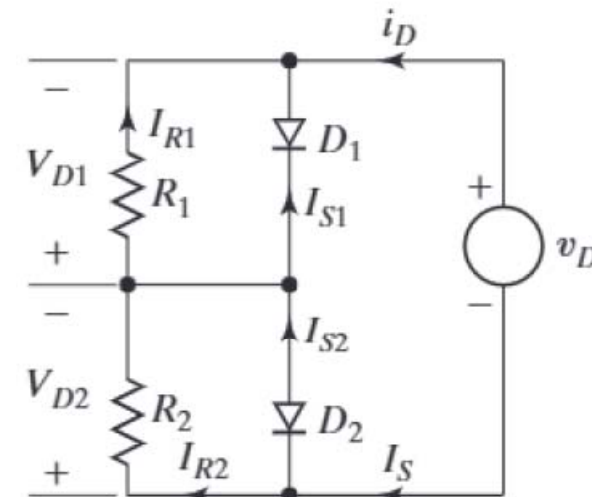


Series-connected diodes

Example 2.3 Finding the Voltage-Sharing Resistors

Two diodes are connected in series, as shown in Figure 2.11a, to share a total dc reverse voltage of $V_D = 5\text{ kV}$. The reverse leakage currents of the two diodes are $I_{S1} = 30\text{ mA}$ and $I_{S2} = 35\text{ mA}$.
(a) Find the diode voltages if the voltage-sharing resistances are equal, $R_1 = R_2 = R = 100\text{ k}\Omega$.
(b) Find the voltage-sharing resistances R_1 and R_2 if the diode voltages are equal, $V_{D1} = V_{D2} = V_D/2$.



(a) Circuit diagram

Series-connected diodes

Example 2.3 Finding the Voltage-Sharing Resistors

Two diodes are connected in series, as shown in Figure 2.11a, to share a total dc reverse voltage of $V_D = 5\text{ kV}$. The reverse leakage currents of the two diodes are $I_{S1} = 30\text{ mA}$ and $I_{S2} = 35\text{ mA}$.

(a) Find the diode voltages if the voltage-sharing resistances are equal, $R_1 = R_2 = R = 100\text{ k}\Omega$.

(b) Find the voltage-sharing resistances R_1 and R_2 if the diode voltages are equal, $V_{D1} = V_{D2} = V_D/2$.

Solution

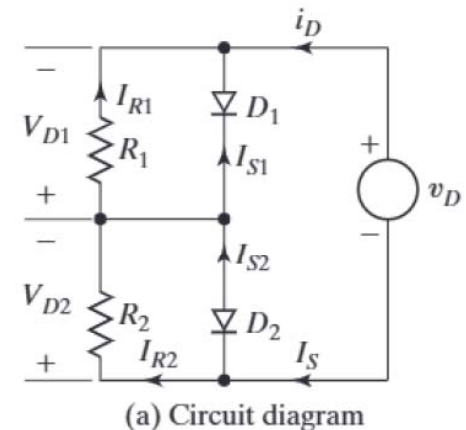
- a. $I_{S1} = 30\text{ mA}$, $I_{S2} = 35\text{ mA}$, and $R_1 = R_2 = R = 100\text{ k}\Omega$. $-V_D = -V_{D1} - V_{D2}$ or $V_{D2} = V_D - V_{D1}$. From Eq. (2.14),

$$I_{S1} + \frac{V_{D1}}{R} = I_{S2} + \frac{V_{D2}}{R}$$

Substituting $V_{D2} = V_D - V_{D1}$ and solving for the diode voltage D_1 , we get

$$\begin{aligned} V_{D1} &= \frac{V_D}{2} + \frac{R}{2} (I_{S2} - I_{S1}) \\ &= \frac{5\text{ kV}}{2} + \frac{100\text{ k}\Omega}{2} (35 \times 10^{-3} - 30 \times 10^{-3}) = 2750\text{ V} \end{aligned} \quad (2.16)$$

and $V_{D2} = V_D - V_{D1} = 5\text{ kV} - 2750 = 2250\text{ V}$.



Series-connected diodes

- b. $I_{S1} = 30\text{mA}$, $I_{S2} = 35\text{mA}$, and $V_{D1} = V_{D2} = V_D/2 = 2.5\text{kV}$. From Eq. (2.13),

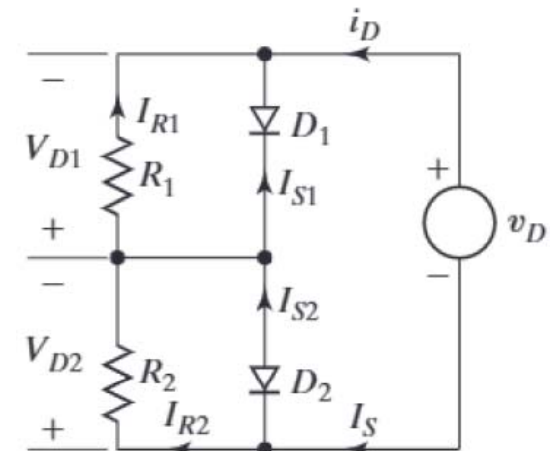
$$I_{S1} + \frac{V_{D1}}{R_1} = I_{S2} + \frac{V_{D2}}{R_2}$$

which gives the resistance R_2 for a known value of R_1 as

$$R_2 = \frac{V_{D2}R_1}{V_{D1} - R_1(I_{S2} - I_{S1})} \quad (2.17)$$

Assuming that $R_1 = 100\text{k}\Omega$, we get

$$R_2 = \frac{2.5\text{kV} \times 100\text{k}\Omega}{2.5\text{kV} - 100\text{k}\Omega \times (35 \times 10^{-3} - 30 \times 10^{-3})} = 125\text{k}\Omega$$

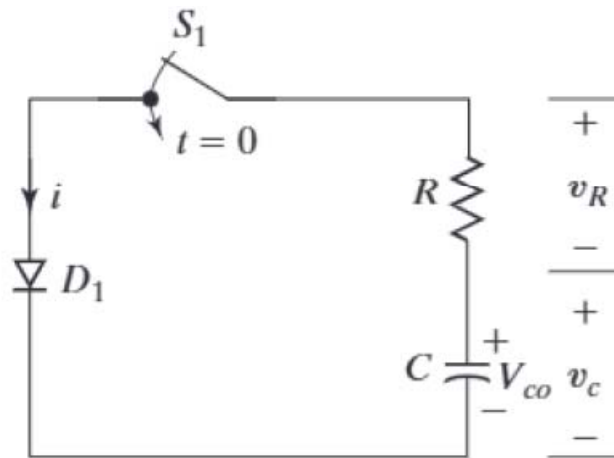


(a) Circuit diagram

Diode switched RL circuit

Example 2.4 Finding the Peak Current and Energy Loss in an RC Circuit

A diode circuit is shown in Figure 2.16a with $R = 44\ \Omega$ and $C = 0.1\ \mu\text{F}$. The capacitor has an initial voltage, $V_{c0} = V_c(t = 0) = 220\text{ V}$. If switch S_1 is closed at $t = 0$, determine (a) the peak diode current, (b) the energy dissipated in the resistor R , and (c) the capacitor voltage at $t = 2\ \mu\text{s}$.



(a) Circuit diagram

FIGURE 2.16

Diode circuit with an RC load.

Diode switched RC circuit

Solution

The waveforms are shown in Figure 2.16b.

- a. Equation (2.20) can be used with $V_s = V_{c0}$ and the peak diode current I_p is

$$I_p = \frac{V_{c0}}{R} = \frac{220}{44} = 5 \text{ A}$$

- b. The energy W dissipated is

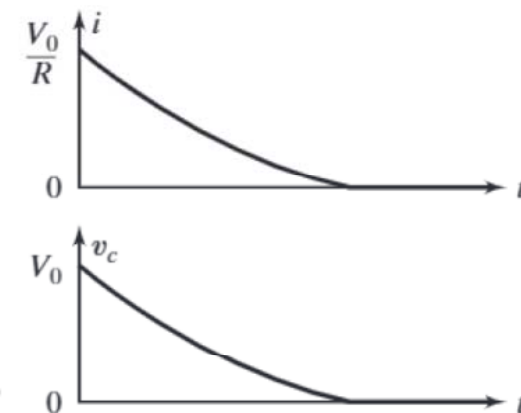
$$W = 0.5CV_{c0}^2 = 0.5 \times 0.1 \times 10^{-6} \times 220^2 = 0.00242 \text{ J} = 2.42 \text{ mJ}$$

- c. For $RC = 44 \times 0.1 \mu = 4.4 \mu\text{s}$ and $t = t_1 = 2 \mu\text{s}$, the capacitor voltage is

$$v_c(t = 2 \mu\text{s}) = V_{c0}e^{-t/RC} = 220 \times e^{-2/4.4} = 139.64 \text{ V}$$

FIGURE 2.16

Diode circuit with an RC load.



(b) Waveforms

Diode switched RL circuit

Example 2.5 Finding the Steady-State Current and the Energy Stored in an Inductor

A diode RL circuit is shown in Figure 2.17a with $V_s = 220\text{ V}$, $R = 4\Omega$, and $L = 5\text{ mH}$. The inductor has no initial current. If switch S_1 is closed at $t = 0$, determine (a) the steady-state diode current, (b) the energy stored in the inductor L , and (c) the initial di/dt .

(d) find the inductor current at $t = 1\text{ ms}$

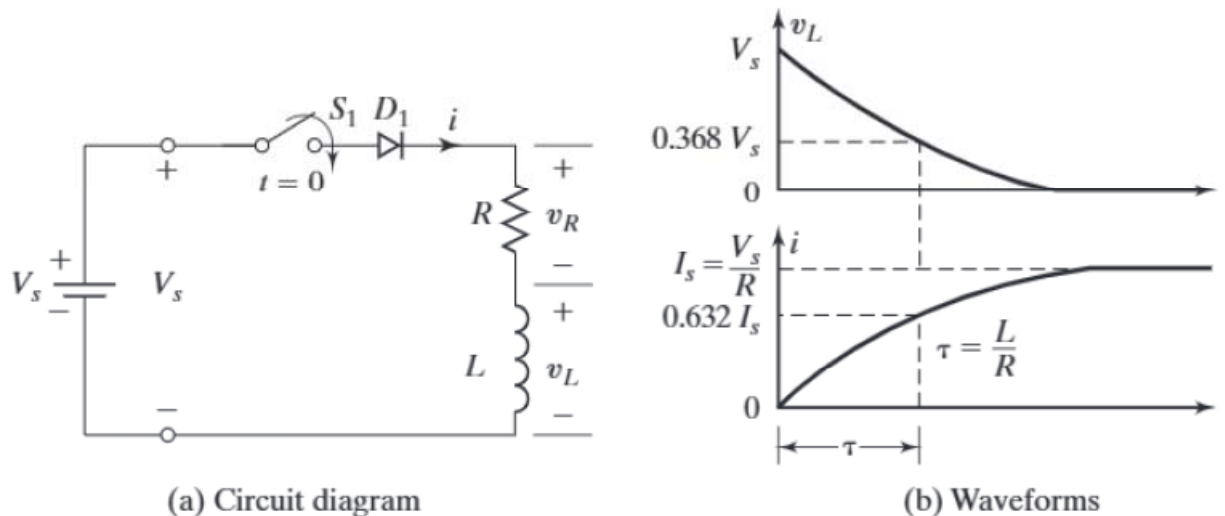


FIGURE 2.17

Diode circuit with an RL load.

Diode switched RL circuit

Solution

The waveforms are shown in Figure 2.17b.

- a. Eq. (2.25) can be used with $t = \infty$ and the steady-state peak diode current is

$$I_p = \frac{V_s}{R} = \frac{220}{4} = 55 \text{ A}$$

- b. The energy stored in the inductor in the steady state at a time t tending ∞

$$W = 0.5 L I_p^2 = 0.5 \times 5 \times 10^{-3} 55^2 = 7.563 \text{ mJ}$$

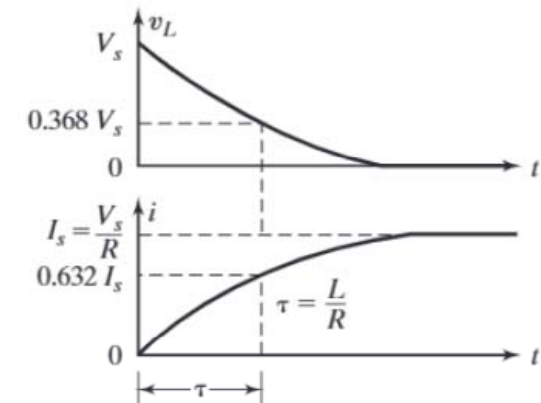
- c. Eq. (2.26) can be used to find the initial di/dt as

$$\frac{di}{dt} = \frac{V_s}{L} = \frac{220}{5 \times 10^{-3}} = 44 \text{ A/ms}$$

- d. For $L/R = 5 \text{ mH}/4 = 1.25 \text{ ms}$, and $t = t_1 = 1 \text{ ms}$, Eq. (2.25) gives the inductor current as

$$i(t = 1 \text{ ms}) = \frac{V_s}{R} (1 - e^{-tR/L}) = \frac{220}{4} \times (1 - e^{-1/1.25}) = 30.287 \text{ A}$$

$$i(t) = \frac{V_s}{R} (1 - e^{-tR/L}) \quad (2.25)$$



(b) Waveforms

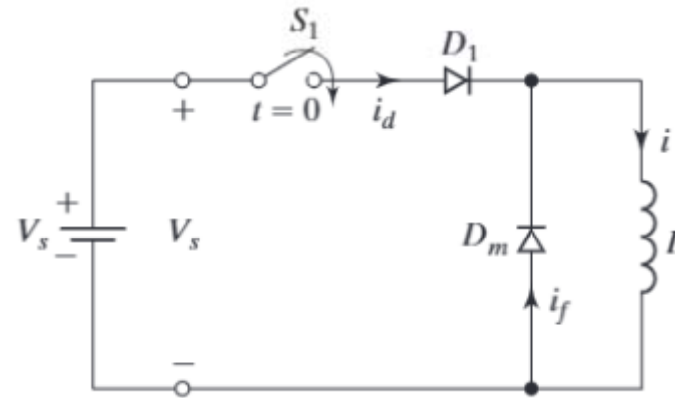
FIGURE 2.17

Diode circuit with an RL load.

Free-wheeling diode with switched RL circuit

Example 2.8 Finding the Stored Energy in an Inductor with a Freewheeling Diode

In Figure 2.24a, the resistance is negligible ($R = 0$), the source voltage is $V_s = 220\text{ V}$ (constant time), and the load inductance is $L = 220\text{ }\mu\text{H}$. (a) Draw the waveform for the load current if the switch is closed for a time $t_1 = 100\text{ }\mu\text{s}$ and is then opened. (b) Determine the final energy stored in the load inductor.



(a) Circuit diagram

FIGURE 2.25

Diode circuit with an L load.

(b) Equivalent circuit

Free-wheeling diode with switched RL circuit

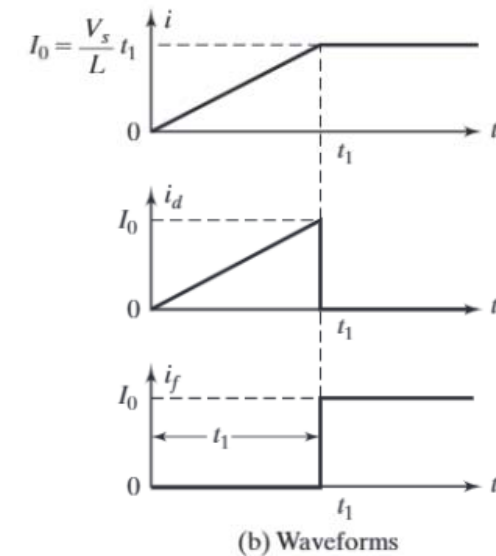
Solution

- a. The circuit diagram is shown in Figure 2.25a with a zero initial current. When the switch is closed at $t = 0$, the load current rises linearly and is expressed as

$$i(t) = \frac{V_s}{L} t$$

and at $t = t_1$, $I_0 = V_s t_1 / L = 220 \times 100 / 220 = 100 \text{ A}$.

- b. When switch S_1 is opened at a time $t = t_1$, the load current starts to flow through diode D_m . Because there is no dissipative (resistive) element in the circuit, the load current remains constant at $I_0 = 100 \text{ A}$ and the energy stored in the inductor is $0.5 L I_0^2 = 1.1 \text{ J}$. The current waveforms are shown in Figure 2.25b.



(b) Equivalent circuit

Example Problem

- 2.1** The reverse recovery time of a diode is $t_{rr} = 5\mu\text{s}$, and the rate of fall of the diode current is $di/dt = 80\text{ A}/\mu\text{s}$. If the softness factor is $\text{SF} = 0.5$, determine **(a)** the storage charge Q_{RR} , and **(b)** the peak reverse current I_{RR} .

Do it for two conditions: 1) When $t_{rr}=t_a$. 2) When $t_{rr}=t_a+t_b$

Example Problem

2.1 The reverse recovery time of a diode is $t_{rr} = 5\mu\text{s}$, and the rate of fall of the diode current is $di/dt = 80\text{ A}/\mu\text{s}$. If the softness factor is $SF = 0.5$, determine **(a)** the storage charge Q_{RR} , and **(b)** the peak reverse current I_{RR} .

Do it for two conditions: 1) When $t_{rr} = t_a$. 2) When $t_{rr} = t_a + t_b$

Solution: The ratio t_b/t_a is known as the *softness factor* (SF).

$$\text{Given: } t_{rr} = 5\mu\text{s}, \frac{di}{dt} = 80 \frac{\text{A}}{\mu\text{s}}, SF = \frac{t_b}{t_a} = 0.5$$

For Condition – 1: $t_{rr} \approx t_a$

$$\text{From } I_{rr} \text{ curve, } I_{rr} = \frac{di}{dt} \times t_a \text{ or } I_{rr} = \frac{di}{dt} \times t_{rr}$$

$$I_{rr} = 80 \frac{\text{A}}{\mu\text{s}} \times 5\mu\text{s} = 400\text{ A}$$

$$\text{From } I_{rr} \text{ curve, } Q_{rr} = \frac{1}{2} \times I_{rr} \times t_{rr} = \frac{1}{2} \times 400\text{ A} \times 5\mu\text{s}$$

$$Q_{rr} = 1000\mu\text{C}$$

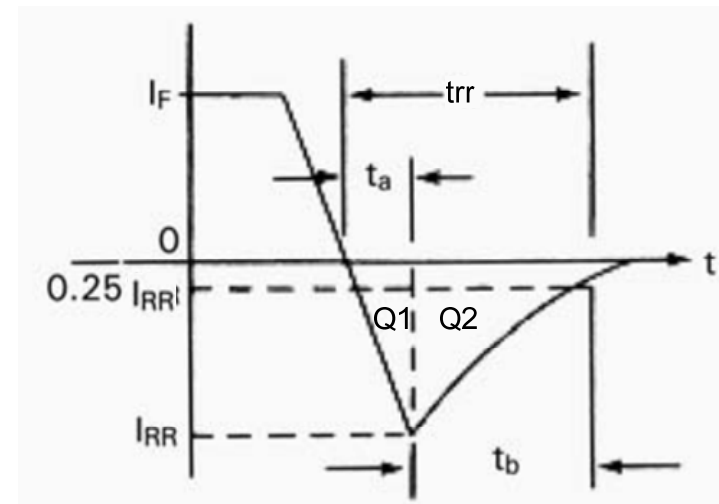


Fig. 1. Diode reverse recovery current

Example Problem

2.1 The reverse recovery time of a diode is $t_{rr} = 5\mu\text{s}$, and the rate of fall of the diode current is $di/dt = 80\text{ A}/\mu\text{s}$. If the softness factor is $SF = 0.5$, determine **(a)** the storage charge Q_{RR} , and **(b)** the peak reverse current I_{RR} .

Do it for two conditions: 1) When $t_{rr}=t_a$. 2) When $t_{rr}=t_a+t_b$

Solution:

$$\text{Given: } t_{rr} = 5\mu\text{s}, \frac{di}{dt} = 80 \frac{\text{A}}{\mu\text{s}}, SF = \frac{t_b}{t_a} = 0.5$$

$$\text{For Condition - 2: } t_{rr} = t_a + t_b = t_a + 0.5t_a = 1.5t_a$$

$$t_a = \frac{t_{rr}}{1.5} = \frac{5\mu\text{s}}{1.5} = 3.33\mu\text{s}$$

$$\text{From } I_{rr} \text{ curve, } I_{rr} = \frac{di}{dt} \times t_a$$

$$I_{rr} = 80 \frac{\text{A}}{\mu\text{s}} \times 3.33\mu\text{s} = 266.67\text{ A}$$

$$\text{From } I_{rr} \text{ curve, } Q_{rr} = \frac{1}{2} \times I_{rr} \times t_{rr} = \frac{1}{2} \times 266.67\text{ A} \times 5\mu\text{s}$$

$$Q_{rr} = 666.67\mu\text{C}$$

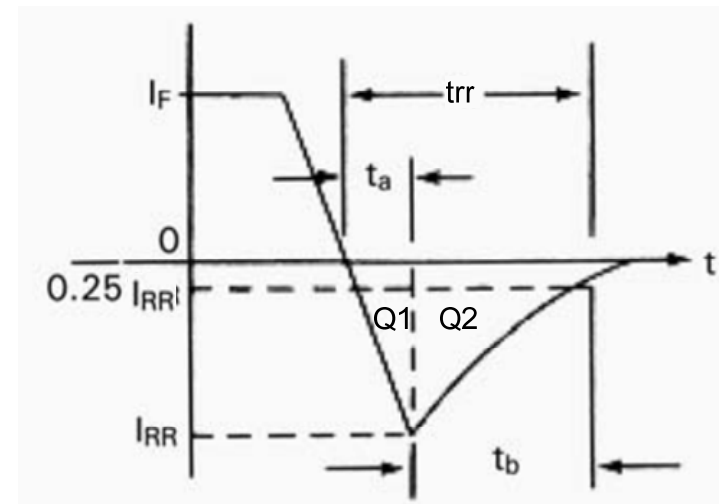


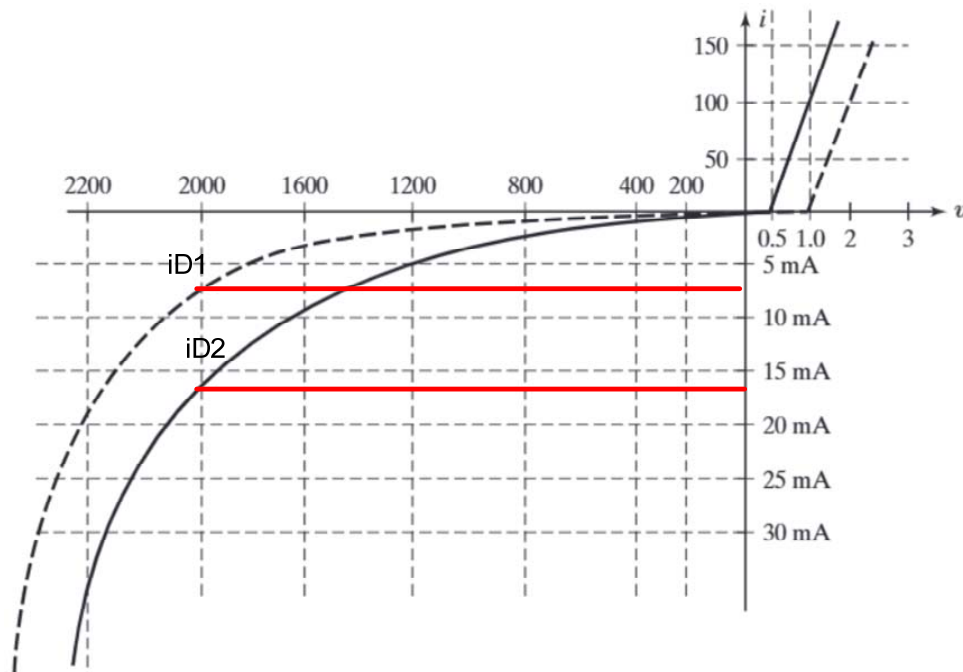
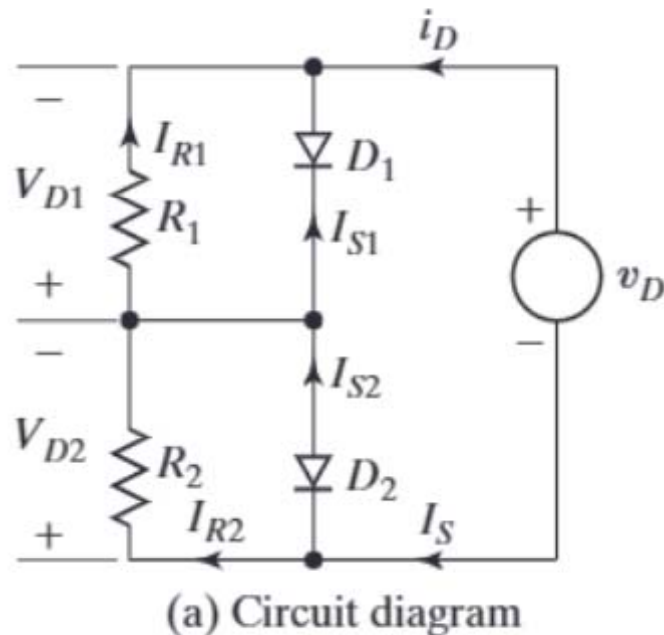
Fig. 1. Diode reverse recovery current

Example Problem

- 2.2** The storage charge and the peak reverse current of a diode are $Q_{RR} = 10000\mu\text{C}$ and $I_{RR} = 4000$. If the softness factor is $SF = 0.5$, determine **(a)** the reverse recovery time of the diode t_{rr} , and **(b)** the rate of fall of the diode current di/dt .

Example Problem

- 2.6** Two diodes are connected in series as shown in Figure 2.11 and the voltage across each diode is maintained the same by connecting a voltage-sharing resistor, such that $V_{D1} = V_{D2} = 2000$ V and $R_1 = 100$ k Ω . The v - i characteristics of the diodes are shown in Figure P2.6. Determine the leakage currents of each diode and the resistance R_2 across diode D_2 .



Example Problem

2.6 Two diodes are connected in series as shown in Figure 2.11 and the voltage across each diode is maintained the same by connecting a voltage-sharing resistor, such that $V_{D1} = V_{D2} = 2000\text{ V}$ and $R_1 = 100\text{ k}\Omega$. The $v-i$ characteristics of the diodes are shown in Figure P2.6. Determine the leakage currents of each diode and the resistance R_2 across diode D_2 .

Solution:

Given: $V_{D1} = V_{D2} = 2000\text{ V}$, $R_1 = 100\text{ k}\Omega$

From Figure P2.6,

$I_{S1} = 7.5\text{ mA}$, $I_{S2} = 17\text{ mA}$

From Circuit:

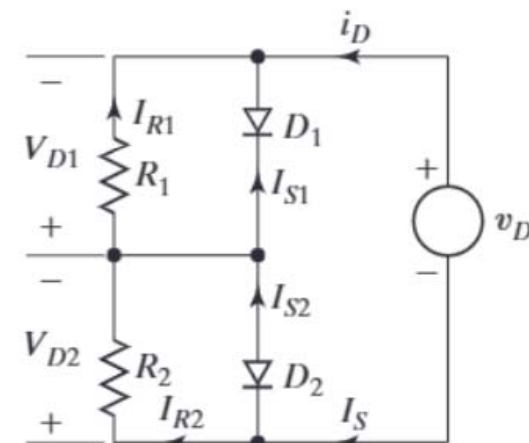
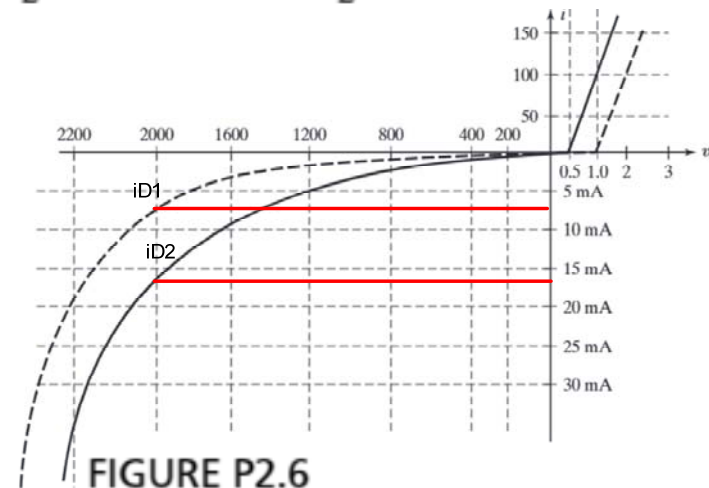
$$I_{S1} + I_{R1} = I_{S2} + I_{R2}$$

$$\text{where, } I_{R1} = \frac{V_{D1}}{R_1} = \frac{2000}{100\text{ k}} = 20\text{ mA}$$

$$7.5\text{ mA} + 20\text{ mA} = 17\text{ mA} + I_{R2}$$

$$I_{R2} = 10.5\text{ mA}$$

$\text{So, } R_2 = \frac{V_{D2}}{I_{R2}} = \frac{2000\text{ V}}{10.5\text{ mA}} = 190.4\text{ k}\Omega$



(a) Circuit diagram

Example Problem

- 2.12** Two diodes are connected in series as shown in Figure 2.11a. The resistance across the diodes is $R_1 = R_2 = 10\text{k}\Omega$. The input dc voltage is 5 kV. The leakage currents are $I_{s1} = 25\text{mA}$ and $I_{s2} = 40\text{mA}$. Determine the voltage across the diodes.

Example Problem

2.12 Two diodes are connected in series as shown in Figure 2.11a. The resistance across the diodes is $R_1 = R_2 = 10\text{k}\Omega$. The input dc voltage is 5 kV. The leakage currents are $I_{S1} = 25\text{mA}$ and $I_{S2} = 40\text{mA}$. Determine the voltage across the diodes.

Solution:

$$\text{Given :}, R_1 = R_2 = 10\text{k}\Omega, V_D = 5\text{kV}$$

$$I_{S1} = 25\text{mA}, I_{S2} = 40\text{mA}$$

$$V_{D2} = V_D - V_{D1} = 5\text{kV} - V_{D1} \quad (i)$$

$$I_{S1} + \frac{V_{D1}}{R_1} = I_{S2} + \frac{V_{D2}}{R_2} \quad (ii)$$

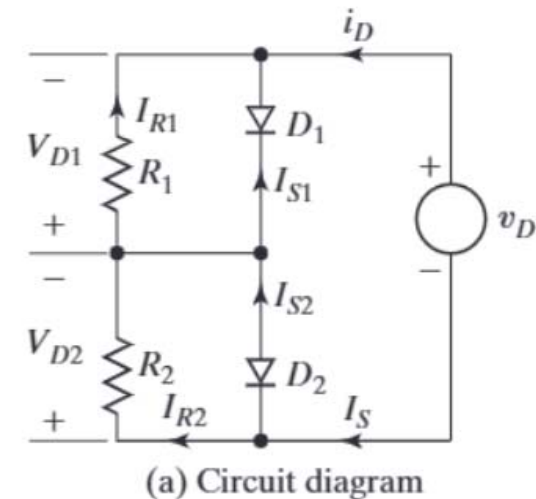
Putting (i) into (ii) and solving, we get

$$V_{D1} = \frac{V_D}{2} + \frac{R}{2}(I_{S2} - I_{S1})$$

$$V_{D1} = \frac{5000}{2} + \frac{10000}{2}(40\text{mA} - 25\text{mA})$$

$$V_{D1} = 2575\text{V}$$

$$V_{D2} = 5000\text{V} - 2575\text{V} = 2425\text{V}$$



Example Problem

- 2.15** The current waveform of a diode is shown in Figure P2.15. Determine the average, root mean square (rms), and peak current ratings of the diode. Assume $I_p = 500\text{ A}$ of a half sine-wave.

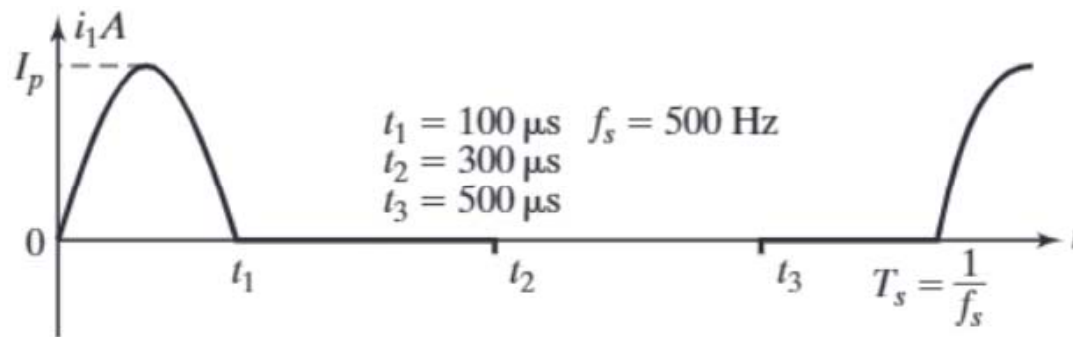


FIGURE P2.15

Example Problem

2.15 The current waveform of a diode is shown in Figure P2.15. Determine the average, root mean square (rms), and peak current ratings of the diode. Assume $I_p = 500\text{ A}$ of a half sine-wave.

Solution:

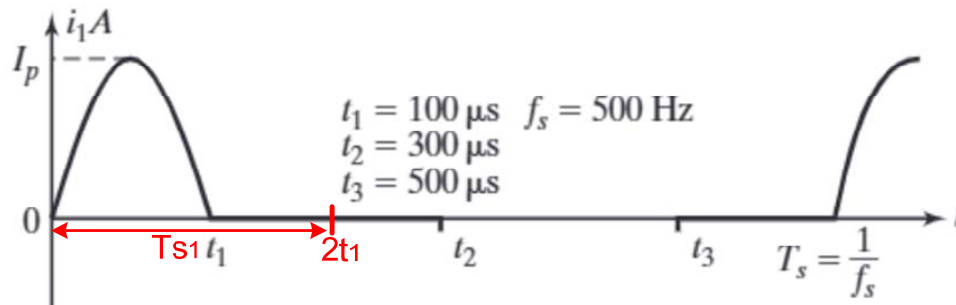


FIGURE P2.15

Given: $t_1 = 100\mu\text{s}$, $I_p = 500\text{ A}$, $f_s = 500\text{ Hz}$

$$T_s = 1 / f_s = 20000\mu\text{s}$$

1) Average value, $I_{p,avg} = ?$

$$I_{p,avg} = \frac{1}{T_s} \int_0^{t_1} I_p \sin \omega t dt \quad \omega = \frac{2\pi}{2t_1}$$

$$I_{p,avg} = \frac{I_p}{T_s} \frac{-\cos \omega t}{\omega} \Big|_0^{t_1} = \frac{I_p}{T_s} \frac{-\cos \frac{2\pi}{2t_1} t}{\frac{2\pi}{2t_1}} \Big|_0^{t_1}$$

$$I_{p,avg} = \frac{I_p t_1}{\pi T_s} \left[-\cos \pi \frac{t_1}{t_1} + \cos 0 \right]$$

$$I_{p,avg} = \frac{I_p t_1}{\pi T_s} [-(-1) + 1]$$

$$I_{p,avg} = \frac{2I_p t_1}{\pi T} = \frac{2 \times 500 \times 100\mu\text{s}}{3.14 \times 2000\mu\text{s}} = 15.92\text{ A}$$

Example Problem

2.15 The current waveform of a diode is shown in Figure P2.15. Determine the average, root mean square (rms), and peak current ratings of the diode. Assume $I_p = 500\text{ A}$ of a half sine-wave.

Solution:

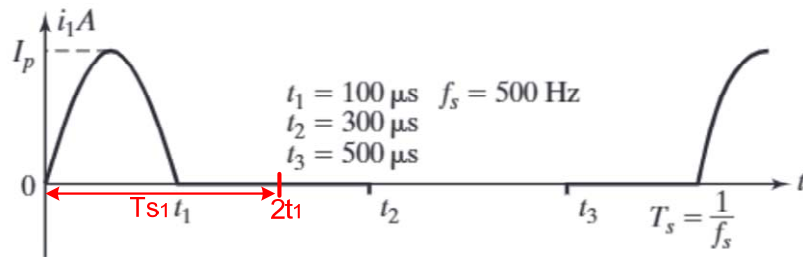


FIGURE P2.15

2) RMS value, $I_{p,rms} = ?$

$$I_{p,rms}^2 = \frac{1}{T} \int_0^{t_1} I_p^2 \sin^2 \omega t \, dt$$

Since $\sin^2 \omega t = \frac{1}{2}(1 - \cos 2\omega t)$

$$I_{p,rms}^2 = \frac{I_p^2}{2T} \int_0^{t_1} (1 - \cos 2\omega t) \, dt$$

$\omega = \frac{2\pi}{2t_1}$

$$I_{p,rms}^2 = \frac{I_p^2}{2T} \left[t \Big|_0^{t_1} - \frac{\sin \frac{4\pi}{2t_1} t}{\frac{4\pi}{2t_1}} \Big|_0^{t_1} \right]$$

$$I_{p,rms}^2 = \frac{I_p^2}{2T} \left[t_1 - \frac{\sin \frac{2\pi}{t_1} t_1}{\frac{4\pi}{2t_1}} + \sin 0 \right] = \frac{I_p^2}{2T} [t_1 - 0 + 0]$$

$$I_{p,rms}^2 = \frac{I_p^2 t_1}{2T} \Rightarrow I_{p,rms} = I_p \sqrt{\frac{t_1}{2T}}$$

$I_{p,rms} = 500 \sqrt{\frac{100\text{ }\mu\text{s}}{2 \times 2000\text{ }\mu\text{s}}} = 79.05\text{ A}$

Example Problem

2.15 The current waveform of a diode is shown in Figure P2.15. Determine the average, root mean square (rms), and peak current ratings of the diode. Assume $I_p = 500\text{ A}$ of a half sine-wave.

Solution:

Given $\therefore t_1 = 100\mu\text{s}, I_p = 500\text{ A}, f_s = 500\text{ Hz}$

$$T = 1 / f_s = 20000\mu\text{s}$$

1) Peak value, $I_{p,peak} = ?$

$$I_{p,peak} = I_p = 500\text{ A}$$

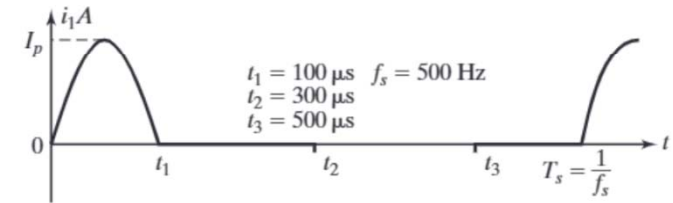
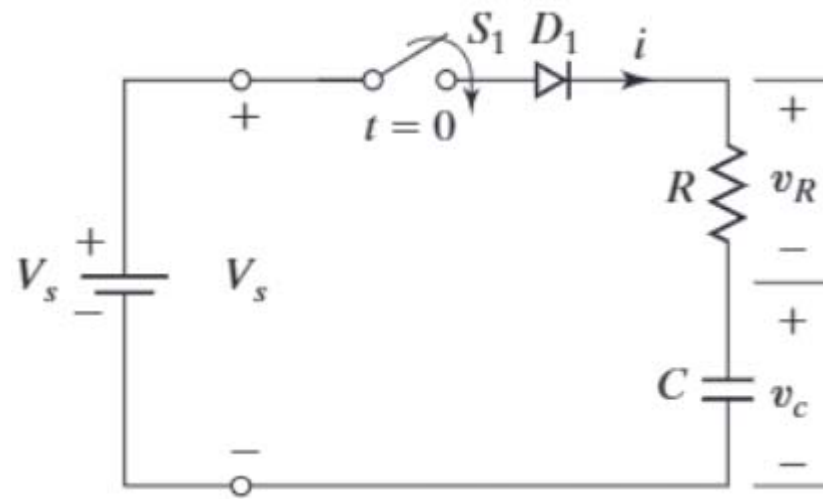


FIGURE P2.15

Example Problem

- 2.22** The diode circuit as shown in Figure 2.15a has $V_s = 220\text{ V}$, $R = 4.7\ \Omega$, and $C = 10\ \mu\text{F}$. The capacitor has an initial voltage of $V_{CO}(t = 0) = 0$. If switch is closed at $t = 0$, determine (a) the peak diode current, (b) the energy dissipated in the resistor R , and (c) the capacitor voltage at $t = 2\ \mu\text{s}$.



(a) Circuit diagram

FIGURE 2.15

Diode circuit with an RC load.

Example Problem

2.22 The diode circuit as shown in Figure 2.15a has $V_s = 220\text{ V}$, $R = 4.7\ \Omega$, and $C = 10\ \mu\text{F}$. The capacitor has an initial voltage of $V_{C0}(t = 0) = 0$. If switch is closed at $t = 0$, determine (a) the peak diode current, (b) the energy dissipated in the resistor R , and (c) the capacitor voltage at $t = 2\ \mu\text{s}$.

Solution:

Given: $V_s = 220\text{ V}$, $R = 4.7\ \Omega$, $C = 10\ \mu\text{F}$

$V_{C0}(t = 0) = 0$

a) Peak diode current, $I_{D,p} = ?$

$$I_{D,p} = \frac{V_s}{R} = \frac{220}{4.7} = 46.8\text{ A}$$

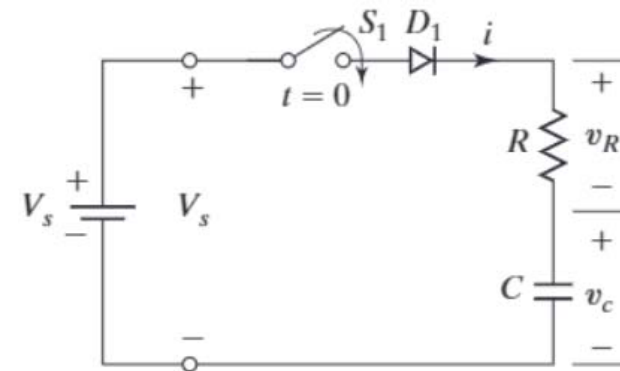
b) Energy dissipated, $W = ?$

$$W = \frac{1}{2} C V_c^2 = \frac{1}{2} \times 10\ \mu \times 220^2 = 0.242\text{ J}$$

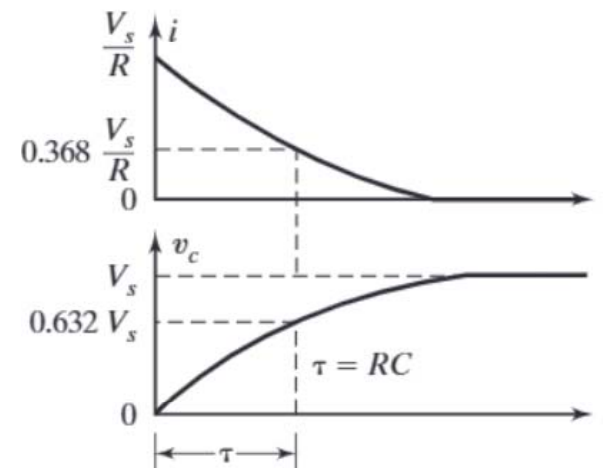
c) Capacitor voltage, $V_c(t = 2\ \mu\text{s}) = ?$

$$V_c = V_s (1 - e^{\frac{-t}{RC}}) = 220 (1 - e^{\frac{-2\ \mu}{4.7 \times 10\ \mu}})$$

$$V_c = 9.165\text{ V}$$



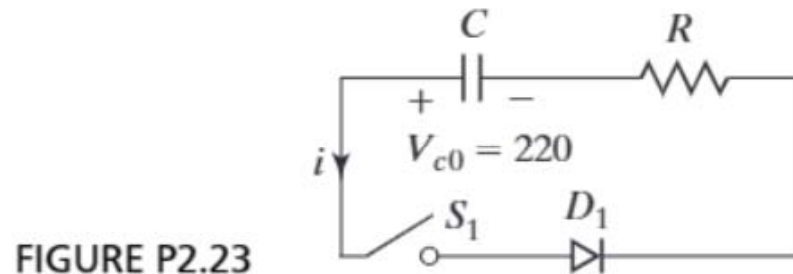
(a) Circuit diagram



(b) Waveforms

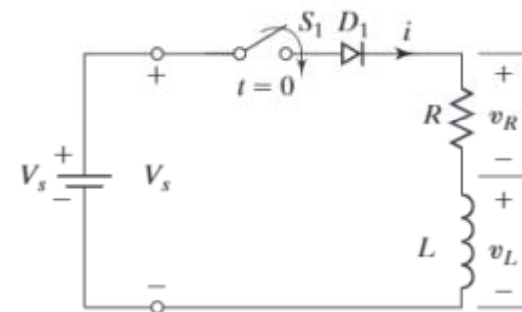
Example Problem

- 2.23** A diode circuit is shown in Figure P2.23 with $R = 22\ \Omega$ and $C = 10\ \mu\text{F}$. If switch S_1 is closed at $t = 0$, determine the expression for the voltage across the capacitor and the energy lost in the circuit.



Example Problem

- 2.24** The diode RL circuit as shown in Figure 2.17a has $V_s = 110\text{ V}$, $R = 4.7\ \Omega$, and $L = 4.5\text{ mH}$. The inductor has no initial current. If switch S_1 is closed at $t = 0$, determine (a) the steady-state diode current, (b) the energy stored in the inductor L , and (c) the initial di/dt .



(a) Circuit diagram

FIGURE 2.17

Diode circuit with an RL load.

Example Problem

2.24 The diode RL circuit as shown in Figure 2.17a has $V_s = 110\text{V}$, $R = 4.7\ \Omega$, and $L = 4.5\text{mH}$. The inductor has no initial current. If switch S_1 is closed at $t = 0$, determine (a) the steady-state diode current, (b) the energy stored in the inductor L , and (c) the initial di/dt .

Solution:

Given: $V_s = 110\text{V}$, $R = 4.7\ \Omega$, $L = 4.5\text{mH}$

$$I_{L0}(t = 0) = 0\text{A}$$

a) Steady state diode current, $I_{D,p} = ?$

$$I_{D,p} = \frac{V_s}{R} = \frac{110}{4.7} = 23.4\text{A}$$

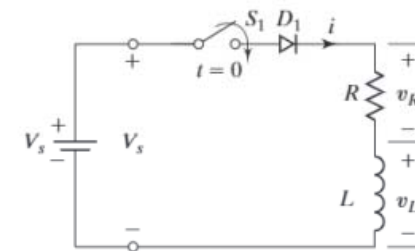
b) Energy dissipated, $W = ?$

$$W = \frac{1}{2} L I_L^2 = \frac{1}{2} \times 4.5\text{m} \times 23.4^2 = 1.23\text{J}$$

c) The initial $di/dt = ?$

$$\frac{di}{dt}(t = 0) = \frac{V_s}{L} = \frac{110}{4.5\text{m}}$$

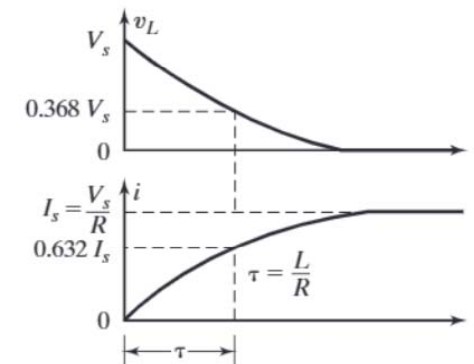
$$\frac{di}{dt} = 2444.4 \frac{\text{A}}{\text{s}}$$



(a) Circuit diagram

FIGURE 2.17

Diode circuit with an RL load.



(b) Waveforms

$$i(t) = \frac{V_s}{R} (1 - e^{-tR/L}) \quad (2.25)$$

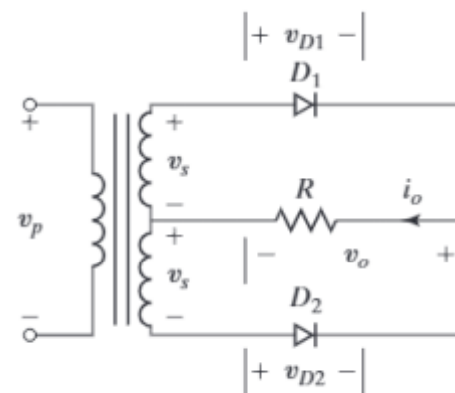
The rate of change of this current can be obtained from Eq. (2.25) as

$$\frac{di}{dt} = \frac{V_s}{L} e^{-tR/L} \quad (2.26)$$

Example Problem

Example 3.1 Finding the Performance Parameters of a Full-Wave Rectifier with a Center-Tapped Transformer

If the rectifier in Figure 3.2a has a purely resistive load of R , determine (a) the efficiency, (b) the FF, (c) the RF, (d) the TUF, (e) the PIV of diode D_1 , (f) the CF of the input current, and (g) the input power factor PF.



(a) Circuit diagram

Example Problem

Example 3.1 Finding the Performance Parameters of a Full-Wave Rectifier with a Center-Tapped Transformer

If the rectifier in Figure 3.2a has a purely resistive load of R , determine (a) the efficiency, (b) the FF, (c) the RF, (d) the TUF, (e) the PIV of diode D_1 , (f) the CF of the input current, and (g) the input power factor PF.

Solution

From Eq. (3.11), the average output voltage is

$$V_{dc} = \frac{2}{T} \int_0^{T/2} V_m \sin \omega t \, dt = \frac{2V_m}{\pi} = 0.6366V_m \quad (3.11)$$

$$V_{dc} = \frac{2V_m}{\pi} = 0.6366V_m$$

and the average load current is

$$I_{dc} = \frac{V_{dc}}{R} = \frac{0.6366V_m}{R}$$

The rms values of the output voltage and current are

$$V_{rms} = \left[\frac{2}{T} \int_0^{T/2} (V_m \sin \omega t)^2 \, dt \right]^{1/2} = \frac{V_m}{\sqrt{2}} = 0.707V_m$$

$$I_{rms} = \frac{V_{rms}}{R} = \frac{0.707V_m}{R}$$

Example Problem

Example 3.1 Finding the Performance Parameters of a Full-Wave Rectifier with a Center-Tapped Transformer

If the rectifier in Figure 3.2a has a purely resistive load of R , determine (a) the efficiency, (b) the FF, (c) the RF, (d) the TUF, (e) the PIV of diode D_1 , (f) the CF of the input current, and (g) the input power factor PF.

$$P_{dc} = V_{dc}I_{dc} \quad (3.1)$$

From Eq. (3.1) $P_{dc} = (0.6366V_m)^2/R$

$$P_{ac} = V_{rms}I_{rms} \quad (3.2)$$

from Eq. (3.2) $P_{ac} = (0.707V_m)^2/R$.

$$\eta = \frac{P_{dc}}{P_{ac}} \quad (3.3)$$

a. From Eq. (3.3), the efficiency $\eta = (0.6366V_m)^2/(0.707V_m)^2 = 81\%$.

b. From Eq. (3.5), the form factor $FF = 0.707V_m/0.6366V_m = 1.11$.

$$FF = \frac{V_{rms}}{V_{dc}} \quad (3.5)$$

c. From Eq. (3.7), the ripple factor $RF = \sqrt{1.11^2 - 1} = 0.482$ or 48.2%.

d. $TUF = \frac{P_{dc}}{V_s I_s}$

$$V_s = V_m/\sqrt{2} = 0.707V_m$$

$$I_s = 0.707V_m / R$$

$$TUF = \frac{(0.6366V_m)^2 / R}{(0.707V_m)^2 / R} = 81\%$$

Example Problem

Example 3.1 Finding the Performance Parameters of a Full-Wave Rectifier with a Center-Tapped Transformer

If the rectifier in Figure 3.2a has a purely resistive load of R , determine (a) the efficiency, (b) the FF, (c) the RF, (d) the TUF, (e) the PIV of diode D_1 , (f) the CF of the input current, and (g) the input power factor PF.

- e. The peak reverse blocking voltage, $PIV = 2V_m$.
- f. $I_{s(\text{peak})} = V_m/R$ and $I_s = 0.707V_m/R$. The CF of the input current is $CF = I_{s(\text{peak})}/I_s = 1/0.707 = \sqrt{2}$.
- g. The input PF for a resistive load can be found from

$$PF = \frac{P_{ac}}{V_s I_s}$$
$$PF = \frac{(0.707V_m)^2 / R}{(0.707V_m)^2 / R} = 1$$

$$\text{from Eq. (3.2) } P_{ac} = (0.707V_m)^2 / R.$$

$$V_s = V_m / \sqrt{2} = 0.707V_m$$

$$I_s = 0.707V_m / R$$