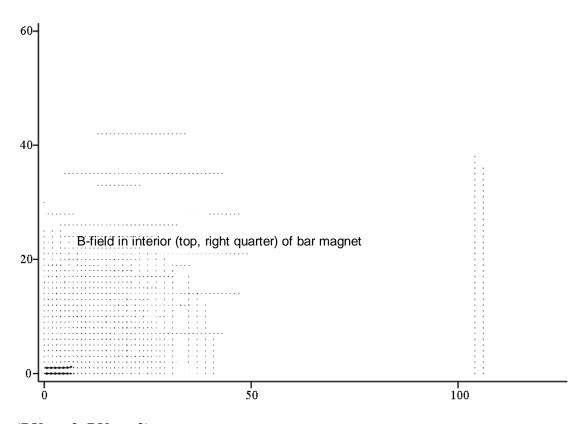
<u>gridOffset</u> := 0 Offset is so that none of the points fall exactly on the edge of the magnet, where the integrals do not converge.

$$\begin{aligned} &xind_i := i \cdot xdel + gridOffset & yind_j := j \cdot ydel + gridOffset \\ &M_{i\,,\,j} := B \Big(xind_i\,, yind_j \Big) \end{aligned}$$

$$BX_{ext2_{i,j}} := (M_{i,j})_0 \quad BY_{ext2_{i,j}} := (M_{i,j})_1$$

 $BXrounded_{ext2_{i,j}} := round(BX_{ext2_{i,j}}, 7)$

 $BYrounded_ext2_{i,j} := round(BY_ext2_{i,j},7)$



(BX_ext2,BY_ext2)

0	1	2	3	4	5
0.969	0.97	0.97	0.971	0.972	0.97
0.966	0.966	0.967	0.968	0.969	0.968
0.962	0.962	0.963	0.964	0.966	0.965
0.957	0.958	0.959	0.96	0.962	0.961
0.951	0.952	0.953	0.955	0.957	0.957
0.944	0.944	0.946	0.948	0.951	0.952
0.934	0.934	0.936	0.94	0.944	0.946
0.921	0.922	0.925	0.929	0.935	0.939
0.904	0.905	0.909	0.915	0.923	0.93
	0.969 0.966 0.962 0.957 0.951 0.944 0.934 0.921	0.969 0.97 0.966 0.966 0.957 0.958 0.951 0.952 0.944 0.944 0.934 0.934 0.921 0.922	0.969 0.97 0.97 0.966 0.966 0.967 0.962 0.962 0.963 0.957 0.958 0.959 0.951 0.952 0.953 0.944 0.944 0.946 0.934 0.934 0.936 0.921 0.922 0.925	0.969 0.97 0.97 0.971 0.966 0.966 0.967 0.968 0.962 0.962 0.963 0.964 0.957 0.958 0.959 0.96 0.951 0.952 0.953 0.955 0.944 0.944 0.946 0.948 0.934 0.934 0.936 0.94 0.921 0.922 0.925 0.929	0.969 0.97 0.97 0.971 0.972 0.966 0.966 0.967 0.968 0.969 0.962 0.962 0.963 0.964 0.966 0.957 0.958 0.959 0.96 0.962 0.951 0.952 0.953 0.955 0.957 0.944 0.944 0.946 0.948 0.951 0.934 0.934 0.936 0.94 0.944 0.921 0.922 0.925 0.929 0.935

 $BXrounded_int = \\$

19	0.881	0.883	0.889	0.898	0.909	0.918
20	0.851	0.854	0.861	0.874	0.89	0.905
21	0.81	0.814	0.824	0.841	0.864	0.889
22	0.756	0.76	0.773	0.796	0.829	0.866
23	0.685	0.689	0.702	0.729	0.776	0.839
24	0.597	0.6	0.61	0.632	0.683	0.801
25	0.5	0.5	0.5	0.5	0.502	

BYrounded_int =

76	77	78	7

	0	-6.12·10 ⁻⁴	-5.91·10 ⁻⁴	-5.7·10 ⁻⁴	-5.5
	1	-6.12·10 ⁻⁴	-5.9·10 ⁻⁴	-5.7·10 ⁻⁴	-5
	2	-6.11·10 ⁻⁴	-5.89·10 ⁻⁴	-5.69·10 ⁻⁴	-5
	3	-6.09· 10 ⁻⁴	-5.88·10 ⁻⁴	-5.67·10 ⁻⁴	-5.4
	4	-6.06·10 ⁻⁴	-5.85·10 ⁻⁴	-5.65·10 ⁻⁴	-5.4
	5	-6.03·10 ⁻⁴	-5.82·10 ⁻⁴	-5.62·10 ⁻⁴	-5.4
	6	-5.99·10 ⁻⁴	-5.78·10 ⁻⁴	-5.59·10 ⁻⁴	-5
:	7	-5.94·10 ⁻⁴	-5.74·10 ⁻⁴	-5.54·10 ⁻⁴	-5.3
	8	-5.89·10 ⁻⁴	-5.69·10 ⁻⁴	-5.5·10 ⁻⁴	-5.3
	9	-5.83·10 ⁻⁴	-5.63·10 ⁻⁴	-5.44·10 ⁻⁴	-5.2
	10	-5.77·10 ⁻⁴	-5.57·10 ⁻⁴	-5.38·10 ⁻⁴	-5.2
	11	-5.69·10 ⁻⁴	-5.5·10 ⁻⁴	-5.32·10 ⁻⁴	-5.1
	12	-5.61·10 ⁻⁴	-5.43·10 ⁻⁴	-5.25·10 ⁻⁴	-5.0
	13	-5.53·10 ⁻⁴	-5.35·10 ⁻⁴	-5.17·10 ⁻⁴	-5.0
	14	-5.44·10 ⁻⁴	-5.26·10 ⁻⁴	-5.09·10 ⁻⁴	-4.9
	15	-5.34·10 ⁻⁴	-5.17·10 ⁻⁴	-5.01·10 ⁻⁴	-4.8

 $BXrounded_ext1 =$

1 2·10-6 9.1·10-5 1.78·10-4 2.61·10-4 2 4·10-6 1.82·10-4 3.57·10-4 5.24·10-4 3 5·10-6 2.79·10-4 5.46·10-4 8.02·10-4 4 8·10-6 3.84·10-4 7.52·10-4 1.103·10-3 5 1·10-5 5.01·10-4 9.81·10-4 1.437·10-3 6 1.3·10-5 6.35·10-4 1.241·10-3 1.816·10-3 7 1.6·10-5 7.9·10-4 1.543·10-3 2.255·10-3 9 2.4·10-5 1.195·10-3 2.329·10-3 3.393·10-3 10 2.9·10-5 1.466·10-3 2.854·10-3 4.148·10-3 11 3.6·10-5 1.804·10-3 3.506·10-3 5.083·10-3 12 4.4·10-5 2.231·10-3 4.328·10-3 6.256·10-3 13 5.5·10-5 2.779·10-3 5.381·10-3 7.751·10-3 14 6.9·10-5 3.495·10-3 6.75·10-3 9.684·10-3 15 8.8·10-5 4.444·10-3 8.559·10-3 0.012	ı					
2			0	1	2	3
3 5·10-6 2.79·10-4 5.46·10-4 8.02·10-4 4 8·10-6 3.84·10-4 7.52·10-4 1.103·10-3 5 1·10-5 5.01·10-4 9.81·10-4 1.437·10-3 6 1.3·10-5 6.35·10-4 1.241·10-3 1.816·10-3 7 1.6·10-5 7.9·10-4 1.543·10-3 2.255·10-3 8 1.9·10-5 9.73·10-4 1.9·10-3 2.773·10-3 9 2.4·10-5 1.195·10-3 2.329·10-3 3.393·10-3 10 2.9·10-5 1.466·10-3 2.854·10-3 4.148·10-3 11 3.6·10-5 1.804·10-3 3.506·10-3 5.083·10-3 12 4.4·10-5 2.231·10-3 4.328·10-3 6.256·10-3 13 5.5·10-5 2.779·10-3 5.381·10-3 7.751·10-3 14 6.9·10-5 3.495·10-3 6.75·10-3 9.684·10-3 15 8.8·10-5 4.444·10-3 8.559·10-3 0.012		1	2·10 ⁻⁶	9.1·10 ⁻⁵	1.78·10 ⁻⁴	2.61·10 ⁻⁴
4 8 · 10 · 6 3.84 · 10 · 4 7.52 · 10 · 4 1.103 · 10 · 3 5 1 · 10 · 5 5.01 · 10 · 4 9.81 · 10 · 4 1.437 · 10 · 3 6 1.3 · 10 · 5 6.35 · 10 · 4 1.241 · 10 · 3 1.816 · 10 · 3 7 1.6 · 10 · 5 7.9 · 10 · 4 1.543 · 10 · 3 2.255 · 10 · 3 8 1.9 · 10 · 5 9.73 · 10 · 4 1.9 · 10 · 3 2.773 · 10 · 3 9 2.4 · 10 · 5 1.195 · 10 · 3 2.329 · 10 · 3 3.393 · 10 · 3 10 2.9 · 10 · 5 1.466 · 10 · 3 2.854 · 10 · 3 4.148 · 10 · 3 11 3.6 · 10 · 5 1.804 · 10 · 3 3.506 · 10 · 3 5.083 · 10 · 3 12 4.4 · 10 · 5 2.231 · 10 · 3 4.328 · 10 · 3 6.256 · 10 · 3 13 5.5 · 10 · 5 2.779 · 10 · 3 5.381 · 10 · 3 7.751 · 10 · 3 14 6.9 · 10 · 5 3.495 · 10 · 3 6.75 · 10 · 3 9.684 · 10 · 3 15 8.8 · 10 · 5 4.444 · 10 · 3 8.559 · 10 · 3 0.012		2	4·10⁻ ⁶	1.82·10 ⁻⁴	3.57·10 ⁻⁴	5.24·10 ⁻⁴
5 1·10-5 5.01·10-4 9.81·10-4 1.437·10-3 6 1.3·10-5 6.35·10-4 1.241·10-3 1.816·10-3 7 1.6·10-5 7.9·10-4 1.543·10-3 2.255·10-3 8 1.9·10-5 9.73·10-4 1.9·10-3 2.773·10-3 9 2.4·10-5 1.195·10-3 2.329·10-3 3.393·10-3 10 2.9·10-5 1.466·10-3 2.854·10-3 4.148·10-3 11 3.6·10-5 1.804·10-3 3.506·10-3 5.083·10-3 12 4.4·10-5 2.231·10-3 4.328·10-3 6.256·10-3 13 5.5·10-5 2.779·10-3 5.381·10-3 7.751·10-3 14 6.9·10-5 3.495·10-3 6.75·10-3 9.684·10-3 15 8.8·10-5 4.444·10-3 8.559·10-3 0.012		3	5·10 ⁻⁶	2.79·10 ⁻⁴	5.46·10 ⁻⁴	8.02·10 ⁻⁴
6 1.3·10-5 6.35·10-4 1.241·10-3 1.816·10-3 7 1.6·10-5 7.9·10-4 1.543·10-3 2.255·10-3 8 1.9·10-5 9.73·10-4 1.9·10-3 2.773·10-3 9 2.4·10-5 1.195·10-3 2.329·10-3 3.393·10-3 10 2.9·10-5 1.466·10-3 2.854·10-3 4.148·10-3 11 3.6·10-5 1.804·10-3 3.506·10-3 5.083·10-3 12 4.4·10-5 2.231·10-3 4.328·10-3 6.256·10-3 13 5.5·10-5 2.779·10-3 5.381·10-3 7.751·10-3 14 6.9·10-5 3.495·10-3 6.75·10-3 9.684·10-3 15 8.8·10-5 4.444·10-3 8.559·10-3 0.012		4	8·10 ⁻⁶	3.84·10 ⁻⁴	7.52·10 ⁻⁴	1.103·10 ⁻³
7 1.6·10-5 7.9·10-4 1.543·10-3 2.255·10-3 8 1.9·10-5 9.73·10-4 1.9·10-3 2.773·10-3 9 2.4·10-5 1.195·10-3 2.329·10-3 3.393·10-3 10 2.9·10-5 1.466·10-3 2.854·10-3 4.148·10-3 11 3.6·10-5 1.804·10-3 3.506·10-3 5.083·10-3 12 4.4·10-5 2.231·10-3 4.328·10-3 6.256·10-3 13 5.5·10-5 2.779·10-3 5.381·10-3 7.751·10-3 14 6.9·10-5 3.495·10-3 6.75·10-3 9.684·10-3 15 8.8·10-5 4.444·10-3 8.559·10-3 0.012		5	1·10 ⁻⁵	5.01·10 ⁻⁴	9.81·10 ⁻⁴	1.437·10 ⁻³
8 1.9·10 ⁻⁵ 9.73·10 ⁻⁴ 1.9·10 ⁻³ 2.773·10 ⁻³ 9 2.4·10 ⁻⁵ 1.195·10 ⁻³ 2.329·10 ⁻³ 3.393·10 ⁻³ 10 2.9·10 ⁻⁵ 1.466·10 ⁻³ 2.854·10 ⁻³ 4.148·10 ⁻³ 11 3.6·10 ⁻⁵ 1.804·10 ⁻³ 3.506·10 ⁻³ 5.083·10 ⁻³ 12 4.4·10 ⁻⁵ 2.231·10 ⁻³ 4.328·10 ⁻³ 6.256·10 ⁻³ 13 5.5·10 ⁻⁵ 2.779·10 ⁻³ 5.381·10 ⁻³ 7.751·10 ⁻³ 14 6.9·10 ⁻⁵ 3.495·10 ⁻³ 6.75·10 ⁻³ 9.684·10 ⁻³ 15 8.8·10 ⁻⁵ 4.444·10 ⁻³ 8.559·10 ⁻³ 0.012		6	1.3·10 ⁻⁵	6.35·10 ⁻⁴	1.241·10 ⁻³	1.816·10 ⁻³
8 1.9·10 ⁻³ 9.73·10 ⁻⁴ 1.9·10 ⁻³ 2.773·10 ⁻³ 9 2.4·10 ⁻⁵ 1.195·10 ⁻³ 2.329·10 ⁻³ 3.393·10 ⁻³ 10 2.9·10 ⁻⁵ 1.466·10 ⁻³ 2.854·10 ⁻³ 4.148·10 ⁻³ 11 3.6·10 ⁻⁵ 1.804·10 ⁻³ 3.506·10 ⁻³ 5.083·10 ⁻³ 12 4.4·10 ⁻⁵ 2.231·10 ⁻³ 4.328·10 ⁻³ 6.256·10 ⁻³ 13 5.5·10 ⁻⁵ 2.779·10 ⁻³ 5.381·10 ⁻³ 7.751·10 ⁻³ 14 6.9·10 ⁻⁵ 3.495·10 ⁻³ 6.75·10 ⁻³ 9.684·10 ⁻³ 15 8.8·10 ⁻⁵ 4.444·10 ⁻³ 8.559·10 ⁻³ 0.012		7	1.6·10 ⁻⁵	7.9·10 ⁻⁴	1.543·10 ⁻³	2.255·10 ⁻³
10 2.9·10-5 1.466·10-3 2.854·10-3 4.148·10-3 11 3.6·10-5 1.804·10-3 3.506·10-3 5.083·10-3 12 4.4·10-5 2.231·10-3 4.328·10-3 6.256·10-3 13 5.5·10-5 2.779·10-3 5.381·10-3 7.751·10-3 14 6.9·10-5 3.495·10-3 6.75·10-3 9.684·10-3 15 8.8·10-5 4.444·10-3 8.559·10-3 0.012	=	8	1.9·10 ⁻⁵	9.73·10 ⁻⁴	1.9·10 ⁻³	2.773·10 ⁻³
11 3.6·10-5 1.804·10-3 3.506·10-3 5.083·10-3 12 4.4·10-5 2.231·10-3 4.328·10-3 6.256·10-3 13 5.5·10-5 2.779·10-3 5.381·10-3 7.751·10-3 14 6.9·10-5 3.495·10-3 6.75·10-3 9.684·10-3 15 8.8·10-5 4.444·10-3 8.559·10-3 0.012		9	2.4·10 ⁻⁵	1.195·10 ⁻³	2.329·10 ⁻³	3.393·10 ⁻³
12 4.4·10 ⁻⁵ 2.231·10 ⁻³ 4.328·10 ⁻³ 6.256·10 ⁻³ 13 5.5·10 ⁻⁵ 2.779·10 ⁻³ 5.381·10 ⁻³ 7.751·10 ⁻³ 14 6.9·10 ⁻⁵ 3.495·10 ⁻³ 6.75·10 ⁻³ 9.684·10 ⁻³ 15 8.8·10 ⁻⁵ 4.444·10 ⁻³ 8.559·10 ⁻³ 0.012		10	2.9·10 ⁻⁵	1.466·10 ⁻³	2.854·10 ⁻³	4.148·10 ⁻³
13 5.5·10-5 2.779·10-3 5.381·10-3 7.751·10-3 14 6.9·10-5 3.495·10-3 6.75·10-3 9.684·10-3 15 8.8·10-5 4.444·10-3 8.559·10-3 0.012		11	3.6·10 ⁻⁵	1.804·10 ⁻³	3.506·10 ⁻³	5.083·10 ⁻³
14 6.9·10-5 3.495·10-3 6.75·10-3 9.684·10-3 15 8.8·10-5 4.444·10-3 8.559·10-3 0.012		12	4.4·10 ⁻⁵	2.231·10 ⁻³	4.328·10 ⁻³	6.256·10 ⁻³
15 8.8·10 ⁻⁵ 4.444·10 ⁻³ 8.559·10 ⁻³ 0.012		13	5.5·10 ⁻⁵	2.779·10 ⁻³	5.381·10 ⁻³	7.751·10 ⁻³
		14	6.9·10 ⁻⁵	3.495·10 ⁻³	6.75·10 ⁻³	9.684·10 ⁻³
16 1 13·10 ⁻⁴ 5 72·10 ⁻³ 0 011 0 016		15	8.8.10-5	4.444.10-3	8.559·10 ⁻³	0.012
1.10 10 0.72 10 0.011 0.010		16	1.13.10-4	5.72·10 ⁻³	0.011	0.016

 $BYrounded_ext1 =$

 $BXrounded_ext2 =$

0

0

12

13

0

0

0

1

1.778·10⁻³

1.117·10⁻³

0

	56	57	58	59	
0	-2.73·10 ⁻⁵	-2.59·10 ⁻⁵	-2.46·10 ⁻⁵	-2.34·10 ⁻⁵	
1	-2.73·10 ⁻⁵	-2.59·10 ⁻⁵	-2.46·10 ⁻⁵	-2.34·10 ⁻⁵	-:
2	-2.72·10 ⁻⁵	-2.58·10 ⁻⁵	-2.45·10 ⁻⁵	-2.33·10 ⁻⁵	-:
3	-2.7·10 ⁻⁵	-2.56·10 ⁻⁵	-2.43·10 ⁻⁵	-2.31·10 ⁻⁵	
4	-2.67·10 ⁻⁵	-2.54·10 ⁻⁵	-2.41·10 ⁻⁵	-2.29·10 ⁻⁵	-:
5	-2.64·10 ⁻⁵	-2.51·10 ⁻⁵	-2.38·10 ⁻⁵	-2.27·10 ⁻⁵	-:
6	-2.6·10 ⁻⁵	-2.47·10 ⁻⁵	-2.35·10 ⁻⁵	-2.24·10 ⁻⁵	-:
7	-2.55·10 ⁻⁵	-2.43·10 ⁻⁵	-2.31·10 ⁻⁵	-2.2·10 ⁻⁵	
8	-2.5·10 ⁻⁵	-2.38·10 ⁻⁵	-2.26·10 ⁻⁵	-2.16·10 ⁻⁵	-:
9	-2.44·10 ⁻⁵	-2.32·10 ⁻⁵	-2.21·10 ⁻⁵	-2.11·10 ⁻⁵	-:
10	-2.37·10 ⁻⁵	-2.26·10 ⁻⁵	-2.16·10 ⁻⁵	-2.06·10 ⁻⁵	-
11	-2.3·10 ⁻⁵	-2.2·10 ⁻⁵	-2.1·10 ⁻⁵	-2.01·10 ⁻⁵	-
12	-2.23·10 ⁻⁵	-2.13·10 ⁻⁵	-2.04·10 ⁻⁵	-1.95·10 ⁻⁵	-
13	-2.15·10 ⁻⁵	-2.06·10 ⁻⁵	-1.97·10 ⁻⁵	-1.89·10 ⁻⁵	-
14	-2.07·10 ⁻⁵	-1.98·10 ⁻⁵	-1.9·10 ⁻⁵	-1.82·10 ⁻⁵	-
15	-1.99·10 ⁻⁵	-1.91·10 ⁻⁵	-1.83·10 ⁻⁵	-1.76·10 ⁻⁵	

2

3.155·10⁻³

2.04·10-3

0

3

3.941.10-3

2.653-10-3

0

4

4.181·10⁻³

2.948-10-3

0

	1	0	1.415·10 ⁻³	2.373·10 ⁻³	2.719·10 ⁻³	2.591·10 ⁻³
	2	0	3.541·10 ⁻³	5.711·10 ⁻³	6.222·10 ⁻³	5.65·10 ⁻³
	3	0	7.881·10 ⁻³	0.012	0.012	9.655·10 ⁻³
	4	0	0.019	0.025	0.02	0.015
	5	0	0.057	0.055	0.034	0.021
	6	0	0.228	0.111	0.045	0.024
=	7	0	0.11	0.082	0.041	0.023
	8	0	0.032	0.037	0.027	0.018
	9	0	0.012	0.017	0.016	0.013
	10	0	5.735·10 ⁻³	9.095·10 ⁻³	9.777·10 ⁻³	8.896·10 ⁻³
	11	0	3.041·10 ⁻³	5.169·10 ⁻³	6.083·10 ⁻³	6.055·10 ⁻³

BYrounded_ext2 =

14	0	7.422 10-4	1.381⋅10-₃	1.849·10 ⁻³	2.126⋅10-3
15	0	5.149·10 ⁻⁴	9.716·10 ⁻⁴	1.328·10 ⁻³	

9	80	
	4	

51.10-4	-5.32·10 ⁻⁴
.5⋅10-4	-5.32·10 ⁻⁴
.5⋅10-4	-5.31·10 ⁻⁴
18· 10 ⁻⁴	-5.3·10 ⁻⁴
16 ⋅10-4	-5.27·10 ⁻⁴
13 ⋅10-4	-5.25·10 ⁻⁴
.4-10-4	-5.22·10 ⁻⁴
36⋅10-4	-5.18·10 ⁻⁴
31.10-4	-5.14·10 ⁻⁴
26-10-4	-5.09·10 ⁻⁴
21.10-4	-5.04·10 ⁻⁴
14-10-4	-4.98·10 ⁻⁴
)8⋅10-4	-4.91·10 ⁻⁴
)1.10-4	-4.85·10 ⁻⁴
93·10 ⁻⁴	-4.77·10 ⁻⁴
35·10 ⁻⁴	

4
3.39·10 ⁻⁴
6.8·10-4
1.039·10 ⁻³
1.429·10 ⁻³
1.86·10 ⁻³
2.348 10-3
2.91·10 ⁻³
3.57·10 ⁻³
4.358·10 ⁻³
5.312·10 ⁻³
6.486·10 ⁻³
7.95·10 ⁻³
9.802·10 ⁻³
0.012
0.015

60

2.23·10⁻⁵ 2.22·10⁻⁵

2.21.10-5

-2.2·10⁻⁵

2.18·10⁻⁵

2.16·10-5

2.13·10-5

-2.1·10⁻⁵

2.06·10⁻⁵

2.02·10⁻⁵

1.97·10⁻⁵

1.92·10⁻⁵

1.87·10⁻⁵

1.81·10⁻⁵

1.75·10⁻⁵