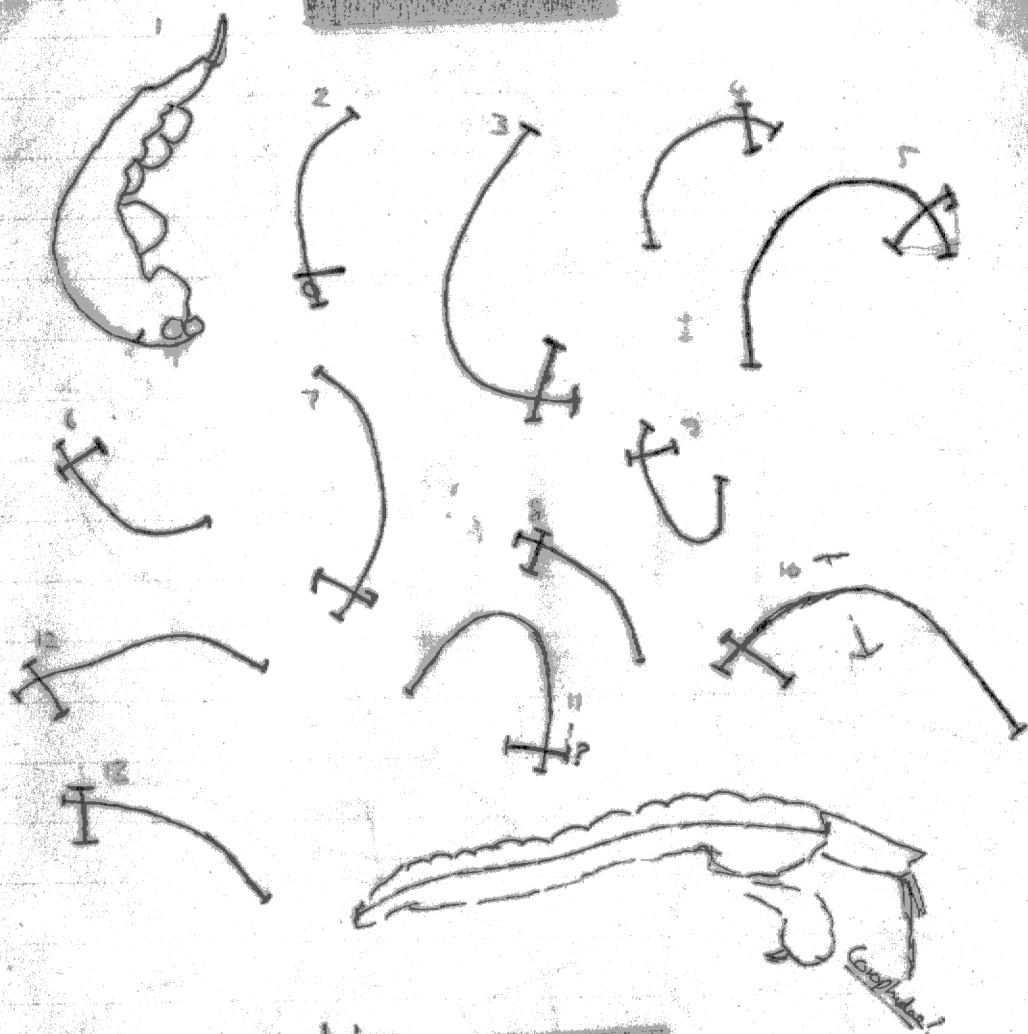


	L	HL	HM
1	1.03	.14	.2
2	.87	.09	.13
3	1.03	.13	.21
4	.61	.1	.12
5	1.03	.13	.21
6	.51	.07	.12
7	.77	.11	.16
8	.50	.08	.11
9	.57	.11	.12
10	1.07	.11	.2
11	.85	.09	.16
12	.74	.11	.16
13	.66	.07	.14

$$y = ax + b$$

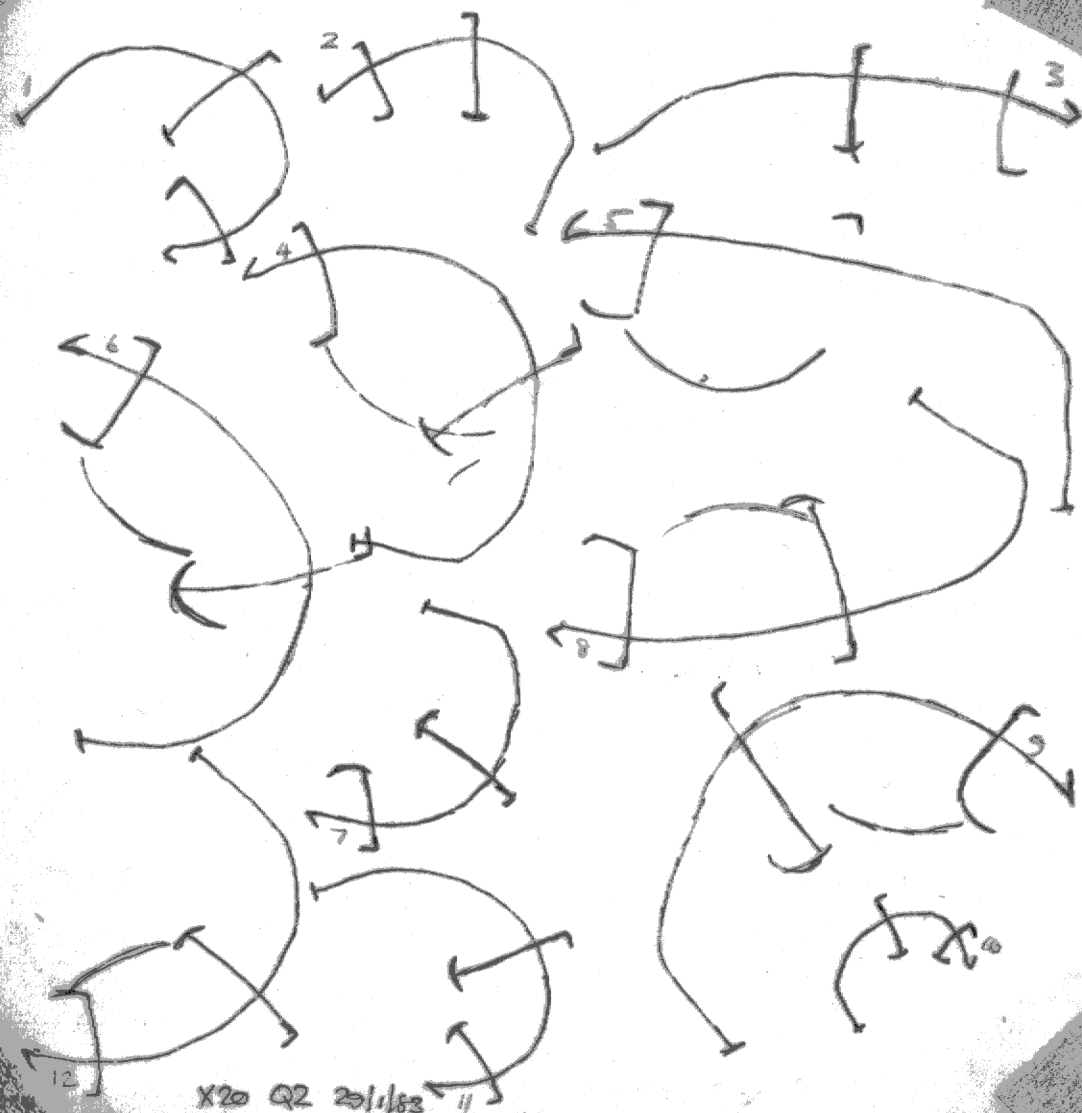
$$T_L = \text{MP} \cdot a \cdot MP + b$$

$$TQ1 = 13$$



X20 Q1 29/1/83

	L	HL	HM
1	1.36	.18	.25
2	1.1	.18	.25
3	1.32	.2	.26
4	1.81	.21	.3
5	1.80	.29	.31
6	1.82	.26	.31
7	1.15	.21	.22
8	1.81	.21	.33
9	1.95	.28	.32
10	.67	.12	.12
11	1.27	.2	.22
12	1.45	.23	.28



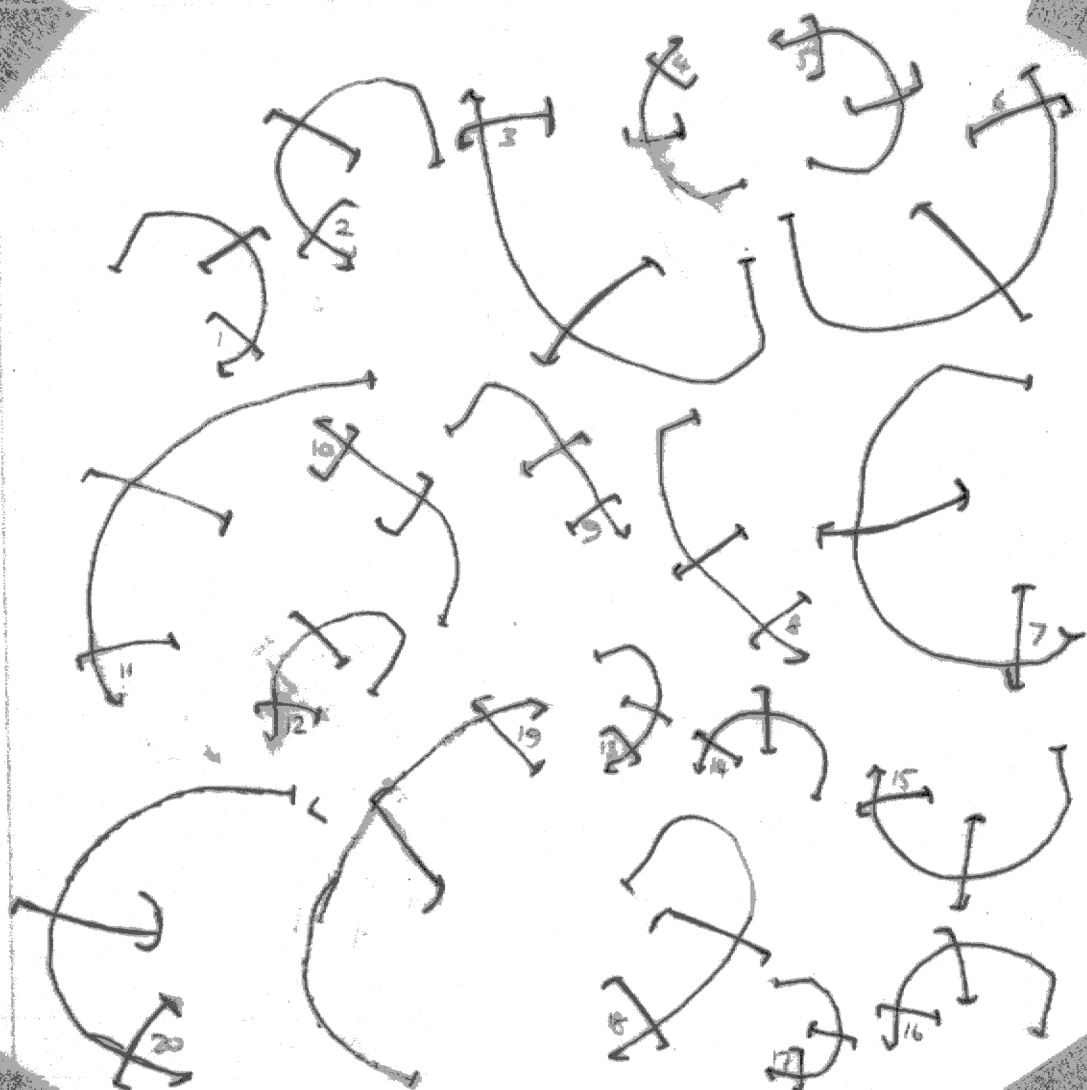
BS

x 2.5

	<u>L</u>	<u>HL</u>	<u>HM</u>	
1	2.05	.3	.425	
2	2.5	.33	.45	
3	3.675	.38	.625	
4	1.6	.25	.3	
5	1.95	.3	.375	
6	3.65	.38	.65	
7	4.03	.55	.675	
8	2.25	.38	.45	
9	1.90	.28	.375	
10	1.93	.28	.375	
11	3.53	.4	.625	
12	2.03	.25	.425	
13	1.28	.23	.275	
14	1.53	.25	.325	
15	2.5	.33	.475	
16	2.13	.28	.4	
17	1.4	.25	.25	- 0.64 int
18	3.08	.38	.55	9.38 st
19	3.93	.48	.6	.923
20	3.85	.5	.625	

$$TL = 9.38 HL - 0.64 \quad r^2 = .923$$

$$HL = 0.091 TL + 0.108 \quad r^2 = .923$$



X20 Q2 25/1/83

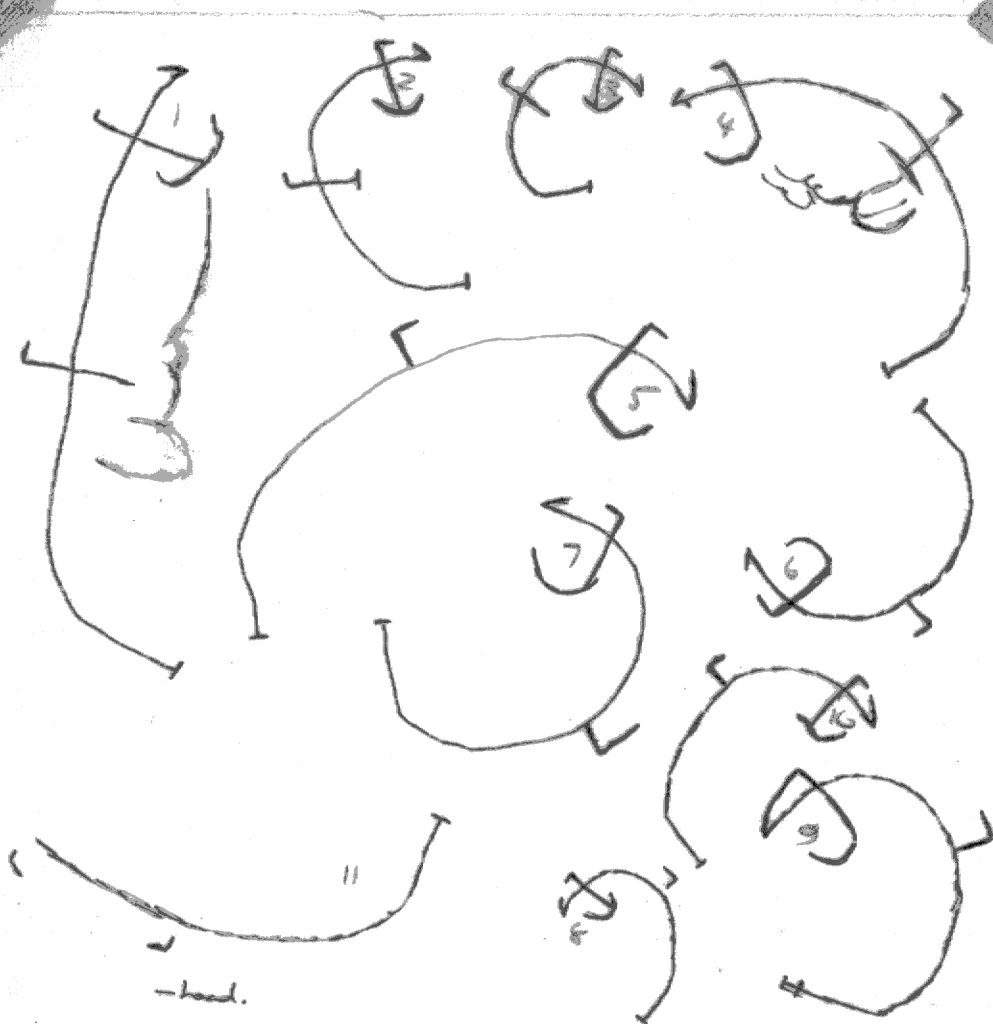
L HL HM

L HL HM

1	25
2	26
3	27
4	28
5	29
6	30
7	31
8	
9	
10	
11	
12	
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14	
15	
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18	
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20	
21	
22	
23	
24	



Q4 x20 25/1/83



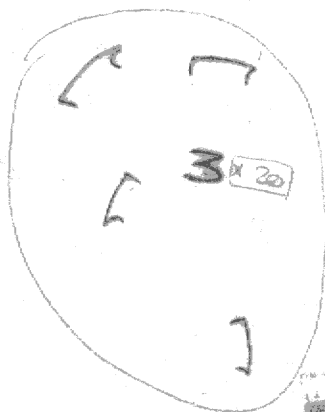
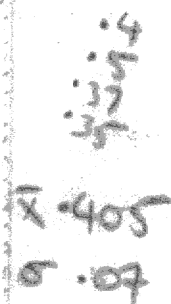
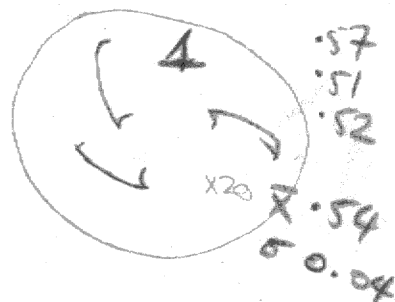
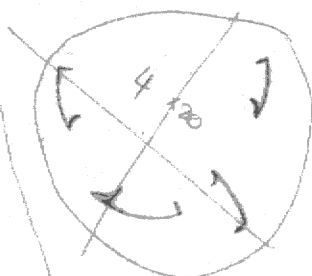
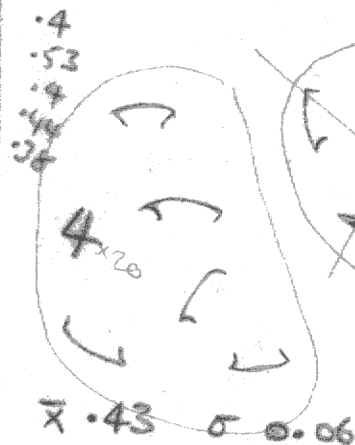
Q4 x20 29/1/83

SEAGRASS D. Wts. JAN.

	T+SQ	-	T	=	SQ
1	7.5		6.1		
2	9.9		6.1		
3	7.7		6.1		
4	9.2		6.1		
5	8.5		6.1		
6	8.9		6.1		

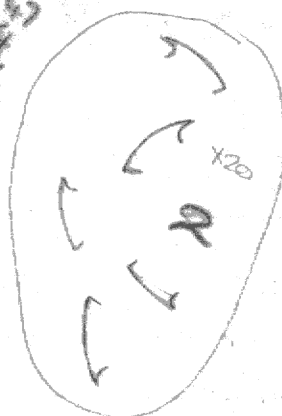
AMPH DWLS

①



$\begin{matrix} .4 \\ .37 \\ .37 \\ .37 \end{matrix}$

$\bar{x} .405 \quad \sigma 0.06$



4
3
3
3
3
3
3
3

9.0.3

23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

8 + 5

6 x 20

7.385
37+ 9.01

39 31 35 37
37 38 39

24 23
22 21
20 19
18 17
16 15
14 13
12 11
10 9
8 7
6 5
4 3
2 1

己未年十月二十四日

1934.10.24

9.34
9.035

2	-	15.527	-	14.301	0.226
4	-	14.425	-	13.810	0.615
8	-	14.105	-	13.820	0.285
5	-	13.423	-	12.995	0.428
3	-	14.503	-	14.034	0.473
7	-	13.932	-	13.298	0.633
6	-	14.346	-	13.987	0.359
1	-	14.580	-	13.647	0.933

Correction = 0.002 due to wt inc

	<u>wt/item</u>	<u>X HL</u>	<u>TL</u>	<u>ASH-FREE wt/Item</u>	<u>% loss</u>
1	.278	.54	4.43	.168/3 = 0.056	39.4
2	.245	.5	4.05	-	-
3	.118	.405	3.16	.405/4 = 0.101	16.83
4	.123	.43	3.39	.545/5 = .109	12.84
5	.061	.366	2.79	.377/7 = .054	12.96
6	.045	.378	2.91	.314/8 = .039	15.38
7	.029	.311	2.28	.566/22 = .026	11.54
8	.012	.25	1.71	.241/24 = .010	20.00
	X		4	-0.216 wt	

$$TL = 9.38 HL - 0.64$$

$$WT = 0.107 TL - 0.216 \quad r^2 = 0.95$$

$$0.107$$

$$r^2 = .95$$

B14

21st FebDRY WTS OF BENTHIC CRUSTACEANS.

2014

<u>Tray No</u>	<u>WT T</u>		<u>WT T+I</u>	<u>WT I</u>
9	12.534	10ha	12.563	0.029 mg.
10	12.560	10ha	12.571	0.011
11	12.757	10ha	12.763	0.006
- 12	13.321	7 co	13.343	0.022 mg.
13	13.291	10ha	13.300(5)	0.009
14	13.891	6 iso	13.906(5)	0.015
15	13.977	10ha	14.001	0.024
16	14.170	10ha	- 14.184	0.014
17	14.052	10ha	14.064	0.012
18	13.896	10ha	13.914	0.018
19	13.510	50ha	13.595	0.085
20	14.709			
21	12.845	10ha	12.856	0.011
22	12.760	10ha	12.772	0.012
23	12.924	control	12.920 + 4	0.006
24	12.976			
25	13.403			
26	13.056			
27	13.446			
28	13.118	15 nematodes	13.146	0.028

$$\bar{x} = 0.0146$$

$$s^2 = 0.0071$$

$$1 \text{ HA} \hat{=} 0.0015 \text{ mg}$$

$$1 \text{ CO} \hat{=} 0.003 \text{ mg.}$$

$$1 \text{ iso} \hat{=} 0.0025 \text{ mg.}$$

$$1 \text{ nm} \hat{=} 0.0019 \text{ mg}$$

$$75 \pm 6 = 1 \text{ amp.}$$

B15

29	13.450	
30	13.079	.002
31	13.203	.001
32	13.075	.021
34	12.415	.002
		.023
35	13.069	.002
33	13.092	

...0005

228

ASH-FREE WTS JAN 23ash
210
cuticle

	T+ Ash	T+ DW	ASH - FREE DWT.	DWT	
1	12.767	12.763	- .004	10 HA .006	—
2	13.137	13.146	.009	15 NM .028	.019
3	13.912	13.914	.002	10 HA .018	.016
4	12.572	12.571	- .001	10 HA .011	—
5	13.365	13.931	.566		—
6	12.860	12.856	- .004	10 HA .01	—
7	14.063	14.064	.001	10 HA .012	.011
8	12.542	12.563	.021	10 HA .029	.008
9	14.182	14.184	.002	10 HA .014	.012
10	13.988	14.001	.023	10 HA .024	.001
11	12.773	12.772	- .001	10 HA .012	
12	13.332	14.001 ?	.669	10 HA .024	
13	13.536	13.595	.059	50 HA .085	.026
14	13.946	13.423	.377		
15	14.412	14.580	.168		
16	13.864	14.105	.241		
17	13.880	14.425	.545		
18	14.032	14.346	.314		
19	14.102	14.507	.405		
20	13.298	13.300	.002	10 HA .009	.007
21	13.893	13.906	.013	618 .015	

ASH-FREE WTS JAN 23

	T+ Ash	T+ DW	ASH - FREE DWt.	DWT	ash exo cuticle
11	12.767	12.763	- .004	10 HA .006	—
28	13.137	13.146	.009	15 NM .028	.019
18	13.912	13.914	.002	10 HA .018	.016
10	12.572	12.571	- .001	10 HA .011	—
7	13.365	13.931	.566		—
21	12.860	12.856	- .004	10 HA .01	—
17	14.063	14.064	.001	10 HA .012	.011
9	12.542	12.563	.021	10 HA .023	.008
16	14.182	14.184	.002	10 HA .014	.012
15	13.988	14.001	.023	10 HA .024	.001
22	12.773	12.772	- .001	10 HA .012	
15	13.332	14.001 ?	.669	10 HA .024	
19	13.536	13.595	.059	50 HA .085	.026
5	13.046	13.423	.377		
1	14.412	14.580	.168		
8	13.864	14.105	.241		
4	13.880	14.425	.545		
6	14.032	14.346	.314		
3	14.102	14.507	.405		
	13.298	13.300	.002	10 HA .009	.0
	13.893	13.906	.013	618 .015	

Wt Tray

13.450

LT

HD

4.4

.48

3.6

.4

4.6

.48

4.72

.52

4.75

.49

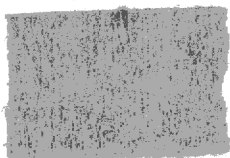
4.1

.5

515

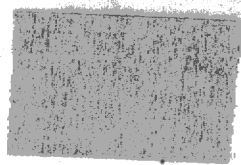
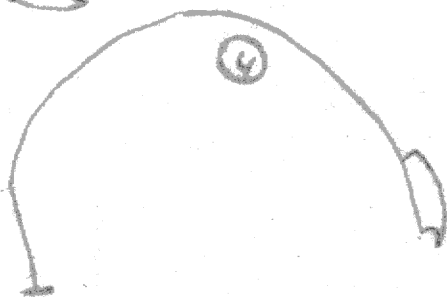
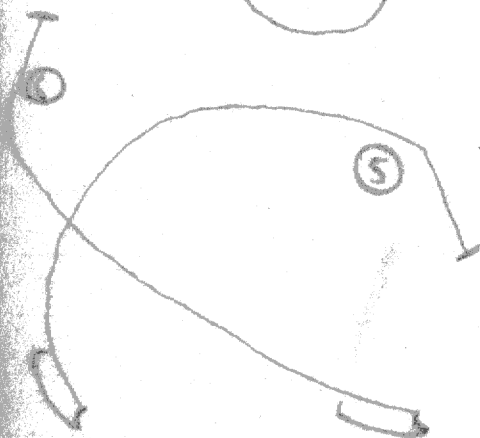
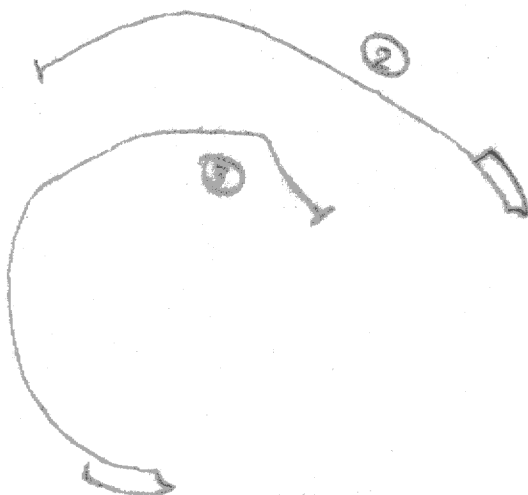
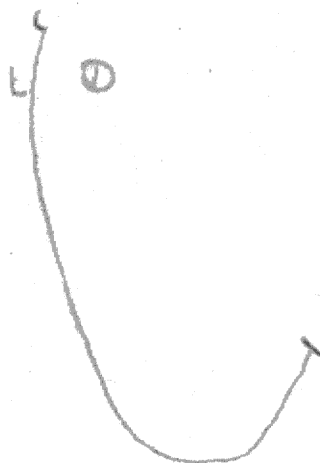
pi 2

LENGTH - WEIGHT



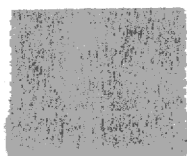
X20

NO 29

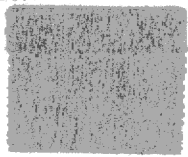
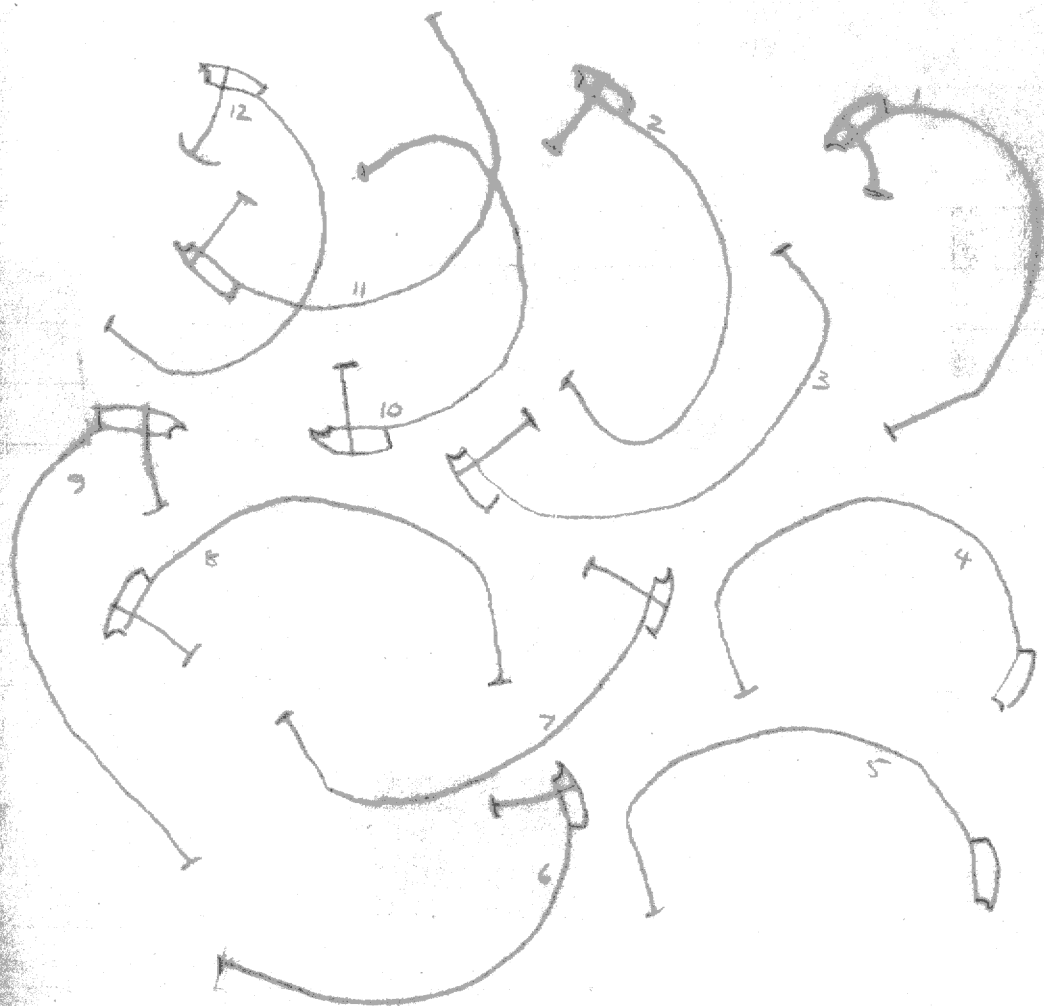


WT Tray

	13.079	HL	<u>HM</u>
1	✓ 3.5	.4	.59
2	✓ 3.6	.39	.59
3	✓ 3.7	.42	.6
4	✓ 3.75	.4	
5	✓ 3.8	.4	
6	✓ 3.25	.36	.55
7	✓ 3.33	.37	.58
8	✓ 3.5	.42	.6
9	✓ 3.9	.5	.62
10	✓ 3.5	.4	.59
11	✓ 3.6	.42	.59
12	3.4	.39	.62



Y20 = 30



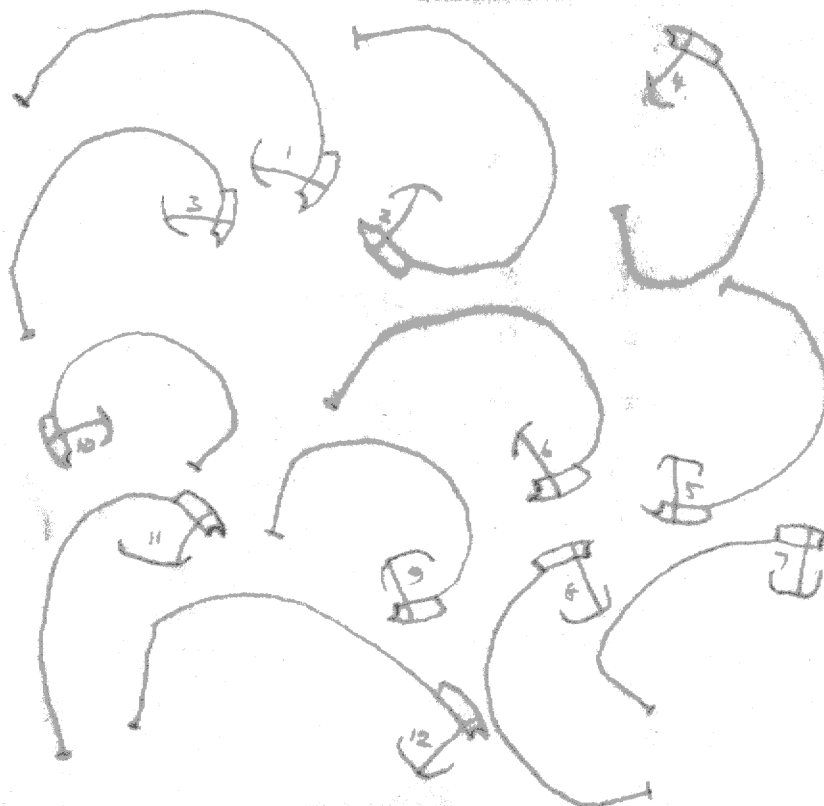
n = 12

Wt Tray

13.203

1	2.98	.35	.52
2	3.25	.35	.52
3	2.72	.31	.45
4	2.73	.32	.5
5	2.48	.31	.41
6	2.97	.37	.48
7	2.2	.3	.45
8	2.6	.35	.49
9	2.62	.32	.43
10	2.38	.29	.43
11	2.47	.3	.45
12	2.98	.4	.55

X20 No 31



$$n = 12$$

Wt Tray

13.075

1	2.3	.29	.4
2	1.92	.25	
3	1.92	.24	.36
4	2.28	.29	.36
5	1.32 2.5	.3	.41
6	1.9	.21	.38
7	2.33	.28	.4
8	2.02	.28	.4
9	2.2	.27	.38
10	1.9	.23	.35

$$y = ax + b$$

$$b/a = 0.069$$

$$a = 0.0945$$

$$r = 0.963$$

$$HL = 0.0945 TL + 0.069$$

$$TL = \frac{HL}{0.0945} - 0.069$$

$$TL = 10.58 HL - 0.069$$

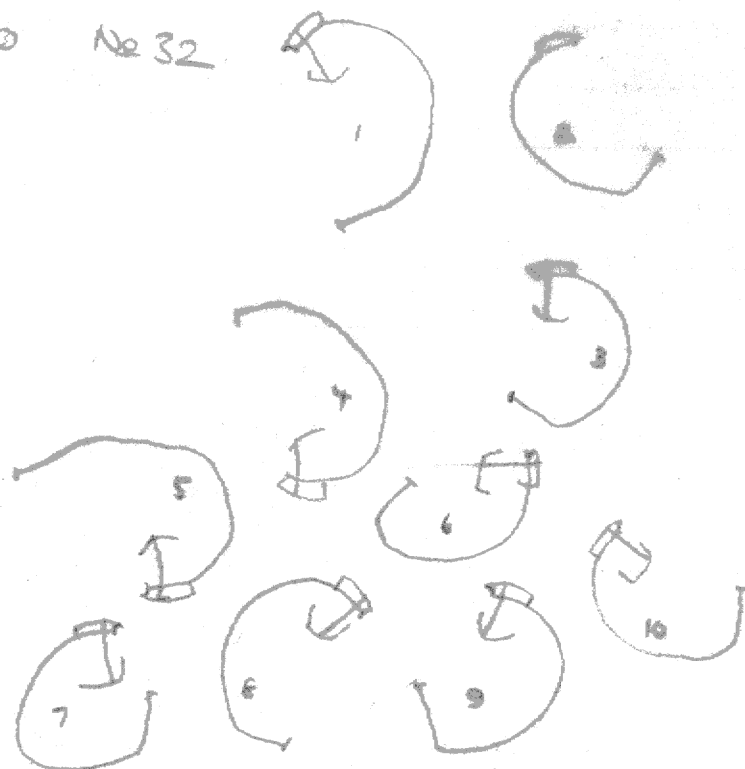
$$TL = 9.83 HL - 0.46$$

$$0.963$$

$$* 9.83 - 0.46 = RST$$

B24

X20 № 32



c - 0.324

a 6.45 r .96

TL = 6.45 MP - 0.324

General methods

① Field sampling

a. Fish

Fish were collected at low tide using a ~~triangular~~ dip net cm across the base. ~~Collections were conducted~~ Sampling was conducted throughout the area to obtain a representative sample from all sections of the seagrass bed. Specimens were bled and preserved in 10% formalin and seawater. To prevent overexploitation of the ~~gob~~ fish population care was taken to select only those sizes and numbers required for analysis.

b) Benthos

~~Benthic samples were collected~~

A 25 cm square quadrat and a small fine meshed dip net were used to collect ~~benthic samples~~ samples of benthic organisms. Random sampling sites ^{were} chosen by dividing the study area into eight sections. A section would be chosen by a random number and from further random number the site would be chosen.

