ELECENG 3EJ4 Lab 1

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Part 1

Q1. The data from these plots indicate that the NPN (in both simulation and in measured experimentation) operates in the active region for V_{CC} between 0.5 V to 5 V when the value of V_E is between -5 V and -1 V. The $i_c - V_{CE}$ characteristics of the NPN in this region is generally linear, which is the expected behaviour of a BJT in the active region. The plots for simulated and measured I_C vs. V_{CE} characteristics are shown in Figure 1.

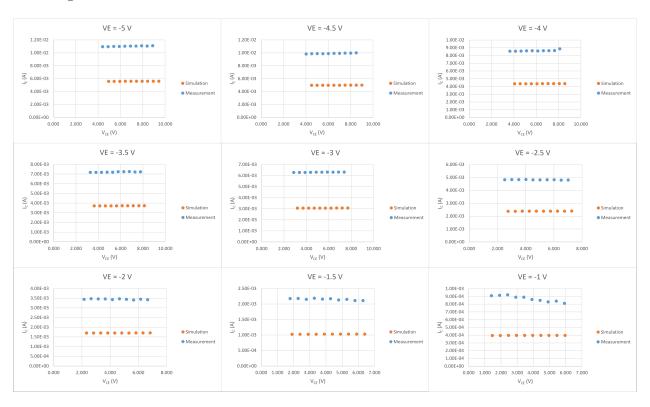


Figure 1: I_C vs. V_{CE} for V_{CC} between 0.5 V and 5 V at various values of V_E for NPN

Q2. The values determined for β , $V_{BE_{on}}$, $|V_A|$, g_m , r_{π} , and r_o in reference V_{CE} in simulation and in measured experiments were generally found to be similar to the expected values for these characteristics. This was verified by comparing these values with the parameters in the SPICE model for the part provided by the manufacturer. The plots for the simulated and measured characters are shown in Figure 2.

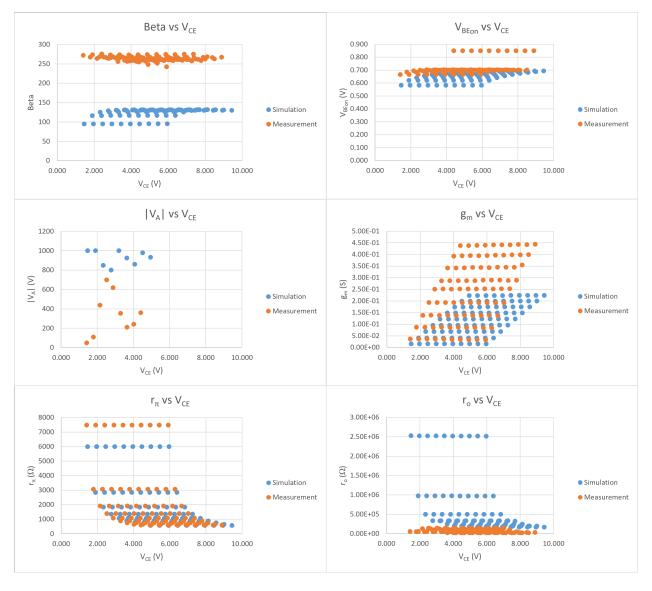


Figure 2: β , $V_{BE_{on}}$, $|V_A|$, g_m , r_π , r_o vs V_{CE} plots for NPN

Q3. In general, there were no discrepancies between the simulated and measured data; they displayed the similar behaviours in the majority of plots in Figures 1 and 2. The only differences were generally slight shifts between the simulated and measured data, which can be due to a number of factors such as tolerances in the physical components and inaccuracies in the measurements taken by the AD2 board.

Part 2

Q4. The data from these plots indicate that the PNP (in both simulation and in measured experimentation) operates in the active region for V_{CC} between -5 V to -0.5 V when the value of V_E is between 5 V and 1 V. The $i_c - |V_{CE}|$ characteristics of the PNP in this region is generally linear, which is the expected behaviour of a BJT in the active region. he plots for simulated and measured I_C vs. $|V_{CE}|$ characteristics are showed in Figure 3.

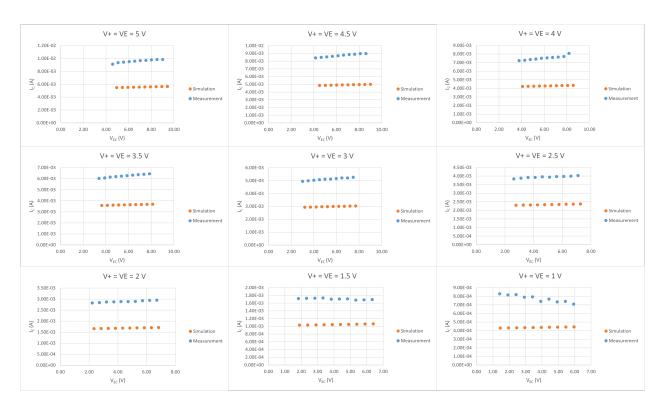


Figure 3: I_C vs. $|V_{CE}|$ for V_{CC} between -0.5 V and -5 V at various values of V_E for PNP

Q5. The values determined for β , $V_{EB_{on}}$, $|V_A|$, g_m , r_π , and r_o in reference $|V_{CE}|$ in simulation and in measured experiments were generally found to be similar to the expected values for these characteristics. This was verified by comparing these values with the parameters in the SPICE model for the part provided by the manufacturer. The plots for the simulated and measured characters are shown in Figure 4.

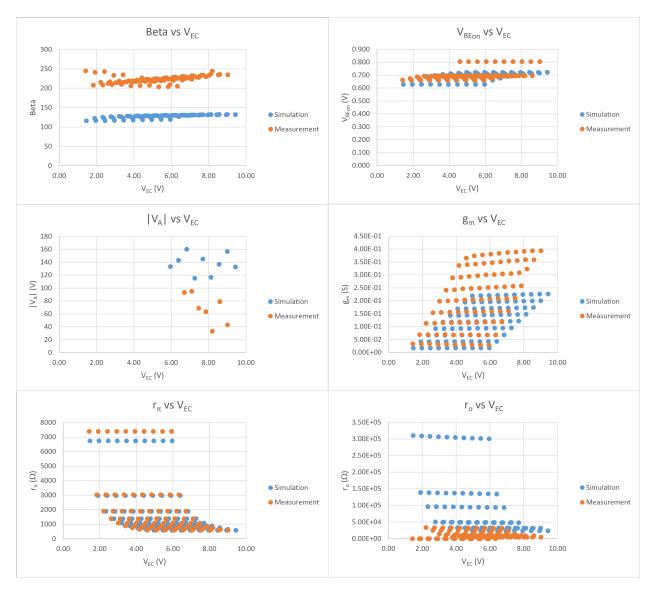


Figure 4: β , $V_{EB_{on}}$, $|V_A|$, g_m , r_π , r_o vs V_{CE} plots for PNP

Q6. In general, there were no discrepancies between the simulated and measured data; they displayed the similar behaviours in the majority of plots in Figures 3 and 4. The only differences were generally slight shifts between the simulated and measured data, which can be due to a number of factors such as tolerances in the physical components and inaccuracies in the measurements taken by the AD2 board.

Part 3

Q7.

$$I_{E} = I_{B} + I_{C}$$

$$I_{C} = \beta I_{B}$$

$$I_{E} = (1 + \beta)I_{B}$$

$$V_{BE} = V_{B} - V_{E}$$

$$V_{B} = V_{BB} - I_{B}R_{BB}$$

$$V_{E} = V_{EE} + I_{E}R_{3}$$

$$V_{E} = V_{EE} + (1 + \beta)I_{B}R_{3}$$

$$V_{BE} = V_{BB} - I_{B}R_{BB} - V_{EE} - (1 + \beta)I_{B}R_{3}$$

$$I_{B}R_{BB} + (1 + \beta)I_{B}R_{3} = V_{BB} - V_{EE} - V_{BE}$$

$$I_{B} = \frac{V_{BB} - (V_{EE} + V_{BE_{on}})}{R_{BB} + (1 + \beta)R_{3}}$$
(1)

- Q8. The difference between equation (1) derived in Q7 and the equation (1.3) derived in the pre-lab is the inclusion of $(1 + \beta)R_3$ in the denominator. The additional term in the denominator increases the value of the denominator, leading to changes in the numerator (such as the change in the power supply voltage, ΔV_{EE}) causing smaller changes in the base current, I_B .
- **Q9.** The π model for the circuit is shown below in Figure 5. The derivation of the output resistance is found below the figure.

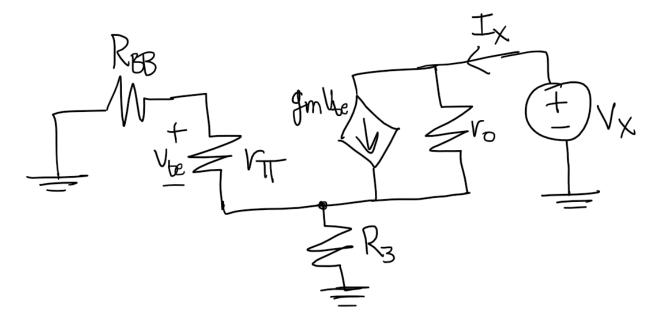


Figure 5: π model for circuit

$$R_{o} = \frac{V_{x}}{I_{x}}$$

$$V_{x} = (R_{3} \parallel (R_{BB} + r_{\pi}))I_{x} + (I_{x} - g_{m}V_{BE})r_{o}$$

$$V_{BE} = \frac{r_{\pi}}{R_{BB} + r_{\pi}} \left[-I_{x}(R_{3} \parallel (R_{BB} + r_{\pi})) \right]$$

$$V_{x} = (R_{3} \parallel (R_{BB} + r_{\pi}))I_{x} + (I_{x} - g_{m} \left[\frac{r_{\pi}}{R_{BB} + r_{\pi}} \left[-I_{x}(R_{3} \parallel (R_{BB} + r_{\pi})) \right] \right] r_{o}$$

$$V_{x} = I_{x}((R_{3} \parallel (R_{BB} + r_{\pi})) + r_{o} + g_{m}r_{o} \left[\frac{r_{\pi}}{R_{BB} + r_{\pi}} (R_{3} \parallel (R_{BB} + r_{\pi})) \right] \right)$$

$$R_{o} = \frac{V_{x}}{I_{x}} = r_{o} + [R_{3} \parallel (R_{BB} + r_{\pi})] \left[1 + g_{m}r_{o} \left(\frac{r_{\pi}}{R_{BB} + r_{\pi}} \right) \right]$$

$$(2)$$

Q10. To account for the increase in $V_{o,min}$ caused by the insertion of the feedback R_3 at the emitter of the BJT, we add the voltage drop across the feedback resistor R_3 (I_ER_3), to the equation for $V_{o,min}$ provided in the lab.

$$V_{o,min} = V_{EE} + I_E R_3 + 0.3 (3)$$

Q11.

$$I_{o} = I_{c}$$

$$V_{o,min} = V_{EE} + I_{E}R_{3} + 0.3$$

$$I_{E}R_{3} = -V_{EE} + V_{o,min} - 0.3$$

$$R_{3} = \frac{-V_{EE} + V_{o,min} - 0.3}{I_{E}}$$

$$R_{3} = \frac{-V_{EE} + V_{o,min} - 0.3}{I_{E}} = \frac{-V_{EE} + V_{o,min} - 0.3}{I_{o}(1 + \frac{1}{\beta})}, \beta = 130$$

$$R_{3} = \frac{5 - 1 - 0.3V}{1.0077mA}$$

$$R_{3} = \frac{3.7V}{1mA}$$

$$R_{3} = 3.67k\Omega$$

This design was verified on PartSim with a DC sweep of V_{CC} with parameters $R_1 = 40k\Omega$, $R_2 = 500k\Omega$ and $V_{EE} = -5V$. The simulation active region current sink current was determined to be $997\mu A$, which is extremely close to the targeted value of 1mA. The simulation plot can be seen in Figure 6.

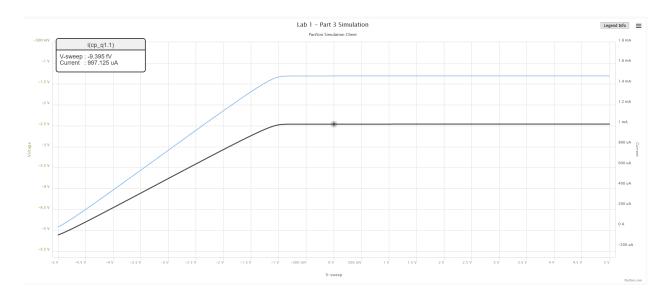


Figure 6: Plot of designed current sink current, I_o , verified to be approximately 1mA.

Q12. The value of $|V_{CE}|$ required for Q_1 to work in the active region was determined by plotting V_E and I_C vs V_{CC} with $R_1, R_2 = 100k\Omega$, $R_3 = 3.67k\Omega$, and $V_{EE} = -5V$. The active region was determined to have began at approximately $V_{CC} = -2.9V$, when $V_E = -3.22V$, this means the value of $|V_{CE}|$ required for Q_1 to operate in the active region was determined to be $|V_{CE}| > 0.32V$. The plots for the simulated V_E and I_C measurements can be seen in Figure 7.

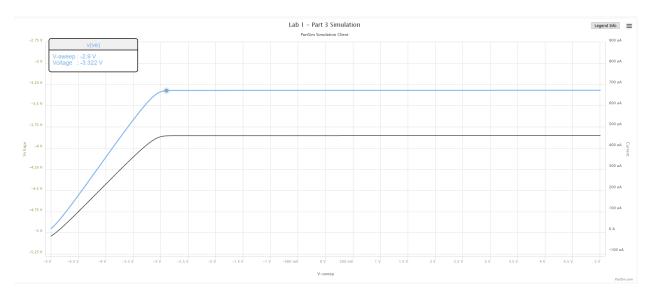


Figure 7: Plot of V_E and I_C vs V_{CC} for $R_1 = 100k\Omega$, $R_2 = 100k\Omega$, $R_3 = 3.67k\Omega$, $V_{EE} = -5V$