# **Differential Kinematics**

## 1 FORWARD KINEMATIC EQUATIONS

Recall the forward kinematics formulation  $f_{FPK}$ 

$$P = f_{FPK}(\Theta) p_x = \lambda_2 c_1 c_2 - \lambda_3 c_1 s_{23} p_y = \lambda_2 s_1 c_2 - \lambda_3 s_1 s_{23} p_z = \lambda_1 - \lambda_2 s_2 - \lambda_3 c_{23} \gamma = \phi_4$$
(1)

where  $\Theta$  is the vector of the joint states,

$$\Theta = \begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \\ \theta_4 \end{bmatrix} \tag{2}$$

and p is the position of the end-effector  $\{4\}$  (expressed in base frame  $\{0\}$ )

$$p = \begin{bmatrix} p_x \\ p_y \\ p_z \end{bmatrix} = {}^{0}p_4 \tag{3}$$

# 2 Inverse Kinematic Formulation

Differentiate the equation set 1, to yield,

$$v_{x} = \frac{dp_{x}}{dt} = -\lambda_{2}s_{1}c_{2}\dot{\theta}_{1} - \lambda_{2}c_{1}s_{2}\dot{\theta}_{2} + \lambda_{3}s_{1}s_{23}\dot{\theta}_{1} - \lambda_{3}c_{1}c_{23}\dot{\theta}_{2} - \lambda_{3}c_{1}c_{23}\dot{\theta}_{3}$$

$$v_{y} = \frac{dp_{y}}{dt} = \lambda_{2}c_{1}c_{2}\dot{\theta}_{1} - \lambda_{2}s_{1}s_{2}\dot{\theta}_{2} - \lambda_{3}c_{1}s_{23}\dot{\theta}_{1} - \lambda_{3}s_{1}c_{23}\dot{\theta}_{2} - \lambda_{3}s_{1}c_{23}\dot{\theta}_{3}$$

$$v_{z} = \frac{dp_{z}}{dt} = \lambda_{1} - \lambda_{2}c_{2}\dot{\theta}_{2} + \lambda_{3}s_{23}\dot{\theta}_{2} + \lambda_{3}s_{23}\dot{\theta}_{3}$$

$$\dot{\gamma} = \frac{d\gamma}{dt} = \dot{\theta}_{4}$$
(4)

This can be represented in matrix form,

$$V = {}^{0}J\dot{\Theta}$$

$$\begin{bmatrix} v_{x} \\ v_{y} \\ v_{z} \\ \dot{\gamma} \end{bmatrix} = \begin{bmatrix} -\lambda_{2}s_{1}c_{2} + \lambda_{3}s_{1}s_{23} & -\lambda_{2}c_{1}s_{2} - \lambda_{3}c_{1}c_{23} & -\lambda_{3}c_{1}c_{23} & 0 \\ \lambda_{2}c_{1}c_{2} - \lambda_{3}c_{1}s_{23} & -\lambda_{2}s_{1}s_{2} - \lambda_{3}s_{1}c_{23} & -\lambda_{3}s_{1}c_{23} & 0 \\ 0 & -\lambda_{2}c_{2} + \lambda_{3}s_{23} & \lambda_{3}s_{23} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\theta}_{1} \\ \dot{\theta}_{2} \\ \dot{\theta}_{3} \\ \dot{\theta}_{4} \end{bmatrix}$$
(5)

where  ${}^{0}J$  is the manipulator Jacobian expressed in base frame  $\{0\}$ .

### 2.1 SINGULARITY ANALYSIS

The determinant of the Jacobian is derived as,

$$\det {}^{0}\mathbf{J} = (-\lambda_{2}s_{1}c_{2} + \lambda_{3}s_{1}s_{23}) \left( (-\lambda_{2}s_{1}s_{2} - \lambda_{3}s_{1}c_{23})(\lambda_{3}s_{23}) - (-\lambda_{2}c_{2} + \lambda_{3}s_{23})(-\lambda_{3}s_{1}c_{23}) \right) \\ + (\lambda_{2}c_{1}c_{2} - \lambda_{3}c_{1}s_{23}) \left( (-\lambda_{2}c_{2} + \lambda_{3}s_{23})(-\lambda_{3}c_{1}c_{23}) - (-\lambda_{2}c_{1}s_{2} - \lambda_{3}c_{1}c_{23})(\lambda_{3}s_{23}) \right) \\ \det {}^{0}\mathbf{J} = -\lambda_{2}\lambda_{3} \left( s_{1}(-\lambda_{2}s_{1}c_{2} + \lambda_{3}s_{1}s_{23})(s_{2}s_{23} + c_{2}c_{23}) - c_{1}(\lambda_{2}c_{1}c_{2} - \lambda_{3}c_{1}s_{23})(c_{2}c_{23} + s_{2}s_{23}) \right) \\ \det {}^{0}\mathbf{J} = \lambda_{2}\lambda_{3} \left( s_{1}^{2}(\lambda_{2}c_{2} - \lambda_{3}s_{23})(s_{2}s_{23} + c_{2}c_{23}) + c_{1}^{2}(\lambda_{2}c_{2} - \lambda_{3}s_{23})(c_{2}c_{23} + s_{2}s_{23}) \right) \\ \det {}^{0}\mathbf{J} = \lambda_{2}\lambda_{3} \left( \lambda_{2}c_{2} - \lambda_{3}s_{23})(s_{2}s_{23} + c_{2}c_{23}) + c_{1}^{2}(\lambda_{2}c_{2} - \lambda_{3}s_{23})(c_{2}c_{23} + s_{2}s_{23}) \right) \\ \det {}^{0}\mathbf{J} = \lambda_{2}\lambda_{3} (\lambda_{2}c_{2} - \lambda_{3}s_{23})(s_{2}s_{23} + c_{2}c_{23}) \\ \end{pmatrix}$$

#### 2.1.1 Singularity Condition 1:

$$\lambda_2 c_2 - \lambda_3 s_{23} = 0 \tag{7}$$

Which corresponds to the end-effector directly above the base.

#### 2.1.2 Singularity Condition 2:

$$s_2 s_{23} + c_2 c_{23} = 0$$

$$s_2 s_2 c_3 + s_2 c_2 s_3 + c_2 c_2 c_3 - c_2 s_2 s_3 = 0$$

$$c_3 = 0$$
(8)

Which corresponds to the arm either folder into itself or completely stretched out.