



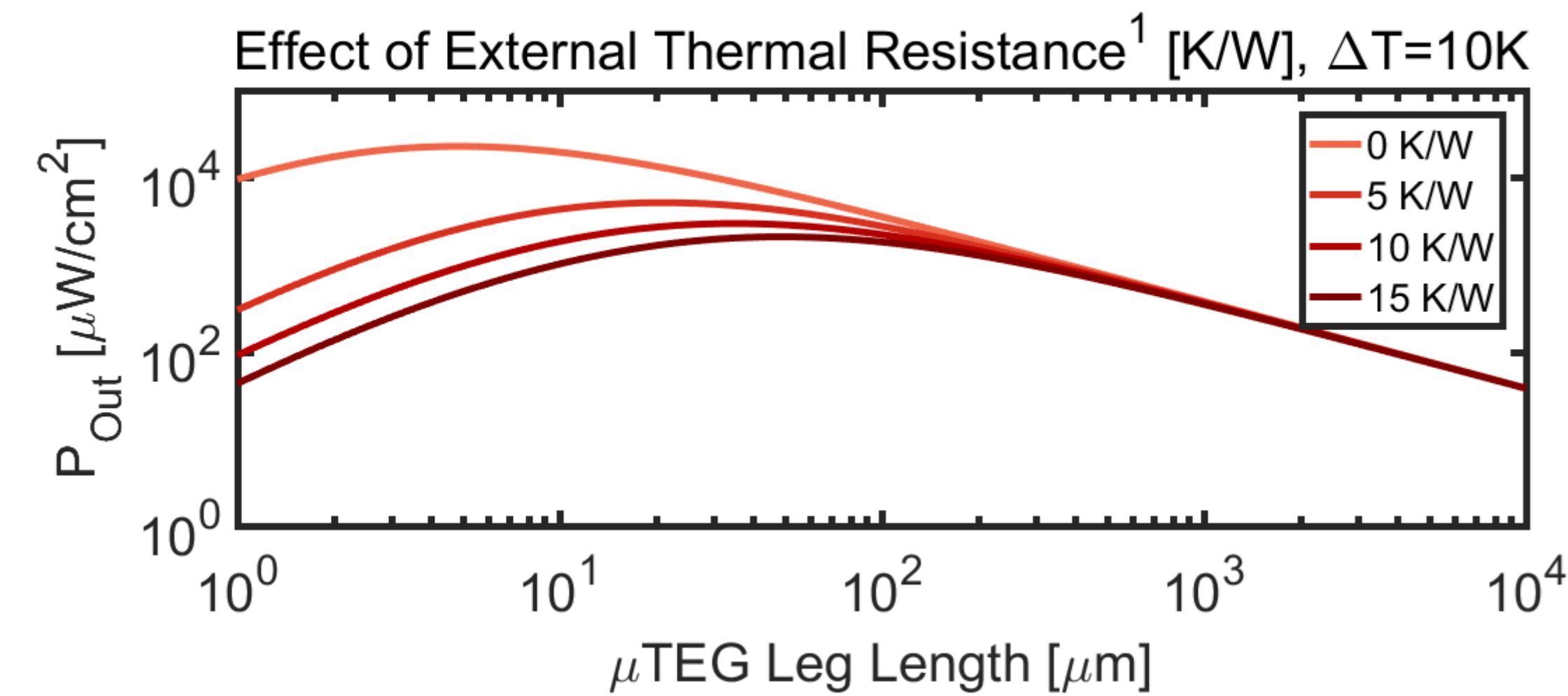
# CFD Modeling and Optimization of Fin Array Packaging Solutions for Micro-Thermoelectric Generator ( $\mu$ TEG) Devices

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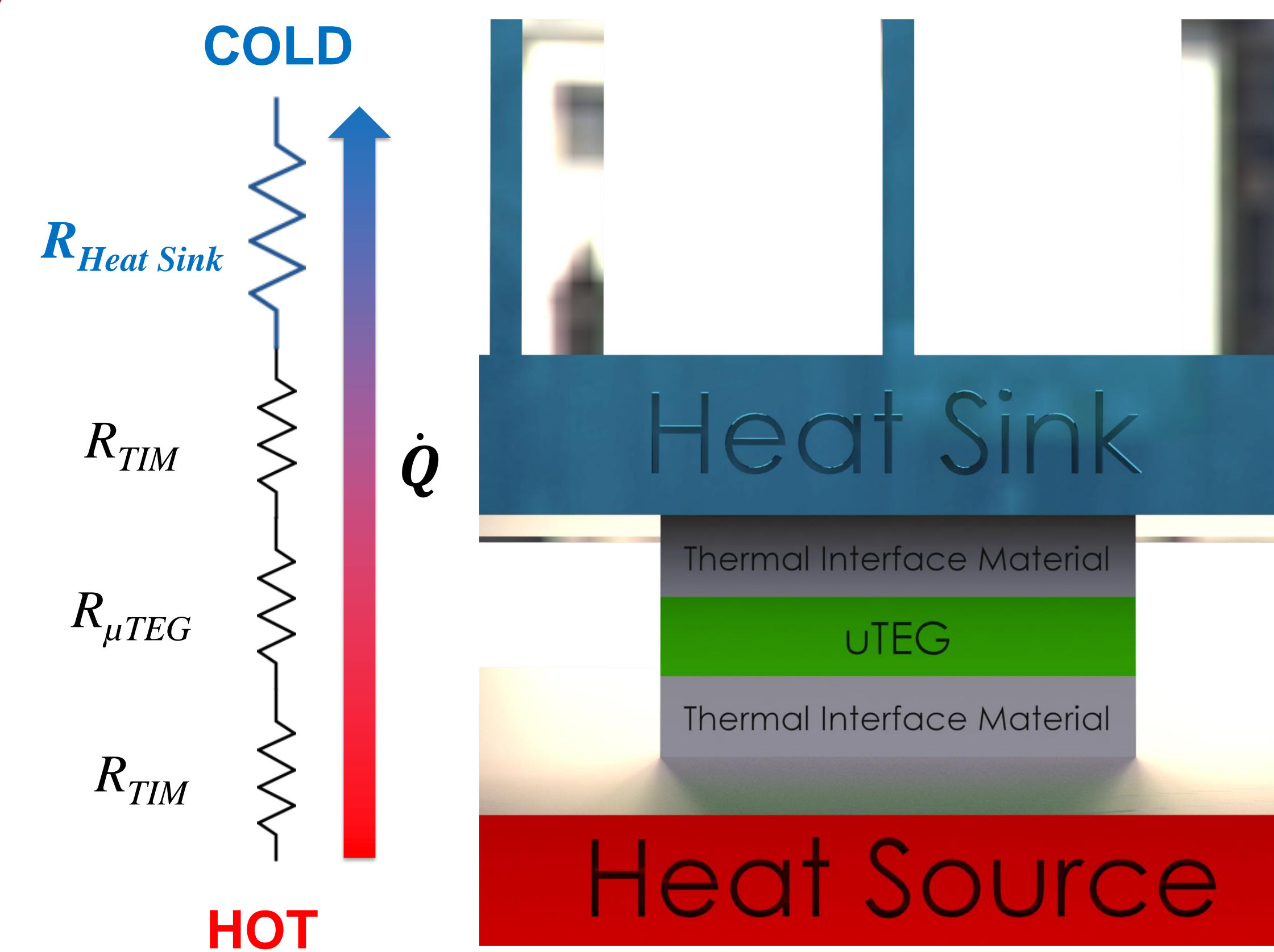
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## Motivation and Background



- Prior work<sup>1</sup> demonstrated that optimization of the thermal packaging is critical for successful implementation of  $\mu$ TEGs.
- The packaging's footprint and thermal resistance are key parameters of this study. A thermal resistance of 20 K/W was adopted as the maximum threshold.



## Simulation Parameters

Comsol Multiphysics: Non-Isothermal Flow

- Heat Transfer
- Laminar Flow

Physical Parameters:

- $\Delta T = T_{\text{TEG}} - T_{\infty}$
- $h$  = height of fins
- $n$  = number of fins
- $t$  = thickness of plate fins
- $d$  = diameter of pin fins
- $w$  = width of heat sink's base (footprint)

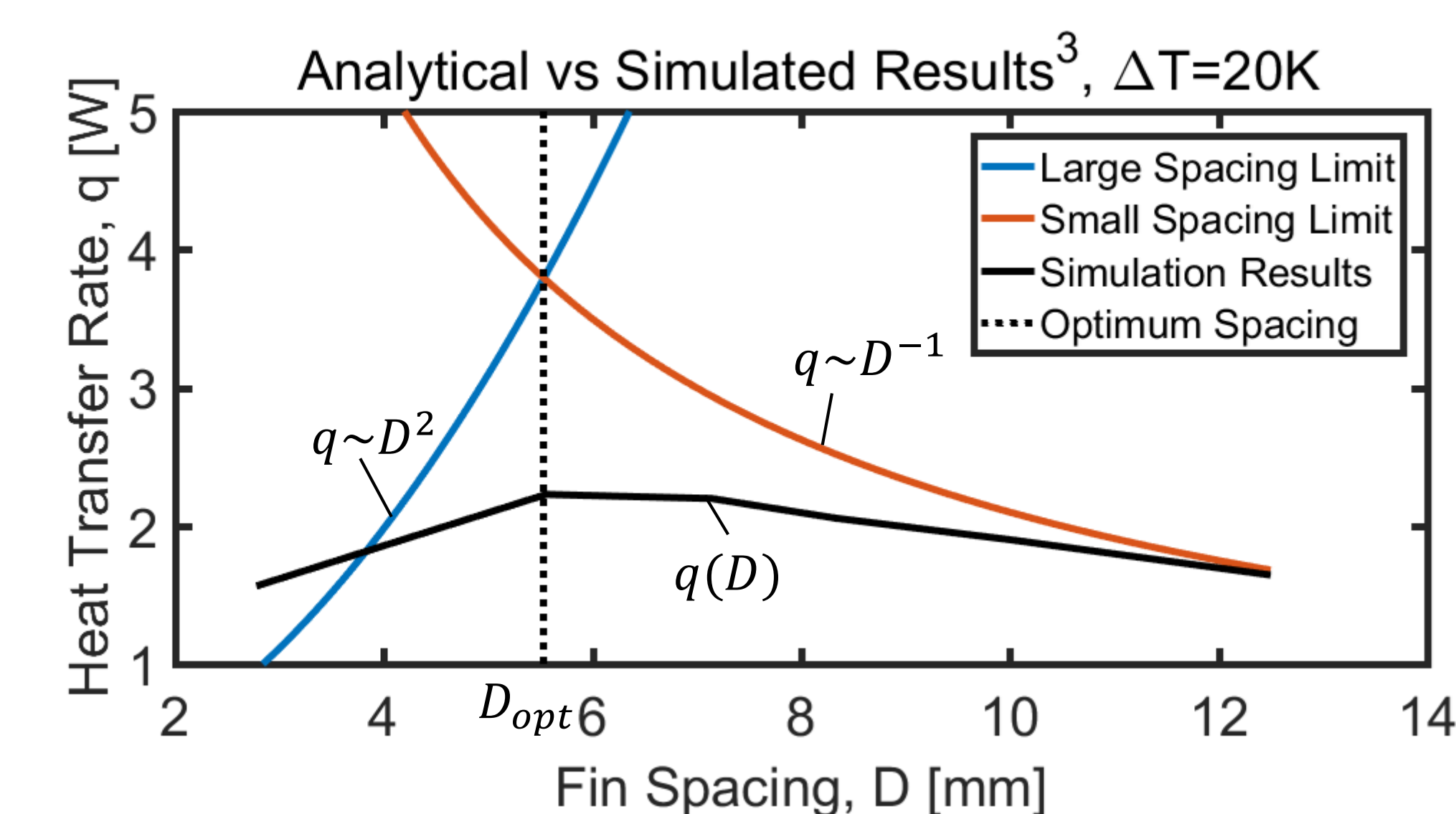
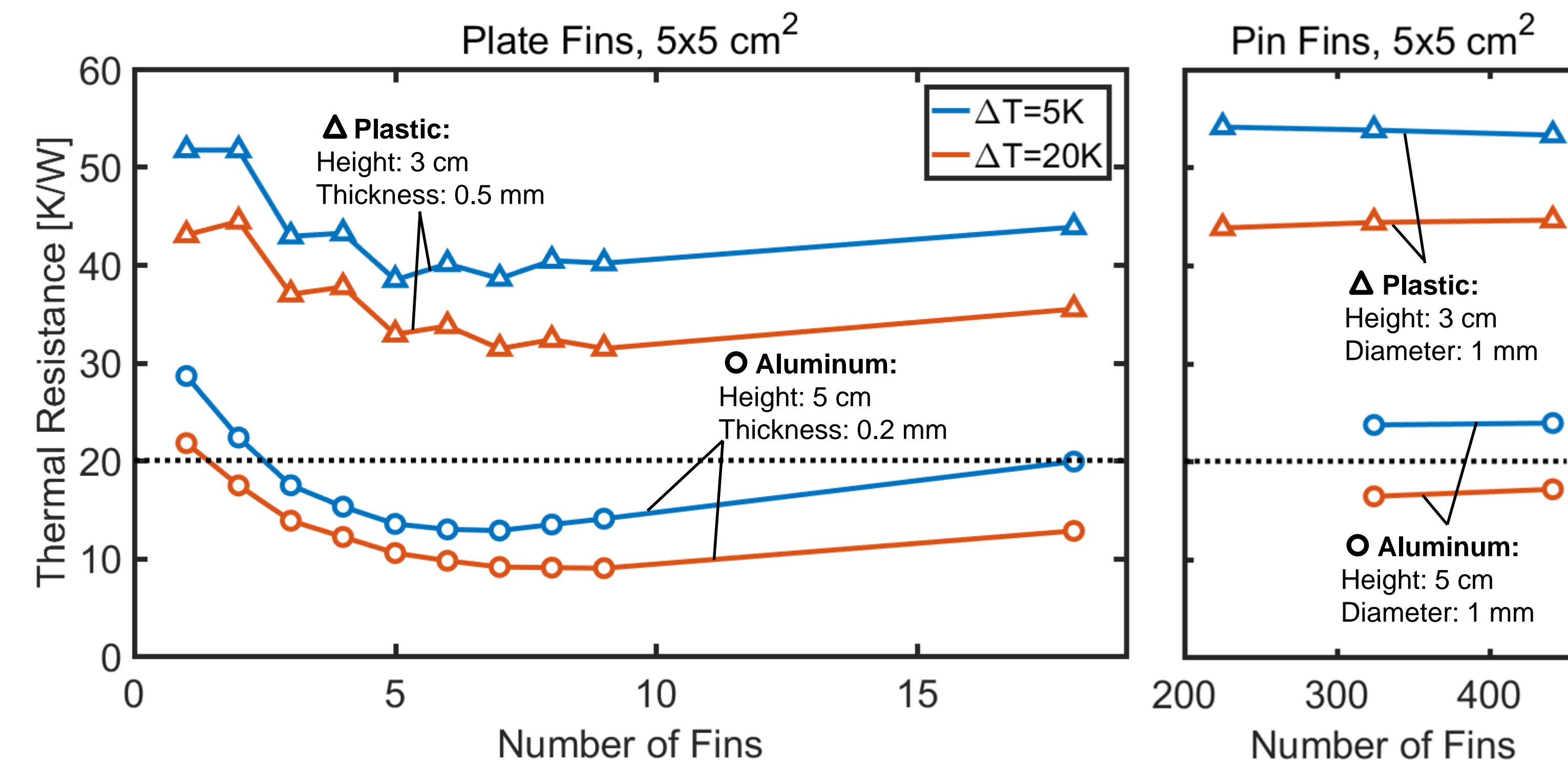
Fin heights were determined using:

- Healing length calculations.
- Max heat fin dimensions:  $5 \times 5 \text{ cm}^2$

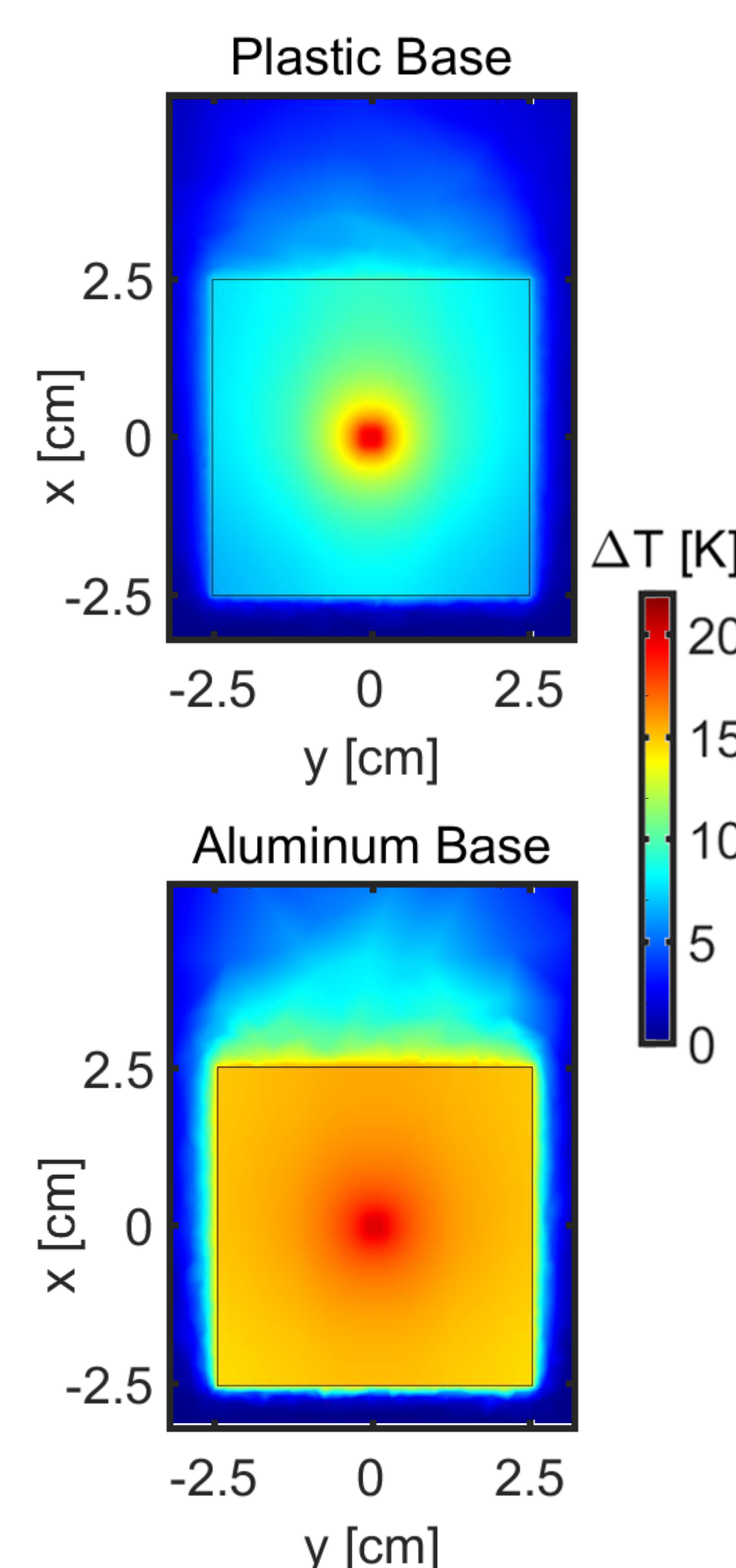
Material	Plastic	Aluminum
Thermal Conductivity [W/m-K]	20	170
Boundary Conditions	Natural Convection	Forced Convection
Fluid	All walls: no slip	Inlet velocity = $v$ [m/s] Outlet gage pressure = 0 Pa Other walls: no slip
Volume Force	Gravity parallel to x-axis.	Not specified
Temperature	Outer walls = 298 K	Inlet wall = 298 K Other outer walls insulating
$\mu\text{TEG} = 298 \text{ K} + \Delta T$		

$$\text{Thermal Resistance} = \frac{\Delta T}{\text{heat flux through } \mu\text{TEG} * \text{surface area of } \mu\text{TEG}}$$

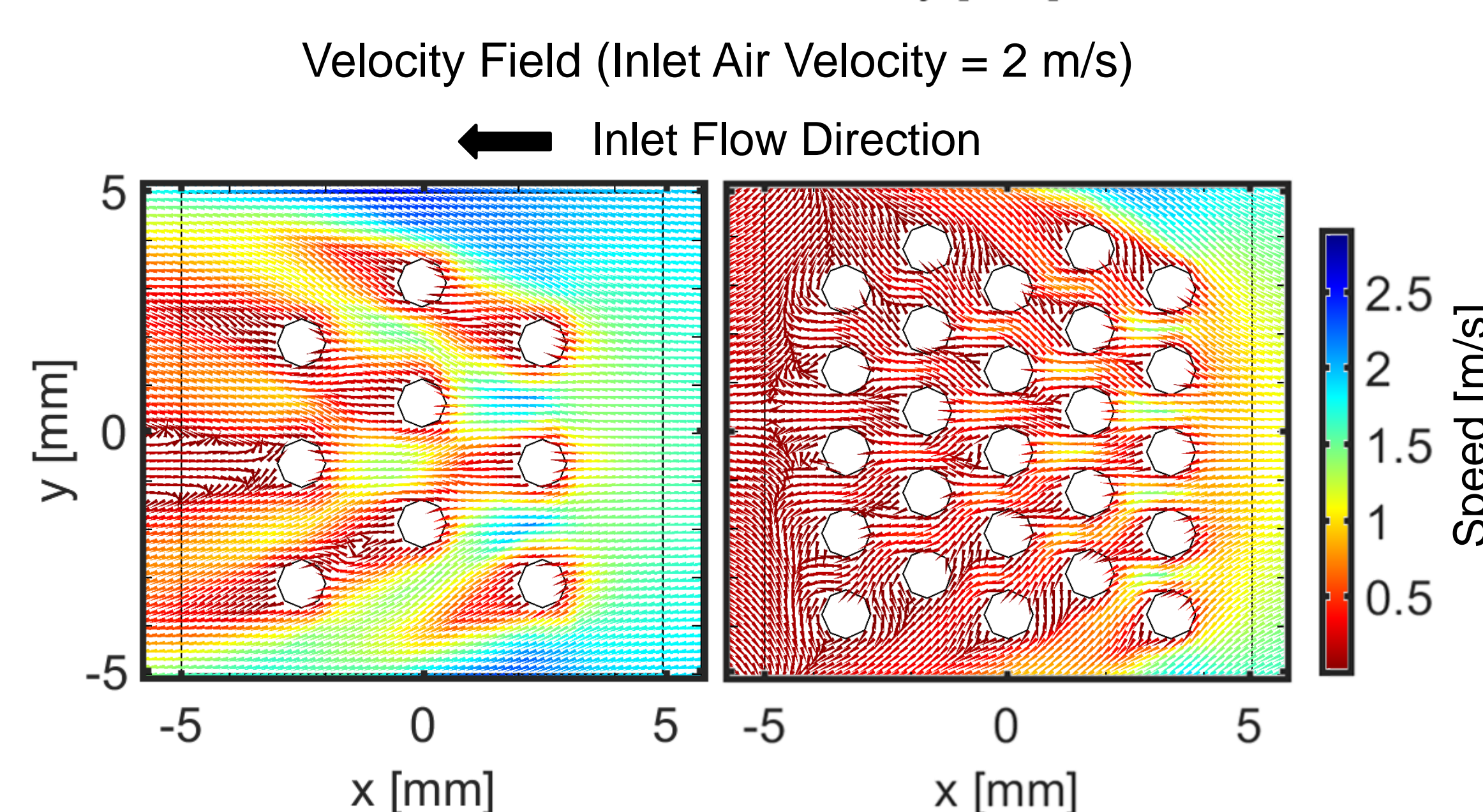
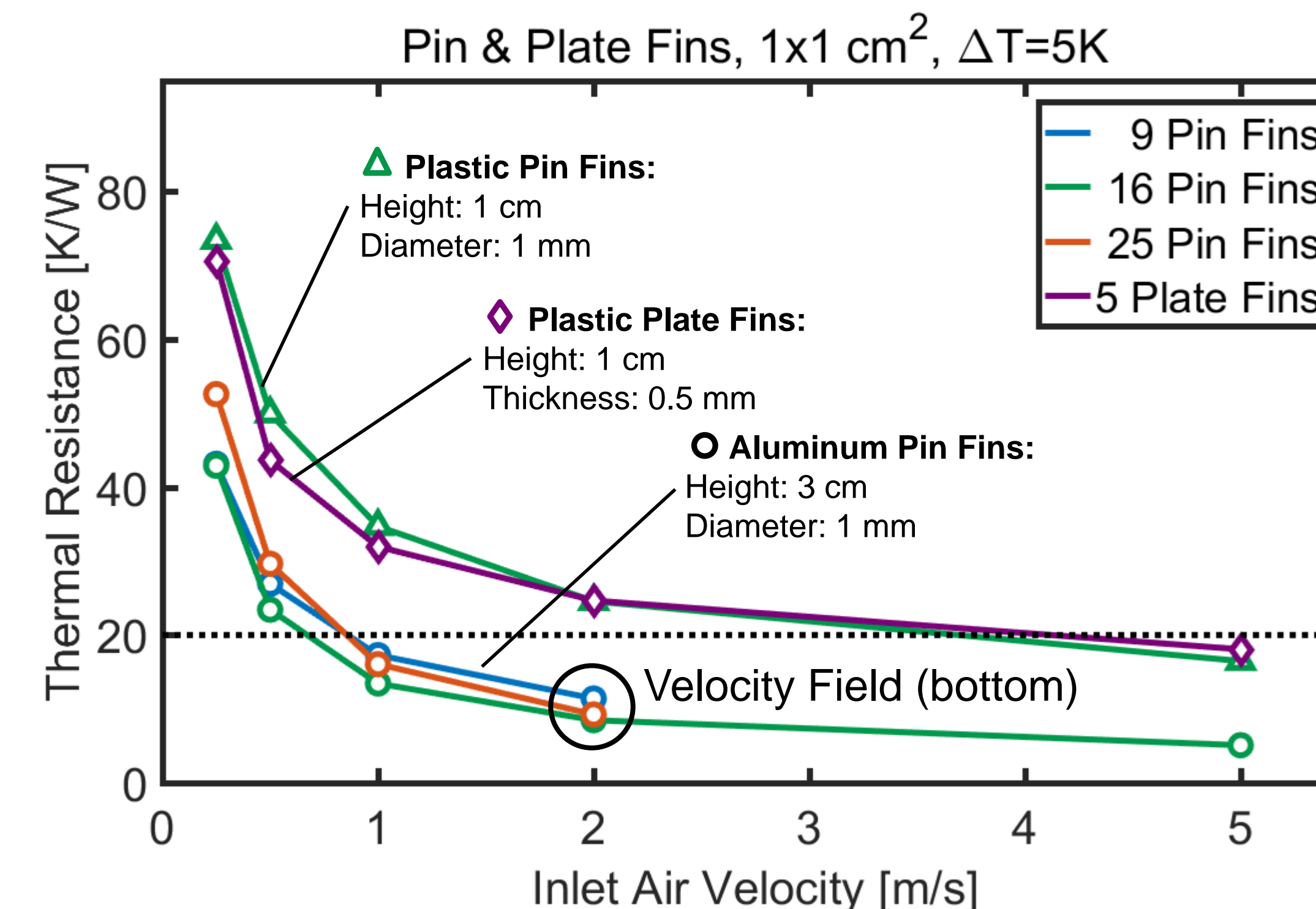
## Natural Convection



- While plate fins have clearly defined optimum number of fins, pin fins' performance change marginally with increasing number of fins.
- The jagged behavior of the plastic plate fins is a result of the centering of plate fins over the heat source.
- The simulation's results ( $\Delta T = 20 \text{ K}$ ) agree with the analytical method's prediction<sup>3</sup> of the optimum fin spacing under the assumption that the fins have a uniform surface temperature of 313 K ( $T_{\infty} = 298 \text{ K}$ ).



## Forced Convection



- There is less variation between plate and pin fins in forced convection. Turbulence in staggered pin fins improves performance in forced convection.
- There is only a marginal difference in thermal resistance with higher pin fin densities. For a larger number of fins, the air velocity surrounding the fins reduce dramatically.
- Increased flow separation causes a decrease in the heat transfer coefficient.

## Conclusions and Future Work

- Under natural & forced convection, plate fins achieve better performance in ideal conditions. However, unlike plate fins, pin fins do not have a preferred flow direction in the x-y plane. Thus, pin fins are expected to perform better in multi-directional flows.
- Natural Convection (Thermal Resistance < 20 K/W):
  - Al plate and pin fins of  $5 \times 5 \text{ cm}^2$  footprint.
- Forced Convection (Thermal Resistance < 20 K/W):
  - Al plate fins of  $1 \times 1 \text{ cm}^2$  footprint for air velocity > 0.5 m/s.
  - Al and plastic pin fins of  $1 \times 1 \text{ cm}^2$  footprint for air velocity > 5 m/s.
- Further studies are currently being done on more complex designs.

<sup>1</sup>Marc T. Dunham, et. al. *Energy* 93 (2015)

<sup>2</sup>Micropelt Thermogenerators. Retrieved from <http://micropelt.com/thermogenerator.php>

<sup>3</sup>Adrian Bejan. *Convection Heat Transfer*. 3<sup>rd</sup> ed., Hoboken, NJ, Wiley, 2004.