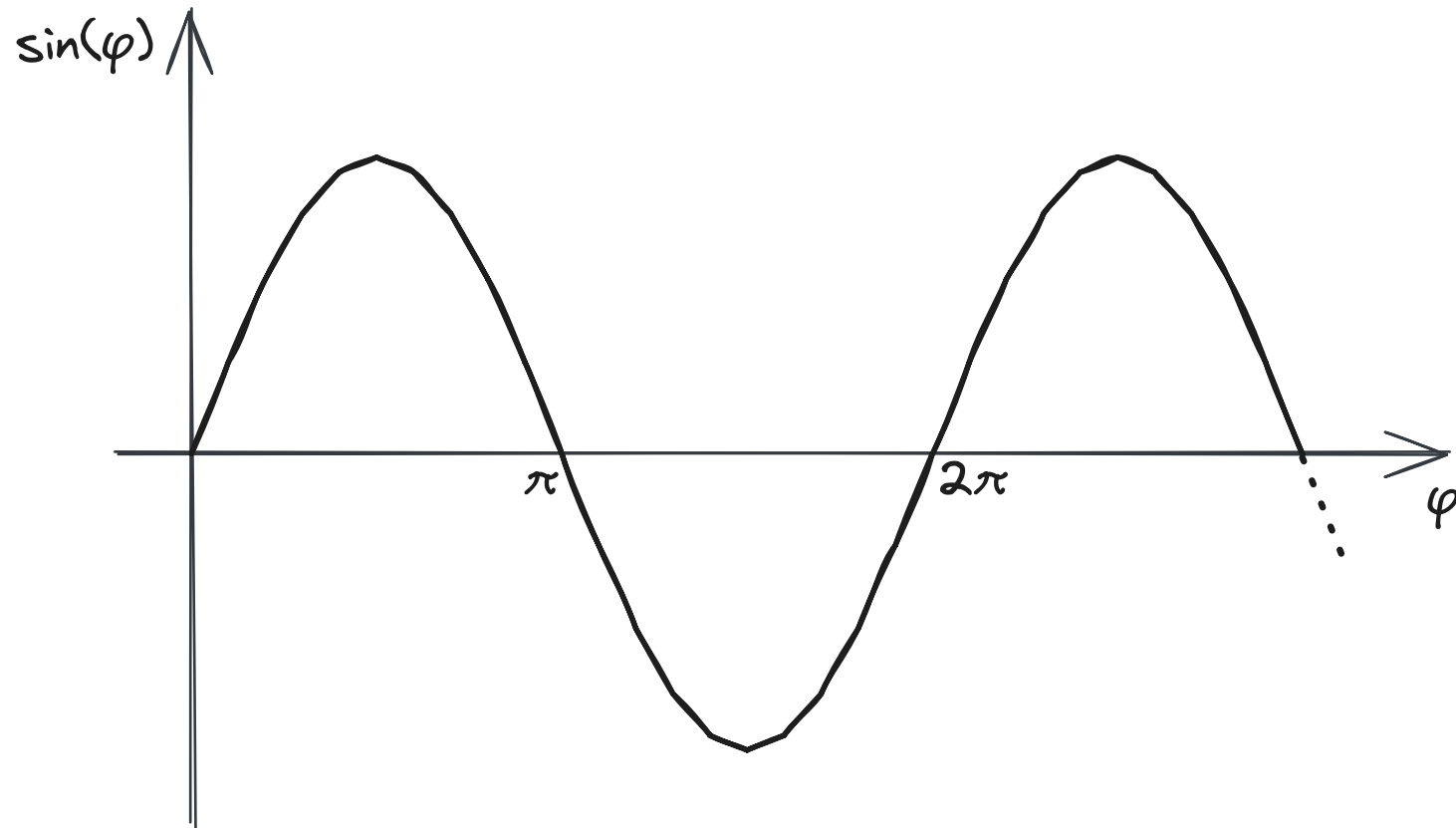


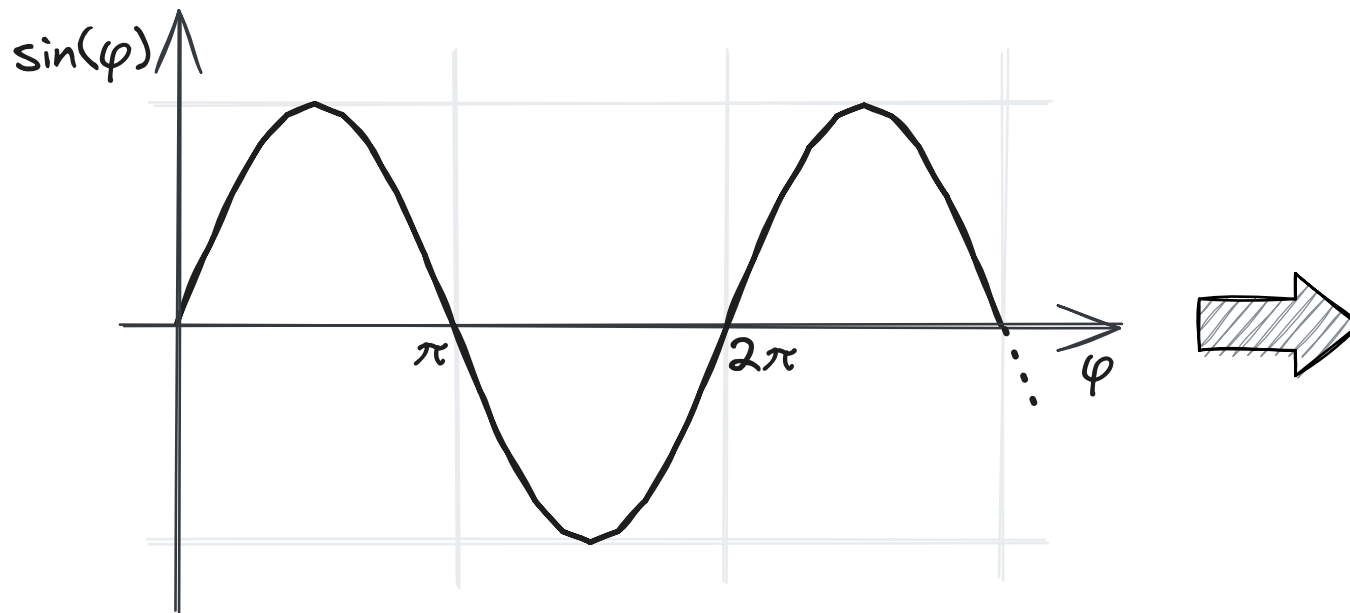
Numerically Controlled Oscillators (NCO)

Shadi Youssef
@Radiohub

How can we generate a sinusoidal signal in the digital domain?



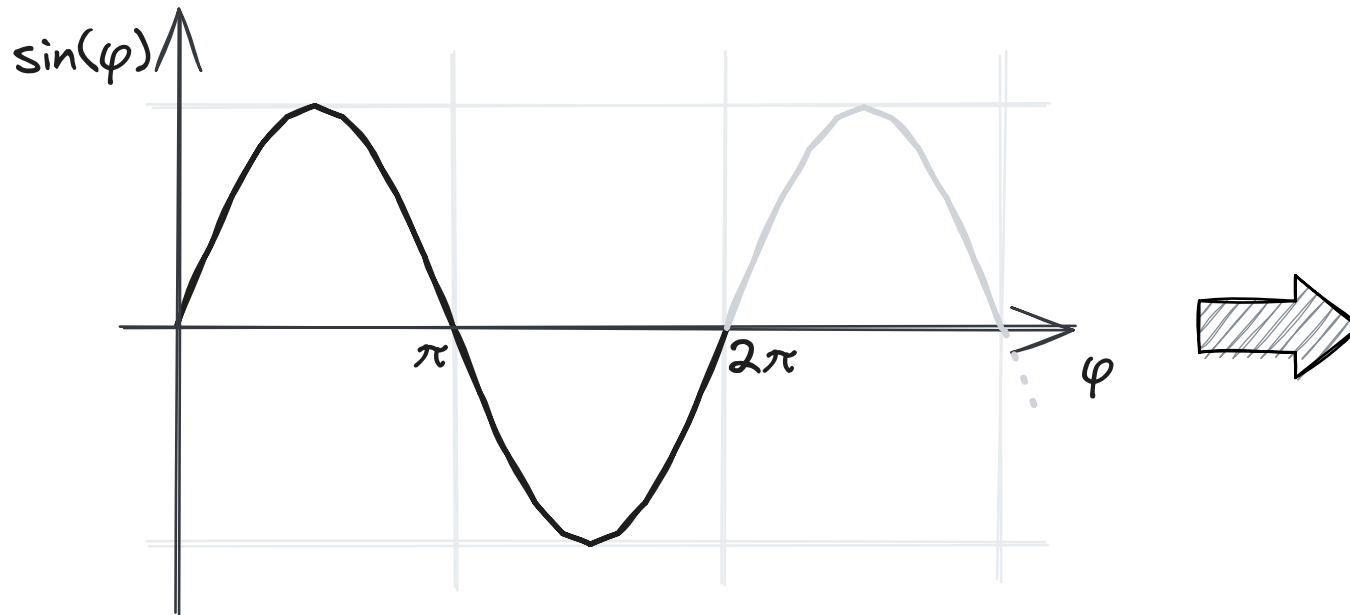
We can record the waveform in memory
 To generate the sine wave, we simply playback the recording



φ	$\sin(\varphi)$
0	$\sin(0)$
φ_0	$\sin(\varphi_0)$
$2\varphi_0$	$\sin(2\varphi_0)$
\vdots	\vdots
$2\pi - \varphi_0$	$\sin(2\pi - \varphi_0)$
2π	$\sin(0)$
$2\pi + \varphi_0$	$\sin(\varphi_0)$
\vdots	\vdots

For now, assume recording has infinite resolution
 This means, $\varphi_0 \rightarrow 0$ and $\sin(\varphi)$ word length $\rightarrow \infty$
 This requires infinite memory (more on this later)


A sine wave repeats every 2π
 So we record one period only and play it back on repeat
 This saves memory



φ	$\sin(\varphi)$
0	$\sin(0)$
φ_0	$\sin(\varphi_0)$
$2\varphi_0$	$\sin(2\varphi_0)$
\vdots	\vdots
$2\pi - \varphi_0$	$\sin(2\pi - \varphi_0)$
2π	$\sin(0)$
$2\pi + \varphi_0$	$\sin(\varphi_0)$
\vdots	\vdots

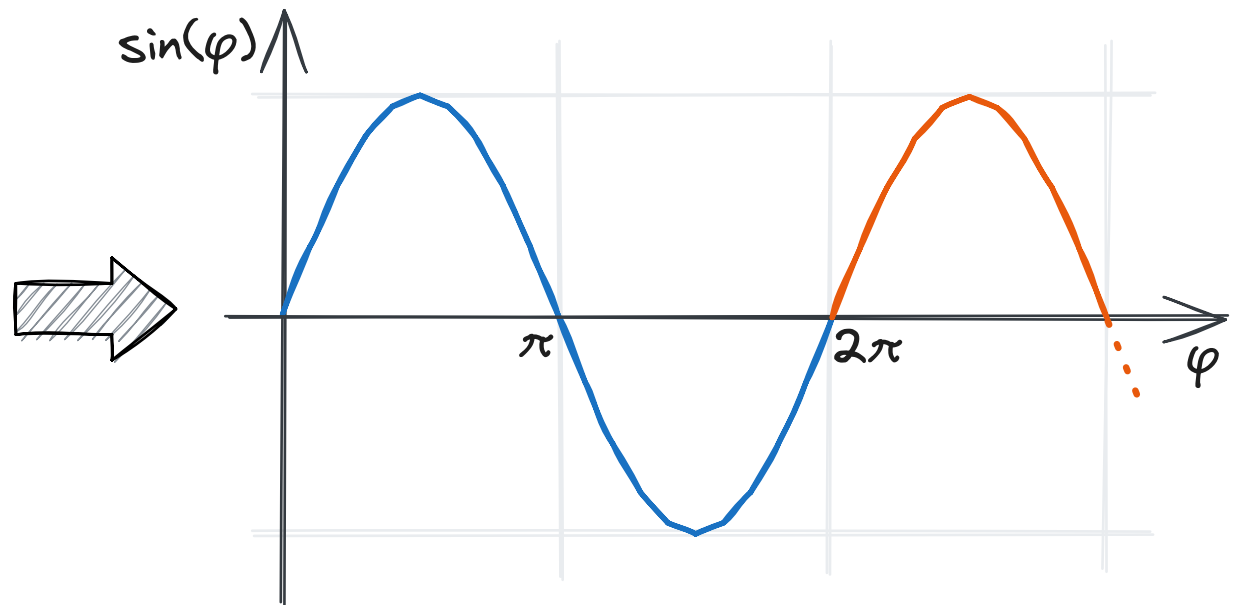
We can save more memory by recording 1/4 period only
 and using a slightly more complicated playback scheme

By cycling through the memory entries, we playback the sine wave
Playback speed = 1 sample per clock cycle $1/f_{clk}$



A diagram showing a wrap-around arrow. A large orange curved arrow starts from the bottom of the table and points back to the top. Three smaller blue curved arrows point downwards from one row to the next, indicating the sequence of memory entries.

φ	$\sin(\varphi)$
0	$\sin(0)$
φ_0	$\sin(\varphi_0)$
$2\varphi_0$	$\sin(2\varphi_0)$
\vdots	\vdots
$2\pi - \varphi_0$	$\sin(2\pi - \varphi_0)$



We don't need φ to read out the corresponding $\sin(\varphi)$ value

Instead we assign an index to each entry

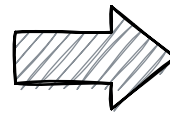
We use the index to look-up values as needed during playback

We don't need this column

φ	$\sin(\varphi)$
0	$\sin(0)$
φ_0	$\sin(\varphi_0)$
$2\varphi_0$	$\sin(2\varphi_0)$
\vdots	\vdots
$2\pi - \varphi_0$	$\sin(2\pi - \varphi_0)$

We add this column instead

index	$\sin(\varphi)$
0	$\sin(0)$
1	$\sin(\varphi_0)$
2	$\sin(2\varphi_0)$
\vdots	\vdots
$2^M - 1$	$\sin(2\pi - \varphi_0)$




Look-up table (LUT)

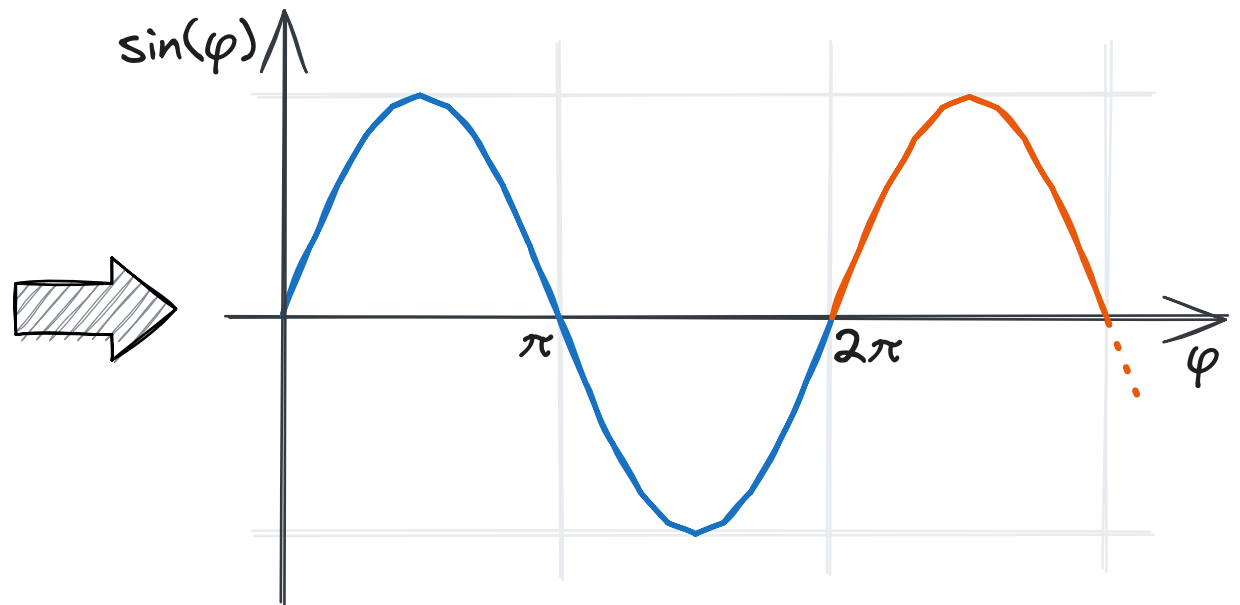
This means there are 2^M points in a 2π period, so phase step $\varphi_0 = 2\pi/2^M$

We are still assuming infinite resolution, so $\varphi_0 \rightarrow 0$ means $M \rightarrow \infty$

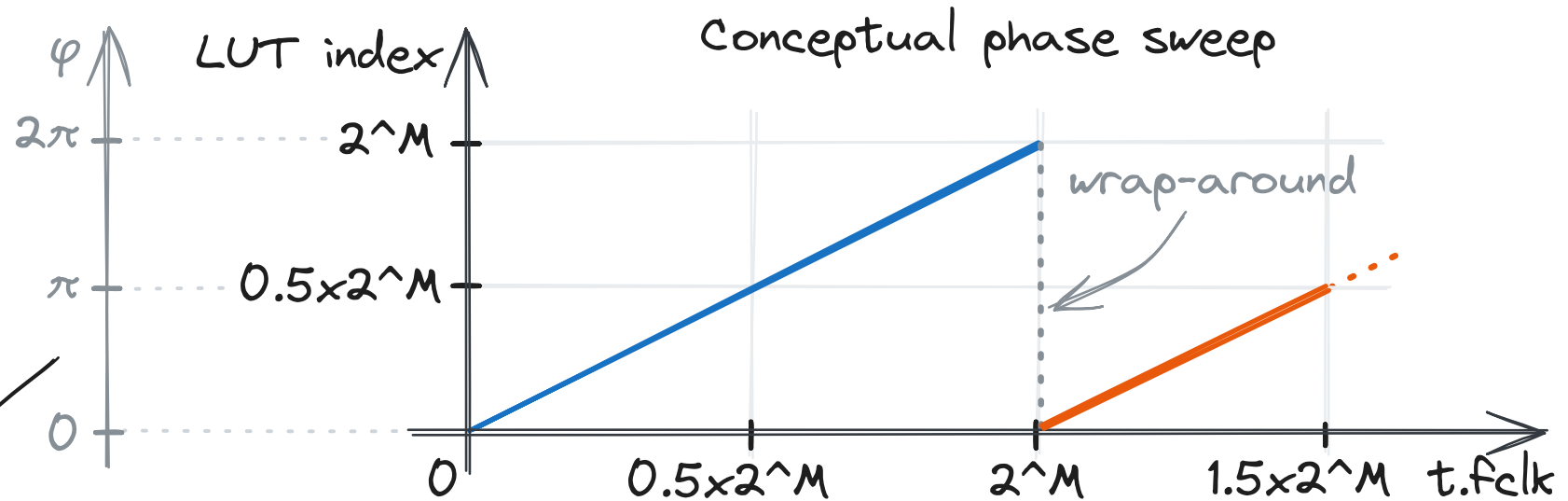
We now cycle through the LUT index instead to playback the sine wave
Playback speed still = 1 sample per clock cycle $1/f_{clk}$



index	$\sin(\varphi)$
0	$\sin(0)$
1	$\sin(\varphi_0)$
2	$\sin(2\varphi_0)$
\vdots	\vdots
2^M-1	$\sin(2\pi-\varphi_0)$

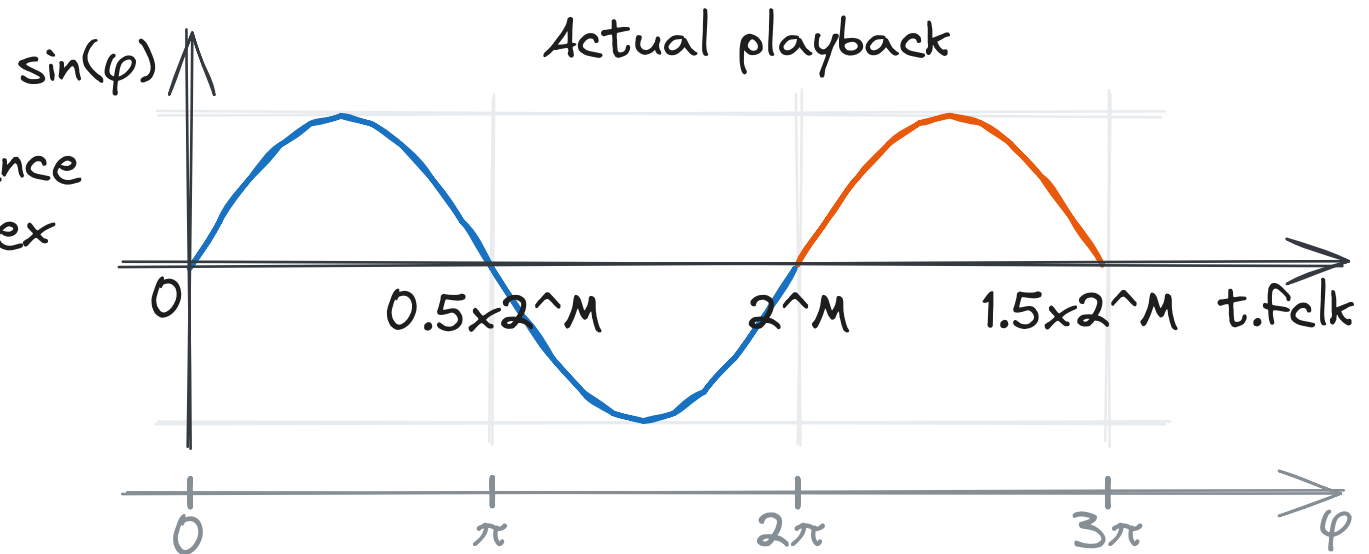


We can see that sweeping LUT index = sweeping sine wave phase



one-to-one correspondence
between φ & LUT index

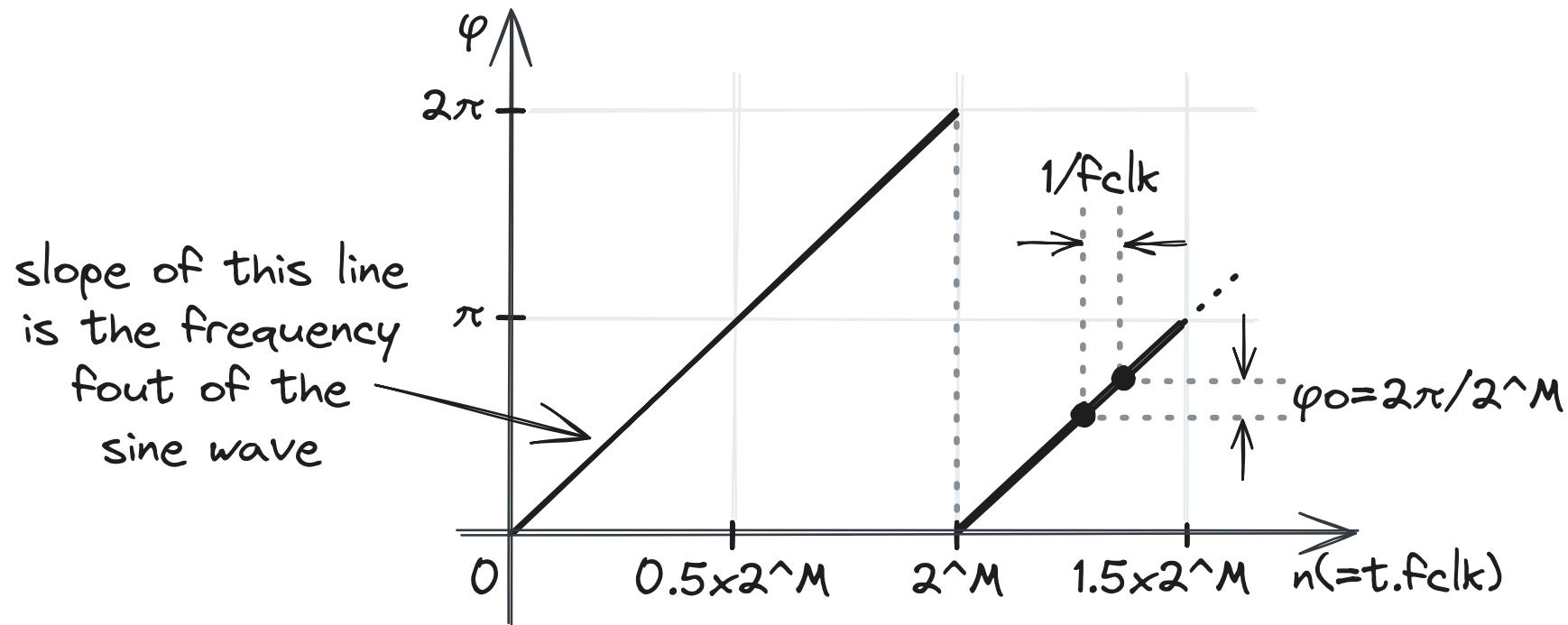
$$\frac{\varphi}{2\pi} = \frac{\text{LUT index}}{2^M}$$



Frequency = rate of change of phase

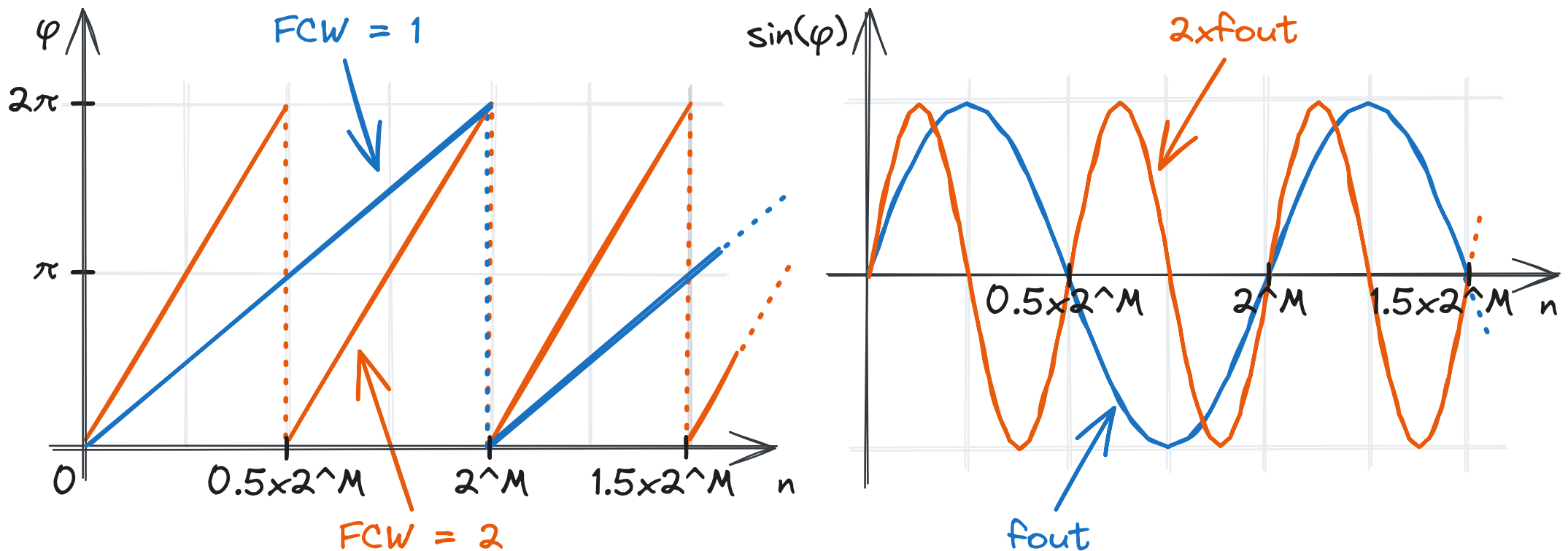
Output sine wave accumulates phase at a rate of φ_0 per clock cycle

$$f_{out} = \frac{\varphi_0}{2\pi} f_{clk} = \frac{2\pi/2^M}{2\pi} f_{clk} = \frac{f_{clk}}{2^M}$$



To make frequency programmable, we simply skip LUT entries during playback
 A frequency control word (FCW) sets the phase step per clock cycle
 Now phase accumulates at a rate of $\text{FCW} \times \varphi_0$ per clock cycle

$$f_{\text{out}} = \frac{\text{FCW}}{2^M} f_{\text{clk}}$$



Summing up what we did so far

We started with a continuous-time sine wave

$$x(t) = \sin(\varphi(t))$$

whose phase accumulates linearly with time at a rate of f_{out}

$$x(t) = \sin(2\pi \times f_{out} \times t)$$

We generated a digital replica of the signal sampled at $t = n/f_{clk}$ intervals

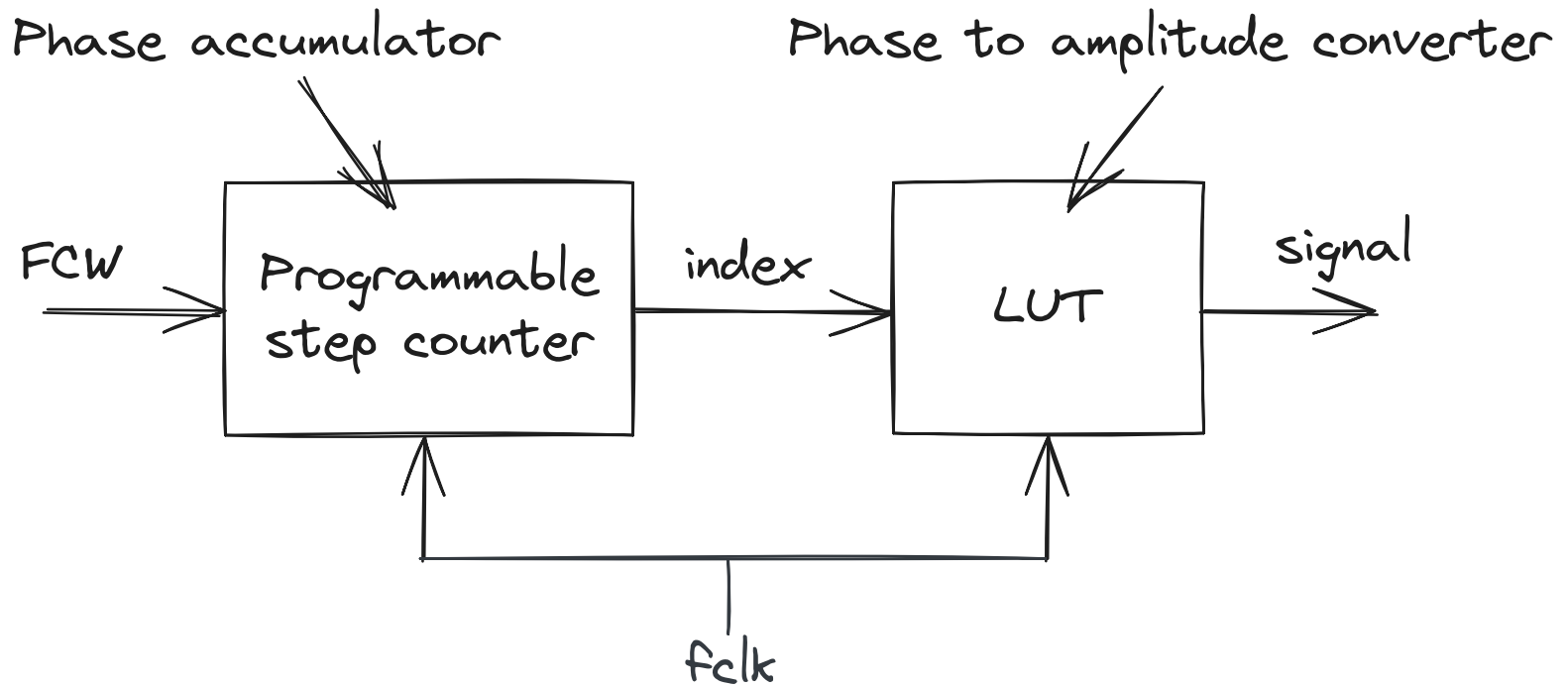
$$x[n] = \sin(2\pi \times f_{out}/f_{clk} \times n)$$

and we made its frequency programmable by introducing a control word FCW

$$x[n] = \sin(2\pi \times FCW/2^M \times n)$$

Putting it all together

We have a numerically controlled oscillator (NCO)

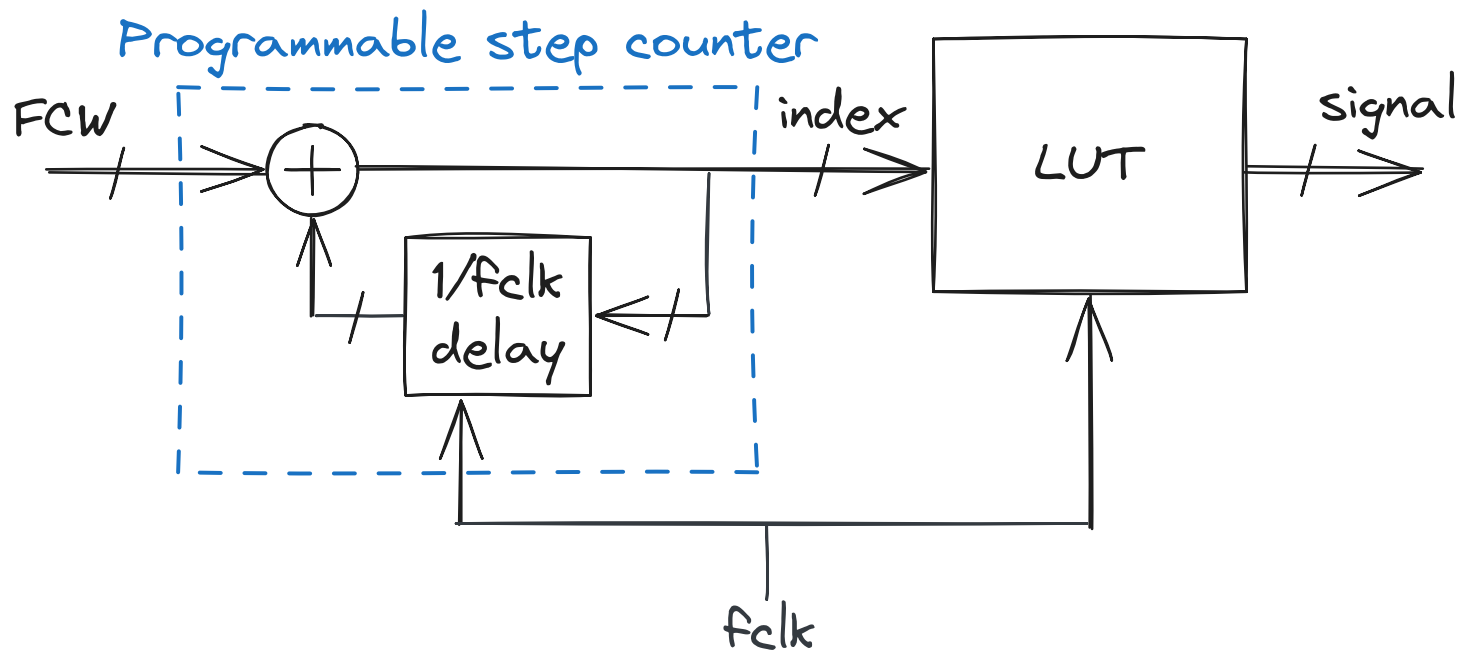


A programmable step counter is a simple accumulator

$$\text{index}[n] = \text{index}[n-1] + \text{FCW}$$

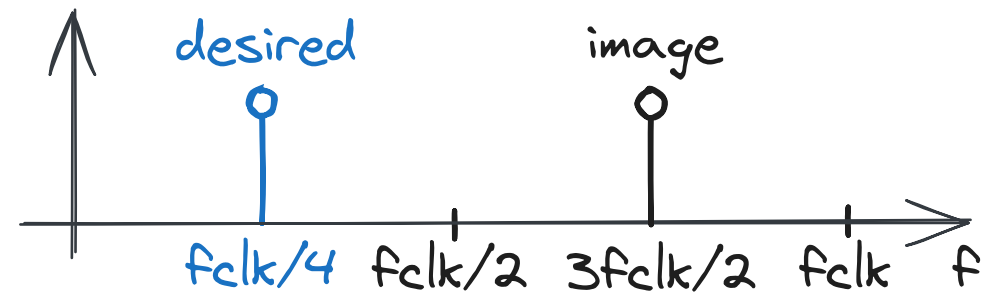
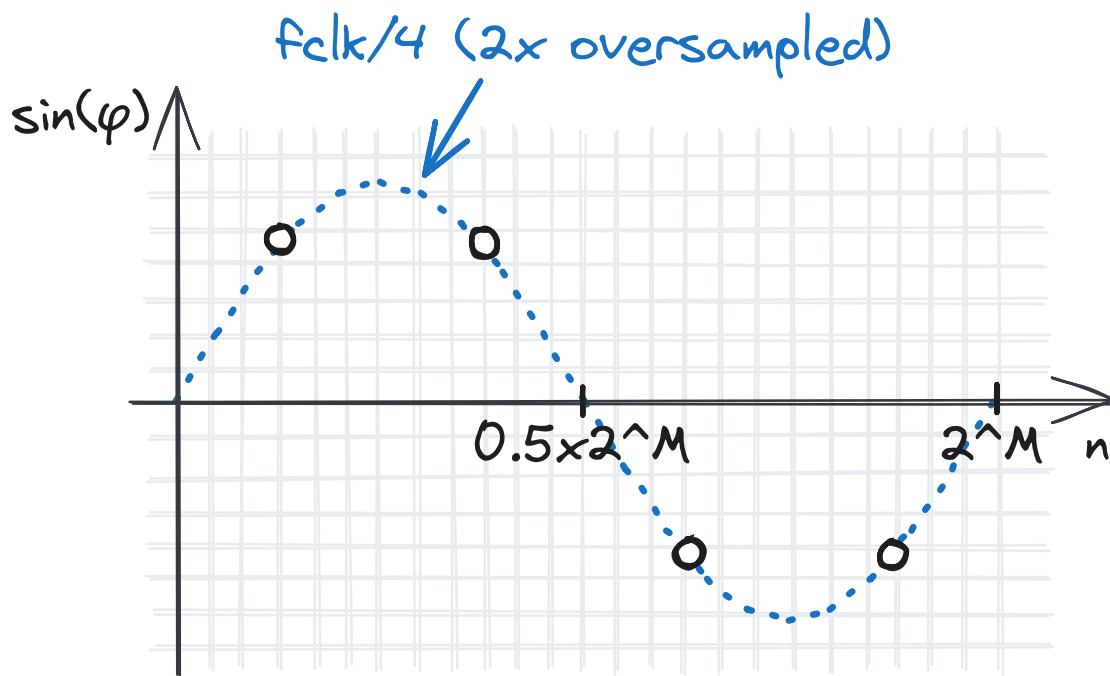
which is equivalent to

$$\varphi[n] = \varphi[n-1] + \text{FCW} \times \varphi_0$$



Frequency Range

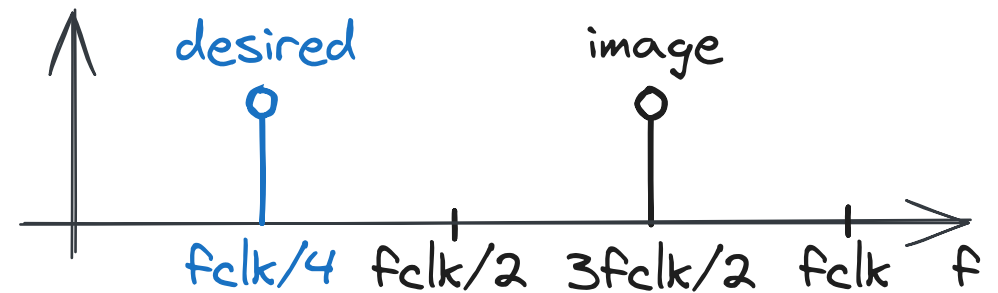
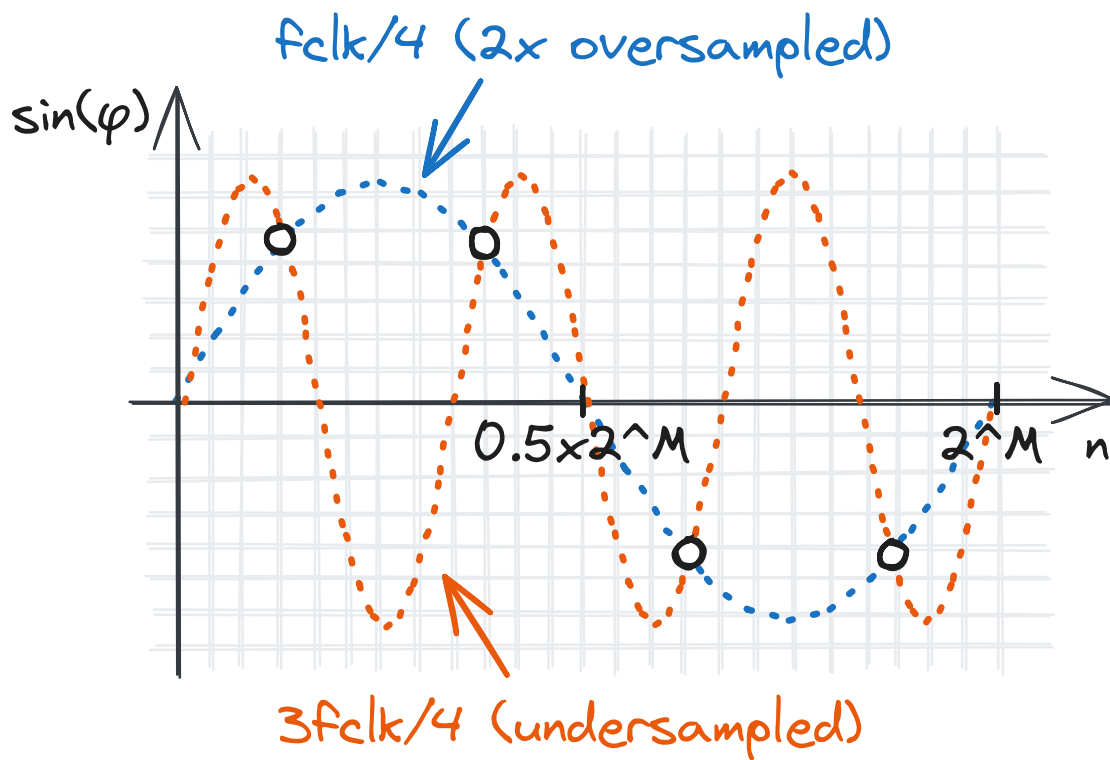
We are generating a sampled version of a sine wave, so Nyquist applies



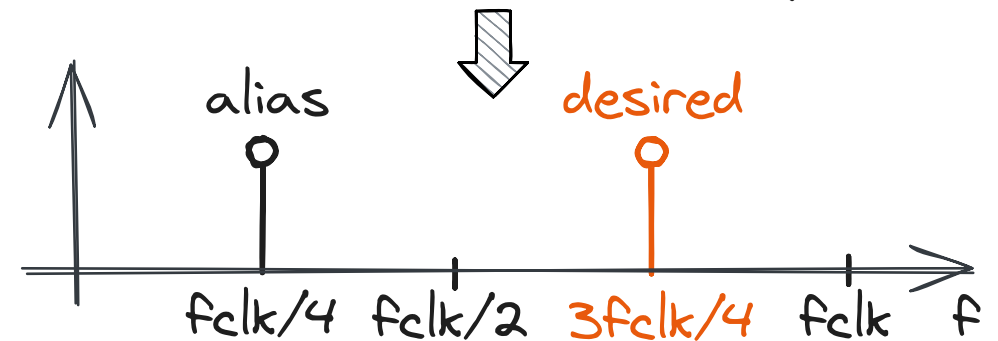
Frequency Range

The NCO can generate unambiguous frequencies from DC to $f_{clk}/2$

$$f_{out} < f_{clk}/2$$



These 2 spectra are indistinguishable



Frequency Range

$$f_{out}/f_{clk} = FCW/2^M$$

No alias condition

$$f_{out}/f_{clk} < 1/2$$

which translates to

$$FCW < 2^{(M-1)}$$



For an M-bit accumulator design, FCW should be (M-1) bits long
Alternatively, FCW is M-bits long, but MSB is never set to 1

Frequency Range

Frequencies corresponding to FCW and $2^M - \text{FCW}$ form signal-image pairs across 1st and 2nd Nyquist zones

Example:

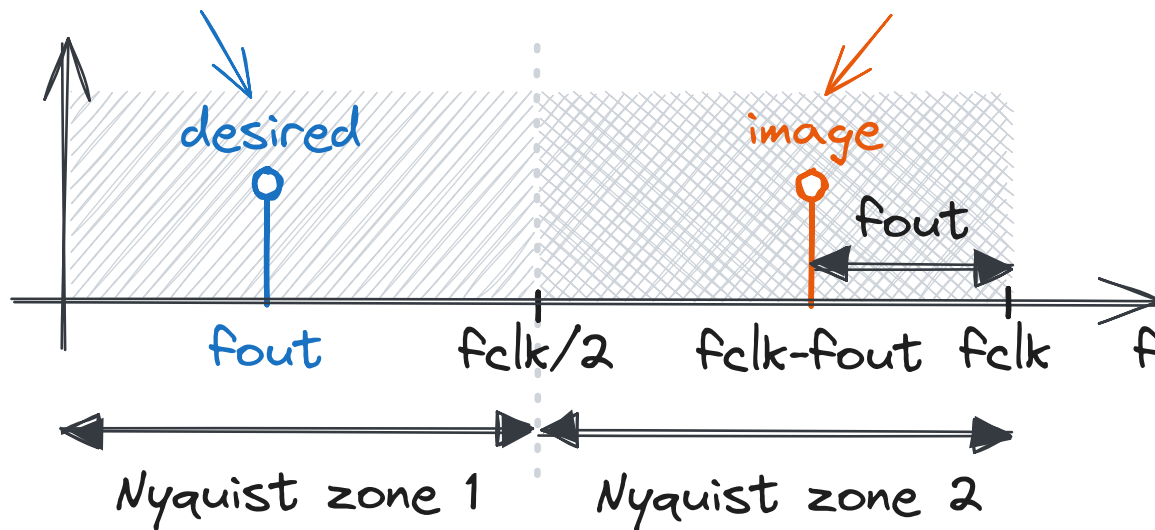
$$M = 16 \text{ \& } f_{\text{clk}} = 100\text{MHz}$$

$$\text{For FCW} = 2^{13} \rightarrow f_{\text{out}} = 12.5\text{MHz}$$

$$\text{For FCW} = 2^{16} - 2^{13} \rightarrow f_{\text{out}} = 87.5\text{MHz} (=100 - 12.5\text{MHz})$$

$$f_{\text{out}} = \text{FCW} \times f_{\text{clk}} / 2^M$$

$$f_{\text{clk}} - f_{\text{out}} = (2^M - \text{FCW}) \times f_{\text{clk}} / 2^M$$

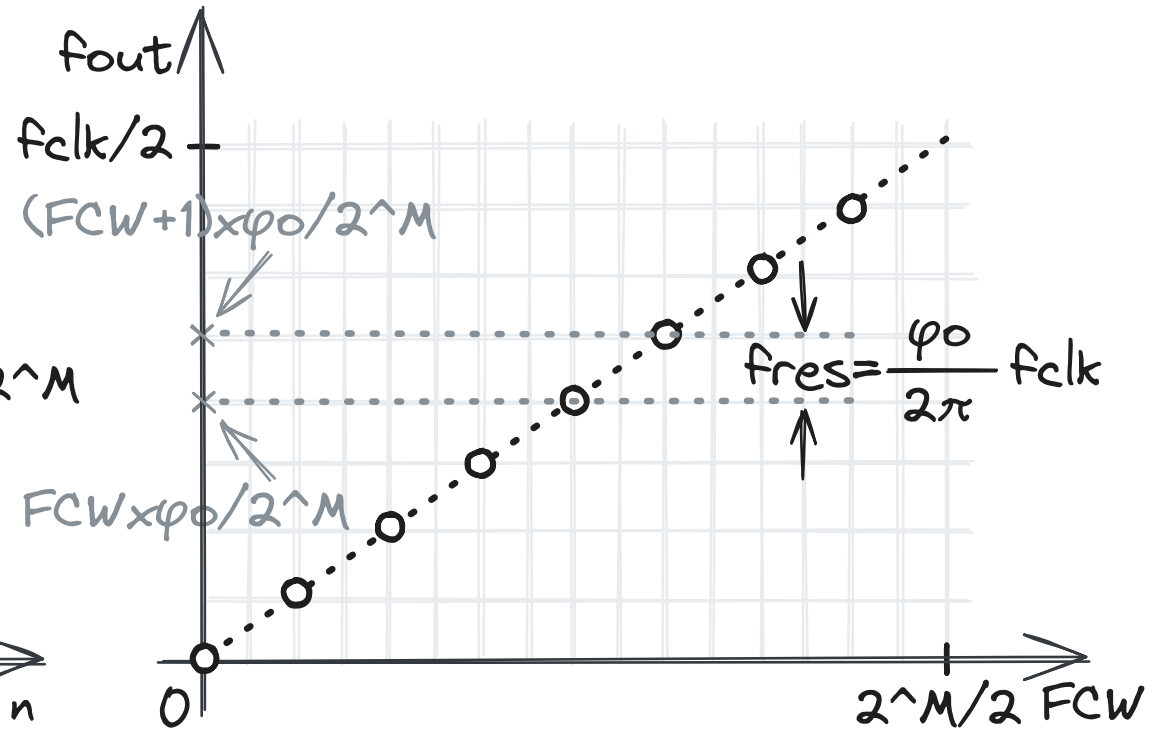
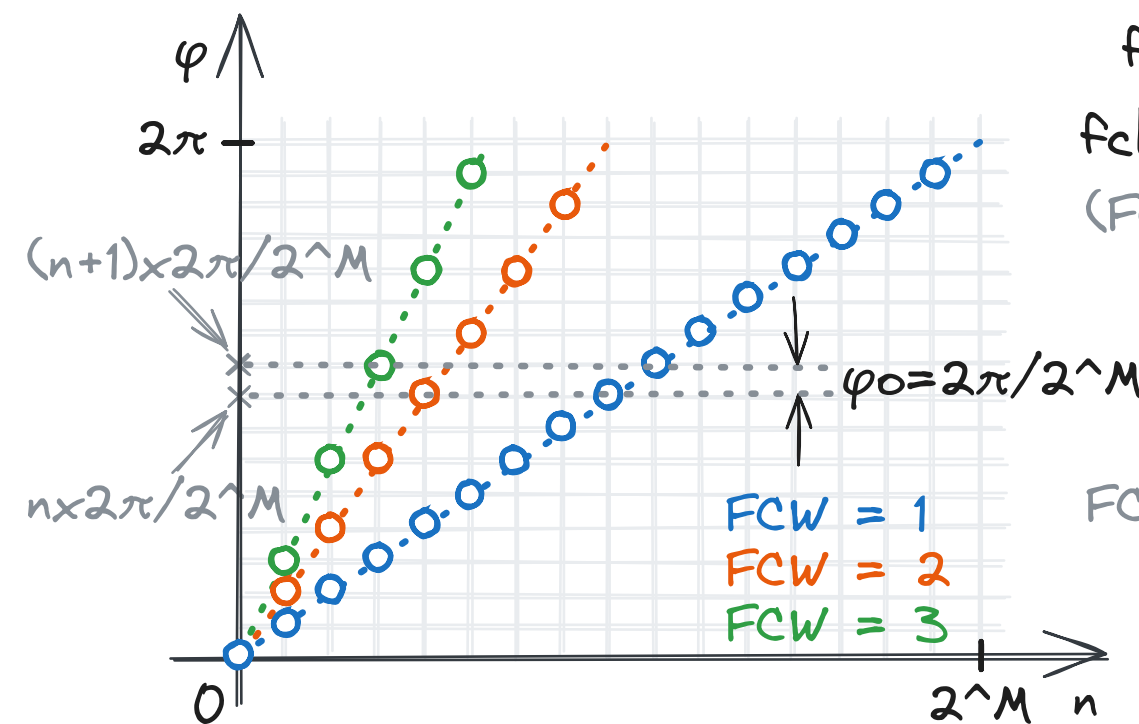


Frequency Resolution

Frequency resolution = min. frequency step possible

Min. frequency step possible corresponds to min. FCW increment, which is 1

$$f_{res} = \frac{f_{clk}}{2^M}$$



Frequency Resolution

How accurate is the output frequency relative to the clock frequency?

$$\text{Frequency accuracy} = f_{\text{out}}/f_{\text{clk}} = 1/2^M$$

We can achieve very high accuracy by increasing index word length

For Example

$$M = 32 \rightarrow \text{NCO accuracy} = 0.2 \text{ ppb}$$

For comparison

Typical XTAL accuracy is 20 ppm

NCO is 10^5 better!

This means
accuracy
is determined
by accuracy
of f_{clk} XTAL
and not
the NCO

Frequency Resolution

Finite frequency precision results in absolute frequency error $< f_{res}/2$
Frequency error causes phase drift between ideal and actual sinusoid

Example:

Requirements: $M = 32$, $f_{clk} = 100\text{MHz}$ & $f_{out} = 13.56\text{MHz}$

$$f_{res} = f_{clk}/2^M = 23.283\text{mHz}$$

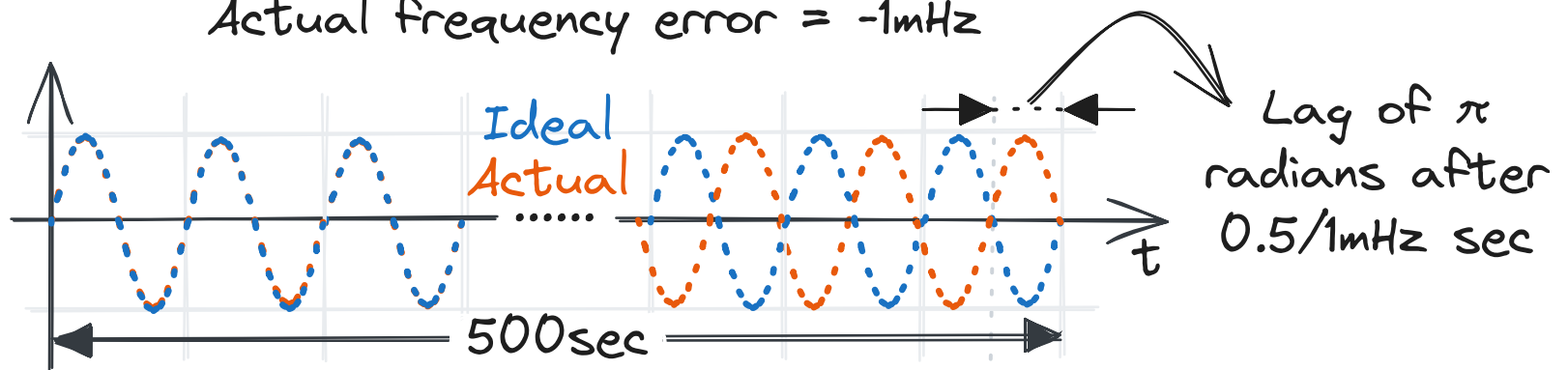
$$\text{Max absolute frequency error} = f_{res}/2 = 11.641\text{mHz}$$

$$\text{Ideal FCW} = 2^M \times f_{out} / f_{clk} = 582,397,565.3376$$

$$\text{Actual FCW (must be integer)} = 582,397,565$$

$$\text{Actual } f_{out} = 13.559\text{MHz}$$

$$\text{Actual frequency error} = -1\text{mHz}$$



Phase Truncation

High frequency resolution comes at the expense of large LUT size

Example:

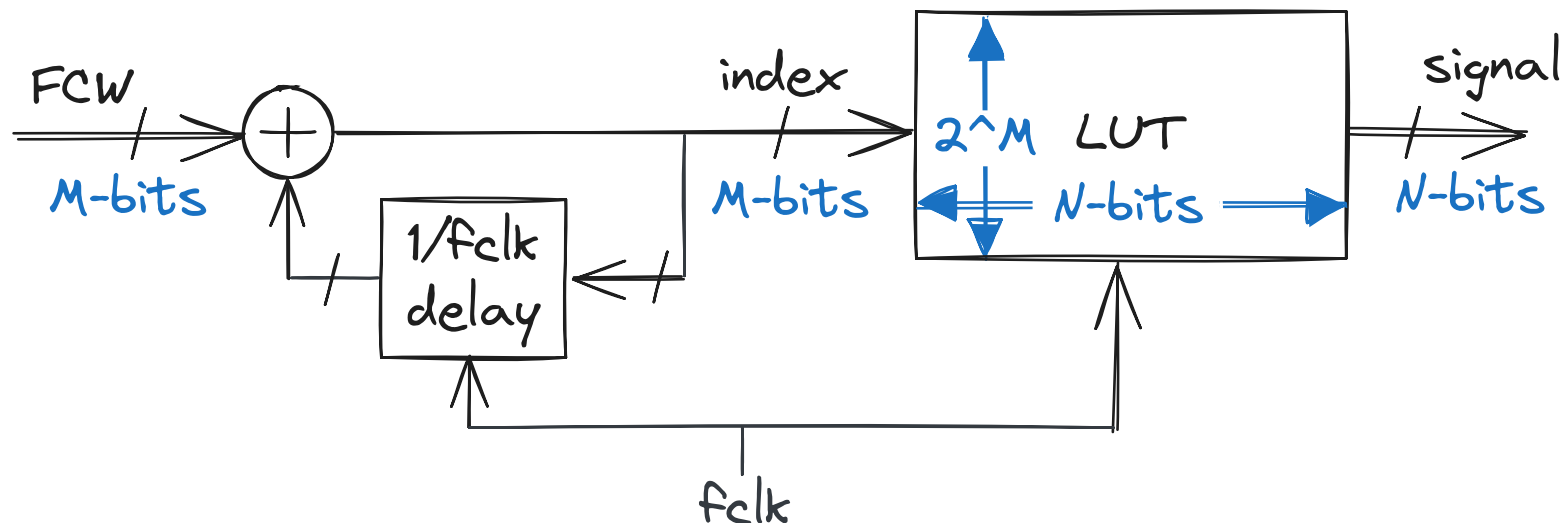
Assume frequency accuracy required $< 1\text{ppb}$

$$\text{ppb error} = 1e9 \times f_{\text{res}}/f_{\text{clk}} = 1e9/2^M \rightarrow M = 30$$

Assuming quantization accuracy required $> 70\text{dB}$

$$\text{SNR} = 6N + 1.76 \rightarrow N = 12$$

This means LUT size = $2^{30} \times 12/8 = 1.5\text{GBytes!}$

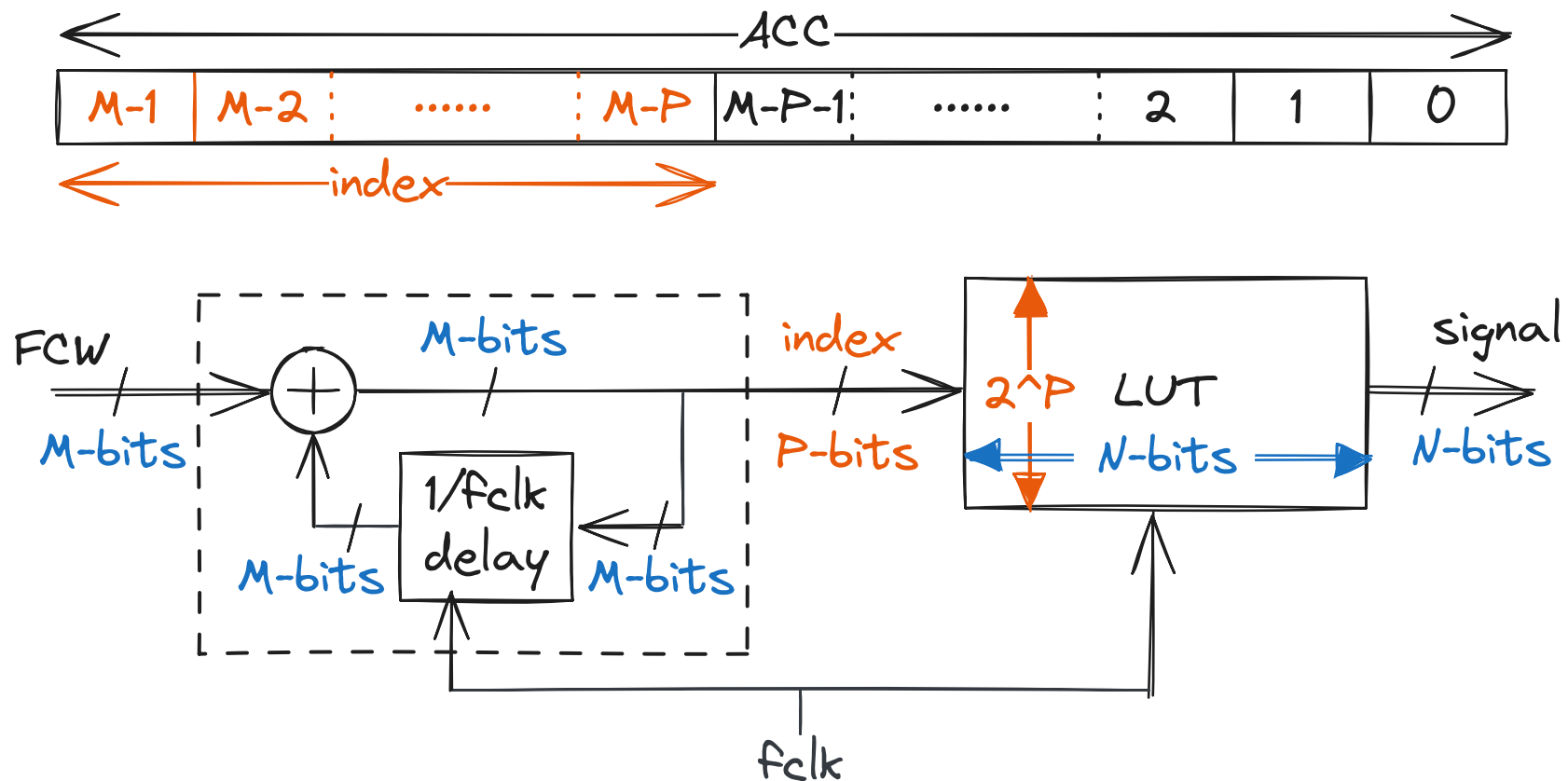


Phase Truncation

We reduce LUT size by truncating the ACC value to P MSBs to access LUT

Frequency resolution still = $f_{clk}/2^M$

But LUT size is now reduced by a factor of $2^{(M-P)}$



Phase Truncation

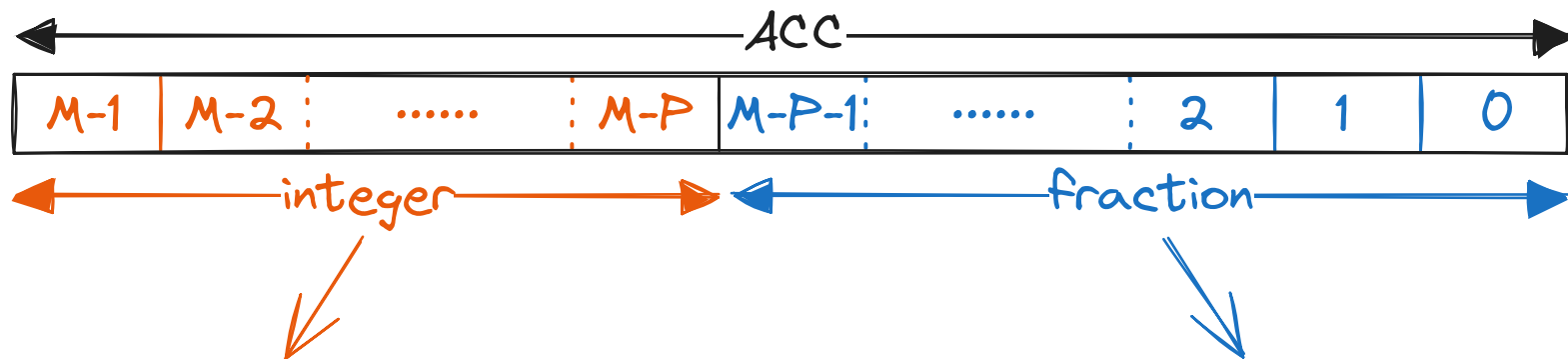
Truncation effectively introduces integer and fractional phase steps

$$\text{Integer phase step } \varphi_0 = 2\pi/2^P$$

$$\text{Fractional phase step } \varphi_f = 2\pi/2^M$$

Only the integer portion is used to access the LUT

Dropping the fractional part introduces a phase truncation error

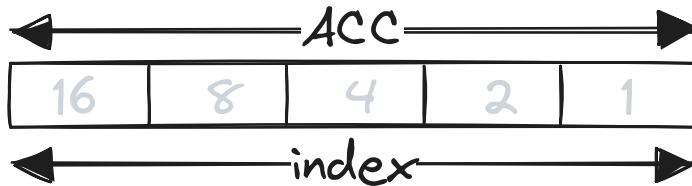


This portion is the LUT index.
As far as the LUT is concerned,
at any given clock cycle, the value
stored here is phase of the sinusoid

ACC continues to accumulate
fractional steps. At any given clock
cycle, value stored here is the
phase truncation error introduced

Phase Truncation

Example: $M=P=5$, $FCW=3$



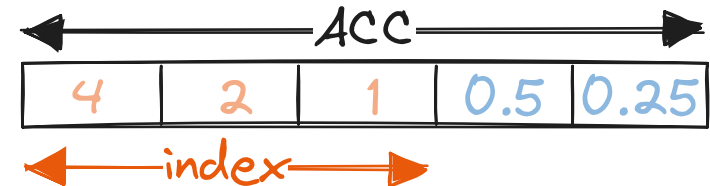
$$\varphi_0 = 360/2^5 = 11.25\text{deg.}$$

$$\varphi_f = 0$$

CLK	ACC (dec.)	ACC (bin.)	φ (deg.)
0	0	00000	0
1	3	00011	3×11.25
2	6	00110	6×11.25
3	9	01001	9×11.25
4	12	01100	12×11.25
5	15	01111	15×11.25
:	:	:	:

$\xrightarrow{\hspace{2cm}}$
 Truncation is
 equivalent to:
 $ACC/2^{(M-P)}$
 $FCW/2^{(M-P)}$
 $\varphi_0 \times 2^{(M-P)}$
 $\xrightarrow{\hspace{2cm}}$

Example: $M=5$, $P=3$, $FCW=3$



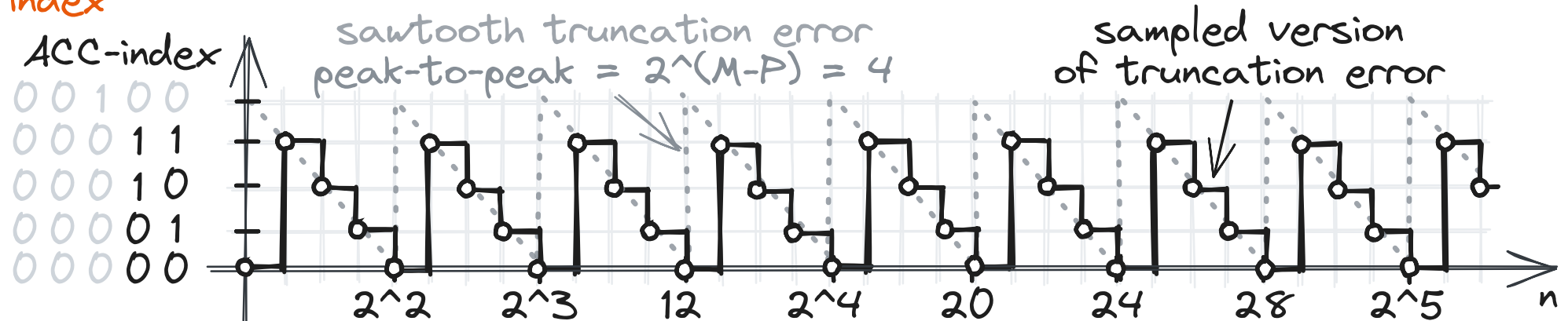
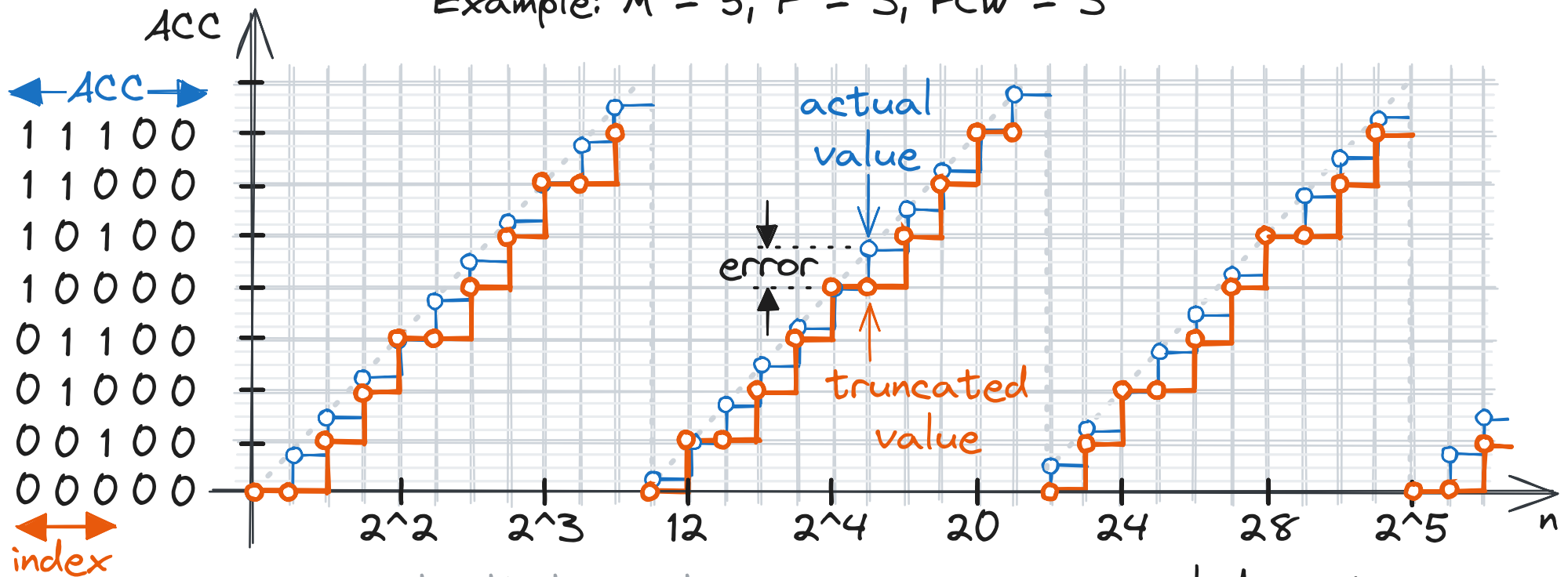
$$\varphi_0 = 360/2^3 = 45\text{deg.}$$

$$\varphi_f = 360/2^5 = 11.25\text{deg.}$$

CLK	ACC (dec.)	ACC (bin.)	φ (deg.)	φ error (deg.)
0	0.0	00000	0	0
1	0.75	00011	0	3×11.25
2	1.5	00110	45	2×11.25
3	2.25	01001	2×45	1×11.25
4	0.0	01100	3×45	0
5	3.75	01111	3×45	3×11.25
:	:	:	:	:

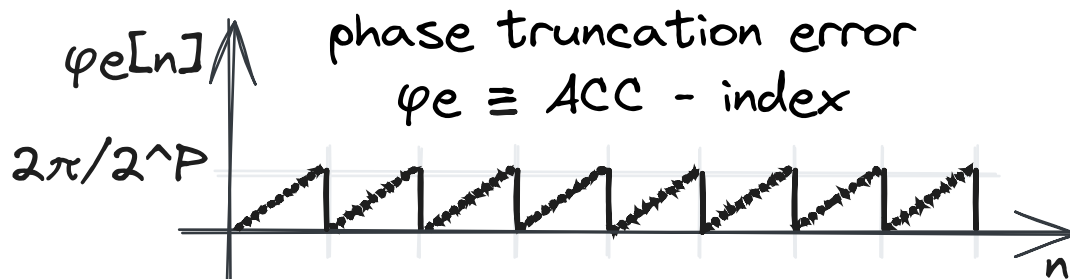
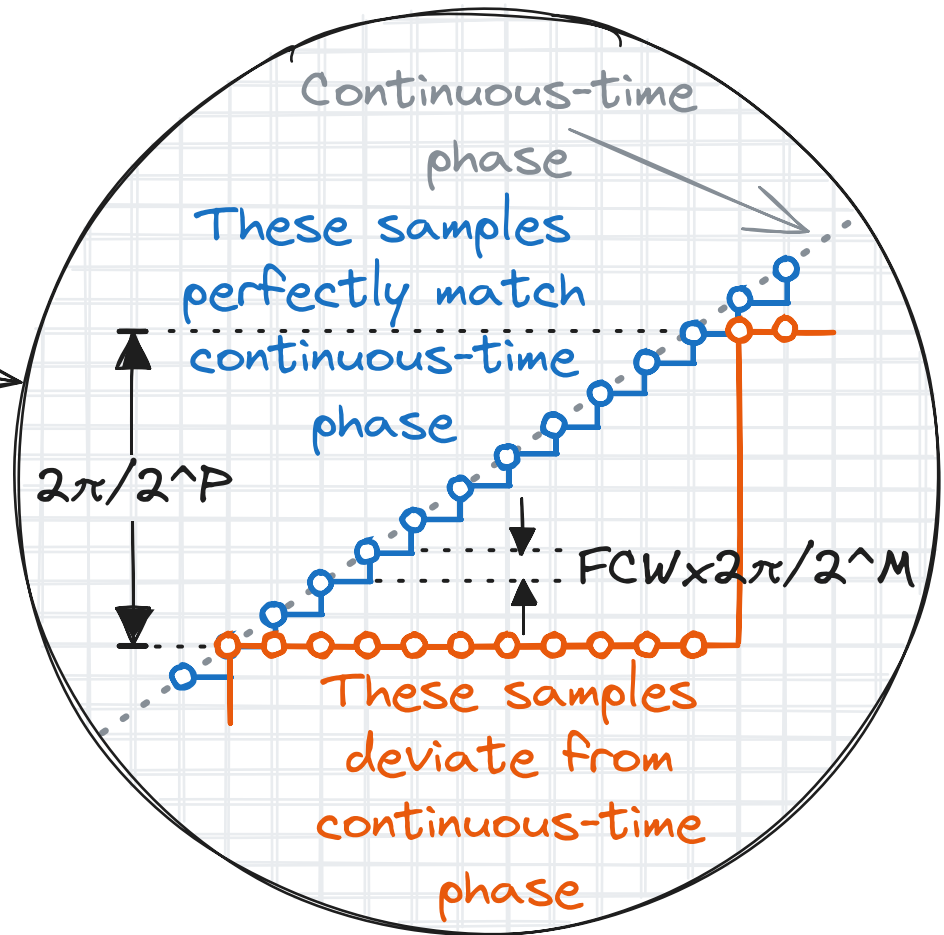
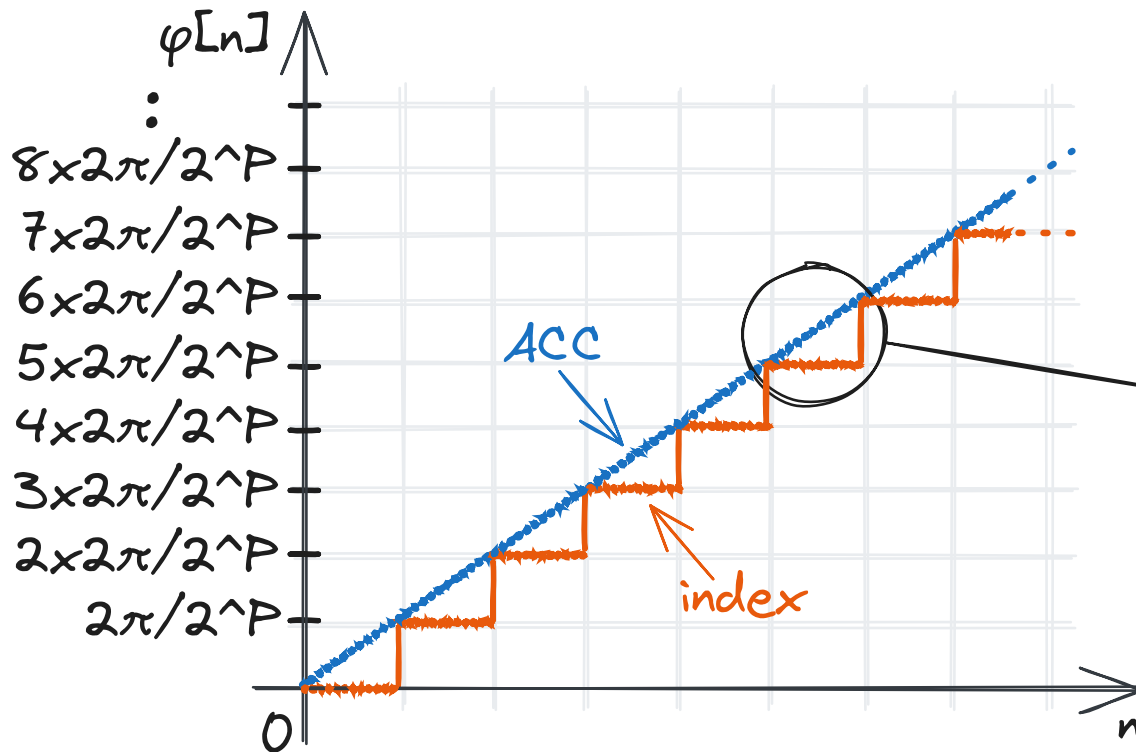
Phase Truncation

Example: $M = 5, P = 3, \text{FCW} = 3$



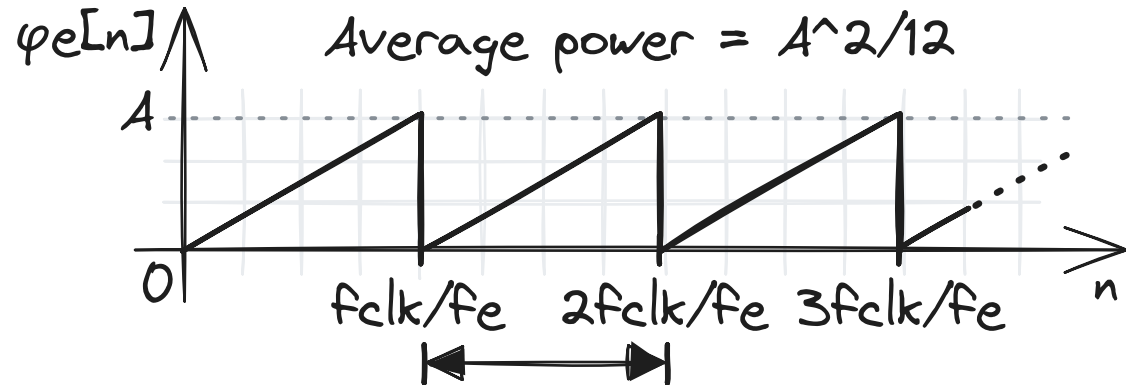
Phase truncation error is a sawtooth waveform

Worst-case (max.) peak-to-peak sawtooth amplitude = $2\pi/2^P$



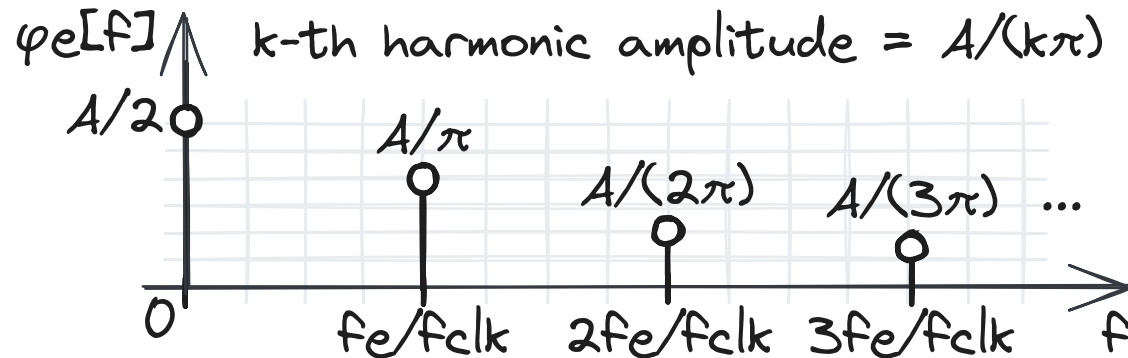
Let's examine the truncation error sequence $\varphi_e[n]$

Time domain



Fundamental period f_{clk}/f_e depends on FCW

Frequency domain

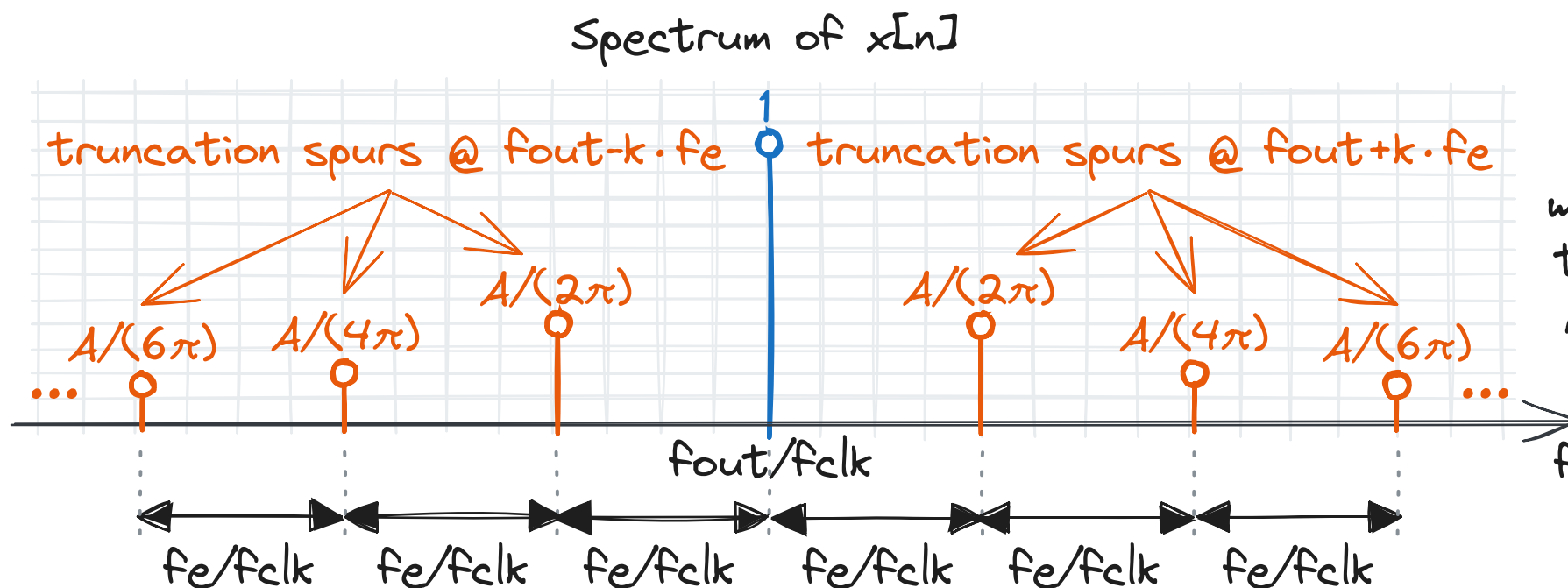


The generated sinusoid now has a phase error term $\varphi_e[n]$ that causes spurs

$$x[n] = \sin(2\pi \times f_{out}/f_{clk} \times n + \varphi_e[n])$$

Expanding the sum of angles and assuming $\varphi_e[n]$ is small

$$x[n] = \underbrace{\sin(2\pi \times f_{out}/f_{clk} \times n)}_{\text{desired sinusoid}} + \underbrace{\varphi_e[n] \times \cos(2\pi \times f_{out}/f_{clk} \times n)}_{\text{phase truncation error } x_e[n]}$$



Note:
Spurs
beyond
 $f_{clk}/2$
will alias
to first
Nyquist
zone

Spurious free dynamic range (SFDR) is the ratio of desired signal to highest spur

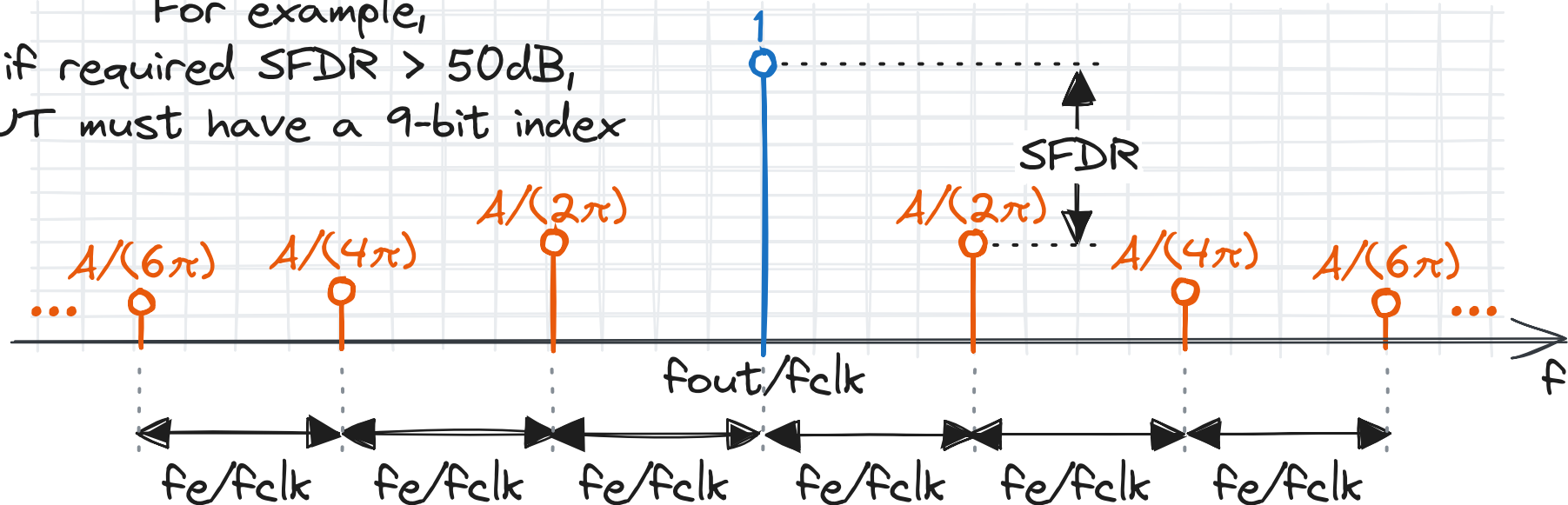
$$\text{SFDR} = 1/(A/(2\pi))$$

Worst-case (min.) SFDR corresponds to max. A which is $2\pi/2^P$

$$\text{SFDR} = 6 \times P \text{ [dB]}$$

Spectrum of NCO output

For example,
if required SFDR > 50dB,
LUT must have a 9-bit index



We can also calculate SNR which is the ratio of desired signal to all spurs

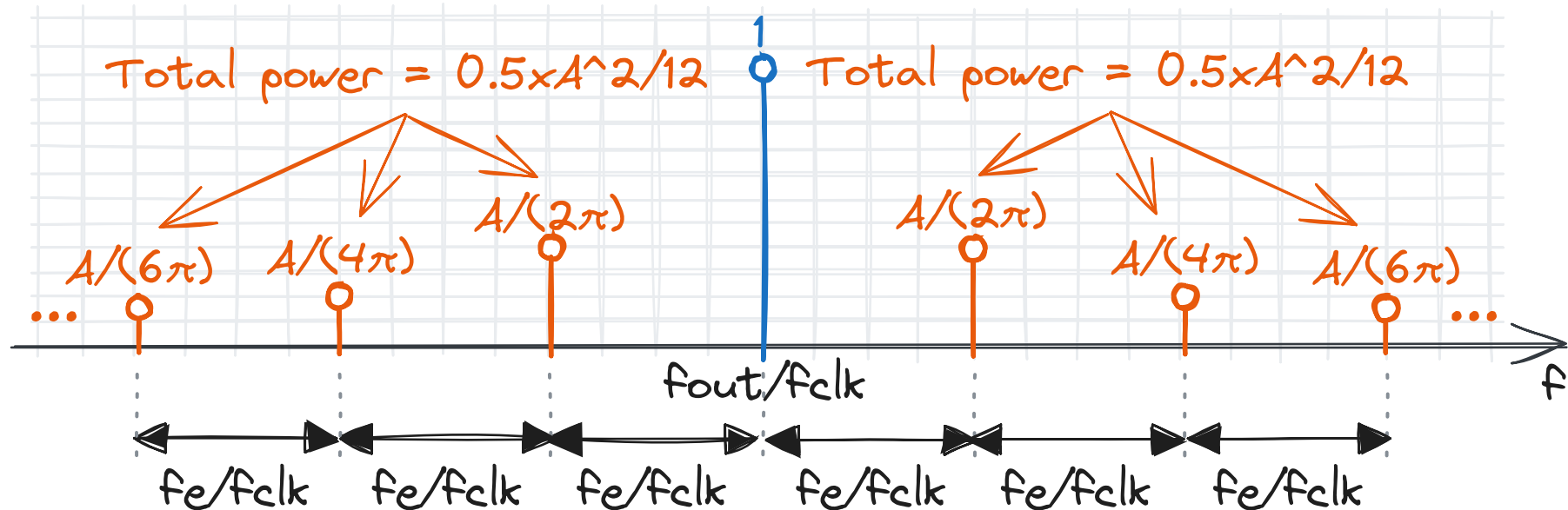
Assuming $\varphi_e[n]$ and quadrature signal are uncorrelated

$$SNR = 1/(A^2/12)$$

Worst-case (min.) SNR corresponds to max. A which is $2\pi/2^P$

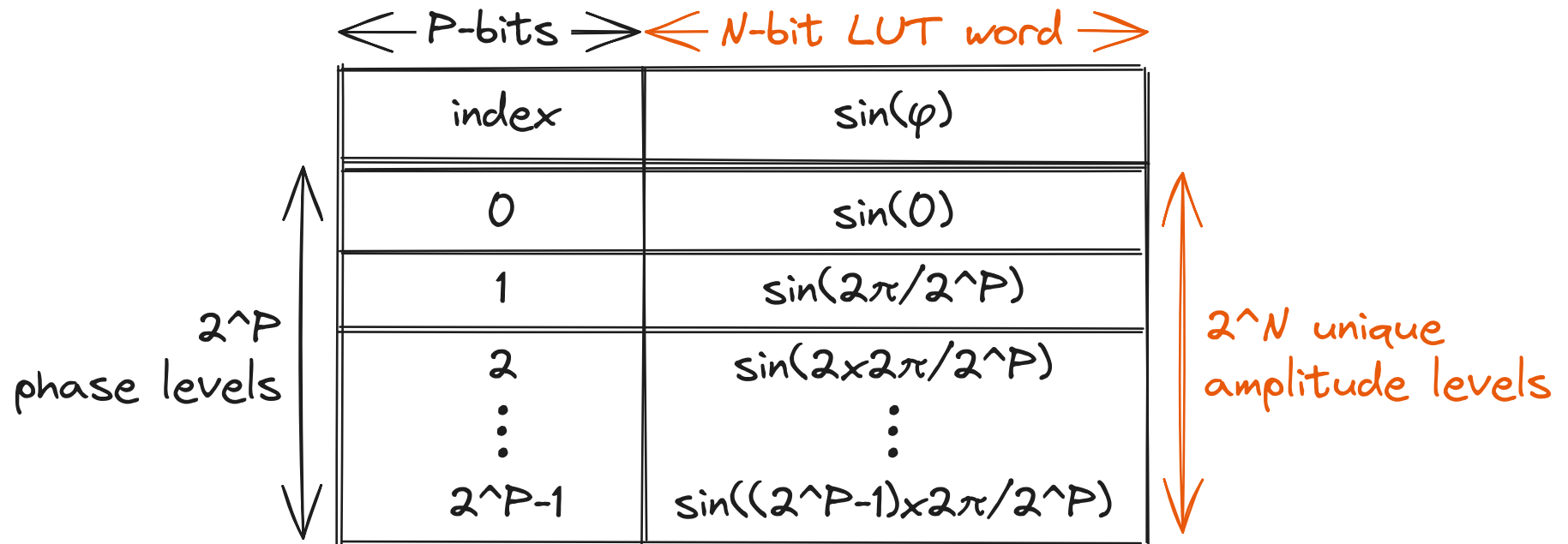
$$SNR_P = 6.02 \times P - 5.17 \text{ [dB]}$$

Spectrum of NCO output



Amplitude Quantization

Finite LUT word length causes amplitude quantization



If $N < P$, some amplitude levels are repeated

For example, if $N = P - 1$, there is one $\sin(\varphi)$ value for every 2 index values

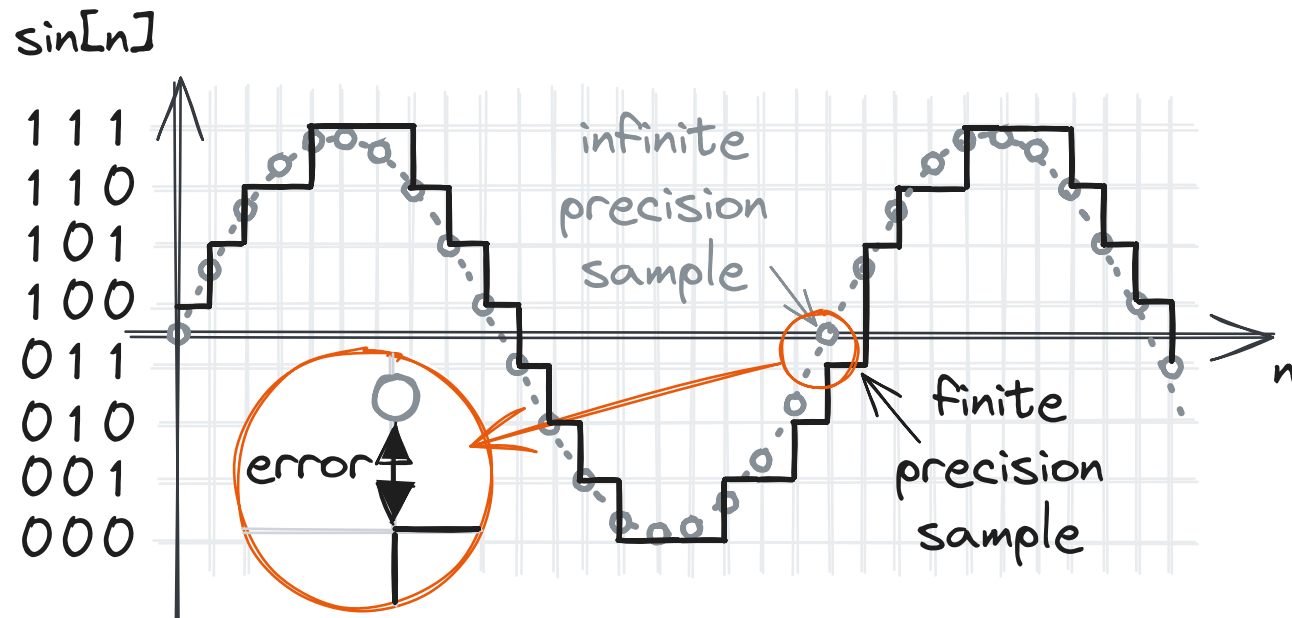
Amplitude Quantization

Amplitude quantization error is similar to DAC/ADC quantization noise
So, for an N -bit LUT word length, the familiar SNR relationship applies

$$SNR_A = 6.02N + 1.76 \text{ [dB]}$$

Example:

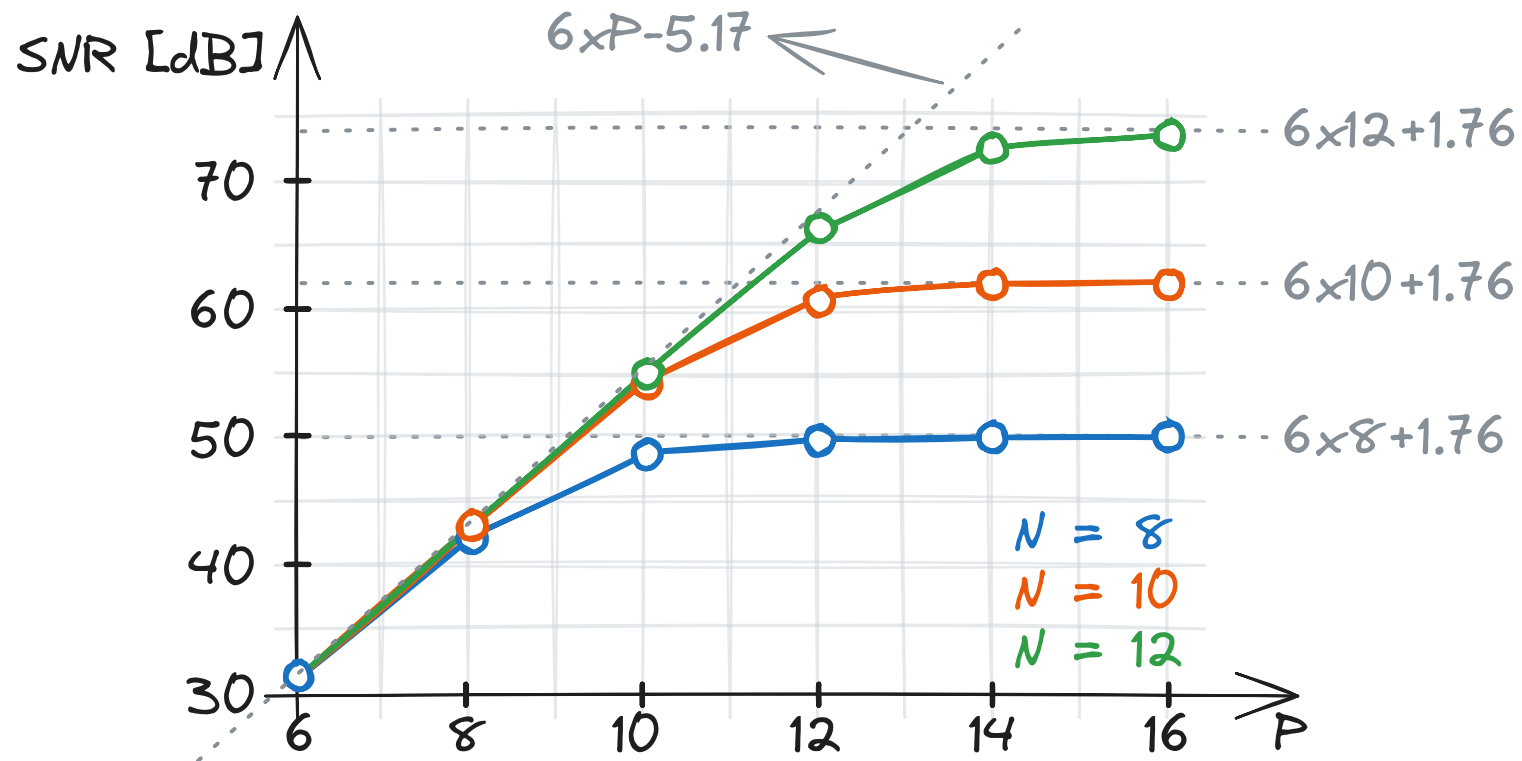
$N = 3 \rightarrow 2^3$ quantization levels $\rightarrow SNR = 19.8\text{dB}$



Phase truncation and amplitude quantization together determine signal quality

Total SNR is the uncorrelated sum of both types of errors

$$1/\text{SNR} = 1/\text{SNR}_A + 1/\text{SNR}_P$$



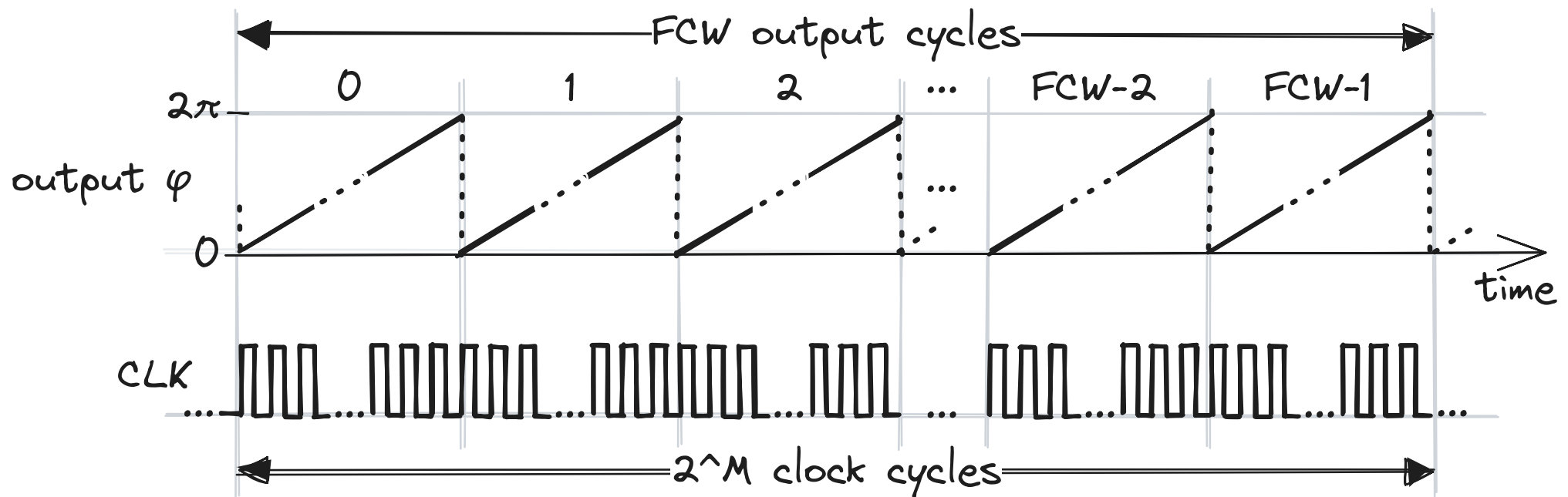
The NCO as a frequency divider

We can re-write the input-output frequency relation of an NCO

$$FCW/f_{out} = 2^M/f_{clk}$$

The above tells us that clocking an M -bit ACC fits 2^M clock cycles into FCW output cycles, for any value of FCW

From this perspective, the NCO is a frequency divider

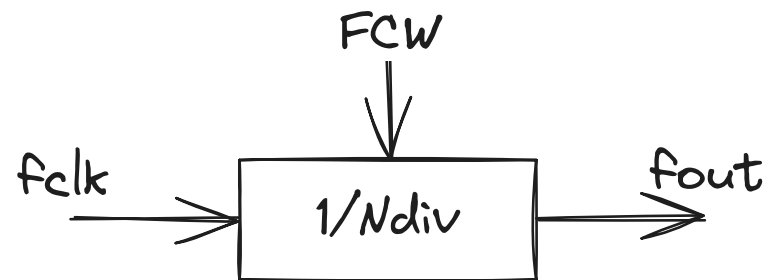


The NCO as a frequency divider

The division ratio is programmable via FCW

$$f_{out} = f_{clk}/N_{div}$$

$$N_{div} = 2^M/FCW$$



The NCO is a divider capable of integer & fractional division

For an M -bit ACC, there are $2^{(M-1)}$ alias-free FCW values

Of those, only M FCW values ($2^0, 2^1, 2^2 \dots 2^{(M-1)}$) result in integer division

All other FCW values (the majority) result in fractional division

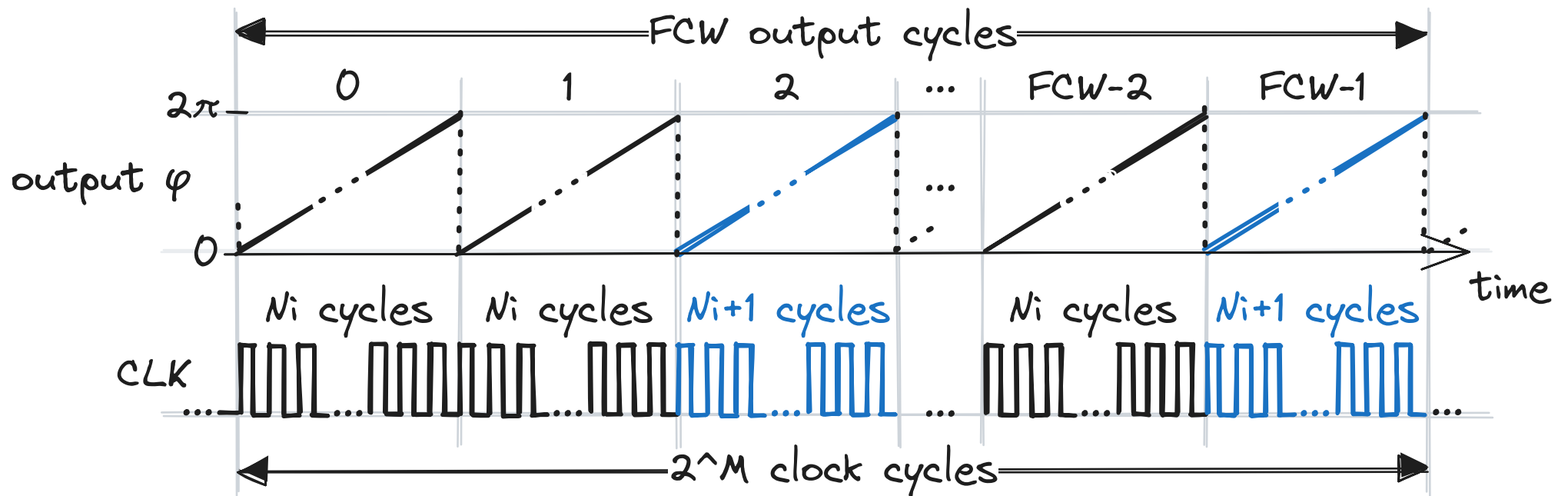
The NCO as a frequency divider

So, generally, division ratio has an integer part N_i and a fractional part K/FCW

$$N_{div} = N_i + K/FCW$$

Fractional division is achieved on "average" over FCW output cycles

The NCO divides by N_i for $FCW-K$ output cycles and by N_i+1 for K output cycles



The NCO as a frequency divider

Example:

$$M = P = 5, \text{FCW} = 7$$

$$N_{\text{div}} = 2^5/7 = 4 + 4/7$$

Divide by 4 for
3 out of 7 cycles

Divide by 5 for
4 out of 7 cycles

Output cycle #	ACC	# of clk cycles
0	0, 7, 14, 21, 28,	5
1	3, 10, 17, 24, 31,	5
2	6, 13, 20, 27,	4
3	2, 9, 16, 23, 30,	5
4	5, 12, 19, 26,	4
5	1, 8, 15, 22, 29	5
6	4, 11, 18, 25,	4
7	0, 7, ..	5
⋮		⋮

↑
7
output
cycles
↓

division
cycle
repeats ←

↑
2⁵
clk
cycles
↓

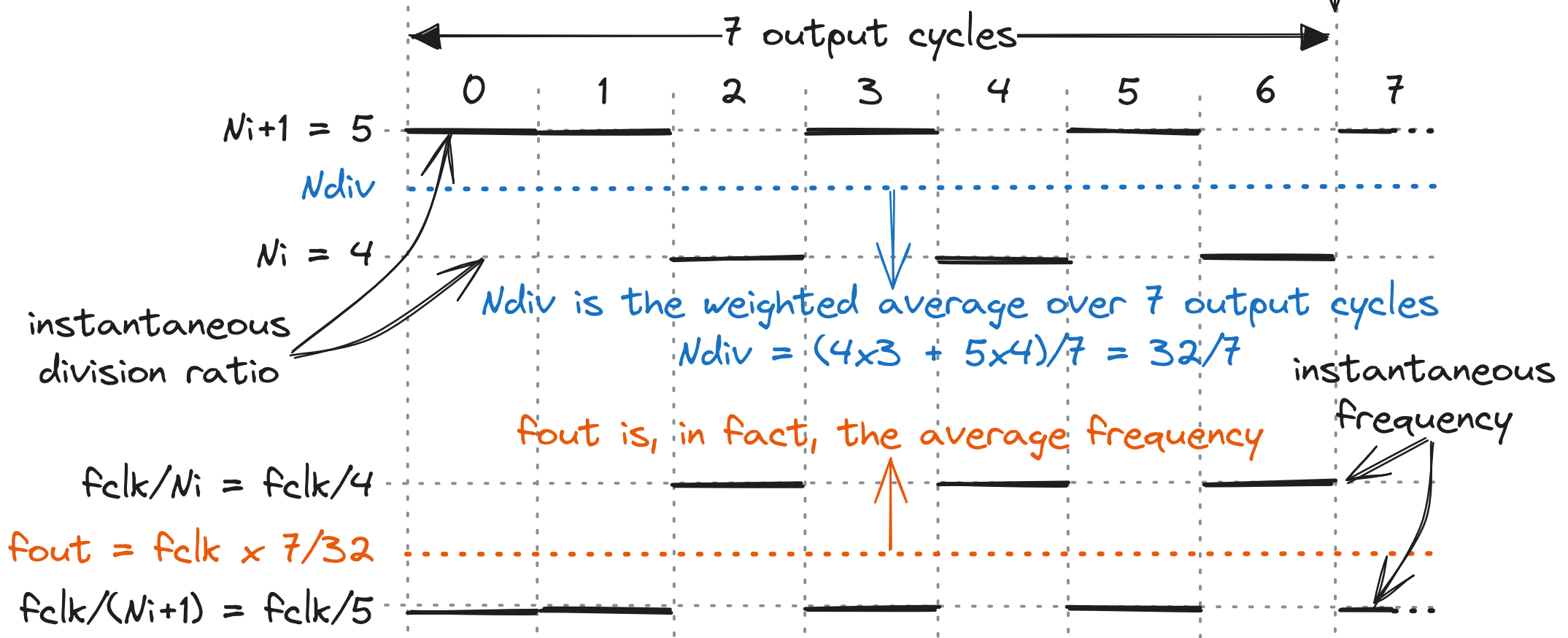
The NCO as a frequency divider

Example:

$$M = P = 5, \text{FCW} = 7$$

$$N_{\text{div}} = 2^5/7 = 32/7$$

division cycle repeats

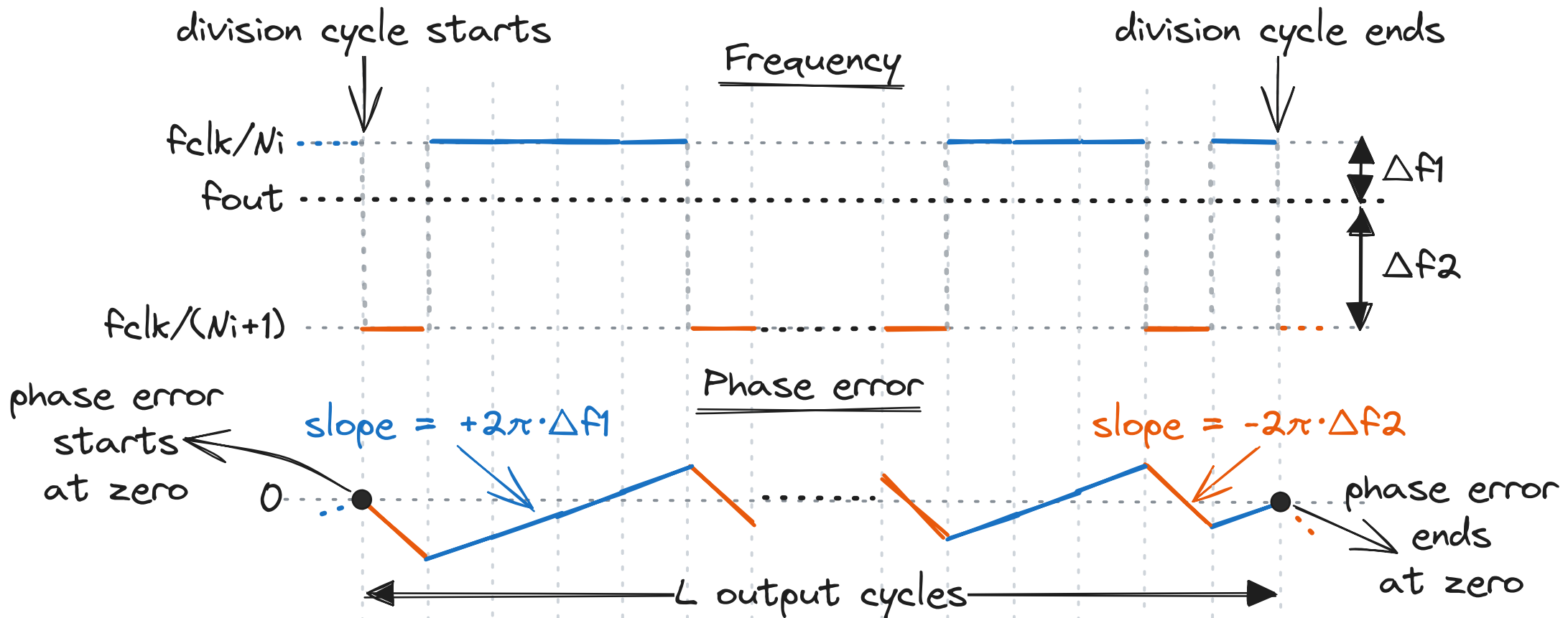


The NCO as a frequency divider

Difference between instantaneous & average frequency results in phase error

As we already know, phase error translates to output spurs

Phase error has a period of L/f_{out} \rightarrow spurs at harmonics of f_{out}/L



The NCO as a frequency divider

We can calculate spur frequencies by finding the phase error period L

How many clock cycles are in those L output cycles?

Remember that over the same L output cycles, ACC pattern also repeats

We also know that for an M -bit ACC, L can't exceed 2^M clock cycles ($FCW = 1$)

So, if FCW has a common divisor with 2^M , L is $< 2^M$ clock cycles

And if FCW has no common divisor with 2^M , $L = 2^M$ clock cycles

The greatest common divisor is $GCD(FCW, 2^M)$

And we call the number of clock cycles in L the grand repetition rate (GRR)

$$GRR = 2^M / GCD(FCW, 2^M)$$

Which results in spur frequencies at

$$f_{spur} = k \times GCD(FCW, 2^M) / 2^M \times f_{clk} \quad k = 0, 1, 2, \dots$$

These spurs occur even without any phase truncation between ACC to LUT

The NCO as a frequency divider

Example 1:

$$M = P = 5, FCW = 7$$

$$f_{out} = 7/32 \times f_{clk}$$

$$GRR = 2^5 / \text{GCD}(2^5, 7) = 32 \text{ clock cycles}$$

$$f_{spur} = 0, f_{clk}/32, 2 \times f_{clk}/32, 3 \times f_{clk}/32 \dots \text{etc.}$$

Example 2:

$$M = P = 8, FCW = 6$$

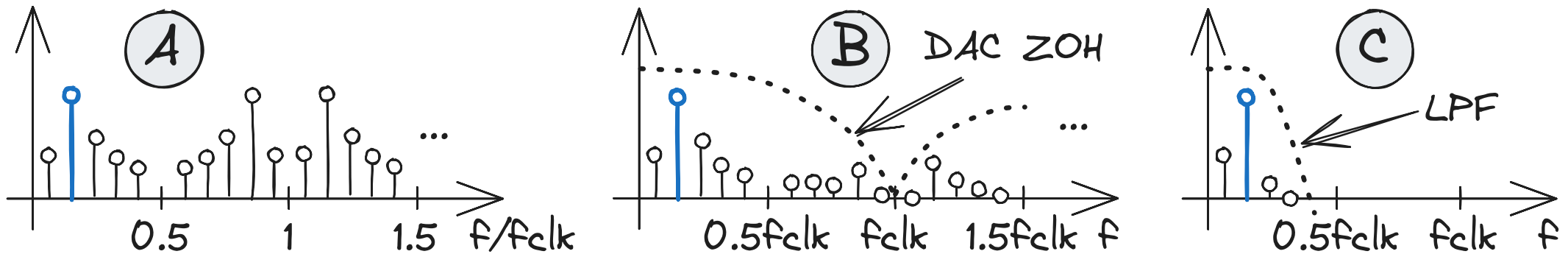
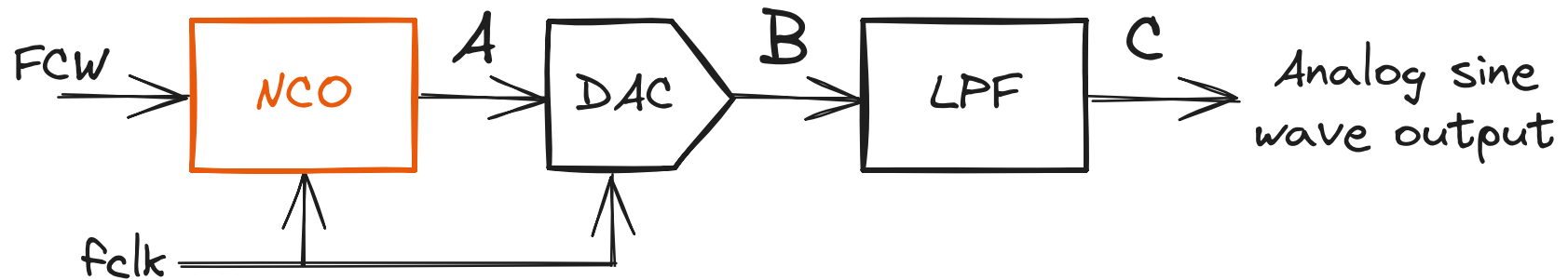
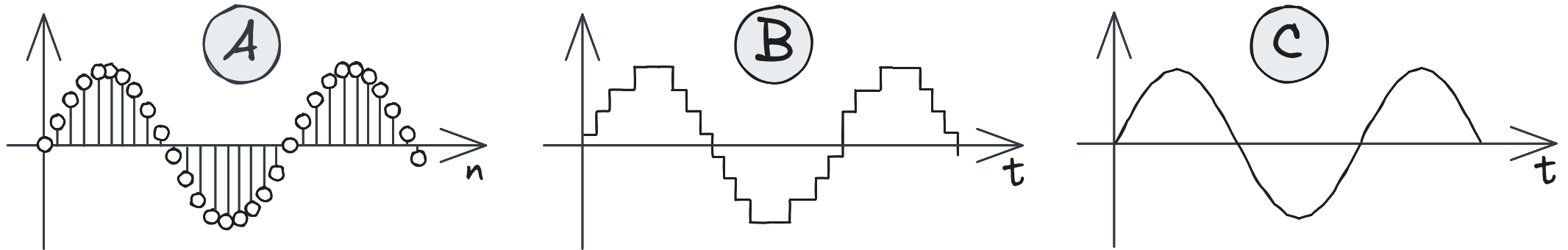
$$f_{out} = 6/256 \times f_{clk} = 3/128 \times f_{clk}$$

$$GRR = 2^8 / \text{GCD}(2^8, 6) = 128 \text{ clock cycles}$$

$$f_{spur} = 0, f_{clk}/128, 2 \times f_{clk}/128, 3 \times f_{clk}/128 \dots \text{etc.}$$

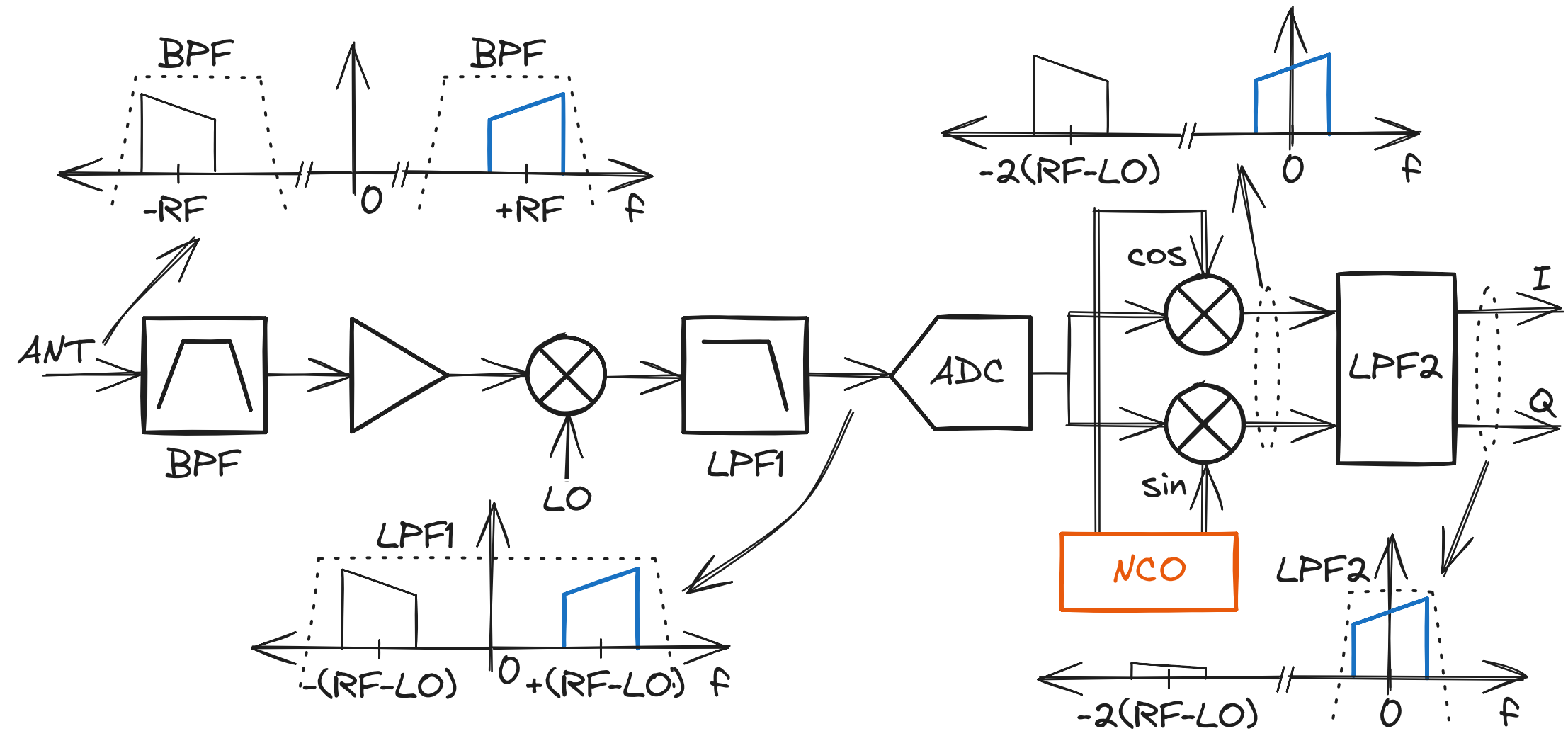
Applications of NCOs

Direct digital synthesis (DDS) of analog reference signal



Applications of NCOs

Digital IQ downconversion in wireless receivers



Applications of NCOs

Carrier synchronization in wireless receivers

