Weak Form for the Self-Adjoint S_N Formalism

1 Self-Adjoint S_N

LHS: =
$$(-\vec{\Omega} \cdot \vec{\nabla} + \sigma_a)(\vec{\Omega} \cdot \vec{\nabla} + \sigma_a)\psi$$
 (1)

$$= \underbrace{-\vec{\Omega} \cdot \vec{\nabla} \vec{\Omega} \cdot \vec{\nabla} \psi}_{\text{(2)}} + \underbrace{\left[\sigma_a \vec{\Omega} \cdot \vec{\nabla} \psi - \vec{\Omega} \cdot \vec{\nabla} (\sigma_a \psi)\right]}_{\text{(2)}} + \underbrace{\sigma_a^2 \psi}_{\text{(3)}}$$

RHS:
$$= (-\vec{\Omega} \cdot \vec{\nabla} + \sigma_a)Q$$
(3)
$$= \underbrace{-\vec{\Omega} \cdot \vec{\nabla}Q}_{\text{(3)}} + \underbrace{\sigma_aQ}_{\text{(5)}}$$

Note that for radiative transfer problem, σ_a is embedded in the source Q:

$$Q = \sigma_a B \tag{5}$$

where B is the Planckian source determined by the temperature.

2 Weak form

Multiply every term in LHS and RHS by basis function b_i and integrate over the problem volume:

LHS:

$$= \underbrace{-\oint (\vec{\Omega} \cdot \vec{\nabla} \psi) \ b_i \ \vec{\Omega} \cdot \vec{n} dA}_{*} + \int (\vec{\Omega} \cdot \vec{\nabla} \psi) (\vec{\Omega} \cdot \vec{\nabla} b_i) dV \tag{7}$$

$$\underbrace{\int 2b_i dV}_{} = \int \left[\sigma_a \vec{\nabla} \cdot (\vec{\Omega}\psi) - \vec{\nabla} \cdot (\sigma_a \vec{\Omega}\psi) \right] b_i dV \tag{8}$$

$$= \int (-\vec{\Omega}\psi \cdot \vec{\nabla}\sigma_a) \ b_i \ dV = \int (-\vec{\Omega}\psi b_i \cdot \vec{\nabla}\sigma_a) dV \tag{9}$$

$$= - \oint \sigma_a \ \psi b_i \ \vec{\Omega} \cdot \vec{n} dA + \int \sigma_a \vec{\nabla} \cdot (\vec{\Omega} \psi b_i) dV$$
 (10)

$$\boxed{\int \Im b_i dV} \\
= \int \sigma_a^2 \psi b_i dV \tag{11}$$

RHS:

$$\int \textcircled{4}b_i dV$$

$$= \int (-\vec{\Omega} \cdot \vec{\nabla}Q)b_i dV \tag{12}$$

$$= - \oint b_i Q \vec{\Omega} \cdot \vec{n} dA + \int Q \vec{\Omega} \cdot \vec{\nabla} b_i dV$$
 (13)

or
$$(14)$$

$$= -\int \vec{\Omega} \cdot \vec{\nabla} (\sigma_a B) \ b_i \ dV \tag{15}$$

$$= -\int \vec{\Omega}(\vec{\nabla}\sigma_a B + \vec{\nabla}B\sigma_a) \ b \ dV$$
(16)

$$\boxed{\int \mathfrak{S}b_i dV}$$

$$= \int \sigma_a Q b_i dV = \int \sigma_a^2 B b_i dV \tag{17}$$

Depending on the order of finite element chosen to represent the solution and material property (opacity (cross-section), source), two different sets of weak form are proposed:

If we choose to use piece-wise constant (0^{th} order) finite element, then it is suggested to use the terms <u>underlined</u> whenever possible (as seen in Eq. (10) and Eq. (13)).

If we choose to use piece-wise linear (1^{st} order) finite element, then it is suggested to use the terms $\underline{double - lined}$ whenever possible (as seen in Eq. (9) and Eq. (16)).

Note that one can choose to use either the $\underline{underlined}$ or the $\underline{double-lined}$, not both. Because they are mathematically equivalent.

3 Boundary condition

For the in-coming directions, we use Dirichlet boundary condition to explicitly specify the value of ψ on the boundary.

For the out-going directions, we use the first order equation:

$$\vec{\Omega} \cdot \vec{\nabla} \psi + \sigma_a \psi = Q \Rightarrow \left[\vec{\Omega} \cdot \vec{\nabla} \psi = Q - \sigma_a \psi \right]$$
 (18)

The out-going boundary condition Eq. (18) is applied to the * term only, where $\vec{\Omega} \cdot \vec{\nabla} \psi$ is replaced by $Q - \sigma_a \psi$, yielding:

$$* = \oint (\vec{\Omega} \cdot \vec{\nabla} \psi) \ b_i \ \vec{\Omega} \cdot \vec{n} dA = \underbrace{-\oint Q \ b_i \ \vec{\Omega} \cdot \vec{n} dA}_{\text{move to RHS}} + \underbrace{\oint \sigma_a \psi b_i \vec{\Omega} \cdot \vec{n} dA}_{\text{keep on LHS}}, \quad \text{for } \vec{\Omega} \cdot \vec{n} > 0$$
(19)

The $\vec{\Omega} \cdot \vec{n} > 0$ portion of this * term is neglected, it is equivalent to force:

$$* = \oint (\vec{\Omega} \cdot \vec{\nabla} \psi) \ b_i \ \vec{\Omega} \cdot \vec{n} dA = 0, \quad \text{for } \vec{\Omega} \cdot \vec{n} < 0$$
 (20)

4 Final form after cancellation of the surface terms

Take the five kernels listed in the above section, using the <u>underlined</u> as seen in Eq. (10) and Eq. (13), and also applying the first order boundary condition Eq. (18) for both out-going and in-coming directions for the boundary term (*), we get:

LHS :=
$$-\oint Q b_i \vec{\Omega} \cdot \vec{n} dA^{II} + \oint \sigma_a \psi b_i \vec{\Omega} \cdot \vec{n} dA^{I} + \int (\vec{\Omega} \cdot \vec{\nabla} \psi) (\vec{\Omega} \cdot \vec{\nabla} b_i) dV$$

$$-\oint \sigma_a \psi b_i \vec{\Omega} \cdot \vec{n} dA^{I} + \left[\int \sigma_a \vec{\nabla} \cdot (\vec{\Omega} \psi b_i) dV \right]$$

$$+ \int \sigma_a^2 \psi b_i dV$$
(21)

RHS :=
$$-\oint b_i Q \vec{\Omega} \cdot \vec{n} dA^{II} + \int Q \vec{\Omega} \cdot \vec{\nabla} b_i dV$$

 $+ \int \sigma_a Q b_i dV$ (22)

We can see that the "I" terms cancels out each other, and the same for the "II" terms. Finally, expand out the boxed term in LHS:

$$\boxed{\int \sigma_a \vec{\nabla} \cdot (\vec{\Omega} \psi b_i) dV} = \int \sigma_a b_i \vec{\Omega} \cdot \vec{\nabla} \psi dV + \int \sigma_a \psi \vec{\Omega} \cdot \vec{\nabla} b_i \tag{23}$$

Our final form becomes:

LHS :=
$$\int (\vec{\Omega} \cdot \vec{\nabla} \psi)(\vec{\Omega} \cdot \vec{\nabla} b_i) dV$$
$$\int \sigma_a b_i \vec{\Omega} \cdot \vec{\nabla} \psi dV + \int \sigma_a \psi \vec{\Omega} \cdot \vec{\nabla} b_i$$
$$+ \int \sigma_a^2 \psi b_i dV$$
$$(24)$$
$$RHS := \int Q \vec{\Omega} \cdot \vec{\nabla} b_i dV$$
$$+ \int \sigma_a Q b_i dV \tag{25}$$

The same as Dr. Ragusa's derivation. However, in my implementation I only used the first order boundary condition for the out-going directions, as explained in the Boundary condition section. Therefore, the "I" and "II" terms doesn't cancel themselves out completely. The in-coming portion of those terms remains.