

# Design and Modeling of Fluid Power Systems

ME 597/ABE 591      Lecture 5

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# Displacement Machines



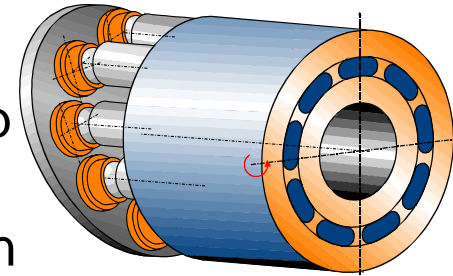
Study different design principles and learn about the following topics

Axial piston pump design solutions (swash plate and bent axis)

Radial piston pumps and motors – piston support

Gear Pumps – internal and external – axial and radial gap

Vane pumps – advantage and disadvantage of this design

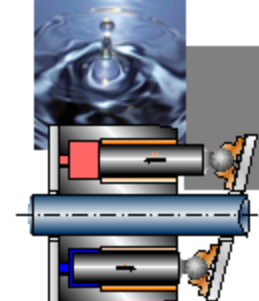
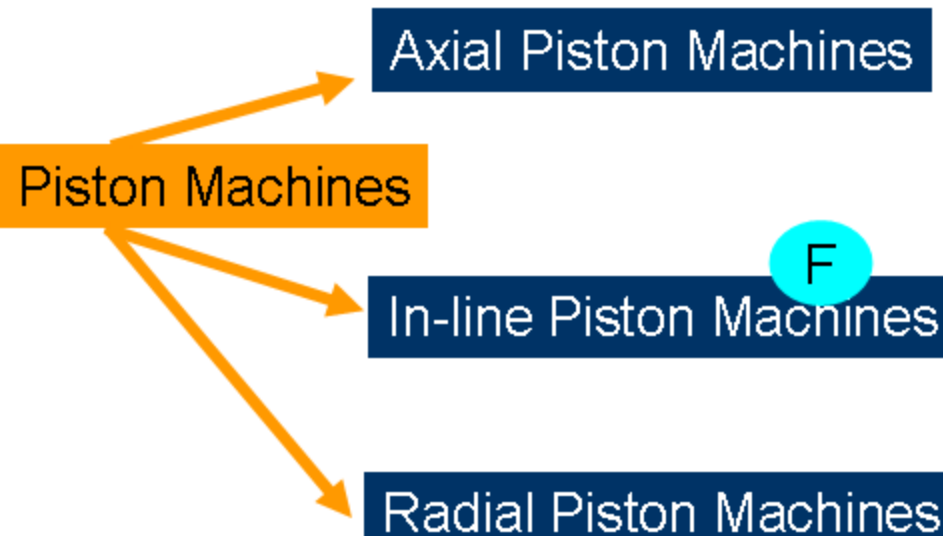


**Please study the appropriate chapters in**

**Ivantysyn, J. and Ivantysynova, M. (2001), *Hydrostatic Pumps and Motors*.  
Akademia Books International. New Dehli. ISBN-81-85522-16-2**

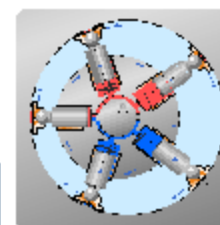
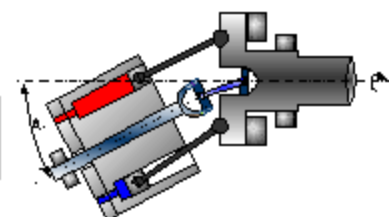
- Aim: - To be able to select the right design for your system application!**
- Knowledge about limitations of each basic design**
  - To apply models on system level for each design**

# Displacement Machines



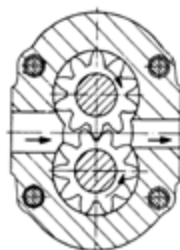
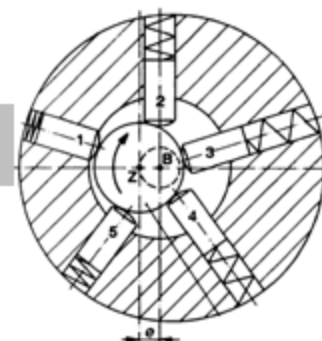
Swash Plate Machines

Bent Axis machines



with external piston support

with internal piston support

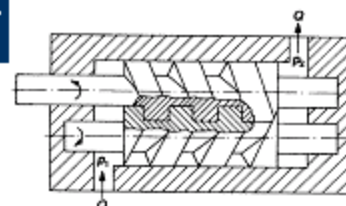
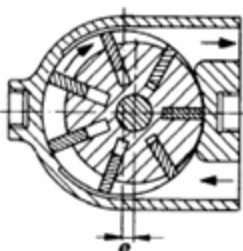


Internal Gear



Annual Gear

Vane Machines



**Screw Machines** **F**

others

Fixed displacement machines

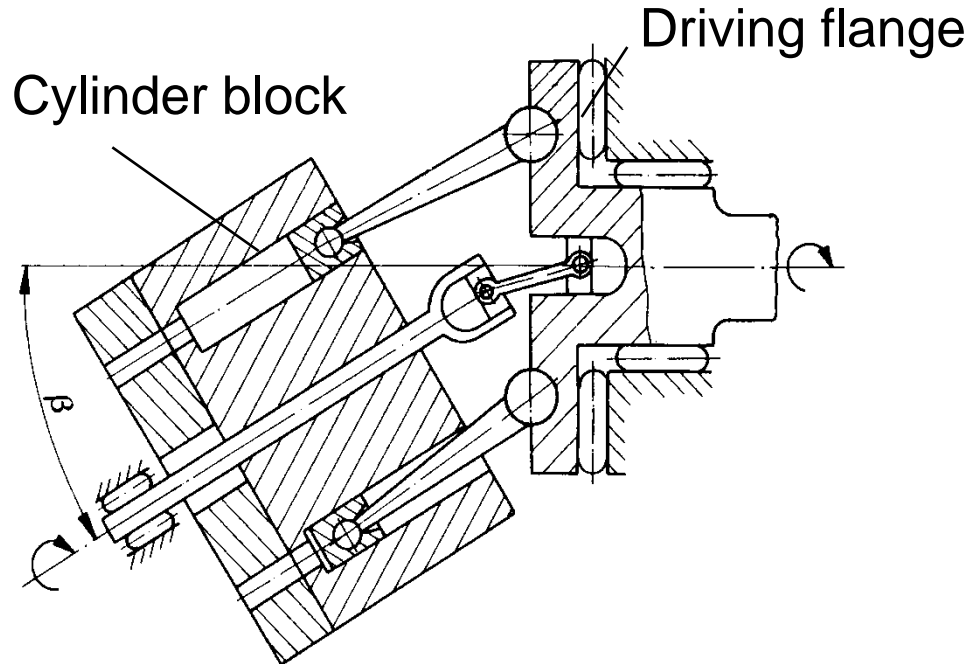


Variable displacement machines

# Bent axis axial piston pumps

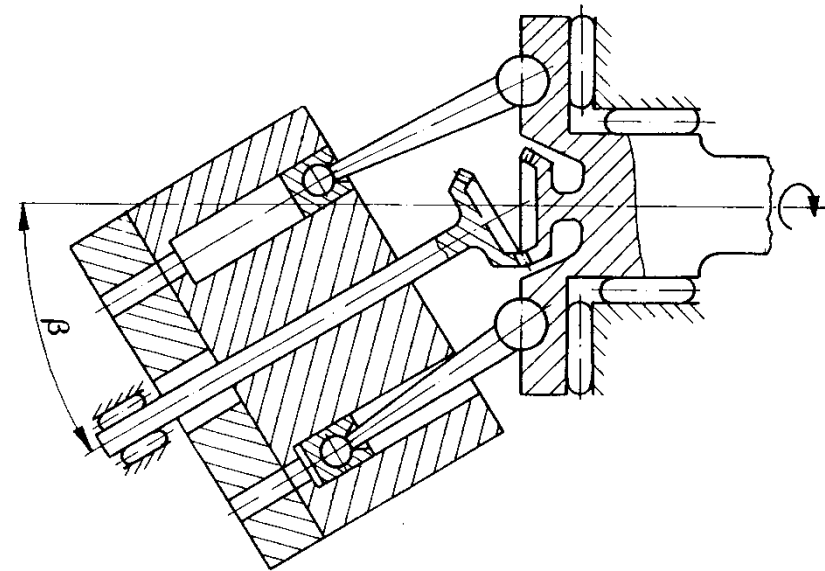


## Synchronization of cylinder block



Using a universal joint

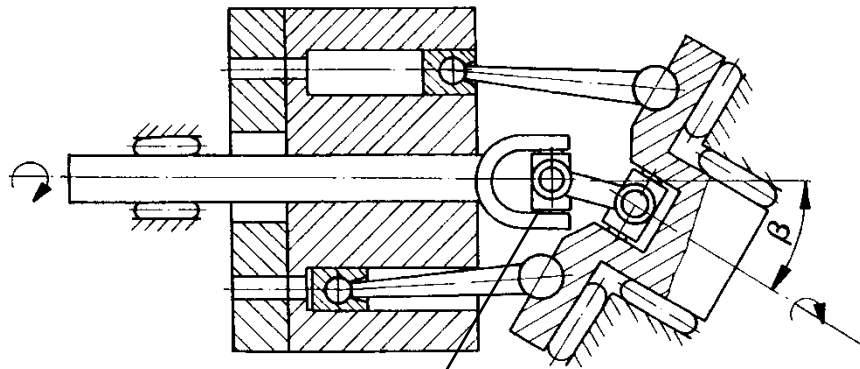
Using a bevel gear



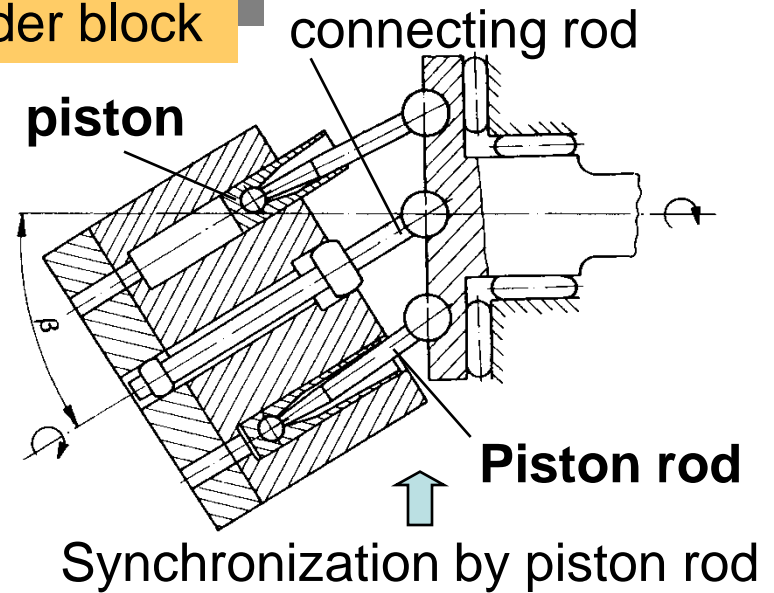
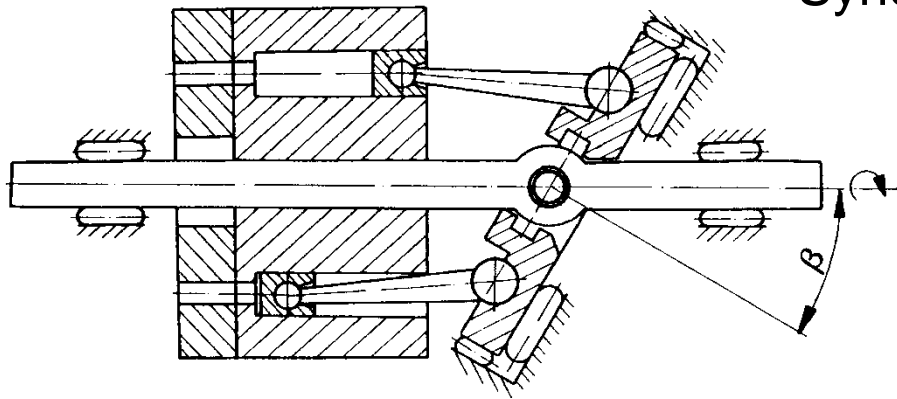
# Bent axis axial piston pumps



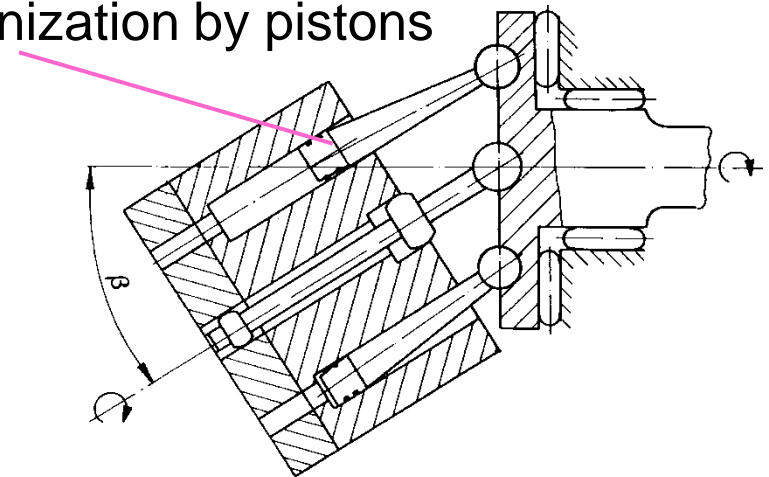
## Synchronization of cylinder block



Cardan joint



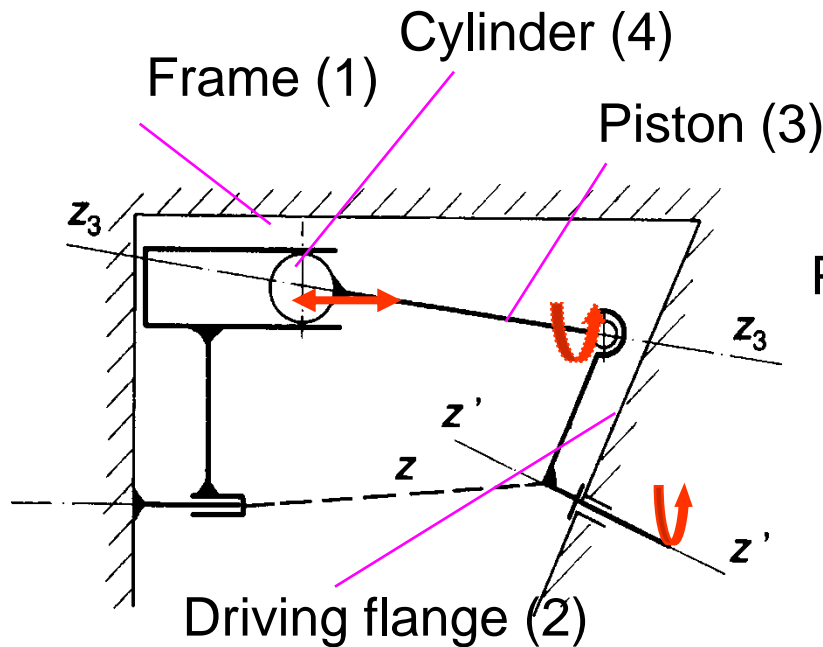
Synchronization by pistons



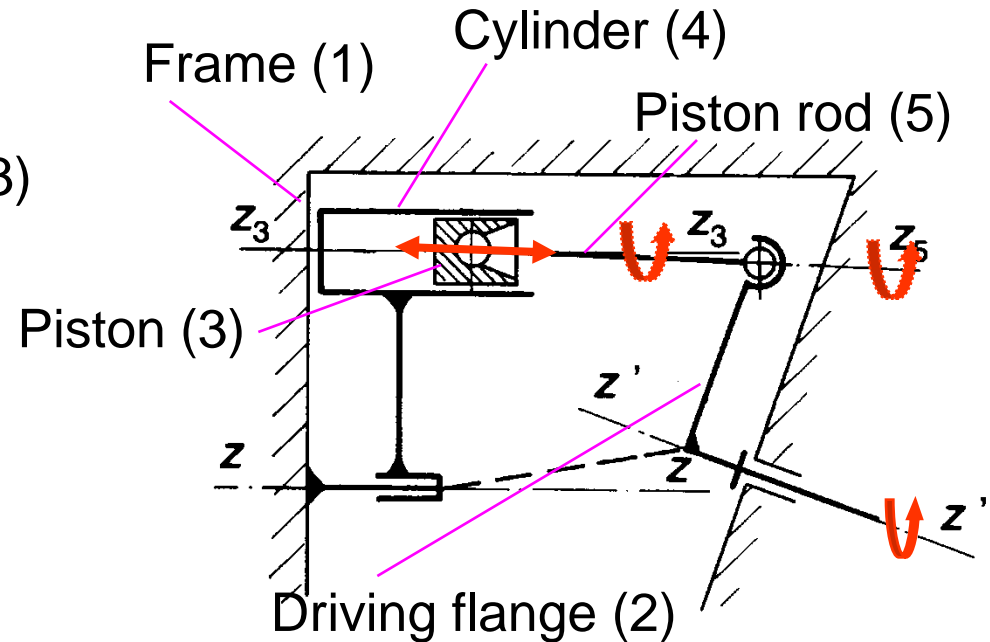
# Kinematics of bent axis pumps



## Four link 3D mechanism



## Five link 3D mechanism



Assuming a fixed connection between link 2 and link 4, achieved by synchronization

mechanism has finally two degrees of freedom

the mechanism has finally three degrees of freedom

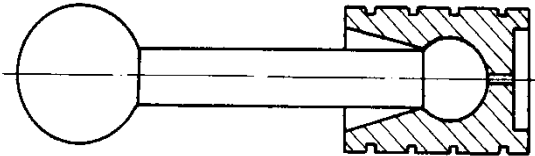
Piston can rotate about  $z_3$ -axis

Piston can rotate about  $z_3$ -axis and piston rod can rotate about  $z_5$ -axis

# Piston Design



Short piston with piston rod

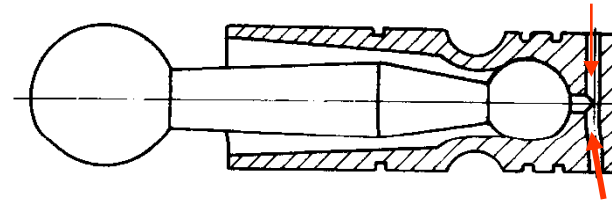


**Synchronization by  
universal joint or bevel gear**

Spherical piston with piston ring

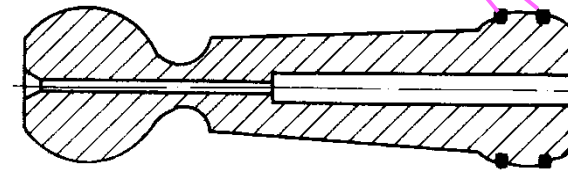


Long piston with piston rod



**Synchronization by  
pistons or piston rods**

Conical piston with piston rings

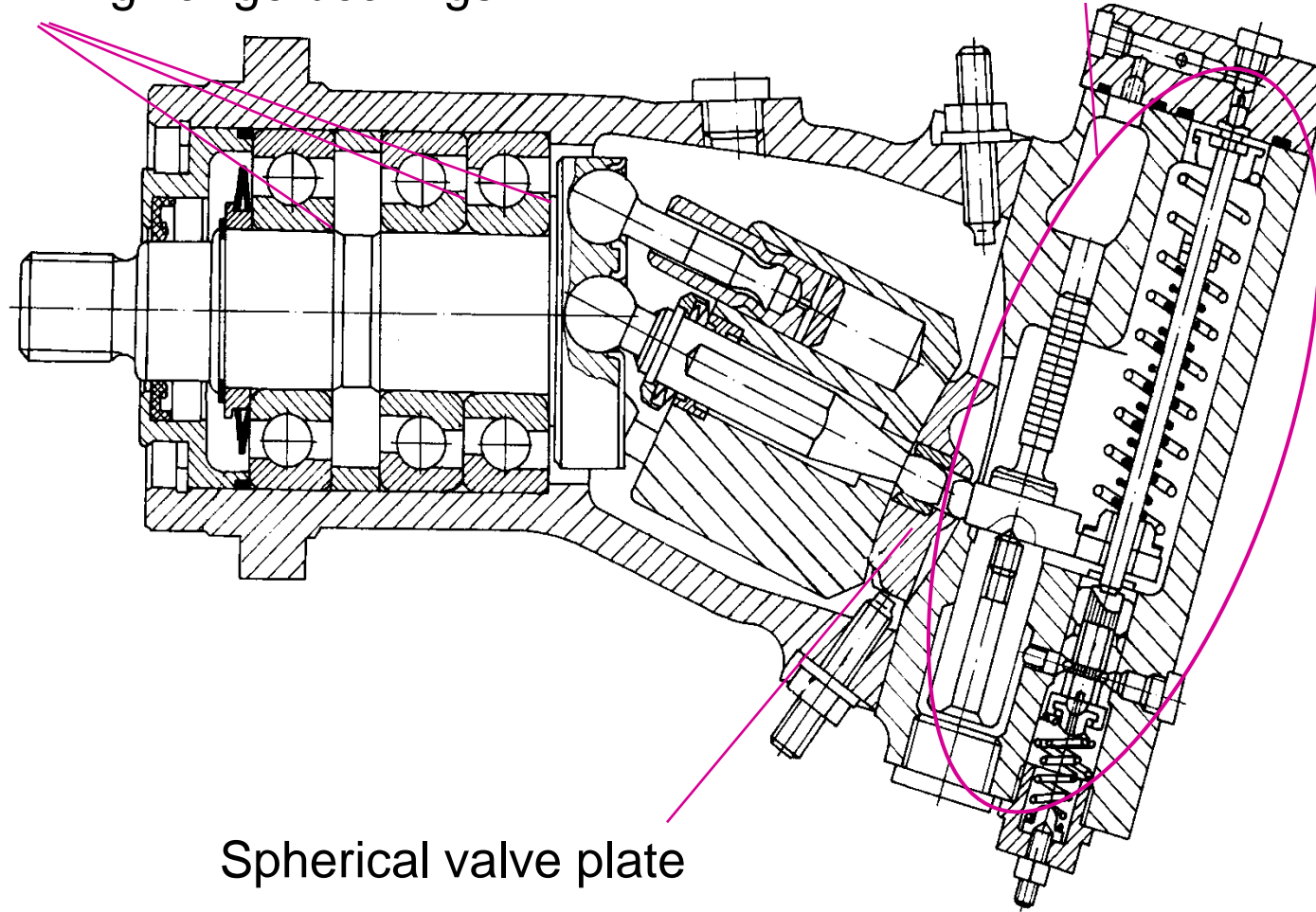


# Design Examples



Driving flange bearings

Pump control device



Spherical valve plate



# Design Examples

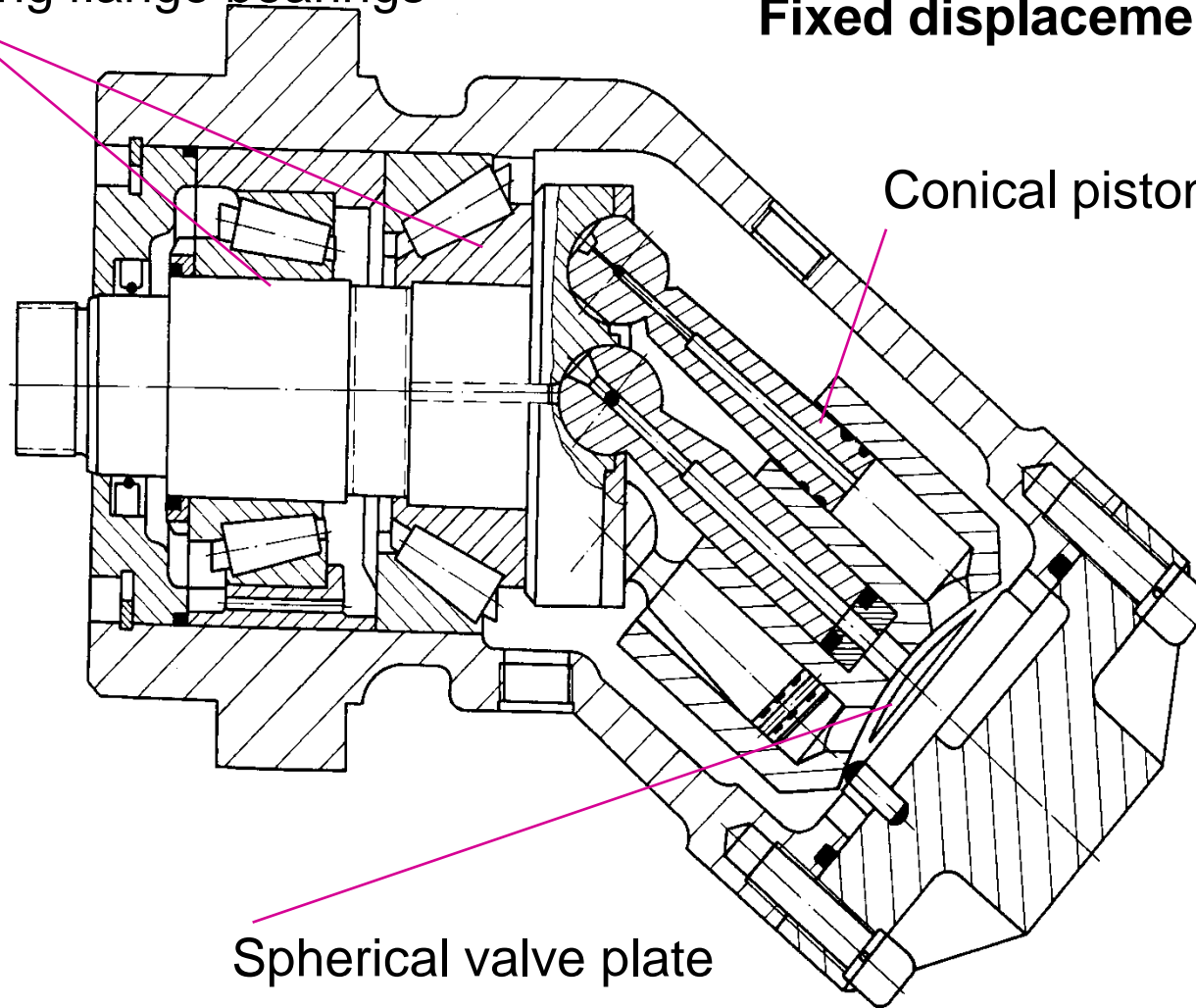


## Fixed displacement pump

Driving flange bearings

Conical piston

Spherical valve plate



# Radial Piston Pumps



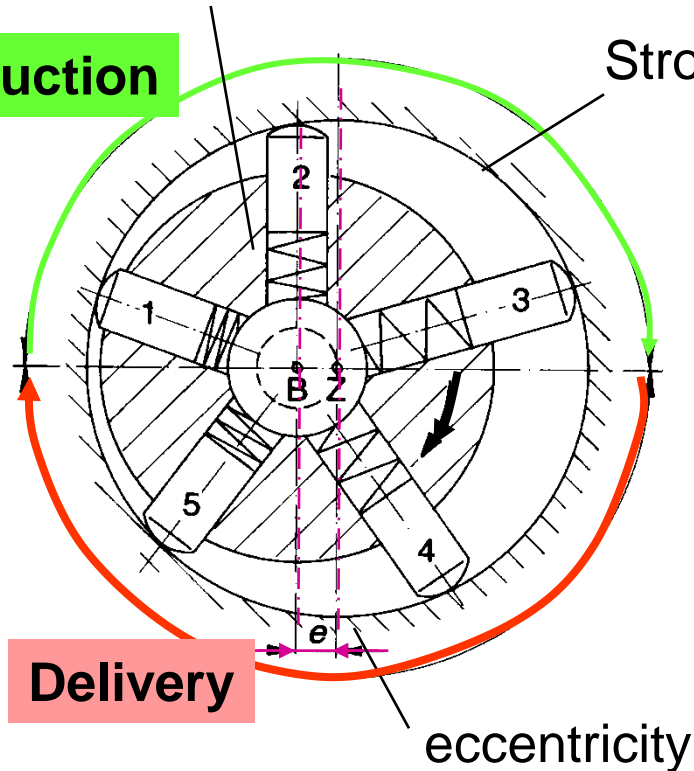
with external piston support

with internal piston support

Rotating cylinder body

Suction

Stroke ring



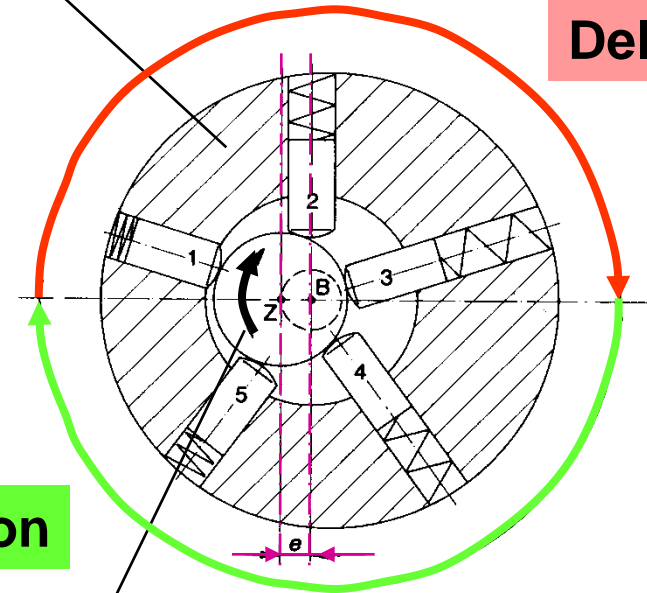
Delivery

eccentricity

Stationary cylinder body

Delivery

Suction



Rotating cam or crankshaft



Displacement volume adjustable by changing eccentricity  $e$

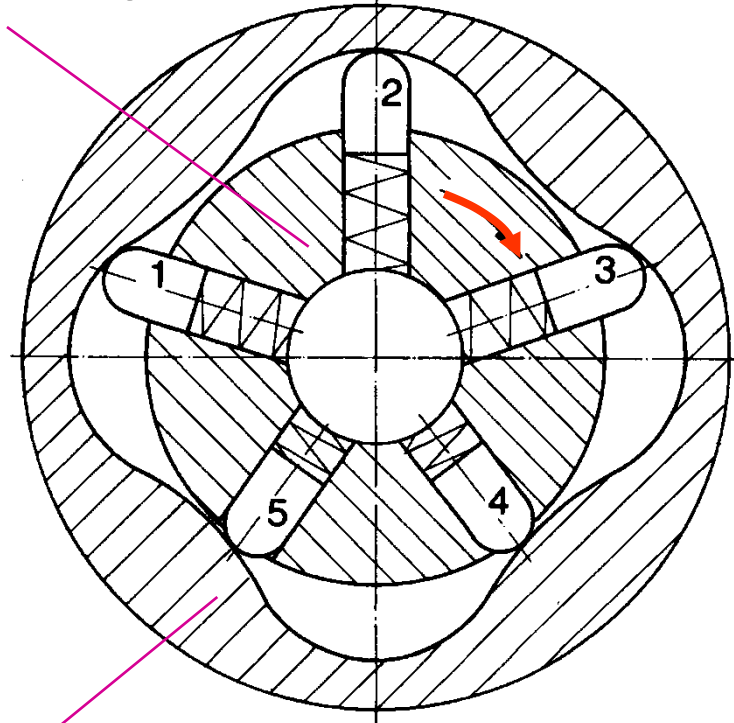
# Radial Piston Pumps



## Multiple stroke radial piston pumps

with external piston support

Rotating cylinder body



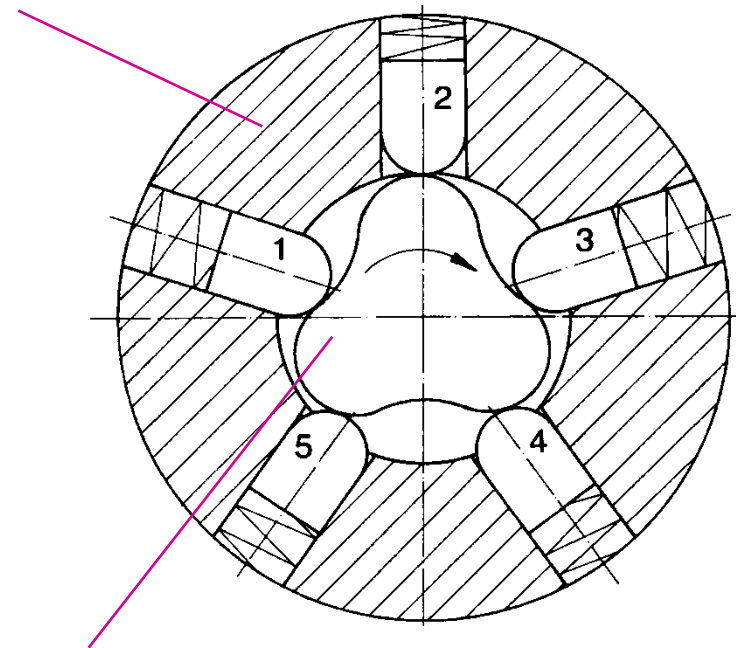
Stationary stroke ring



Only fixed displacement pumps realizable!

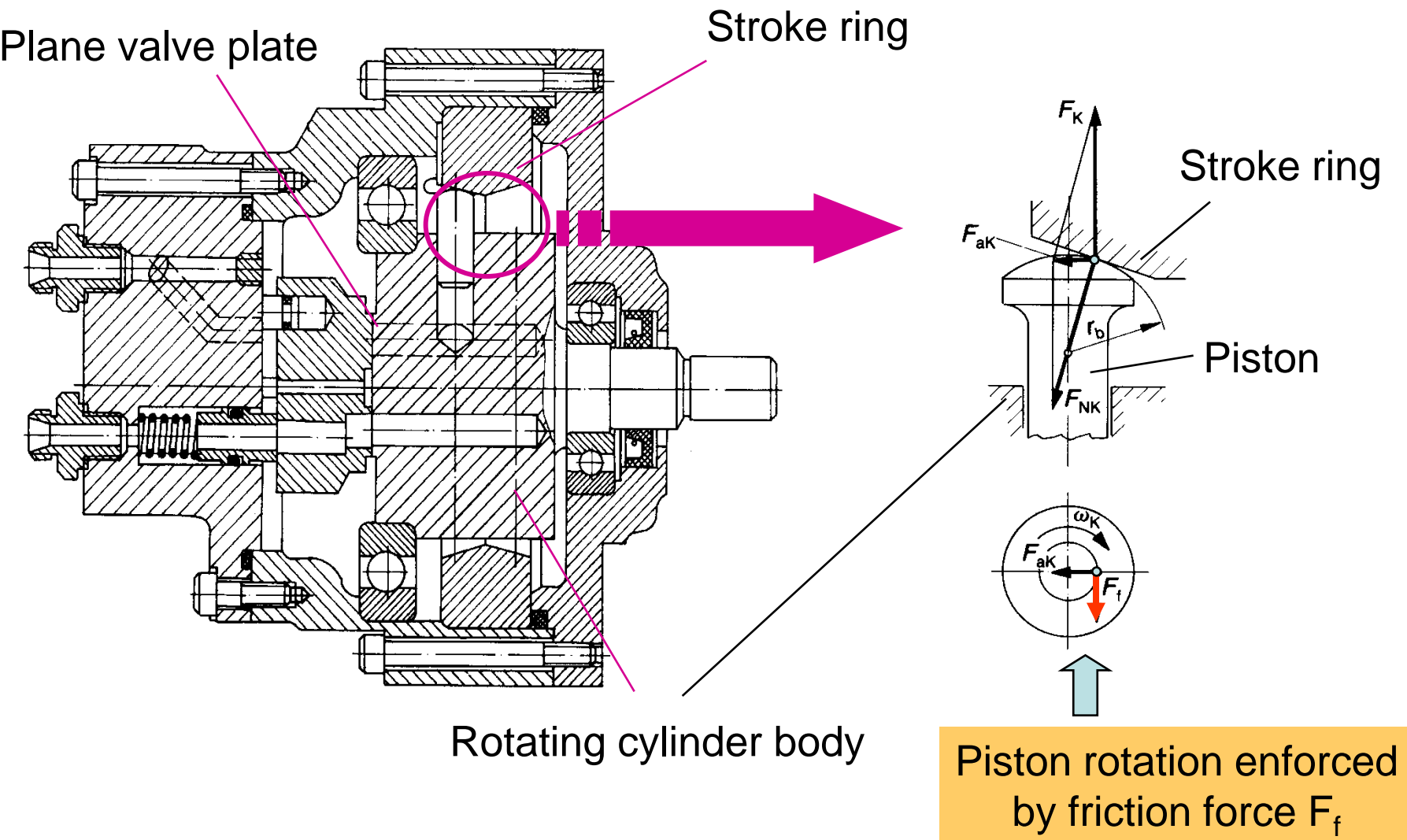
with internal piston support

Stationary cylinder body

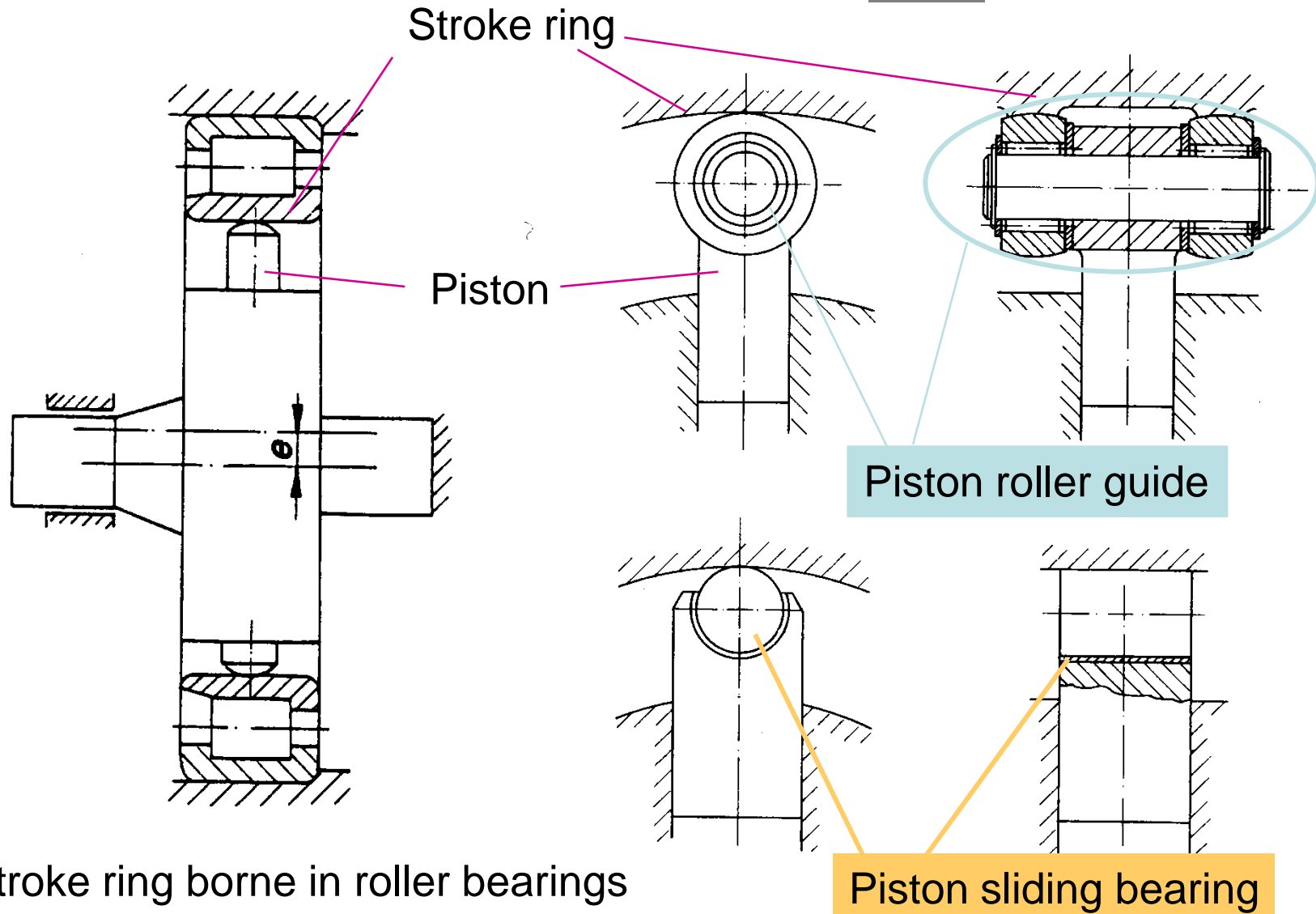


Rotating cam

# Piston support on outer stroke ring



# Piston support on outer stroke ring



Stroke ring borne in roller bearings

Piston sliding bearing

# Piston support on outer stroke ring



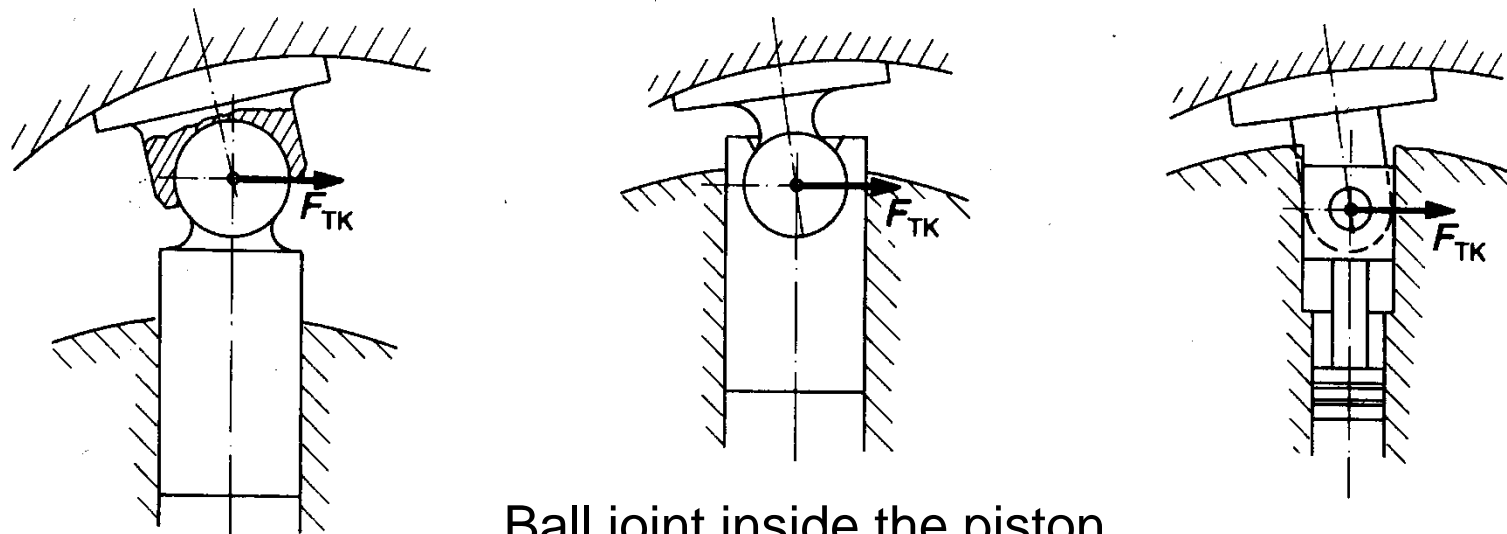
Slipper support

Stroke ring

Slipper pocket

Hydrodynamically balanced slipper

Hydrostatically balanced slipper

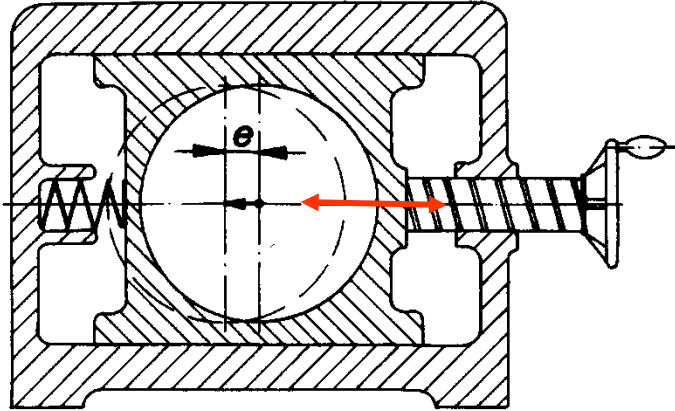


Ball joint inside the piston

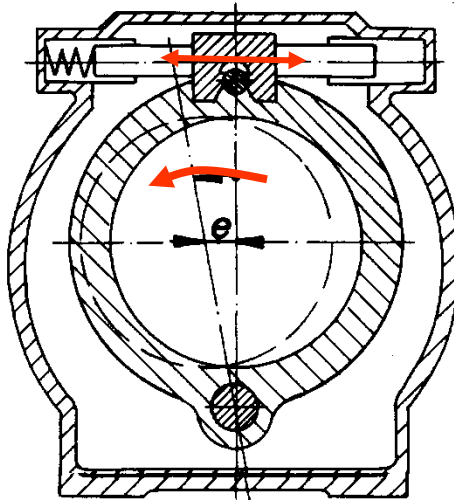
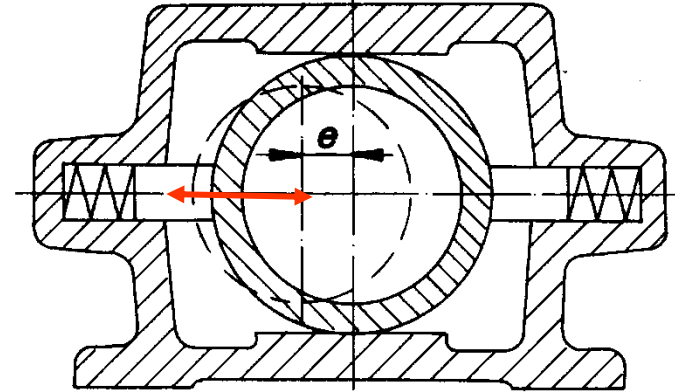
# Stroke ring support



Using a sliding carriage



supported using line contact

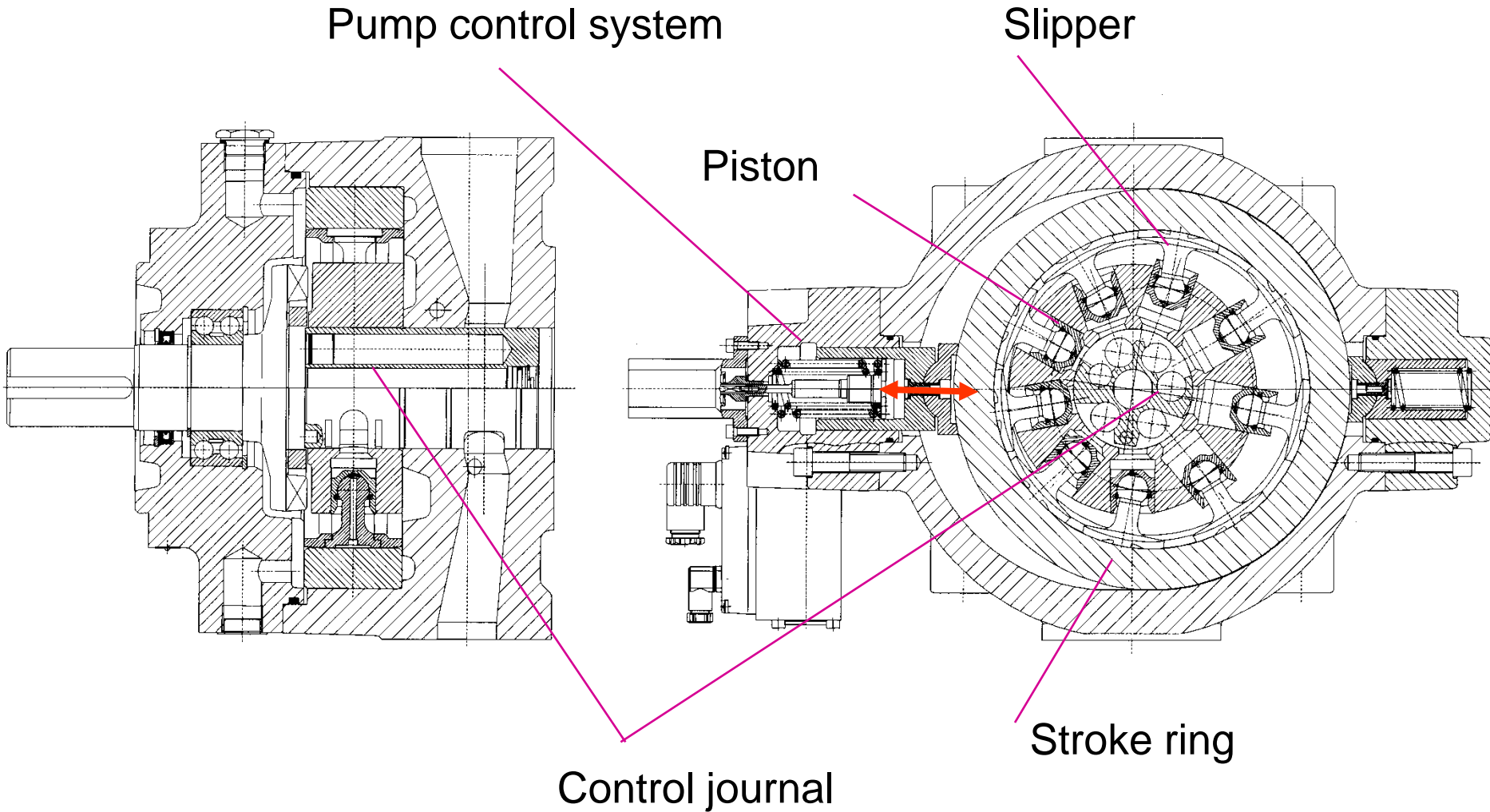


Stroke ring mounted on a pivot

Change of eccentricity by pivoting  
the stroke ring about pivot axis



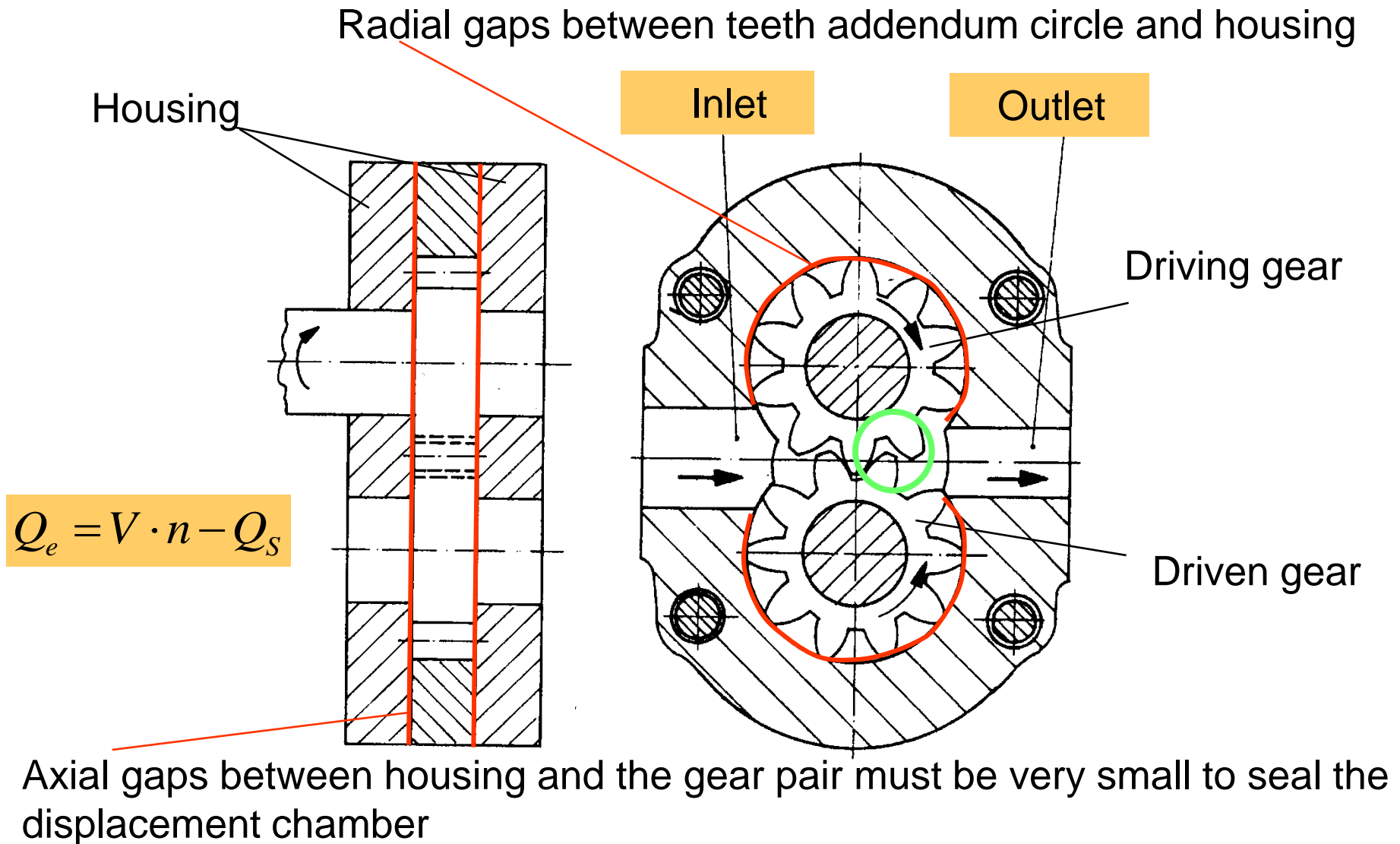
# Design Example



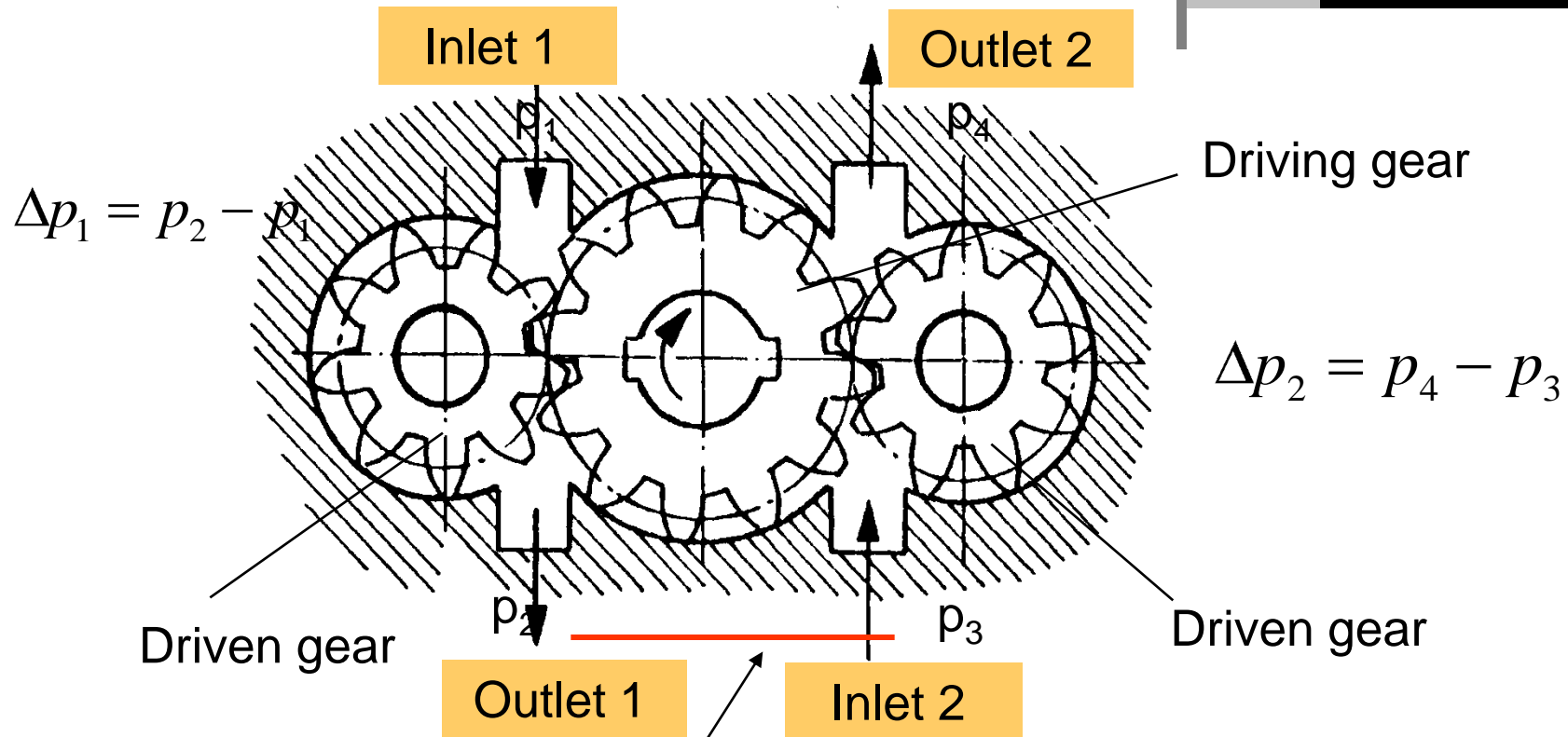


# External gear pump

## Basic principle



# Two stage gear pump



Outlet 1 and inlet 2 can be connected  $\Rightarrow p_2 = p_3$

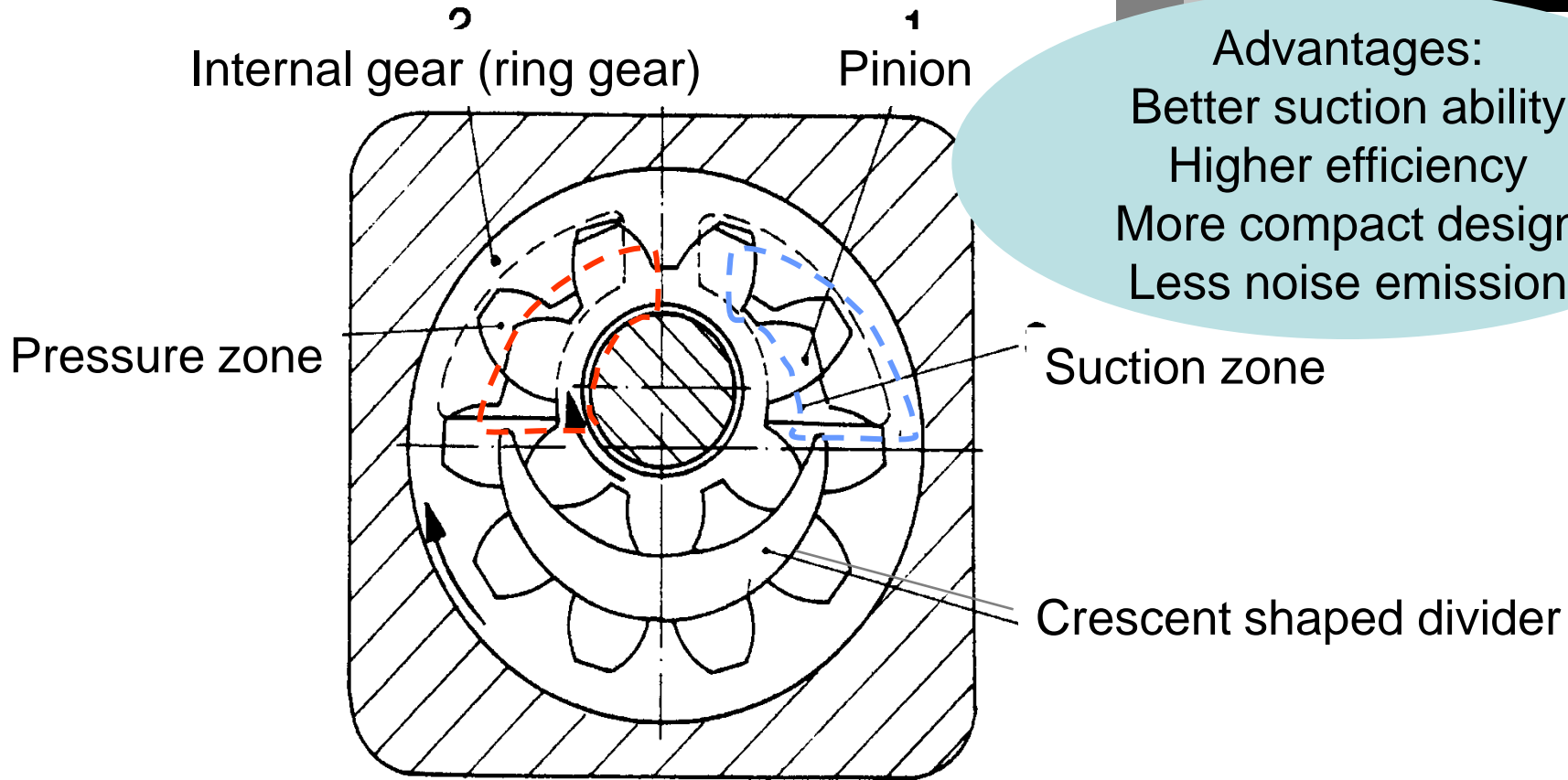
or the pump can have two separate outlets  $\Rightarrow p_1 = p_3$

$\Delta p_1 \approx \Delta p_2$   $\Rightarrow$  the driving gear is pressure balanced!

# Internal gear pump



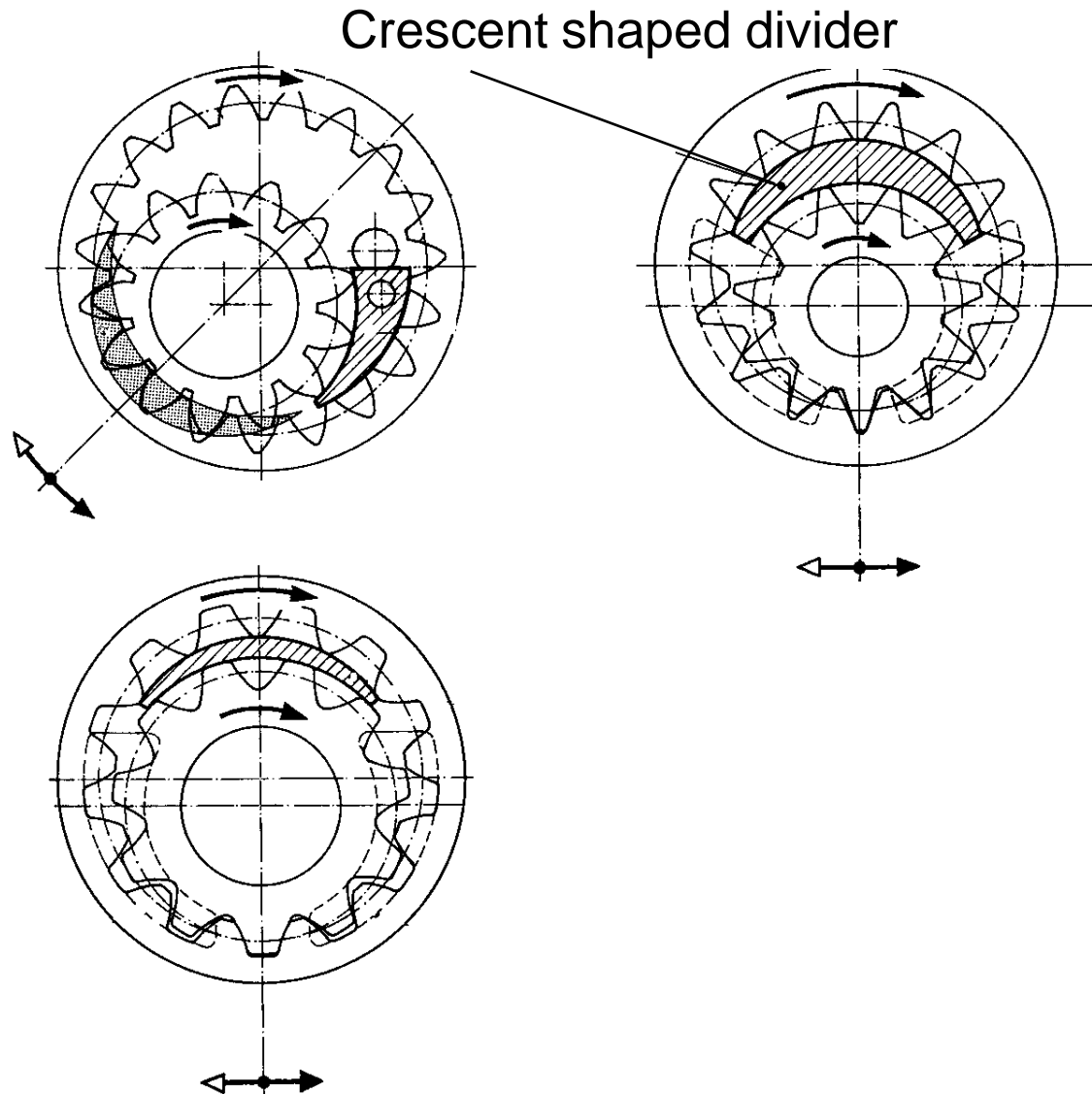
Advantages:  
Better suction ability  
Higher efficiency  
More compact design  
Less noise emission



Using teeth of standard involute design requires a combination where the pinion has two or more fewer teeth than the ring gear! Pinion and ring gear are then separated by a crescent shaped divider.

➡ Longer duration of teeth meshing leads to better sealing function

# Internal gear pump

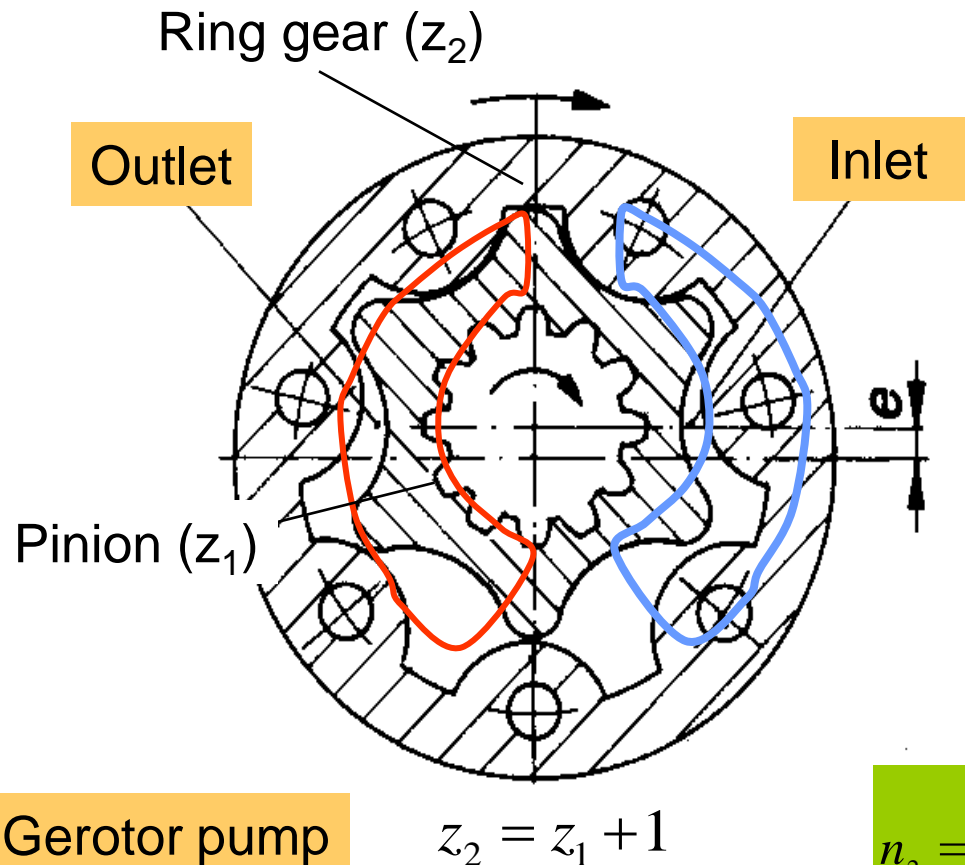


Many different tooth profiles have been applied in the recent past.

# Annular gear pumps



Applying specially generated tooth curves it can be achieved, that the inner rotor (the pinion) has only one tooth less than the ring gear, thus eliminating the crescent-shaped divider.



Each tooth of the pinion maintains continuous sliding contact with a tooth of the ring gear, providing fluid tight engagement.

Relative sliding velocity between pinion and ring gear is very small



quiet operation and long service life

Gerotor pump

$$z_2 = z_1 + 1$$

$$n_2 = n_1 \cdot \frac{z_1}{z_2} = n_1 \cdot \left(1 - \frac{1}{z_2}\right) = n_1 \cdot \left(1 + \frac{1}{z_1}\right)^{-1}$$

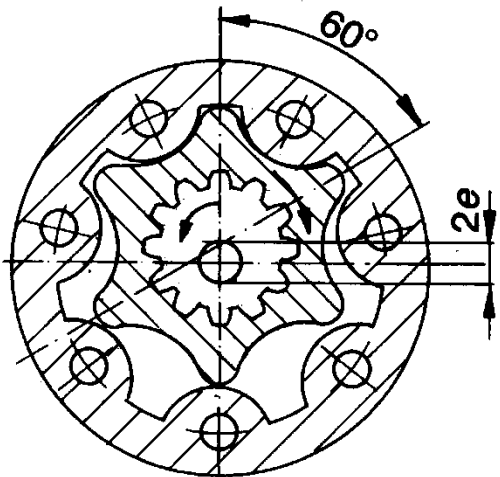
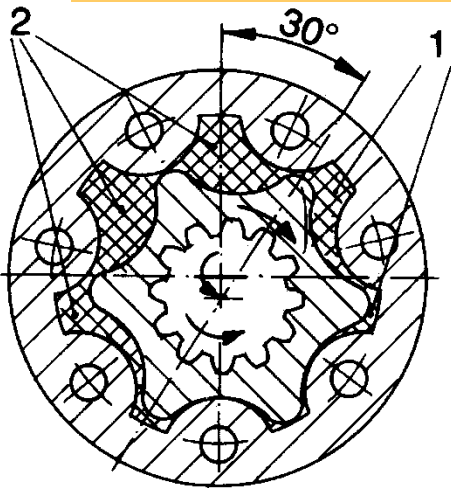
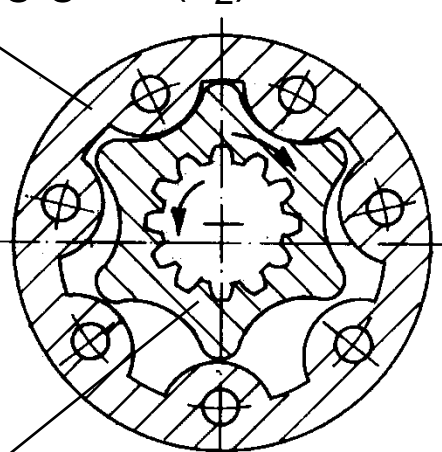
# Annular gear pump – Orbit principle



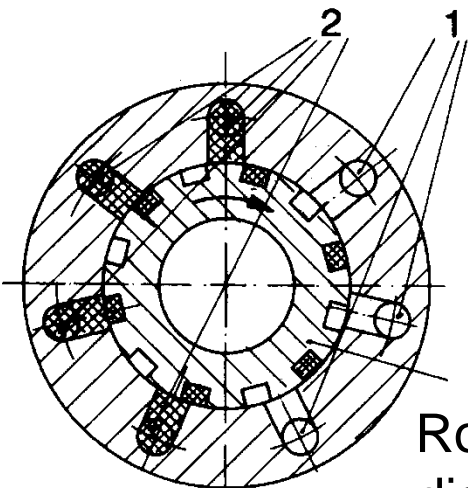
2 Pressure port

$$z_2 = z_1 + 1$$

Ring gear ( $z_2$ ) fixed



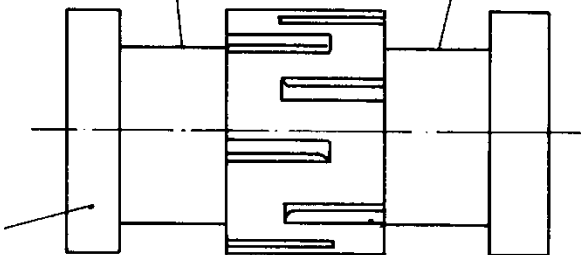
Rotating pinion ( $z_1$ )



Outlet

Inlet

Displacement volume is given by  $z_1$  times  $z_2$  tooth spaces



Rotating distributor

1 Suction port

Multiple delivery of each tooth space



$$A = (0.1 \div 1.3) \frac{F_z}{p_2}$$

Sliding bearing

Sealing ring

Pressurized area A

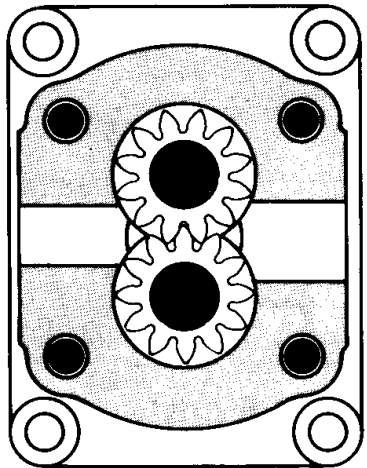
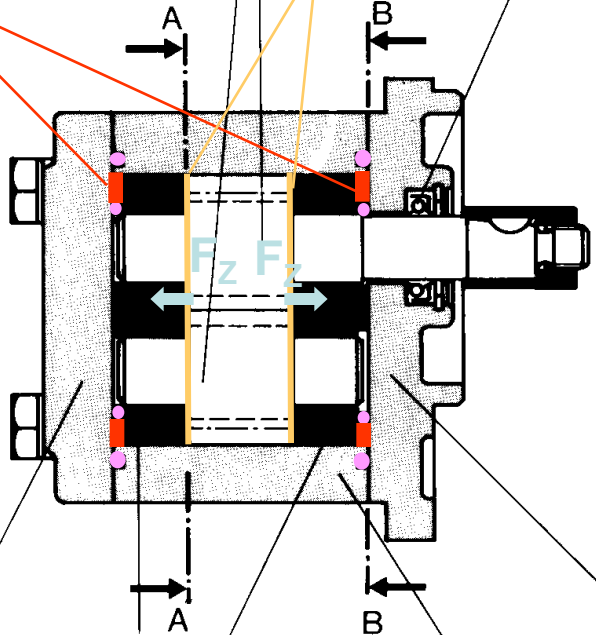
Gear pair

Shaft seal

Axial gap



B-B



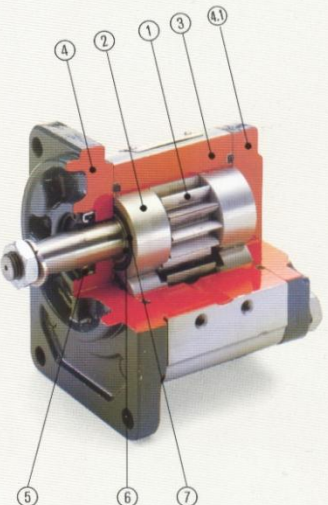
A-A

End cap

Bearing bushings

housing

Front cover



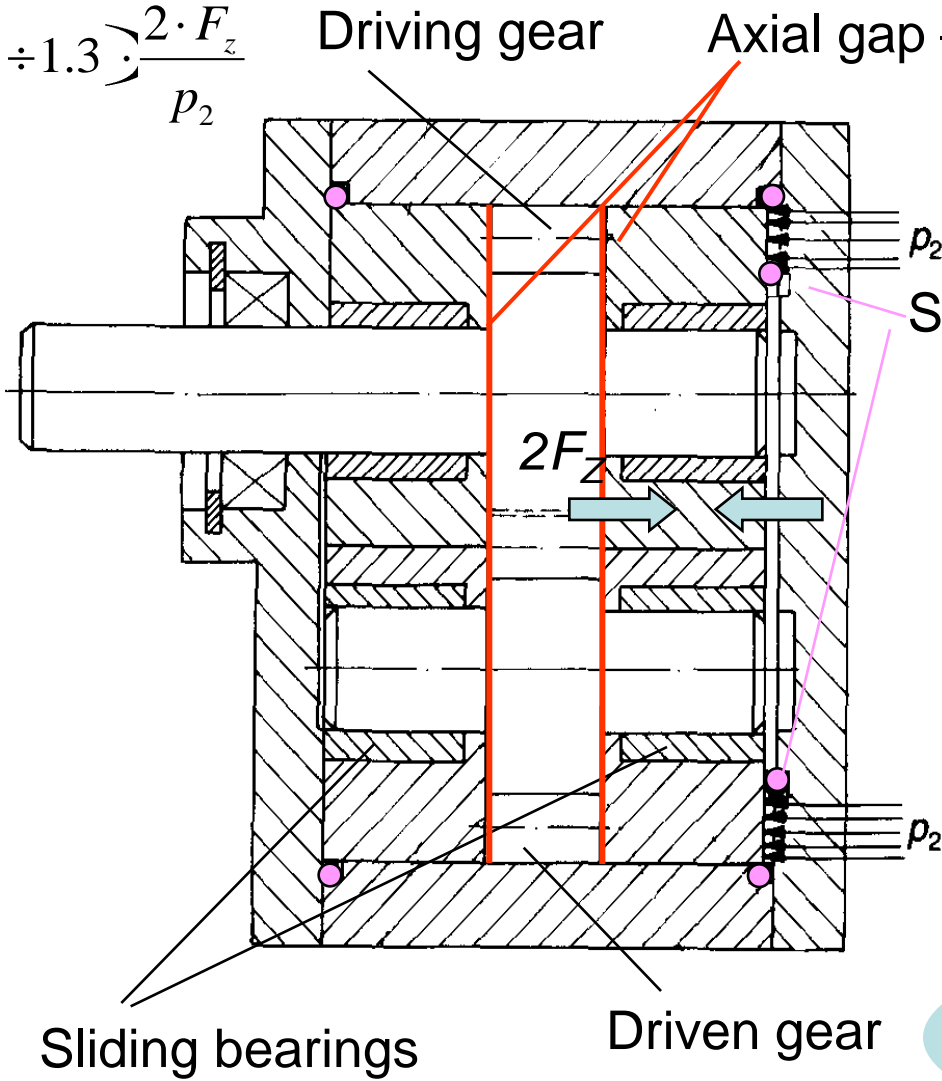
Only one direction of shaft rotation possible!



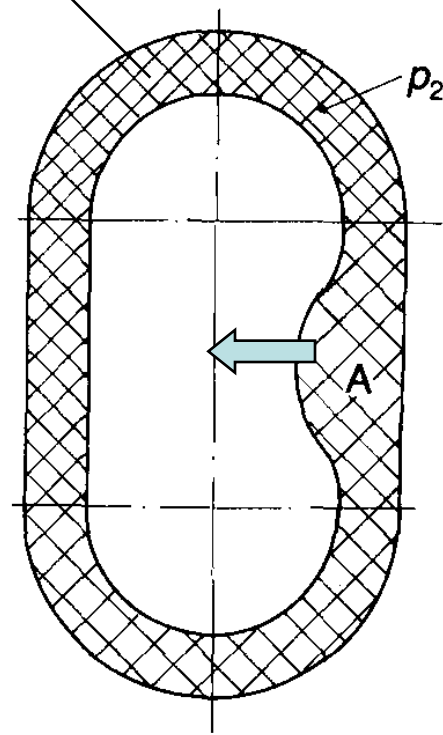
# Pressure compensated axial gaps



$$A = (0.1 \div 1.3) \frac{2 \cdot F_z}{p_2}$$



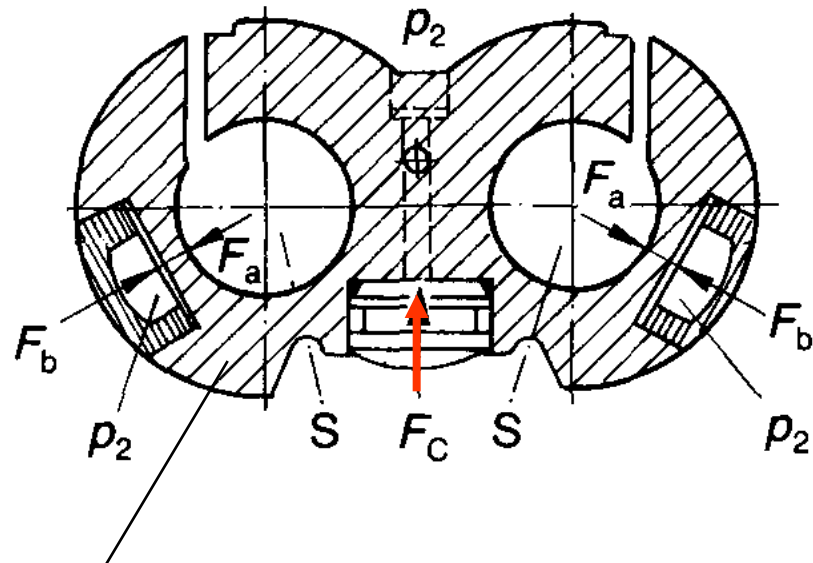
Pressurized area



Improved volumetric efficiency



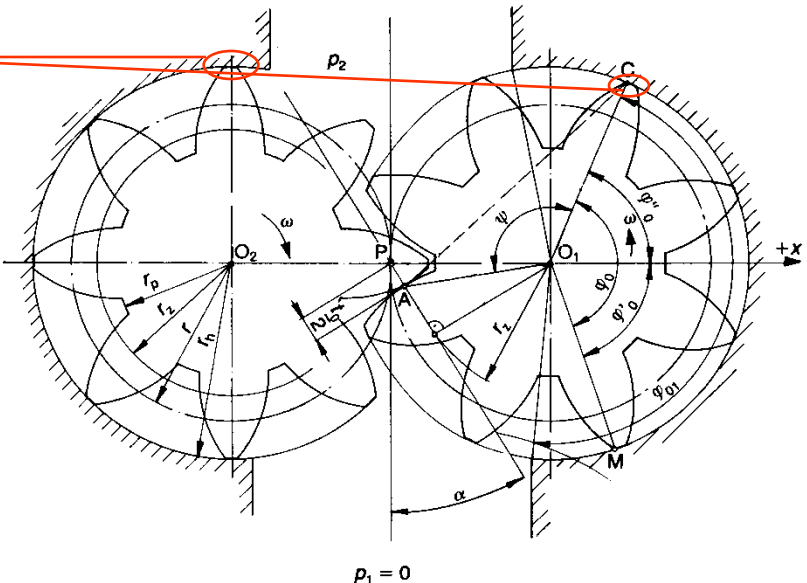
Radial gap compensation



Bearing bushing

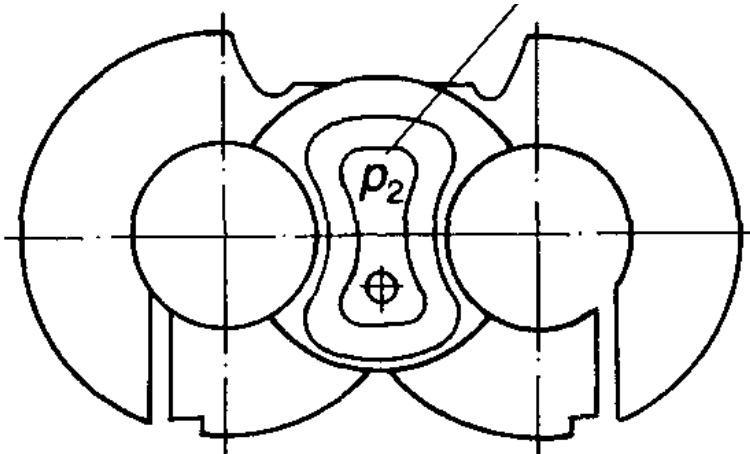


Small pressure zone achievable

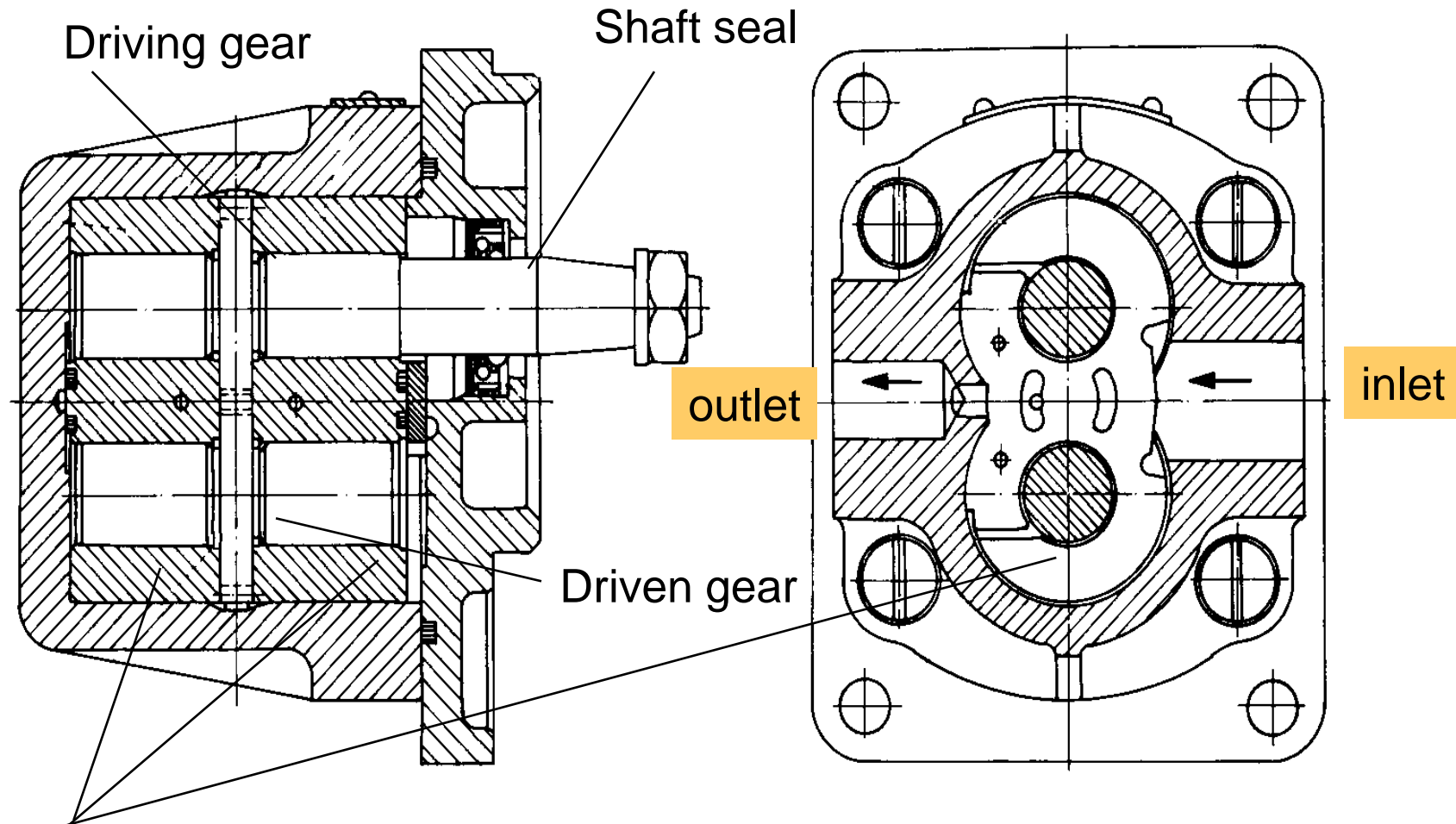


Axial gap compensation

Pressurized area

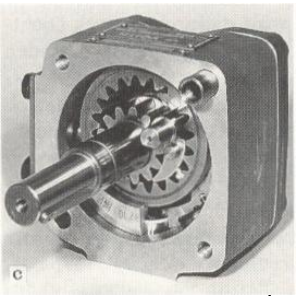


# Gear pump – design example

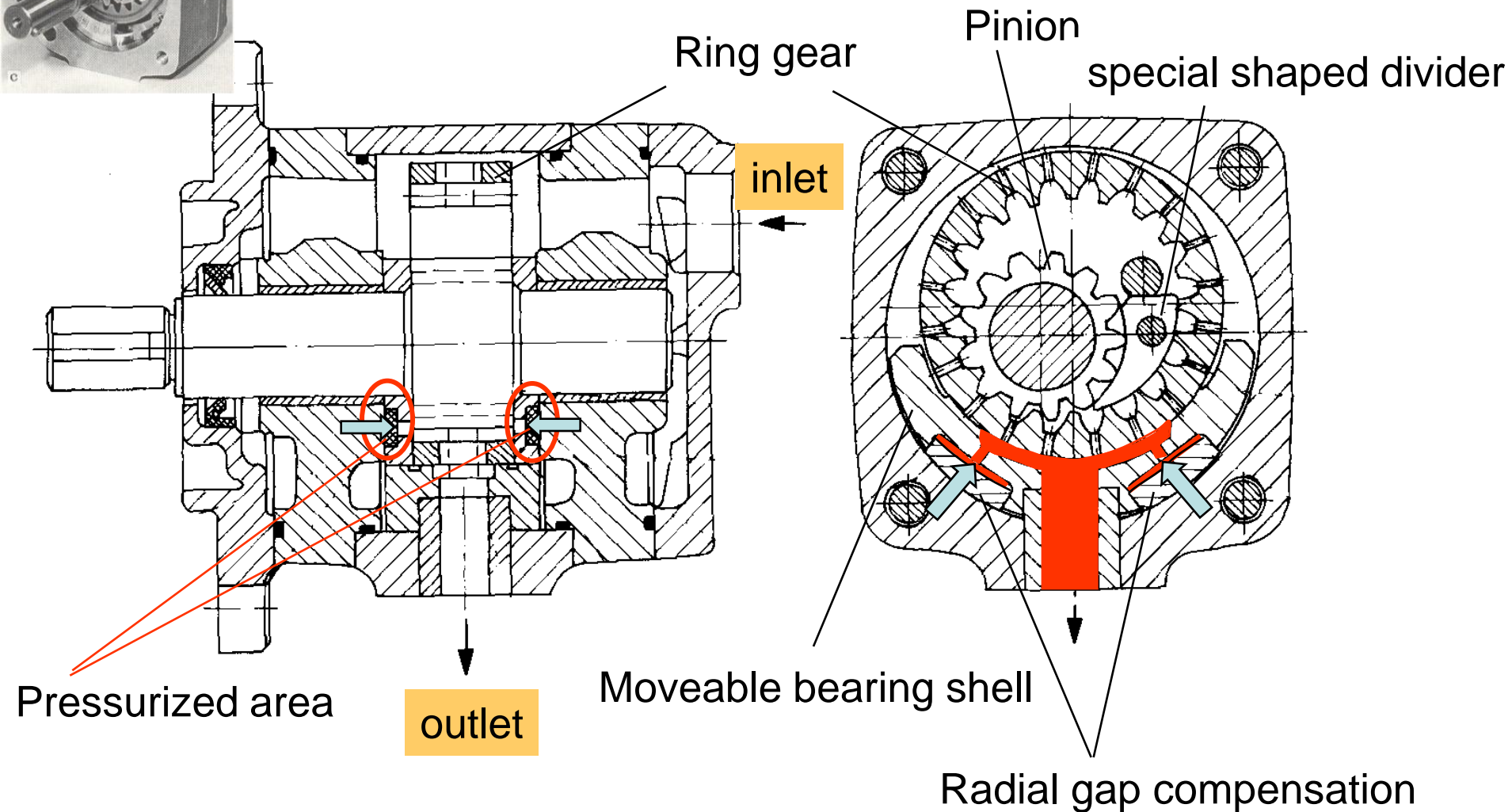


Bearing bushing performing a radial and axial gap compensation

# Internal gear pump- design example



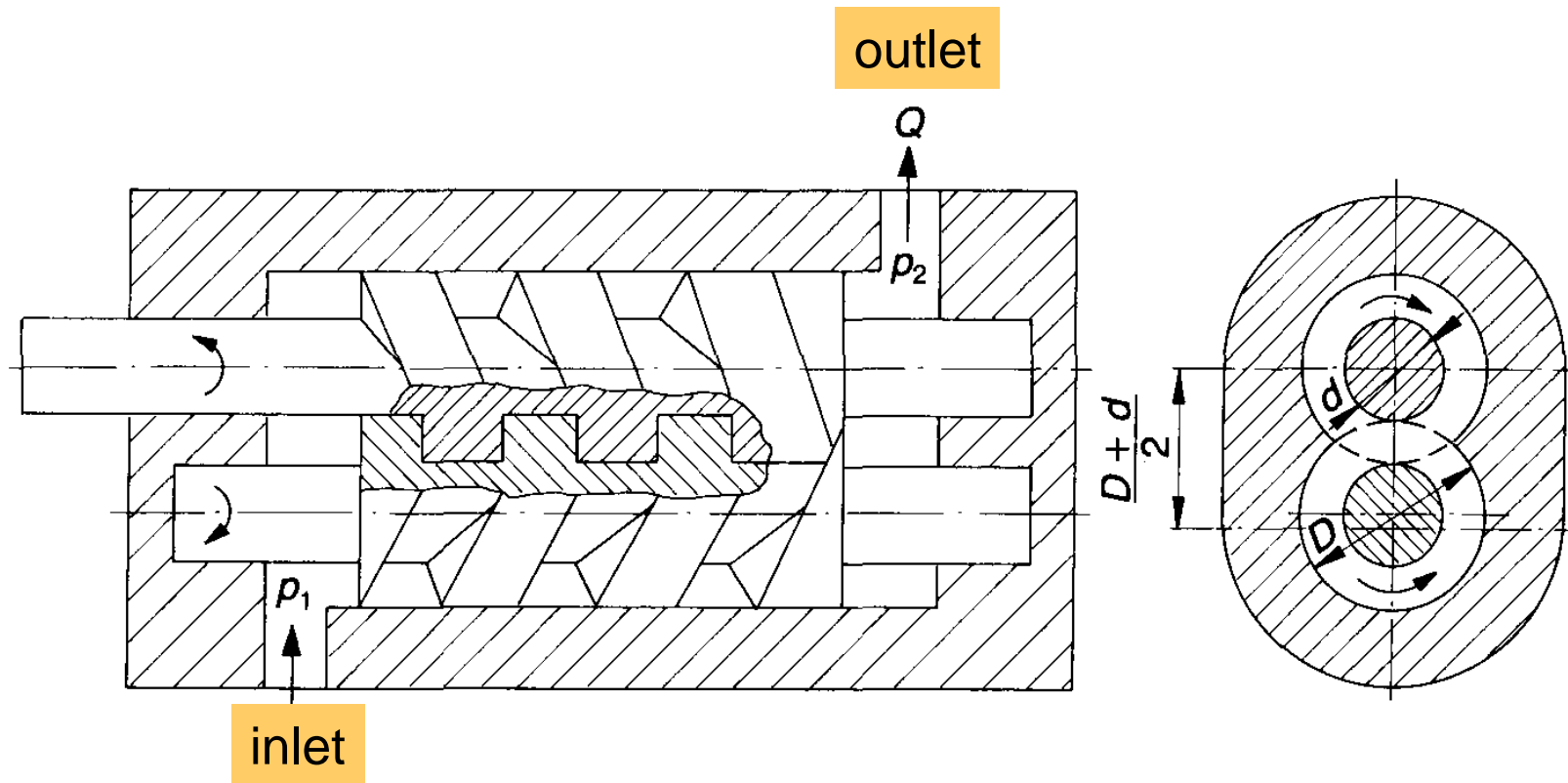
Internal gear pump with axial and radial gap compensation



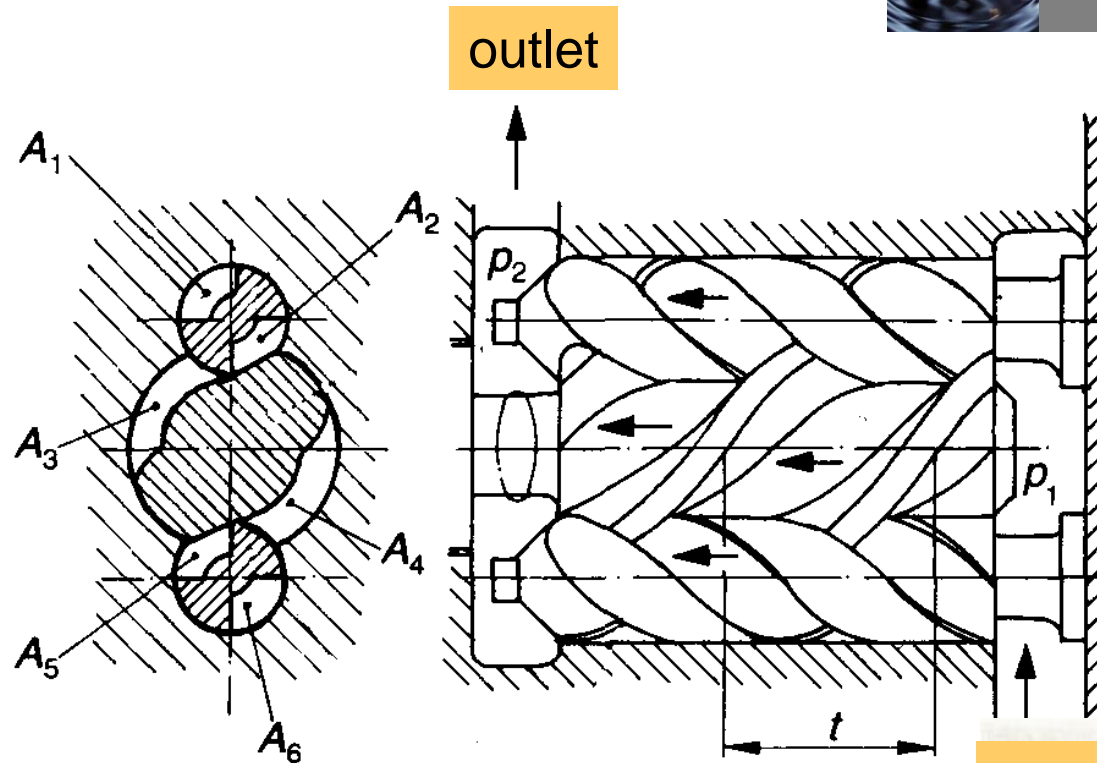
# Screw Pumps



With two meshing screws

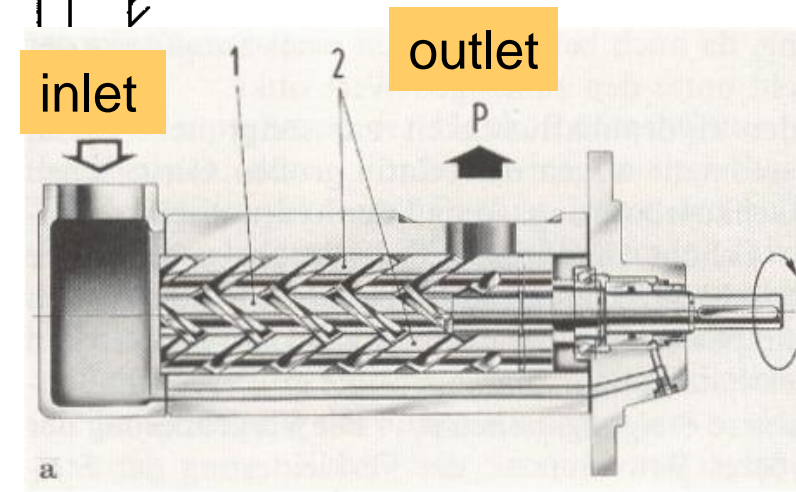


# Screw Pumps



t...thread pitch

With three meshing screws

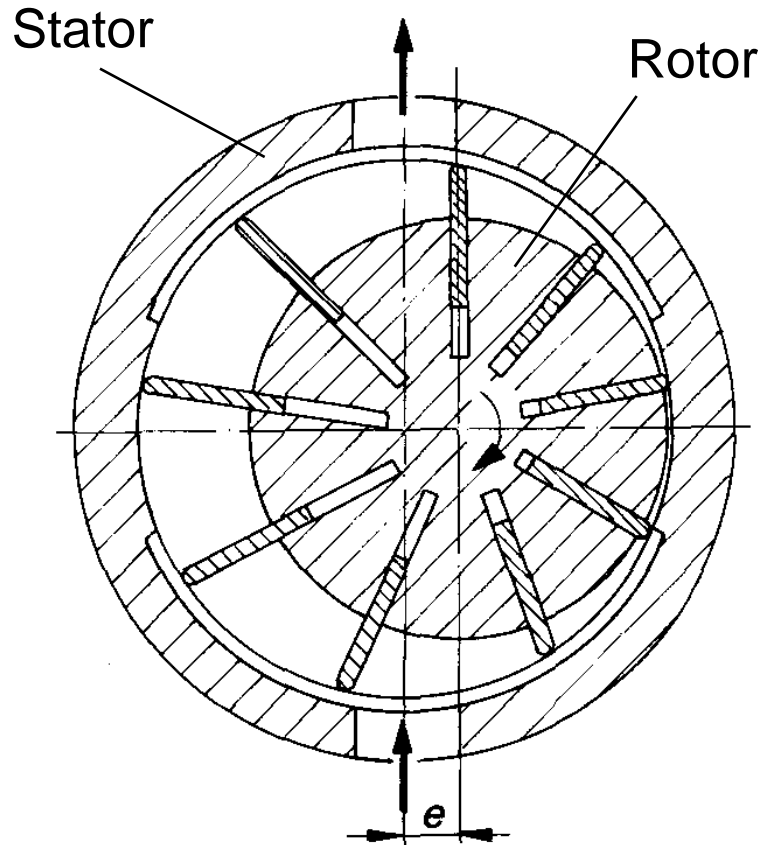


# Vane Pumps

## Classification of vane pumps

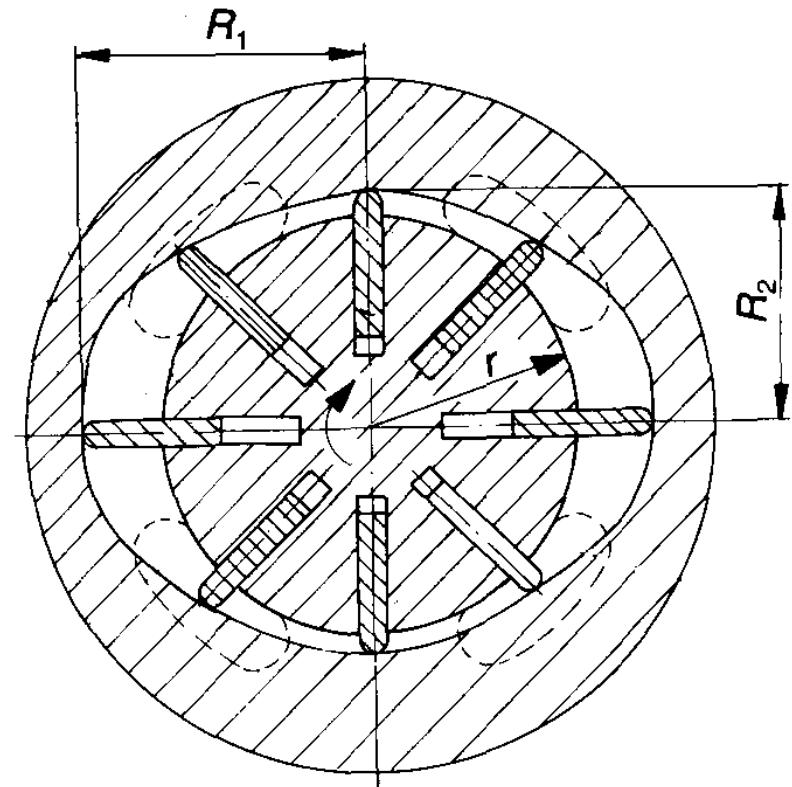


Unbalanced vane pump



Fixed and variable pump design

Balanced vane pump



Only fixed displacement pump



# Vane pumps- basic working principle



Single stroke vane pump – variable displacement volume

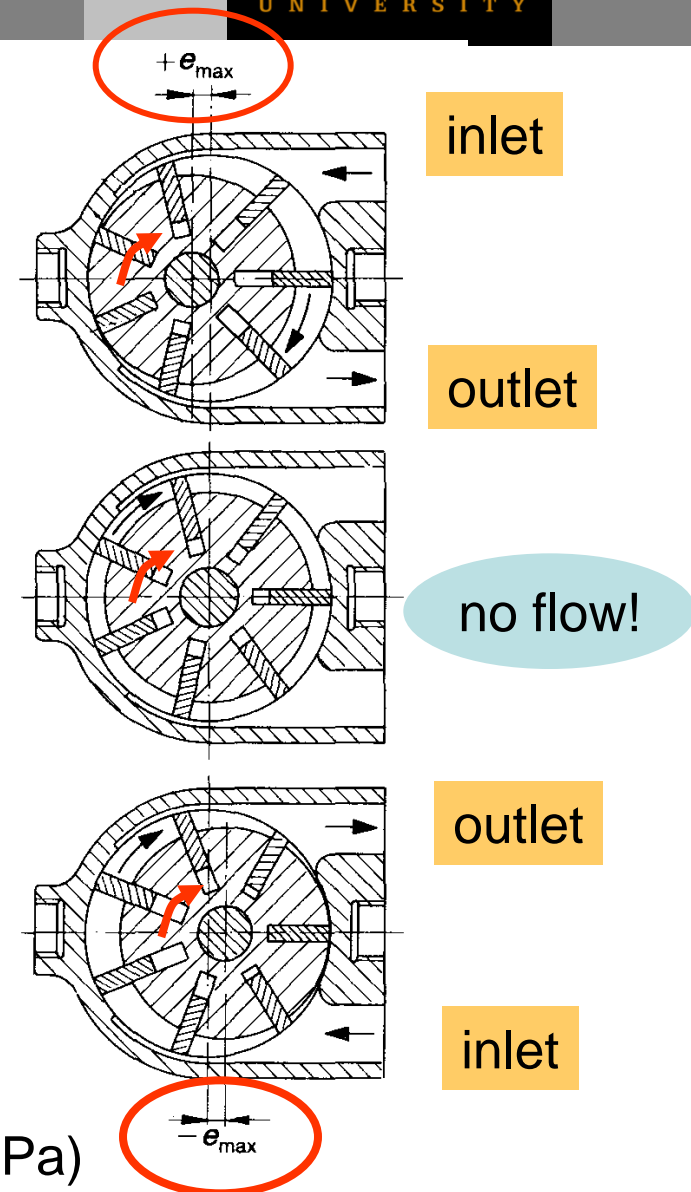
Overcentre pump – the direction of flow can be reversed by change of eccentricity, i.e. without changing the direction of rotation of the drive shaft

Relatively high friction between  
axial moveable vanes and rotor  
&  
between vanes and stator

Large radial forces exerted on the rotor



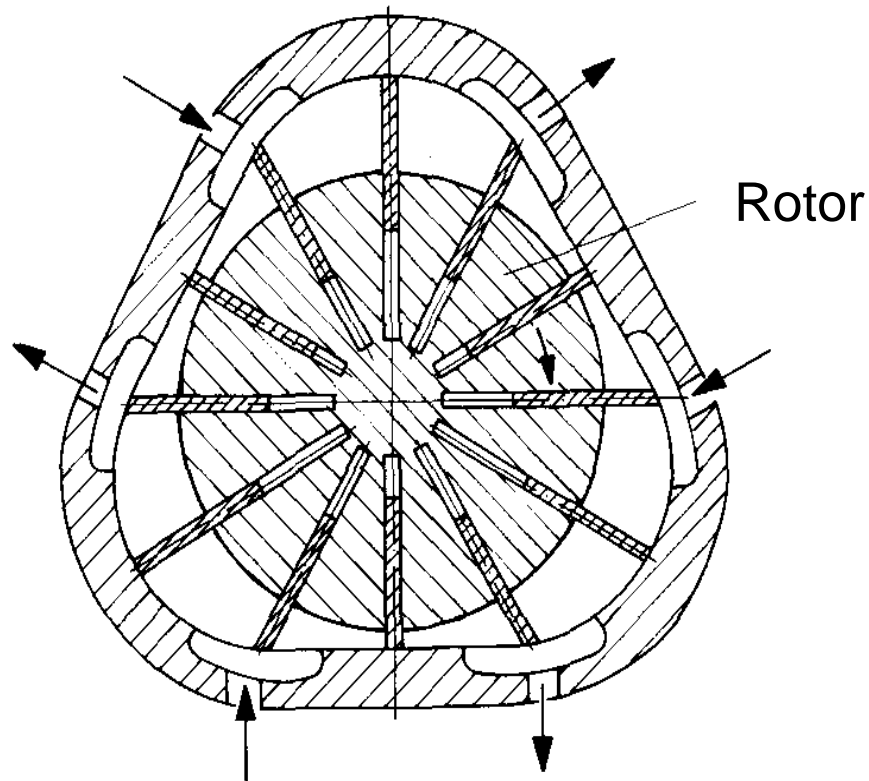
Limitation of max. operating pressure (20 MPa)



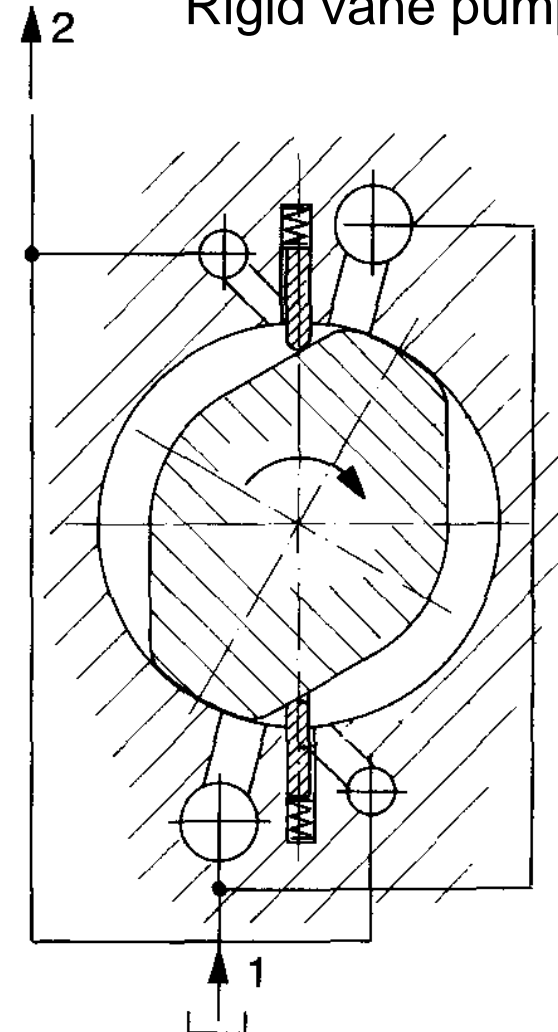
# Vane pumps- classification



Multiple stroke vane pump



Rigid vane pump

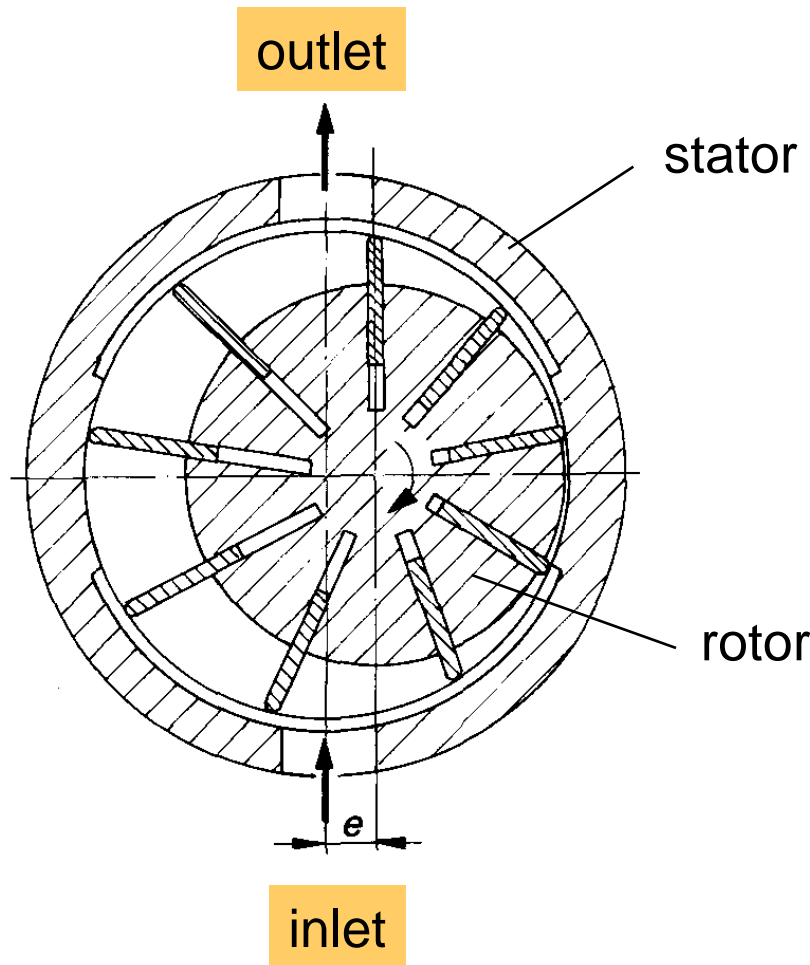




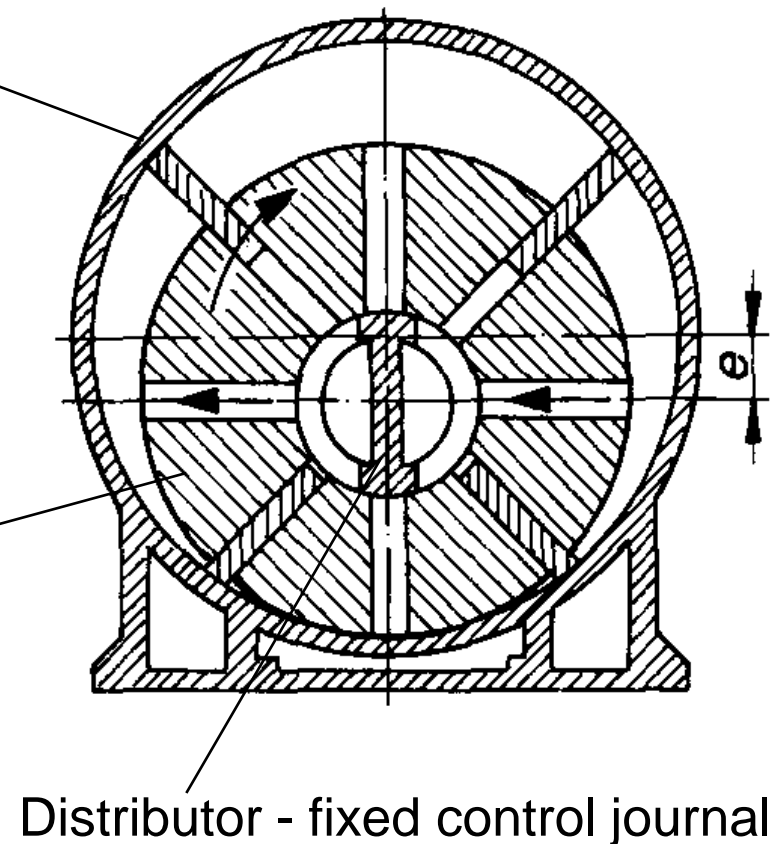
# Fluid distribution



External fluid distribution



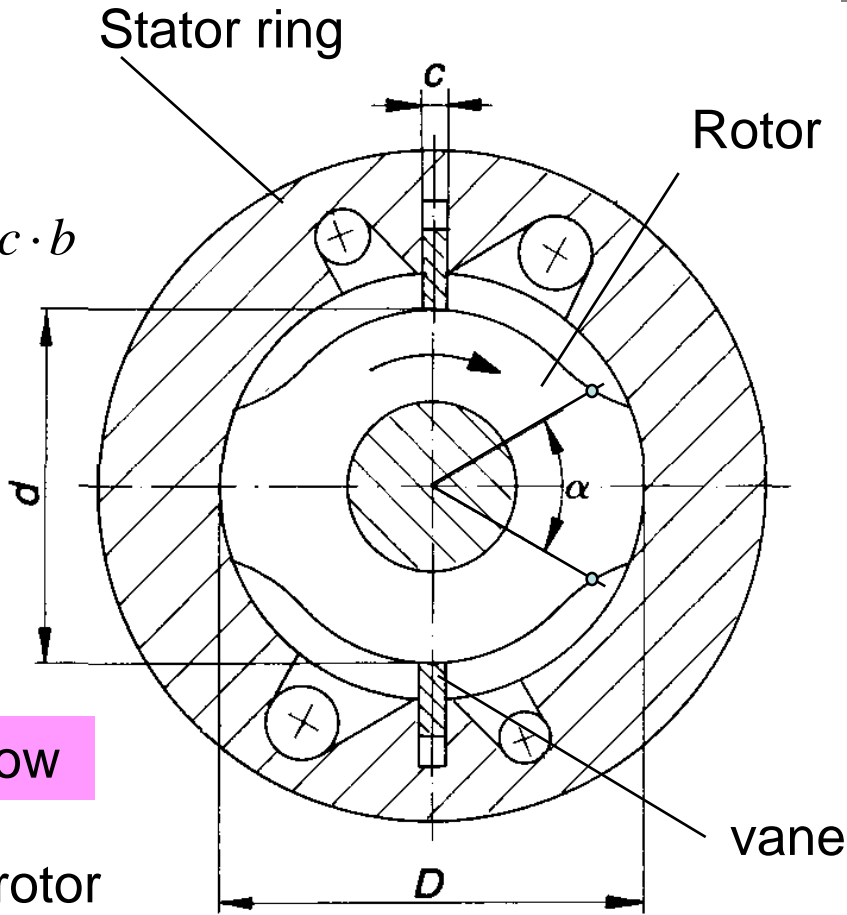
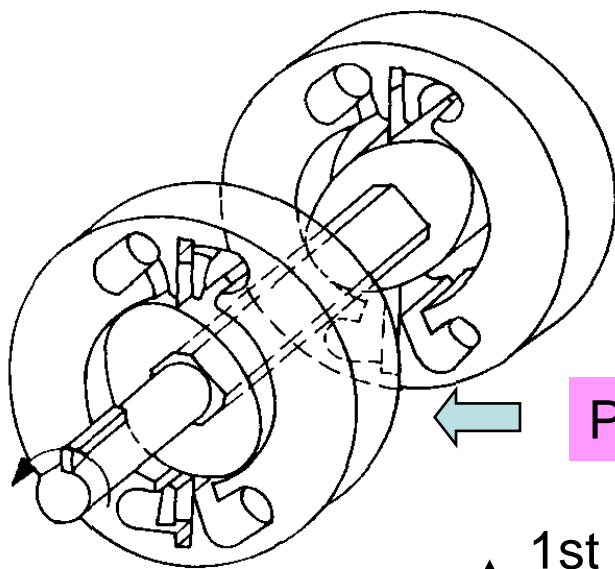
Internal fluid distribution



# Rigid vane pump

Displacement volume:

$$V_g = 2 \cdot \frac{\pi \cdot (D^2 - d^2)}{4} \cdot \frac{180 - \alpha}{180} \cdot b - 2 \cdot \left( \frac{D}{2} - \frac{d}{2} \right) \cdot c \cdot b$$



Pulsation free flow

