

1

(a) Name two advantages of MOSFET. (b) Draw the cross sectional diagram for an enhancement NMOSFET and describe very briefly the structure. Are $I_G = 0$ and $I_D = I_S$?

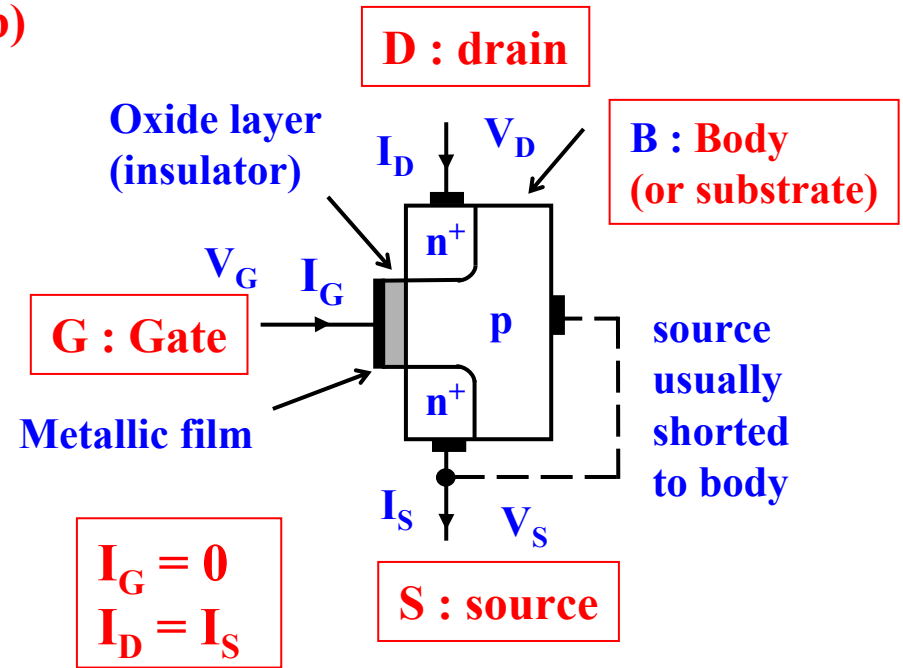
(16)

(a)

small size (scaled down easily)
and low power consumption.

(4)

(b)



(1)

An NMOSFET consists of a **metal gate** insulated from a **p-type semiconductor** substrate (or body) by an insulating layer of **silicon dioxide**. On either side of the gate there are **n type** regions forming the **drain and source**.

(11)

(14)

1

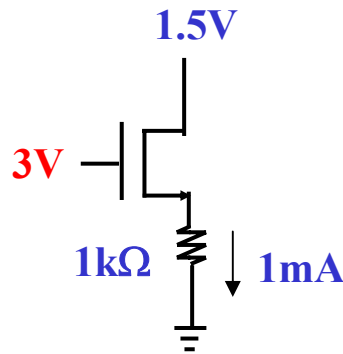
In the circuit, find the MOSFET constant K . Show clearly your reasons. (14)

Given that $V_T = 1V$.

(c)

At triode region, $V_{GS} \geq V_T$, $V_{DS} < V_{GS} - V_T$, $I_D = 2K(V_{GS} - V_T)V_{DS} - KV_{DS}^2$

At saturation region, $V_{GS} \geq V_T$, $V_{DS} \geq V_{GS} - V_T$, $I_D = K[(V_{GS} - V_T)^2]$



$$V_{GS} = 2V \quad V_{DS} = 0.5V \quad (4)$$

Hence NMOS is triode since

$$\begin{aligned} 1. & V_{GS} > V_T \\ 2. & V_{DS} < V_{GS} - V_T \end{aligned} \quad (2)$$

$$\therefore I = 2K[(V_{GS} - V_T)V_{DS} - \frac{V_{DS}^2}{2}]$$

$$\therefore 1mA = 2K[1 * 0.5 - \frac{0.5^2}{2}]$$

$$\therefore K = \frac{1mA}{0.75} = \frac{4}{3} mA/V^2 \quad (8)$$

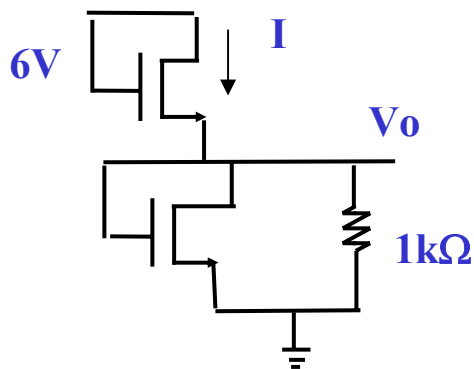
2 Find V_o . Show clearly your reasons. (23)

Given the NMOS are identical,

$$V_T = 1V, K = 0.25m A/V^2.$$

At triode region, $V_{GS} \geq V_T$, $V_{DS} < V_{GS} - V_T$, $I_D = 2K(V_{GS} - V_T)V_{DS} - KV_{DS}^2$

At saturation region, $V_{GS} \geq V_T$, $V_{DS} \geq V_{GS} - V_T$, $I_D = K[(V_{GS} - V_T)^2]$



Assume 2 NMOS are in saturation

$$\therefore I_D = K (V_{GS} - V_T)^2$$

$$\therefore I = 0.25m * (6 - V_o - 1)^2 = 0.25m * (V_o - 1)^2 + \frac{V_o}{1k\Omega}$$

(8)

$$0.25 * (5 - V_o)^2 = 0.25 * (V_o - 1)^2 + V_o$$

$$(5 - V_o)^2 = (V_o - 1)^2 + 4V_o$$

$$25 - 10V_o + V_o^2 = V_o^2 - 2V_o + 1 + 4V_o$$

$$24 - 12V_o = 0$$

$$V_o = 2V$$

(9)

$$V_{GS1} = 4V \quad V_{DS1} = 4V$$

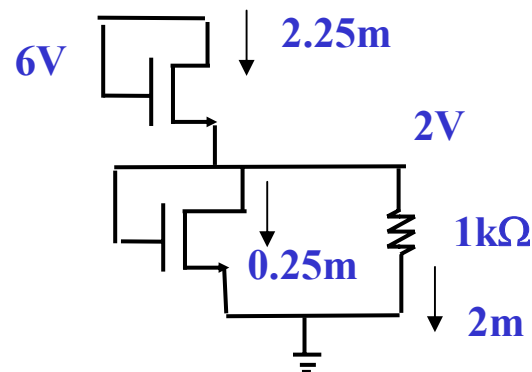
$$V_{GS2} = 2V \quad V_{DS2} = 2V$$

Hence NMOS is saturate since

$$1. V_{GS} > V_T$$

$$2. V_{DS} > V_{GS} - V_T$$

(6)



3

- (a) Find the conductivity of intrinsic (pure) silicon (Si).
Find also the resistivity.
- (b) The pure silicon is doped to n-type Si with a conductivity of $20 / \Omega\text{m}$, suggest a dopant atom. Find also the electron concentration (in atoms / m^3).
- (c) $1 \times 10^{21} / \text{m}^3$ boron atoms are used to dope the pure Si. Find the electron density n , hole density p , and conductivity σ . Is the doped Si n-Si or p-Si?
- (d) Name two III-V compound semiconductor.

Given that $\sigma = e(n\mu_n + p\mu_p)$, $\rho = 1/\sigma$, $np = n_i^2$, $n_i = 1.5 \times 10^{16} / \text{m}^3$, $\mu_p = 0.048 \text{ m}^2/\text{Vs}$, $\mu_n = 0.135 \text{ m}^2/\text{Vs}$, $e = 1.6 \times 10^{-19} \text{ C}$.
Some atoms : group 3 (boron B, gallium Ga, indium In) ; group 5 (nitrogen N, phosphorus P, arsenic As) (40)

(a) The conductivity of intrinsic (pure) Si

$$\begin{aligned}\sigma_i &= e(\mu_n n_i + \mu_p n_i) = en_i(\mu_p + \mu_n) \\ &= 1.6 \times 10^{-19} \times 1.5 \times 10^{16} \times (0.048 + 0.135) \cong 4.39 \times 10^{-4} / \Omega\text{m}\end{aligned}\quad (6)$$

$$\rho_i = \frac{1}{\sigma_i} = \frac{1}{4.39 \times 10^{-4}} \cong 2277 \Omega\text{m} \quad (4)$$

(b) $\therefore \sigma_N = e(\mu_p p + \mu_n n) \cong e(\mu_n n) = 20 / \Omega\text{m}$

$$\therefore n = \frac{20}{1.6 \times 10^{-19} \times 0.135} \cong 9.26 \times 10^{20} / \text{m}^3 \quad (6)$$

P or As. (3)

(c) P-type (2)

$$\therefore p \cong 1 \times 10^{21} \text{ holes} / \text{m}^3 \quad (4)$$

$$\therefore n = \frac{n_i^2}{p} = \frac{(1.5 \times 10^{16})^2}{1 \times 10^{21}} \quad (6)$$

$$\cong 2.25 \times 10^{11} \text{ electrons} / \text{m}^3$$

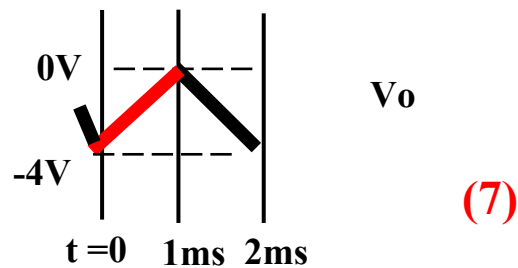
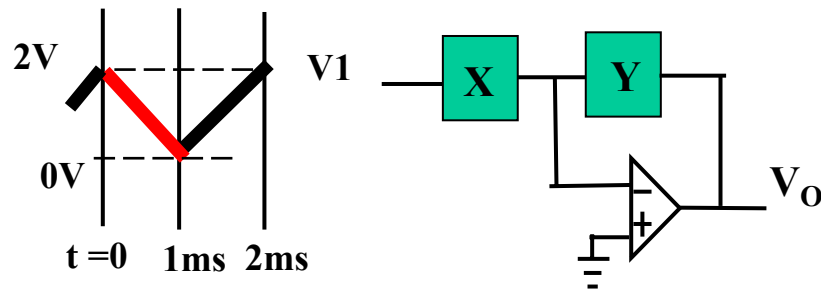
$$\begin{aligned}\therefore \sigma_N &= e(\mu_p p + \mu_n n) \cong e(\mu_p p) \\ &= 1.6 \times 10^{-19} \times 0.048 \times 1 \times 10^{21} \\ &= 7.68 / \Omega\text{m}\end{aligned}\quad (5)$$

(d) III-V compound GaAs, InP etc (4)

4

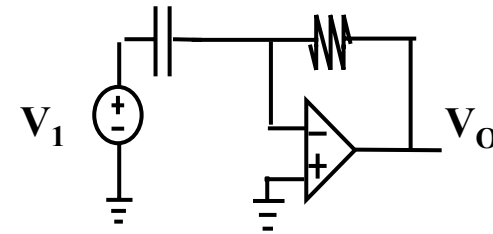
(a)

- (i) If $X = 1\text{k}\Omega$, $Y = 2\text{k}\Omega$, draw the waveform of V_o .
- (ii) If $X = 1\mu\text{F}$, $Y = 1\text{k}\Omega$, derive the equation for the output voltage V_o , and hence draw the waveform of V_o .
- Assume the op amp is ideal. (21)



(21)

$$C = 1\mu\text{F} \quad R = 1\text{k}\Omega$$

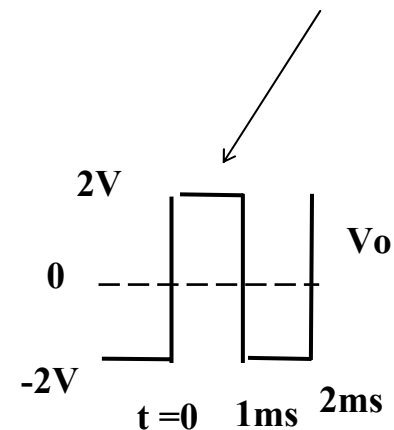


$$-\frac{V_o}{R} = C \frac{dV_1}{dt}$$

$$V_o = -CR \frac{dV_1}{dt}$$

$$V_o = -1\text{ms} * \frac{-2\text{V}}{1\text{ms}} = 2\text{V}$$

(9)



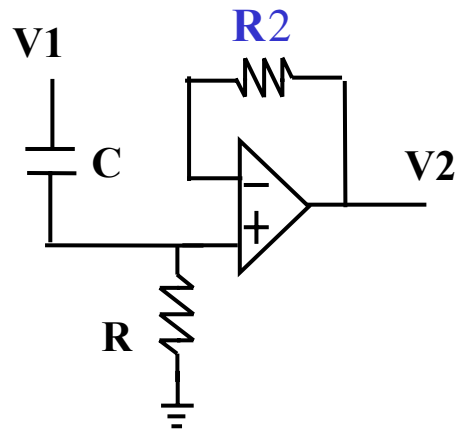
4

(b)

Find the complex transfer function $G (= V_2 / V_1)$ in terms of R , C , R_2 and $j\omega$.

Is the ideal op amp circuit a low pass filter?

(11)



(b)

$$V_2 = V_1 * \frac{R}{R + \frac{1}{j\omega C}}$$

$$G = \frac{V_2}{V_1} = \frac{1}{1 - j/\omega CR} \quad (8)$$

Circuit is a high pass filter (3)

5

In an ideal op amp filter circuit, the complex transfer function $G (= V_o / V_s)$ is given as. $\frac{-20}{1+2j\omega CR}$

- (a) If $V_s(t) = 1 \cos 400kt$ V, find $V_o(t)$.
 (b) Plot the magnitude of G ($|G|$) versus ω . Show clearly the value of $|G|$ when $\omega = 0$, $\omega = \infty$, and $\omega = \omega_O$ (cut-off frequency) in your plot. Find also ω_O .

Given that $1/CR = 800 \text{krad/s}$. (22)

(a)

$$G = \frac{-20}{1+2j*400k*CR} = \frac{-20}{1+j} \quad (5)$$

$$\therefore V_o = 1 \angle 0^\circ * \frac{-20}{1+j} \cong \frac{-20}{\sqrt{2} \angle 45^\circ} \quad (5)$$

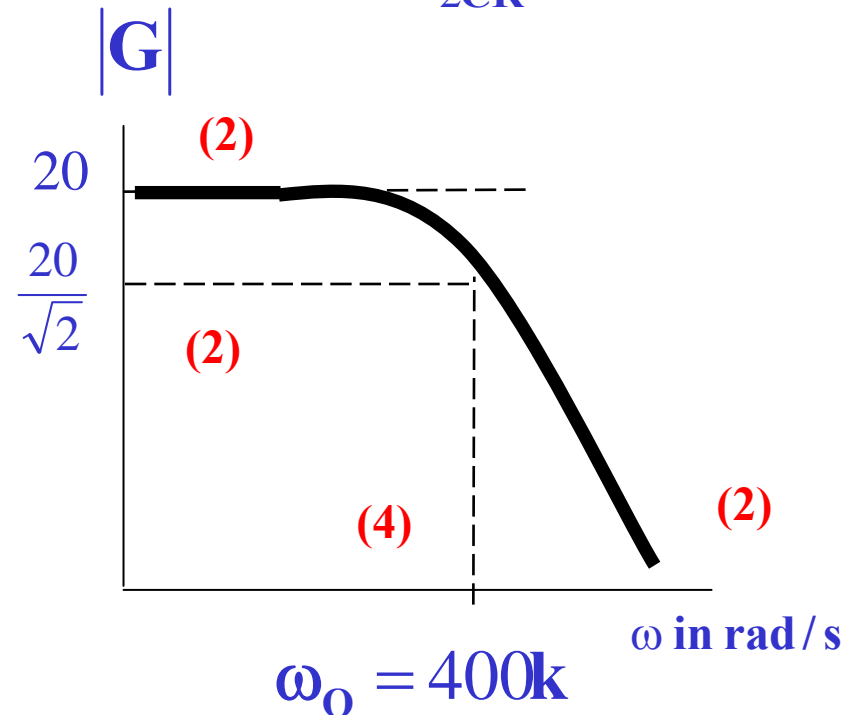
$$V_o(t) = -\frac{20}{\sqrt{2}} \cos(400kt - 45^\circ) \text{ V} \quad (2)$$

$$(b) \quad |G| = 20$$

$$\text{At cut-off frequency, } |G| = \frac{20}{\sqrt{2}}$$

$$G = \frac{-20}{1+j} \Rightarrow 2\omega CR = 1$$

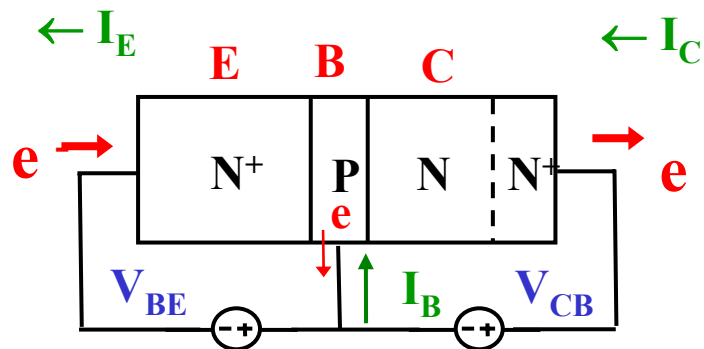
$$\omega = \omega_o = \frac{1}{2CR} = 400 \text{krad/s}$$



6

Draw the cross sectional structure of a NPN BJT transistor operated in the amplifier mode. Describe the movement of electrons, the designs in the emitter/base/collector, and explain briefly the equation $I_E \approx I_C / \alpha$. Given $I_C \cong \beta I_B$, find β in terms of α . (16)

(a)



(4)

1. EB Junction is a forward bias (on) diode and BC is reverse bias (off) diode

2. E is very heavily doped (N^+ for NPN). E has many electrons,

3. B is very thin. So most electrons injected from E (to B) are attracted to C and

$$I_C \cong \alpha I_E \quad (7)$$

$$I_E \cong \frac{I_C}{\alpha} = I_B + I_C = \frac{I_C}{\beta} + I_C$$

$$\text{hence } \frac{1}{\alpha} = \frac{1}{\beta} + 1$$

$$\alpha = \frac{\beta}{\beta + 1}$$

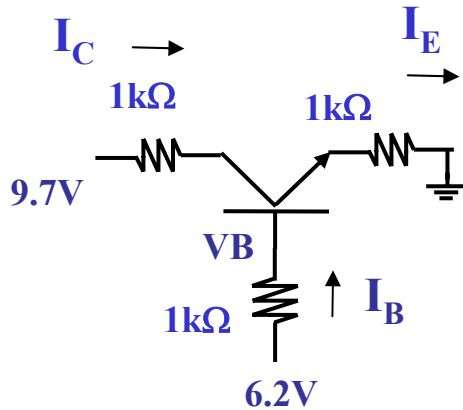
$$\beta = \frac{\alpha}{1 - \alpha} \quad (5)$$

7

- (a) Find the mode of the BJT.
 (b) If $V_B = 5.7V$, find I_C/I_B .

Show clearly your reasons. For the BJT, given

$$V_{BE(ON)} = 0.7V, \beta = 100, V_{CESAT} = 0.2V. \quad (24)$$



(a)

when $V_{CE} = V_{CESAT}$

$$I_C \cong I_E = \frac{9.7V - 0.2V}{2k\Omega} = 4.75mA$$

$$\text{Now } 6.2V = I_B R_B + V_{BE} + I_E R_E \\ \cong 0.7V + I_E 1k\Omega$$

$$\therefore I_E \cong \frac{5.5V}{1k\Omega} \cong 5.5mA$$

Hence BJT is SAT

(11)

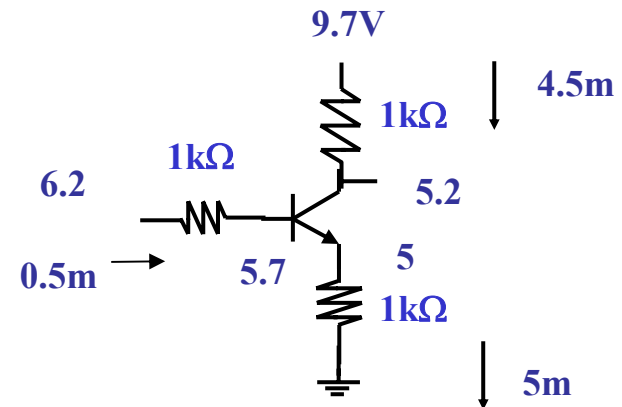
(24)

$$(b) \quad I_B = 0.5mA \quad (2)$$

$$\begin{aligned} \therefore 9.7V &= I_C R_C + V_{CE} + I_E R_E \\ &= \beta' I_B R_C + V_{CE} + (1 + \beta') I_B R_E \\ &= (1 + 2\beta') 0.5mA * 1k\Omega + 0.2V \end{aligned}$$

$$\therefore \beta' = \left(\frac{9.7V - 0.2V}{0.5mA * 1k\Omega} - 1 \right) * \frac{1}{2} = 9$$

(11)

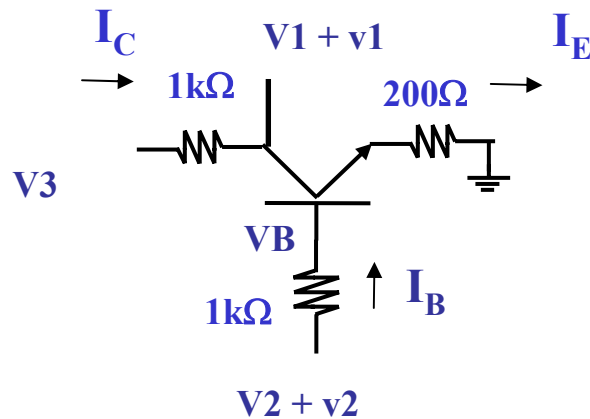


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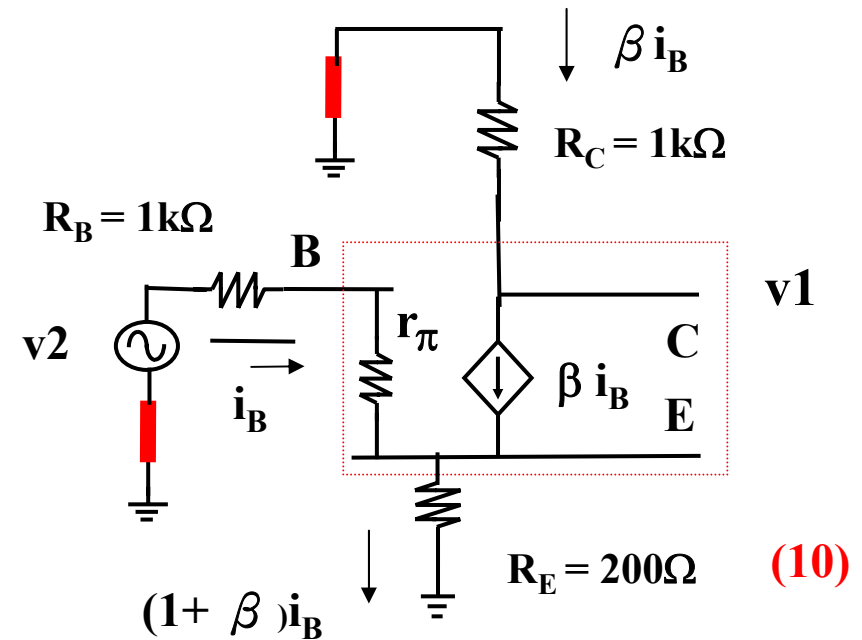
(a) Draw the small signal (AC) equivalent circuit of the BJT amplifier and find the voltage gain $A_v (= v_1 / v_2)$.

(b) The circuit is also a self bias BJT circuit. Explain very briefly why the circuit can have a stable Q point.

Given $r_\pi = 0\Omega$, $\beta = 100$, and $V_{CESAT} = 0.2V$, $V_{BE(ON)} = 0.7V$. (28)



(a)



$$\therefore A_v = \frac{v_1}{v_2} = \frac{-\beta i_B R_C}{i_B (R_B + r_\pi) + (1 + \beta) i_B R_E} \quad (6)$$

$$= \frac{-\beta R_C}{R_B + r_\pi + (1 + \beta) R_E}$$

$$= \frac{-(100)(1k\Omega)}{1000\Omega + 101 * 200\Omega} \cong -4.7 \quad (4)$$

(b)

Since $V_B \sim \text{constant}$

Hence $I_C \uparrow$, $I_E R_E \uparrow$, $V_{BE(ON)} \downarrow$, $I_C \downarrow$

I_C is almost a constant

OR

(8)

$$V_2 = I_B R_B + V_{BE(ON)} + I_E R_E$$

$$\sim V_{BE(ON)} + \beta I_B R_E \sim \text{constant} (= V_B)$$

Hence $I_C = \beta I_B$ is almost a constant

9

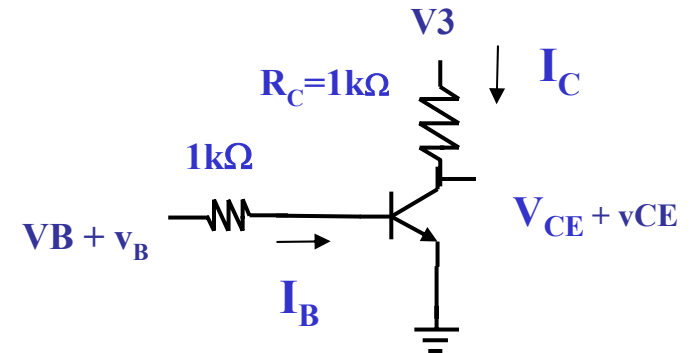
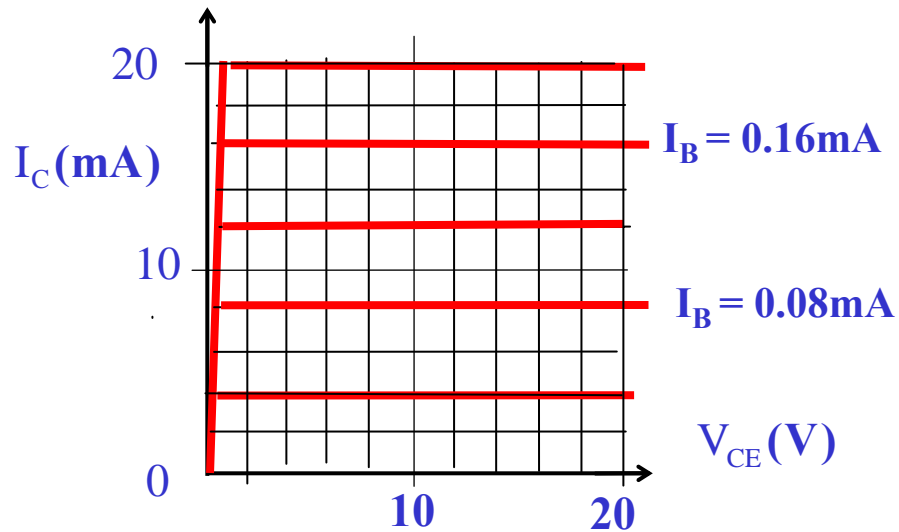
Given the BJT circuit below and the I_C - V_{CE} curve of the BJT. If the Q point is chosen to be $V_{CEQ} = 8V$, $I_{CQ} = 10mA$.

(a) Find V_3 , V_B , draw the load line $V_{CE} = V_3 - I_C R_C$ and locate the Q point on the load line.

(b) If $v_B = 0.02\cos\omega t$ V, estimate the voltage gain v_{CE} / v_B from the load line and I_C - V_{CE} curves. Show also on the load line the range of movement of the bias point.

(c) If $V_{BE(ON)}$ of BJT is changed from 0.7V to 0.68V, sketch and label $V_O(t)$. (34)

For the BJT, given $V_{BE(ON)} = 0.7V$, $V_{CESAT} = 0.2V$.



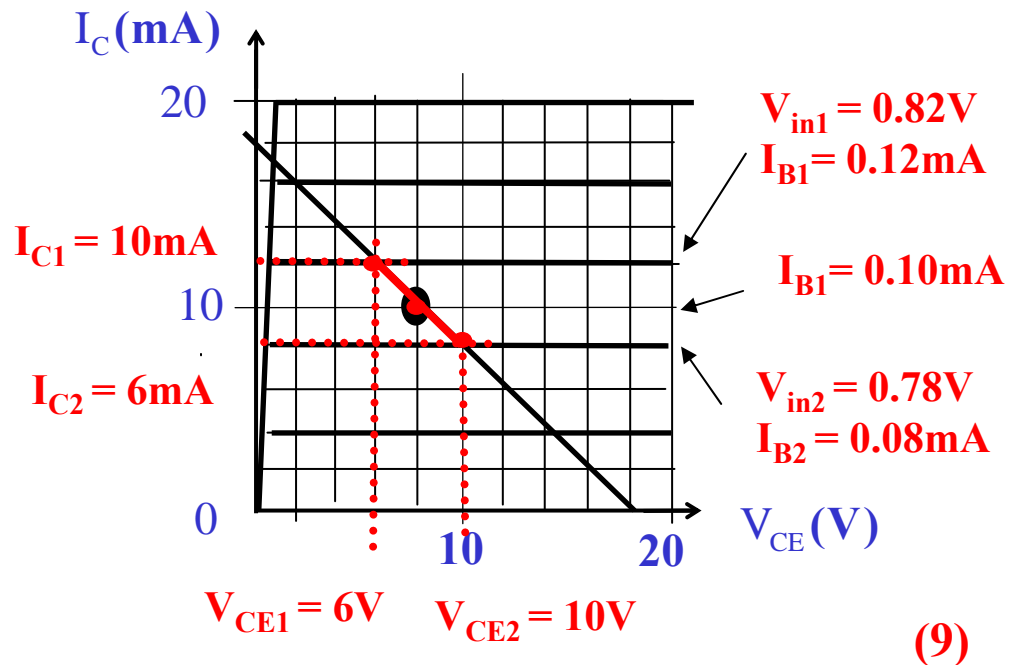
Draw load line, Draw Q point,

(a)

$$\therefore V_3 = 8V + 10mA * 1k\Omega = 18V \quad (4)$$

$$\therefore I_{BQ} = 0.1mA \quad (2)$$

$$\therefore V_B = 0.7V + 0.1mA * 1k\Omega = 0.8V \quad (4)$$



(b)

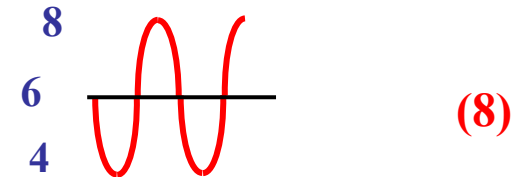
$$\text{voltage gain } A_v = \frac{V_{CE}}{V_B} = \frac{V_{CE2} - V_{CE1}}{V_{in2} - V_{in1}} \cong \frac{10V - 6V}{0.78V - 0.82V} = -100 \quad (7)$$

(c)

Q point shifts to

$$\therefore I_B = \frac{0.8V - 0.68V}{1k\Omega} = 0.12mA$$

V_{CE} roughly ~



(22)

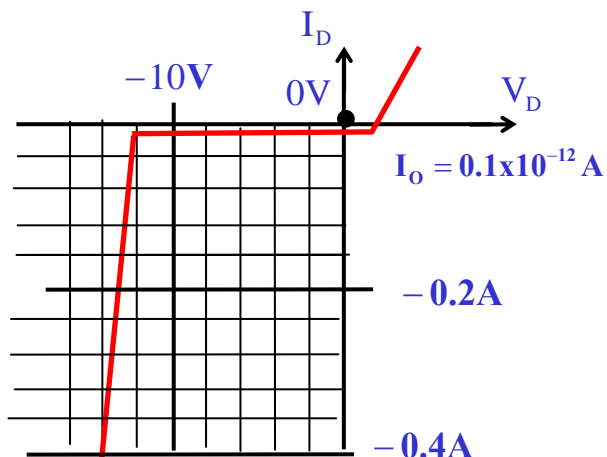
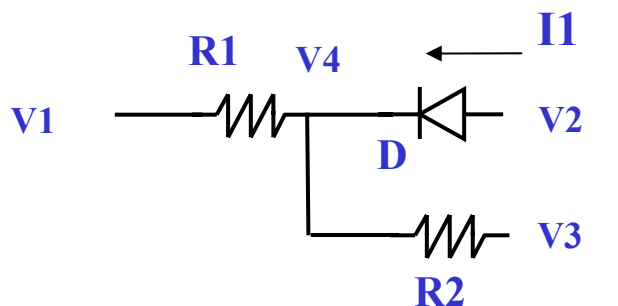
10

- (i) Find the model of the diode at breakdown.
 (ii) Find V_4 if $I_1 = -0.1\text{A}$, $R_1 = R_2 = 10\Omega$, $V_2 = V_3 = 1\text{V}$.
 (iii) Find I_1 if $V_1 = 20\text{V}$, $R_1 = R_2 = 10\Omega$, $V_2 = V_3 = 0\text{V}$.

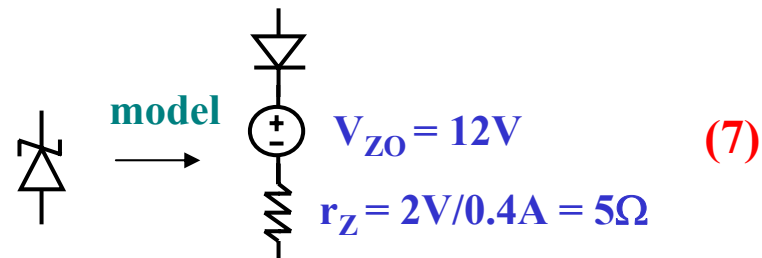
(a)

Show clearly your reasons. (22)

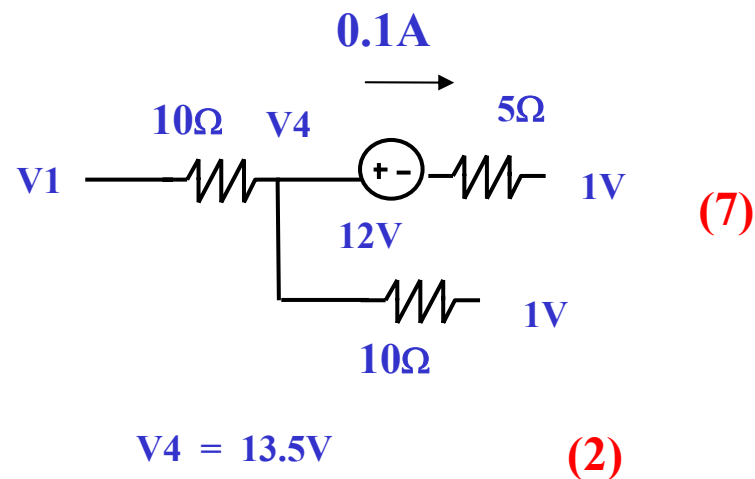
Given that the diode equation is $I_D = I_0 * [e^{\frac{V_D}{25\text{mV}}} - 1]$
 and the diode has the I-V curve as shown.



(i)



(ii)



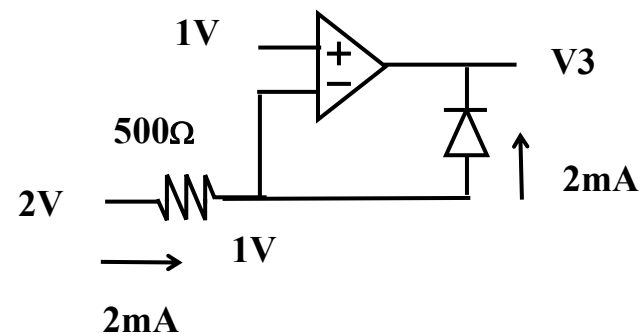
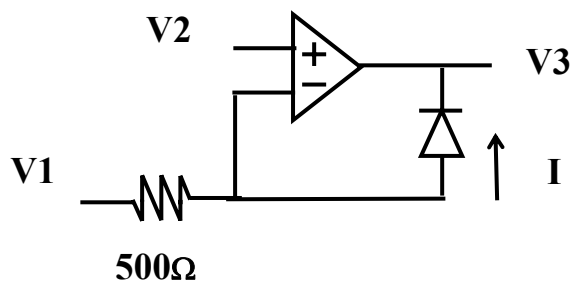
(iii)

$V_4 = 10\text{V}$, D is OFF,
 $I_1 = -0.1\text{pA}$

10

(b)

(The diode in part (a) is used in the ideal op amp circuit,
find V_3 if $V_1 = 2V$, $V_2 = 1V$. (14)



$$\therefore 2\text{mA} = I_0 (e^{\frac{V_D}{25\text{mV}}} - 1) \cong 0.1 \times 10^{-12} (e^{\frac{V_D}{25\text{mV}}}) \quad (7)$$

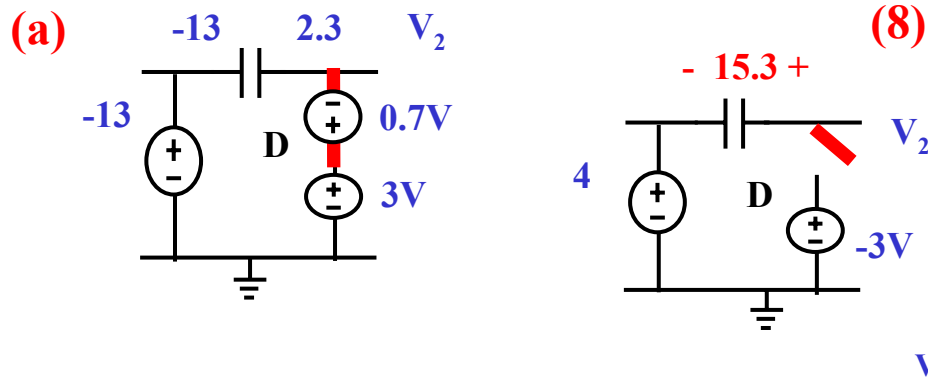
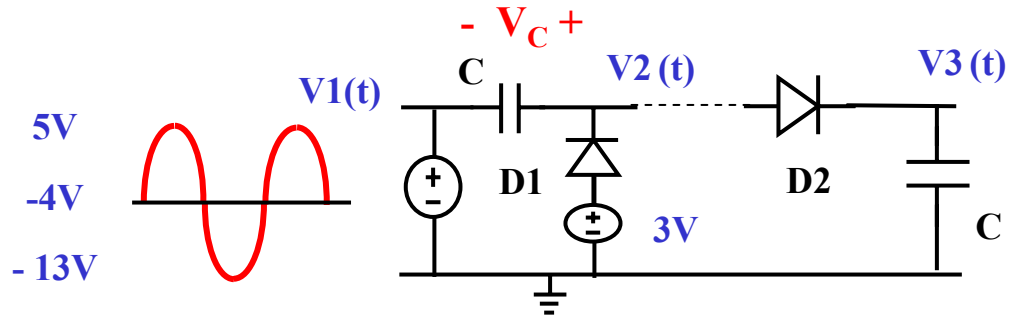
$$\therefore V_D \cong 25\text{mV} * \ln \frac{2\text{mA}}{0.1 \times 10^{-12} \text{A}} \cong 0.593\text{V} \quad (3)$$

$$\therefore V_3 \approx 1\text{V} - 0.593\text{V} = 0.407\text{V} \quad (4)$$

11

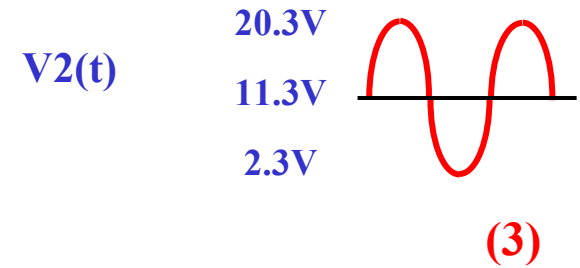
- (a) In the diode circuit, find V_c . Hence sketch and label clearly $V_2(t)$.
- (b) If the capacitor filter (D2 and C circuit) is connected to V_2 , sketch $V_3(t)$.

D1 and D2 are offset diodes with $V_F = 0.7V$. (21)

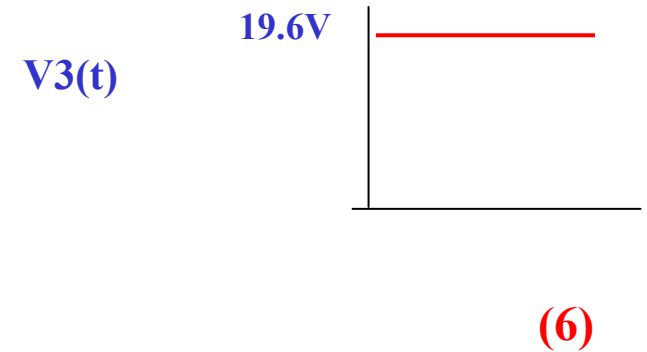


$$V_2 = V_1 + V_c = V_1 + 15.3V$$

(4)



(b)

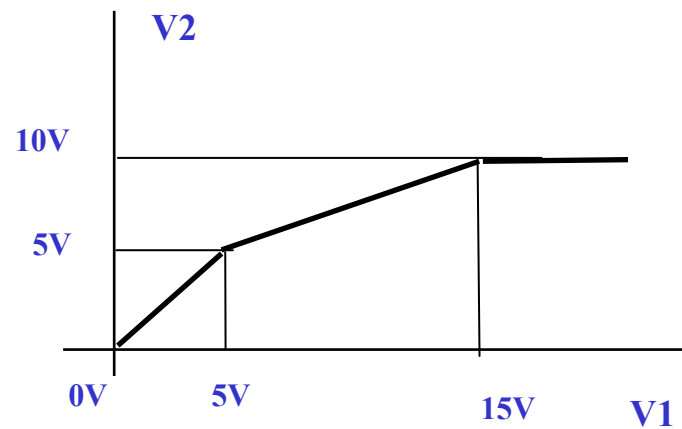
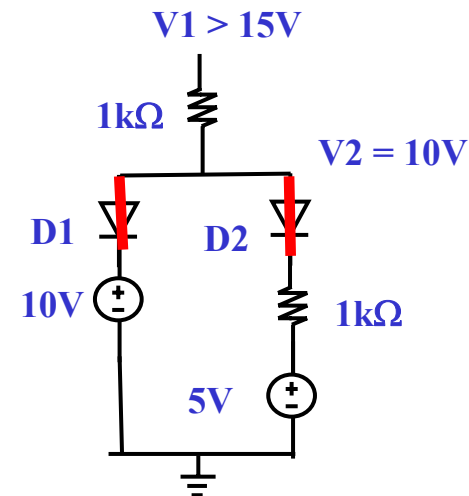
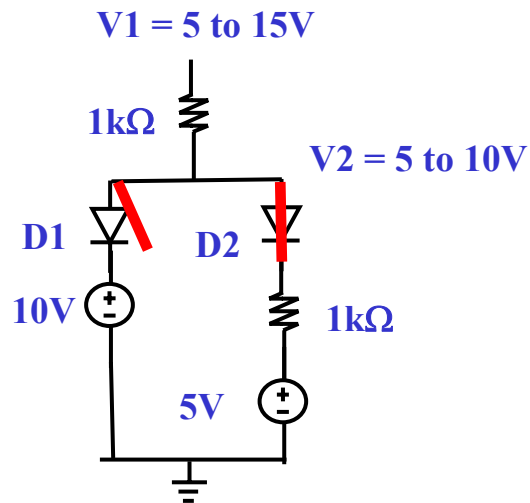
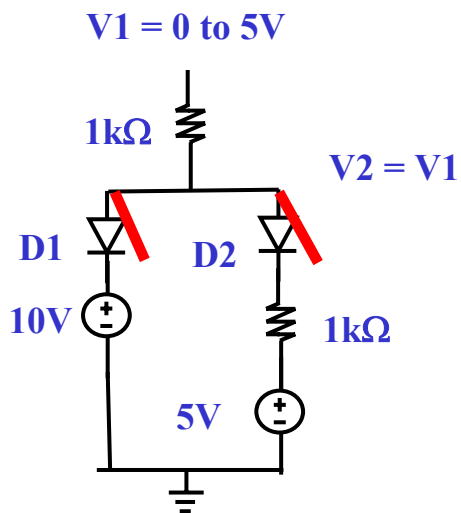
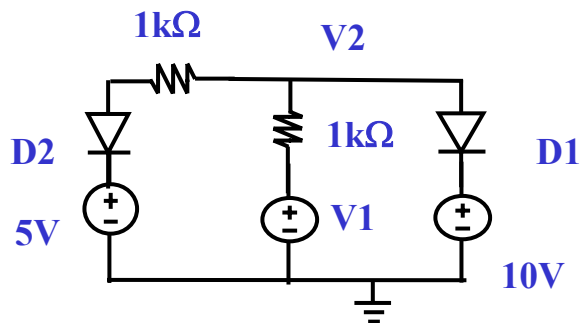


(22)

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In the ideal diode circuit, plot V_2 versus V_1 for $20V \geq V_1 \geq 0V$. (22)

(c)



(7)

(8)

(7)