

ECE110 ‘Condensed Notes’

Dear 2T3s (and upcoming froshes),

This document is basically my ‘condensed notes’, which is summary of whole course. It is based on professor Mojahedi’s lecture in 2018-2019 academic year. Hopefully it will guide your study for this course! **Please do not rely on this note though**, as curriculum can vary by year, and professors are doing examples which will aid your understandings on course materials. This note is written to show the concepts in relatively short time, not for giving examples. **Make sure to go to your own lectures!!**

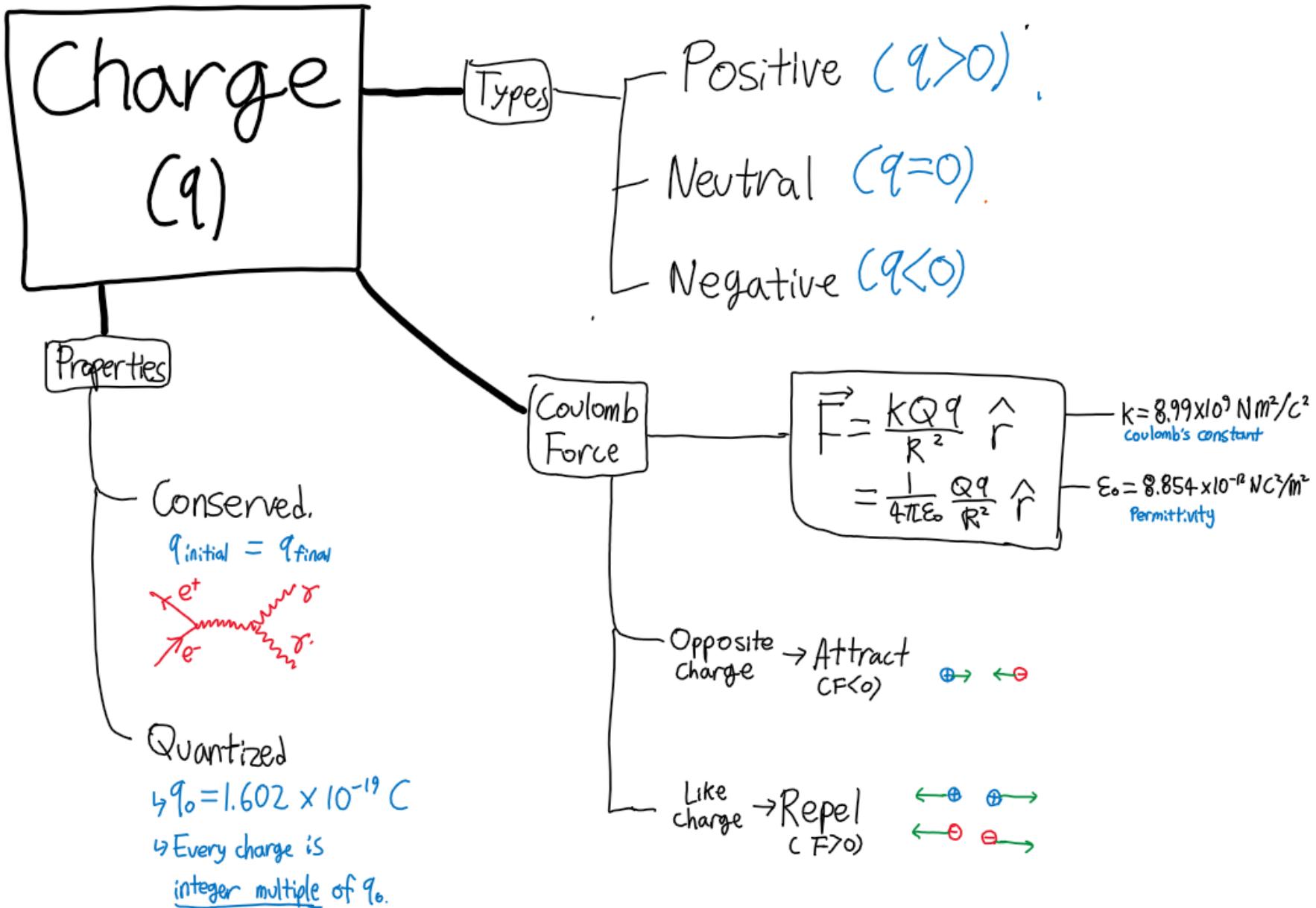
You will see most of concepts in second year and onward! First part of ECE110 is repeated with calculus 3 concepts in ECE221, and second part is repeated and continued in ECE212 (then 231). So DO NOT forget those concepts!!

The note is taken in OneNote and snipped afterwards, so some points might be blurry! Also don’t freak out with 50+ pages, I had to break my notes for clear images. Good luck with your second semester!!

Unit 1 Condensed Notes

Friday, January 18, 2019

1:18 AM



Unit 2 Condensed Notes

Friday, January 18, 2019

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$$\vec{F}_{q_1, q_2} = \frac{1}{4\pi\epsilon_0} \frac{q_1 q_2}{R^2} \hat{r}$$

$$\vec{E}_{q_2} = \frac{\vec{F}_{q_1, q_2}}{q_1} = \frac{1}{4\pi\epsilon_0} \frac{q_2}{R^2} \hat{r}$$

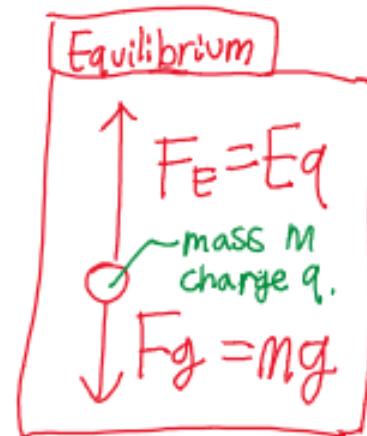
- Assume $q_1 > 0$

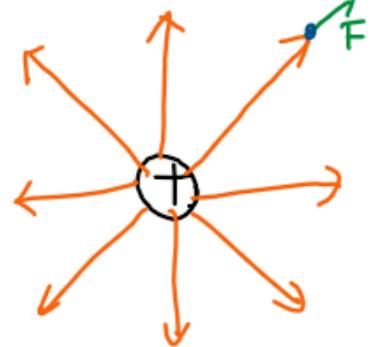
- q_1 is too small \rightarrow 'Test charge'

- Charge as 'particle'

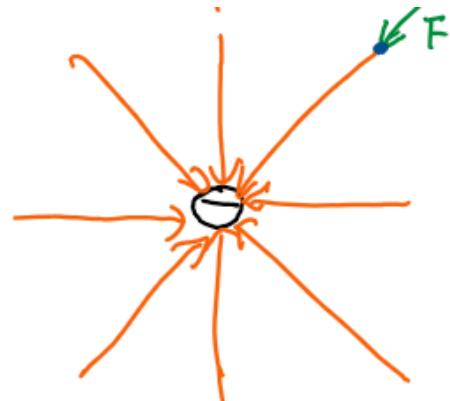
Particle motion

$$V = V_0 + at$$
$$S = S_0 + V_0 t + \frac{1}{2} a t^2$$
$$V^2 = V_0^2 + 2 a (X - X_0)$$
$$S = \frac{V_0 t + V t}{2}$$

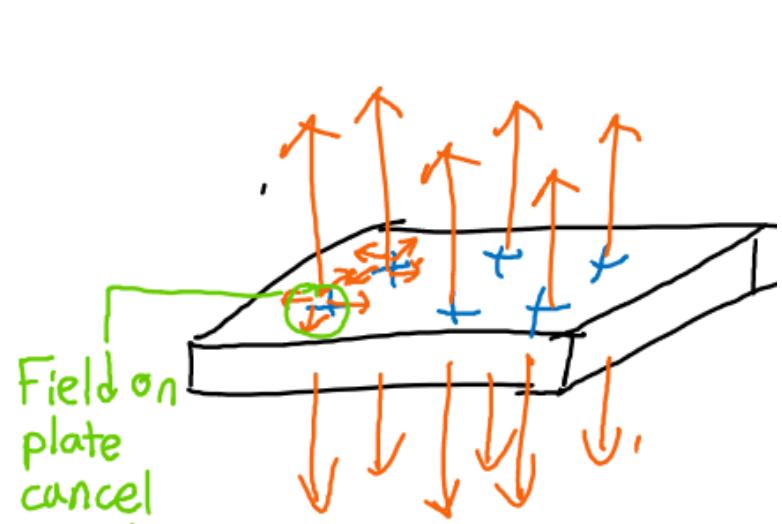




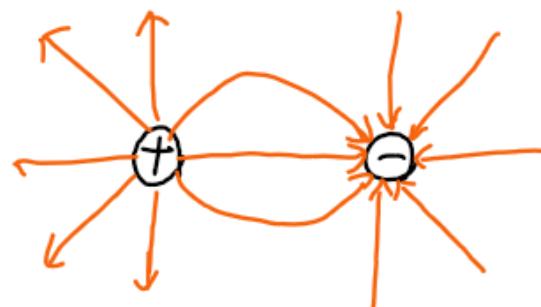
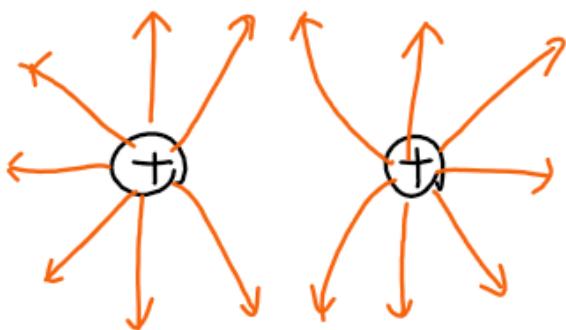
Start
from
positive

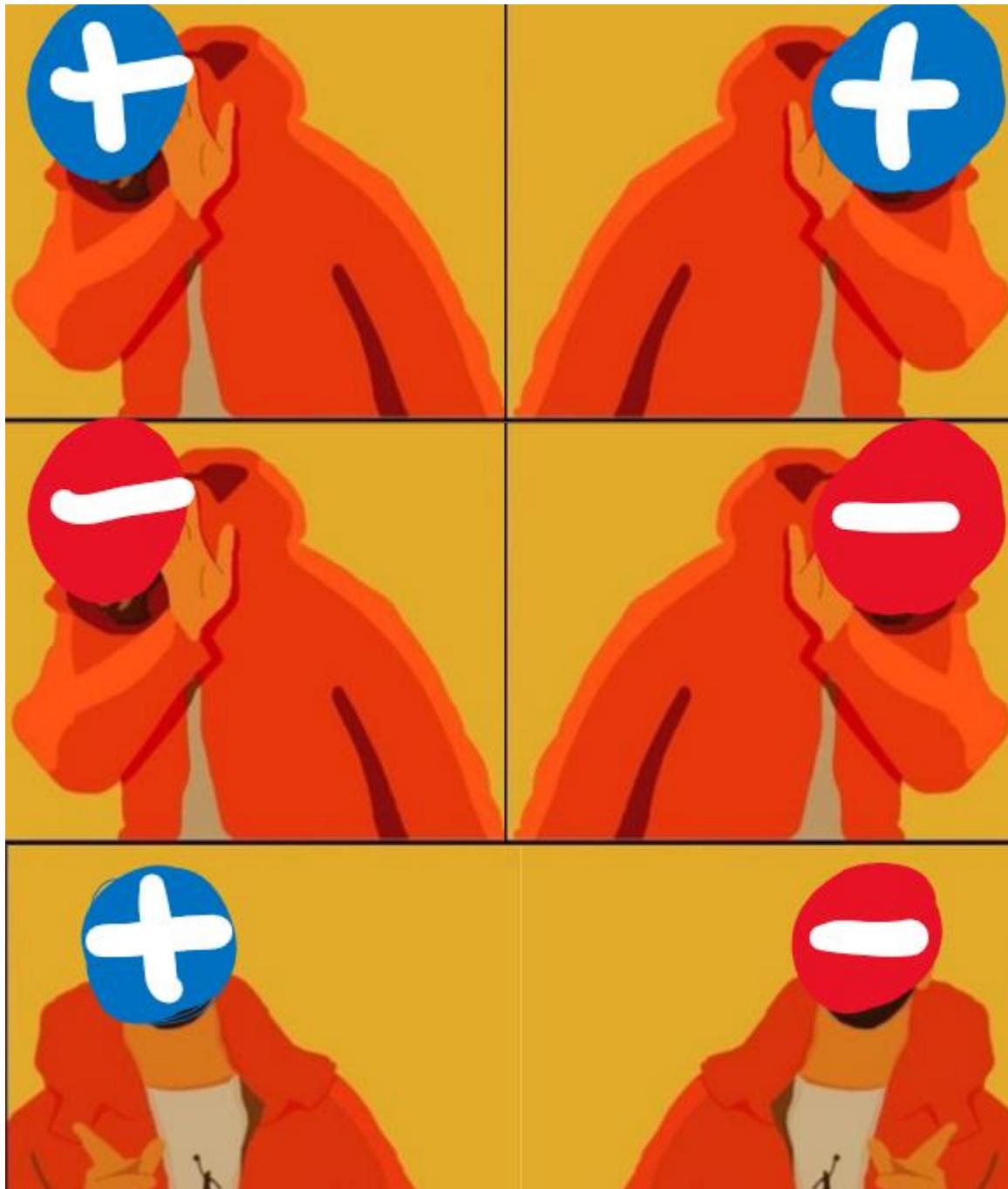


Field
Line



Field on
plate
cancel
out

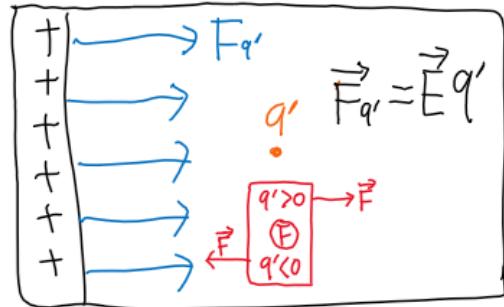




Unit 3 Condensed Notes

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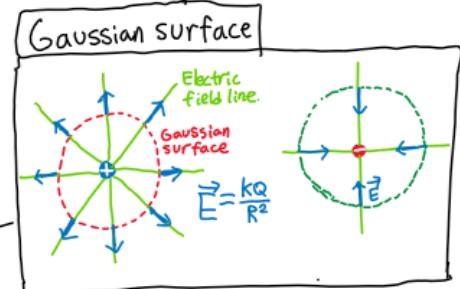
Gauss Law

$$\Phi = \iint_S \vec{E} \cdot d\vec{A} = \frac{q_{enc}}{\epsilon_0}$$

Flux

Surface integral
(Closed surface)

Enclosed charge



3.1 Electric Flux

Electric flux

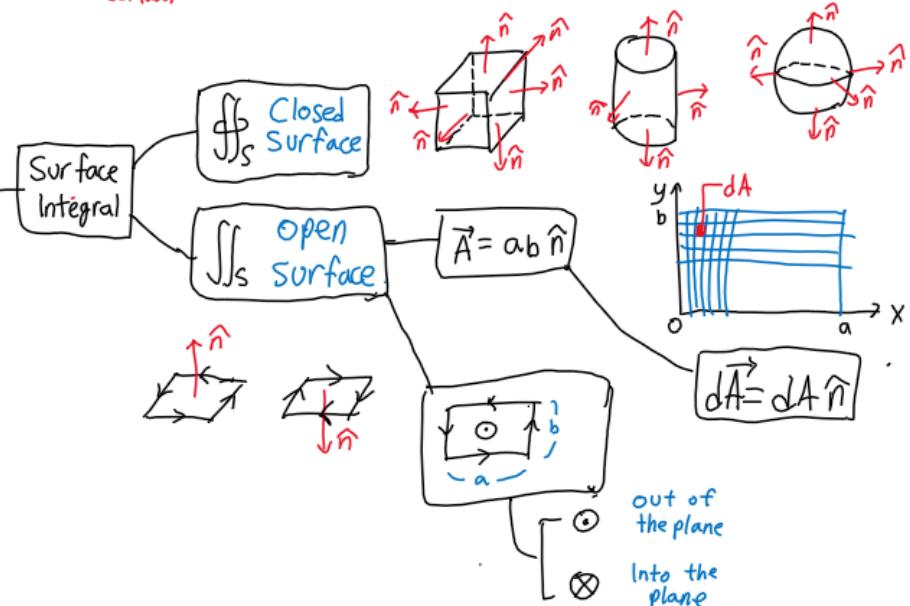
Flat surface Uniform field

$$\Delta \Phi = (E \cos \theta) \Delta A = \vec{E} \cdot \Delta \vec{A}$$

$$\Phi = \sum \text{(total flux)} \vec{E} \cdot \Delta \vec{A} = \int \vec{E} \cdot d\vec{A} = E A \cos \theta$$

$$\Phi_{net} = \iint_S \vec{E} \cdot d\vec{A}$$

(closed)



3.2

GAUSS Law

$$\epsilon_0 \Phi = q_{\text{enc}} (\text{enclosed})$$

Coulomb Force

$$\vec{F}_{q_0} = \frac{kQq}{R^2} \hat{r}$$

$$= \frac{1}{4\pi\epsilon_0} \frac{Qq}{R^2} \hat{r}$$

$$\vec{E} = \vec{E}_0 = \frac{1}{4\pi\epsilon_0 r^2} Q$$

$$q_{\text{enc}} = \epsilon_0 \oint_S \vec{E} \cdot d\vec{A}$$

Enclosed Charge
(q_{enc})

Total Charge.

Charge entered
into equation
with algebraic sign.

$q_1 = 2nC$	$q_3 = -2nC$
$q_2 = 3nC$	$q_4 = -5nC$

$$S_1 \rightarrow 2-2=0nC$$

$$\Phi = 0$$

$$S_3 \rightarrow 2-2-5=-5nC$$

$$\Phi < 0$$

$$S_2 \rightarrow 2+3=5nC$$

$$\Phi > 0$$

$$\oint_S \vec{E} \cdot d\vec{A} = \frac{Q_{\text{enc}}}{\epsilon_0}$$

Use RIGHT Gaussian surface!

$$\langle \vec{E}, \hat{n} \rangle = 0 \rightarrow \cos(\angle \vec{E}, \hat{n}) = 1$$

$$\oint_S \vec{E} \cdot d\vec{A} = \oint_S E dA \cos(\angle \vec{E}, \hat{n}) = \frac{Q_{\text{enc}}}{\epsilon_0}$$

$$E \oint_S dA = \frac{Q_{\text{enc}}}{\epsilon_0}$$

$$E = \frac{Q}{4\pi R^2 \epsilon_0}$$

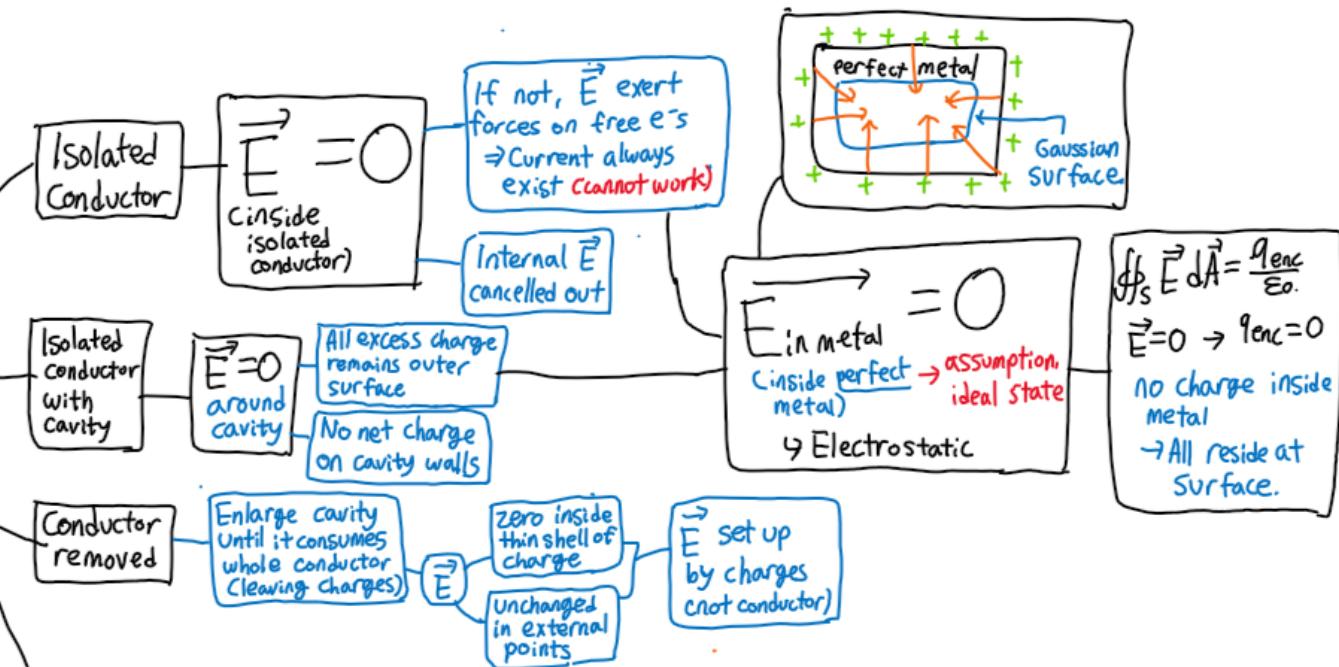
④ Q $q' \quad \vec{F}_{q'} = \vec{E} q'$

Point charge

- because of symmetry, electric field (\vec{E}) should be radial (same magnitude)

3.3

A charged isolated conductor



Charge Density

Linear density λ

$$q_{\text{tot}} = \int \lambda dx$$

$$= \int \lambda(x) dx$$

Surface density σ

$$q_{\text{tot}} = \iint \sigma dA$$

$$= \iint \sigma(x,y) dxdy$$

Volume ρ density

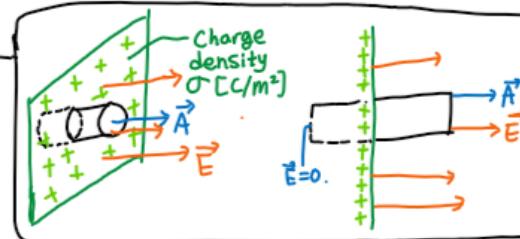
$$q_{\text{tot}} = \iiint \rho dV$$

$$= \iiint \rho(x,y,z) dxdydz$$

(QType)

Convert charge density into Q_{enc}

External Electric Field



$$\text{Let } \Phi = \int \int_S \vec{E} \cdot d\vec{A} \approx EA$$

$$\Phi = \frac{q_{\text{enc}}}{\epsilon_0}, \quad q_{\text{enc}} = \sigma A$$

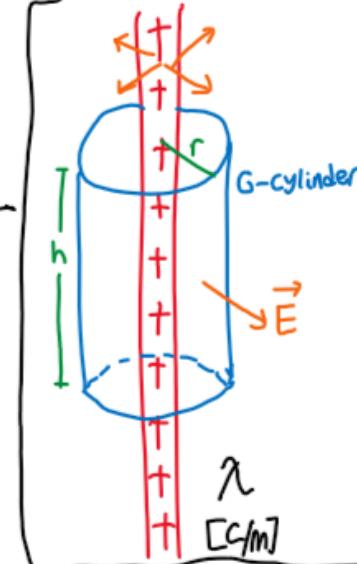
$$\Phi = EA = \frac{\sigma A}{\epsilon_0}$$

$$E = \frac{\sigma}{\epsilon_0}$$

Applying Gauss' Law

3.4

Cylindrical Symmetry



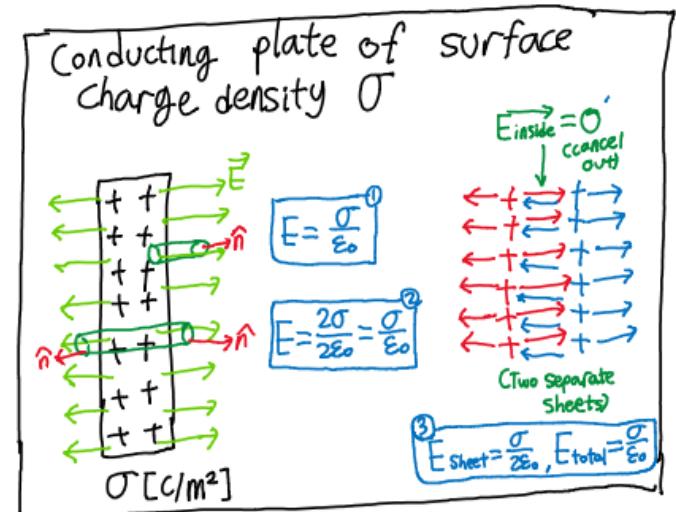
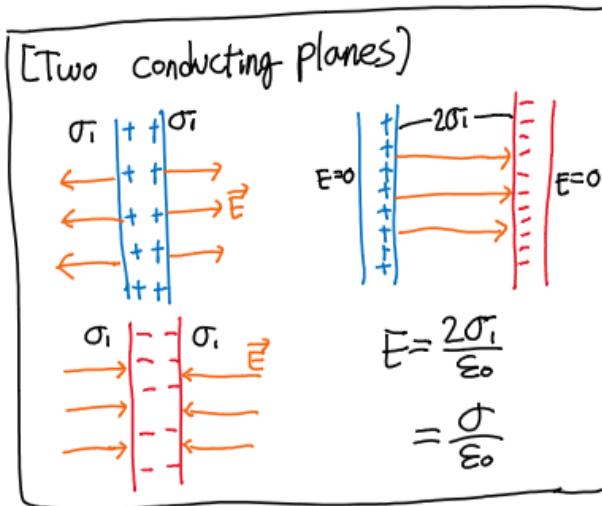
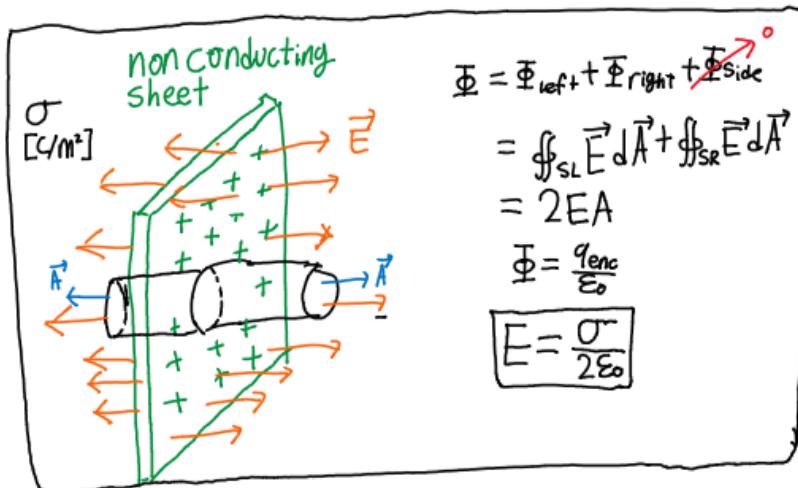
$$\epsilon_0 \oint_S \vec{E} \cdot d\vec{A} = q_{enc} \\ \approx \lambda h$$

$$\Phi_{tot} = \Phi_{top} + \Phi_{bot} + \Phi_{Side} \\ = \epsilon_0 E 2\pi r h = \lambda h$$

$$E = \frac{\lambda}{2\pi\epsilon_0 r}$$

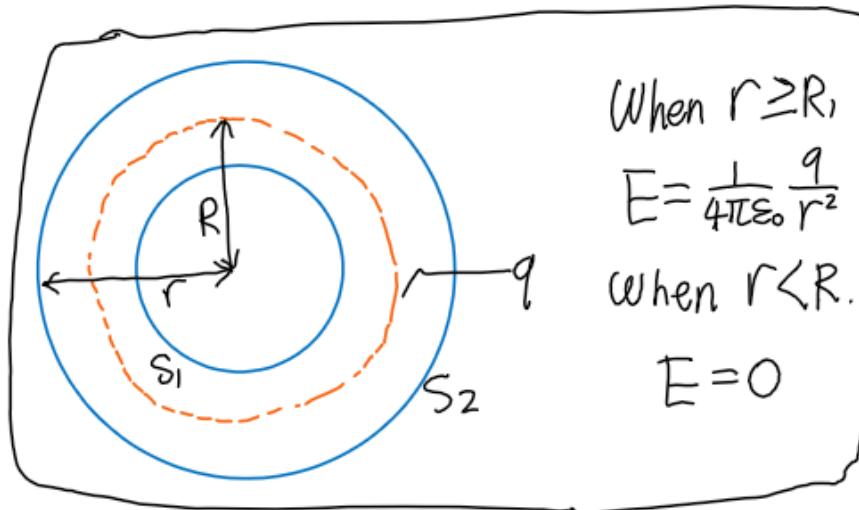
3.5

Planar Symmetry



3.6

Spherical Symmetry

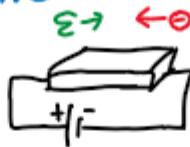


Internal Field	External Field
<p>$q_{enc} = q', \rho' [C/m^3]$</p> <p>Gaussian surface</p> $E = \frac{1}{4\pi\epsilon_0} \frac{q'}{r^2}$ $\rho' = \frac{q'}{\frac{4}{3}\pi r^3}$	<p>$\rho [C/m^3]$</p> <p>$q_{enc} = q$</p> <p>Gaussian surface</p> $E = \frac{1}{4\pi\epsilon_0} \frac{q}{r^2}$ $\rho = \frac{q}{\frac{4}{3}\pi r^3}$
<p>Charge is Uniformly spreaded</p> $\frac{q'}{\frac{4}{3}\pi r^3} = \frac{q}{\frac{4}{3}\pi R^3}$ $q' = q \frac{r^3}{R^3}$	$E = \frac{1}{4\pi\epsilon_0} \frac{q'}{r^2} = \frac{1}{4\pi\epsilon_0} \frac{q(r/R)^3}{r^2}$ $E = \left(\frac{q}{4\pi\epsilon_0 R^3} \right) r$ <p style="color: red;">External</p>

$$E = \frac{q}{4\pi\epsilon_0 r^2}$$

Conductors

metals - good conductors



- Charge move due to electrons

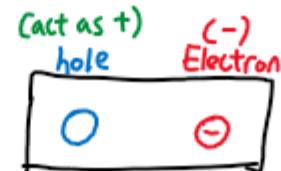
Shiny (reflect light)

Insulators

not good conductors
(e⁻'s tied)

Semiconductors

2 charge carriers



4-1

Electric Potential

Conservation of Energy

$$U_i + K_i + W_{\text{appl}} = U_f + K_f$$

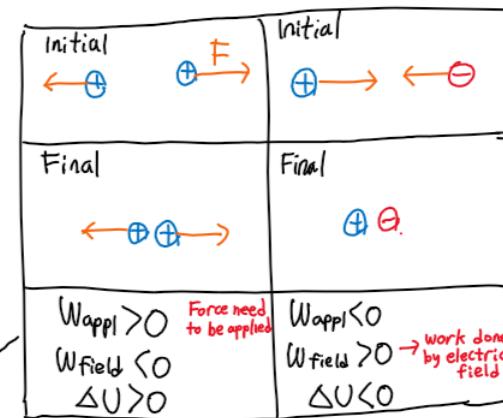
(If assume $K_i = K_f$, $W_{\text{appl}} = U_f - U_i = -W_{\text{field}}$)

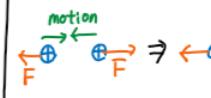
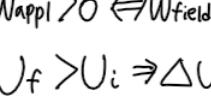
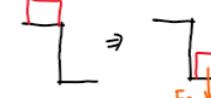
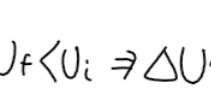
$$\Delta U = U_f - U_i = W_{\text{appl}} = -W_{\text{field}} \quad [J]$$

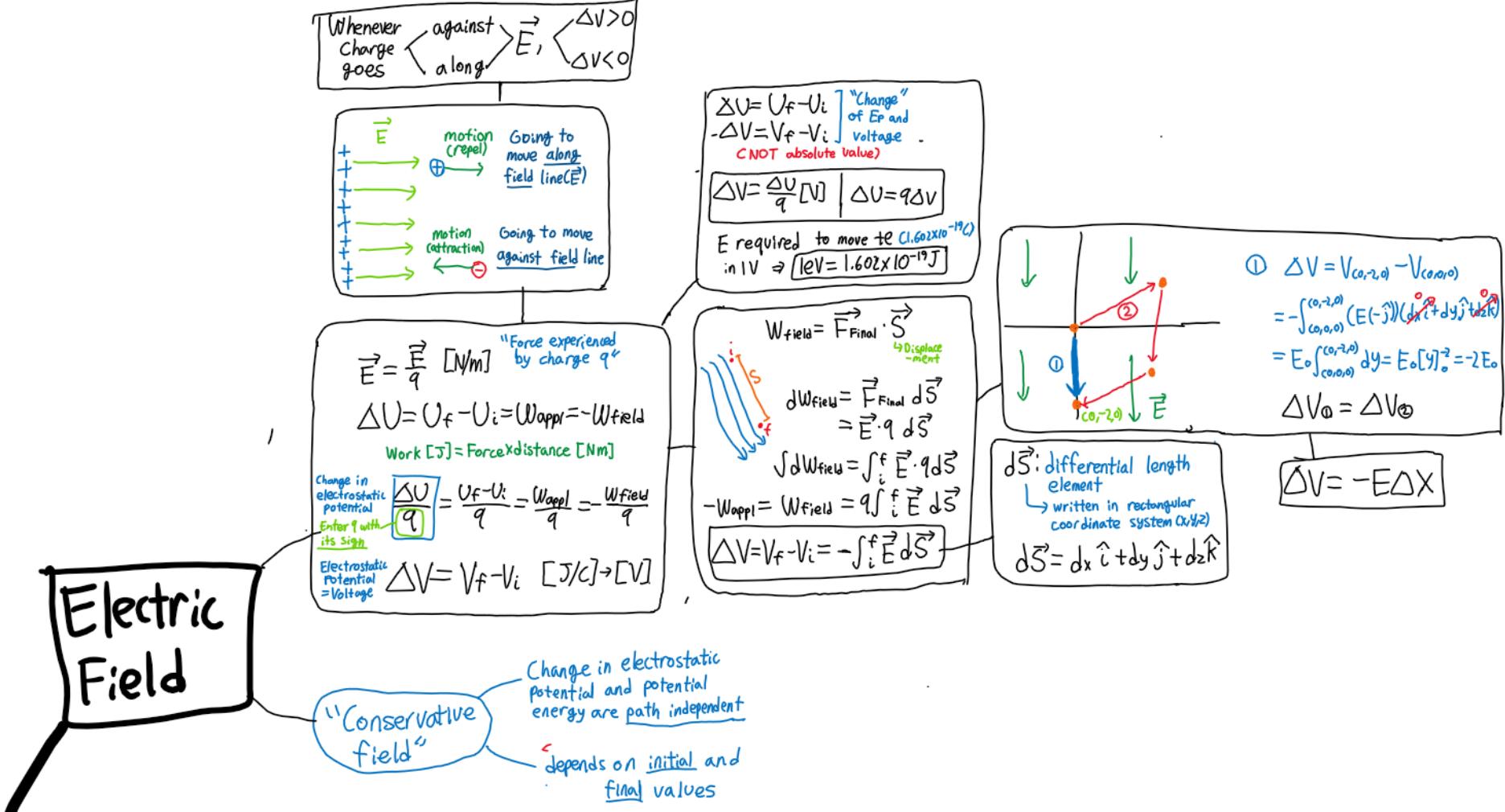
Change in potential energy
Potential Energy Final state
Potential Energy Initial state
Work done externally applied to system
Work done by field

$$\Delta U = U_f - U_i = W_{\text{applied}} = -W_{\text{field}} (= W)$$

applied work
Work done by field
Book convention



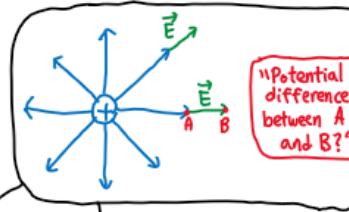
Potential	Gravitational	Electrical	Relationships
Work by external agent	initial  final 	initial  final 	$W_{\text{appl}} > 0 \Leftrightarrow W_{\text{field}} < 0$ $U_f > U_i \Rightarrow \Delta U > 0$
Work done by field	initial  final 	initial  final 	$W_{\text{appl}} < 0 \Leftrightarrow W_{\text{field}} > 0$ $U_f < U_i \Rightarrow \Delta U < 0$



4 - 2
4 - 3

Equipotential
Surfaces, electric
field and potential
due to charged particle

Potential Due to charged particle



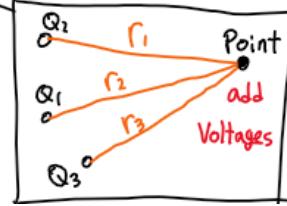
$$r_2 \rightarrow \infty \quad V_{r_2} \rightarrow 0 \quad V_{r_1} = \frac{Q}{4\pi\epsilon_0 r}$$

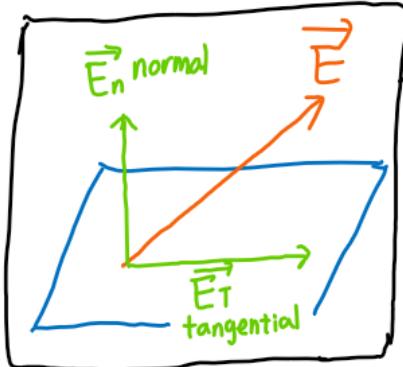
Charge → Positive → Positive voltage
negative → Negative voltage

$$\Delta V = V_f - V_i = - \int_i^f \vec{E} \cdot d\vec{S}$$
$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{r}$$
$$d\vec{S} = dr \hat{r}$$

(Spherical coordinate)

$$\begin{aligned}\Delta V &= - \int_i^f \vec{E} \cdot d\vec{S} = - \int_{r_1}^{r_2} \frac{Q}{4\pi\epsilon_0 r^2} dr \hat{r} \cdot \hat{r} \\ &= - \frac{Q}{4\pi\epsilon_0} \int_{r_1}^{r_2} \frac{1}{r^2} dr = - \frac{Q}{4\pi\epsilon_0} \left[-\frac{1}{r} \right]_{r_1}^{r_2} \\ &= \frac{Q}{4\pi\epsilon_0} \left(\frac{1}{r_2} - \frac{1}{r_1} \right) \\ \Delta V &= \frac{Q}{4\pi\epsilon_0} \left(\frac{1}{r_2} - \frac{1}{r_1} \right) = \frac{kQ}{r_2} - \frac{kQ}{r_1}\end{aligned}$$



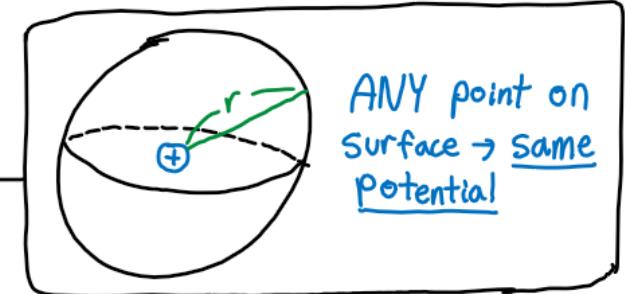


Equipotential Surfaces

$$V_r = \frac{Q}{4\pi\epsilon_0 r}$$

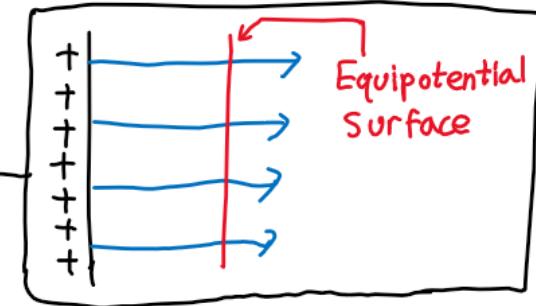
"Equipotential Surfaces"

Points in space that all points on equipotential surface has some electric potential or potential energy



ANY point on Surface \rightarrow Same potential

Always perpendicular to electric field



4-7

Electric Potential Energy of a system of charged particles

$$\Delta U = U_f - U_i \\ = q(V_f - V_i)$$

$$V = \frac{1}{4\pi\epsilon_0} \frac{q_2}{r}$$

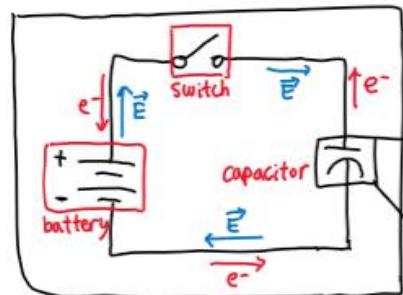
(cov)

$$U = q_1 \Delta V = \frac{q_1 q_2}{4\pi\epsilon_0 r}$$
$$U = \frac{q_1 q_2}{4\pi\epsilon_0 r} = \frac{k q_1 q_2}{r}$$

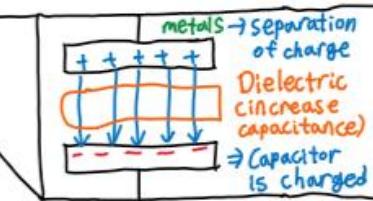
ASSUME
 $U_i = 0$
C assume q_1 located at
 $r = \infty$ initially)

5-1 5-2

Capacitance



Perfect Wire
↳ Conduit to charge (electron) to move.



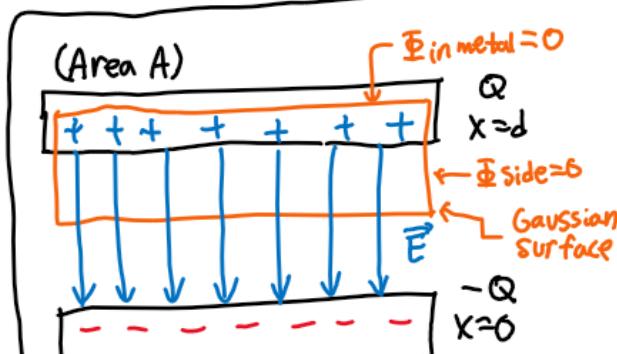
Capacitance = $\frac{Q}{V}$
NOT total charge.
↳ charge stored in one plate
↳ Potential Difference between two plates

$$C = \frac{Q}{V} [F]$$

Farad.

* If V is very large!

Parallel Plate Capacitor



Electric Field

$$\oint_S \vec{E} \cdot d\vec{A} = \frac{Q_{\text{enc}}}{\epsilon_0}$$

($Q_{\text{enc}} = Q$)

$$\oint_B \vec{E} \cdot d\vec{A} = \frac{Q}{\epsilon_0} \quad (\angle(\vec{E} \cdot d\vec{A}) = 0)$$

$$E \iint dA = EA = \frac{Q}{\epsilon_0}$$

$$E = \frac{Q}{A\epsilon_0} = \frac{C}{\epsilon_0}$$

$$\vec{E} = \frac{Q}{A\epsilon_0} (-\hat{i})$$

Potential Difference

$$V = - \int \vec{E} \cdot d\vec{S}$$

* E [V/m]

$$V_{x=d} - V_{x=0} = - \int_{x=0}^{x=d} \frac{Q}{A\epsilon_0} (-\hat{i}) dx \hat{i}$$

(remember $d\vec{S} = dx \hat{i} + dy \hat{j} + dz \hat{k}$)

$$V = \frac{Q}{A\epsilon_0} d \quad * \epsilon_0 = 8.854 \times 10^{-12} [\text{F/m}]$$

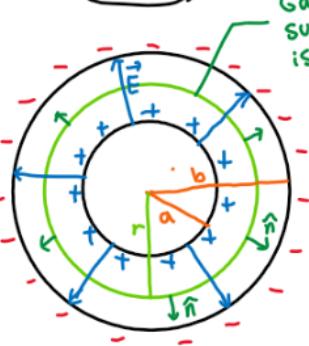
$$C_{\parallel} = \frac{Q}{V} = \frac{A\epsilon_0}{d} [F]$$

Let's say dielectric constant is 1. for now...

Cylindrical Capacitor



Gaussian surface is a cylinder



Electric Field

$$\oint \vec{E} \cdot d\vec{A} = \frac{Q_{\text{enc}}}{\epsilon_0} \quad (Q_{\text{enc}} = Q)$$

$$\oint_{\text{side}} \vec{E} \cdot d\vec{A} = \frac{Q}{\epsilon_0} \quad (\angle(\vec{E}, \hat{n}) = 0)$$

$$E \cdot 2\pi r L = \frac{Q}{\epsilon_0}$$

$$E = \frac{Q}{2\pi\epsilon_0 L r}$$

$$\vec{E} = \frac{Q}{2\pi\epsilon_0 L r} \hat{r}$$

$\hat{r} = \frac{\vec{r}}{|\vec{r}|}$
direction vector

* r is radius of Gaussian Surface

Potential Difference

$$V = V_{r=a} - V_{r=b} = - \int_{r=b}^{r=a} \vec{E} \cdot d\vec{S}$$

$d\vec{S} = dr \hat{r} + d\phi \hat{\phi} + dz \hat{z}$ $d\vec{S} = dr \hat{r}$

$$V = - \int_b^a \frac{Q}{2\pi\epsilon_0 L r} \hat{r} dr \hat{r}$$

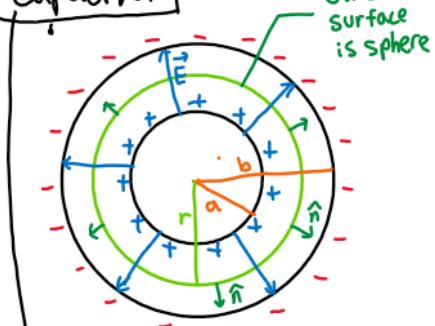
$$= - \frac{Q}{2\pi\epsilon_0 L} \int_b^a \frac{1}{r} dr$$

$$= - \frac{Q}{2\pi\epsilon_0 L} \ln \frac{a}{b}$$

$$V = \frac{Q}{2\pi\epsilon_0 L} \ln \frac{b}{a}$$

$$C_{\text{cyl}} = \frac{Q}{V} = \frac{2\pi\epsilon_0 L}{\ln \frac{b}{a}}$$

Spherical Capacitor



Electric Field

$$\oint_s \vec{E} d\vec{A} = \frac{Q}{\epsilon_0}$$

$$E \cdot 4\pi r^2 = \frac{Q}{\epsilon_0}$$

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2}$$

This is where $E = kQ/r^2$ from.

Potential Difference

$$V = V_a - V_b = - \int_{r=b}^{r=a} \vec{E} d\vec{s}$$

$$= - \int_b^a \left(\frac{Q}{4\pi\epsilon_0 r^2} \hat{r} \right) dr \hat{r}$$

$$= - \frac{Q}{4\pi\epsilon_0} \left[-\frac{1}{r} \right]_b^a$$

$$V = \frac{Q}{4\pi\epsilon_0} \left(\frac{1}{a} - \frac{1}{b} \right)$$

Capacitance

$$C = \frac{Q}{V} = \frac{4\pi\epsilon_0}{\frac{1}{a} - \frac{1}{b}}$$

$$C_{\text{sph}} = \frac{4\pi\epsilon_0 ab}{a-b} \quad (C > 0)$$

Capacitance of singular sphere

$$C = \frac{4\pi\epsilon_0 a}{1 - \frac{a}{b}}$$

$b \rightarrow \infty$

$$C_{\infty \rightarrow a} = 4\pi\epsilon_0 a$$

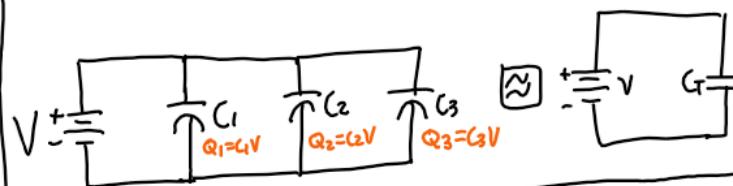
$$C_{\text{Singsph}} = 4\pi\epsilon_0 r$$

5-3

Capacitors in parallel/series

Parallel (||) Connection

Every capacitor has EQUAL voltage



$$Q_T = Q_1 + Q_2 + Q_3$$

$$\downarrow Q_T = C_T V$$

$$C_T = C_1 + C_2 + C_3$$

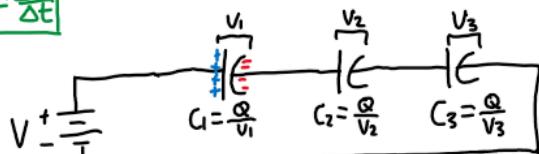
Series (↔) Connection

$$V_T = V_1 + V_2 + V_3$$

$$Q_T = Q_1 = Q_2 = Q_3$$

(Conservation of energy)

$$I = \frac{\Delta Q}{\Delta t}$$



$$V = \frac{Q}{C}$$

$$V_T = \frac{Q}{C_T} = \sum \frac{Q}{C}$$

$$\frac{1}{C_T} = \sum \frac{1}{C}$$

$$\frac{1}{C_T} = \frac{1}{C_1} + \frac{1}{C_2} + \frac{1}{C_3}$$



5-4

Energy stored in Electric Field

How much E can capacitor store?

$$\Delta V = \frac{\Delta U}{q}$$

$$\Delta U = q\Delta V \quad [C = \frac{q}{\Delta U} = \frac{\epsilon_0 A}{d}]$$

$$U = \int dU = \int qdV = \int CVdV$$

$$U = \frac{1}{2}CV^2 = \frac{1}{2}\frac{q^2}{C} = \frac{1}{2}qV$$

Energy Density (U)

$$U = \frac{U}{\text{Volume}} \quad [\text{J/m}^3]$$

$$U_{||} = \frac{U}{Ad}$$

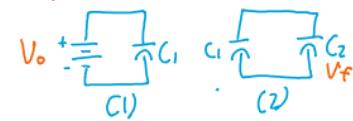
$$U_{||} = \frac{CV^2}{2Ad}$$

$$U_{||} = \frac{k\epsilon_0 A E^2 d}{2d Ad}$$

$$U_{||} = \frac{1}{2}k\epsilon_0 E^2 = \frac{1}{2}k\epsilon_0 \vec{E} \cdot \vec{E}$$

EX

Capacitor C_1 is charged by battery (V_0). Then disconnected and connected to uncharged capacitor C_2 . Final voltage of combination?



$$Q_{(1)} = Q_{(2)}, V_0 \neq V_f$$

$$C_1 V_0 = C_f V_f = C(C_1 + C_2) V_f$$

$$V_f = \frac{C_1}{C_1 + C_2} V_0$$

5-5

Capacitor with a dielectric

"How can we store more E in capacitor?"

$$C = \frac{\epsilon_0 A}{d}$$

- increase area
- decrease distance between 2 plates.

inefficient?
→ Put dielectric between two pieces of metals.

Dielectric constant

$K = \epsilon_r$ "Relative permittivity" → As a number:

$$K\epsilon_0 = 8.854 \times 10^{-12} \text{ F/m} \rightarrow \text{vacuum}$$

$K_{Si} = 12$
 $K_{Ge} = 16$
 $K_{Polyesterine} = 2.6$
 $K_{Vacuum} = 1$
($K > 1$ for anything else).

$$C_{\text{parallel}} = \frac{k\epsilon_0 A}{d}$$

$$C_{\text{cylindrical}} = \frac{k\epsilon_0 2\pi L}{\ln(\frac{b}{a})}$$

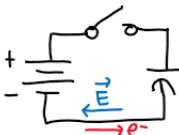
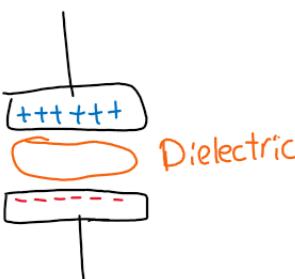
$$C_{\text{spherical}} = \frac{k\epsilon_0 4\pi ab}{a-b}$$

$$F = \frac{1}{4\pi k\epsilon_0} \frac{q_1 q_2}{r^2}$$

$$E = \frac{Q}{4\pi k\epsilon_0 r^2} = \frac{J}{K\epsilon_0}$$

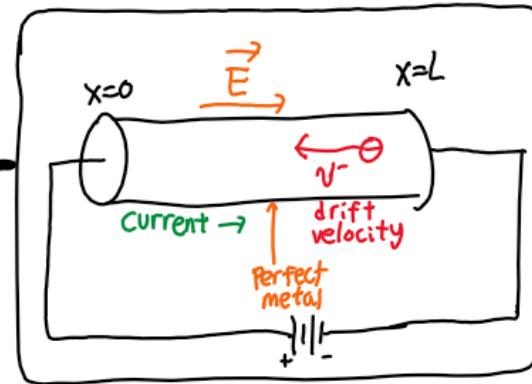
$$V = \frac{Q}{4\pi k\epsilon_0 r}$$

$$U = \frac{Q^2}{4\pi k\epsilon_0 r}$$



6-1 | 6-3 | 6-4

Electric current, Resistance and Ohm's Law



$$C = \frac{Q}{V} = \frac{A\epsilon_0}{d} [F]$$

$$R = \frac{V}{I} [\Omega] \text{ ohm}$$

$$I = \frac{dQ}{dt} [A] \text{ Ampere}$$

$(\int dQ = \int I dt)$

I - Current (movement of charges)
Doesn't have to be dependent on time

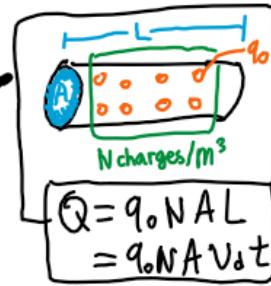
6-2 | 6-3

Resistivity and Current density

$$I = \iint \vec{J} d\vec{A} = JA$$

$$J = \frac{I}{A} \text{ [A/m}^2\text{]}$$

Current density
add up
(never cancel out)



$$I = \frac{Q}{t} = q_0 N A V_d t$$

$$Q = q_0 N A L = q_0 N A V_d t$$

$$\vec{J} = N q_0 \vec{V}_d$$

Current density
[A/m²]
Total charge per volume

Elementary charge
drift speed

$$\rho = \frac{|\vec{E}|}{|\vec{J}|} \text{ [\Omega m]}$$

ρ - Resistivity
 \vec{J} - Current density [A/m²]
 \vec{E} - Electric Field [V/m]

$$\vec{J} = \frac{1}{\rho} \vec{E} = \sigma \vec{E}$$

$$\sigma = \frac{1}{\rho} \text{ [S/m]}$$

conductivity

$$R = \frac{V}{I} = \frac{-\int_L^0 \vec{E} \cdot d\vec{s}}{JA}$$
$$= \frac{-\int_L^0 E \hat{i} \cdot d\hat{x} \hat{i}}{JA} = \frac{El}{JA}$$

$$R = \frac{El}{JA} = \rho \frac{l}{A}$$

6-5

Power in electric circuits

$$dU = q dV$$

$$dV = R dI$$

$$\int^U dU = \int q R dI$$

$$U = q R I$$

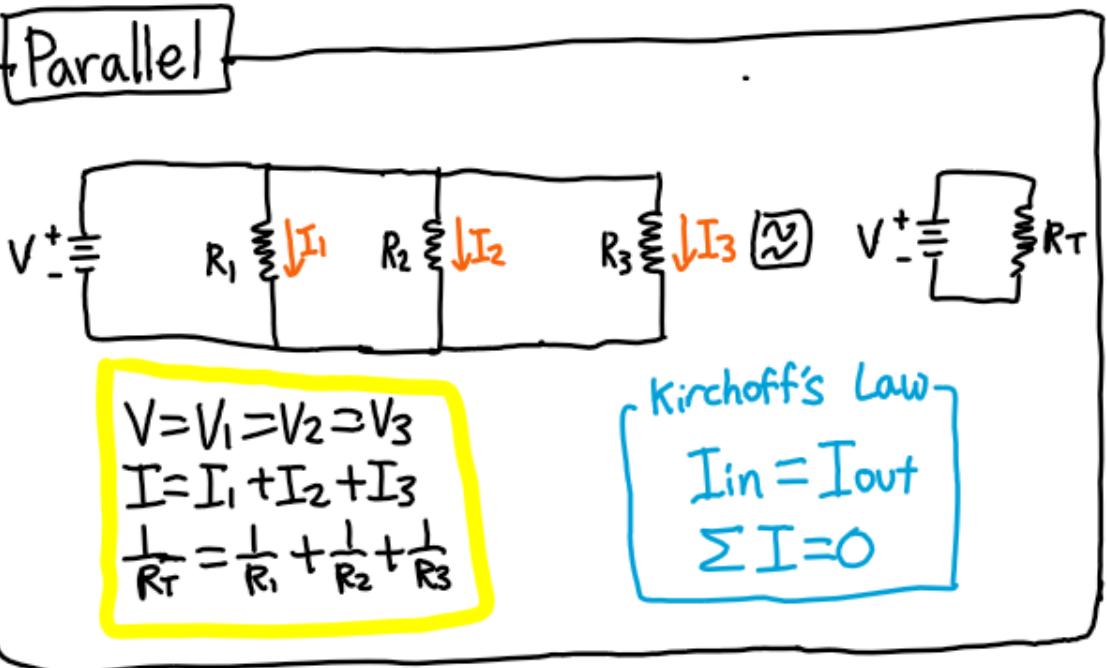
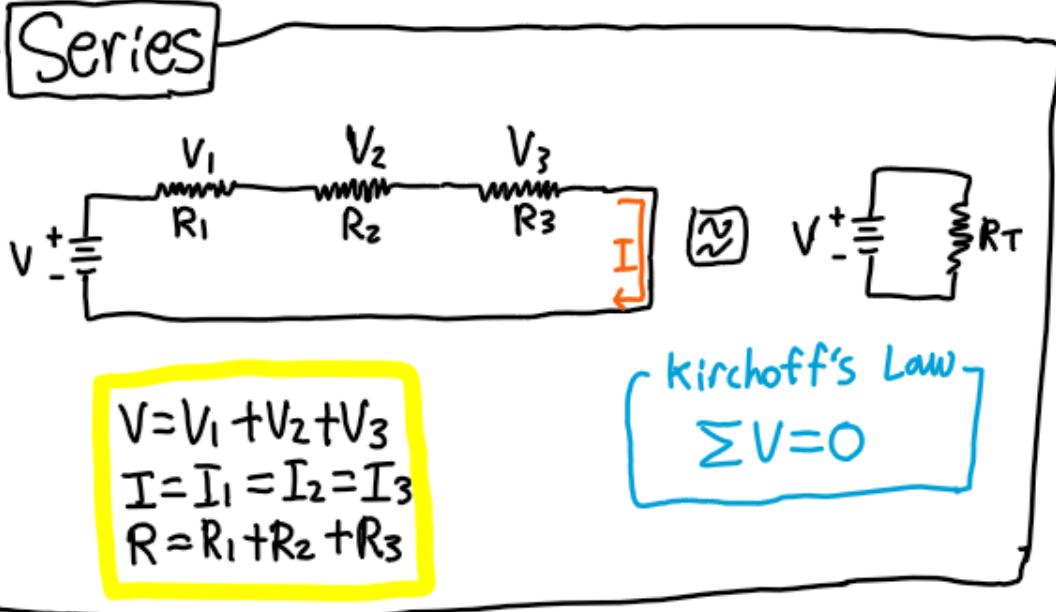
$$\text{Power} = \frac{dU}{dt} \\ I = \frac{dq}{dt}$$

Power dissipated by resistor
Power = $\frac{dU}{dt} = RI \frac{dq}{dt}$

$$\text{Power} = I^2 R = \frac{V^2}{R} = VI$$

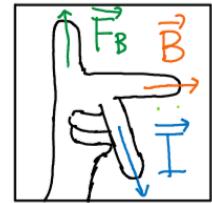
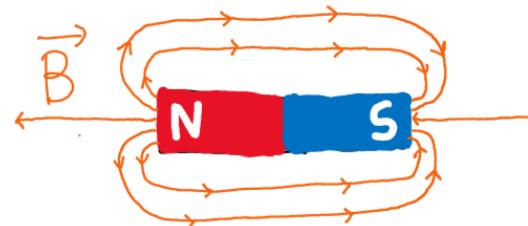
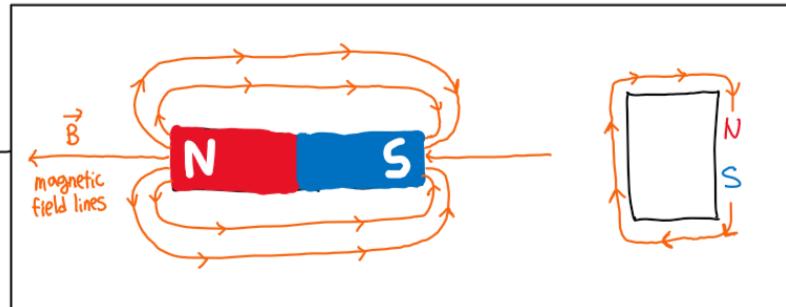
6-A

Parallel & series circuits



7-1 Magnetic Fields and Definition of \vec{B}

Magnetic field lines form a loop (no magnetic charge)



Current (movement of charge) produces magnetic field

$$\vec{F}_E = q \vec{E}$$

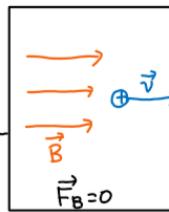
Electric force

$$\vec{F}_B = q \vec{v} \times \vec{B}$$

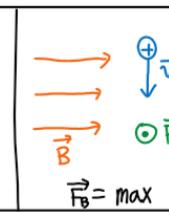
$$\vec{F} = \vec{F}_E + \vec{F}_B = q \vec{E} + q(\vec{v} \times \vec{B})$$

Lorentz Force

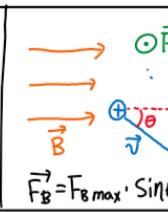
q - Charge with algebraic sign
 v - velocity of charge
 B - magnetic field



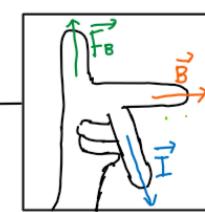
$\vec{F}_B = 0$



$\vec{F}_B = \text{max}$



$$\vec{F}_B = F_{B \text{ max}} \cdot \sin\theta$$



Unit for magnetic field

$$[\frac{\text{N} \cdot \text{S}}{\text{C} \cdot \text{m}}] = [\frac{\text{V} \cdot \text{S}}{\text{m} \cdot \text{m}}] = \left[\frac{\text{Weber}}{\text{m}} \right] = \left[\frac{\text{T}}{\text{Tesla}} \right]$$

$\hookrightarrow \text{N/C} = \text{V/m}$

$$\vec{F}_B = q \vec{v} \times \vec{B}$$

$$F_B = B q v \sin \theta$$

$$d\vec{F} = d\vec{q} \vec{v} \times \vec{B}$$

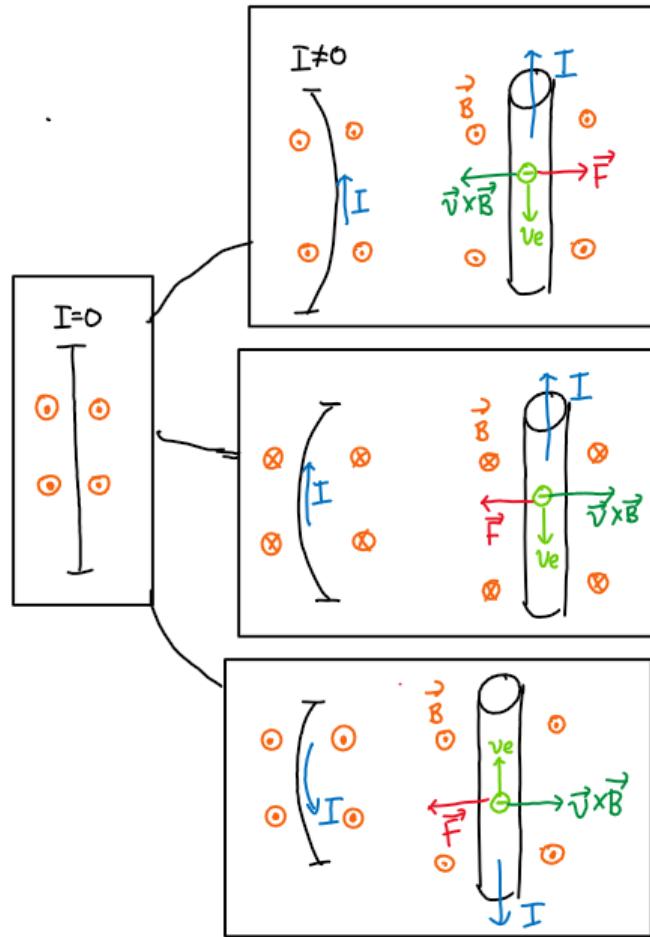
$$= I d\vec{l} \vec{v} \times \vec{B}$$

$$\vec{v} = \frac{d\vec{l}}{dt} \quad I = \frac{dq}{dt}$$

$$\vec{F}_B = I \vec{l} \times \vec{B}$$

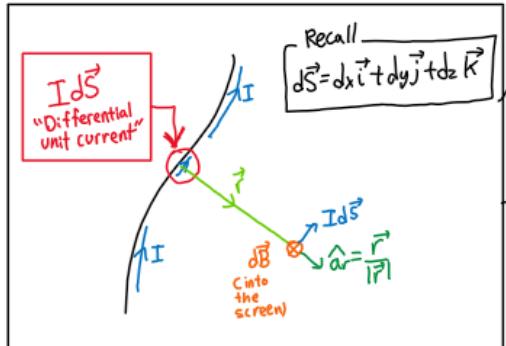
$$F_B = B I l \sin \theta$$

"Wire is straight, \vec{B} and I are constant"



7-6 Magnetic force
on a Current-carrying wire

8-1 Magnetic Field due to current



Biot-Savart Law

$$d\vec{B} = \frac{Mo \cdot Id\vec{s} \times \hat{ar}}{4\pi r^2}$$

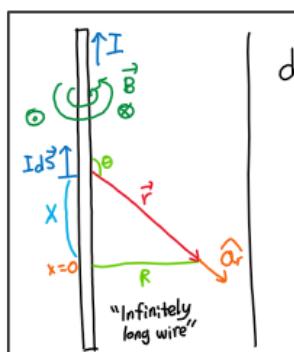
\hookrightarrow Magnetic field produced by small current $Id\vec{s}$

M_0 - Permeability of vacuum

$$M_0 = 4\pi \times 10^{-7} [H/M]$$

$[H/m = Tm^2/Am = Tm/A = VS/A \cdot 1/m]$

$\hookrightarrow \epsilon_0$ Permittivity



$$dB = \frac{Mo \cdot Id\vec{s} \times \hat{ar}}{4\pi r^2}$$

$$= \frac{Mo \cdot I \cdot ds \sin\theta}{4\pi r^2}$$

$$\int_{-\infty}^{\infty} dB = \int_{-\infty}^{\infty} \frac{Mo \cdot I \sin\theta}{4\pi r^2} ds$$

$$ds = dx$$

$$B = \frac{Mo \cdot I}{4\pi} \int_{x=-\infty}^{x=\infty} \frac{\sin\theta}{r^2} dx$$

($r, \sin\theta$ depends on x)

R - distance to measure

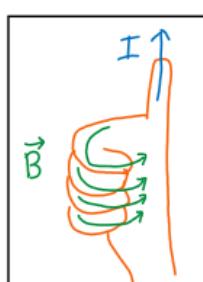
$$r^2 = x^2 + R^2$$

$$\sin\theta = \sin(\pi - \theta) = \frac{R}{r} = \frac{R}{\sqrt{x^2 + R^2}}$$

$$B = \frac{Mo \cdot I}{4\pi} \cdot 2 \int_0^{\infty} \frac{R}{(x^2 + R^2)^{3/2}} dx$$

$$= \frac{Mo \cdot I}{2\pi} \left[\frac{x}{\sqrt{x^2 + R^2}} \right]_0^{\infty}$$

$\boxed{B = \frac{Mo \cdot I}{2\pi R}}$



"semi-infinite wire"

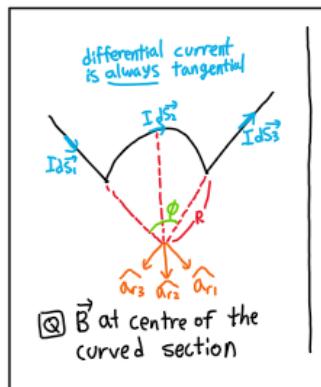
$$B = \frac{Mo \cdot I}{4\pi} \int_0^{\infty} \frac{\sin\theta}{r^2} dx$$

$$r^2 = R^2 + x^2$$

$$\sin\theta = \frac{R}{\sqrt{R^2 + x^2}}$$

$$B = \frac{Mo \cdot I}{4\pi} \int_0^{\infty} \frac{R}{(R^2 + x^2)^{3/2}} dx$$

$\boxed{B = \frac{Mo \cdot I}{4\pi R}}$



$$B_T = B_2 = \frac{Mo \cdot I}{4\pi} \int_0^\phi \frac{d\vec{s}_2}{R^2}$$

$$= \frac{Mo \cdot I}{4\pi} \int_0^\phi \frac{R d\phi'}{R^2}$$

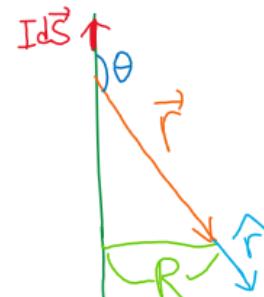
$$= \frac{Mo \cdot I \phi}{4\pi R}$$

(ϕ in radians)

$d\vec{s} = R d\phi$

\vec{B} at centre of loop

$B = \frac{Mo \cdot I \phi}{4\pi R}$



B-2

Force between two parallel currents

The diagram shows two vertical parallel wires. The left wire carries current I_a upwards, indicated by an arrow at the top. The right wire carries current I_b upwards, also indicated by an arrow at the top. A horizontal dimension line between them is labeled d . To the left of the left wire, there is a circle with a dot, labeled \vec{B}_b , representing the magnetic field due to current I_b . To the right of the right wire, there is a circle with a cross, labeled \vec{B}_a , representing the magnetic field due to current I_a . Between the wires, two red arrows point towards each other, labeled $\vec{F}_{a,b}$ and $\vec{F}_{b,a}$, representing the forces exerted by one current on the other.

$|F_{b,a}| = |F_{a,b}| = \frac{\mu_0 I_a I_b}{2\pi d}$

$B_a = \frac{\mu_0 I_a}{2\pi d}$

$\vec{F}_{b,a} = I_b l \vec{l} \times \vec{B}_a$
 $= I_b l B_a \sin(\vec{l}, \vec{B}_a)$
 $\text{Since } \theta = 90^\circ, \sin 90^\circ = 1$

$\vec{F}_{b,a} = I_b l B_a = I_b l \frac{\mu_0 I_a}{2\pi d}$

TIP: $\frac{\mu_0}{2\pi} = \frac{4\pi \times 10^{-7}}{2\pi} = 2 \times 10^{-7}$

8-3 Ampere's Law

Diagram showing three loops with enclosed currents:

- Loop 1: Enclosed current $I_1 = 3\text{mA}$. Magnetic field \vec{B} is directed outwards.
- Loop 2: Enclosed current $I_2 = 2\text{mA}$. Magnetic field \vec{B} is directed clockwise.
- Loop 3: Enclosed current $I_3 = 4\text{mA}$. Magnetic field \vec{B} is directed counter-clockwise.

Gauss' Law/Electric Flux

$$\oint \vec{E} \cdot d\vec{A} = \frac{Q_{enc}}{\epsilon_0}$$

Ampere's Law

$$\oint_c \vec{B} \cdot d\vec{s} = \mu_0 I_{enc}$$

Line Integral

Enclosed current in loop (sign included)

Amperian Loop (A.L.)

$I_{enc} = 2 - 3 = -1\text{mA}$

Projection of \vec{B} along $d\vec{s}$

$\vec{B} \cdot d\vec{s} = B ds \cos(\angle \vec{B}, d\vec{s})$

* $d\vec{s}$ always tangential to the curve

Derivation of Ampere's Law for a circular loop:

$$\oint_c \vec{B} \cdot d\vec{s} = \int B \cos(\angle \vec{B}, d\vec{s}) ds = \mu_0 I_{enc}$$

$$\cos(\angle \vec{B}, d\vec{s}) = 1$$

$$\int B ds = \mu_0 I = \int_0^{2\pi} BR d\phi = BR \cdot 2\pi$$

$$B = \frac{\mu_0 I}{2\pi R}$$

Choose amperian loop/gaussian surface CAREFULLY

Diagram of a cylindrical Amperian loop with radius R and length L , carrying current I .

Amperian loop

$d\vec{s}$ is tangential

Magnitude of magnetic field remains same in loop

Derivation:

$$\oint_c \vec{B} \cdot d\vec{s} = \mu_0 I_{enc}$$

$$= \int_c B \cos(\angle \vec{B}, d\vec{s}) ds$$

$$\cos \theta = 1$$

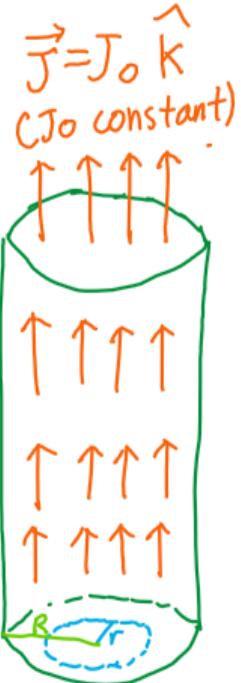
$$\Rightarrow \mu_0 I = B \int_c ds$$

$$C ds = R d\phi$$

$$\mu_0 I = B \int_c R d\phi$$

$$= BR \cdot 2\pi$$

$$B = \frac{\mu_0 I}{2\pi R}$$



B outside

$$B = \frac{\mu_0 I}{2\pi r}$$

Q B if $0 < r < R$?
 Magnetic field inside?

Total current = I

$$\oint_c \vec{B} d\vec{s} = \mu_0 I_{enc} \rightarrow \int B ds = \int_0^{2\pi} Br d\phi = 2\pi Br$$

$$I_{tot} = \pi R^2 J_0.$$

(total cylinder)

$$I_{enc} = \iint \vec{J} dA = \pi r^2 J_0.$$

$$\frac{I_{enc}}{I} = \frac{r^2}{R^2}$$

$$I_{enc} = \frac{r^2}{R^2} I$$

$$\oint \vec{B} d\vec{s} = 2\pi Br = \mu_0 I_{enc} = \mu_0 I_{tot} \frac{r^2}{R^2}$$

$$2\pi Br = \mu_0 I_{tot} \frac{r^2}{R^2}$$

$$B = \frac{\mu_0 I_{tot} r}{2\pi R^2}$$

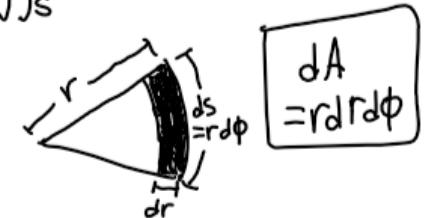
$$I_{enc} = \iint_S \vec{J} d\vec{A} = \iint_S J \cos(\vec{J}, \vec{dA}) dA$$

$$= \iint_S J_0 dA$$

$$= J_0 \int_{r=0}^r \int_{\phi=0}^{2\pi} r' dr' d\phi$$

$$= 2\pi \frac{r^2}{2} J_0 = \pi r^2 J_0$$

$$I_{enc} = \pi r^2 J_0$$



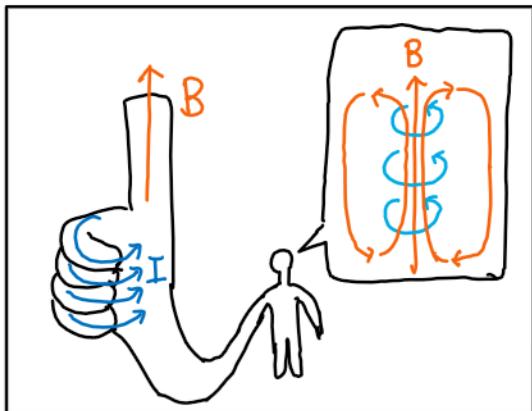
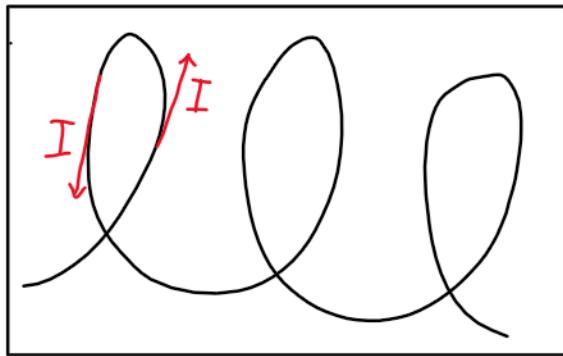
current depends on
 r , not ϕ

" J is $J(r) \rightarrow$ not constant?"

$$I = \iint \vec{J} d\vec{A} = \iint J \cos(\vec{J}, \vec{dA}) dA$$

$$= \iint J dA = \int_0^r \int_0^{2\pi} J(r) \cdot r dr d\phi$$

B-4 Solenoids



Ideal Solenoid

Magnetic field is ONLY inside loop.

A cross-section diagram of an ideal solenoid. It shows a rectangle with width a , height b , and thickness $h[m]$. Inside, there are n turns of wire per unit length. Magnetic field lines are shown as loops within the rectangle, with arrows pointing outwards from the top and bottom edges. A red arrow labeled B points to the right, indicating the direction of the magnetic field inside the solenoid.

No magnetic field outside
⇒ Cancelled

Let n "turns/meter"

(ex) 10 loops/cm
1000 loops/m.

$I_{enc} = nhI$
 $\mu_0 I_{enc} = \mu_0 n h I$

$$\int \vec{B} d\vec{s} = \int_a^b \vec{B} d\vec{s} + \int_c^d \vec{B} d\vec{s} + \int_d^e \vec{B} d\vec{s} + \int_e^a \vec{B} d\vec{s}$$

$$\angle \vec{B} \cdot d\vec{s} = 0 \quad \vec{B} \perp d\vec{s}$$

outside

$$= \int_a^b B ds = B(b-a) = Bh$$

Hence:

$$\int \vec{B} d\vec{s} = \mu_0 I_{enc}$$

$B = \mu_0 n I$

h doesn't matter
→ magnetic field in solenoid

9-1

Faraday's Law & Lenz's Law

Magnetic field induced by current

$$B = \frac{\mu_0 I}{2\pi r}$$

Current induces magnetic field!

$$\mathcal{E} = -N \frac{\partial \Phi_B}{\partial t}$$

$$= -N \frac{\partial}{\partial t} \iint \vec{B} d\vec{A}$$

(EMF in N loops)

Lenz' Law
Direction of induced current
EMF are against induced
magnetic field

$$\Phi_B = \iint \vec{B} d\vec{A}$$

Magnetic Flux Open integral [Wb]

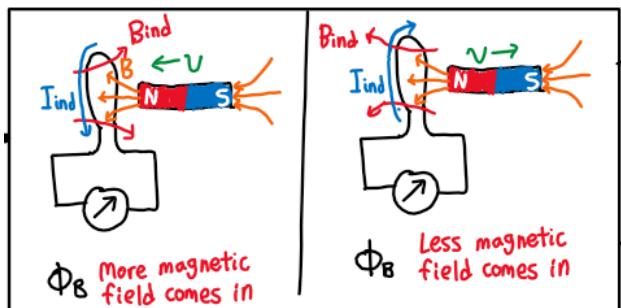
$$\mathcal{E} = -\frac{\partial}{\partial t} \Phi_B$$

$$= - \frac{\partial}{\partial t} \iint \vec{B} d\vec{A}$$

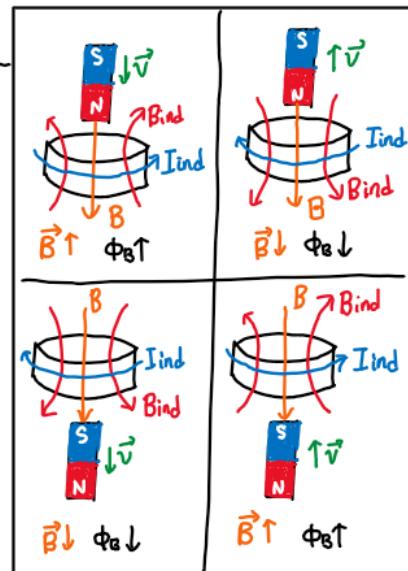
Partial derivative

Φ_B is function
of space & time

If Φ_B doesn't
change over time,
 \mathcal{E} (EMF) = 0



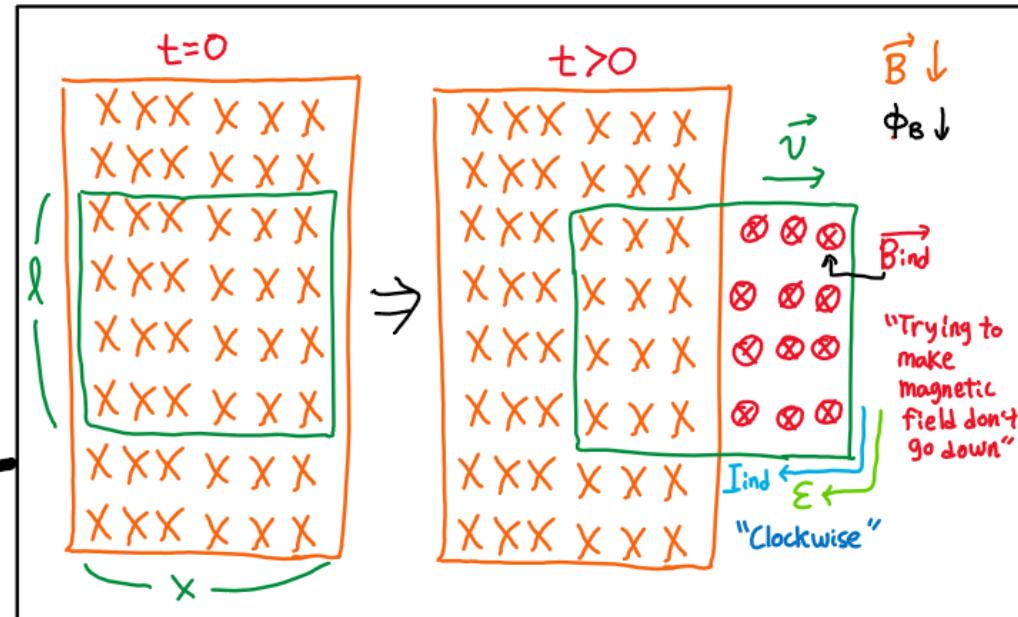
I_{ind} - induced current
EMF(E) - voltage
Bind - induced magnetic field



Faraday's Law
EMF is proportional
to change in magnetic
flux w/r/t time

9-2

Induction & Energy Transfer



$P_{\text{supp}} = \vec{F} \cdot \vec{v}$
 $\vec{F}_{\text{wire}} = I_{\text{ind}} (\vec{x} \times \vec{B}_{\text{orig}})$
 $\vec{F} + \vec{F}_2 = \vec{F}_{\text{net}} = m\vec{a}$
If $a=0$, $|\vec{F}| = |\vec{F}_2|$
 $\vec{F}_2 = I_{\text{ind}} \vec{L} \times \vec{B}$ (LB)
 $= I_{\text{ind}} LB = F$
 $P_{\text{supp}} = Fv = I_{\text{ind}} LBv$
 $= \frac{B^2 L^2 v^2}{R}$ (single loop)

$$|\mathcal{E}| = \left| -\frac{\partial}{\partial t} \Phi_B \right|$$

$$I_{\text{ind}} = \frac{\mathcal{E}}{R} \quad (\text{Ohm's Law})$$

$$\Phi_B = \iint \vec{B} d\vec{A} = BLx \quad (\vec{B} \parallel d\vec{A})$$

$$|\mathcal{E}| = -\frac{\partial}{\partial t} \Phi_B = BL \frac{dx}{dt} = BvL$$

One loop
 $\mathcal{E} = (-) BV_x l$

N loops
 $\mathcal{E} = (-) NBV_x l$

 $I = \frac{NBV_x l}{R}$

[Power dissipated]

$$P = \frac{V^2}{R} = VI = I^2 R$$

$$= \frac{N^2 B^2 V^2 l^2}{R} [W]$$

Power provided by external Agent
 $P_{\text{Supply}} = P_{\text{dissipated}}$
Conservation of energy

Capacitor \rightarrow $Q=CV$

Resistor \rightarrow $V=IR$

Solenoid (Loop) is an inductor



$$B = \mu_0 n I$$

[Inductance (L)]

$$L = \frac{N\Phi_B}{I} [H]$$

N - total # of turns

$$\Phi_B = \iint \vec{B} d\vec{A}$$
$$= BA = \mu_0 n IA$$

$$L = \frac{BA N}{I} = N \mu_0 n A$$

$$N = nl$$

9-4

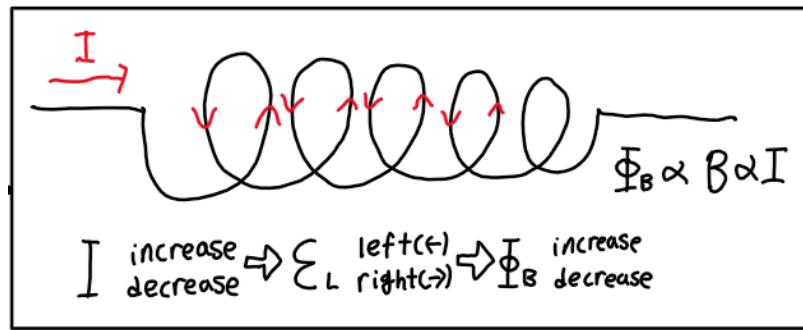
Inductors &
Inductance

$$L = \ell n^2 A \mu_0$$

$$(\mu_0 = 4\pi \times 10^{-7} \text{ H/m})$$

9-5

Self-Induction

 ϵ_L - Self induced emf

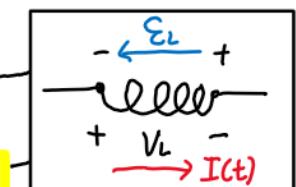
$$\epsilon_L = -N \frac{\partial}{\partial t} \Phi_B$$

$$L = \frac{N \Phi_B}{I} \Rightarrow N \Phi_B = LI$$

$$\epsilon_L = -N \frac{\partial}{\partial t} \Phi_B = -L \frac{d}{dt} I(t)$$

$$V_L = -\epsilon_L = L \frac{d}{dt} I(t)$$

V_L - Voltage across inductor



9-7

Energy stored in magnetic field

Energy

$$U = qV$$

$$dU = dq V = q dV$$

$$I = \frac{dq}{dt} \Rightarrow dq = I dt$$

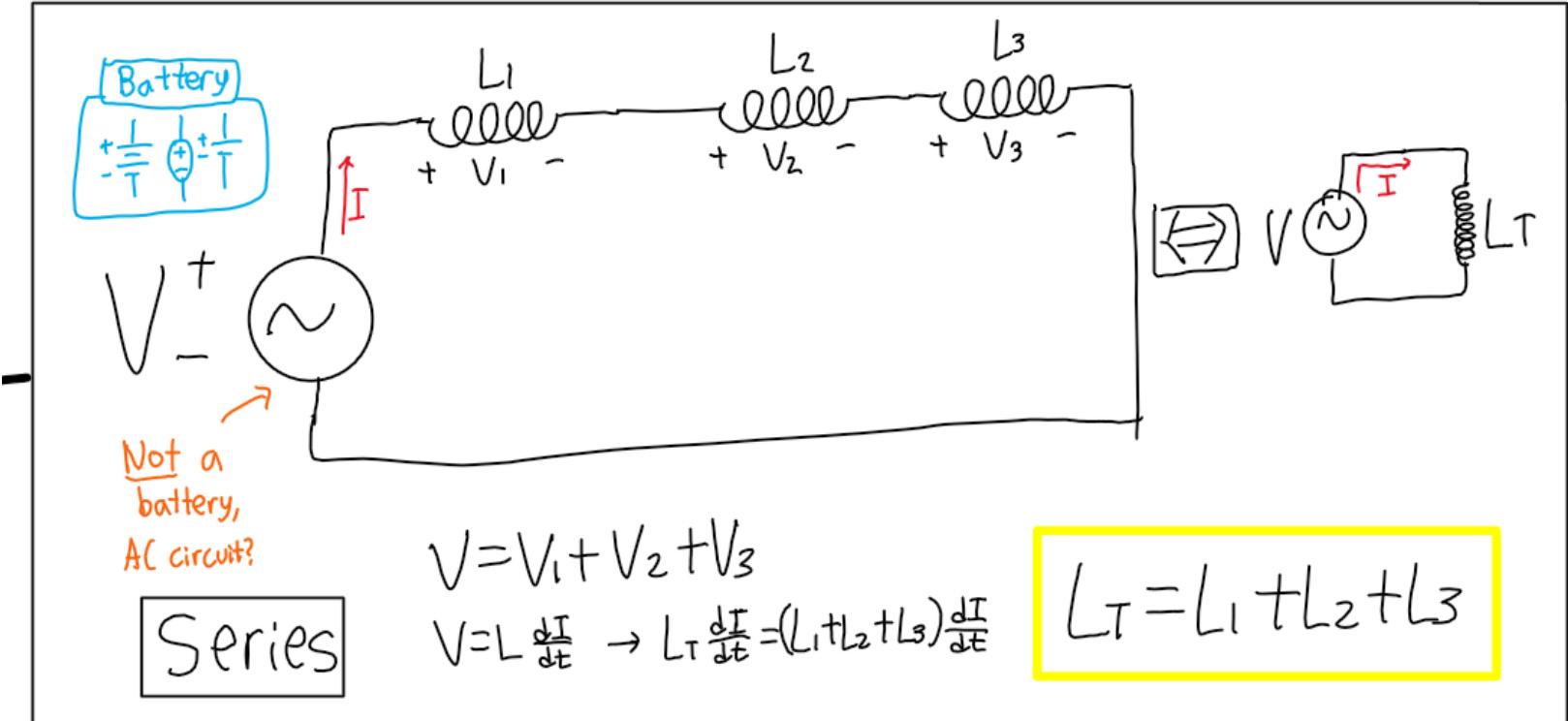
$$\text{Power} = \frac{dU}{dt} = IV$$

$$V = L \frac{dI}{dt}$$

$$\frac{dU}{dt} = IL \left(\frac{dI}{dt} \right)$$

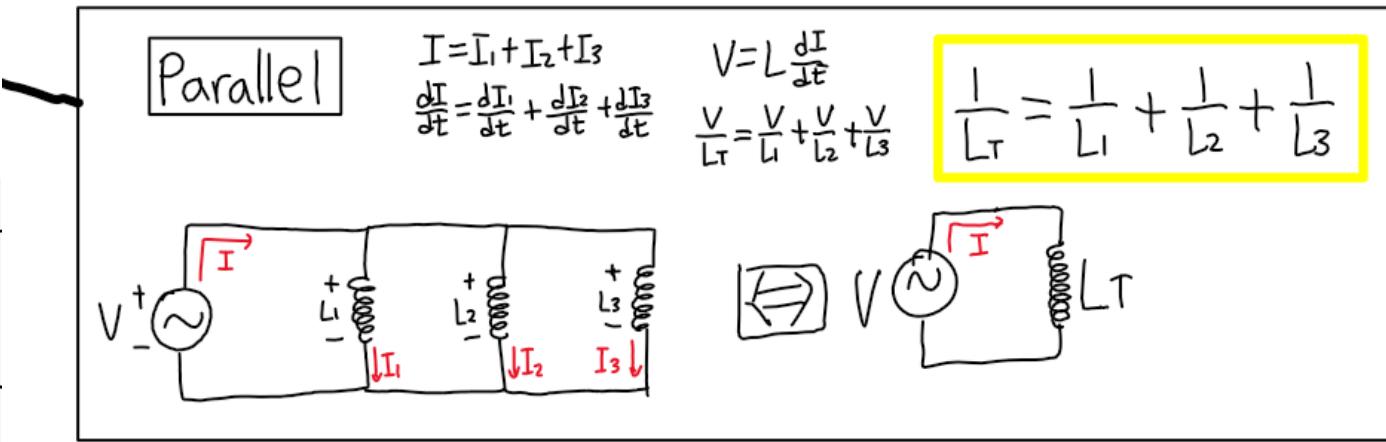
$$dU = IL dI$$

$$U = \frac{1}{2} LI^2$$



9-A

Series & Parallel Inductors



Basic SI units

Length	Meter	M
Time	second	S
Current	Ampere	A
mass	kilogram	kg
temperature	Kelvin	K
luminosity	candela	cd

System of units

SI prefixes

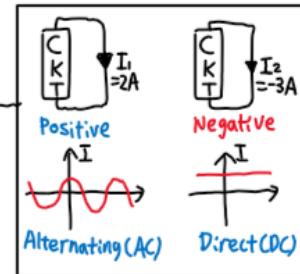
10^{-15}	10^{-12}	10^{-9}	10^{-6}	10^{-3}	1	10^3	10^6	10^9	10^{12}	10^{15}
femto	pico	nano	micro	milli	1	Kilo	mega	giga	tera	Peta
f	p	n	m	m		K	M	G	T	P

Basic Quantities

$$I(t) = \frac{dQ(t)}{dt}$$

$$Q(t) = \int_{-\infty}^t I(x)dx$$

Polarity
the way which current is moving



$$V(t) = \frac{W(t)}{q}$$

$$V = \frac{dW}{dq}$$

$$VI = \frac{dW}{dq} \frac{dq}{dE} = \frac{dW}{dE} = P$$

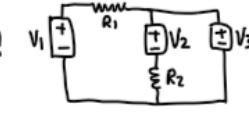
$$\Delta W = \int_{t_1}^{t_2} P dt = \int_{t_1}^{t_2} VI dt$$

$$P = IV$$

2 terminal devices

- Resistor $\circ - \text{---} - \circ$ $V = IR$
- Capacitor $\circ - \text{---} - \circ$ $I_C = C \frac{dV}{dt}$
- Inductor $\circ - \text{---} - \circ$ $V_L = L \frac{dI}{dt}$

Battery can use power!
 \rightarrow unit J

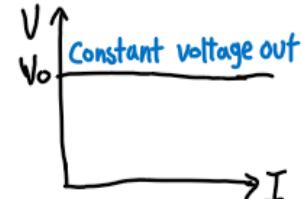
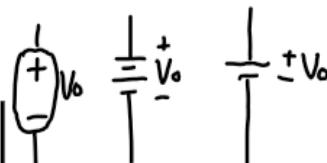


10-3

Circuit elements

Independent sources

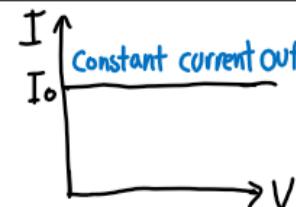
Independent Voltage source



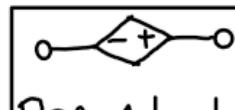
Independent Current source



Transistors/
Diodes



Dependent sources

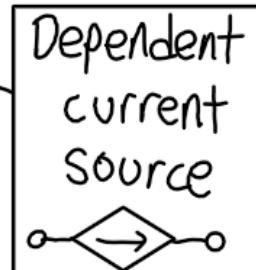


Dependent
Voltage
source

Voltage-control
(dependent)
Voltage source



$$V = \alpha \cdot V_x$$



Dependent
current
source

Current-control
(dependent)
Voltage source



$$V = r \cdot I_x$$



Voltage-control
(dependent)
current source



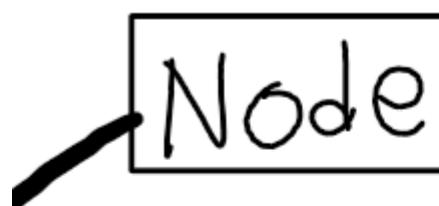
$$I = g \cdot V_x$$



Current-control
(dependent)
current source



$$I = \beta \cdot I_x$$



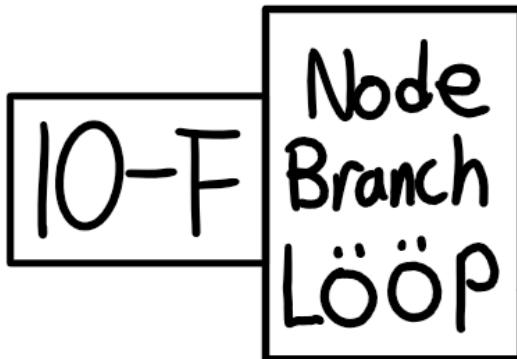
Point on circuit
that $2+$ elements
come together
→ Kirchoff's current law

A simple circuit diagram showing a central circular node connected to three separate horizontal lines, representing three different branches meeting at a single node.



Section of circuit that
contains only one element
(and $1+$ terminals)
→ mathematical line
(can be stretched)

A simple circuit diagram showing a vertical line segment with two open terminals at the ends, representing a branch as a mathematical line that can be stretched.



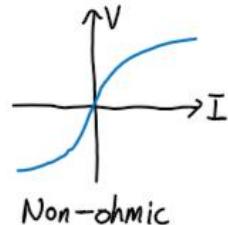
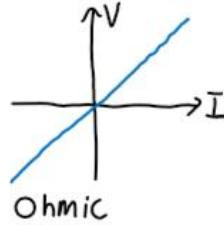
Closed path:
Start from one node
→ visit other node (ONLY once)
→ return back to origin node

→ Kirchoff's
Voltage
law

II-1

Ohm's Law

$$V(t) = R \cdot I(t) \quad [R \geq 0]$$



$$\begin{aligned} P(t) &= V(t) I(t) \\ &= R I^2(t) \\ &= \frac{V^2(t)}{R} \end{aligned}$$

$$\begin{aligned} R=0 \quad V(t) &= R I(t) = 0 \\ R=\infty \quad I(t) &= \frac{V(t)}{R} = 0 \end{aligned}$$

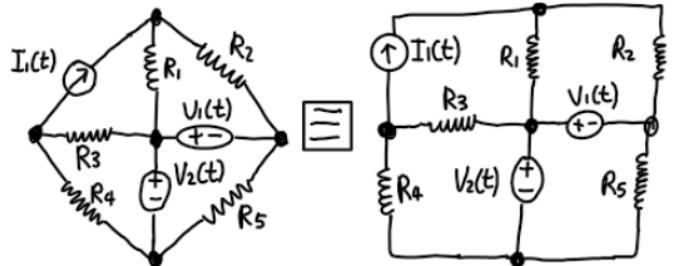
$$\begin{aligned} I(t) &= G \cdot V(t) \\ P(t) &= \frac{I^2(t)}{G} \\ &= G V^2(t) \end{aligned}$$

Conductance

$$G = \frac{1}{R} = \frac{I}{V} \quad [\text{S}]$$

11-2

Kirchhoff's Laws



Algebraic sum of current entering & leaving at each node must be zero

$$\sum_{j=1}^N I_j(t) = 0$$

$$\sum I_{\text{enter}} = \sum I_{\text{leave}}$$

- Book** Current enter (+)
Current leave (-)
Prof Current enter (-)
Current leave (+)
- NO DIFF

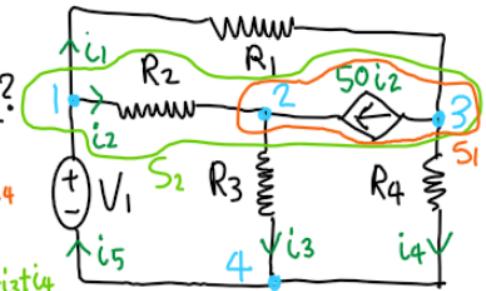
KCL for Closed Surface?

Surface 1

$$i_1 + i_2 = i_3 + i_4$$

Surface 2

$$i_1 + i_5 = i_3 + i_4$$

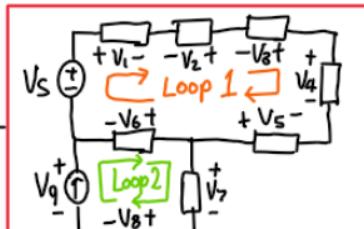


Algebraic sum of voltages around a loop must be zero

$$\sum_{j=1}^N V_j(t) = 0$$

$$\sum V_{\text{inc}} = \sum V_{\text{dec}}$$

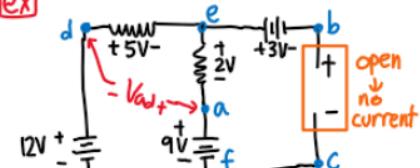
- Book** V drop +
V rise -
Prof V drop -
V rise +
- NO DIFF



$$\text{Loop 1} \Rightarrow V_1 + V_4 + V_6 = V_5 + V_2 + V_3 + V_5$$

$$\text{Loop 2} \Rightarrow V_9 + V_6 = V_7 + V_8$$

ex



$$V_{fd} = V_{af} + V_{at} + V_{af}$$

$$12 = 5 + (-2) + V_{af}$$

$$V_{af} = 9V$$

$$V_{af}, V_{ad}, V_{bc}, V_{bf}?$$

$$V_{bc} + V_{eb} = V_{fa} + V_{ae}$$

$$V_{bc} + 3 = 9 - 2$$

$$V_{bc} = 4V = V_{bf}$$

$$V_{at} + V_{fd} = V_{af}$$

$$V_{at} + 12 = 9$$

$$V_{at} = -3V$$

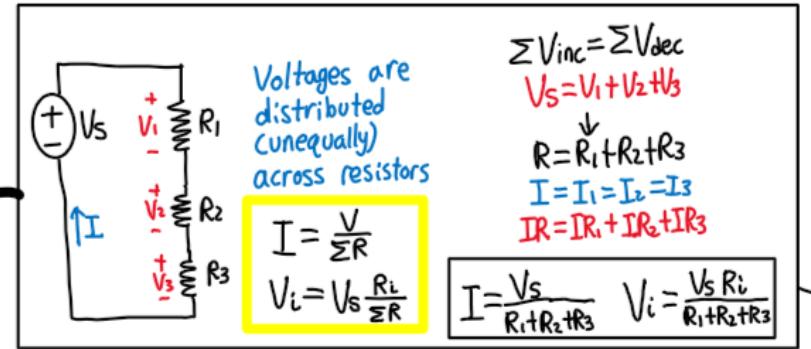
Kirchhoff's voltage law

II-3

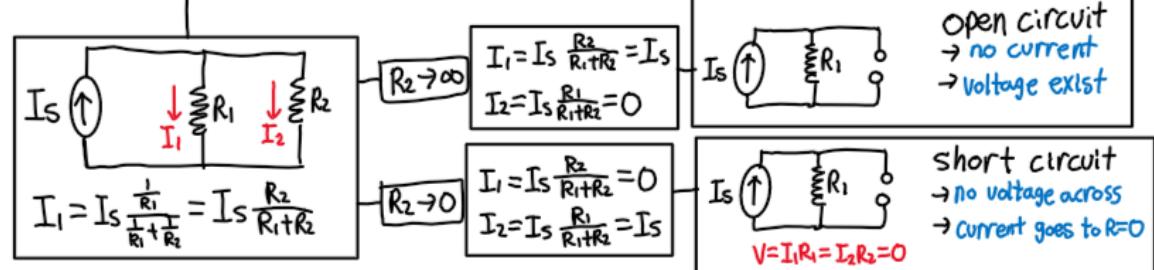
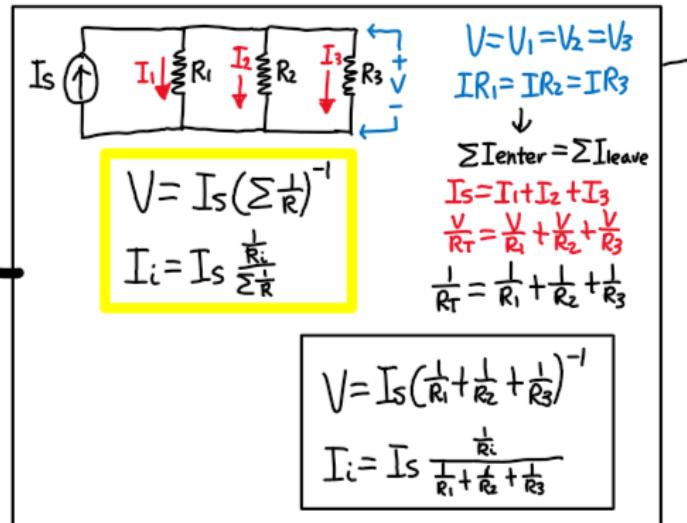
Single-Loop
Circuits &
Single-Node
-Pair Circuits

II-4

SINGLE LOOP/ Voltage Divider

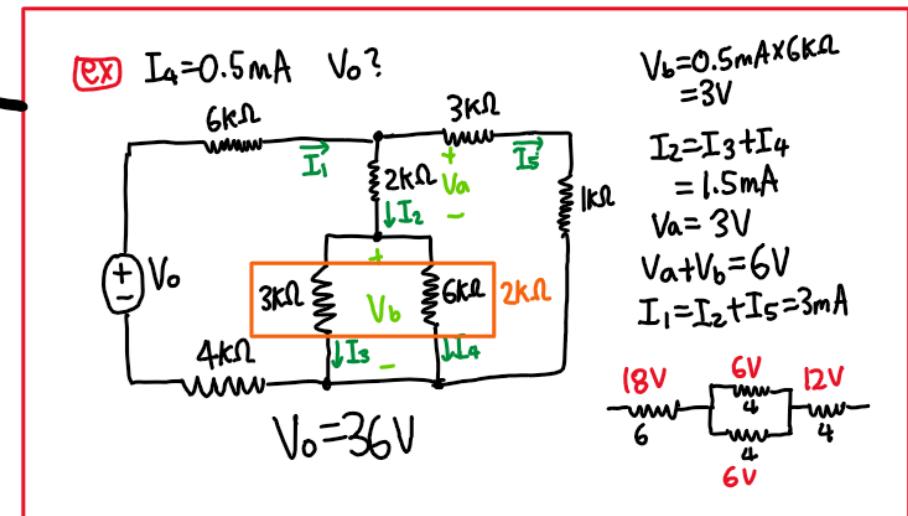
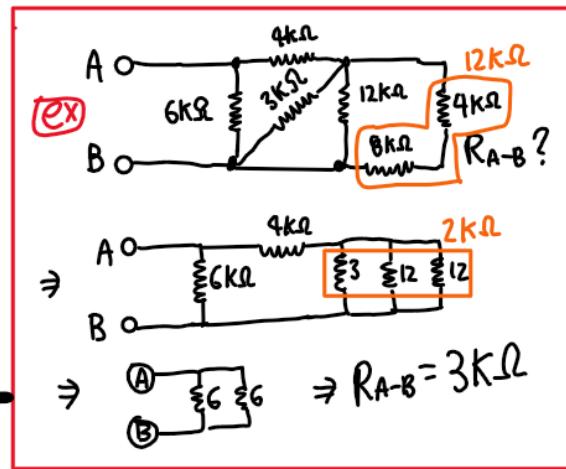


SINGLE NODE-PAIR/ Current Divider



II-5

Series and parallel resistor combinations



12-1

No nodal Analysis

Nodal Analysis

Calculate/solve for "voltages at nodes"

systems of linearly coupled, algebraic equations

set one node as 'reference' and calculate voltages in other nodes

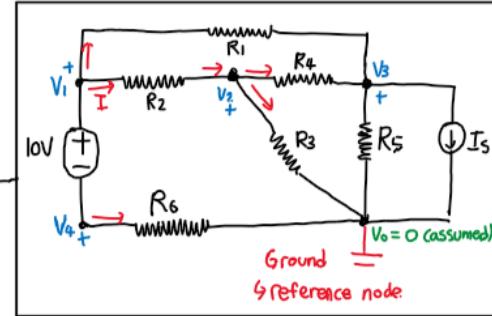
$$\# \text{ equations needed} = N - 1 - N_v \quad \begin{matrix} \text{ref} \\ \text{ence} \end{matrix} \quad \begin{matrix} \text{cst of} \\ \text{voltage} \\ \text{sources} \end{matrix}$$

Independent or dependent "constraint"

Use Kirchoff's current law to make systems of equations

$$+ \xrightarrow{I} \frac{V_m - V_n}{R} + \frac{V_m - V_h}{R} \quad I = \frac{V_m - V_h}{R}$$

- two nodes connected by voltage source
- none of them are reference node



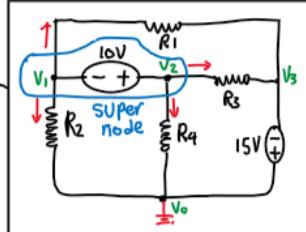
$$V_1 = V_4 + 10V$$

$$\textcircled{1} \quad \frac{V_1 - V_2}{R_2} + \frac{V_1 - V_3}{R_1} + \frac{V_4 - V_0}{R_6} = 0$$

$$\textcircled{2} \quad \frac{V_1 - V_2}{R_2} = \frac{V_2 - V_3}{R_4} + \frac{V_2 - V_0}{R_3}$$

$$\textcircled{3} \quad \frac{V_2 - V_0}{R_5} + I_S = \frac{V_2 - V_3}{R_4} + \frac{V_1 - V_3}{R_1}$$

Supernode



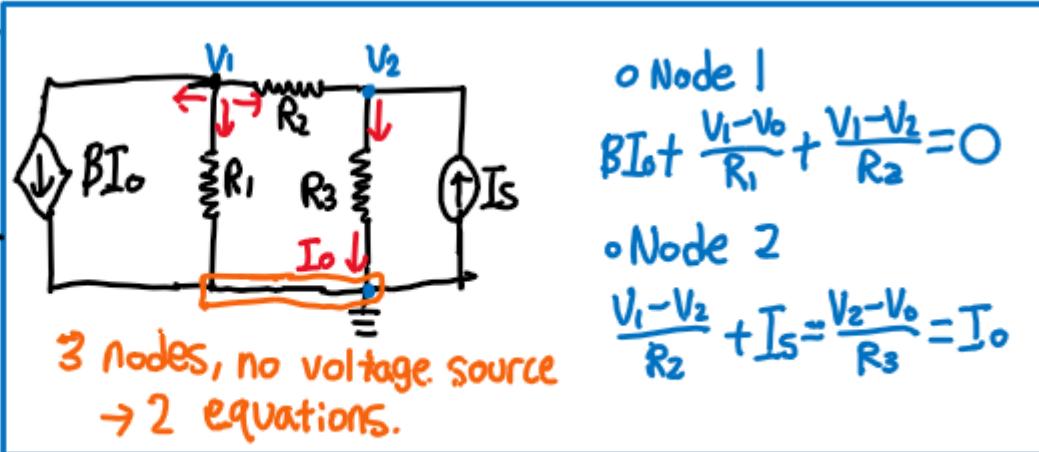
4 nodes, 2 voltage source
→ 1 equation

$$V_3 = -15V, V_2 = V_1 + 10V.$$

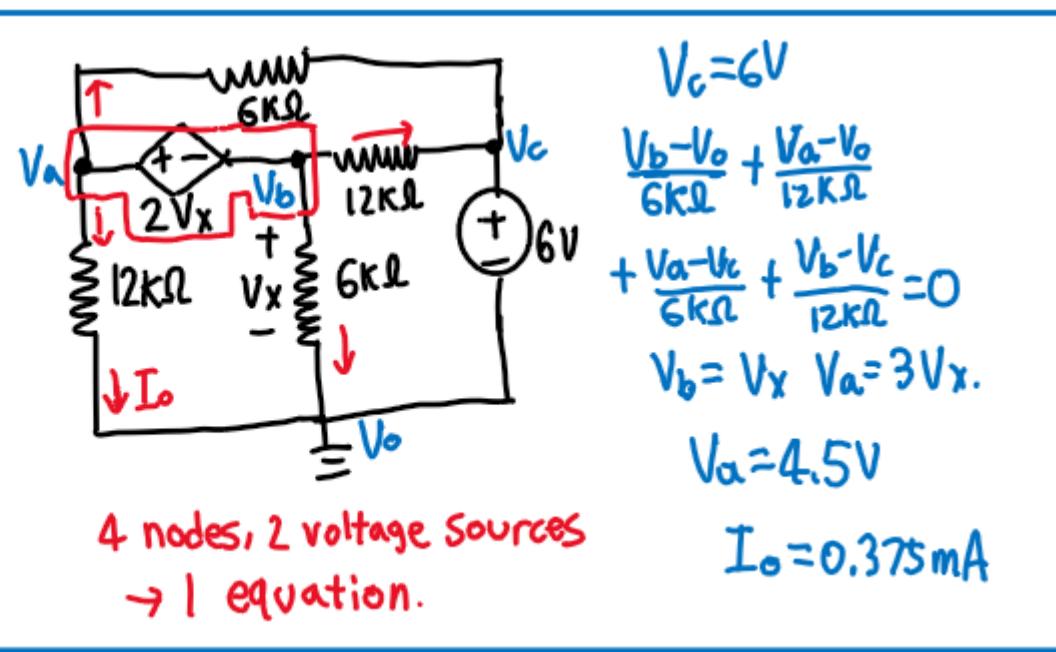
$$\frac{V_1 - V_3}{R_1} + \frac{V_1 - V_0}{R_2} + \frac{V_2 - V_0}{R_4} + \frac{V_2 - V_3}{R_3} = 0$$

$$\frac{V_1 + 15}{R_1} + \frac{V_1}{R_2} + \frac{V_1 + 10}{R_4} + \frac{V_1 + 25}{R_3} = 0$$

Dependent source



Dependent source + super node



12-2

Loop (Mesh) Analysis

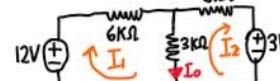
Mesh Analysis

Use Kirchoff's Voltage Law

$$\begin{aligned} \text{# Equations Needed} &= (\text{# of loops}) - N_I \\ &= B - N + I - N_I \end{aligned}$$

Independent or dependent "constant"

ex



2 equations needed.

$$\text{Loop 1 } \sum V_{\text{dec}} = \sum V_{\text{inc}}$$

$$6k\Omega \cdot I_1 + 6k\Omega(I_1 - I_2) = I_2$$

$$12k\Omega \cdot I_1 - 6k\Omega \cdot I_2 = I_2$$

$$\text{Loop 2 } \sum V_{\text{dec}} = \sum V_{\text{inc}}$$

$$6k\Omega(I_2 - I_1) + 3k\Omega \cdot I_2 + 3 = 0$$

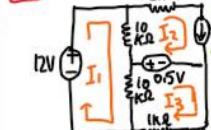
$$-6k\Omega \cdot I_1 + 9k\Omega \cdot I_2 = -3$$

$$I_1 = \frac{5}{4} \text{ mA}$$

$$I_2 = \frac{1}{2} \text{ mA}$$

$$I_o = \frac{3}{4} \text{ mA}$$

ex



#Eq=3-1=2

$$\text{Loop 2 } \sum V_{\text{dec}} = \sum V_{\text{inc}}$$

$$10k\Omega(I_2 - I_1) + 10k\Omega(I_1 - I_3) = I_2$$

$$20k\Omega \cdot I_1 - 10k\Omega \cdot I_3 = I_2 + 2.5$$

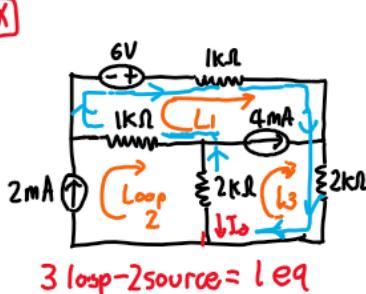
$$\text{Loop 3 } 0.5 \text{ mA} \cdot I_3 + 10k\Omega(I_3 - I_1) = 0$$

$$-10k\Omega \cdot I_1 + 10k\Omega I_3 = -0.5$$

$$I_1 = 3.35 \text{ mA} \quad I_2 = 3 \text{ mA}$$

$$V = 4V$$

ex



Supermesh ($L_1 + L_3$)

$$\begin{aligned} I_1 + 4 \text{ mA} &= I_3 \\ 1k\Omega \cdot I_1 + 2k\Omega \cdot I_3 &+ 2k\Omega(I_3 - I_2) \\ + 1k\Omega(I_1 - I_2) &+ 1k\Omega(I_1 - I_2) = 0 \end{aligned}$$

$$\begin{aligned} I_1 &= -\frac{2}{3} \text{ mA} \quad I_3 = \frac{10}{3} \text{ mA} \\ I_o &= I_2 - I_3 = -\frac{4}{3} \text{ mA} \end{aligned}$$

ex



$$\begin{aligned} \text{Loop 1 } 2k\Omega \cdot I_1 + 4k\Omega(I_1 - I_2) &= I_2 \\ 4k\Omega \cdot I_1 + 4k\Omega(I_2 - I_1) &+ 6k\Omega(I_2 - I_1) = 0 \end{aligned}$$

$$I_2 = -\frac{12}{19} \text{ mA} \quad V_o = -\frac{72}{19} \text{ V}$$

Super mesh

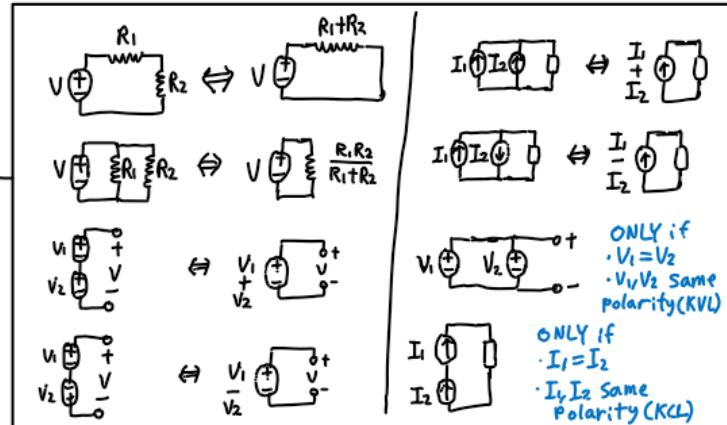
When current source is shared between two loops



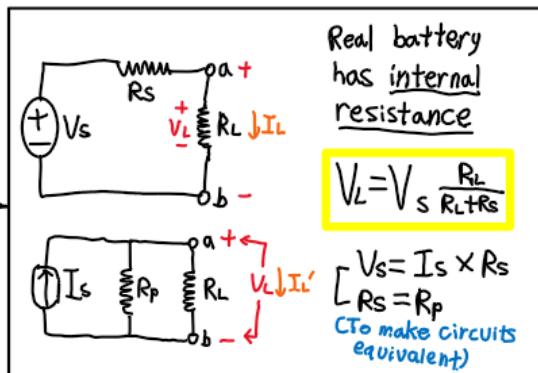
13-1

More techniques

Equivalence

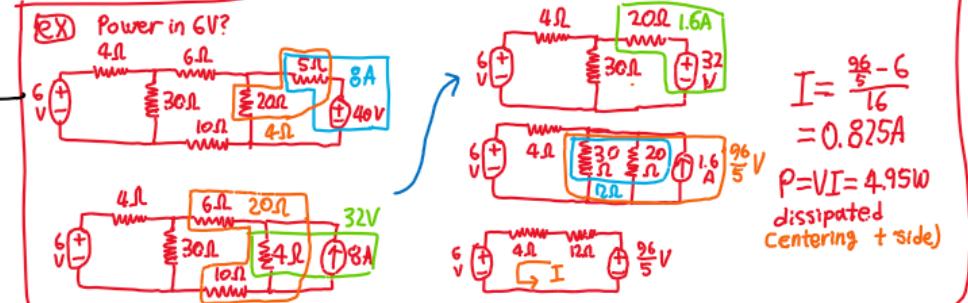


SOURCE transformation



$$\begin{aligned} I_{L'} &= I_S \frac{R_p}{R_p + R_L} \\ V_{ab}' &= I_S \frac{R_p R_L}{R_p + R_L} \\ &= \frac{V_s}{R_p} \frac{R_p R_L}{R_p + R_L} = V_{ab} \end{aligned}$$

Equivalent!

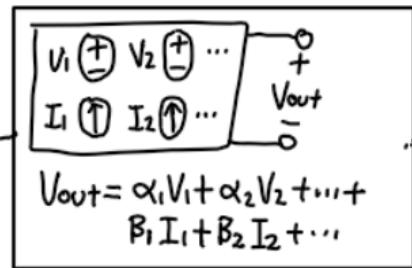


$$I = \frac{\frac{96}{5} - 6}{16} = 0.825A$$

$$P = VI = 4.95W$$

dissipated (centering + side)

Linearity



ex] Linear network
 - 1 independent current source
 - 1 independent voltage source

$$\begin{aligned} V_s & \quad I_s & V_{out} \\ 10V & + 0A & = 3.5V \\ 10V & + 1A & = 0.5V \\ 4V & + 1A & = ? \\ \alpha = 0.35 & \quad \beta = -3 & ? = -1.6V \end{aligned}$$

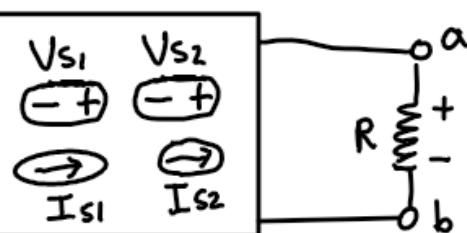
ex] Use linearity
 to find I_o when
 $I_s = 6mA$



$$\begin{aligned} \text{Assume } I_o &= 1mA \\ V \text{ across } 3k\Omega &\Rightarrow 3V \\ \text{ " } 6k\Omega &\Rightarrow 3V \end{aligned}$$

$$\begin{aligned} I \text{ across } 2k\Omega &\Rightarrow 1.5mA \\ I_s \text{ across } 12k\Omega &\Rightarrow 1.5mA \\ V \text{ across } I_s &= 1.5 \times 2 + 6 \times 0.5 = 6V \\ \text{ " } 12k\Omega &= 6V \\ &\Rightarrow 0.5mA \\ I_s &= 2mA \quad (I_s : I_o = 2 : 1) \\ I_o &= 3mA \end{aligned}$$

13-2 Superposition



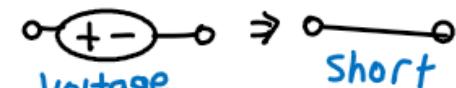
Deactivate all sources
 except one source!
 (Repeat for each voltage/
 current source)

Superposition
 holds for I & V
 but not power

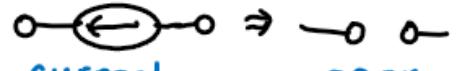
$I_1 \rightarrow$ current through R
 due to V_1 only
 $I_2 \rightarrow$ current through R
 due to V_2 only
 ...

$$\begin{aligned} I_{tot} &= I_1 + I_2 + \dots \\ P_{tot} &= I_{tot}^2 R \\ &= (I_1 + I_2 + \dots)^2 R \\ &\rightarrow \text{Quadratic relationship} \end{aligned}$$

Deactivate
 SOURCE?



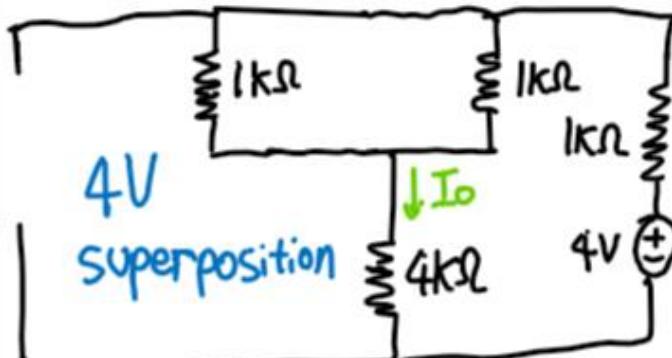
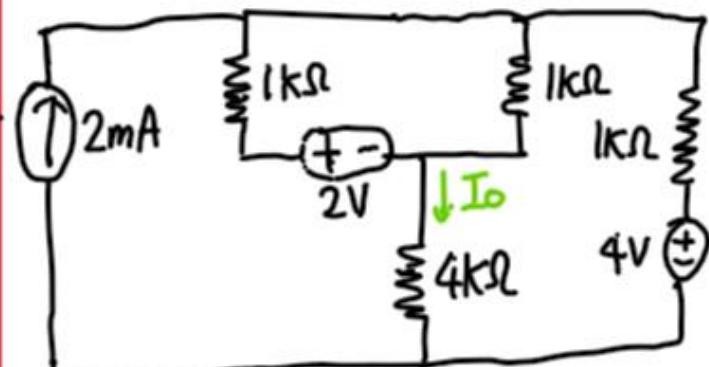
Short
 Voltage X
 Current V



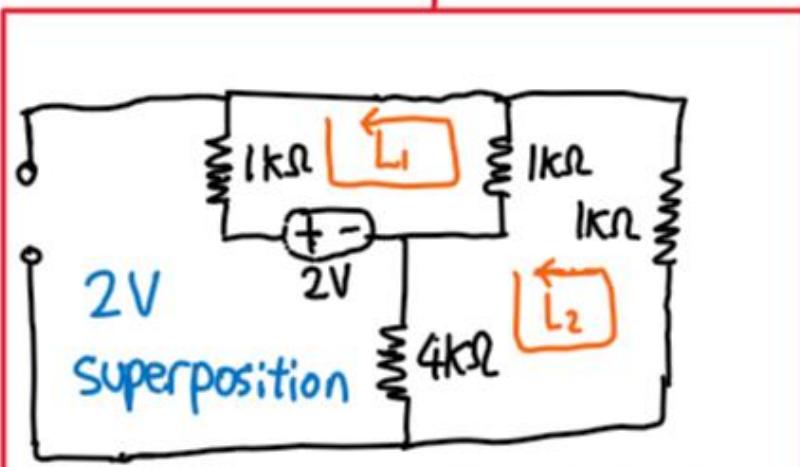
open
 voltage V
 current X

ex

$$I_{\text{total}} = I_{o-2V} + I_{o-4V} + I_{o-2mA}$$
$$= \frac{10}{11} \text{ mA}$$



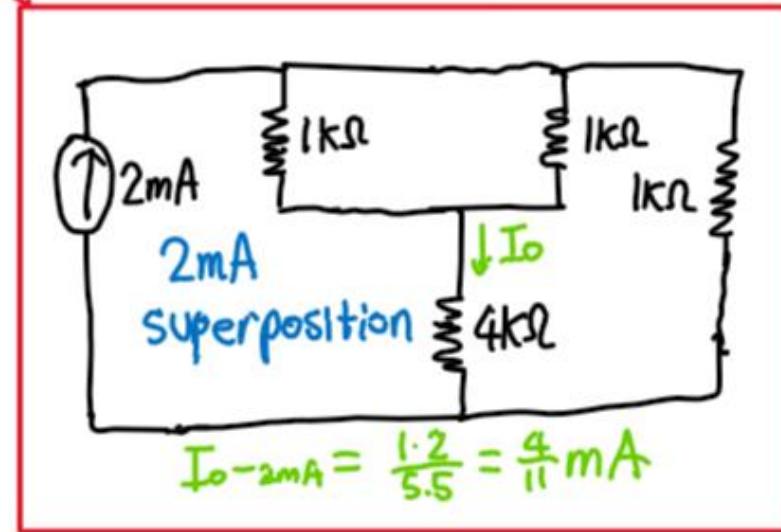
$$I_{o-4V} = \frac{4}{5.5} \approx \frac{8}{11} \text{ mA}$$



$$L_1: I_1 \cdot 1k\Omega + 2 + (I_1 - I_2) 1k\Omega = 0$$

$$L_2: (4+1)k\Omega \cdot I_2 + (I_2 - I_1) 1k\Omega = 0$$

$$\begin{bmatrix} 2 & -1 \\ -1 & 5 \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} 0 \\ -5 \end{bmatrix}$$
$$I_2 = -\frac{2}{11} \text{ A}$$
$$= I_{o-2V}$$

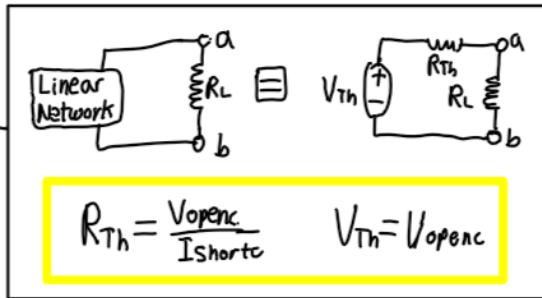


$$I_{o-2mA} = \frac{1 \cdot 2}{5.5} = \frac{4}{11} \text{ mA}$$

13-3

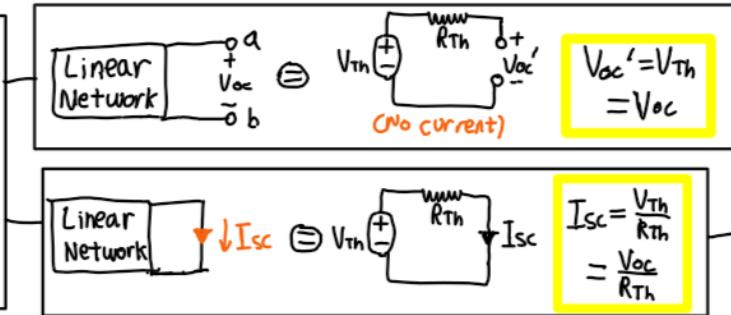
Thevenin / Norton Theorem

Thevenin Theorem



$$R_{Th} = \frac{V_{open}}{I_{short}}$$

$$V_{Th} = V_{open}$$



$$V_{oc}' = V_{Th} = V_{oc}$$

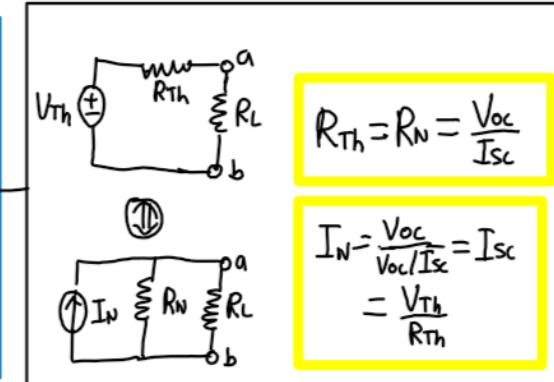
$$I_{sc} = \frac{V_{Th}}{R_{Th}} = \frac{V_{oc}}{R_{Th}}$$

- ① Change R_L into open circuit and get V_{oc}
- ② Change R_L into short circuit and get I_{sc}
- ③ $R_{Th} = \frac{V_{oc}}{I_{sc}}$

Norton Theorem

If there are independent sources

- ① Get V_{oc} .
 - ① Deactivate sources. voltage source \rightarrow short current source \rightarrow open
 - ② Replace R_L into virtual voltage source. Using series/parallel, find equivalent resistor (R_{Th})
 - ③ $R_{Th} = R_N, I_N = I_{sc}$



$$R_{Th} = R_N = \frac{V_{oc}}{I_{sc}}$$

$$I_N = \frac{V_{oc}}{V_{oc}/I_{sc}} = I_{sc} = \frac{V_{Th}}{R_{Th}}$$

If Question asks

$I_o \rightarrow$ Use loop, mesh, ... analysis methods

$V_{Th} \rightarrow$ Replace R_L into V_{oc} ($= V_{Th}$)

$R_{Th} \rightarrow$ $[V_s \rightarrow$ short $I_s \rightarrow$ open $R_L \rightarrow$ voltage (imaginary)]

Get net resistance

Multiple Thevenin usage



$$V_{oc} = 12 \cdot \frac{6}{3+6} = 8V$$

$$R_{Th} ? = 4k\Omega$$

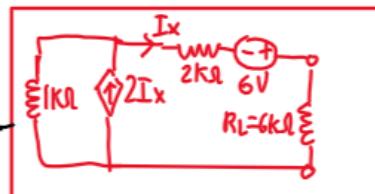
$$8V$$

$$R_{Th} = 8k\Omega$$

$$V_{8k\Omega} = 16V$$

$$V_o = 8V$$

Controlling variables in dependent sources cannot be separated



$$I_x = 0, 2I_x = 0, V_{oc} = 6V$$

$$\text{Supermesh}$$

$$2I_1 + I_2 = 6$$

$$I_{sc} = 6mA$$

$$R_{Th} = 1k\Omega$$

$$\frac{V_x}{2000} \leftarrow 2k\Omega \rightarrow -U_x + 4k\Omega \rightarrow 3V$$

$$I_4 + 2mA = \frac{V_x}{2000}$$

$$V_x + 8V = 2V_x$$

$$V_x = 8V$$

$$V_{oc} = \frac{V_x}{2k} + 2k + 3 = 11V$$

$$I_2 = 1.5mA$$

$$R_{Th} = 2k\Omega$$

$$I_4 + 2mA = \frac{V_x}{2k}$$

$$I_{sc} = 5.5mA$$

Ex: V_{Th}, R_{Th} in terms of R_L

$$oR_L \rightarrow V_{oc}$$

$$I_1 R_1 + I_2 (R_2 + R_3) = V_s$$

$$I_2 - I_1 = I_s \quad \text{current divider}$$

$$10R_1 + 30R_2 = 50$$

$$I_2 - I_1 = 1.5$$

$$I_2 = \frac{13}{8}A$$

$$V_{Th} = V_{oc} = V_{ab} = \frac{13}{8} \times 20 = 32.5V$$

$$oR_L \rightarrow I_{sc}$$

$$I_2 - I_1 = I_s$$

$$R_1 I_1 + R_2 I_2 = V_s$$

$$I_2 - I_1 = 1.5$$

$$10I_1 + 10I_2 = 50$$

$$I_{sc} = I_2 = 3.25A$$

$$R_{Th} = \frac{V_{oc}}{I_{sc}} = 10\Omega$$

$$V_{Th} = 32.5V$$

$$I_L \downarrow R_L$$

$$I_N = -3.25A$$

$$R_N = \frac{V_{Th}}{I_N} = 10\Omega$$

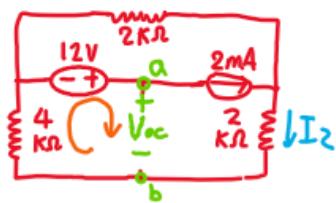
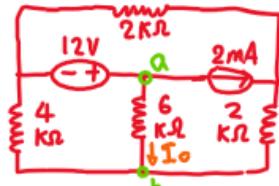
Using Norton

$$① \text{ Deactivate sources.}$$

$$R_{Th} = 10\Omega$$

$$② \text{ Virtual voltage source.}$$

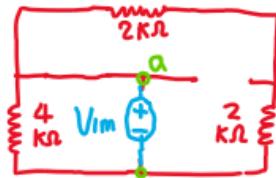
Ex Thevenin/Norton
→ Find I_o



$$I_z = 2\text{mA} \cdot \frac{2\text{k}\Omega}{(2+6)\text{k}\Omega} = 0.5\text{mA}$$

$$V_{oc} + \frac{1}{2}\text{mA} \cdot 4\text{k}\Omega = 12\text{V}$$

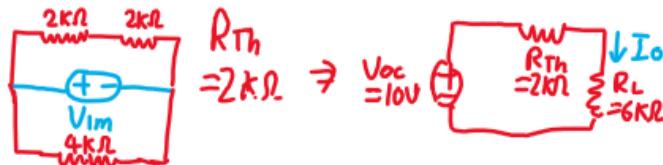
$$V_{oc} = V_{Th} = 10\text{V.}$$



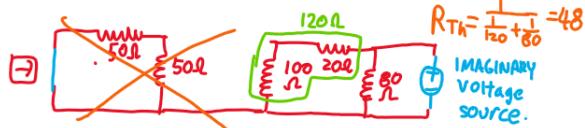
$$I_o = \frac{10\text{V}}{(2+6)\text{k}\Omega}$$

$$= 1.25\text{mA.}$$

$$P_{dissipated} = I_o^2 R.$$



Exam Thevenin
→ power in R_L .



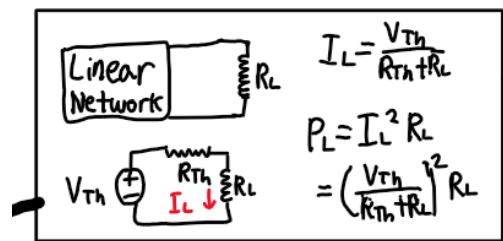
$$I_L = \frac{V_{oc}}{R_{th} + R_L} = \frac{800}{48 + 100} = 5.405\text{A}$$

$$V_{RL} = I_L R_L = 540.5 \cdot 100 = 54054\text{V}$$

$$P_{RL} = V_{RL} I_L = 2921.84\text{W}$$

13-4

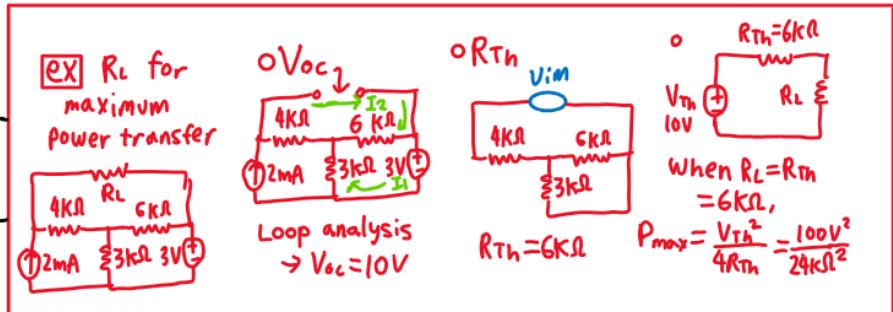
Maximum Power Transfer



Max. P_L in terms of R_L

$$\frac{dP_L}{dR_L} = V_{Th}(R_L + R_{Th})(R_L - R_{Th})$$

$$P_{L\max} = P_{out\max} = \frac{V_{Th}^2 R_{Th}}{4 \cdot R_{Th}^2} = \frac{V_{Th}^2}{4 R_{Th}}$$



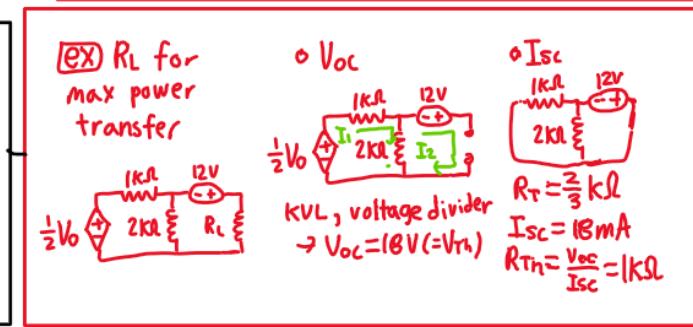
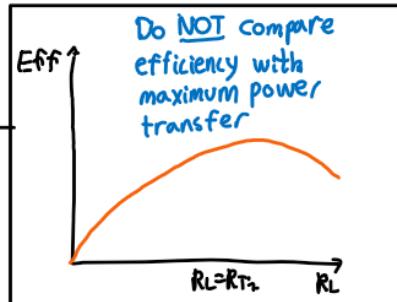
- Efficiency

$$= \frac{P_{out}}{P_{in}}$$

(dissipated by load)
(supplied)

$$P_{in} = \frac{V_{Th}^2}{R_L + R_{Th}}$$

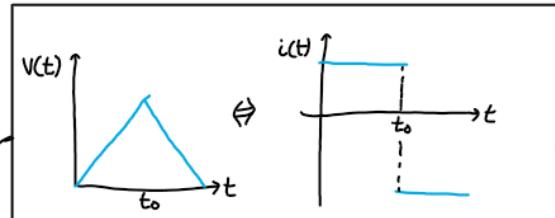
$$P_{out} = \frac{V_{Th}^2 R_L}{(R_L + R_{Th})^2}$$



14-1 Capacitors

$+ V_c(t) -$

 $i_c(t)$
 $q(t) = C \cdot V_c(t)$
 $i_c(t) = \frac{dq(t)}{dt}$
 $= C \cdot \frac{dV_c(t)}{dt}$



$$\begin{aligned} dV &= \frac{1}{C} i(t) dt \\ V(t) &= \int_{t'=t_0}^{t'=t} \frac{1}{C} i(t') dt' \\ dV &= \frac{1}{C} \int_{-\infty}^{t'=t} i(t') dt' \\ V &= \frac{1}{C} \int_{-\infty}^{t'=t_0} i(t') dt' + \frac{1}{C} \int_{t'=t_0}^{t'=t} i(t') dt' \\ V &= V(t_0) + \frac{1}{C} \int_{t'=t_0}^{t'=t} i(t') dt' \end{aligned}$$

$$\begin{aligned} P &= \frac{dW}{dt} = V(t)i(t) \\ dW &= CV(t) dV \\ (W = U = \frac{1}{2}CV^2) \\ \int dW &= \int_{-\infty}^{t'=t} CV dV \\ W(t) &= C \int_{-\infty}^{t'=t_0} V dV + C \int_{t'=t_0}^{t'=t} V dV \\ W_c(t) &= \frac{1}{2} C [V(t)]^2 \end{aligned}$$

What if V is discontinuous?
 $i \rightarrow \infty$, not possible
 V_c must be continuous
 $V_c(t_0^-) = V_c(t_0^+)$

What if There is DC signal $i_c = 0$
 To DC signal, capacitor looks like
open circuit

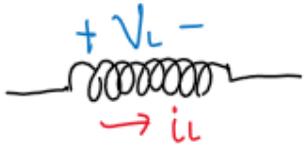
Ex Current through capacitor $C=4F$.
 $V(t), P(t), W_c(t)$

$t[s]$	$i(t)$	$v(t)$	$P(t)$	$W_c(t)$
$(-\infty, 0)$	0	0	0	0
$[0, 2]$	$8t$	$\frac{0+t}{2} = \frac{t}{2}$	$8t^3$	$2t^4$
$[2, 4]$	-8	$-2t + 8^{(1)}$	$16t - 128$	$2(8-2t)^2$
$[4, \infty)$	0	0	0	0

$I = V(2) + \frac{1}{2} \int_2^t i(t) dt$
 $= 4 + \frac{1}{2}[-8]_2^t = -2t + 8$

14-2

Inductors



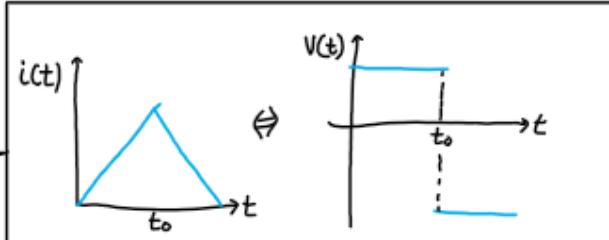
$$L = \frac{N\phi_B}{i}$$

$$L_i = N\phi_B$$

$$L \frac{di}{dt} = N \frac{d\phi_B}{dt}$$

$$= V_L = -E$$

$$V_L = L \frac{di_L}{dt}$$



$$di = \frac{1}{L} V(t) dt$$

$$i(t) = i(t_0) + \frac{1}{L} \int_{t'=t_0}^{t=t} V(t') dt'$$

$$P(t) = V(t) I(t)$$

$$= i(t) L \frac{di}{dt}$$

$$dW = L i(t) di$$

$$W = \int_{-\infty}^{t=t} L i(t) di$$

$$W = \frac{1}{2} L [i(t)]^2$$

What if I is discontinuous?
 $V(t) \rightarrow \infty \Rightarrow$ impossible.

I_L should be continuous
 $i_L(t_0^-) = i_L(t_0^+)$

What if There is DC signal $V_L = 0$
 Inductor regarded as short circuit



14-3

Capacitor -
Inductor
Combinations



	SERIES	PARALLEL
Inductor	$L_T = \sum_i L_i$	$\frac{1}{L_T} = \sum_i \frac{1}{L_i}$
Capacitor	$\frac{1}{C_T} = \sum_i \frac{1}{C_i}$	$C_T = \sum_i C_i$
Resistor	$R_T = \sum_i R_i$	$\frac{1}{R_T} = \sum_i \frac{1}{R_i}$

15 -1

Introduction to transient circuits

$$C \frac{dV_c(t)}{dt} + \frac{V_c(t)}{R} = 0$$

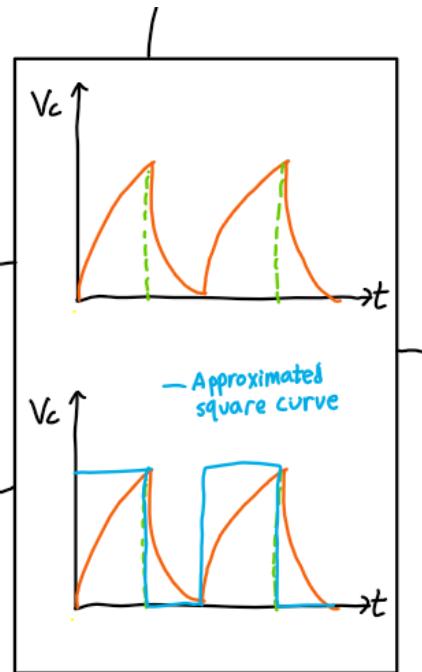
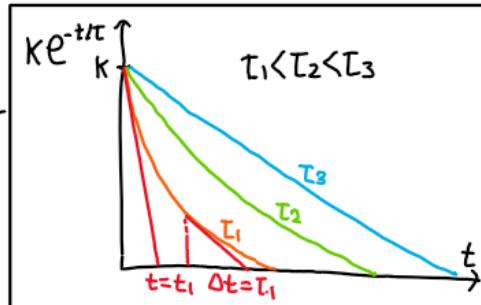
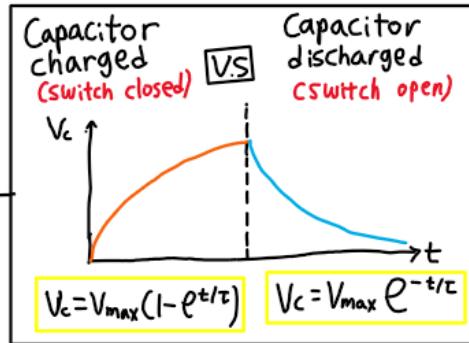
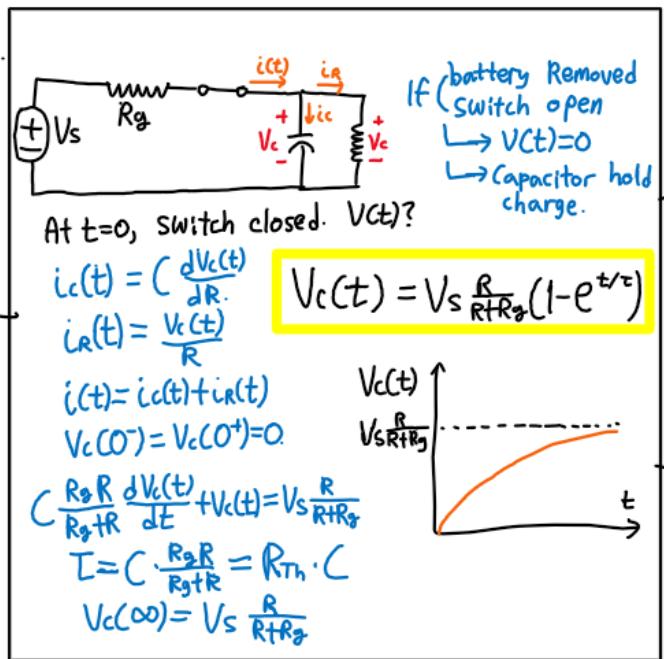
$$\frac{dV_c(t)}{dt} + \frac{V_c(t)}{RC} = 0$$

$$V_c(t) = V_0 e^{-\frac{t}{RC}}$$

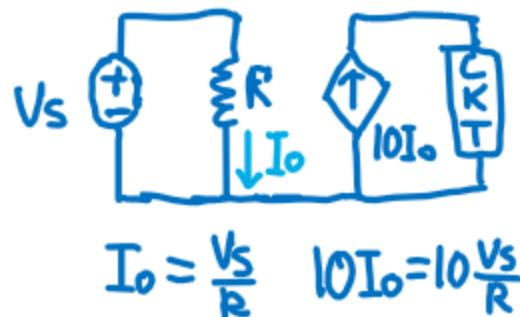
15-2

First-order transient circuits

Resistor
—
Capacitor



Do not confuse
Cdependent
source)



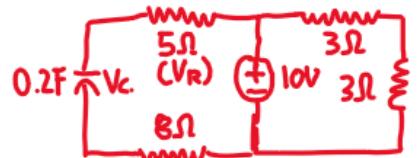
Ex At $t=0$, switch A \rightarrow B
Find $V_c(t)$ & $V_R(t)$ for $0 \leq t < \infty$



$0 - \infty < t < 0^-$



$0^+ \leq t < \infty$



$$V_R(0^-) = 0V$$

$$V_c(0^-) = 1A \cdot 4\Omega = 4V$$

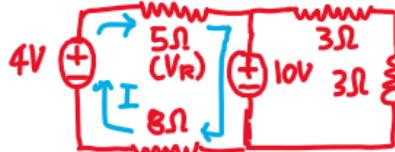
(No current passing)

$$V_c(\infty) = 10V$$

$$V_R(\infty) = 0V$$

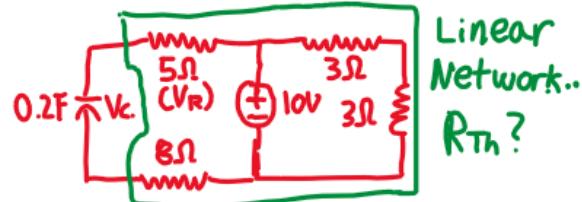
(no current)

$\cdot t=0^+$. Replace capacitor to $\oplus 4V$...

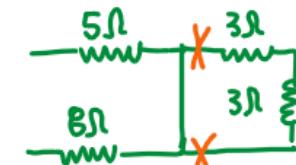


$$13I + 10 = 4$$

$$V_R(0^+) = I \cdot 5 = -\frac{6}{13} \cdot 5 = -2.3V.$$



Linear Network...
 R_{Th} ?



$$R_{Th} = 13\Omega$$

$$I = R_{Th}; C = 2.6s$$

Answer: $0^+ \leq t < \infty$

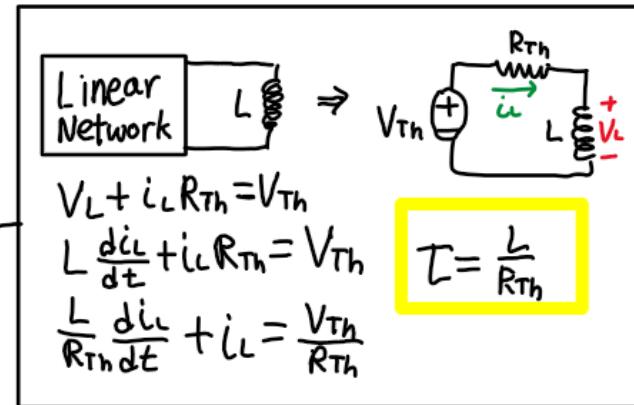
$$V_c(t) = 10 - 6e^{-t/2.6}$$

$$V_R(t) = -2.3e^{-t/2.6}$$

$$V(t) = V(\infty) + (V(t_0) - V(\infty)) e^{-t/\tau}$$

$$\tau = R_{Th} \cdot C = \frac{L}{R_{Req}}$$

Resistor
—
Inductor



EX) Calculate $V_o(t)$ for time interval $-\infty < t < 1, 1 < t < 2, 2 < t < \infty$



① $-\infty < t < 1$
 $V_s(t) = 0, V_o(1^-) = 0$
 $V_o(1^-) \neq V_o(1^+)$
 Not necessary but conservation of charge
 $I_o(1^-) = I_o(1^+)$
 $V_o(1^-) = V_o(1^+) = 0$

② $1 < t < 2$
 Steady state
 V_{o1-2} ?
 \downarrow
 $V_o(\infty) = 4V$

Time constant R_{Th} ? $\tau = \frac{L}{R_{Th}}$
 $R_{Th} = 3\Omega, \tau = \frac{2}{3}s$
 $V_o(t) = 4(1 - e^{-\frac{2}{3}(t-1)/2})$
 $V_o(2^-) = 3.11V$
 ③ $2 < t < \infty$
 $V_o(\infty) = 0, \tau = \frac{2}{3}$
 $V_o(2^-) = V_o(2^+) = 3.11V$
 $V_o(t) = 3.11e^{-\frac{2}{3}(t-2)/2}$

16-A

Complex Numbers

$$\begin{aligned} z &= x + jy = |z| e^{j\theta} \\ &= \sqrt{x^2 + y^2} e^{j \tan^{-1}(y/x)} \\ &= |z| \angle \theta \end{aligned}$$

Rectangular $x + y i$

$$-\frac{\pi}{2} \leq \tan^{-1} \theta \leq \frac{\pi}{2}$$

$$\theta = \tan^{-1}\left(\frac{y}{x}\right)$$

Polar $r(\cos \theta + j \sin \theta)$

$$\begin{aligned} j &= \sqrt{-1} = 1 \angle \frac{\pi}{2} = e^{j\frac{\pi}{2}} = \cos \frac{\pi}{2} + j \sin \frac{\pi}{2} \\ -j &= 1 \angle -\frac{\pi}{2} = e^{-j\frac{\pi}{2}} = \frac{1}{j} \\ 1 &= e^{j0} = 1 \angle 0 \\ -1 &= j \cdot j = e^{j\pi} = 1 \angle \pi \end{aligned}$$

Euler
(exponential)

$$r e^{j\theta}$$

$$e^{j\theta} = \cos \theta + j \sin \theta$$

$$A e^{j\theta} = A(\cos \theta + j \sin \theta)$$

$$\sin(wt + \theta) = \cos(wt + \theta - \frac{\pi}{2})$$

$$\cos(wt + \theta) = \sin(wt + \theta + \frac{\pi}{2})$$

$$-\sin(wt + \theta) = \sin(wt + \theta - \pi)$$

$$-\cos(wt + \theta) = \cos(wt + \theta + \pi)$$

$$z = x + jy$$

$$\operatorname{Re}[z] = x$$

$$\operatorname{Im}[z] = y$$

$$\bar{z} = x - jy$$

Conjugate

$$\begin{aligned} z_1 &= x_1 + y_1 j \\ z_2 &= x_2 + y_2 j \end{aligned}$$

$$z_1 + z_2 = (x_1 + x_2) + j(y_1 + y_2)$$

$$z_1 - z_2 = (x_1 - x_2) + j(y_1 - y_2)$$

$$z_1 \times z_2 = (x_1 x_2 - y_1 y_2) + j(x_1 y_2 + x_2 y_1)$$

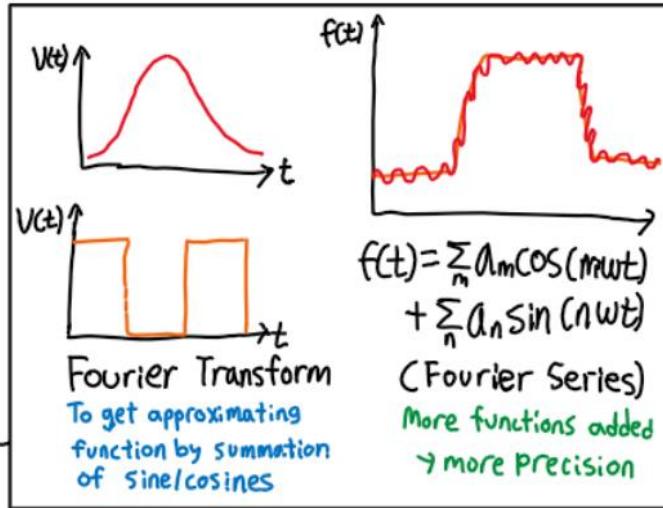
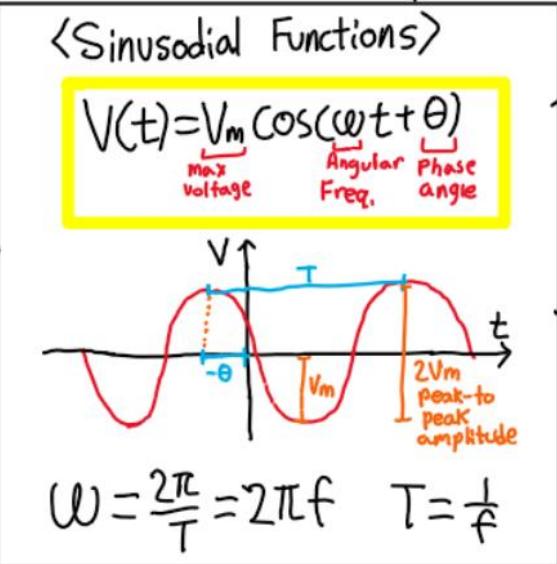
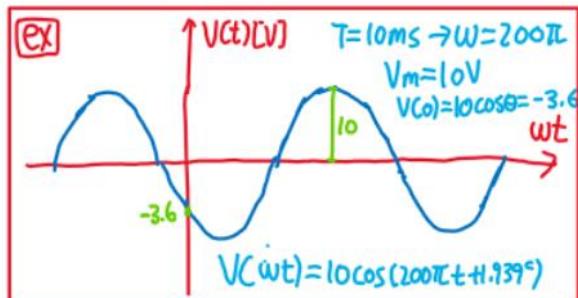
$$\frac{z_1}{z_2} = \frac{z_1 \cdot \bar{z}_2}{z_2 \cdot \bar{z}_2} = \frac{(x_1 x_2 + y_1 y_2) + j(x_2 y_1 - x_1 y_2)}{x_2^2 + y_2^2}$$

$$z = |z| e^{j\theta} = |z| \angle \theta$$

$$z_1 z_2 = |z_1 \cdot z_2| \angle \theta_1 + \theta_2$$

$$\frac{z_1}{z_2} = \frac{|z_1|}{|z_2|} \angle \theta_1 - \theta_2$$

16-1 Sinusodials



Ex

$$i_1(t) = 2 \sin(400t + 45^\circ)$$

$$i_2(t) = \cos(400t + 10^\circ)$$

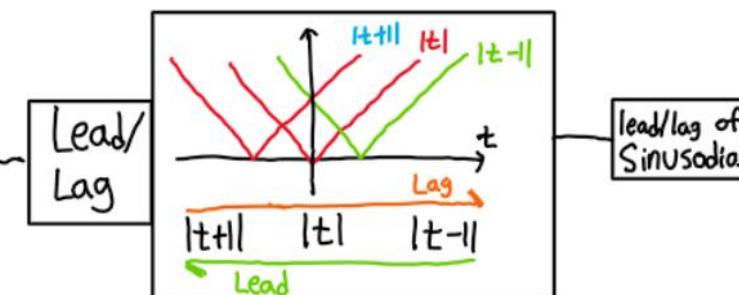
$$= \sin(400t + 100^\circ)$$

$$i_3(t) = -\frac{1}{4} \sin(400t + 60^\circ)$$

$$= \frac{1}{4} \sin(400t - 120^\circ)$$

Lag Lead

$i_3 = 165^\circ$ $i_1 = 55^\circ$ i_2



- Same frequency (f)
- All functions → all Sine or Cosine
- All amplitudes → all positive or negative
- $0 \leq \text{separation} < 180^\circ$

16

2 Complex forcing
functions, phasors,
impedance and
admittance

$$V(t) = V_m \cos(\omega t + \theta_v)$$

$$= \operatorname{Re}[V_m e^{j\omega t + \theta_v}]$$

$$= \operatorname{Re}[V_m e^{j\theta_v} e^{j\omega t}]$$

$$= \operatorname{Re}[\underline{V} e^{j\omega t}]$$

$$\underline{V}_{\text{phasor}} = V_m e^{j\theta_v} = V_m \angle \theta_v$$

$$i(t) = I_m \sin(\omega t + \theta_i)$$

$$V(t) = V_m \sin(\omega t + \theta_v)$$

$$= V_m \cos(\omega t + \theta_v - \frac{\pi}{2})$$

$$= \operatorname{Re}[V_m e^{j(\omega t + \theta_v - \frac{\pi}{2})}]$$

$$= \operatorname{Re}[V_m e^{j(\theta_v - \frac{\pi}{2})} e^{j\omega t}]$$

$$= \operatorname{Re}[\underline{I} e^{j\omega t}]$$

$$\underline{I} = V_m e^{j(\theta_v - \frac{\pi}{2})} = V_m \angle \theta_v - \frac{\pi}{2}$$

$$V(t) = V_m \cos(\omega t + \theta_v) = \operatorname{Re}[\underline{V} e^{j\omega t}]$$

$$i(t) = I_m \cos(\omega t + \theta_i) = \operatorname{Re}[\underline{I} e^{j\omega t}]$$

$$V(t) = L \frac{di(t)}{dt}$$

$$\operatorname{Re}[\underline{V} e^{j\omega t}] = \operatorname{Re}[L \frac{d}{dt} \underline{I} e^{j\omega t}]$$

$$= \operatorname{Re}[L j\omega \underline{I} e^{j\omega t}]$$

$$\underline{V} = j\omega L \underline{I}$$

$$\underline{Z}_L = j\omega L \quad [\Omega]$$

$$\underline{I} = \frac{\underline{V}}{j\omega L} = \frac{V_m}{\omega L} \angle \theta_v - \frac{\pi}{2}$$

$$= I_m \angle \theta_i \quad (\theta_i = \theta_v - \frac{\pi}{2})$$

$$I_m = \frac{V_m}{\omega L}$$

$$i(t) = \frac{V_m}{\omega L} \cos(\omega t + \theta_v - \frac{\pi}{2})$$

$$Z = \frac{\underline{V}}{\underline{I}} \quad [\Omega]$$

impedance

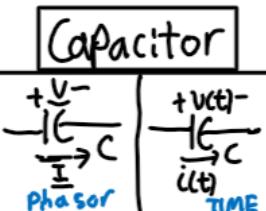
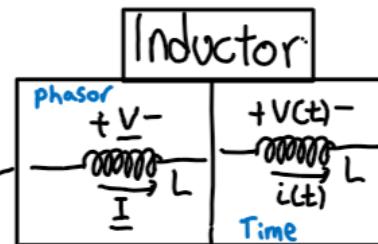
$$= Z_{R\text{eff}} + j Z_{L\text{m}}$$

$$= R + j X$$

$$Y = \frac{1}{Z} = G + j B$$

Admittance

Conductance Susceptance



$$Z_R = R \quad [\Omega]$$

$$V_R(t) = I_R(t) \cdot R$$

$$V(t) = V_m \cos(\omega t + \theta_v) = \operatorname{Re}[\underline{V} e^{j\omega t}]$$

$$i(t) = I_m \cos(\omega t + \theta_i) = \operatorname{Re}[\underline{I} e^{j\omega t}]$$

$$i(t) = C \frac{dV(t)}{dt}$$

$$\operatorname{Re}(I e^{j\omega t}) = C \frac{d}{dt} \operatorname{Re}(e^{j\omega t})$$

$$= \operatorname{Re}(C \underline{V} j\omega e^{j\omega t})$$

$$I_m \angle \theta_i = \omega C L \frac{\pi}{2} V_m \angle \theta_v$$

$$\theta_i = \theta_v + \frac{\pi}{2}$$

$$I_m = \omega C V_m$$

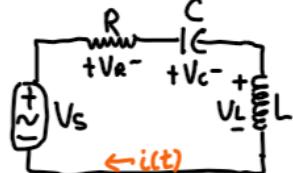
$$i(t) = V_m \omega C \cos(\omega t + \theta_v + \frac{\pi}{2})$$

$$\underline{Z}_1 + \underline{Z}_2 + \underline{Z}_3 = \underline{Z}_{\text{eq}}$$

$$\underline{Z}_{\text{eq}} = \frac{1}{\underline{Z}_{\text{eq}}} = \frac{1}{Z_1} + \frac{1}{Z_2} + \frac{1}{Z_3}$$

Case

$$V_S = V_m \cos(\omega t + \theta_v)$$



$$\underline{V}_S = \underline{V}_R + \underline{V}_C + \underline{V}_L$$

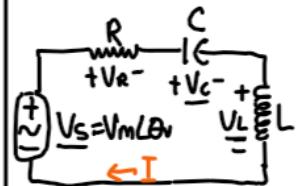
$$\underline{V}_R = R \underline{I}_R \quad \underline{V}_C = -\frac{j}{\omega C} \underline{I}_C$$

$$\underline{V}_L = j \omega L \underline{I}_L$$

$$V_m \angle \theta_v = I (CR + j(\omega L - \frac{1}{\omega C}))$$

$$I = \frac{V_m \angle \theta_v}{R + j(\omega L - \frac{1}{\omega C})} \quad \phi = \tan^{-1} \frac{\omega L - \frac{1}{\omega C}}{R}$$

$$= \frac{V_m}{\sqrt{R^2 + (\omega L - \frac{1}{\omega C})^2}} \angle \theta_v - \phi$$

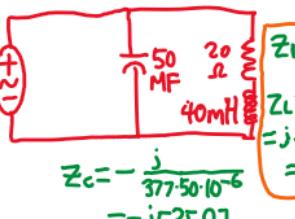


$$i(t) = \frac{V_m}{\sqrt{R^2 + (\omega L - \frac{1}{\omega C})^2}} \cos(\omega t + \theta_v - \phi)$$

Ex

$$V_S(t) = 120 \sin(37t + 60^\circ)$$

$$120 \cos(37t - 30^\circ)$$



$$\begin{aligned} Z_R &= 20\Omega \\ Z_L &= j\omega L = j37 \cdot 40 \cdot 10^{-3} = j15[\Omega] \\ Z_C &= -\frac{j}{\omega C} = -j53[\Omega] \\ Z_T &= \frac{(20+j15)(-j53)}{20+(15-53)} \\ &= \frac{795-j1060}{20-38} \\ &= 30.5 + j4.89 \\ &= 30.9 \angle 9.11^\circ [\Omega] \end{aligned}$$

Ex 2 elements in series

$$\omega = 1000 \text{ rad/s} \quad Z_{eq} = 5 + j4$$

$$\begin{aligned} \frac{1}{j5\Omega} &= \frac{1}{1300/\text{s}} \quad Z_{eq} ? \\ Z_L &= j\omega L \quad Z_C = -\frac{j}{\omega C} \\ Z_R &= R \text{ positive imaginary} \rightarrow \text{inductor.} \end{aligned}$$

$$R = 5 \quad Z_L \rightarrow j4 = j1000L \quad L = 0.004$$

$$Z = 5 + j5.2$$

$$j1300L = j5.2$$

Ex For the circuit shown, what should be value of L if current has same phase angle as V_S ?

$$\begin{aligned} \text{a) } & \text{Circuit diagram showing a series RLC circuit with voltage } V_S(t) \text{ across the source and current } I_S(t) \text{ flowing clockwise. Components include a } 100\text{MF capacitor, a } 12\text{V DC voltage source, a } 4\Omega \text{ resistor, and an inductor } L. \\ & V_S = 12 \cos(1000t + 75^\circ) \\ & Z_L = j1000L \\ & Z_C = -10j \\ & L = 10 \text{ mH} \\ & I = \frac{V_S}{4 + j1000L - 10j} \\ & \phi = \tan^{-1} \frac{1000L - 10}{4} \end{aligned}$$

Past Exam

$$10 \cos(200t - 90^\circ)$$

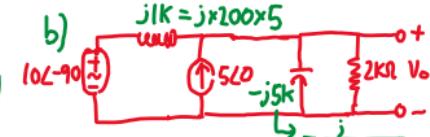
$$V_S(t) = 10 \sin(200t)[V]$$

$$I_S(t) = 5 \cos(200t)[mA]$$

a) Contribution of DC voltage to V_o

b) Impedances

c) contribution of AC sources to $V_o(t)$, use superposition



$$\begin{aligned} b) \quad j1k &= j \times 200 \times 5 \\ 10 \angle -90^\circ & \text{ (AC source)} \\ Z_T &= j + \frac{2(-j5)}{2-j5} \\ &= 10 \angle -90^\circ \left(\frac{-10j}{2-j5} \right) \end{aligned}$$

$$\begin{aligned} &= 10 \angle -90^\circ (0.899 - j0.562) \\ &= 10.6 \angle -122^\circ \end{aligned}$$

$$\begin{aligned} c) \quad j1k & \text{ (DC source)} \\ 10 \angle -90^\circ & \text{ (AC source)} \\ Z_T &= \frac{1}{5k} + \frac{1}{-j5k} + \frac{1}{2k} = \frac{9+5j}{10jk} \end{aligned}$$

$$\begin{aligned} V_{o1} &= 10 \angle -90^\circ \left(\frac{-10j}{\frac{9+5j}{10jk}} \right) \\ &= 10 \angle -90^\circ (0.899 - j0.562) \\ &= 10.6 \angle -122^\circ \end{aligned}$$

$$V_{o2} = 5L0 \cdot Z_T = 5.3 \angle 58^\circ$$

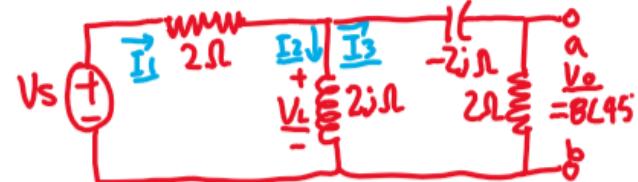
$$V_{ot} = 5.3 \angle -122^\circ$$

$$V_o(t) = \operatorname{Re}(5.3 \angle -122^\circ e^{j200t}) = 5.3 \cos(200t - 122^\circ)$$

16-7

Basic Analysis w/ Kirchhoff's Laws

Ex



a) Voltages/currents shown

$$\underline{I_3} = \frac{8L45}{2} = 4L45$$

$$\underline{V_L} = V_{2-2j} = (2\Omega + 2\Omega j)(2-2j) \\ = 8\sqrt{2}\angle 0$$

$$\underline{I_2} = \frac{8\sqrt{2}\angle 0}{2L90} = 4\sqrt{2}L-90$$

$$\underline{I_1} = (2\Omega + 2\Omega j) - 4\Omega j \\ = 4L-45$$

$$\text{KVL: } \underline{Vs} = \underline{I_1} \cdot 2 + \underline{V_L} \\ = 2 \cdot 4L-45 + 8\sqrt{2}\angle 0 \\ = 12\sqrt{2}-4\sqrt{2}j \\ = 8\sqrt{5}L-18.435$$

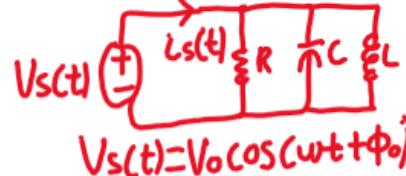
b) Z_{eq} for a-b

$$\begin{aligned} & \text{Circuit diagram: } (2\Omega || 2j\Omega) \leftrightarrow -2j \parallel 2 \\ & Z_{eq} = \frac{1}{\frac{1}{2\Omega} + \frac{1}{2j\Omega} - 2j} \\ & = 0.8 - 0.4j \end{aligned}$$

c) V_{Th} ? ($= V_{oc}$)

$$= 8L45$$

EXAM
TYPE



a) Circuit into phasor domain

$$Vs(t) = V_o \angle \phi_0 \quad Z_C = -\frac{j}{\omega C} \\ Z_R = R \quad Z_L = j\omega L$$

b) $\underline{Z} = \frac{Vs}{I_s}$. ω_0 for $Z \in R$?

$$\frac{1}{Z_{eq}} = \frac{1}{R} + j\omega C - \frac{j}{\omega L} \\ = \frac{L\omega + j(\omega^2 CRL - R)}{RL\omega}$$

$$Z_{eq} = \frac{RL\omega}{L\omega + j(\omega^2 CRL - R)} \\ = \frac{RL\omega [L\omega - j(\omega^2 CRL - R)]}{(L\omega)^2 + (\omega^2 CRL - R)^2}$$

$$R(\omega^2 C_L - 1) = 0 \quad R=0 \text{ or } \omega^2 C_L = 1$$

$$\omega_0 = \frac{1}{\sqrt{CL}}$$

Resonance frequency

$$Z_C|_{\omega=\omega_0} = -\frac{j}{\omega_0 C} \\ = -\sqrt{\frac{L}{C}} j$$

$$Z_L|_{\omega=\omega_0} = j\omega_0 L \\ = j\sqrt{\frac{L}{C}}$$

Phase difference 180°

At $\omega = \omega_0$, $Z_L = -Z_C$

$$I_L Z_L = I_C (-Z_C)$$

$$I_L = -I_C$$