

1 Transient Response of Langmuir Turbulence to Abrupt Onset of
2 Surface Heating

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9

Abstract

10 Langmuir turbulence (LT) plays an important role in enhancing vertical mixing in the ocean
 11 surface boundary layer (OSBL). Such enhanced mixing is strongly affected by the diurnally varying
 12 heat flux, especially in the early morning when there is a transition from cooling to heating. In
 13 this period, turbulence is weakened, yet the surface heat flux is changing rapidly, such that the
 14 deviation of transient turbulence from its equilibrium state is large. This may lead to biases in the
 15 parameterization of turbulent mixing due to LT in large-scale ocean circulation models, in which
 16 an equilibrium of the turbulence state with the surface forcing is often assumed. In this study,
 17 we investigate the transient response of LT to an abrupt onset of surface heating using idealized
 18 large eddy simulations, and compare it with the transient response of wind-driven shear turbulence
 19 (ST). Near the surface, the destabilizing Stokes shear force competes with the stabilizing surface
 20 heating, resulting in a gradual decay of the turbulence intensity, in contrast to ST whose intensity
 21 decreases rapidly at first and then partially recovers due to the formation of a stronger jet in the
 22 surface warm layer. Below the surface, the decay of coherent downwelling plumes of LT occurs
 23 faster than shear turbulence, resulting in a quicker response of LT than ST at depth. The vertical
 24 velocity variance of LT at depth decays at a rate initially following t^{-1} and later transitioning to
 25 t^{-2} . We also examine the impact of details of the Stokes forcing on the transient response of LT.
 26 These results may help improve vertical mixing parameterizations in the OSBL.

27 **I. INTRODUCTION**

28 The ocean surface boundary layer (OSBL) serves as a critical interface mediating air-sea
 29 exchanges of heat, momentum, and gases through many processes that involve interactions
 30 among wind forcing, solar radiation, surface gravity waves, etc. [1, 2]. Among these pro-
 31 cesses, Langmuir turbulence arising from wave-current interaction via the Craik-Leibovich
 32 instability [3–5] is of particular interest due to its significant effects on enhancing vertical
 33 mixing in the OSBL and modulating air-sea fluxes [2, 6–9]. However, such a small-scale pro-
 34 cess in the OSBL is not resolved in large-scale ocean general circulation models (GCM) and
 35 its effects require parameterizations. During the past two decades, significant efforts have

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36 been made to parameterize the effects of Langmuir turbulence in regional and global ocean
37 simulations [10–14], yet large uncertainties persist (see a recent review and comparison in
38 Ref. [15]). In particular, correctly representing OSBL mixing due to Langmuir turbulence
39 during a diurnal cycle remains challenging [16–18].

40 Under strong diurnal surface heating, a diurnal warm layer (DWL) is formed, trapping
41 heat near the OSBL surface and blocking turbulent exchange with the layer below, so that
42 a diurnal jet develops and shear turbulence is enhanced [19–23]. The presence of Langmuir
43 turbulence inhibits the formation of a DWL due to enhanced turbulent mixing and deepens
44 the DWL when it forms [18, 24]. Existing scalings of the DWL depth work reasonably
45 well in describing the quasi-steady DWL depth around the heating peak during the day
46 [16, 18], but less so when surface heating is changing rapidly, especially in the early morning.
47 Improvement of such scalings requires a better understanding of the transient response of
48 Langmuir turbulence to diurnally varying surface heating.

49 A typical diurnal cycle in the OSBL consists of distinct phases that can be roughly
50 categorized into the following four [17]. (I) *Nighttime convection*, when the surface condition
51 is largely unstable and convective turbulence develops. (II) *Morning detrainment*, when the
52 surface buoyancy flux transits from unstable to stable as solar radiation begins to increase.
53 As a result, convective turbulence ceases and the resulting entrainment buoyancy flux is
54 suppressed. While the surface becomes stable, the remaining turbulence below the surface
55 decays due to the loss of the driving forces [25], during which weak turbulent mixing may
56 still persists. (III) *Daytime stable boundary layer*, when the daytime solar radiation is strong
57 enough to significantly suppress turbulence driven by surface wind and waves. A balance
58 between the stabilizing effect of solar radiation and the destabilizing effect of wind and
59 waves results in a shallow weakly stratified warm layer [16, 19]. (IV) *Afternoon entrainment*,
60 when solar radiation weakens and its stabilizing effect on turbulence is reduced. Turbulence
61 transits from a stable regime to an unstable regime, driven by a combination of wind, waves,
62 and destabilizing surface buoyancy flux. Strong entrainment occurs at the bottom of the
63 boundary layer, and the boundary layer deepens rapidly.

64 Existing Langmuir turbulence parameterizations are mostly based on scaling laws derived
65 from a large set of large-eddy simulations (LES) of Langmuir turbulence under steady surface
66 forcing in neutral [26], stable [16], or unstable [13] conditions in a quasi-equilibrium state.
67 These scaling laws describe the equilibrated response of Langmuir turbulence to steady

surface forcing. Under time variable forcing, these scaling laws are also expected to be applicable in situations where the surface forcing evolves relatively slowly as compared to the turbulence adjustment time scale, such that turbulence quickly reaches a quasi-equilibrium with the surface forcing. In the context of a diurnal cycle with relatively steady wind and wave forcings, this could happen at both the nighttime in phase (I) and daytime in phase (III), when the surface buoyancy flux varies relatively slowly. This may also apply to afternoon entrainment in phase (IV). Although the surface buoyancy flux transits from stable to unstable rapidly during phase (IV), intense convective turbulence develops because of the destabilizing surface buoyancy flux, which has a relatively short adjustment time scale. In other words, turbulence adjusts sufficiently quickly to the changing forcing, and thus a quasi-equilibrium state may be reached. Indeed, Langmuir turbulence parameterizations based on these scaling laws of quasi-equilibrium responses have fairly good skills in describing turbulent mixing under realistic transient surface forcings, especially in destabilizing surface conditions [15]. However, during morning detrainment in phase (II), surface buoyancy flux transits rapidly from unstable to stable conditions, yet the turbulence intensity is relatively weak and the turbulence adjustment time scale is relatively long. The turbulence may not be able to adjust sufficiently quickly to the rapidly changing surface forcing. Therefore, scaling laws derived from LESs under steady forcing that describe the quasi-equilibrium response may fail [16, 18].

In this study, we focus on the morning detrainment in phase (II). During this phase, the stabilizing solar radiation is rapidly changing, and the boundary layer turbulence is adjusting as a result but cannot reach equilibrium with the forcing. An accurate description of the turbulence state in this scenario requires a good understanding of the transient non-equilibrium response of Langmuir turbulence to continuously changing forcing, which is still lacking. To simplify the problem, here we study the response of Langmuir turbulence to an abrupt onset of surface heating. In addition, we assume that the heating is applied to the surface, in contrast to penetrative solar radiation in reality, which is absorbed in the upper few meters depending on the water turbidity [e.g., 27]. This is an idealized representation of the morning detrainment phase of a diurnal cycle, representing a first step towards a more comprehensive understanding of the transient non-equilibrium response of Langmuir turbulence to rapidly changing surface forcing. In particular, we conduct idealized LES experiments to study the transient evolution of the intensity and structure of Langmuir

100 turbulence after an abrupt onset of surface heating. We also contrast the transient response
101 of Langmuir turbulence with that of wind-driven shear turbulence to better understand the
102 effect of surface waves.

103 The remainder of this paper is structured as follows. Section II describes the configuration
104 of the LES model and the setup of the experiments. The time evolution of the intensity and
105 structure of Langmuir turbulence after the abrupt onset of surface heating are discussed and
106 compared with those of wind-driven shear turbulence in Section III. The impact of details
107 in the surface wave forcing is also explored. This paper ends with a brief discussion and the
108 main conclusions in Section IV.

109 II. METHODS

110 A. Model Description

111 The idealized LES experiments in this study are performed using Oceananigans (v0.91.5),
112 a Julia-based GPU-accelerated software package for numerical simulations of geophysical
113 fluid dynamics [28, 29]. Oceananigans utilizes a finite-volume spatial discretization scheme
114 and offers flexible configurations for LES through various combinations of subgrid-scale
115 (SGS) closures, advection schemes, and time-stepping methods. While relatively new, it
116 has gradually gained popularity in ocean modeling and has been used in solving various
117 problems in geophysical fluid dynamics, including modeling ocean surface boundary layer
118 turbulence under different forcing conditions [29–34].

119 Using the `NonhydrostaticModel` in Oceananigans, we solve the wave-averaged Boussi-
120 nesq equation, or the Craik-Leibovich (CL) equation [3, 4], written as a prognostic equation
121 for the Lagrangian velocity [35, 36],

$$\partial_t \mathbf{u}^L + (\mathbf{u}^L \cdot \nabla) \mathbf{u}^L = -(f \hat{\mathbf{z}} - \nabla \times \mathbf{u}^S) \times \mathbf{u}^L - \nabla p + b \hat{\mathbf{z}} + \mathcal{D}^u + \partial_t \mathbf{u}^S, \quad (1)$$

$$\nabla \cdot \mathbf{u}^L = 0, \quad (2)$$

$$\partial_t b + (\mathbf{u}^L \cdot \nabla) b = \mathcal{D}^b, \quad (3)$$

122 where f is the Coriolis parameter, $\hat{\mathbf{z}}$ is the vertical unit vector, p is the kinematic pressure,
123 b is the buoyancy, and \mathcal{D}^u and \mathcal{D}^b are the SGS diffusion of momentum and buoyancy. The
124 Lagrangian velocity $\mathbf{u}^L = \mathbf{u} + \mathbf{u}^S$ is the sum of the Eulerian velocity \mathbf{u} and Stokes drift

125 \mathbf{u}^S . Stokes drift for a monochromatic deep-water wave aligned with the wind direction
126 (x -direction) can be written as

$$\mathbf{u}^S(z) = \omega k A^2 e^{2kz} \hat{\mathbf{x}}, \quad (4)$$

127 where ω is the angular frequency, $k = \omega^2/g$ is the wavenumber, g is the gravitational
128 acceleration, A is the wave amplitude, and $\hat{\mathbf{x}}$ is a unit vector in x -direction. It is assumed
129 that \mathbf{u}^S is not affected by turbulent motions (thus prescribed following (4)) and remains
130 constant in time ($\partial_t \mathbf{u}^S = 0$). In this study, equations (1)-(3) are solved in Oceananigans using
131 a combination of the anisotropic minimum dissipation closure scheme [37], the fifth-order
132 WENO advection scheme, and the third-order Runge-Kutta time-stepping method with
133 adaptive time step according to the Courant-Friedrichs-Lowy condition. Sensitivity tests
134 using the ninth-order WENO advection scheme without an explicit SGS closure [e.g., 38]
135 show similar results, especially in the presence of Langmuir turbulence (not shown), which
136 increases the turbulent length scale and reduces the sensitivity of the resolved turbulent flow
137 to the SGS closure under stabilizing surface heating.

138 **B. Experimental Design**

139 Idealized LES experiments are guided by classical LES studies of Langmuir turbulence
140 [e.g., 6]. The surface wind forcing is given by a constant surface wind stress τ in the
141 x -direction with a friction velocity $u_* = \sqrt{\tau/\rho_o} = 6.1 \times 10^{-3}$ m s $^{-1}$, corresponding to
142 a surface wind speed of 5 m s $^{-1}$. Without surface wave forcing, this generates classical
143 wind-driven shear turbulence (hereafter denoted by ST). Typical Langmuir turbulence as
144 in Ref. [6] is generated with the same wind forcing, but is additionally driven by a steady
145 Stokes drift profile aligned with the surface wind according to (4) with wavenumber $k =$
146 $2\pi/60$ m $^{-1}$ and wave amplitude $A = 0.8$ m (hereafter denoted by LT). This yields a surface
147 Stokes drift $u_0^S \approx 6.8 \times 10^{-2}$ m s $^{-1}$, corresponding to a turbulent Langmuir number $\text{La}_t =$
148 $(u_*/u_0^S)^{1/2} \approx 0.3$, and an e-folding decay depth of the Stokes drift profile $\delta^S = 1/2k \approx 4.8$ m.
149 Additional experiments are carried out with different La_t but the same δ^S (LT2 and LT3),
150 and different δ^S but the same La_t (LT4 and LT5). The forcing parameters of all experiments
151 are summarized in Table I.

152 Under these horizontally homogeneous forcing conditions, wind-driven shear turbulence
153 or Langmuir turbulence quickly develops in the initial mixed layer of 33 m and erodes into

TABLE I. A summary of forcing parameters in the idealized LES experiments. Shown are the wavenumber k , wave amplitude A , turbulent Langmuir number La_t , e-folding decay depth of Stokes drift δ^S , initial mixed layer at the onset of surface heating h_i (defined by the depth where $\overline{w'b'}$ reaches its minimum), and surface heat fluxes.

	k (m $^{-1}$)	A (m)	La_t	δ^S (m)	h_i (m)	Q_0 (W m $^{-2}$)
ST	-	-	-	-	30.0	50, 100, 200, 400, 800
LT	$2\pi/60$	0.8	0.3	4.8	31.5	50, 100, 200, 400, 800
LT2	$2\pi/60$	0.533	0.45	4.8	31.0	50, 200, 800
LT3	$2\pi/60$	0.4	0.6	4.8	30.8	50, 200, 800
LT4	$2\pi/30$	0.476	0.3	2.4	30.8	50, 200, 800
LT5	$2\pi/15$	0.283	0.3	1.2	31.0	50, 200, 800

154 a constant stratification $\partial_z \bar{b} = N_0^2 = 10^{-4}$ s $^{-2}$ below. Here we use an overline $(\overline{\cdot})$ to denote
 155 the horizontal average, and later a prime $(\cdot)'$ to denote the deviation from the horizontal
 156 average. No surface buoyancy flux is imposed during the first 64 hours of these simulations,
 157 allowing wind-driven shear turbulence or Langmuir turbulence to develop fully before the
 158 abrupt onset of surface heating (defined as $t = 0$) with various strengths (Table I). A linear
 159 equation of state with a thermal expansion coefficient $\alpha = 2 \times 10^{-4}$ °C $^{-1}$ is assumed to link
 160 the surface heat flux Q_0 (defined as positive for surface warming) and the surface buoyancy
 161 flux $B_0 = -\alpha g Q_0 / c_p \rho_o$, where $c_p = 3991$ J kg $^{-1}$ °C $^{-1}$ and $\rho_o = 1026$ kg m $^{-3}$ are the
 162 specific heat and density of seawater. All experiments continue for another 48 hours after
 163 the abrupt onset of surface heating, and horizontally averaged fields and turbulent statistics
 164 are recorded at 3-minute intervals for subsequent analysis.

165 The Coriolis parameter is defined as $f = 2\pi/T_f$ with an inertial period $T_f = 57600$ s
 166 (16 hours), corresponding to a latitude of 48.6°N. To minimize the unwanted inertial oscillation
 167 associated with a sudden onset of the surface wind, which is unbalanced with the initial
 168 zero Lagrangian velocity, the surface wind stress is smoothly initialized in all simulations
 169 using a time-dependent scaling factor following Ref. [39],

$$F(t) = \begin{cases} \frac{1}{2} \left[1 - \cos \frac{\pi t}{T_0} \right], & 0 \leq t \leq T_0, \\ 1, & t > T_0, \end{cases} \quad (5)$$

170 where $T_0 = 86400$ s. This smooth onset of surface wind forcing effectively eliminates inertial
171 oscillation in the simulated horizontal velocity fields (see Appendix A). Note that iner-
172 tial oscillation is inevitably generated when an abrupt onset of surface heating is imposed.
173 However, this smooth onset of surface wind forcing during the spinup phase ensures that
174 no inertial oscillation preexists that may complicate the diagnosed response of Langmuir
175 turbulence to the abrupt onset of surface heating.

176 All simulations are conducted in a computational domain of $256\text{ m} \times 256\text{ m} \times 64\text{ m}$,
177 evenly discretized into $512 \times 512 \times 256$ grid boxes. The corresponding horizontal grid
178 spacing is $\Delta x = \Delta y = 0.5\text{ m}$ and the vertical grid spacing is $\Delta z = 0.25\text{ m}$. Testing
179 confirmed that this resolution is sufficient to resolve the energy-carrying eddies and resulting
180 turbulent fluxes due to wind-driven shear turbulence and Langmuir turbulence. While a
181 much higher resolution may be required to accurately describe small scale turbulence under
182 strong surface heating conditions in a quasi-equilibrium state, the resolution used here is
183 sufficient to describe the transient stage. The computational domain is doubly periodic in
184 the horizontal directions. A sponge layer nudging the velocity and buoyancy to their initial
185 values is used near the bottom to avoid the reflection of internal waves [29].

186 III. RESULTS

187 We focus our discussion of the transient response of Langmuir turbulence to abrupt onset
188 of surface heating in the LT case, contrasting the results with wind-driven shear turbulence
189 in the ST case wherever appropriate. We also examine the impact of details of the Stokes
190 forcing with the help of other LT cases.

191 A. An Overview of the Transient Response

192 As an example, Fig. 1 compares the time evolution of horizontally averaged and normal-
193 ized stratification, squared vertical shear of horizontal Lagrangian velocity, vertical velocity
194 variance, and vertical buoyancy flux in the LT and ST cases before and after the abrupt
195 onset of surface heating with $Q_0 = 200\text{ W m}^{-2}$. The near-surface stratification quickly
196 increases in response to the onset of surface heating in the ST case (Fig. 1e), blocking the
197 connection between the surface where wind forcing is applied and the layers below. This

198 results in a sudden drop in turbulence intensity near the surface (as indicated by the vertical
199 velocity variance $\overline{w'^2}$ in Fig. 1g). However, the intensity of near-surface turbulence partially
200 recovers quickly due to the development of strong velocity shear (Fig. 1f) as the momentum
201 input from the wind is now trapped in a much shallower surface warm layer, as well as
202 the buoyancy input from the surface heating which enhances the near-surface stratification
203 (Fig. 1h). This mechanism is well-understood, which explains the formation of the DWL
204 and a diurnal jet [21–23]. In contrast, in the LT case, the presence of Langmuir turbulence
205 inhibits the formation of strong stratification near the surface (Fig. 1a) that suppresses tur-
206 bulence. Therefore, the turbulence intensity does not exhibit a sudden drop as severely as
207 in the ST case (Fig. 1c) and the resulting warm layer is much deeper than in the ST case, in
208 which the momentum is more well mixed (Fig. 1b) and the surface heat flux is distributed
209 to a deeper depth (Fig. 1d).

210 Significantly different responses are also seen below the surface between the LT and ST
211 cases. With abrupt onset of surface heating, while the turbulence below the surface is
212 blocked from the surface wind forcing in the ST case and decays slowly with a time scale
213 that increases with depth (Fig. 1g), the decay of the turbulence below the surface in the LT
214 case occurs more rapidly and does not exhibit a strong dependence on depth (Fig. 1c). This
215 is probably due to the fact that, in the LT case, the surface and the layer below are more
216 well connected than in the ST case by coherent Langmuir turbulence that extends deeply
217 in the mixed layer. An abrupt surface heating weakens the driving force for these coherent
218 turbulence structures, leading to an immediate response to the changes of surface forcing
219 throughout the mixed layer. As a result, the decaying coherent Langmuir turbulence in the
220 LT case also contributes to a burst of vertical buoyancy flux that exceeds its equilibrium
221 value right after the abrupt onset of surface heating (Fig. 1d, around $t = 1$ h), which is not
222 seen in the ST case (Fig. 1h).

223 Within a few hours after the abrupt onset of surface heating, the destabilizing Langmuir
224 turbulence and stabilizing surface heating in the LT case reach a quasi-equilibrium, and the
225 mixed layer depth slowly transitions to its equilibrium value (black cross sign in Fig. 1d).
226 Note that the mixed layer depth in the heating phase is defined as the depth where $\overline{w'b'} =$
227 $0.05B_0$, in contrast to the initial phase before surface heating, where it is defined as the
228 depth where $\overline{w'b'}$ reaches its minimum (horizontal dotted lines in Fig. 1). This definition is
229 roughly consistent with the definition in Ref. [16], in which a linear fit of the $\overline{w'b'}$ profile was

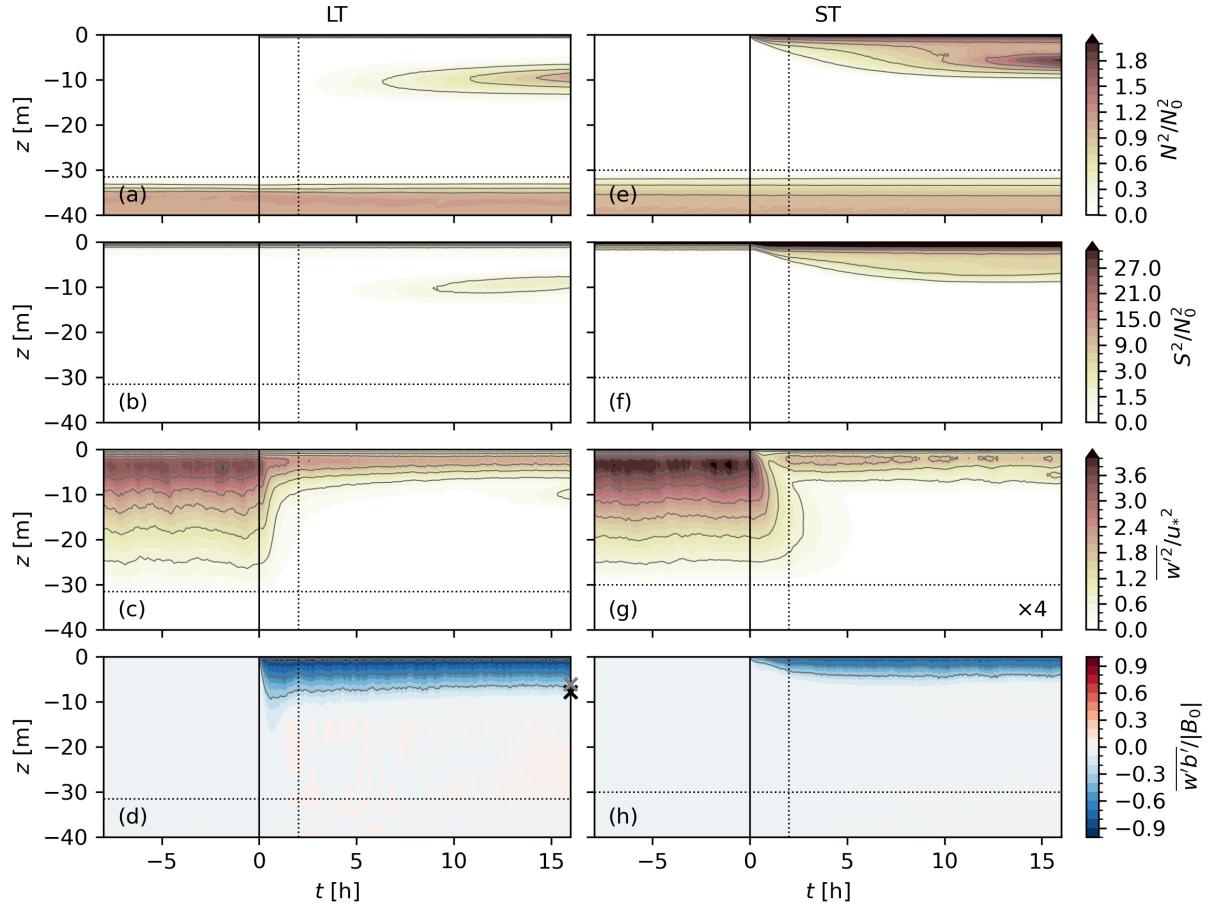


FIG. 1. Time evolution of the horizontally averaged (a,e) stratification $N^2 = \partial_z \bar{b}$ normalized by the stratification below the mixed layer N_0^2 , (b,f) squared vertical shear of horizontal Lagrangian velocity $S^2 = [(\partial_z \bar{u}^L)^2 + (\partial_z \bar{v}^L)^2]$ normalized by N_0^2 , (c,g) vertical velocity variance $\overline{w'^2}$ normalized by the surface friction velocity u_* , and (d,h) buoyancy flux $\overline{w'b'}$ normalized by the magnitude of the surface buoyancy flux $|B_0|$ in the (a-d) LT and (e-h) ST cases, before and after the abrupt onset of surface heating with $Q_0 = 200 \text{ W m}^{-2}$. Horizontal dotted lines mark the initial mixed layer depth $z = -h_i$ at the onset of surface heating and vertical dotted lines denote the time ($t = 2 \text{ h}$) when snapshots of w in Figs. 2 and 3 are taken. Black and gray cross signs in panel (d) mark the equilibrium mixed layer depth diagnosed in the simulation (see the text for the definition) and according to the scaling of Ref. [16], respectively. To enhance clarity, selected contours are shown (corresponding to the labeled values excluding 0.0 in the respective colorbar), a two-part color scale (two linear scales below and above 3.0) is used for S^2 , and $\overline{w'^2}$ in the ST case in panel (g) is multiplied by a factor of 4.

used and the mixed layer depth was defined as the depth at which the fitted line reaches zero. For reference, the equilibrium mixed layer depth according to the scaling in Ref. [16] is also marked (gray cross sign in Fig. 1d). The equilibrium mixed layer depth in our simulations, taken as the average over the last inertial period (from $t = 32$ h to $t = 48$ h), and the scaling in Ref. [16] are compared for all cases in Appendix B.

235 B. Suppression of Vertical Motions by Surface Heating

Fig. 2 shows snapshots of the simulated vertical velocity in the LT case at different depths at $t = 0$ h and $t = 2$ h, illustrating the effects of the abrupt onset of surface heating with different strengths on the intensity and structure of Langmuir turbulence. Characteristic structures of Langmuir turbulence [6] are clearly seen before the onset of surface heating, with stripes of downwelling regions roughly aligning with the wind and waves and slightly veering to the right due to the Coriolis force near the surface (Fig. 2a). These elongated downwelling regions merge and grow in size at deeper depths (Fig. 2e), veering further to the right and leaving a strong signature even near the base of the mixed layer (Fig. 2i). The deeply penetrating plumes of Langmuir turbulence [40] are reminiscent of convective plumes and have a similar impact on the anisotropy of turbulence [39]. Indeed, these plume-like structures contribute significantly to the vertical transport of turbulent kinetic energy (TKE) in the mixed layer [6], and distinguish Langmuir turbulence from wind-driven shear turbulence [39]. As shown in Fig. 3, which shows the snapshots of the simulated vertical velocity in the ST case, wind-driven shear turbulence exhibits smaller and more isotropic turbulence structures than Langmuir turbulence, especially below the surface.

Two hours of relatively weak surface heating with $Q_0 = 50 \text{ W m}^{-2}$ does not change the near-surface turbulence structure too much in the LT case (Fig. 2b). Even with $Q_0 = 200 \text{ W m}^{-2}$, the small scale stripes of downwelling regions are not very different from that before the heating (Fig. 2c). Only when the surface heating is sufficiently strong with $Q_0 = 800 \text{ W m}^{-2}$, these characteristic turbulence structures collapse (Fig. 2d). This is consistent with Ref. [41] which reported that the breakdown of Langmuir cells under surface heating occurs when the Hoenikker number $\text{Ho} = 2B_0/(ku_0^S u_*^2)$ reaches $\sim 1-2$. Here, $\text{Ho} = [0.18, 0.72, 2.90]$ for the LT case with surface heating of $Q_0 = [50, 200, 800] \text{ W m}^{-2}$.

Near the surface, the vertical shear of the Stokes drift is strong. So, there is direct

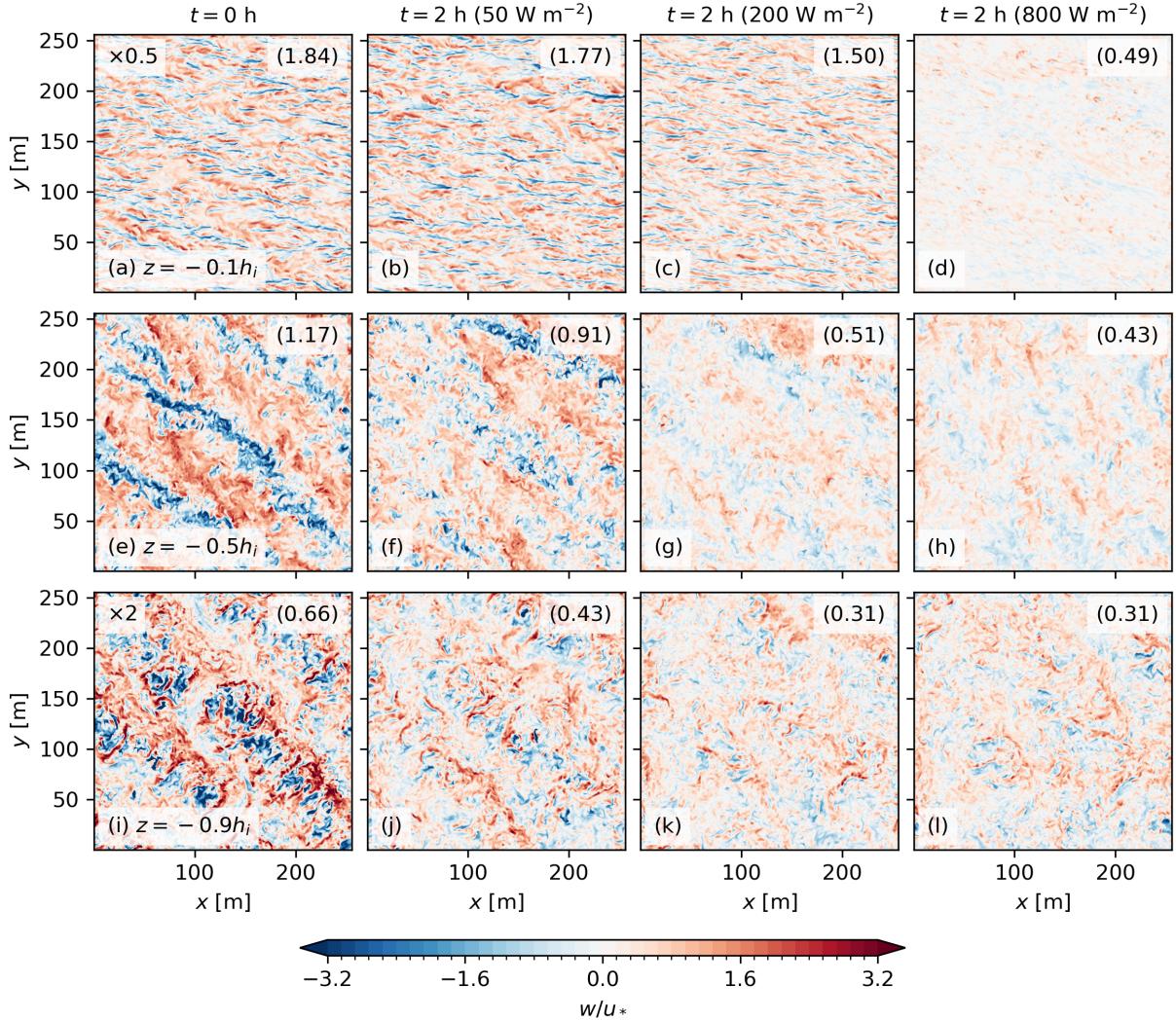


FIG. 2. Snapshots of normalized vertical velocity w/u_* illustrating the impact of abrupt onset of surface heating on the turbulence intensity and structure in the LT case. Different rows show snapshots at different depths: (a-d) $z = -0.1h_i$, (e-h) $z = -0.5h_i$, and (i-l) $z = -0.9h_i$. The left column (a,e,i) shows the snapshots before the onset of surface heating ($t = 0$ h), and the other three columns show the snapshots after 2 hours of surface heating for the cases of (b,f,j) $Q_0 = 50 \text{ W m}^{-2}$, (c,g,k) $Q_0 = 200 \text{ W m}^{-2}$, and (d,h,l) $Q_0 = 800 \text{ W m}^{-2}$. Numbers in parentheses in each panel show the root-mean-square value of the normalized vertical velocity. To highlight the turbulence structure, the vertical velocity in (a-d) and (i-l) are multiplied by 0.5 and 2, respectively, when plotting using the same color scale as (e-h).

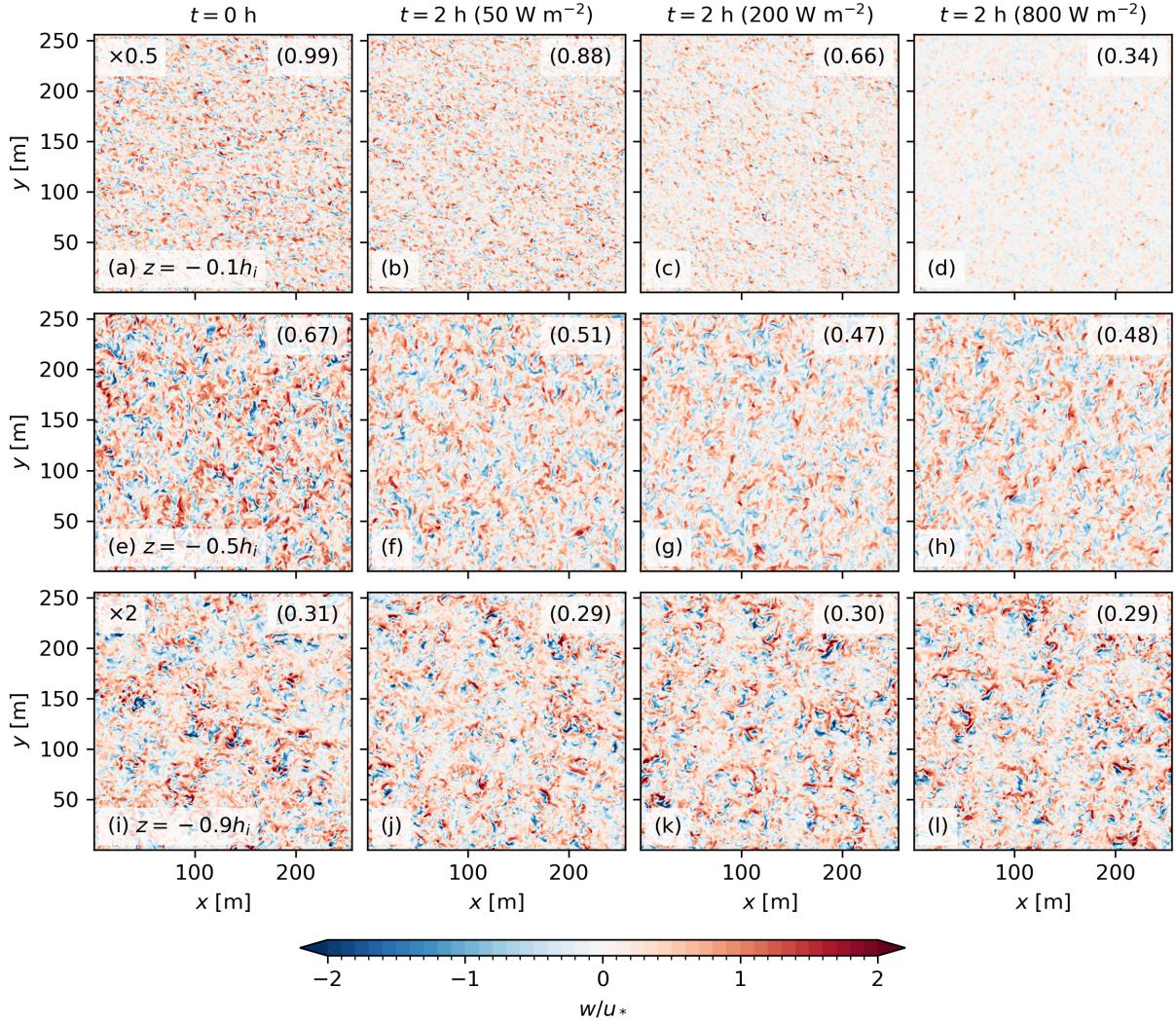


FIG. 3. Same as Fig. 2, but for the ST case.

competition between the destabilizing CL vortex force [3, 4] (more intuitively, the Stokes shear force [36]) and the stabilizing surface heating [41]. The CL instability makes the near-surface turbulence structures more resilient than wind-driven shear turbulence to the stabilizing effect of surface heating. For example, two hours of surface heating with $Q_0 = 200 \text{ W m}^{-2}$ reduces the root-mean-square (RMS) vertical velocity at $z = -0.1h_i$ by $\sim 18\%$ in the LT case (Fig. 2c), compared to over 33% in the ST case (Fig. 3c).

Below the surface, the turbulence intensity in the LT case is more prone to the effects of surface heating. The RMS vertical velocity is reduced by 56% at $z = -0.5h_i$ and 53% at $z = -0.9h_i$ after two hours of surface heating with $Q_0 = 200 \text{ W m}^{-2}$ (Fig. 2g,k). Further increasing the surface heating strength to $Q_0 = 800 \text{ W m}^{-2}$ does not change the results

270 too much (Fig. 2h,l). This is due to the fact that the driving force of the downwelling
271 plumes in Langmuir turbulence is the downward push by the Stokes shear force, which is
272 mainly confined near the surface where Stokes drift shear is strong [36]. Without stable
273 stratification, these downwelling plumes can penetrate deeply throughout the mixed layer
274 [40]. With sufficiently strong surface heating, the resulting stable stratification inhibits the
275 formation and penetration of these downwelling plumes, just as in the case of convective
276 turbulence. Turbulence away from the surface is effectively blocked from its driving force
277 and freely decays, while largely preserving its structure (e.g., elongated downwelling regions
278 similar to those before surface heating are still visible in Fig. 2g). In contrast, wind-driven
279 shear turbulence at depth is not as tightly connected to the surface forcing as Langmuir
280 turbulence. It also has a much smaller spatial scale than Langmuir turbulence. Therefore,
281 the decay of wind-driven shear turbulence below the surface is much slower (Fig. 3e-l).

282 These different responses to the abrupt onset of surface heating between Langmuir tur-
283 bulence and wind-driven shear turbulence can also be seen from the pre-multiplied energy
284 spectrum kE_w of the vertical velocity w in Fig. 4. Note that the energy spectrum E_w is
285 multiplied by the wavenumber k here, so the area below the curve kE_w reflects the energy
286 contributed by the wavenumber k on the logarithmic scale. After two hours of relatively
287 weak surface heating with $Q_0 = 50 \text{ W m}^{-2}$ (dashed lines in blue), changes in the pre-
288 multiplied energy spectrum are small in the ST case, with stronger reductions at $z = -0.5h_i$
289 (Fig. 4e) than at $z = -0.5h_i$ and $z = -0.9h_i$. In the LT case, however, reductions in
290 vertical velocity variance on relatively large scales are clearly seen at $z = -0.5h_i$ (Fig. 4b)
291 and more pronounced over all scales at $z = -0.9h_i$ (Fig. 4c). With stronger surface heating
292 $Q_0 = 200 \text{ W m}^{-2}$ (dashed lines in orange), the further reductions in vertical velocity vari-
293 ance on the energy-containing scales are greater near the surface and barely seen at deeper
294 depths in the ST case. In contrast, the further reductions are greater at $z = -0.5h_i$ and
295 $z = -0.9h_i$ than at $z = -0.1h_i$ in the LT case. In addition, these reductions occur at
296 all scales at deeper depths, in contrast to only large scales near the surface. The energy-
297 containing scales near the surface in the LT case correspond to the stripes of roll structures
298 that characterize Langmuir turbulence, which persist after two hours of surface heating with
299 $Q_0 = 200 \text{ W m}^{-2}$ (Fig. 2c). The collapse of Langmuir turbulence under strong surface heat-
300 ing with $Q_0 = 800 \text{ W m}^{-2}$ (Fig. 2d) is reflected in the pre-multipiled energy spectrum as
301 a reduction of vertical velocity variance over all scales near the surface, especially over the

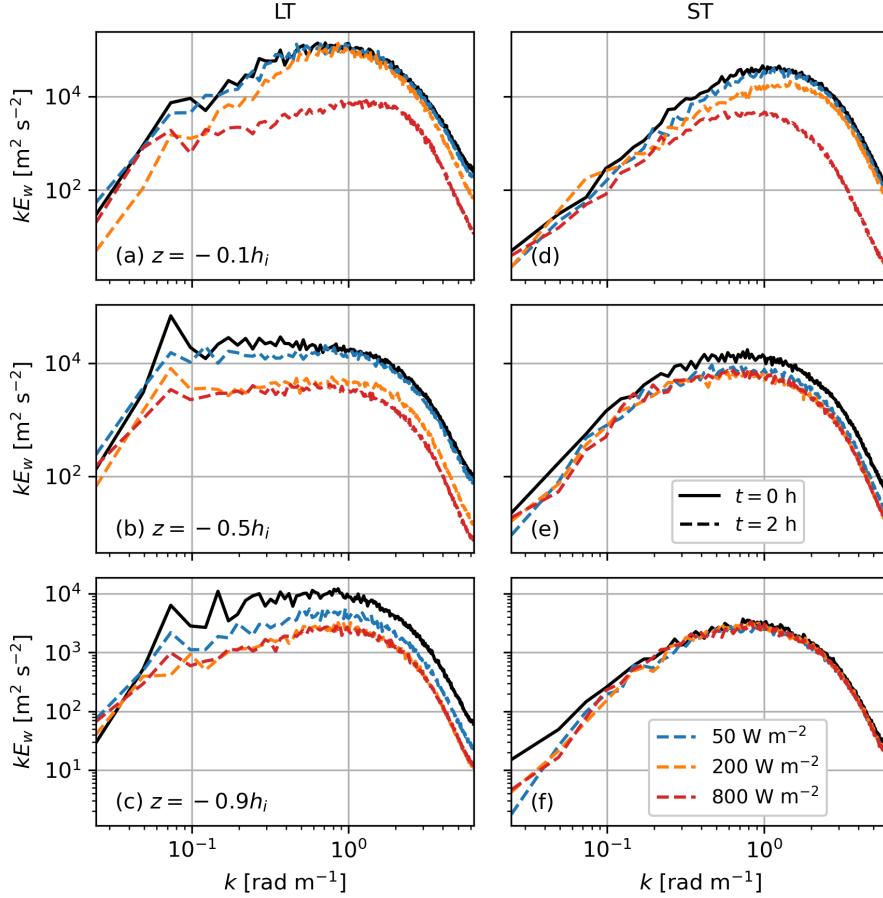


FIG. 4. Pre-multiplied energy spectrum of the vertical velocity w at (a,d) $z = -0.1h_i$, (b,e) $z = -0.5h_i$, and (c,f) $z = -0.9h_i$ for the (a–c) LT and (d–f) ST cases, corresponding to the vertical velocity snapshots in Figs. 2 and 3. Solid and dashed lines show the spectrum before ($t = 0$ h) and after ($t = 2$ h) the onset of surface heating, respectively. Different heating scenarios with $Q_0 = 50 \text{ W m}^{-2}$, $Q_0 = 200 \text{ W m}^{-2}$, and $Q_0 = 800 \text{ W m}^{-2}$ are shown in blue, orange, and red, respectively.

energy-containing scales (dashed line in red in Fig. 4a). At deeper depths, a stronger surface heating does not make much difference beyond $Q_0 = 200 \text{ W m}^{-2}$, suggesting a complete blocking of the driving force for the characteristic deeply penetrating plumes of Langmuir turbulence with intermediate surface heating. In the ST case, the small-scale vertical velocity variance near the surface continues to drop in response to the strong surface heating (dashed line in red in Fig. 4d), and no significant changes are observed at deeper depths.

308 C. Transient Response of TKE and Turbulence Anisotropy

309 Fig. 5 shows the transient response of TKE, defined as $e = \frac{1}{2} (\overline{u'^2} + \overline{v'^2} + \overline{w'^2})$, and its
 310 three components to the abrupt onset of surface heating with $Q_0 = 200 \text{ W m}^{-2}$ at different
 311 depths. Near the surface at $z = -0.1h_i$, the TKE in the LT case decays exponentially with
 312 time after the onset of surface heating (Fig. 5a). The dominance of $\overline{w'^2}$ and $\overline{v'^2}$ over $\overline{u'^2}$, which
 313 distinguishes Langmuir turbulence from wind-driven shear turbulence with $\overline{u'^2} > \overline{v'^2} > \overline{w'^2}$
 314 as shown in Fig. 5d, persists, consistent with the persistence of small-scale stripes of the
 315 downwelling regions in Fig. 2c. In the ST case, there is an initial decay of the TKE to less
 316 than 1/2 of its initial value at a rate faster than that of the LT case until around $t = 1 \text{ h}$,
 317 after which the TKE recovers quickly to around 3/4 of its initial value within an hour and
 318 stays stable afterward. The relative importance of its three components also remains roughly
 319 unchanged, consistent with the turbulence structures in Fig. 3c.

320 Below the surface at both $z = -0.5h_i$ and $z = -0.9h_i$, the TKE remains unchanged
 321 for a while before decaying exponentially over time. Consistent with Fig. 1c,g, the TKE
 322 remains unchanged longer in the ST case than in the LT case (Fig. 3e,f versus Fig. 3b,c),
 323 and at deeper depth than at shallower depth (Fig. 3c,f versus Fig. 3b,e). While the relative
 324 importance of the three components of the TKE remains roughly unchanged in the ST case
 325 (except the relative importance of $\overline{u'^2}$ and $\overline{v'^2}$, which may be related to the development of
 326 an inertial oscillation of the velocity shear), $\overline{w'^2}$ decays faster than the other two components
 327 in the LT case. At $z = -0.5h_i$, $\overline{w'^2}$ quickly stops dominating the TKE about half an hour
 328 after the onset of surface heating (Fig. 5b). At $z = -0.9h_i$, $\overline{w'^2}$ is the smallest before the
 329 onset of surface heating and becomes even smaller afterward (Fig. 5c). These changes in the
 330 anisotropy of the turbulence in the LT case below the surface are due to the faster decay
 331 of large-scale roll structures of Langmuir turbulence than small-scale turbulence, which are
 332 driven nonlocally from the surface where Stokes drift shear is strong, as shown in Fig. 2g.

333 To better understand the transient response of the TKE to the abrupt onset of surface
 334 heating, we also analyze the TKE budget. The budget equation for the TKE is [e.g., 6],

$$\partial_t e = \underbrace{-\overline{w' \mathbf{u}'_h} \cdot \partial_z \bar{\mathbf{u}}_h}_{P} - \underbrace{-\overline{w' \mathbf{u}'_h} \cdot \partial_z \mathbf{u}^S}_{P^S} + \underbrace{\overline{w' b'}}_{B} - \underbrace{-\partial_z \overline{w' p'}}_{T} - \underbrace{-\partial_z \overline{w' e}}_{D} - \varepsilon, \quad (6)$$

335 where $\mathbf{u}_h = [u, v]$ is the horizontal component of the velocity. The terms on the right-hand
 336 side are shear production (P), Stokes production (P^S), buoyancy production (B), pressure

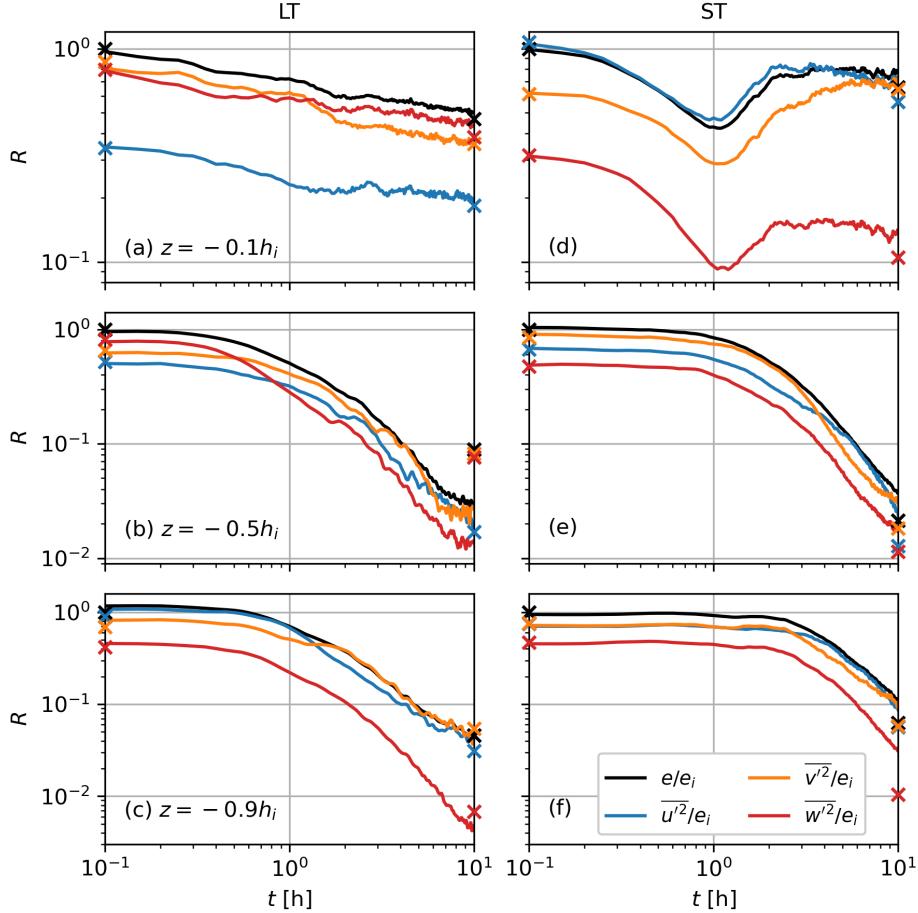


FIG. 5. Transient response of the TKE (black lines) and its three components (colored lines) to the abrupt onset of surface heating with $Q_0 = 200 \text{ W m}^{-2}$ at (a,d) $z = -0.1h_i$, (b,e) $z = -0.5h_i$, and (c,f) $z = -0.9h_i$ in the (a–c) LT and (d–f) ST cases. Cross signs at the left and right sides of each panel mark the mean values averaged over an inertial period before the onset of surface heating (from $t = -16 \text{ h}$ to $t = 0 \text{ h}$) and at the end of the simulations (from $t = 32 \text{ h}$ to $t = 48 \text{ h}$), respectively. All quantities are normalized by the initial mean TKE e_i before the heating. Note that both axes are in logarithmic scale.

correlation and TKE transport terms (T), and dissipation (D).

The transient evolution of these TKE budget terms at different depths in the LT and ST cases after an abrupt onset of surface heating with $Q_0 = 200 \text{ W m}^{-2}$ is shown in Fig. 6. Near the surface at $z = -0.1h_i$, Stokes production still dominates the TKE source in the LT case after the onset of heating, and shear production still dominates the TKE source in the ST case. The magnitude follows the trend of the TKE in Fig. 5. This suggests that Langmuir

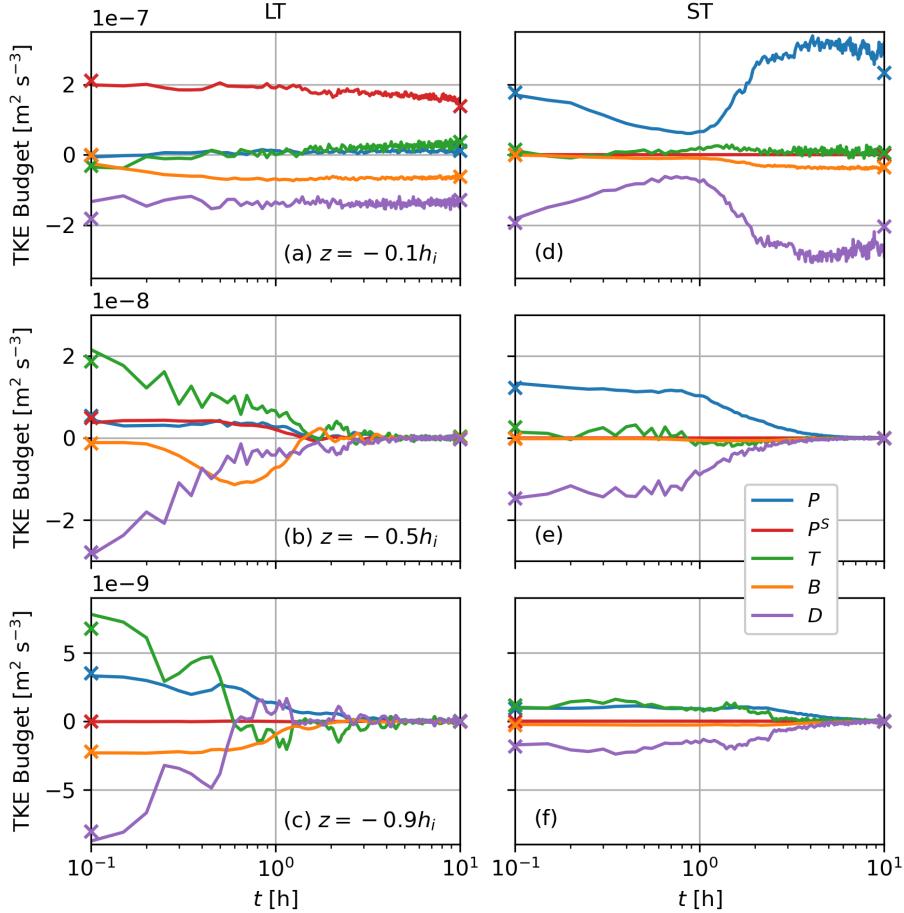


FIG. 6. Same as Fig. 5, but for the TKE budget terms in Eq. (6), shown by lines in different colors. Note that, unlike Fig. 5, the horizontal axis is in logarithmic scale but the vertical axis is in linear scale.

turbulence in the LT case and wind-driven shear turbulence in the ST case are weakened but not completely shut down by surface heating. Note that with $Q_0 = 800 \text{ W m}^{-2}$, the dominant TKE source in the LT case changes from Stokes production to shear production after about 1 hour of surface heating (not shown), consistent with the breakdown of Langmuir cells in Fig. 2d. Interestingly, the buoyancy production, which serves as a sink of TKE due to the stabilizing surface heating, is playing a much bigger role in the LT case than in the ST case (orange lines in Fig. 6a,d), especially immediately following the onset of surface heating (e.g., before $t = 1 \text{ h}$). This is due to the coherent rolls of Langmuir turbulence that effectively transport heat downward, inhibiting the formation of a shallow warm layer with strong stratification, which strongly suppresses turbulence in the ST case before strong

shear develops but not in the LT case. Another interesting feature in the TKE budget in the LT case is the transition of the TKE transport term from a sink before the surface heating to a source after (green line in Fig. 6a). This may result from a shoaling of the mixed layer, in which case the coherent rolls of Langmuir turbulence are restricted by the stratification and unable to transport TKE generated near the surface down to a deeper depth.

Below the surface at both $z = -0.5h_i$ and $z = -0.9h_i$, TKE transport still dominates the TKE source in the LT case, but its magnitude rapidly decays over time. Shear production plays an increasingly important role at $z = -0.9h_i$ as TKE transport decays faster than shear production (Fig. 6c). In the ST case, shear production dominates the TKE source at $z = -0.5h_i$ and TKE transport dominates at $z = -0.9h_i$. However, unlike the rapid decay of the TKE source in the LT case, shear production remains roughly unchanged for around 1 hour at $z = -0.5h_i$ and almost 3 hours at $z = -0.9h_i$ before decaying at a faster rate. The TKE transport also decays much slower than in the LT case. Note that the distinction of the buoyancy production term between the LT and ST cases is more pronounced than near the surface. In particular, there is a burst of $\overline{w'b'}$ at $z = -0.5h_i$ that peaks around $t = 0.6$ h (Fig. 6b) in the LT case, but not in the ST case. This burst of $\overline{w'b'}$ can be clearly seen in Fig. 1d, which extends over depths roughly from $z = -8$ m to $z = -18$ m. This is the result of the decaying downwelling plumes of Langmuir turbulence (e.g., Fig. 2g) that transport positive buoyancy due to surface heating downward (thus $\overline{w'b'} < 0$).

D. Impact of Surface Wave Forcing

The turbulent structure of Langmuir turbulence depends not only on the surface Stokes drift [42], but also on the decay length scale of Stokes drift [43]. To examine to what extent the transient response of Langmuir turbulence to abrupt surface heating as described in the previous sections is affected by different surface wave forcing, we compare the LT case with four additional Langmuir turbulence cases (Table I) with a weaker surface Stokes drift u_0^S (thus larger La_t , LT2 and LT3) or with a smaller decay length scale δ^S (LT4 and LT5). To assist in the comparison, we also show the results from an auxiliary run that represents the decay of convective turbulence [25]. The setup of this auxiliary run (hereafter denoted as CT) is the same as other runs, except that the initial turbulent flows before the abrupt onset of surface heating are driven by a steady surface cooling of 50 W m^{-2} without surface

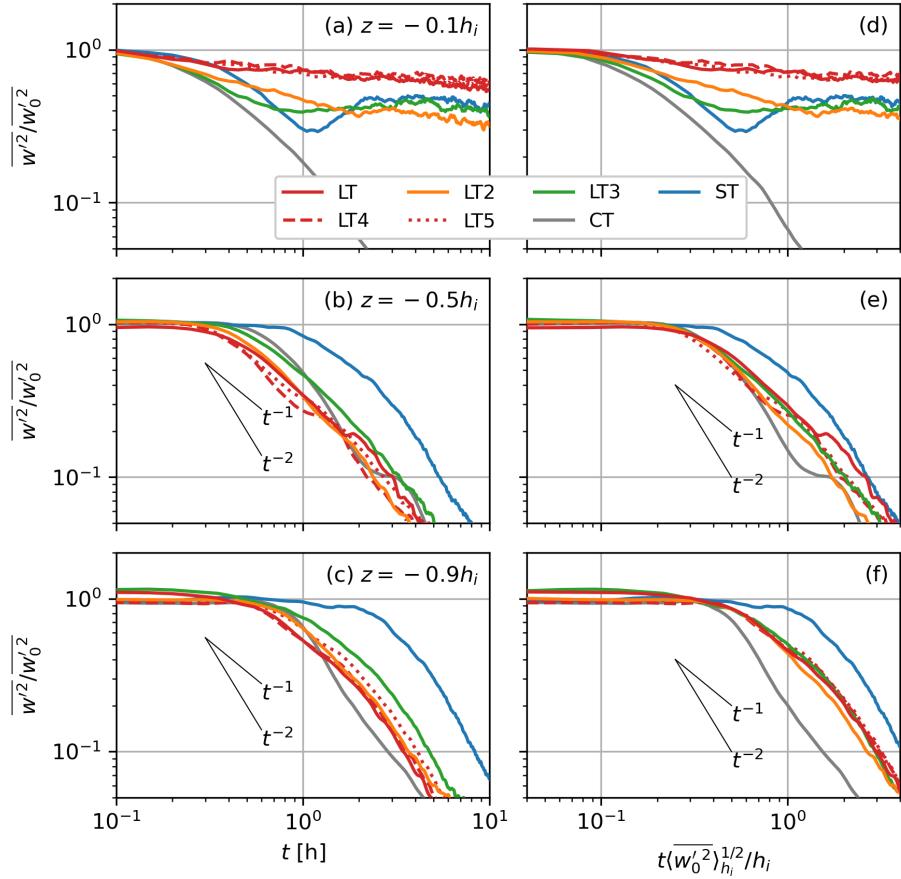


FIG. 7. Transient response of the vertical velocity variance $\overline{w'^2}$ to abrupt onset of surface heating with $Q_0 = 200 \text{ W m}^{-2}$ at (a,d) $z = -0.1h_i$, (b,e) $z = -0.5h_i$, and (c,f) $z = -0.9h_i$ in different cases with different surface wave forcing (colored lines). The $\overline{w'^2}$ is normalized by its mean value $(\overline{w'_0}^2)$ averaged over an inertial period before the onset of surface heating (from $t = -16 \text{ h}$ to $t = 0 \text{ h}$). The time in the right panels (d–f) are normalized by $\overline{w'_0}^2$ averaged over the initial mixed layer $\langle \overline{w'_0}^2 \rangle_{h_i}$ and h_i . Slopes in (b,c,e,f) show the power relation of t^{-1} and t^{-2} as a reference.

383 wind and waves. The initial depth of the mixed layer at the beginning of surface heating is
 384 $h_i = 35.8 \text{ m}$. For demonstration purposes, we only include the CT case with surface heating
 385 of $Q_0 = 200 \text{ W m}^{-2}$. Different magnitudes of surface heating result in almost identical
 386 response (decay) of convective turbulence except very close to the surface where strong
 387 stratification develops.

388 Fig. 7 compare the transient response of the vertical velocity variance $\overline{w'^2}$ to the abrupt
 389 onset of surface heating with $Q_0 = 200 \text{ W m}^{-2}$ in different cases. Near the surface at

390 $z = -0.1h_i$, a weaker surface Stokes drift leads to closer resemblance of the ST case. For
 391 example, the evolution of $\overline{w'^2}$ shows two distinct phases in the LT3 case, with a rapid decay
 392 before $t \sim 1$ h followed by a weak partial recovery, but not in the LT2 case, which shows
 393 more similarity to the LT case but faster decay due to weaker Langmuir turbulence (Fig. 7a).
 394 However, the initial rapid decay in the LT3 case is faster than in the ST case, more similar
 395 to the CT case. This suggests a faster decay of the larger-scale Langmuir cells, which show
 396 some similarities with the convective plumes. On the other hand, reducing the decay length
 397 scale of the Stokes drift in the LT4 and LT5 cases does not seem to change the decay rate
 398 of $\overline{w'^2}$ too much.

399 Below the surface at both $z = -0.5h_i$ and $z = -0.9h_i$, the evolution of $\overline{w'^2}$ shows similar
 400 correlations with surface wave forcing. With weaker surface Stokes drift, the decay of $\overline{w'^2}$
 401 starts later, showing more influences of wind-driven shear turbulence as in the ST case. The
 402 decay length scale of the Stokes drift changes the decay of $\overline{w'^2}$ in a subtler way. There is
 403 a noticeable delay of decay of $\overline{w'^2}$ at $z = -0.9h_i$ in the LT5 case compared to the LT case
 404 (Fig. 7c), probably due to the less coherent Langmuir cells of large scale in the LT5 case
 405 in which Stokes drift shear is restricted in a shallower region. Rescaling the time using the
 406 initial mixed layer averaged vertical velocity variance $\langle w'_0{}^2 \rangle_{h_i}$ and h_i reduces the spread of the
 407 transient response of Langmuir turbulence in different cases (Fig. 7d–f). This is especially
 408 true for the starting time of decay at $z = -0.5h_i$ and $z = -0.9h_i$, which is earlier than in
 409 the ST case but somewhat later than in the CT case. Unlike in the CT case, in which the
 410 decay of $\overline{w'^2}$ follows a t^{-2} power law [25], the decay of $\overline{w'^2}$ in the Langmuir turbulence cases
 411 below the surface seems to follow a t^{-1} power law initially (roughly $t < 2$ h), consistent with
 412 the results of Ref. [16], but then transits to the t^{-2} power law later. This transition to the
 413 t^{-2} power law may indicate a loss of the characteristic anisotropy of Langmuir turbulence
 414 at later times when the downwelling plumes start to resemble convective plumes in the CT
 415 case [39].

416 The above conclusions on the decay of Langmuir turbulence at $z = -0.9h_i$ can be ex-
 417 tended to cases with weaker or stronger surface heating, as shown in Fig. 8. Significantly
 418 slower decay of $\overline{w'^2}$ than in the cases with $Q_0 = 200 \text{ W m}^{-2}$ is seen in the LT, LT4 and LT5
 419 cases with $Q_0 = 50 \text{ W m}^{-2}$ (thin lines in red). In these cases, the surface heating is not
 420 strong enough to prevent the downwelling plumes of Langmuir turbulence from reaching the
 421 bottom of the mixed layer, so that the evolution of $\overline{w'^2}$ does not purely reflect the decay of

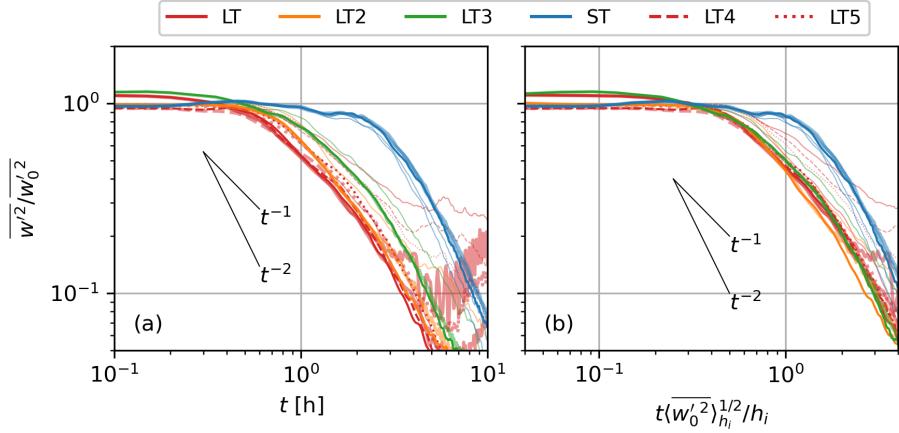


FIG. 8. Same as Fig. 7c,f, but for all cases in Table I. Thick and thin semi-transparent lines show cases with surface heating Q_0 larger and smaller than 200 W m^{-2} , respectively.

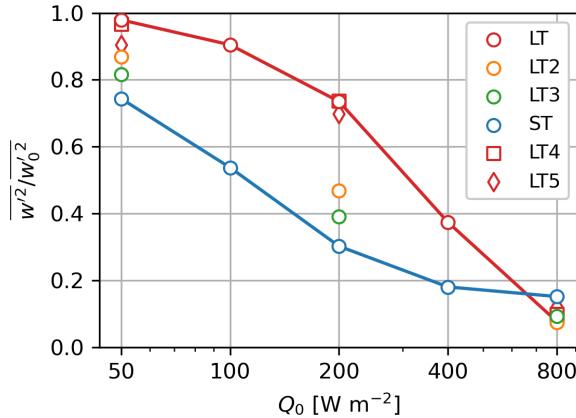


FIG. 9. The ratio of $\overline{w'^2}$ to its initial value before the onset of surface heating at $z = -0.1h_i$ and $t = 1 \text{ h}$ for all cases.

422 Langmuir turbulence. With $Q_0 = 800 \text{ W m}^{-2}$ (thick lines in red), intense internal waves are
 423 generated near the surface by inertially oscillating velocity shear as stratification increases,
 424 propagating downward and affecting $\overline{w'^2}$ at $z = -0.9h_i$ after around $t = 5 \text{ h}$. Rescaling the
 425 time using $\langle w_0'^2 \rangle_{h_i}$ and h_i seems to collapse the curves for all other Langmuir turbulence
 426 cases (Fig. 8b). This suggests that there may exist a simple scaling law to describe the decay
 427 of Langmuir turbulence, though it should be noted that the forcing conditions explored here
 428 are rather limited.

429 This rescaling of time does not seem to be as helpful in collapsing the curves at $z =$

430 $-0.1h_i$ as at deeper depths (Fig. 7a,d), suggesting the complex competition between Stokes
 431 production of TKE and buoyancy destruction (Fig. 6a). It is beyond the scope of this study
 432 to explore a scaling law to describe the complex relationship between Stokes production of
 433 TKE and buoyancy destruction at the surface, which requires a larger set of LES that span a
 434 much wider range of forcing conditions. However, using this limited set of LES, we can still
 435 qualitatively describe the effect of surface wave forcing on the initial response of Langmuir
 436 turbulence to an abrupt onset of surface heating near the surface.

437 Fig. 9 shows the ratio of $\overline{w'^2}$ to its initial value before the onset of surface heating at
 438 $z = -0.1h_i$ and $t = 1$ h for all cases. This is a measure of the initial decay of $\overline{w'^2}$ near
 439 the surface, which is not necessarily exponential, but certainly monotonic, for all cases (not
 440 shown). Except for the cases with $Q_0 = 800 \text{ W m}^{-2}$, $\overline{w'^2}$ decays the fastest in the ST
 441 case and the slowest in the LT case, with progressively stronger surface wave forcing (lower
 442 value of La_t) leading to progressively slower decay as shown by the LT2 and LT3 cases.
 443 The e-folding depth of Stokes drift δ^S also affects the initial decay of $\overline{w'^2}$, with shallower
 444 δ^S corresponding to faster decay, as shown by the LT4 and LT5 cases. This is probably
 445 because the driving force of Langmuir turbulence (Stokes drift shear) is more confined near
 446 the surface for shallower δ^S , and thus is more affected by surface heating. For the cases with
 447 $Q_0 = 800 \text{ W m}^{-2}$, $\overline{w'^2}$ decreases to less than 20% of its initial value at $t = 1$ h and shows less
 448 dependence on surface wave forcing. Interestingly, the decay of $\overline{w'^2}$ seems to level off beyond
 449 $Q_0 = 400 \text{ W m}^{-2}$ in the ST case, but not in the LT case, likely due to the breakdown of
 450 Langmuir cells in the latter which further decreases $\overline{w'^2}$.

451 IV. DISCUSSION AND CONCLUSIONS

452 In this study, we investigated the transient response of Langmuir turbulence to an abrupt
 453 onset of surface heating using a set of idealized LES. This complements previous studies
 454 on the equilibrium response of Langmuir turbulence under steady surface heating by, e.g.,
 455 Refs. [7, 16, 41]. We compared the results with the transient response of wind-driven shear
 456 turbulence under the same surface heating conditions. Near the surface, enhanced vertical
 457 mixing by Langmuir turbulence inhibits the formation of near-surface stratification, and
 458 the intensity of Langmuir turbulence decreases monotonically after the onset of surface
 459 heating. This is in contrast to wind-driven shear turbulence, which is initially suppressed

460 by the formation of strong near-surface stratification but later partially recovers due to the
461 development of strong shear in the near-surface warm layer. Under sufficiently strong surface
462 heating, Langmuir cells break down and the results become similar to the wind-driven shear
463 turbulence. These results are consistent with the existing literature on the dynamics of
464 DWL [19–23], the effect of Langmuir turbulence on DWL [18, 24], and the breakdown of
465 Langmuir turbulence under strong surface heating [41].

466 Below the surface, sufficiently strong surface heating effectively blocked the connection
467 between the deeply penetrating downwelling plumes due to Langmuir turbulence and their
468 driving force near the surface, where Stokes drift shear is strong, resulting in almost immedi-
469 ate decay of these large-scale coherent structures. This is similar to the decay of convective
470 turbulence, in which convective cells quickly decay after losing their driving force with the
471 onset of surface heating [25], and occurs much earlier (after a short steady period of ∼15–
472 30 minutes depending on the depth) than the decay of wind-driven shear turbulence (which
473 occurs after a steady period of ∼1–2 hours). With the help of coherent downwelling plumes
474 in Langmuir turbulence, the effect of changes in surface heating is felt much quicker at depth
475 than the wind-driven shear turbulence. But different from the decay of convective turbu-
476 lence, in which the vertical velocity variance decays at a rate following t^{-2} [25], the vertical
477 velocity variance of Langmuir turbulence decays at a rate initially following t^{-1} [16] and
478 later transitioning to t^{-2} . This transition of the decay rate seems to be robust in different
479 cases with different surface forcing. An investigation of its mechanisms and timing is left
480 for future research.

481 We also explored the impact of surface wave forcing on the transient response of Langmuir
482 turbulence by varying the surface value of Stokes drift (thus La_t) or its decay depth δ^S . With
483 progressively weaker surface wave forcing (larger La_t), the transient response of Langmuir
484 turbulence progressively approaches that of wind-driven shear turbulence. Shallower decay
485 depth of Stokes drift appears to result in a slightly earlier decrease of $\overline{w'^2}$ near the surface,
486 but a slightly later decay at depth, probably due to less coherent downwelling plumes in these
487 cases. Rescaling the time using the initial mixed layer averaged vertical velocity variance
488 $\langle \overline{w'_0}^2 \rangle_{h_i}$ and the initial mixed layer depth h_i seems to collapse the curves for the decay of $\overline{w'^2}$
489 at depth. Thus, existing scaling laws of $\langle \overline{w'_0}^2 \rangle_{h_i}$ for Langmuir turbulence such as Refs. [26, 44]
490 could potentially be useful. However, the significantly quicker response of $\overline{w'^2}$ to changes of
491 surface forcing in Langmuir turbulence than in wind-driven shear turbulence calls for further

492 investigation of the possible dependence on factors other than $\langle \overline{w'_0}^2 \rangle_{h_i}$ and h_i . The response
493 of $\overline{w'^2}$ near the surface is more complex due to the competition between destabilizing Stokes
494 shear force and stabilizing surface heating. It is beyond the scope of this study to explore a
495 scaling law that describes the near-surface behavior of Langmuir turbulence to the abrupt
496 onset of surface heating. A larger set of LES that covers a wider range of forcing conditions
497 is likely needed. In addition, penetrative solar radiation will surely affect the response of
498 Langmuir turbulence differently than surface heating [e.g., 16]. Since the penetration depth
499 of solar radiation is often of magnitude similar to the decay depth of Stokes drift, quantifying
500 the competition between the destabilizing Stokes shear force and stabilizing solar radiation
501 is even more challenging. Similar LES simulations with an abrupt onset of penetrative solar
502 radiation are currently underway to explore its effects.

503 Nevertheless, these results have important implications for parameterizing vertical mix-
504 ing due to Langmuir turbulence under transient forcing conditions, such as in the early
505 morning during a diurnal cycle as introduced in Section I. Existing Langmuir turbulence pa-
506 rameterizations based on the popular K-Profile Parameterizations [45] such as Ref. [13] (see
507 also a recent review in Ref. [15]) produce instantaneous response of turbulent fluxes to the
508 changes of surface forcing, assuming that the turbulence adjusts quickly into an equilibrium
509 state. As shown here, this assumption fails when the surface forcing changes sufficiently
510 fast. The transient response of Langmuir turbulence can occur over a time period of a few
511 hours or longer. Modifications will be needed in these parameterizations to account for the
512 transient response of the turbulence statistics to the varying surface forcing. One possi-
513 ble route forward may be to relax the equilibrium assumption by incorporating a transient
514 response time scale that depends on the forcing conditions. In addition, even Langmuir
515 turbulence parameterizations based on two-equation models such as Ref. [11], which evolve
516 prognostic equations of the TKE and a turbulent length scale (thus having memories of
517 previous turbulence state), may require modifications to account for the differential decay
518 rates of the three components of the TKE (thus the anisotropy of turbulence) in Langmuir
519 turbulence, perhaps by modifying the closure model for the pressure-strain terms (see, e.g.,
520 Ref. [46]). Exploration of these ideas in a Langmuir turbulence parameterization is left for
521 future research.

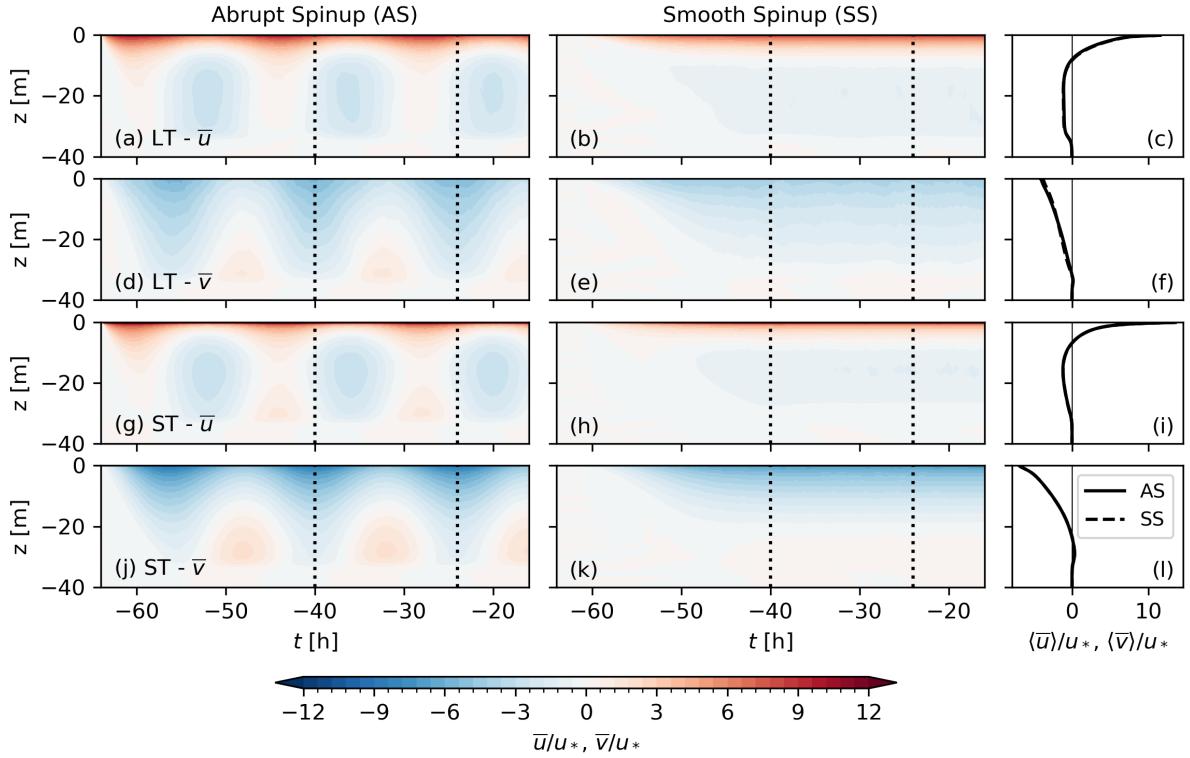


FIG. 10. Comparison between (a,d,g,j) an abrupt spinup (AS) with a sudden onset of the surface wind at the beginning of the simulation and (b,e,h,k) a smooth spinup (SS) with surface wind stress gradually increasing to the target value using a time-dependent scaling factor according to (5). The left two columns show the time evolution of horizontally averaged velocity \bar{u} and \bar{v} in the LT and ST cases. Solid and dashed lines in the right column show the mean profiles of velocity $\langle \bar{u} \rangle$ and $\langle \bar{v} \rangle$ for the abrupt and smooth spinup, respectively, averaged over the first inertial period after the smooth onset of surface wind stress (between dotted lines in the left two columns). The velocity components are normalized by the friction velocity u_* .

522 Appendix A: Abrupt Versus Smooth Spinup

523 The effect of a “Smooth Spinup” with gradually increasing surface wind stress by applying
 524 the scaling factor in Equation (5) is demonstrated in Fig. 10 by comparing to an “Abrupt
 525 Spinup” in which steady surface wind stress is applied at the beginning of the simulation
 526 at $t = -64$ h. While significant inertial oscillations of \bar{u} and \bar{v} are seen in both ST and LT
 527 cases with “Abrupt Spinup”, they are almost completely suppressed with “Smooth Spinup”.
 528 As shown in the right column, the mean profiles for \bar{u} and \bar{v} averaged over an inertial period

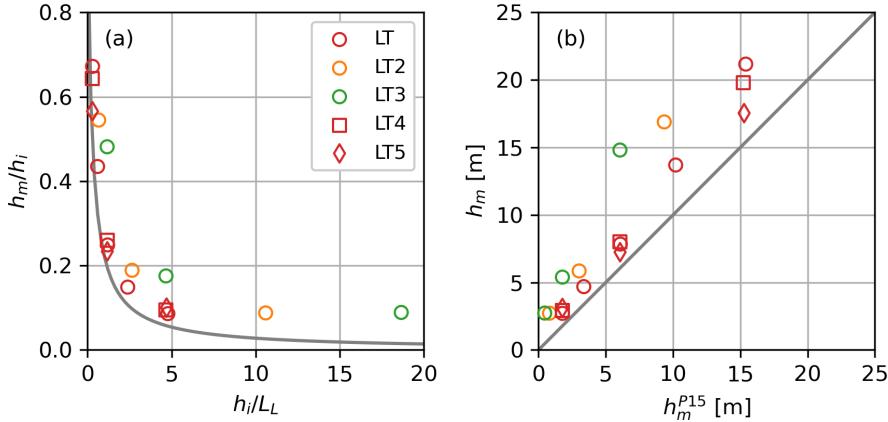


FIG. 11. Comparison between the equilibrium mixed layer depth h_m in our Langmuir turbulence simulations with the scaling in [16]. In panel (a), h_m/h_i is plotted against h_i/L_L (where $L_L = -u_*^2 u_0^S/B_0$), corresponding to Fig. 10a in [16], in which the gray curve shows the scaling according to their Equation (4). In panel (b), h_m is plotted directly against the value derived from the scaling in [16] h_m^{P15} .

529 are not changed by the different spinup strategies.

530 **Appendix B: Equilibrium Mixed Layer Depth**

531 The equilibrium mixed layer depth under the combined forcing of Langmuir turbulence
 532 and surface heating in our simulations is compared with the scaling according to Equation (4)
 533 in Ref. [16] in Fig. 11. As shown in panel (a), the equilibrium mixed layer depth in our
 534 simulations is generally consistent with the scaling in Ref. [16], but seems to be systematically
 535 deeper, which is better illustrated in panel (b). This is probably due to the much stronger
 536 surface heating (thus, smaller $L_L = -u_*^2 u_0^S/B_0$) used in our simulations than in Ref. [16]. In
 537 particular, the range of h_i/L_L covered in the set of LES here (up to 18) is much larger than
 538 that of Ref. [16] (less than 3). So, it is likely that the turbulence in our simulations with
 539 stronger surface heating may not have reached an equilibrium state after 48 hours of surface
 540 heating, which may explain the deeper h_m seen here. Given our focus on the transient
 541 response of Langmuir turbulence in the initial stage after the onset of surface heating, it
 542 may not be necessary to run these simulations into equilibrium, which may require much
 543 longer simulations.

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550 **DATA AVAILABILITY STATEMENTS**

551 The data that support the findings of this article are openly available [47].

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