

Conversion terms

Mean Available Potential Energy to Mean Kinetic Energy

$$C(P_m, K_m) = - \int_V g \bar{\rho} \bar{w} dV$$

Eddy Available Potential Energy to Eddy Kinetic Energy

$$C(P_e, K_e) = - \int_V g \overline{\rho' w'} dV$$

Eddy Kinetic Energy to Mean Kinetic Energy

$$C(K_e, K_m) = \int_V (\rho_o \overline{u' u'} \nabla \bar{u} + \rho_o \overline{v' u'} \cdot \nabla \bar{v}) dV$$

Eddy Available Potential Energy to Mean Available Potential Energy

$$C(P_e, P_m) = - \int_V \frac{g}{n_o} \overline{\rho' u'} \cdot \nabla_h \bar{\rho} dV$$

Generation Terms

Generation of Mean Available Potential Energy

$$G(P_m) = - \int_S g \frac{\alpha_{o,1}}{n_o} \bar{J}_s \bar{\rho}^* dS - \int_S g \frac{\beta_{o,1}}{n_o} \bar{G}_s \bar{\rho}^* dS$$

here J is surface temperature flux

G is surface salinity flux

$\alpha_{o,1}$ and $\beta_{o,1}$ are coefficient of expansions at the top layer

$J_s = \frac{H}{\rho_s c}$ and H is surface heat flux

$G_s = S_1(E - P)$

E is evaporation and P is precipitation

S_1 is the surface salinity

$$\rho^* = \rho - \rho_{ref}$$

$$\rho_{ref} = \langle \bar{\rho} \rangle \text{ where } \langle \dots \rangle \text{ refer to area averaging}$$

Generation of mean Kinetic Energy

$$G(K_m) = \int_S (\overline{\tau_x} \bar{u} + \overline{\tau_y} \bar{v}) dS$$

Generation of Eddy Kinetic Energy

$$G(K_e) = \int_S (\overline{\tau'_x} u' + \overline{\tau'_y} v') dS$$

Generation of Eddy Available Potential Energy

$$G(P_e) = - \int_S g \frac{\alpha_{o,1}}{n_o} \overline{J'_s \rho'} dS - \int_S g \frac{\beta_{o,1}}{n_o} \overline{G'_s \rho'} dS$$

Energy reservoirs

Mean Potential Energy

$$P_m = - \int_V \frac{g}{2n_0} \overline{\rho^*}^2 dV$$

Mean Kinetic Energy

$$K_m = \int_V \frac{1}{2} \rho_0 \left(\overline{u}^2 + \overline{v}^2 \right)$$

Eddy Potential Energy

$$P_e = - \int_V \frac{g}{2n_0} \overline{\rho^{*'}^2} dV$$

Eddy Kinetic Energy

$$K_e = \int_V \frac{1}{2} \rho_0 \left(\overline{u'^2} + \overline{v'^2} \right)$$

Fields to be writtten from POP2 Output

Primes to be calculated

$$\overline{\rho' u'}$$
$$\overline{u' u'} = \overline{u' u'} + \overline{u' v'} + \overline{u' w'}$$
$$\overline{v' u'} = \overline{v' u'} + \overline{v' v'} + \overline{v' w'}$$
$$\overline{\rho' w'}$$
$$\overline{J'_s \rho'}$$
$$\overline{G'_s \rho'}$$
$$\overline{\tau'_x u'}$$
$$\overline{\tau'_y v'}$$

On the value of n_o and Assumptions made for ρ , α , and β

$$\frac{d\rho}{dt} = \left(\frac{\partial \rho}{\partial \theta} \right)_{p,S} \frac{d\theta}{dt} + \left(\frac{\partial \rho}{\partial S} \right)_{p,\theta} \frac{dS}{dt} + \left(\frac{\partial \rho}{\partial z} \right)_{\theta,S} w$$

$$\frac{d\theta}{dt} = \frac{\partial J}{\partial z} \text{ and } \frac{dS}{dt} = \frac{\partial G}{\partial z}$$

This gives us

$$\frac{\partial \rho}{\partial t} + \mathbf{u}_h \cdot \nabla_h \rho + w \left(\frac{\partial \rho}{\partial z} - \left(\frac{\partial \rho}{\partial z} \right)_{S,\theta} \right) = \left(\frac{\partial \rho}{\partial \theta} \right)_{S,p} \frac{\partial J}{\partial z} + \left(\frac{\partial \rho}{\partial S} \right)_{S,\theta} \frac{\partial G}{\partial z}$$

$$\frac{\partial \rho}{\partial t} + \mathbf{u}_h \cdot \nabla_h \rho + w \left(\frac{\partial \rho}{\partial z} \right) = \alpha_o(\lambda, \phi, z) \frac{\partial J}{\partial z} + \beta_o(\lambda, \phi, z) \frac{\partial G}{\partial z}$$

$$\frac{\partial \rho}{\partial z} - \left(\frac{\partial \rho}{\partial z} \right)_{S,\theta} = \frac{\partial \rho}{\partial z}$$

is vertical local potential density gradient

$$\frac{\partial \rho}{\partial z} \approx \frac{\partial \langle \bar{\rho} \rangle}{\partial z} = n_o(z)$$

$$\left(\frac{\partial \rho}{\partial \theta} \right)_{S,p} \approx \left(\frac{\partial \bar{\rho}}{\partial \theta} \right)_{S,p} = \alpha_o(\lambda, \phi, z)$$

$$\left(\frac{\partial \rho}{\partial S} \right)_{\theta,p} \approx \left(\frac{\partial \bar{\rho}}{\partial S} \right)_{\theta,p} = \beta_o(\lambda, \phi, z)$$

The value of α and β used in POP2 in linear Equation of State

$$\alpha_o = \left(\frac{\partial \rho}{\partial T} \right)_{S,p} = 2.55 \times 10^{-4} \text{ gr/cm}^3/\text{K}$$

$$\beta_o = \left(\frac{\partial \rho}{\partial S} \right)_{T,p} = 7.64 \times 10^{-1} \text{ gr/cm}^3/\text{msu}$$

$$1 \text{ gram/kg} = 0.001 \text{ msu}$$

Results

Red are for relative wind forcing

Blue are for absolute wind forcing

Black is from paper [An Estimate of the Lorenz Energy Cycle for the World Ocean Based on the 1/10 STORM/NCEP Simulation](https://journals.ametsoc.org/doi/full/10.1175/JPO-D-12-079.1?searchText=Complex%2BTerrain%2BMesoscale%2BConvective%2BSystems&af=f)
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