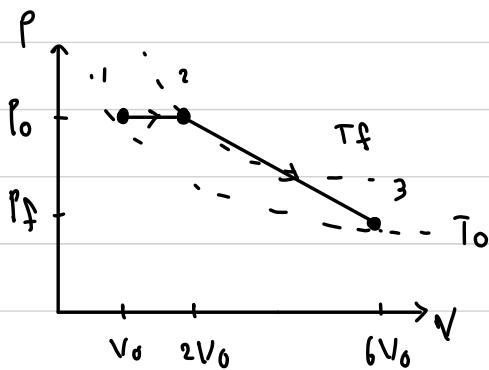


Homework * 2: Thermodynamics

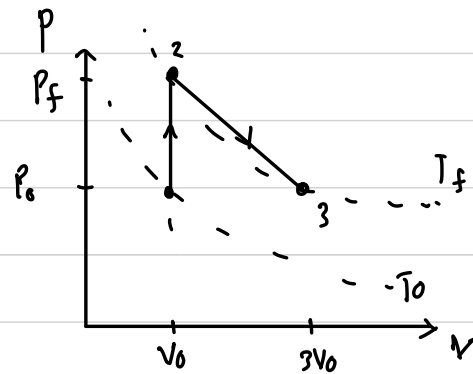
Gornain Af

21/081767/TK/53170

Problem * 1: Gas Expansion



Process A



Process B

Gas is ideal with n moles and molar specific heat C_v in sealed container

[A] Determine the value of P_f and T_f in these process!

* Process A

Process 1 to 2

$$PV = nRT$$

$P = \text{constant}$

$$P = \frac{nRT}{V}$$

$$P_0 = P_0 \quad (\text{Isobaric})$$

$$\frac{nRT_0}{V_0} = \frac{nRT_f}{2V_0}$$

$$T_f = 2T_0$$

Process 2 to 3

The equation is

$$PV = nRT$$

$nR = \text{constant}$

$$PV = T$$

$$\frac{P_2 V_2}{P_3 V_3} = \frac{T_2}{T_3}$$

$$\frac{P_0 2V_0}{P_f 6V_0} = \frac{T_f}{T_0}$$

We know that

$$T_f = 2T_0$$

$$\frac{2P_0}{6P_f} = \frac{2T_0}{T_0}$$

$$P_0 = 6P_f$$

$$P_f = \frac{1}{6} P_0$$

From the table, we know

$$\begin{aligned} \text{that } P_0 &= \frac{nRT_0}{V_0} = \frac{nRT_f}{2V_0} \\ &= \frac{nR2T_0}{2V_0} = \frac{nRT_0}{V_0} \end{aligned}$$

$$P_f = \frac{1}{6} \frac{nRT_0}{V_0}$$

$$\boxed{\begin{aligned} \text{Thus, } P_f &= \frac{nRT_0}{6V_0} \\ \text{and } T_f &= 2T_0 \end{aligned}}$$

* Process B

Process 1 to 2 (isochoric)

$$PV = nRT$$

$$\frac{P}{T} = \frac{nR}{V} = \text{constant}$$

$$\frac{P_1}{T_1} = \frac{P_2}{T_2} \rightarrow \frac{P_0}{T_0} = \frac{P_f}{T_f}$$

$$\text{We know that } P_0 = \frac{nRT_0}{V_0}$$

$$\frac{nRT_0}{V_0 T_0} = \frac{P_f}{T_f}$$

<p>* Process 2 to 3 (isothermik)</p> $P_V = nRT = \text{constant}$ $P_2 V_2 = P_3 V_3$ $P_f V_f = P_0 V_0$ $P_f = 3P_0$	<p>We know that</p> $Q = \Delta E_{th} - W$ <p>or $\Delta E_{th} = n C \Delta T$</p> <p>and $W = - n R \Delta T$</p>	$W = - \frac{C_V}{R} [P_3 V_3 - P_2 V_2]$ $= - \frac{C_V}{R} [P_f V_0 - P_0 2V_0]$ $= - \frac{C_V V_0}{R} [6P_f - 2P_0]$ <p>we know that $P_f = \frac{1}{6} P_0$</p> $W = - \frac{C_V V_0}{R} [P_0 - 2P_0]$ $W = \frac{C_V V_0 P_0}{R}$
<p>Now substitute $P_f = 3P_0$ into</p> $\frac{P_f}{T_f} = \frac{nR}{V_0}$ $\frac{3P_0}{T_f} = \frac{nR}{V_0}$	<p>* Process A</p> <p>Q in process 1 to 2 (isobaric)</p> $Q_{12} = \Delta E_{th} - W$ $\Delta E_{th} = n C_V (T_f - T_0)$ $W = - n R (T_f - T_0)$	$Q_{23} = \Delta E_{th} - W$ $= n C_V T_0 - \frac{C_V V_0 P_0}{R}$ $= C_V (n T_0 - \frac{V_0 P_0}{R})$ <p>we know $P_0 V_0 = n R T_0$</p> $= C_V (n T_0 - \frac{n R T_0}{R}) = 0$
<p>We know that $P_0 = \frac{n R T_0}{V_0}$</p> $\frac{3 n R T_0}{T_f V_0} = \frac{n R}{V_0}$ $T_f = 3 T_0 //$	$Q_{12} = n C_V (T_f - T_0) + n R (T_f - T_0)$ $= n (T_f - T_0) (C_V + R)$ <p>We know that</p> $T_f = 2 T_0$ $Q_{12} = n (2 T_0 - T_0) (C_V + R)$ $= n T_0 (C_V + R)$	<p>$Q_{23} = 0 //$ because adiabatic has no heat transfer between system and environment.</p> <p>So the total heat added into the system A is</p> $Q_{12} + Q_{23} = Q_{12} + 0$ $= n T_0 (C_V + R) //$
<p>Substitute to $\frac{P_f}{T_f} = \frac{n R}{V_0}$</p> $\frac{P_f}{3 T_0} = \frac{n R}{V_0}$ $P_f = n R 3 T_0 V_0 //$	<p>Q in process 2 to 3 (adiabatic)</p> $Q_{23} = \Delta E_{th} - W$ $\Delta E_{th} = n C_V \Delta T = n C_V T_0$ $W = - \frac{1}{\gamma - 1} (P_3 V_3 - P_2 V_2)$ <p>we know that Laplace constant</p> $\gamma = \frac{C_P}{C_V} = \frac{C_V + R}{C_V}$ $W = - \frac{1}{\frac{R}{C_V}} (P_3 V_3 - P_2 V_2)$	<p>* Process B</p> <p>Q in process 1 to 2 (isobaric)</p> $Q_{12} = \Delta E_{th} - W$ $\Delta E_{th} = n C_V \Delta T = n C_V (T_f - T_0)$ <p>we know that $T_f = 3 T_0$</p> $\Delta E_{th} = 2 n C_V T_0$ <p>$W = 0$ because isobaric has no change on system volume.</p>
<div style="border: 1px solid black; padding: 5px; margin-bottom: 10px;"> <p>Thus, $T_f = 3 T_0$ and $P_f = n R 3 T_0 V_0$</p> </div> <p>Q Determine the amount of heat Q added into the system during this process.</p>		

$$Q_{12} = \Delta E_{th} - 0 \\ = 2nCvT_0$$

Q in process 2 to 3
(isothermic)

$$Q_{23} = \Delta E_{th} - W$$

Because it is isothermic

process, the thermal energy

is constant; thus $\Delta E_{th} = 0$

$$Q_{23} = -W$$

$$W = \int_{V_0}^{V_f} p dV; p = \frac{nRT}{V} \\ \int_{V_0}^{V_f} nRT \frac{dV}{V} = nRT \int_{V_0}^{V_f} \frac{dV}{V}$$

$$V_f = 3V_0$$

$$W = nRT \int_{V_0}^{3V_0} \frac{dV}{V} = nRT \ln \frac{3V_0}{V_0}$$

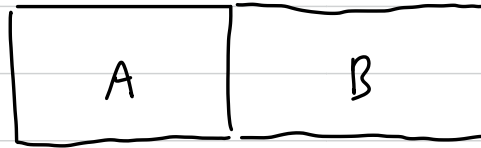
$$W = nRT \ln 3; T_f = 3T_0$$

$$W = 3nRT_0 \ln 3$$

So, the Q total in system B is

$$Q_{12} + Q_{23} = 2nCvT_0 + 3nRT_0 \ln 3 \\ = nT_0 (2Cv + R \ln 3) //$$

Problem #2 : Thermal Equilibrium



M_a, C_a, T_a M_b, C_b, T_b

specific heat = C_a, C_b .

[A] Determine the final temperature T_f of the two metal blocks!

Assume that $T_a > T_b$;

We know thermodynamic

prinsip that $Q_{\text{released}} = Q_{\text{accept}}$,

then the equation can be expressed as

$$Q_{\text{released}} = Q_{\text{accept}}$$

$$Q_A = Q_B$$

$$M_a C_a (T_a - T_f) = M_b C_b (T_f - T_b)$$

$$M_a C_a T_a - M_a C_a T_f = M_b C_b T_f - M_b C_b T_b$$

$$M_a C_a T_a + M_b C_b T_b = M_a C_a T_f + M_b C_b T_f$$

$$M_a C_a T_a + M_b C_b T_b = T_f (M_a C_a + M_b C_b)$$

$$T_f = \frac{M_a C_a T_a + M_b C_b T_b}{M_a C_a + M_b C_b}$$

So, the final temperature at equilibrium
galory is equal to

$$T_f = \frac{M_a C_a T_a + M_b C_b T_b}{M_a C_a + M_b C_b} //$$

[B] Determine the change in blocks'

temperature $\Delta T_a = T_f - T_a$ and

$$\Delta T_b = T_f - T_b$$

We know that $T_f = \frac{M_a C_a T_a + M_b C_b T_b}{M_a C_a + M_b C_b}$ //

$$\Delta T_a = T_f - T_a$$

$$= \frac{M_a C_a T_a + M_b C_b T_b - M_a C_a T_a - M_b C_b T_a}{M_a C_a + M_b C_b}$$

$$= \frac{M_b C_b (T_b - T_a)}{M_a C_a + M_b C_b} = \Delta T_a$$

$$\Delta T_b = T_f - T_b$$

$$= \frac{M_a C_a T_a + M_b C_b T_b - T_b}{M_a C_a + M_b C_b}$$

$$= \frac{M_a C_a T_a + M_b C_b T_b - M_a C_a T_b - M_b C_b T_b}{M_a C_a + M_b C_b}$$

$$= \frac{M_a C_a (T_a - T_b)}{M_a C_a + M_b C_b} = \Delta T_b$$

[C] Assume $M_a = M_b$, $|\Delta T_a| > |\Delta T_b|$
Which metal block has higher specific heat?

We know that :

$$\Delta T_a = \frac{M_b C_b (T_b - T_a)}{M_a C_a + M_b C_b}$$

$$\Delta T_b = \frac{M_a C_a (T_a - T_b)}{M_a C_a + M_b C_b}$$

Now Substitute to $Q_a = Q_b$

$$M_a C_a \Delta T_a = M_b C_b \Delta T_b$$

because $M_a = M_b$, then

$$C_a \Delta T_a = C_b \Delta T_b$$

$$\frac{C_a}{\Delta T_b} = \frac{C_b}{\Delta T_a} \text{ we cannot compare in this way!}$$

Now , because $|\Delta T_a| > |\Delta T_b|$ then

$$|\Delta T_a| = \frac{Q_a}{M_a C_a} > |\Delta T_b| = \frac{Q_b}{M_b C_b}$$

$$\frac{Q_a}{M_a C_a} > \frac{Q_b}{M_b C_b} \rightarrow \frac{Q_a}{C_a} > \frac{Q_b}{C_b}$$

We know that $Q_a = Q_b$ at equilibrium temperature

$$\frac{Q_a}{C_a} > \frac{Q_b}{C_b}$$

$$\frac{1}{C_a} > \frac{1}{C_b} \text{ it means ,}$$

$$C_b > C_a //$$

Thus C_b has higher specific heat compare to C_a .

Problem * 3 : Maxwell - Boltzmann Distribution

Maxwell - Boltzmann Distribution :

$$N_v(v) = 4\pi N_0 \left(\frac{m}{2\pi k_B T} \right)^{3/2} v^2 e^{-mv^2/2k_B T}$$

[A] Prove $v_{rms} = \sqrt{\frac{3k_B T}{m}}$

$$N_V(v) = 4\pi N_0 \left(\frac{m}{2\pi k_B T} \right)^{3/2} v^2 e^{-mv^2/2k_B T}$$

$$V_{rms} = \sqrt{\frac{3k_B T}{m}}$$

We know that

$$N_V(v) dv = 4\pi N_0 \left(\frac{m}{2\pi k_B T} \right)^{3/2} v^2 e^{-mv^2/2k_B T} dv$$

The formula for V_{rms} in general is

$$V_{rms} = \left(\frac{\sum n_i v_i^2}{\sum n_i} \right)^{1/2}$$

Because it is a continuous function, then we can use calculus for the sigma notation

$$V_{rms}^2 = \frac{\sum n_i v_i^2}{\sum n_i}$$

calculus notation:

$$V_{rms}^2 = \frac{\int_0^\infty v^2 N_V(v) dv}{\int_0^\infty N_V(v) dv}$$

We know that $N = \int_{v_1}^{v_2} N_V(v) dv$ so

$$\begin{aligned} &= \frac{\int_0^\infty v^2 N_V(v) dv}{N_0} \\ &= \frac{1}{N_0} \int_0^\infty v^2 4\pi N_0 \left(\frac{m}{2\pi k_B T} \right)^{3/2} v^2 e^{-mv^2/2k_B T} dv \\ &= 4\pi \left(\frac{m}{2\pi k_B T} \right)^{3/2} \int_0^\infty v^4 e^{-mv^2/2k_B T} dv \end{aligned}$$

We know that $\int_0^\infty x^4 e^{-ax^2} = \frac{3}{8} \sqrt{\frac{\pi}{a^5}}$

Where $a = \frac{m}{2k_B T}$

Substitute the equation into the integral equation

$$\begin{aligned} V_{rms}^2 &= 4\pi \left(\frac{m}{2\pi k_B T} \right)^{3/2} \int_0^\infty v^4 e^{-mv^2/2k_B T} dv \\ &= 4\pi \left(\frac{m}{2\pi k_B T} \right)^{3/2} \left(\frac{3}{8} \sqrt{\frac{\pi}{\left(\frac{m}{2k_B T} \right)^5}} \right) \\ &= 4\pi \left(\frac{m}{2\pi k_B T} \right)^{3/2} \frac{3}{8} \sqrt{\pi} \sqrt{\frac{(2k_B T)^5}{m^5}} \\ &= \frac{4\pi}{2\pi k_B T} \frac{\sqrt{m}}{\sqrt{2k_B T}} \frac{3}{8} \sqrt{\pi} \left(\frac{2k_B T}{m} \right)^2 \sqrt{\frac{2k_B T}{m}} \end{aligned}$$

$$V_{rms}^2 = \frac{3k_B T}{m}$$

$$V_{rms} = \sqrt{\frac{3k_B T}{m}} \quad \text{proved}$$

Q3 Prove $V_{avg} = \sqrt{\frac{8k_B T}{\pi m}}$

The formula of V_{avg} in general is expressed as :

$$V_{avg} = \frac{\sum n_i v_i}{\sum n_i} \quad \text{we can convert into integral notation}$$

$$V_{avg} = \frac{\int_0^\infty v N_V(v) dv}{\int_0^\infty N_V(v) dv};$$

We know that $N = \int_{v_1}^{v_2} N_V(v) dv$, so

$$V_{avg} = \frac{\int_0^{\infty} V N_V(V) dV}{N_0}$$

$$= \frac{1}{N_0} \int_0^{\infty} V 4\pi N_0 \left(\frac{m}{2\pi k_B T}\right)^{3/2} V^2 e^{-mv^2/2k_B T} dV$$

$$= 4\pi \left(\frac{m}{2\pi k_B T}\right)^{3/2} \int_0^{\infty} V^3 e^{-mv^2/2k_B T} dV$$

We know from the question that:

$$\int_0^{\infty} x^3 e^{-ax^2} = \frac{1}{2a^2}$$

Where $a = \frac{m}{2k_B T}$; so

$$V_{avg} = 4\pi \left(\frac{m}{2\pi k_B T}\right)^{3/2} \frac{1}{2\left(\frac{m}{2k_B T}\right)^2}$$

$$= 2\pi \frac{m}{2\pi k_B T} \sqrt{\frac{m}{2\pi k_B T}} \left(\frac{2k_B T}{m}\right)^2$$

$$= \frac{m}{k_B T} \sqrt{\frac{m}{2\pi k_B T}} \left(\frac{k_B T}{m}\right)^2 4$$

$$V_{avg} = \sqrt{\frac{16\pi k_B T^2}{2\pi k_B T m^2}} = \sqrt{\frac{8 k_B T}{\pi m}} \quad \text{proved}$$

[C] Prove $V_{mp} = \sqrt{\frac{2k_B T}{m}}$

V_{mp} is the maximum number of molecule at speed of V to $V+dV$.

So, the expression can be expressed as:

$$N_V(V)dV = 4\pi N_0 \left(\frac{m}{2\pi k_B T}\right)^{3/2} V^2 e^{-mv^2/2k_B T} dV$$

Now, the molecule that having the speed of V is equal to $\frac{N_V(V)}{N}$; so

$$\frac{d N_V(V)}{dV N_0} = 4\pi \left(\frac{m}{2\pi k_B T}\right)^{3/2} V^2 e^{-mv^2/2k_B T} dV$$

$$= 4\pi \left(\frac{m}{2\pi k_B T}\right)^{3/2} \left(V^2 e^{-mv^2/2k_B T} dV\right)$$

$$= 4\pi \left(\frac{m}{2\pi k_B T}\right)^{3/2} \left(2V e^{-mv^2/2k_B T} + V^2 e^{-mv^2/2k_B T} \left(-\frac{2mV}{2k_B T}\right)\right)$$

$$= 4\pi \left(\frac{m}{2\pi k_B T}\right)^{3/2} V e^{-mv^2/2k_B T} \left(2 - \frac{V^2 m}{k_B T}\right)$$

The maximum distribution of speed had value

$$\text{of } \frac{d N_V(V)}{dV N} = 0 \quad \text{so}$$

$$0 = 4\pi \left(\frac{m}{2\pi k_B T}\right)^{3/2} V e^{-mv^2/2k_B T} \left(2 - \frac{V^2 m}{k_B T}\right)$$

$$2 - \frac{V^2 m}{k_B T} = 0$$

$$\frac{V^2 m}{k_B T} = 2 \rightarrow V^2 = \frac{2 k_B T}{m}$$

$$V = \sqrt{\frac{2 k_B T}{m}}$$

Thus, the maximum / most possible distribution of speed:

$$V_{mp} = \sqrt{\frac{2 k_B T}{m}} \quad \text{proved}$$