## Cambridge Part III Maths

Michaelmas 2020

# Fluid Dynamics of Climate

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#### **Contents**

1	Flui	d motion in a rotating reference frame	2			
	1.1	Local Cartesian coordinates	3			
	1.2	Scale analysis	4			
	1.3	Taylor-Proudman Theorem	5			
2	Departures from geostrophy					
	2.1	Inertial (free) oscillations	6			
	2.2	Ekman layer	6			
	2.3	Ekman transport	7			
	2.4	Ekman pumping	7			
3	Rotating shallow water equations					
	3.1	Potential vorticity (PV)	9			
4	Small amplitude motions in rotating SW					
	4.1	Steady flows	10			
	4.2	Waves in an unbounded domain	11			
5	Geostrophic adjustment					
	5.1	Steady solutions	12			
	5.2	Transients	12			
	5.3	Energetics	13			
6	Quasi-geostrophic equations					
	6.1	Waves in QG	14			
	6.2	Physical interpretation of Rossby waves	15			
7	Large scale ocean circulation 19					
	7.1	Sverdrup flow	15			
	7.2	Western boundary currents	16			

8	Stratification and internal gravity waves			
	8.1	Boussinesq approximation	19	
	8.2	Stratification in the atmosphere and ocean	20	
	8.3	Small-amplitude motion about a state of rest	20	

## $\begin{array}{c} \textbf{Lecture 1} \\ 12/10/20 \end{array}$

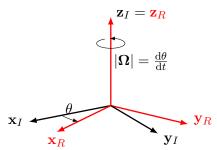
## 1 Fluid motion in a rotating reference frame

In a non-rotating frame, the Navier-Stokes equations are

$$\rho \frac{\mathrm{D}\boldsymbol{u}}{\mathrm{D}t} = -\nabla p - \rho \nabla \phi + \rho \boldsymbol{F}$$

The body forces are assumed to be conservative with potential  $\phi$ , e.g.  $\phi = gz$  for gravitational force.  $\mathbf{F}$  is the frictional force.

Consider a reference frame rotating about the z-axis with constant angular velocity  $\Omega$ . Axes in the inertial frame are denoted with a subscript I and axes in the rotating frame are denoted with a subscript I.



For a point with position vector x and velocity  $u_R = \left(\frac{\mathrm{d}x}{\mathrm{d}t}\right)_R$  in the rotating reference frame

$$\left(\frac{\mathrm{d}\boldsymbol{x}}{\mathrm{d}t}\right)_I = \left(\frac{\mathrm{d}\boldsymbol{x}}{\mathrm{d}t}\right)_R + \boldsymbol{\Omega} \times \boldsymbol{x}$$

or equivalently  $u_I = u_R + \Omega \times x$ . Hence the acceleration is

$$\begin{split} \left(\frac{\mathrm{d}\boldsymbol{u}}{\mathrm{d}t}\right)_I &= \left(\frac{\mathrm{d}}{\mathrm{d}t}\left[\boldsymbol{u}_R + \boldsymbol{\Omega} \times \boldsymbol{x}\right]\right)_R + \boldsymbol{\Omega} \times (\boldsymbol{u}_R + \boldsymbol{\Omega} \times \boldsymbol{x})_R \\ &= \left(\frac{\mathrm{d}\boldsymbol{u}_R}{\mathrm{d}t}\right)_R + 2\boldsymbol{\Omega} \times \boldsymbol{u}_R + \boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \boldsymbol{x}) \end{split}$$

The first term is the acceleration in the rotating frame, the second term is the *Coriolis acceleration* and the third term is the *centrifugal acceleration*. Note that we can write the centrifugal acceleration in the form of a conservative force

$$m{\Omega} imes (m{\Omega} imes m{x}) = 
abla \phi_c$$
 
$$\phi_c = -rac{1}{2} \left| m{\Omega} imes m{x} 
ight|^2$$

Hence the Navier-Stokes equations in a rotating reference frame are

$$\rho \left( \frac{\mathrm{D}\boldsymbol{u}}{\mathrm{D}t} + 2\boldsymbol{\Omega} \times \boldsymbol{u} \right) = -\nabla p - \rho \nabla \left( \phi + \phi_c \right) + \rho \boldsymbol{F}$$
 (1)

We group the potential terms into a geopotential  $\Phi \equiv \phi + \phi_c$ . The surface of a stationary ocean or atmosphere has a constant geopotential height described by an oblate spheroid.

Imagine a spherical earth. At sea level, the polar radius is 21.4km smaller than the equatorial radius: see figure 1. In reality, the surface of the Earth is also very close to a geopotential surface. Hence *geopotential coordinates* are very useful for planetary scale motion.

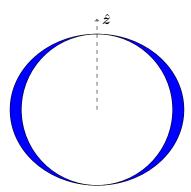


Figure 1: Geopotential ocean surface relative to a spherical Earth.

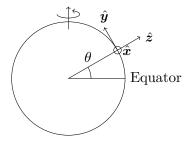


Figure 2: Local Cartesian coordinates

#### 1.1 Local Cartesian coordinates

For small motions, it is much more convenient to define local Cartesian coordinates (figure 2). In this coordinate system  $\Omega = (0, \Omega \cos \theta, \Omega \sin \theta)$ . Hence if  $\mathbf{u} = (u, v, w)$  then

$$2\mathbf{\Omega} \times \mathbf{u} = (2\Omega w \cos \theta - 2\Omega v \sin \theta, 2\Omega u \sin \theta, -2\Omega u \cos \theta)$$
$$= (-fv + f^*w, fu - f^*u)$$

where  $f \equiv 2\Omega \sin \theta$  is the *Coriolis parameter* and  $f^* \equiv 2\Omega \cos \theta$ .

**Example.** In Cambridge,  $\theta = 52.1^{\circ}N$  so

$$f = 2\Omega \sin \theta$$
=  $2 \cdot \frac{2\pi}{3600 \cdot 24} \cdot 0.79s^{-1}$ 
 $\approx 1.14 \times 10^{-4} s^{-1}$ 

At mid-latitudes,  $f \sim 10^{-4}$  is a good approximation.

We can simplify the Coriolis acceleration expression; often  $f^*w \ll fv$  and  $f^*u \ll g$ . Hence

$$2\mathbf{\Omega} \times \mathbf{u} \approx (-fv, fu, 0) = f\hat{\mathbf{z}} \times \mathbf{u}$$

This is the *traditional approximation*. This is *not* always a good approximation, particularly at intermediate scales.

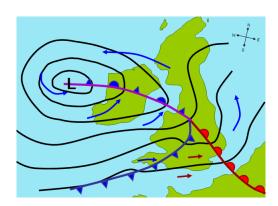


Figure 3: Lines of constant pressure p act as streamlines for the horizontal flow.

#### 1.2 Scale analysis.

Define characteristic scales for length L, time T, and velocity U. Non-dimensional variables are denoted with a superscript star:  $\mathbf{u}^* = \mathbf{u}/U$ , etc.

Using these scalings with  $\mathbf{F} = \nu \nabla^2 \mathbf{u}$  we have

$$\frac{U}{T}\frac{\partial \boldsymbol{u}^{*}}{\partial t^{*}}+\frac{U^{2}}{L}\boldsymbol{u}^{*}\cdot\nabla^{*}\boldsymbol{u}^{*}+fU\hat{\boldsymbol{z}}\times\boldsymbol{u}^{*}=-\frac{1}{\rho}\nabla\left(p+\rho\Phi\right)+\frac{\nu U}{L^{2}}\nabla_{*}^{2}\boldsymbol{u}^{*}$$

Dividing through by fU leaves the Coriolis acceleration term  $\operatorname{ord}(1)$  with other terms scaled relatively.

$$\frac{1}{fT}\frac{\partial \boldsymbol{u}^*}{\partial t^*} + \operatorname{Ro}\boldsymbol{u}^* \cdot \nabla^*\boldsymbol{u}^* + \hat{\boldsymbol{z}} \times \boldsymbol{u}^* = -\frac{1}{\rho f U}\nabla\left(p + \rho\Phi\right) + \operatorname{E}\nabla_*^2\boldsymbol{u}^*$$

where Ro  $\equiv \frac{U}{fL}$  is the Rossby number and E  $\equiv \frac{\nu}{fL^2}$  is the Ekman number.

**Example.** For an atmospheric storm,  $U\sim 10ms^{-1}, L\sim 1000km, f\sim 10^{-4}s^{-1}.$  Thus Ro  $\sim 0.1, E\sim 10^{-13}.$ 

**Lecture 2** 14/10/2020

Further, if T = L/U, then Ro = U/fL = 1/fT. For small Ro, E, on surfaces of constant  $\Phi$ ,  $f\hat{z} \times u \approx -\frac{1}{\rho}\nabla p$ . This is geostrophic balance. In components, we have

$$-fv = -\frac{1}{\rho} \frac{\partial p}{\partial x}$$
$$fu = -\frac{1}{\rho} \frac{\partial p}{\partial y}$$

The equations of geostrophic balance can be arranged to give the horizontal velocity:  $u_H$ 

$$\boldsymbol{u}_H \equiv (u, v) = \frac{1}{\rho f} \hat{\boldsymbol{z}} \times \nabla p$$

Horizontal velocity is perpendicular to  $\nabla p$  and hence parallel to isobars (lines of constant p), i.e. pressure acts like a streamfunction (see figure 3).

In the Northern Hemisphere, air moves clockwise around high p and anticlockwise around low p. A cyclonic rotation is in the same sense as  $\Omega$ , anticyclonic in the opposite sense as  $\Omega$ .

#### 1.3 Taylor-Proudman Theorem

Consider an incompressible, ideal fluid in geostrophic balance (small Ro, E)

$$\nabla \cdot \boldsymbol{u} = 0$$

$$2\boldsymbol{\Omega} \times \boldsymbol{u} = -\frac{1}{\rho} \nabla p \tag{2}$$

Taking the curl of (2) we have

$$\nabla \times (\mathbf{\Omega} \times \mathbf{u}) = \varepsilon_{ijk} \partial_j \varepsilon_{klm} \Omega_l u_m$$

$$= \varepsilon_{kij} \varepsilon_{klm} \Omega_l \partial_j u_m$$

$$= (\delta_{il} \delta_{jm} - \delta_{im} \delta_{jl}) \Omega_l \partial_j u_m$$

$$= \Omega_i \partial_j u_j - \Omega_j \partial_j u_i$$

The first term is 0 by incompressibility. Thus

$$-\nabla \times (\mathbf{\Omega} \times \mathbf{u}) = \mathbf{\Omega} \cdot \nabla \mathbf{u} = 0$$

For  $\Omega = (0, 0, \Omega)$ , this implies  $\frac{\partial w}{\partial z} = 0$ . If w = 0 on some horizontal surface (e.g. ground) then w = 0 everywhere.

Also,  $u_x + v_y = 0$ , i.e. horizontal velocity is non-divergent in geostrophic balance. Fluid moves in 'columns' parallel to  $\Omega$ , called Taylor columns.

### 2 Departures from geostrophy

Consider an incompressible, rotating fluid with constant density  $\rho_0$  with angular velocity  $\Omega = (0, 0, f/2)$ . Assume small amplitude motions (i.e.  $|\boldsymbol{u}|^2 \ll |\boldsymbol{u}|$ ), i.e. neglect  $\boldsymbol{u} \cdot \nabla \boldsymbol{u}$  and  $\nu \nabla^2 \boldsymbol{u}$ . From (1),

$$u_t - fv = -\frac{p_x}{\rho_0} \tag{3}$$

$$v_t + fu = -\frac{p_y}{\rho_0} \tag{4}$$

$$w_t = -\frac{p_z}{\rho_0} \tag{5}$$

$$u_x + v_y + w_z = 0 ag{6}$$

We will eliminate variables in favour of p.

$$\nabla \cdot ((3) - (5)) \implies \nabla^2 p = \rho_0 f (v_x - u_y)$$
$$\partial_x (4) - \partial_y (3) \& (6) \implies (v_x - u_y)_t = f w_z$$

Combining these and using (5) we have

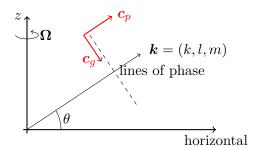
$$\nabla^2 p_{tt} + f^2 p_{zz} = 0$$

which is a wave equation for p. Seek plane wave solutions with ansatz

$$p = \hat{p}e^{i(kx+ly+mz-\omega t)}$$

and dispersion relation

$$\omega^2 = \frac{f^2 m^2}{k^2 + l^2 + m^2} = f^2 \sin^2 \theta$$



This is the dispersion relation for rotating internal waves. They have phase speed  $c_p = w/k$  and group velocity

$$c_g = \frac{\partial w}{\partial \mathbf{k}} = \pm f \frac{(-km, -lm, k^2 + l^2)}{|\mathbf{k}|^{3/2}}$$

**Lecture 3** 16/10/2020

Note that  $c_p \cdot c_g = 0$ . Also note  $|\omega| \leq |f|$ .

#### 2.1 Inertial (free) oscillations

Assume  $\nabla p = \mathbf{0}$ . The x and y components of geostrophic balance (3), (4) give

$$u_{tt} + f^2 u = 0$$

Thus  $u = U \sin ft$  where f is the *inertial frequency*. Similarly, we have  $v = U \cos ft$ . For a particle with position  $(x_p, y_p)$  floating on an ocean surface z = 0 moving with the fluid velocity, we have

$$\frac{\mathrm{d}x_p}{\mathrm{d}t} = u \implies x_p = -\frac{U}{f}\cos ft + x_0$$

$$\frac{\mathrm{d}y_p}{\mathrm{d}t} = v \implies y_p = -\frac{U}{f}\sin ft + y_0$$

Thus the motion of fluid particles describes describes inertial circles with radius  $\frac{2U}{f}$ .

#### 2.2 Ekman layer

Look for a *steady* ocean response to a constant wind stress  $\tau_w$ . Use local Cartesian coordinates and make the following assumptions:

- 1. Steady, i.e.  $\partial_t \equiv 0$
- 2. Neglect horizontal variations, i.e.  $\partial_x = \partial_y = 0$
- 3. Neglect surface waves, i.e. w(z=0)=0
- 4. No flow in deep ocean, i.e.  $\lim_{z\to-\infty} u = 0$
- 5. Constant density  $\rho$
- 6. Traditional approximation

Continuity (incompressibility) says  $u_x + v_y + w_z = 0$ . Assumptions 2 and 3 then imply w = 0 everywhere. The horizontal momentum equations are

$$-fv = \nu u_{zz} \tag{7}$$

$$fu = \nu v_{zz} \tag{8}$$

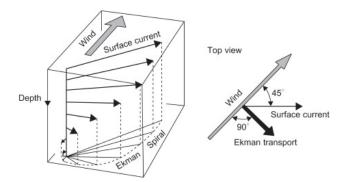


Figure 4: Ekman spiral.

Define the complex velocity  $\mathcal{V} \equiv u + iv$ . Then

$$\mathcal{V}_{zz} = \frac{if}{\nu} \mathcal{V} \tag{9}$$

Without loss of generality, assume  $\tau_w$  is aligned with the x-axis:  $\tau_w = (\tau_w, 0) = (\rho \nu u_z, 0)$ . Boundary conditions for (9) are

$$\mathcal{V}_z = \left(\frac{\tau_w}{\rho\nu}, 0\right) \quad \text{at } z = 0$$

$$\mathcal{V} = (0, 0) \quad \text{as } z \to -\infty$$

Thus  $\mathcal{V} = Ae^{(1+i)z/\delta}$  where  $\delta = \sqrt{\frac{2\nu}{f}}, A = \frac{\tau_w \delta(1-i)}{2\rho\nu}$ . In terms of the velocity components, we have

$$u = \frac{\tau_w}{\rho\sqrt{\nu f}} e^{z/\delta} \cos\left(-\frac{z}{\delta} + \frac{\pi}{4}\right)$$
$$v = -\frac{\tau_w}{\rho\sqrt{\nu f}} e^{z/\delta} \sin\left(-\frac{z}{\delta} + \frac{\pi}{4}\right)$$

A top view of the ocean shows an *Ekman spiral*: see figure 4.

#### 2.3 Ekman transport

Integrate the horizontal momentum equations (7),(8) to the base of the Ekman layer where  $\nu u_z \approx 0$  at z = -h. Since  $\nu u_z(z=0) = (\tau_w/\rho, 0)$ , the Ekman transport  $U_T$  is

$$U_T \equiv \int_{-h}^{0} u \, dz = 0$$
$$V_T \equiv \int_{-h}^{0} v \, dz = -\frac{\tau_w}{\rho f}$$

This is the net transport of fluid in the Ekman layer and is oriented 90° to the right of the applied wind shear stress (in the Northern Hemisphere).

#### 2.4 Ekman pumping

Consider a wind stress  $\tau_w(y)$  that varies over large scales. Then from incompressibility

$$\int_{-h}^{0} w_z \, dz = -\int_{-h}^{0} u_x \, dz - \int_{-h}^{0} v_y \, dz$$

Thus for h constant,

$$-w(z=-h) = -\frac{\partial V_T}{\partial y} = \frac{\partial}{\partial y} \left(\frac{\tau_w}{\rho f}\right)$$

In general we have

$$w(z=-h) = \hat{\boldsymbol{z}} \cdot \nabla \times \frac{\boldsymbol{\tau}_w}{\rho f}$$

Lecture 4 19/10/20

## 3 Rotating shallow water equations

Consider a thin layer of fluid with constant density  $\rho$ . Define characteristic scales

- length L = horiz., H = vert.
- $\bullet$  velocity U
- $\bullet$  time T
- $\bullet$  pressure P

such that  $\partial_x, \partial_y \sim \frac{1}{L}, \partial_z \sim \frac{1}{H}$ . Define the aspect ratio  $\delta \equiv H/L$ . We will assume  $\delta \ll 1$ . From continuity (incompressibility) we have

$$\frac{\partial w}{\partial z} = -\frac{\partial u}{\partial x} - \frac{\partial v}{\partial y}$$

$$\implies \frac{w}{H} = \mathcal{O}(U/L)$$

$$\implies w = \mathcal{O}(\delta U)$$

Using the traditional approximation and assuming the fluid is inviscid, the x-momentum equation

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} - fv = -\frac{1}{\rho} \frac{\partial p}{\partial x}$$
(10) scaling:  $\frac{U}{T} + \frac{U^2}{L} + \frac{U^2}{L}$ 

Thus if  $p_x$  appears at leading order then

$$P \sim \rho U \max(L/T, U, fL)$$

Similarly the z-momentum equation and its scalings are

$$\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial x} - g \quad (11)$$
 scaling:  $\frac{w}{T} \frac{Uw}{L} \frac{Uw}{L} = \frac{w^2}{H} = \frac{P}{\rho H}$ 

Hence  $\frac{Dw}{Dt} \sim \max(\frac{w}{T}, \frac{Uw}{L})$ . Comparing with the pressure term, we have

$$\frac{\frac{Dw}{Dt}}{\frac{1}{\rho}\frac{\partial p}{\partial z}} \sim \frac{\max(\frac{w}{T}, \frac{Uw}{L})}{\frac{U}{H}\max(\frac{L}{T}, \frac{U}{L}, f)}$$
$$\sim \delta^2 \frac{\max(\frac{1}{T}, \frac{U}{L})}{\max(\frac{1}{T}, \frac{U}{L}, f)}$$

Therefore to  $\mathcal{O}(\delta^2)$  we have hydrostatic balance. To this order, (11) becomes

$$\frac{\partial p}{\partial z} - \rho g \implies p = \rho g(\eta - z)$$

assuming p=0 at  $z=\eta(x,y,t)$ . Similarly, we have  $\frac{1}{\rho}p_x=g\eta_x$  and  $\frac{1}{\rho}p_y=g\eta_y$ . Hence horizontal acceleration (i.e. the LHS of (10)) is independent of z. Motivated by this, we assume that horizontal velocity is also independent of z. For  $Ro \ll 1$ , this follows from the Tayor-Proudman theorem. Re-writing (10) with these results we have

$$u_t + uu_x + vu_y - fv = -g\eta_x \tag{12}$$

$$v_t + uv_x + vv_y + fu = -g\eta_y \tag{13}$$

since  $u_z = v_z = 0$  by assumption. Integrating the continuity equation gives

$$w = -z(u_x + v_y) + A(x, y, t)$$

where A is to be determined by the boundary conditions. Requiring no normal flow at  $z = -H_0 + h_b$  is imposed by  $\mathbf{u} \cdot \hat{\mathbf{n}} = 0$  where  $\mathbf{n} = \nabla(z - h_b)$ . Thus

$$-u\frac{\partial h_b}{\partial x} - v\frac{\partial h_b}{\partial y} + w = 0$$

Hence

$$A(x, y, t) = u \frac{\partial h_b}{\partial x} + v \frac{\partial h_b}{\partial y} + (-H_0 + h_b)(u_x + v_y)$$

The kinematic boundary condition at  $z = \eta$  is  $\frac{D\eta}{Dt} = w$  which may be written as

$$\eta_t + u\eta_x + v\eta_y - w = 0$$

where  $w = -\eta(u_x + v_y) + u\frac{\partial h_b}{\partial x} + v\frac{\partial h_b}{\partial y} + (-H_0 + h_b)(u_x + v_y)$ . Combining these boundary conditions gives

$$\eta_t + [(H_0 - h_b + \eta)u]_x + [(H_0 - h_b + \eta)v]_y = 0$$
(14)

If  $H \equiv H_0 - h_b + \eta$  is the total depth of the fluid, then since  $H_t = \eta_t$ ,

$$H_t + (uH)_x + (vH)_y = 0 (15)$$

which is a statement of the conservation of volume (equivalently mass, since  $\rho$  is constant). Equations (12), (13), and (14) are the rotating shallow water (SW) equations.

#### 3.1 Potential vorticity (PV)

Denote the vertical vorticity by  $\zeta = v_x - u_y$ . Consider  $\partial_x(13) - \partial_y(12)$ , which gives

$$\zeta_t + u\zeta_x + v\zeta_y + vf_y = -(\zeta + f)(u_x + v_y)$$

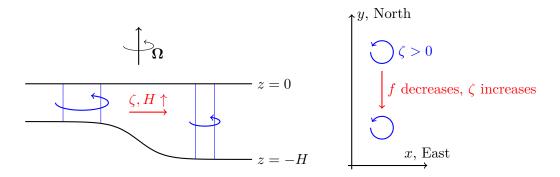
Now from conservation of volume (15),

$$u_x + v_y = -\frac{1}{H} \frac{\mathrm{D}H}{\mathrm{D}t}$$

Combining these relates the material derivative of  $\zeta$  and H by

$$\frac{\mathrm{D}\zeta}{\mathrm{D}t} + \frac{\mathrm{D}f}{\mathrm{D}t} = \frac{\zeta + f}{H} \frac{\mathrm{D}H}{\mathrm{D}t} \implies \frac{\mathrm{D}}{\mathrm{D}t} \left(\frac{\zeta + f}{H}\right) = 0 \tag{16}$$

Let  $q \equiv \frac{\zeta + f}{H}$ , the shallow water potential vorticity (SWPV). SWPV is conserved following fluid motion. We call  $\zeta$  the relative vorticity and f the planetary vorticity.  $\zeta$  and f will change as a fluid moves to conserve SWPV (changing f) and angular momentum (changing depth).



Lecture 5 21/10/20

## 4 Small amplitude motions in rotating SW

Consider a stationary fluid with depth  $H_s(x,y) = H_0 - h_b$ . The fluid surface is then perturbed by  $\eta(x,y,t)$  where  $\eta \ll H_s$ . The total depth is  $H(x,y,t) = H_s + \eta$ . For  $|\boldsymbol{u}|^2 \ll |\boldsymbol{u}|$ , linearise the shallow water equations:

$$u_t - fv = -g\eta_x \tag{17}$$

$$v_t + fu = -g\eta_y \tag{18}$$

$$\eta_t + (uH_s)_x + (vH_s)_y = 0$$

Assuming f is constant, we have from  $\partial_x(17) + \partial_y(18)$  and  $\partial_y(17) - \partial_x(18)$ :

$$\partial_t \left[ \left( \partial_t^2 + f^2 \right) \eta - \nabla \cdot (gH_s \nabla \eta) \right] - fgJ(H_s, \eta) = 0$$
(19)

where the Jacobian  $J(a,b) = a_x b_y - a_y b_x$ . For the velocity components we have

$$\left(\partial_t^2 + f^2\right)u = -g\left(\eta_{xt} + f\eta_y\right) \tag{20}$$

$$\left(\partial_t^2 + f^2\right)v = -g\left(\eta_{yt} + f\eta_x\right) \tag{21}$$

#### 4.1 Steady flows

We now assume  $\partial_t = 0$ . From (20), (21),

$$u = -\frac{g}{f}\eta_y, \qquad v = \frac{g}{f}\eta_x$$

This is shallow water geostrophic balance: the surface displacement  $\eta$  acts as a streamfunction. Applying the steady assumption to (19) gives  $J(H_s, \eta) = 0$  which implies  $\eta = \eta(H_s(x, y))$ . Hence linearised steady geostrophic flow in shallow water follows contours of constant depth. Steady PV conservation follows from (16) with  $\partial_t = 0$  and assuming  $\zeta \ll f$ 

$$\mathbf{u} \cdot \nabla \frac{f}{H_s} = 0$$

Thus when f varies, the flow follows contours of constant  $f/H_s$ .

#### 4.2 Waves in an unbounded domain

Assume  $H_s$  is constant. From (19), we have

$$\left(\partial_t^2 + f^2\right)\eta - gH_s\nabla^2\eta = 0$$

Seek plane wave solutions to this wave equation with ansatz  $\eta = \eta_0 \exp(i(kx + ly - \omega t))$ . The dispersion relation is then

$$\omega^2 = f^2 + gH_s(k^2 + l^2) \tag{22}$$

If f=0, i.e. no rotation, then the frequency is  $\omega=\pm\sqrt{gH_s}|\boldsymbol{k}|=\omega_0$  and the phase speed is  $|c_p|=\frac{|\omega|}{|\boldsymbol{k}|}=\sqrt{gH_s}=c_0$ . For  $f\neq 0$ , we get *Poincaré* waves with

$$\omega^2 > \omega_0^2, \qquad |c_p| > c_0$$

i.e. rotation increases the frequency and phase speed. Define the Rossby deformation scale  $R_D \equiv \frac{c_0}{f}$ . From (22),

$$\frac{\omega^2}{f^2} = 1 + R_D^2 |\boldsymbol{k}|^2$$

Without loss of generality, let l = 0, by reorienting x and y. If  $\eta = \eta_0 \cos(kx - \omega t)$  then (20), (21) imply the fluid velocity is

$$u = \frac{\omega_0 \eta_0}{kH_s} \cos(kx - \omega t)$$
$$v = \frac{f\eta_0}{kH_s}$$

Thus the motion is an ellipse, also known as a *tidal ellipse*, which reduces to intertial circles if  $\omega_0 = f$ :

$$u^2 + \frac{\omega_0^2}{f^2}v^2 = \frac{\omega_0^2 \eta_0^2}{k^2 H_s^2}$$

Since  $\omega > f$ , the fluid moves anticylonically. The Rossby deformation scale  $R_D$  is the length scale for which rotation becomes important. Consider short and long waves:

- Short waves:  $|\mathbf{k}|R_D \gg 1$ . We have  $\omega^2 \to gH_s|\mathbf{k}|^2$  i.e. non-rotating shallow water gravity waves
- Long waves:  $|\mathbf{k}|R_D \ll 1$ . We have  $\omega^2 \to f^2$  i.e. inertial waves where fluid moves in inertial circles. Gravity is not involved.

23/10/20

## 5 Geostrophic adjustment

Consider the response of rotating shallow water to an initial state *not* in geostrophic balance. Here, we consider  $\eta(x, y, ) = \eta_0 \operatorname{sgn}(x)$ ,  $\boldsymbol{u}(x, y, 0) = \boldsymbol{0}$ , so the initial PV is 0.

Assume f is constant, the perturbation is small  $\eta_0 \ll H$ , the PV is small  $\zeta \ll f$ , and the bottom is flat  $H_s = H_0$ . Linearise the shallow water PV:

$$q = \frac{f+\zeta}{H_0+\eta} = \frac{f}{H_0} \left( 1 + \frac{\zeta}{f} + \dots \right) \left( 1 - \frac{\eta}{H_0} + \dots \right) \approx \frac{f}{H_0} \left( 1 + \frac{\zeta}{f} - \frac{\eta}{H_0} \right)$$

Since PV is conserved, we have

$$\frac{\zeta}{f} - \frac{\eta}{H_0} = -\frac{\eta_0}{H_0} \operatorname{sgn}(x) \qquad \forall t \tag{23}$$

By symmetry,  $\partial_y \equiv 0$  so the PV is  $\zeta = v_x$ . The linearised shallow water equations in this case

$$u_t - fv = -g\eta_x$$
$$v_t + fu = 0$$
$$\eta_t + H_0 u_x = 0$$

Using these equations we have

$$\zeta = v_x = \frac{u_{xt} + g\eta_{xx}}{f} = -\frac{1}{fH_0}\eta_{tt} + \frac{g}{f}\eta_{xx}$$

Now conservation of potential vorticity (23) gives

$$\eta_{tt} - c^2 \eta_{xx} + f^2 \eta = f^2 \eta_0 \operatorname{sgn}(x)$$

where  $c^2 \equiv gH_0$ . This is a Klein-Gordon equation where the  $f^2\eta$  term adds elasticity to the waves.

#### 5.1 Steady solutions

Consider steady solutions. Owing to the step forcing, our BCs are to match  $\eta_x$  and  $\eta$  at x=0. We find

$$\eta = \eta_0 \begin{cases} 1 - e^{-x/R_d} & x > 0 \\ -1 + e^{x/R_d} & x < 0 \end{cases}$$
 (24)

where  $R_d \equiv \sqrt{gH_0}/f$  is the deformation radius. From the equations of geotrophic balance we have the velocity components

$$u = 0, \qquad v = \frac{g\eta_0}{fR_d}e^{-|x|/R_d}$$

$$\eta \qquad \qquad \eta_0$$

#### 5.2 Transients

The steady solution (24) solves the geostrophic adjustment equation, but it does not match the initial conditions. We add this particular solution to a solution to the homogeneous equation

$$\eta_{tt} - c^2 \eta_{xx} + f^2 \eta = 0$$

with initial condition

$$\eta = \eta_0 \operatorname{sgn}(x) - \eta_{\text{steady}} = \eta_0 e^{-|x|/R_d} \operatorname{sgn}(x)$$

We seek solutions of plane wave form

$$\eta = \hat{\eta}e^{i(kx - \omega t)}$$

with  $\omega^2 = f^2 + c^2 k^2$ . These are Poincaré waves.

#### 5.3 Energetics

The change in potential energy per unit length in the y direction is

$$PE_{\text{initial}} - PE_{\text{final}} = \int_{-\infty}^{\infty} \int_{0}^{\eta_{i}} \rho_{0}gz \,dz \,dx - \int_{-\infty}^{\infty} \rho_{0}gz \,dz \,dx$$
$$= 2\rho_{0}g \left[ \int_{0}^{\infty} \frac{\eta_{i}^{2}}{2} \,dx - \int_{0}^{\infty} \frac{\eta_{f}^{2}}{2} \,dx \right]$$
$$= \rho_{0}g\eta_{0}^{2} \int_{0}^{\infty} \left[ 1 - (1 - e^{-x/R_{d}})^{2} \right] dx$$
$$= \frac{3}{2}\rho_{0}g\eta_{0}^{2}R_{d}$$

The change in kinetic energy per unit length in the y direction is

$$\begin{split} KE_{\text{initial}} - KE_{\text{final}} &= \int_{-\infty}^{\infty} \int_{-H}^{\eta_i} \frac{1}{2} \rho_0 v_i^2 \, \mathrm{d}z \, \mathrm{d}x - \int_{-\infty}^{\infty} \int_{-H}^{\eta_f} \frac{1}{2} \rho_0 v_f^2 \, \mathrm{d}z \, \mathrm{d}x \\ &\approx 0 - \frac{1}{2} \rho_0 \int_{-\infty}^{\infty} H_s v_f^2 \, \mathrm{d}x \\ &= -\rho_0 H_s \int_{0}^{\infty} \frac{g^2 \eta_0^2}{f^2 R_d^2} e^{-2x/R_d} \, \mathrm{d}x \\ &= -\rho_0 \frac{R_d^2 g \eta_0^2}{R_d^2} \cdot - \frac{R_d}{2} \cdot \left[ e^{-2x/R_d} \right]_{0}^{\infty} \\ &= -\rho_0 g \eta_0^2 \frac{R_d}{2} \end{split}$$

Only  $\frac{1}{3}$  of the potential energy released is converted into kinetic energy of the geostrophic flow. The remainder is radiated away by Poincaré waves.

## 6 Quasi-geostrophic equations

Lecture 7 26/10/20

Large scale motions in the ocean and atmosphere are associated with small Rossby number  $Ro \equiv \frac{U}{fL} \ll 1$ . In this limit, the rotating shallow water equations are approximated by the SW quasi-geostrophic (SW QG) equation. Start from the SW PV equation:

$$\frac{\mathrm{D}}{\mathrm{D}t} \left( \frac{\zeta + f}{H} \right) = 0 \tag{25}$$

**Assumption 1:**  $Ro \ll 1$  Assuming a small Rossby number implies the flow is close to geostrophic balance with

$$f\hat{\boldsymbol{k}} \times \boldsymbol{u} \approx -g\nabla \eta$$

where  $\hat{k}$  is the vertical unit vector. Define the geostrophic streamfunction  $\psi \equiv \frac{g\eta}{f}$ . In terms of this streamfunction we have

$$\mathbf{u} \approx -\nabla \times (\psi \hat{\mathbf{k}})$$
  
 $\zeta = (\nabla \times \mathbf{u})\hat{\mathbf{k}} \approx \nabla^2 \psi$ 

**Assumption 2: small changes in** f Recall the Coriolis parameter  $f = 2\Omega \sin \theta$  where  $\theta$  is latitude. Expand in a Taylor series about  $\theta = \theta_0$  to get

$$f = f_0 + y \frac{\mathrm{d}f}{\mathrm{d}y}|_{\theta_0} + \dots \approx f_0 + \beta y$$

where y is in the direction of local North,  $f_0 = 2\Omega \sin \theta_0$  and  $\beta$  is defined as

$$\beta = \frac{1}{R} \frac{\mathrm{d}f}{\mathrm{d}\theta} |_{\theta_0} = \frac{2\Omega}{R} \cos \theta_0$$

with R the radius of Earth. For characteristic length scale L, assume  $\frac{\beta L}{f_0} \ll 1$ . This is the  $\beta$ -plane approximation.

Assumption 3: small changes in fluid height. This is consistent with small Rossby number: from geostrophic balance, we know  $\eta \sim \frac{fUL}{g}$  and  $\frac{\eta}{H_0} \sim \frac{fUL}{gH_0} = \frac{U}{fL} \frac{L^2}{R_D^2}$ . Therefore  $\eta/H_0 \ll 1$  if  $Ro \ll \frac{R_D^2}{L^2}$ . For  $L \sim R_D$ ,  $Ro \ll 1$  implies  $\eta/H_0 \ll 1$ . Further, we assume  $h_b/H_0 \ll 1$ .

Quasi-geostrophic equations. With these assumptions, SWPV becomes

$$\frac{\zeta + f}{H_0 - h_b + \eta} \approx \frac{f_0}{H_0} \frac{1 + \frac{\beta y}{f_0} + \frac{\zeta}{f_0}}{1 - \frac{h_b}{H_0} + \frac{\eta}{H_0}}$$

$$\approx \frac{f_0}{H_0} \left( 1 + \frac{\beta y}{f_0} + \frac{\nabla^2 \psi}{f_0} + \frac{h_b}{H_0} - \frac{f_0 \psi}{g H_0} \right)$$

$$= \frac{f_0}{H_0} P_g$$

where  $P_g$  is the quasi-geostrophic potential vorticity and  $\zeta = \nabla^2 \psi$ ,  $\eta = \frac{f_0 \psi}{g}$ . Hence from SWPV conservation (25),

$$\frac{\partial P_g}{\partial t} + \boldsymbol{u} \cdot \nabla P_g \approx 0$$

Using  $\mathbf{u} \approx -\nabla \times (\psi \hat{\mathbf{k}}), \ \mathbf{u} = -\psi_y, v = \psi_x \text{ so}$ 

$$\frac{\partial P_g}{\partial t} + J(\psi, P_g) \approx 0 \tag{26}$$

This is the *shallow water Quasi-geostrophic* (SWQG) equation, which is one equaiton for one unknown  $\psi$ , as opposed to SWPV with 2 unknowns  $\zeta, \eta$ .

#### 6.1 Waves in QG

Assume a flat bottom  $h_b = 0$ . Linearise (26) about a state of rest (i.e. neglect terms  $\mathcal{O}(\psi^2)$ ). Then

$$\frac{\partial}{\partial t} \left( \nabla^2 \psi - \frac{f_0^2}{gH_0} \psi \right) + \frac{\partial \psi}{\partial x} \beta = 0$$

Seek plane wave solutions of the form

$$\psi = \psi_0 e^{i(kx + ly - \omega t)}$$

with dispersion relation

$$\omega = \frac{-k\beta}{k^2 + l^2 + R_D^{-2}}, \qquad R_D \equiv \frac{\sqrt{gH_0}}{f_0}$$

This is the Rossby wave dispersion relation. Note  $\omega = 0$  (i.e. no waves) if  $\beta = 0$ . Also, if  $h_b = 0$  and  $\beta = 0$  there are no wave solutions unlike rotating SW. Thus the QG system 'filters' out Poincaré waves. Note that  $\beta = \frac{2\Omega}{R}\cos\theta \ge 0$ , hence  $c_p = \frac{\omega}{k} \le 0$ . Rossby wave speed is always directed to the west.

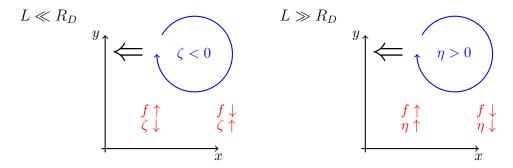
Consider the size of the dynamic terms in  $P_g$ , specifically the ratio of relative vorticity to surface height

$$\frac{\nabla^2 \psi}{-\frac{f_0^2 \psi}{qH_0}} \sim \frac{R_D^2}{L^2}$$

Hence relativity vorticity dominates at scales small compared to  $R_D$  whilst surface height dominates at scales large compared to  $R_D$ .

#### 6.2 Physical interpretation of Rossby waves

Consider  $L \ll R_d$  ( $L \gg R_D$ ) and a small perturbation in the dominant term for the scale,  $\zeta$  ( $\eta$ ). For  $L \ll R_D$ , the planetary vorticity increases (thus  $\zeta$  decreases) on the westward side, whilst the planetary vorticity decreases (thus  $\zeta$  increases) on the eastward side. Hence the perturbation propagates westwards. For  $L \gg R_D$ , the planetary vorticity increases ( $\eta$  increases) on the westward size and decreases ( $\eta$  decreases) on the eastward side as before. Thus the perturbation propagates to the west also. These are Rossby waves.



## 7 Large scale ocean circulation

#### 7.1 Sverdrup flow

Seek steady solutions for rotating shallow water driven by a wind stress  $\tau_w$ . We have

$$\frac{\mathrm{D}\boldsymbol{u}}{\mathrm{D}t} + f\hat{\boldsymbol{k}} \times \boldsymbol{u} = -g\nabla \eta + \frac{\boldsymbol{\tau}_w}{\rho H}$$
 (27)

$$H_t + \nabla \cdot (\boldsymbol{u}H) = 0 \tag{28}$$

Consider  $\nabla \times (27) \cdot \hat{k}$  and (28) which implies modified PV conservation

$$\frac{\mathrm{D}}{\mathrm{D}t} \left( \frac{\zeta + f}{H} \right) = \frac{1}{H} \nabla \times \left( \frac{\tau_w}{\rho H} \right) \cdot \hat{\mathbf{k}}$$
 (29)

Thus we see frictional forcing modifies PV conservation. Assuming H is constant,  $\zeta \ll f$  ( $Ro \ll 1$ ), and using the  $\beta$ -plane approximation  $f = f_0 + \beta y$ , (29) becomes

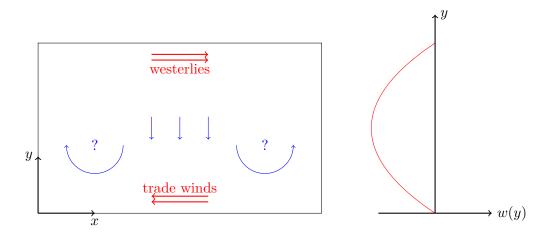
$$\beta v = \frac{1}{\rho H} \left( \nabla \times \boldsymbol{\tau}_w \right) \cdot \hat{\boldsymbol{k}} \tag{30}$$

This is called *Sverdrup balance*. Physically, the North/South advection of planetary vorticity  $\boldsymbol{u} \cdot \nabla f$  balances the vorticity input by wind.

#### 7.2 Western boundary currents

Consider steady circulation in a rectangular basin, driven by a wind stress curl

$$w(y) = \frac{(\nabla \times \boldsymbol{\tau}_w) \cdot \hat{\boldsymbol{k}}}{\rho H}$$



From (30),  $w < 0 \implies v < 0$ . Recall  $\mathbf{u} = -\nabla \times \psi \hat{\mathbf{k}}$ . Boundary conditions are no normal flow at the boundaries, i.e.  $\psi$  is constant. Sverdrup balance (30)  $\beta \psi_x = w(y)$  gives

$$\psi = \frac{xw(y)}{\beta} + G(y)$$

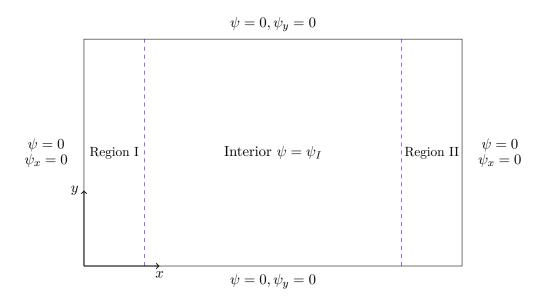
for some arbitary function G(y). This presents a problem: we cannot meet the boundary conditions at both x = 0 and x = L. Hence we need extra terms and boundary layers. Following Musk, we include horizontal friction in (27):

$$\frac{\mathrm{D}\boldsymbol{u}}{\mathrm{D}t} + f\hat{\boldsymbol{k}} \times \boldsymbol{u} = -g\nabla \eta + \frac{\boldsymbol{\tau}_w}{\rho H} + \nu \nabla^2 \boldsymbol{u}$$
(31)

Note here we are using the horizontal gradient  $\nabla \equiv (\partial_x, \partial_y)$ . Consider  $\nabla \times (31) \cdot \hat{k}$  with  $\zeta \ll f$ . Then

$$\beta \psi_x = w(y) + \nu \nabla^4 \psi \tag{32}$$

The PDE is now fourth order, so we need four boundary conditions.



Lecture 8 30/10/20

In region I we have  $\psi \approx \psi_I + \psi^{(1)}$  and in region II we have  $\psi \approx \psi_I + \psi^{(2)}$ . The full solution is  $\psi = \psi_I + \psi^{(1)} + \psi^{(2)}$  with interior flow  $\psi_I = x \frac{w(y)}{\beta} + G(y)$ .

**Region I.** Let  $\varepsilon = \nu$  with  $\varepsilon \ll 1$ . Define a rescaled coordinate  $\tilde{x} \equiv \frac{x}{\varepsilon^a}$  with  $\partial_x = \varepsilon^{-a} \partial_{\tilde{x}}$ . Note: if a > 0 then  $\partial_x \gg \partial_y$ . This is the *method of undetermined coefficients*. From the PDE (32) for  $\psi$  we have

$$\beta \psi_x^{\mathbf{I}} + \beta \varepsilon^{-a} \tilde{\psi}_{\tilde{x}}^{(1)} = \varepsilon^{1-4a} \tilde{\psi}_{\tilde{x}\tilde{x}\tilde{x}\tilde{x}}^{(1)} + \mathbf{x}$$

Matching exponents, we have  $a = \frac{1}{3}$ . Hence

$$\beta \tilde{\psi}_{\tilde{x}}^{(1)} = \tilde{\psi}_{\tilde{x}\tilde{x}\tilde{x}\tilde{x}\tilde{x}}^{(1)}$$

Seek solutions of the form  $\tilde{\psi} = \tilde{\psi}_0 e^{r\tilde{x}}$ . Then  $r^4 - \beta r = 0$  so  $r = 0, \beta^{1/3}, -\frac{1}{2}\beta^{1/3} \pm i\frac{\sqrt{3}}{2}\beta^{1/3}$ . The general solution is therefore

$$\tilde{\psi}^{(1)} = A(y) + B(y)e^{\beta^{1/3}\tilde{x}} + C(y)e^{-\beta^{1/3}\frac{\tilde{x}}{2}}e^{i\frac{\sqrt{3}}{2}\beta^{1/3}\tilde{x}} + D(y)e^{-\beta^{1/3}\frac{\tilde{x}}{2}}e^{-i\frac{\sqrt{3}}{2}\beta^{1/3}\tilde{x}}$$

In order for the interior and boundary layer flows to match asymptotically, we apply the matching condition  $\lim_{\tilde{x}\to\infty} \tilde{\psi}^{(1)} = 0$ . Thus A(y) = B(y) = 0. For convenience we re-define C and D to get

$$\tilde{\psi}^{(1)} = C(y)e^{-\beta^{1/3}\frac{\tilde{x}}{2}}\cos\left(\frac{\sqrt{3}}{2}\beta^{1/3}\tilde{x} + D(y)\right)$$

We now apply the boundary conditions.  $\psi = 0$  at x = 0 gives  $\tilde{\psi}^{(1)} = -\psi^I|_{x=0}$ . Hence

$$C(y)\cos D(y) = -G(y)$$

 $\psi_x = 0 \text{ at } x = 0 \text{ gives } \psi_x^{(1)} = -\psi_x^I|_{x=0}. \text{ Hence}$ 

$$\varepsilon^{-1/3}\tilde{\psi}_{\tilde{x}}^{(1)} = -\frac{w(y)}{\beta}$$

$$\varepsilon^{-1/3}(-\frac{1}{2}\beta^{1/3})C(y)\cos D(y) - \varepsilon^{-1/3}\frac{\sqrt{3}}{2}\beta^{1/3}C(y)\sin D(y) = -\frac{w(y)}{\beta}$$

Since  $\varepsilon \ll 1$  and can be taken arbitrarily small, we require

$$-\frac{1}{2}\cos D(y) = \frac{\sqrt{3}}{2}\sin D(y)$$

$$\implies \tan D(y) = -\frac{1}{\sqrt{3}}$$

$$\implies D(y) = -\frac{\pi}{6}$$

Combining the boundary conditions we also have  $C(y) = -\frac{2}{\sqrt{3}}G(y)$ . Finally we have

$$\tilde{\psi}^{(1)} = -\frac{2}{\sqrt{3}}G(y)e^{-\beta^{1/3}\frac{\tilde{x}}{2}}\cos\left(\frac{\sqrt{3}}{2}\beta^{1/3}\tilde{x} - \frac{\pi}{6}\right)$$

**Region II.** Here, we define a rescaled coordinate  $\tilde{x} = \frac{x-L}{\varepsilon^{1/3}}$ . The same PDE is satisfied in region II, so the general solution is the same. Here, the matching condition is  $\lim_{\tilde{x}\to-\infty}\tilde{\psi}^{(2)}=0$  which gives A(y)=C(y)=D(y)=0, so

$$\tilde{\psi}^{(2)} = B(y)e^{\beta^{1/3}\tilde{x}}$$

We now apply the boundary conditions.  $\psi_x = 0$  at x = L gives

$$\begin{split} \varepsilon^{-1/3} \tilde{\psi}^{(2)} &= -\psi_x^I \quad \text{at} \quad x = L \\ \varepsilon^{-1/3} \beta^{1/3} B(y) &= -\frac{w(y)}{\beta} \\ \Longrightarrow B(y) &= -\frac{\varepsilon^{1/3} w(y)}{\beta^{4/3}} \end{split}$$

To enforce  $\psi = 0$  at x = L, note  $\lim_{\varepsilon \to 0} B(y) = 0$ , so  $\tilde{\psi}^{(2)}|_{x=L} \to 0$  as  $\varepsilon \to 0$  so we instead require  $\psi^I|_{x=L} = 0$ .

$$\implies G(y) = -\frac{w(y)L}{\beta}$$

Hence we have

$$\tilde{\psi}^{(2)} = -\varepsilon^{1/3} w(y) \beta^{-4/3} e^{\beta^{1/3} \tilde{x}}$$

**Full solution.** The full solution  $\psi = \psi^I + \psi^{(1)} + \psi^{(2)}$  is

$$\begin{split} \psi &= \frac{x-L}{\beta} w(y) & \text{interior} \\ &+ \frac{2w(y)L}{\sqrt{3}\beta} e^{-\beta^{1/3} \frac{x}{2\nu^{1/3}}} \cos\left(\frac{\sqrt{3}}{2}\beta^{1/3}\nu^{-1/3}x - \frac{\pi}{6}\right) & \text{western boundary correction} \\ &- \nu^{1/3}\beta^{-4/3} w(y) e^{\beta^{1/3} \frac{x-L}{\nu^{1/3}}} & \text{eastern boundary correction} \end{split}$$

Note that the Eastern boundary correction is  $\mathcal{O}(\nu^{1/3})$  whilst the Western boundary correction is  $\mathcal{O}(1)$ .

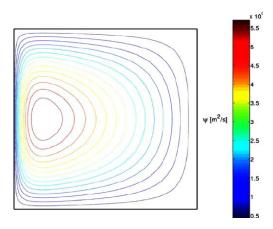
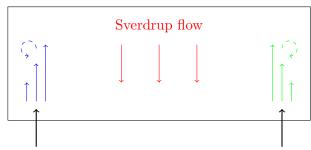


Figure 5: Streamlines of  $\psi$  demonstrating western boundary currents.

**Physical explanation.** The cause of western boundary currents can be physically explained by vorticity. The wind stress curl w < 0 inputs negative vorticity in the interior flow. The flow in the western boundary layer inputs positive vorticity to compensate.



friction adds positive vorticity

friction adds negative vorticity

2/11/20

## 8 Stratification and internal gravity waves

#### 8.1 Boussinesq approximation

We will consider stably stratified flow under the Boussinesq approximation: we assume the density  $\rho$  may be split into two parts  $\rho_0$  and  $\rho'$  with  $\rho_0$  constant and  $\rho'/\rho_0 \ll 1$ . The pressure may then also be split into two parts,  $p_0(z)$ , such that  $-p'_0(z) = \rho_0 g$ , and the remainder p'. The vertical component of the momentum equations may then be written

$$\begin{split} \frac{\mathrm{D}w}{\mathrm{D}t} &= -\frac{1}{\rho_0 + \rho'} \frac{\partial p_0}{\partial z} - \frac{1}{\rho_0 + \rho'} \frac{\partial p'}{\partial z} - g \\ &= -\frac{1}{\rho_0} \frac{\partial p_0}{\partial z} + \frac{\partial p_0}{\partial z} \left[ \frac{1}{\rho_0} - \frac{1}{\rho_0 + \rho'} \right] - \frac{\partial p'}{\partial z} \frac{1}{\rho_0 + \rho'} - g \\ &\approx -\frac{1}{\rho_0} \frac{\partial p'}{\partial z} - \frac{\rho'}{\rho_0} g \end{split}$$

where terms including  $\rho'$  are discarded unless multiplying g. The Boussinesg equations are therefore

$$\frac{\mathbf{D}\boldsymbol{u}}{\mathbf{D}t} + \boldsymbol{f} \times \boldsymbol{u} = -\frac{1}{\rho_0} \nabla p' + \frac{\rho'}{\rho_0} \boldsymbol{g}$$
$$\nabla \cdot \boldsymbol{u} = 0$$
$$\frac{\mathbf{D}\rho'}{\mathbf{D}t} = 0$$

These equations make clear the role of buoyancy: a light fluid parcel experiences an upward force and a heavy fluid parcel experiences a downward force.

It is further useful to write  $\rho'(x, y, z, t) = \rho_s(z) + \tilde{\rho}(x, y, z, t)$  where  $\rho_s(z)$  is a background or reference density and  $\tilde{\rho}$  is the dissturbance density which is zero for fluid at rest.

The stability of the reference density state is determined by the buoyancy frequency or Brunt-Väisäla frequency N defined by

$$N^2 = -\frac{g}{\rho_0} \frac{\mathrm{d}\rho_s}{\mathrm{d}z}$$

#### 8.2 Stratification in the atmosphere and ocean

In the ocean, the buoyancy frequency N is typically  $10^{-2}s^{-1}$  in the upper ocean where stratification is strong, and  $5 \times 10^{-4}s^{-1}$  in the deep ocean, where stratification is weak.

In the atmosphere, calculating N needs to take account of compressibility, because the density  $\rho$  is not conserved by a fluid parcel in reversible, dissipationless motion. The quantity that is instead conserved is the *potential temperature* 

$$\theta = T \left(\frac{p}{p_0}\right)^{-2/7}$$

where T is temperature. The corresponding buoyancy frequency is

$$N^2 = -\frac{g}{\theta} \frac{\mathrm{d}\theta}{\mathrm{d}z}$$

In this course we will use the Boussinesq approximation for the atmosphere and ocean, despite issues with compressibility.

#### 8.3 Small-ampltiude motion about a state of rest

We linearise about a resting state with density structure represented by the buoyancy frequency N. For simplicity, background rotation is ignored for the time being. We define the buoyancy  $\sigma = \rho' g/\rho_0$  for convenience.

$$\tilde{\boldsymbol{u}}_t = -\frac{1}{\rho_0} \nabla \tilde{p} + \tilde{\sigma} \hat{\boldsymbol{z}}$$

$$\nabla \cdot \tilde{\boldsymbol{u}} = 0$$

$$\tilde{\sigma} + N^2 \tilde{w} = 0$$

where the notation  $\tilde{u}$  denotes the disturbance quantities away from a state of rest. These can be combined into a single equation for  $\tilde{w}$ :

$$\nabla^2 \tilde{w}_t t + N^2 (\tilde{w}_{xx} + \tilde{w}_{yy}) = 0$$

Assuming  $N^2$  is constant, seek plane wave solutions  $\tilde{w} = \hat{w}e^{i(kx+ly+mz-\omega t)}$ . This gives a dispersion relation

$$\omega^2 = N^2 \frac{k^2 + l^2}{k^2 + l^2 + m^2}$$

Note that if  $N^2>0$  we get oscillatory motion, and if  $N^2<0$  we get exponentially growing disturbances. We also have  $0\leq |\omega|\leq N$  with the lower limit achieved in the limit  $k^2+l^2\ll m^2$ . Define  $\theta=\tan^{-1}(m(k^2+l^2)^{-1/2})$ , the angle a surface of constant phase makes with the vertical. Then  $\omega=\pm N\cos\theta$ . Owing to incompressibility  $\nabla\cdot \boldsymbol{u}=0$ , the velocity vector is perpendicular to  $\boldsymbol{k}$ . Thus  $\theta$  is also the angle that fluid parcel trajectories make with the vertical.

The fact  $|\omega| \leq N$  implies only disturbances with a sufficiently low frequency can propagate as waves. Localised forcing with frequency greater than N will remain localised rather than propagating. Further, note the group velocity is

$$c_g \equiv \frac{\partial \omega}{\partial \mathbf{k}} = \pm \frac{N}{(k^2 + l^2)^{1/2} (k^2 + l^2 + m^2)^{3/2}} (km^2, lm^2, -m(k^2 + l^2))$$

which gives  $c_q \cdot k = 0$ , i.e. the group velocity is perpendicular to phase surfaces.