



KTU NOTES APP



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Oscillators

circuit which generates oscillations without giving any output.

Positive feedback is applying here.

An amplifier and feedback circuit is used in circuits.

Types of oscillators:

① Sinusoidal or harmonic \rightarrow produces sine wave as output

② Non-sinusoidal or relaxation \rightarrow other waves as output

① RC oscillator \rightarrow eg: RC phase shift oscillator

\downarrow works in low freq or audio freq regions

② LC oscillator \rightarrow High frequency oscillator & in feedback circuit capacitor or Inductance is used.

③ Crystal oscillator \rightarrow (quartz made of crystal) is used to produce oscillations.
[Made up of piezoelectric material]

It is most common used oscillator as it is stable and frequency of operation is high.

7) -ve resistance

- oscillator used ~~for~~ as tunnel diode

Factors affecting frequency stability

① Operating point or Q-point:

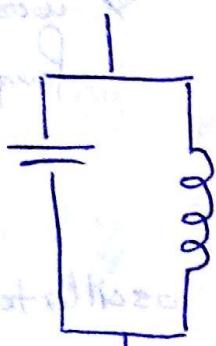
② circuit component

③ Supply voltage

④ % load

⑤ Inter element or stray capacitance

Tank circuit



Both capacitor & inductive

are passive.

charge P_s

stored as electric field

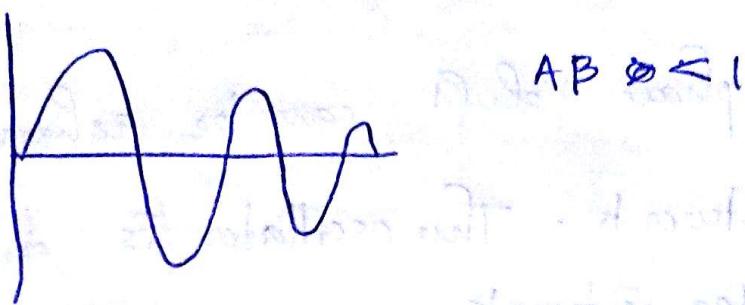
charge I_s

stored as magnetic field

amplifier P_s used to sustain the oscillation

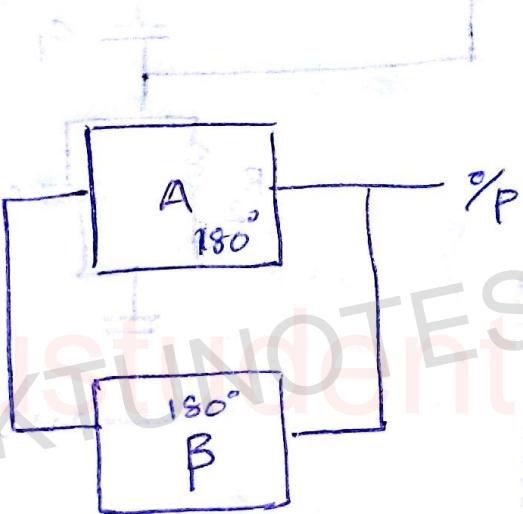
so an amplifier is needed for oscillation.

Nominal damped wave form of tank circuit



$$AB \phi < 1$$

In order to prevent this damping we use amplifiers in oscillator



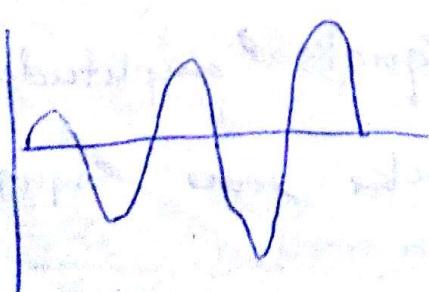
* Barkhausen condition for sustained oscillation:

① $AB = 1$ we get constant wave form

(condtn for sustained waveform)

② total phase shift circuit is either 360° or 0° .

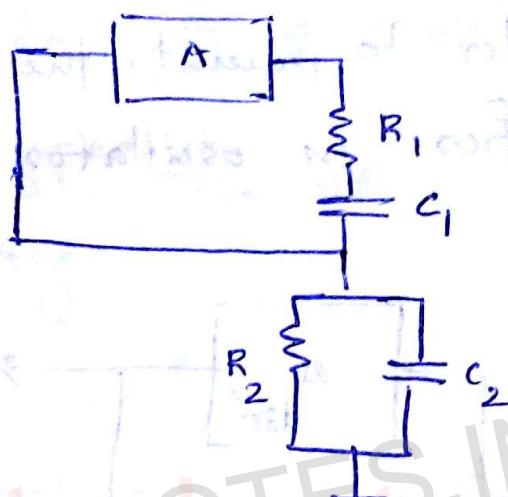
$$AB > 1$$



we will not get sustained oscillation over damp.

Wein bridge oscillator

Any phase shift can be achieved by using RC network. This oscillator is a combination lead & lag network.



→ This circuit
is both lead
and lag
phase shift.



This is lead

network
phase shift leads

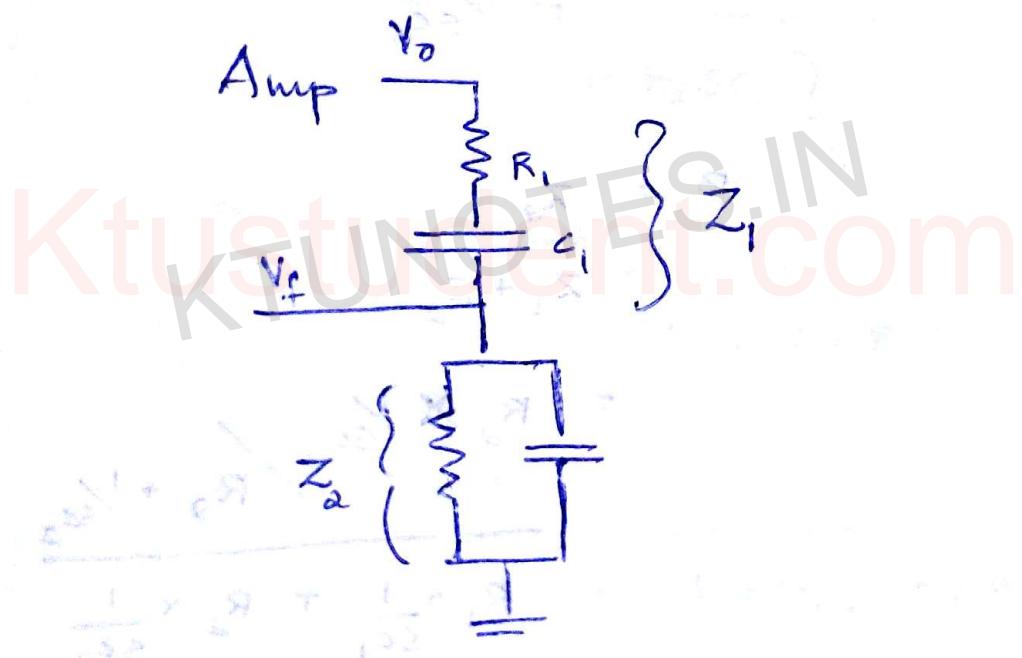
This is a lag
network

phase shift lags

low frequency signals & amplitude reduce becz
of C_1 as it blocks some signal & high

frequency equal's amplitude decreases b/c
of capacitor C_2 as it has low impedance
some current flows through C_2 and get
grounded

feedback components determine the frequency
of V_F signal.



$$\beta = \frac{V_F}{V_o}$$

$$\therefore V_F = \frac{V_o}{\beta} \times Z_d$$

$$\therefore \beta = \frac{Z_d}{Z_1 + Z_2}$$

from above by substitution

Hartley oscillator

$$f = \frac{1}{2\pi \sqrt{c(L_1 + L_2)}}$$

h_{FE} - gain

Real part = 0

$$-\omega^2 (L_2 + M) \left[(1 + h_{FE}) (L_1 + M) - \frac{1}{\omega^2 c} \right] = 0$$

$$(1 + h_{FE}) (L_1 + M) - \frac{1}{\omega^2 c} = 0$$

$$\frac{1}{\omega^2 c} = L_1 + L_2 + 2M$$

$$(1 + h_{FE}) (L_1 + M) - \frac{L_1 + L_2 + 2M}{L_1 + L_2 + 2M} = 0$$

~~$$h_{FE} L_1 + M + L_1 h_{FE} + M h_{FE} - L_1 \cancel{+} L_2 \cancel{+} 2M = 0$$~~

$$- 2M h_{FE} (L_1 + M) \cancel{+} L_2 = 0$$

$$\text{gain (A)} = \frac{h_{FE}}{1 + M} = \frac{M + L_2}{L_1 + M}$$

we know

$$A\beta = 1$$

$$\therefore \beta = \frac{1}{A} = \boxed{\frac{L_1 + M}{L_2 + M}}$$

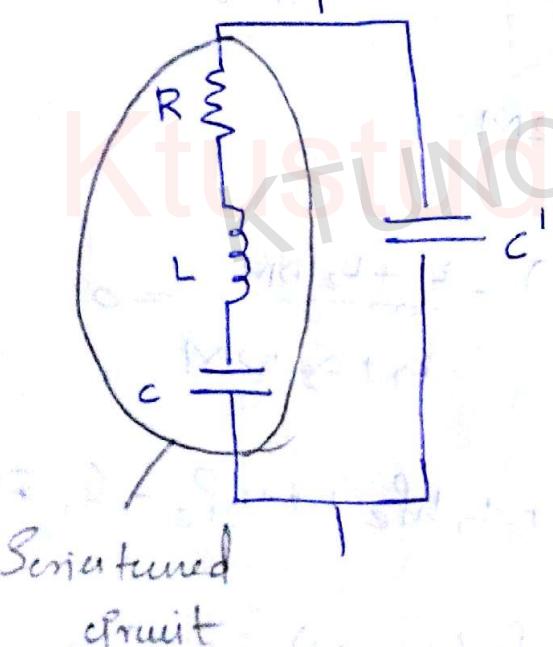
Crystal oscillator

Quality factor

$$Q\text{-factor} = \frac{LW}{R}$$

Q-factor of crystal oscillator is very high.

feedback element is piezoelectric crystal (Quartz)



when voltage applies, a mechanical deformation occurs.

C_1 is mounting capacitance or capacitance of entire crystal

for a crystal oscillator, there are:

- series tuned frequency
- parallel tuned frequency

ω_s and f_{p_s} are angular frequency and series frequency

$$f_s \text{ (series resonance frequency)} = \frac{1}{2\pi\sqrt{LC}}$$

$$f_p = \frac{1}{2\pi\sqrt{LC}}$$

$$\times C_{\text{equi}} = \frac{C_1}{C + C_1}$$

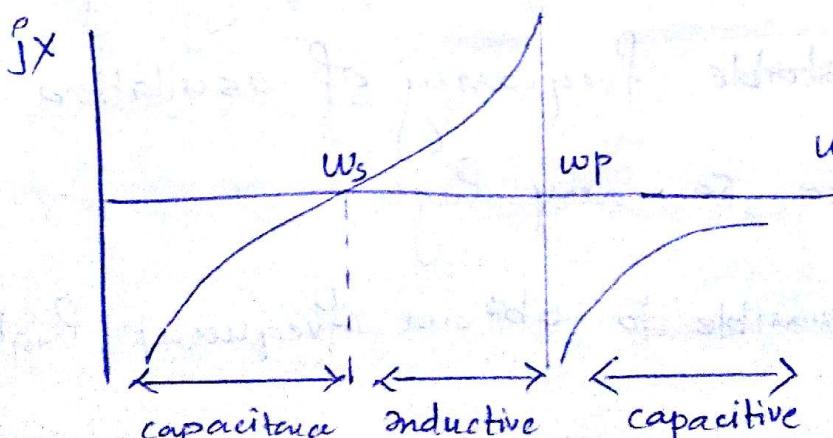
$$\text{Net impedance } jX = \left(j\omega L + \frac{1}{j\omega C} \right) \parallel \frac{1}{j\omega C}$$

$$= \left(j\omega L + \frac{1}{j\omega C} \right) \frac{1}{j\omega C}$$

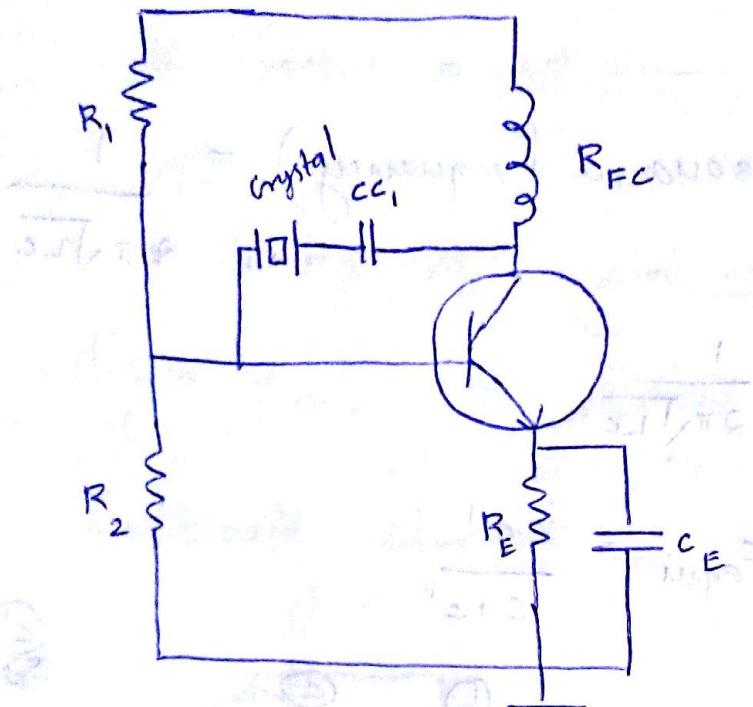
$$j\omega L + \frac{1}{j\omega C} + \frac{1}{j\omega C}$$

on simplifying:

$$= \frac{-j}{\omega C} \left(\frac{\omega^2 - \omega_s^2}{\omega^2 - \omega_p^2} \right)$$



Circuit



Advantage

Very high frequency stability

Very low frequency drift due to change in temp & other parameters

It is possible to obtain very high precise and stable frequency of oscillations

Q-factor is very high

It is possible to obtain frequency higher than

fundamental frequency by operating crystal
in overtone mode.

Drawbacks

- ⇒ They are suitable only for high frequency applications
- ⇒ Crystals of low fundamental frequencies are not easily available.

Applications

As a crystal clock in microprocessors.

In the frequency synthesis

In the radio and TV transmitters

In special type of vacuums

Advantages of Hartley oscillators

Easy to tune

Can operate a wide frequency range

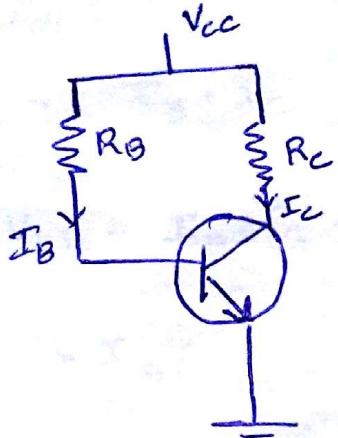
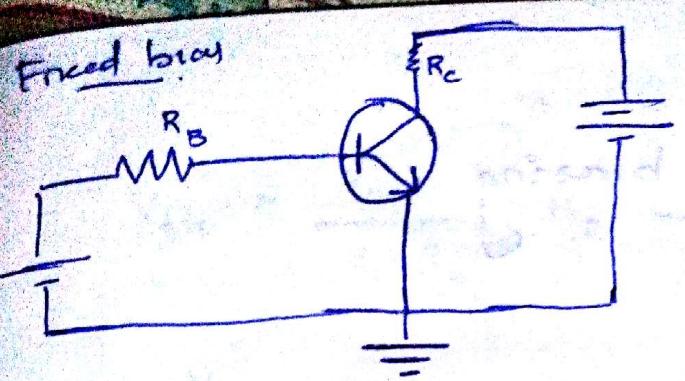
Easy to change freq. by a variable capacitor

Applications of Hartley

- ⇒ Used as Local oscillator in radio & TV receivers
- ⇒ In functional generator
- ⇒ In radio frequency sources

Disadvantages of Hartley Oscillator

Poor frequency stability



Consider the input loop:

$$V_{CC} = I_B R_B + V_{BE}$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$

$$I_C = \beta I_B$$

$$\frac{\beta V_{CC}}{R_B}$$

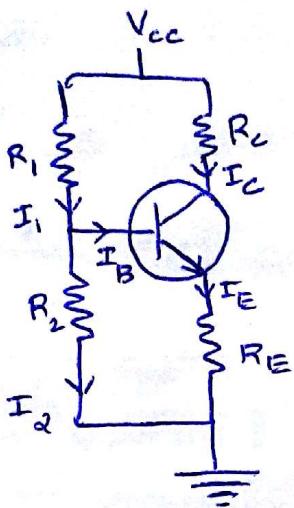
$$V_{CC} = I_C R_C + V_{CE}$$

$$V_{CE} = V_{CC} - I_C R_C$$

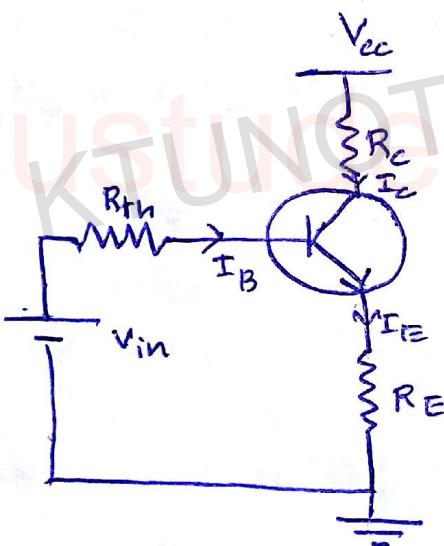
$$S = \frac{\beta + 1}{1}$$

$$S = \underline{\underline{\beta + 1}}$$

Voltage divider biasing



Using Thevenin's theorem



R_{th} - equivalent ip resistance of voltage divider circuit

V_{th} - equivalent ip voltage to the base.

$$V_{th} = \frac{V_{cc}}{R_1 + R_2} \times R_2$$

$$V_{th} = I_B R_{th} + V_{BE} + I_E R_E$$

$$I_E = I_B + I_C$$

$$\therefore V_{th} = I_B R_{th} + V_{BE} + I_B R_E + I_C R_E$$

$$= I_B (R_{th} + R_E) + V_{BE} + I_C R_E$$

$$I_B = \frac{V_{th} - V_{BE} - I_C R_E}{R_{th} + R_E}$$

constant

$$\frac{dI_B}{dI_C} = 0 - \frac{d}{dI_C} \left(\frac{I_C R_E}{R_{th} + R_E} \right)$$

$$= \frac{-R_E}{R_{th} + R_E}$$

$$s = \frac{\beta + 1}{1 + \beta R_E}$$

$$= \frac{R_{th} + R_E}{R_{th} + R_E}$$

The operating point

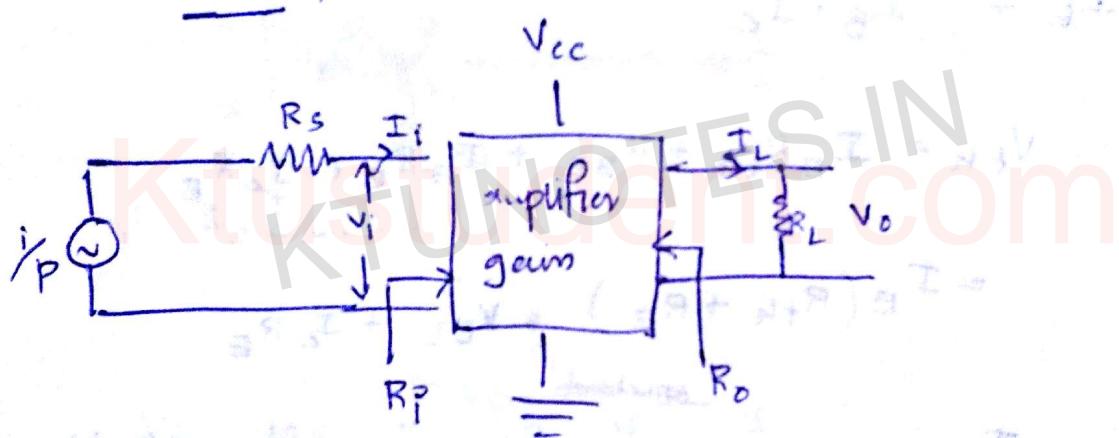
$$V_E = V_B - V_{BE}$$

$$I_E = \frac{V_B - V_{BE}}{R_E} \approx I_C$$

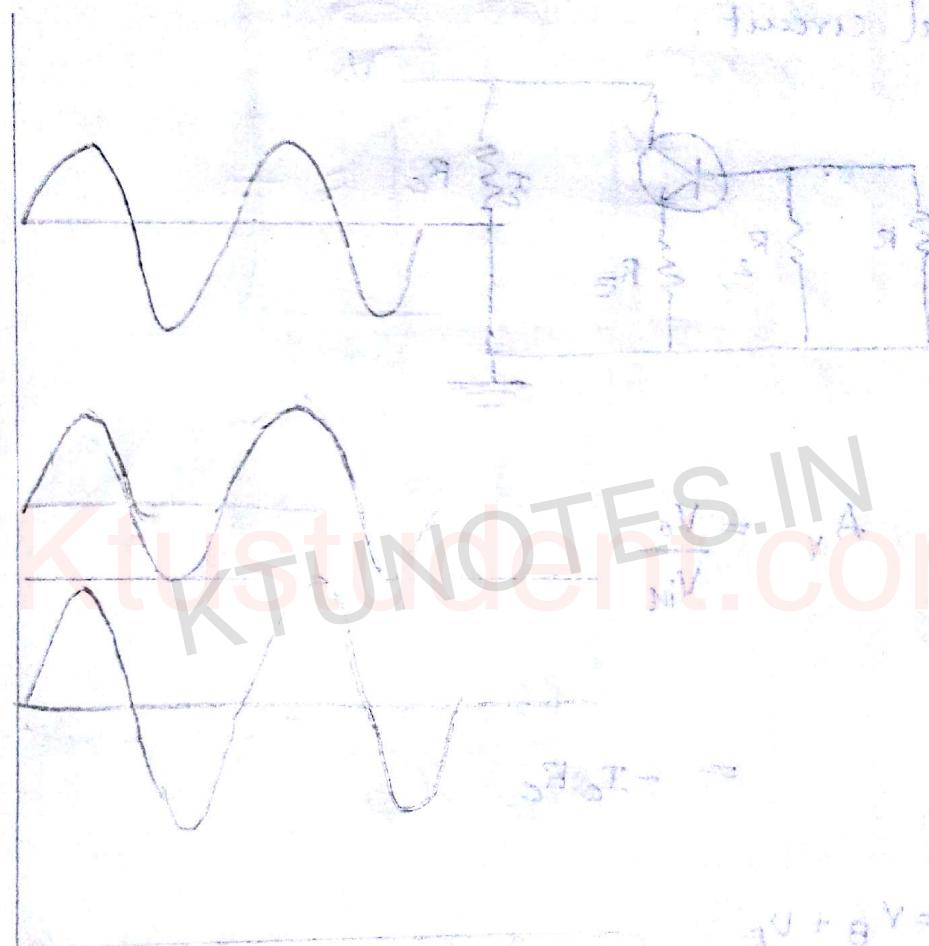
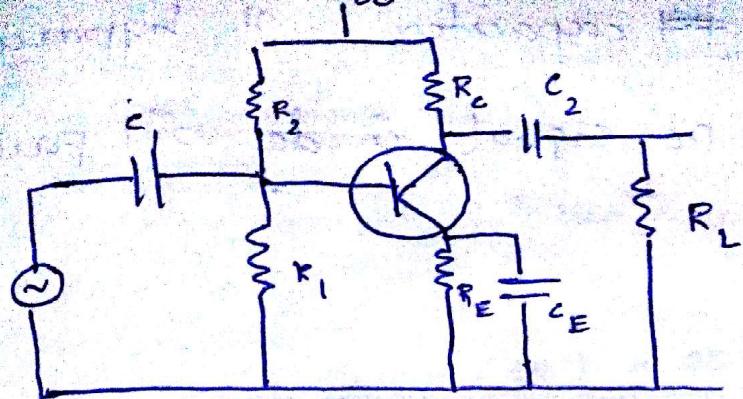
$$V_{CC} = I_C R_C + V_{CE} + I_E R_E$$

$$V_{CE} = V_{CC} - I_C R_C - I_E R_E$$

BJT amplifier

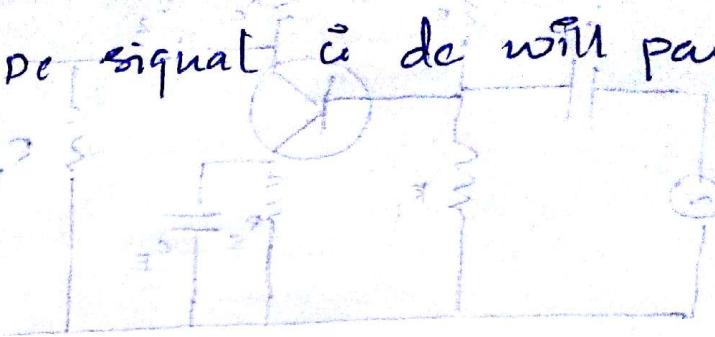


V_{CC} - amplification biasing



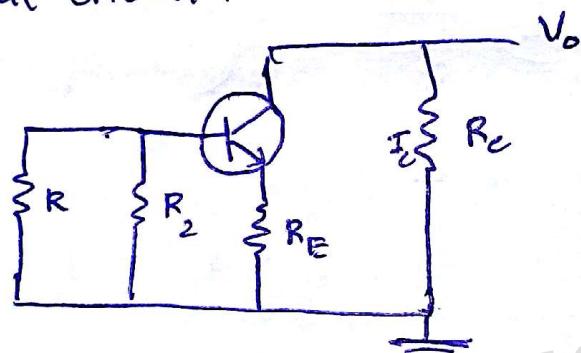
C_1 or C_2 are coupling capacitors. This will block DC components. C_1 blocks DC components from the AC signal.

C_E is bypassed capacitor. It bypasses ac signal because dc will pass through R_E .



$$V_{R1} = V_{BE} + V_{RE}$$

internal circuit:



$$A_V = \frac{V_o}{V_{in}}$$

$$= -I_C R_C$$

$$V_{in} = V_B + V_E$$

$$= I_C r_e' + I_E R_E$$

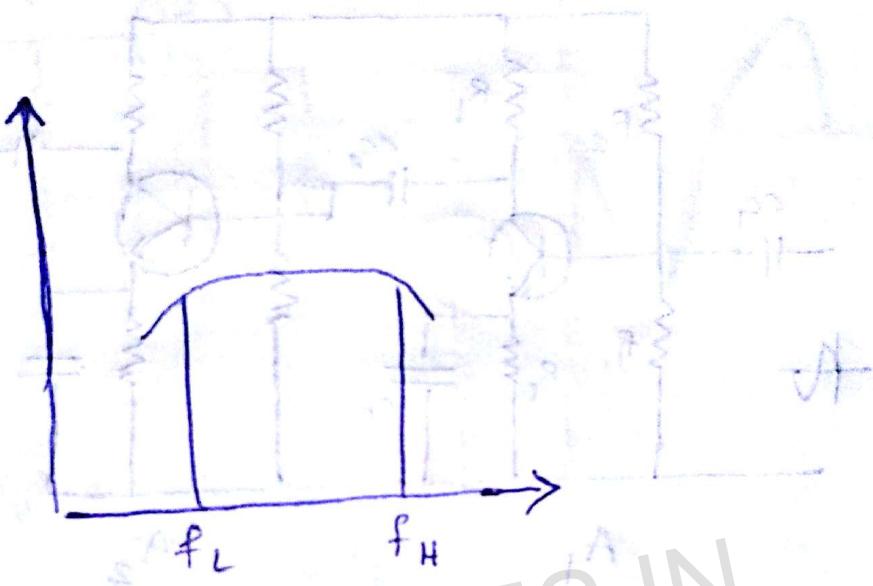
$$I_E = I_B + I_C$$

$$A_V = \frac{V_o}{V_{in}} = \frac{-I_C R_C}{I_C (R_E + r_e')}$$

$$\frac{R_C}{R_E + R_C} \quad \left(\frac{V_C^L = 25mV}{I_C} \right)$$

$$= \frac{R_C}{r_{in}} \quad (\text{no bypass capacitor})$$

$$\text{gain (dB)} = 20 \log \frac{V_o}{V_{in}}$$



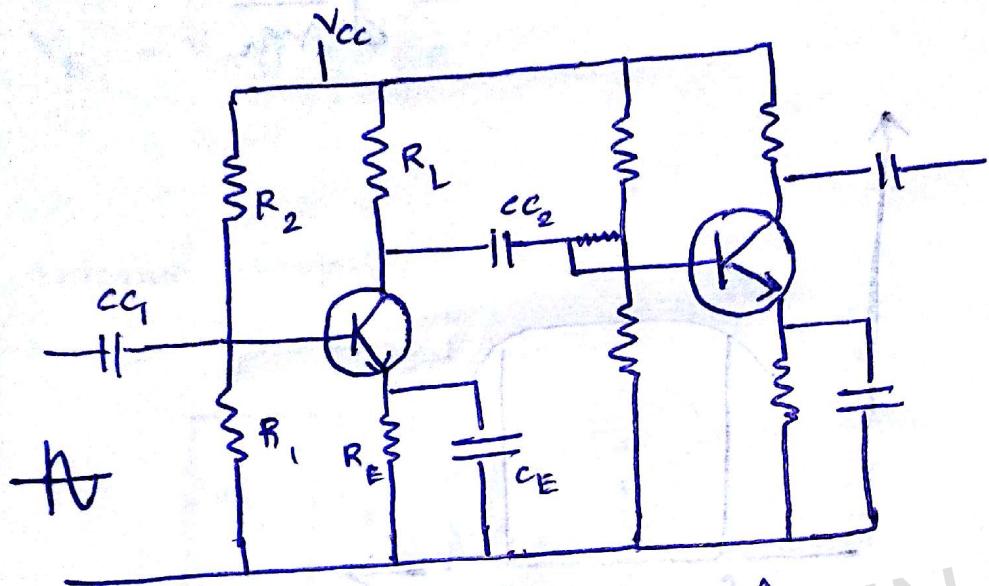
$$A_v(\text{low}) = \frac{A_v(\text{mid})}{\sqrt{1 + (f_L/f)^2}}$$

$$A_v(\text{high}) = \frac{A_v(\text{mid})}{\sqrt{1 + (f/f_H)^2}}$$

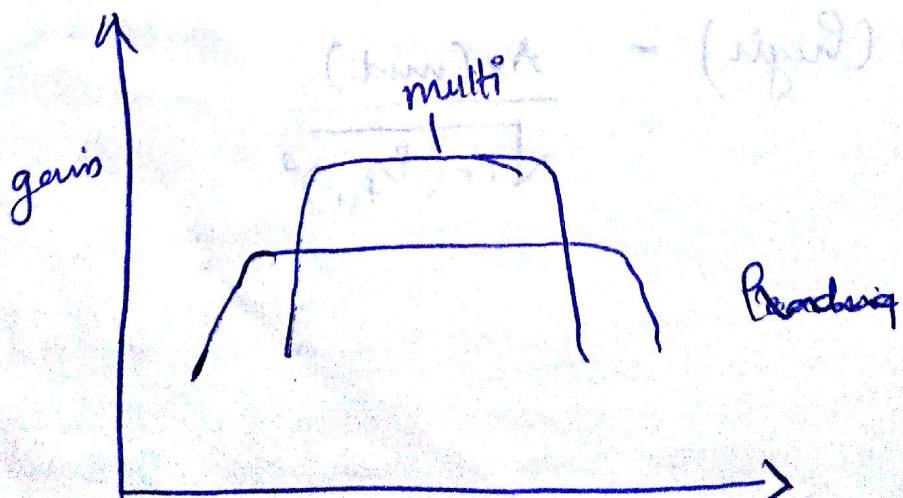
Multistage Amplifier

1. Cascade amplifier CE, CE

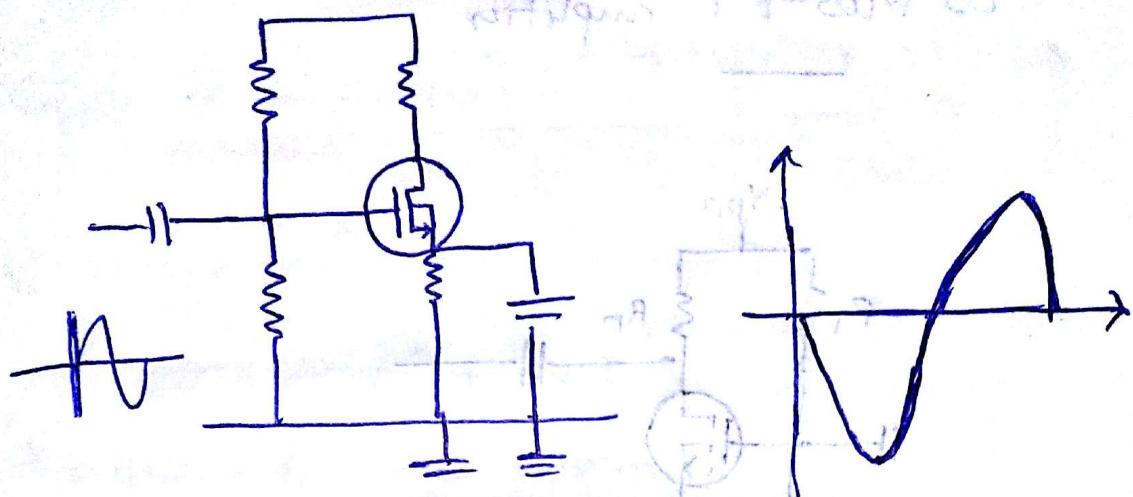
2. cascade CE, CB



- 1) RC coupling
- 2) transformer
- 3) Direct



common Source MOSFET (with R_s)



$$A_V = \frac{-g_m R_D}{1 + g_m R_s}$$

$$= -\frac{g_m R_D}{g_m R_s}$$

$$\approx -R_D / R_s$$

r/p Impedance $\approx R_1 // R_2$

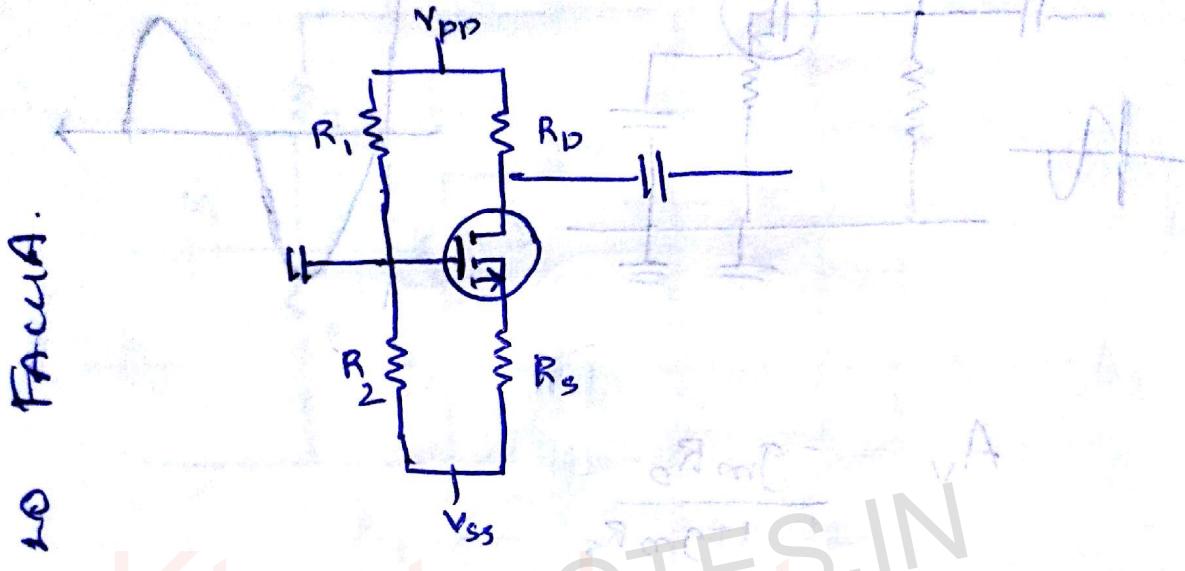
% P Impedance $\approx R_D // R_s$

$$A_V = -g_m (\tau_o / R_o)$$

$$1/p \text{ Impedance} = R_1 // R_2$$

$$O/P \text{ impedance} = \frac{r_o}{1 + A_{vD}} // R_D$$

CS MOSFET amplifier



Feedback IC circuits

- \Rightarrow Amplifier gain is unstable due to change in the supply voltage
- \Rightarrow Change in the parameter of active base
- \Rightarrow Ageing
- \Rightarrow r_o Due to rise in leakage current

Positive feed back

v_p & $\%_p$ are in same phase

Types of amplifiers

① voltage amplifier:

② current amplifier:

③ transconductance amplifier:

④ transresistance amplifier:

⑤ Voltage amplifier:

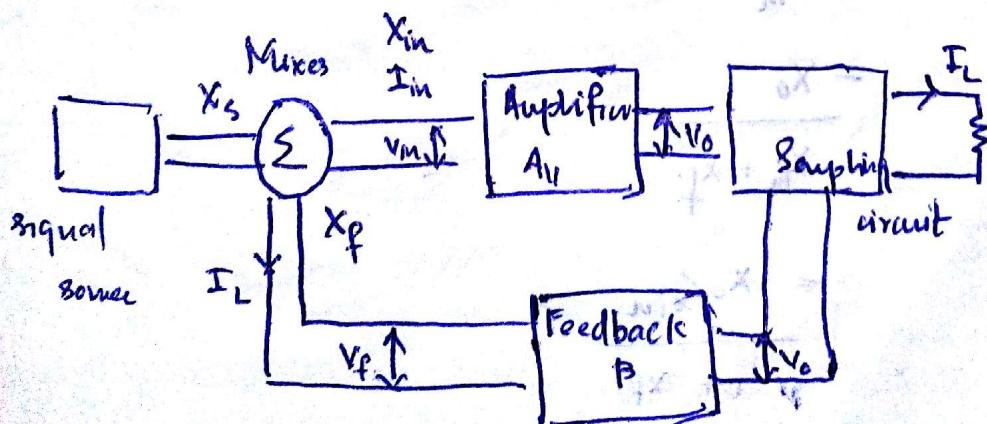
⑥ current amplifier:

⑦ transconductance amplifier:

⑧ transresistance amplifier:

| $\frac{v_p}{v_s}$ | $\frac{\%_p}{v_s}$ | R_{in} | R_{out} | transfer fun |
|-------------------|--------------------|----------|-----------|-------------------------|
| V | I | ∞ | 0 | $A_V = \frac{V_o}{V_s}$ |
| I | I | 0 | ∞ | $A_I = \frac{I_L}{I_s}$ |
| Y | I | ∞ | ∞ | $G_m = \frac{I_L}{V_s}$ |
| I | V | 0 | 0 | $R_m = \frac{V_o}{I_s}$ |

Feedback block



$$X_m = X_s - X_f$$

$$X_s = X_{in} + X_f$$

Gain Stability : Reduced nonlinear distortion

Reduced by $\frac{1}{1+AB}$

Reduced Noise by a factor $\frac{1}{1+AB}$

Increased bandwidth by $\sqrt{1+AB}$

Increased ω_p impedance by a factor $1+AB$

Reduced ω_p impedance by a factor $\frac{1}{1+AB}$

Reduced gains by a factor $\frac{1}{1+AB}$

Negative feedback

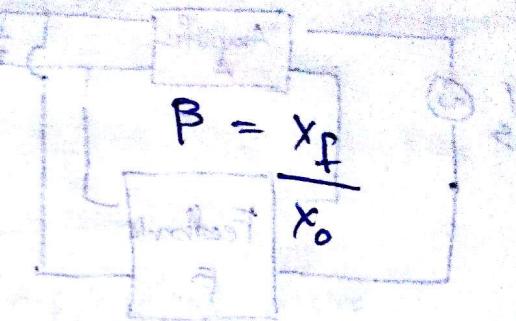
$$A = \frac{X_o}{X_{in}}$$

$$= \frac{X_o}{X_{in} + X_f}$$

$$= \frac{\frac{X_o}{X_{in}}}{1 + \frac{X_f}{X_{in}}}$$

$$A_f = \frac{A}{1 + \frac{X_f}{X_o} \cdot \frac{X_o}{X_{in}}}$$

$$= \frac{A}{1 + AB}$$



Positive feedback

$$A_f = \frac{A}{1 - AB}$$

4 types of feedback amplifier

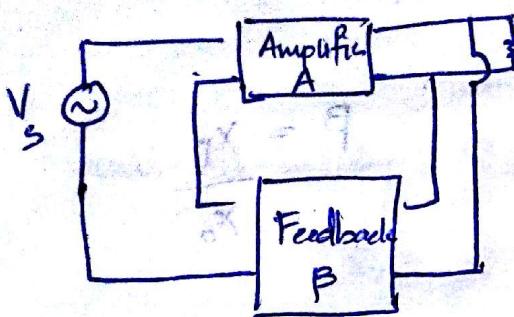
Voltage -series feedback amplifier

Voltage shunt n

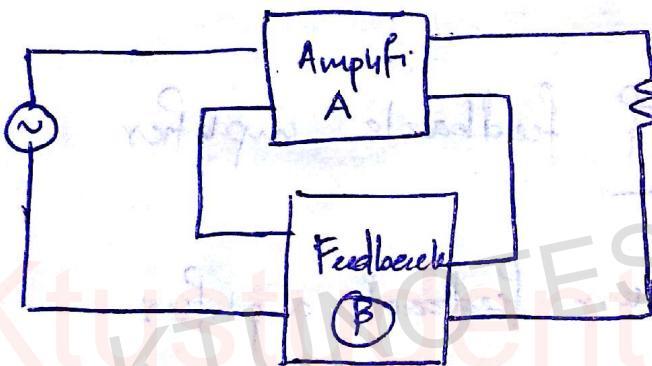
Current series n

current shunt n

Voltage Source



current source



amplifier

e.g. CE amplifier without bypass capacitor

%P IP gain A feedback B

Voltage gain

V

V

$$A_v = \frac{V_o}{V_{in}}$$

$$B = \frac{V_f}{V_{out}}$$

Voltage shunt

V

I

$$R_{in} = \frac{V_{out}}{I_{in}}$$

$$\frac{I_f}{V_{out}}$$

current series
gain

I

V

$$g_{ms} = \frac{I_{out}}{V_{in}}$$

$$\frac{V_f}{I_{out}}$$

current shunt

I

I

$$A_i = \frac{I_{out}}{I_{in}}$$

$$\frac{I_f}{I_{out}}$$