



- 1. Introduction
- 2. Levelized Cost of Electricity (LCOE)
- 3. Capital Cost Model
- 4. Operation and Maintenance (O&M) Costs
- 5. Surface Power Plant
- 6. Wellbore Model
- 7. Geologic Reservoir Model
- 8. Well Pattern and Spacing

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genGEO: motivation

genGEO is an open-source package for the **gen**eralizable **GEO**thermal techno-economic simulator from sedimentary basins. genGEO (version 0.0.1) couple the following modules:

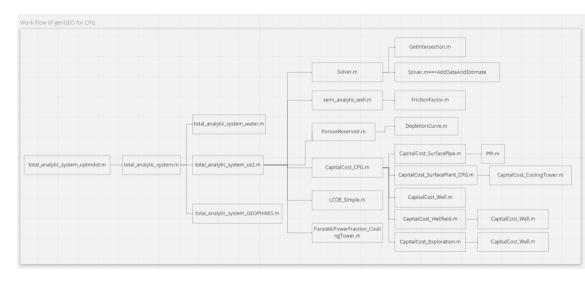
- Levelized Cost of Electricity
- Capital cost
- Surface power plant
- Well model
- Reservoir model



genGEO: Links

- This presentation is hosted in the overleaf project under this Link []
- The Overleaf project for the genGEO draft for future submission to SoftwareX, Link
- The Miroboard planning project Link

genGEO: workflow for CPG



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Module 01: Levelized Cost of Electricity

Simplified LCOE model

The simplified LCOE [\$/W-h] for any geothermal project can be estimated using Equation 1

$$LCOE = \frac{C_{geothermal}}{\bar{W}} \times \frac{CRF + F_{O\&M}}{CF \times 8760}$$
 (1)

where, $C_{geothermal}$: captial cost model [Watts], \overline{W} : Average plant capacity [MWe], $F_{O\&M}$: O&M Cost Fraction [MWe], CF: Capacity Factor [-]. The CRF is the capacity recovery factor (Equation 2)

CRF =
$$\frac{A}{P} = \frac{d \times (1+d)^{FP}}{(1+d)^{FP} - 1}$$
 (2)

where, d: discount rate [-], and FP: Finanical Period[year]

Code repo.

The Matlab code repo. is LCOE_Simple.m

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Capital Cost Model

$$C_{\text{Geothermal}} = C_{\text{Plant}} + C_{\text{Wells}} + C_{\text{SurfacePiping}} + C_{\text{Wellfield}} + C_{\text{Exploration}} + C_{\text{Stimulation}} \tag{3}$$

Code repo.

For a CPG, the Matlab code repo. is CapitalCost_CPG.m Link



Module 02: Capital Cost Model Multipliers for Indirect Costs and Contingency

[A] Indirect Costs multiplier, X_{IC}
X_{IC} calls Engineering, Procurement, and
Construction Management (EPCM) costs,
which are necessary costs for administration,
planning, and design that are separate from
the plant material and labor costs

[B] Contingency Costs multiplier, X_{PC} X_{PC} accounts for unknown costs that are omitted or unforeseen due to a lack of complete project definition and engineering, even though contingencies cannot be explicitly determined at the time the estimate is prepared."

Multipliers for Indirect Costs and Contingency

Component	X _{IC}	X _{PC}
Surface plant	X _{IC-p} : 1.12	X _{PC-p} : 1.15
Wells	X _{IC-well} : 1.05	X _{PC-well} : 1.15
Surface piping	X _{IC-pipe} : 1.12	X _{PC-pipe} : 1.15
Wellfield	X _{IC-wf} : 1.05	X _{PC-wf} : 1.15
Exploration	X _{IC-expl} : 1.05	X _{PC-expl} : 1.15
Stimulation	X _{IC-stim} : 1.05	X _{PC-stim} : 1.15

2.1: Surface Power Plant, CPlant

$$C_{Plant} = X_{PC-p} \times X_{IC-p} \times C_{Plant-BEC}$$
 (4)

where,

$$C_{Plant\text{-BEC}} = C_{Plant\text{-TEC}} \times (1 + X_{CL} + X_{CM} + X_{ST} + X_{F})$$
 (5)

$$C_{Plant-TEC} = C_{Plant-PEC} \times X_{SE}$$
 (6)

$$C_{Plant-PEC} = C_{T-G} + C_{Pump} + C_{C-Tower} + C_{HeatExchanger} + ...$$
 (7)

2.1: Surface Power Plant, CPlant

Cost Multiplier	Value	Description
X _{IC-p}	1.12	Indirect cost multiplier
X _{PC-p}	1.15	Project contingency multiplier
X _{CL}	0.58	Construction Labor Cost (building and assembling, including fringe)
X _{CM}	0.11	Construction Material Cost (concrete, pipe, wire, rentals, etc.)
X _{ST}	0.00	Sales Tax
X_{F}	0.04	Equipment Freight
X _{SE}	1.39	Secondary Equipment Cost (control system, pumps, valves, building, etc.)

2.1: Surface Power Plant, C_{Plant}

2.1.1: Turbine-Generator Cost, C_{T-G}

In genGEO, the specific turbine-generator cost is the GETEM flash turbine-generator cost, with an added coefficient (i.e. 0.67) so the genGEO curve passes through the average NETL coal plant steam turbine cost (Equation 8).

$$C_{\text{T-G}} = 0.67 \times \text{PPI}_{\text{T-G}} \ \left[S_{\text{T-fluid}} \times 2830 \times \left(\dot{W}_{\text{Turbine}} \right)^{0.745} + 3680 \times \left(\dot{W}_{\text{Turbine}} \right)^{0.617} \right] \tag{8}$$

where, $\dot{W}_{Turbine}$ is the turbine-generator gross power [kW_e]. $S_{T-fluid=CO2}$ = 1.20 and for other fluids $S_{T-fluid=other}$ = 1.00

2.1: Surface Power Plant, C_{Plant}

2.1.2: Pump Cost, C_{Pump}

Pumps (injection, production, circulation,...) in geothermal induce a pressure gradient and causing movement. Two type of production well pumps (located several hundred meters below the surface in the production well) are used in geothermal power plant: (1) Lineshaft (considered in genGEO), and (2) Submersible (not considered in genGEO). In genGEO, the total pump cost, C_{Pump}, is given in Equation 9 and is a function of the type of pump (surface or lineshaft) and the pump material.

$$C_{\text{Pump}} = \text{PPI}_{\text{Pump}} \times S_{\text{Pump}} \times C_{\text{Pump-(Surface, Lineshaft)}} \tag{9}$$

where, the pump material multiplier, S_{Pump}, is of 1.00 or 2.09, for Water-based or CO₂-based geothermal power plant, respectively. All sources are given in the table next slide.

$$C_{\text{Pump-Surface}} = 1750 \times \left(1.34 \times \dot{W}_{\text{Pump}}\right)^{0.7} \tag{10}$$

$$C_{\text{Pump-Lineshaft}} = 1750 \times \left(1.34 \times \dot{W}_{\text{Pump}}\right)^{0.7} + 5750 \times \left(1.34 \times \dot{W}_{\text{Pump}}\right)^{0.2} \tag{11}$$

2.1: Surface Power Plant, C_{Plant}

2.1.3: Cooling/Condensing Tower Cost, C_{C-Tower}

In genGEO, the total cost of a cooling or condensing tower, $C_{C\text{-}Tower}$, is determined by a two-step process (Equations): 1) finding the cost of a Baltimore Aircoil Company (BAC) cooling tower with a nominal cooling capacity of 1 MW_{th}, and 2) up-scaling the cost to the cooling capacity required.

$$C_{\text{C-Tower}} = C_{\text{Ref-BAC}} \times \left(\frac{\dot{Q}_{\text{Cooling}} + \dot{Q}_{\text{Condensing}}}{\dot{Q}_{\text{Ref-BAC}}}\right)^{0.8} \tag{12}$$

where,

$$C_{\text{Ref-BAC}} = \text{PPI}_{\text{PE}} \times \dot{Q}_{\text{Ref-BAC}} \times \text{TDC} \times (F_{\text{Cooling}} \times c_{\text{Cooling}} + (1 - F_{\text{Cooling}}) \times c_{\text{Condensing}}) \tag{13}$$

$$F_{Cooling} = \frac{\dot{Q}_{Cooling}}{\dot{Q}_{cooling} + \dot{Q}_{Condensing}}$$
 (14)

2.1: Surface Power Plant, CPlant

2.1.4: Heat Exchanger cost, C_{HeatExchanger}

Heat exchangers are used within a geothermal power cycle to transfer heat from one fluid to another, for instance, within evaporators or condensers. The cost of the heat exchanger is the product of the heat exchanger type cost and the heat exchanger cost index, PPI_{HX}. There are four types of heat exchanger costs in genGEO: shell&tube (C_{S&T}), gasketed plate (C_{GasketedPlate}), welded plate (C_{WeldedPlate}), and bonded plate (C_{BondedPlate}) (as shown in Equation 15)

$$C_{\text{HeatExchanger}} = \text{PPI}_{\text{HX}} \times C_{\text{S\&T, GasketedPlate, WeldedPlate, BondedPlate}} \tag{15}$$

where.

$$C_{S\&T} = 239 \times A_{HX} + 13400 \tag{16}$$

$$C_{\text{GasketedPlate}} = 29 \times A_{\text{HX}} + 1560 \tag{17}$$

$$C_{\text{WeldedPlate}} = 69 \times A_{\text{HX}} + 4670 \tag{18}$$

$$C_{BondedPlate} = 2.6 \times (69 \times A_{HX} + 4670) \tag{19}$$

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2.1: Surface Power Plant, C_{Plant} - Heat Exchanger Cont.

Assuming that the heat transferred through the exchanger, \dot{Q} , is known, then Equation 20 is used to calculate the Heat Transfer Area, A_{HX} .

$$\dot{Q} = U \times A_{HX} \times \Delta T_{LMTD} \tag{20}$$

where, ΔT_{LMTD} is the Log Mean Temperature Difference, and U is the overall Heat Transfer Coefficient,

$$\Delta \mathsf{T}_{\mathsf{LMTD}} = \frac{\Delta \mathsf{T}_{\mathsf{A}} - \Delta \mathsf{T}_{\mathsf{B}}}{\ln \left(\frac{\Delta \mathsf{T}_{\mathsf{A}}}{\Delta \mathsf{T}_{\mathsf{B}}}\right)} \tag{21}$$

It is a function of the temperature differences at arbitrarily assigned ends "A", ΔT_B , and "B", ΔT_B

2.2: Well Cost, Cwells

The total cost of the wells in genGEO is the sum of the cost of each of the total number of wells drilled, C_{Wells}, as provided in Equations 22.

$$C_{\text{Wells}} = \sum_{i=1}^{G_{\text{wells}}} \left(C_{\text{Well-drilling},i} + \Delta C_{\text{CO2-Well},i} \right) \tag{22}$$

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In the following slide, all equations costs are based on 2002\$. Therefore, costs are adjusted by year using the pipe cost index, PPI_{O8G}

2.2: Well Cost, Cwells

2.2.1: Geothermal Drilling Success Rate, C_{Well-drilling}

$$C_{\text{Well-drilling}} = \frac{C_{\text{Well}}}{S_{\text{Well}}} \tag{23}$$

The values of the well success rate in genGEO, S_{Well} , is given as 95%, 75%, and 90% for oil-gas (sedimentary), traditional geothermal (fractured), and EGS (basement), respectively.

2.2.2: Geothermal Well Cost, Cwell: Cost in 2002\$

$$C_{Well}(Baseline) = X_{IC\text{-well}} \times X_{PC\text{-well}} \times PPI_{O\&G} \times \left(0.105 \times L_{Well}^2 + 1776 \times L_{Well} \times D_{Well} + 275300\right) \ (24)$$

$$C_{\text{Well}}(\text{Ideal}) = X_{\text{IC-well}} \times X_{\text{PC-well}} \times \text{PPI}_{\text{O\&G}} \times (1288 \times L_{\text{Well}} \times D_{\text{Well}} - 62 \times L_{\text{Well}} + 275300) \tag{25}$$

2.2.3: Well Cost Adjustment for CO_2 , $\triangle C_{CO2\text{-Well}}$

$$\Delta C_{\text{CO2-Well}} = X_{\text{IC-well}} \times X_{\text{PC-well}} \times \text{PPI}_{\text{O\&G}} \times \left(265 \frac{\$}{\text{m}^2} \times L_{\text{Well}} \times D_{\text{Well}} + 133 \frac{\$}{\text{m}} \times L_{\text{Well}}\right) \tag{26}$$

2.3: Surface Piping System Cost, C_{Surface Piping}

Surface Piping System Cost (or field gathering system) is predominantly the pipe cost to connect the wellheads to the central generating plant (Equations).

$$C_{SurfacePiping} = X_{IC\text{-Pipe}} \times X_{PC\text{-Pipe}} \times PPI_{Pipe} \times (c_{SpecfSurfacePiping} \times L_{Pipe})$$
 (27)

where,

$$c_{\text{SpectSurfacePiping}} = 2205 \frac{\$}{\text{m}^3} \times D_{\text{Pipe}}^2 + 134 \frac{\$}{\text{m}}$$
 (28)

The above equations are given based on 2002\$ cost.

2.4: Wellfield Development Costs, Cwellfield

Wellfield development costs include the cost to permit and develop a geothermal power plant site. For CO₂-based geothermal system, additional permit and monitoring wells and equipment must be included (Equation 29).

$$C_{\text{Wellfield}} = C_{\text{Permitting}} + \Delta C_{\text{Permitting-CO}_2} + \Delta C_{\text{Monitoring-CO}_2}$$
 (29)

For CO_2 monitoring well, the wellfield costs are normalized by the Active Monitoring Area (AMA), $A_{CO2-AMA}$, of the CCS development. The AMA is the Area of Review (AOR), $A_{CO2-AOR}$, plus a 0.5 mile (800 m) buffer on all sides.

$$\begin{split} A_{\text{CO2-AOR}} &= (L_{\text{Wellzone}})^2 \\ A_{\text{CO2-AMA}} &= (L_{\text{Wellzone}} + 1600\text{m})^2 \end{split} \tag{30}$$

2.4: Wellfield Development Costs, Cwellfield

2.4.1: Base Wellfield Development Costs, C_{Permitting}

$$C_{\text{Permitting}} = X_{\text{IC-wf}} \times X_{P\text{C-wf}} \times PPI_{\text{Permit}} \times \left(665700 \frac{\$}{\text{site}}\right)$$
(31)

2.4.2: Wellfield Cost Adjustment for CO_2 permitting, $\triangle C_{Permitting-CO_2}$

$$\Delta C_{\text{Permitting-CO}_2} = X_{\text{IC-wf}} \times X_{\text{PC-wf}} \times \text{PPI}_{\text{Permit}} \times \left(45000 \frac{\$}{\text{km}^2}\right) \times \frac{1 \text{ km}^2}{10^6 \text{ m}^2} \times A_{\text{CO}_2,\text{AMA}} \tag{32}$$

2.4.3: Wellfield Cost Adjustment for CO₂ monitoring, $\Delta C_{Monitoring-CO_2}$

$$\Delta C_{Monitoring-CO_2} = C_{MonitoringWells-CO_2} + C_{SurfaceMonitoring-CO_2}$$
(33)

where,

$$C_{\text{MonitoringWells-CO}_2} = G_{\text{MonitoringWells-CO}_2} \times C_{\text{Well,D=21.6 cm}} \tag{34}$$

$$C_{\text{SurfaceMonitoring-CO}_2} = X_{\text{IC-wf}} \times X_{\text{PC-wf}} \times \text{PPI}_{\text{O\&G-s}} \times \left(138000 \frac{\$}{\text{km}^2}\right) \times \frac{1 \text{ km}^2}{10^6 \text{ m}^2} \times A_{\text{CO2,AMA}} \tag{35}$$

2.5: Exploration Costs, C_{Exploration}

The exploration cost, consists of two primary tasks: drilling exploration wells and reservoir modeling.

$$C_{\text{Exploration}} = C_{\text{Modeling}} + \Delta C_{\text{CharaterizationWells}} + \Delta C_{\text{Modeling,CO}_2}$$
 (36)

where,

$$C_{\text{Modeling}} = X_{\text{IC-expl}} \times X_{\text{PC-expl}} \times PPI_{\text{O\&G-s}} \times \left(508000 \frac{\$}{\text{site}}\right)$$
(37)

$$\Delta C_{\text{CharacterizationWells}} = 0.2 \times C_{\text{Well}} \times \frac{G_{\text{CharacterizationWells}}}{S_{\text{Well}}} \tag{38}$$

$$\Delta C_{\text{Modeling, CO}_2} = X_{\text{IC-expl}} \times X_{\text{PC-expl}} \times \text{PPI}_{\text{O\&G-s}} \times \left(44800 \frac{\$}{\text{km}^2}\right) \times \frac{1 \text{ km}^2}{10^6 \text{ m}^2} \times A_{\text{CO}_2,\text{AMA}} \tag{39}$$

2.6: Well Stimulation Costs, C_{Stimulation}

$$C_{\text{Stimulation}} = \begin{cases} 0, & (\text{Hydrothermal}) \\ X_{\text{IC-stim}} \times X_{\text{PC-stim}} \times G_{\text{Wells}} \times 715000, & (\text{EGS}) \end{cases}$$
(40)

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Module 03: Operation and Maintenance (O&M) Costs

Operation and maintenance (O&M) costs, $C_{O\&M}$, are needed to calculate the Levelized Cost of Electricity (LCOE) of any electricity generator. genGEO reports O&M cost in this analysis with respect to three commonly reported sub-costs: 1) Labor, 2) Material, and 3) Taxes and Insurance. genGEO suggests the O&M cost fraction, $F_{O\&M}$, may be approximated as 5.5%.

$$C_{\text{O\&M}} = 0.055 \times C_{\text{Geothermal}} \tag{41}$$

where, $C_{\text{Geothermal}}$ can be estimated using Equation 3.

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4.1: Surface Power Plant Type



4.2: Organic Rankine Cycle (ORC)

4.3: ORC Design Optimizations

4.3.1: Maximize Specific Electric Power

4.3: ORC Design Optimizations

4.3.2: Minimize Specific Electric Cost

4.3: ORC Design Optimizations

4.3.3: Optimization Results

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Module 05: Wellbore Model

The heat conduction through the wellbore is found by applying a 1-D analytical solution of radial heat conduction in a semi-infinite solid from Carslaw & Jaeger (1959) to each element. The wellbore is numerically solved for pressure, P, (Equation 42) and enthalpy, h, (Equation 43) for each element, *i*.

$$P_{i+1} = P_i - (\rho \times g \times \Delta z) - \Delta P_{Loss,i}$$
(42)

$$h_{i+1} = h_i - g \times \Delta z - \frac{\dot{Q}_{Loss,i}}{\dot{m}} \tag{43}$$

where,

$$\dot{Q}_{\rm Loss,i} = \Delta z \times 2 \times \pi \times k_{\rm Rock} \times \beta \times (T_{\rm w,\,i} - T_{\rm e,i}) \tag{44} \label{eq:Qloss}$$

$$\beta = \begin{cases} (\pi \times t_d)^{-0.5} + \frac{1}{2} - \frac{1}{4} \left(\frac{t_d}{\pi} \right)^{0.5} + \frac{1}{8} t_d, & t_d \le 2.8 \\ \\ \frac{2}{\ln(4 \times t_d) - 1.16} - \frac{1.16}{(\ln(4 \times t_d) - 1.16)^2}, & t_d > 2.8 \end{cases}$$
(45)

$$t_{d} = \frac{k_{Rock}}{\rho_{Rock} \times c'_{Rock}} \frac{4 \times t}{D_{Woll}^{2}}$$
(46)

Module 05: Wellbore Model

5.1: Effect of Wellbore Heat Loss

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Module 06: Geologic Reservoir Model

6.1: Reservoir Impedance Model

The reservoir impedance is the ratio of the pressure difference between the injection well downhole and production well downhole to the mass flowrate through the reservoir. This value is essential to determine (I) the circulation flowrate of a geofluid, (II) how much pumping is required, (III) the ease at which geothermal heat can be extracted from a reservoir, (Iv) and ultimately the profitability of doing so.

For 5-spot well pattern: (Equation 47)

$$\frac{\Delta P}{\dot{m}} = \frac{\bar{\mu}}{\bar{\rho}} \times \frac{1}{\kappa b} \times \frac{1}{4} \times \ln\left(\frac{4L}{\pi D}\right) \tag{47}$$

• For a well-doublet: (Equation 48)

$$\frac{\Delta P}{\dot{m}} = \frac{\bar{\mu}}{\bar{\rho}} \times \frac{1}{\kappa b} \times \frac{1}{\pi} \times \ln\left(\frac{L}{eD}\right)$$
 (48)

where e is Euler's number.

Code repo.

The Matlab code repo. is PorousReservoir.m

Module 06: Geologic Reservoir Model

6.2: Thermal Depletion Model

Two types of geothermal reservoirs:

- Thermally replenishing reservoirs are connected to deep, high-temperature heat sources via
 fractures, and thus the production temperature of geofluid removed from them tends to be
 relatively constant through fluid advection.
- Thermally isolated reservoirs have no connections to deep heat sources and have only a finite
 amount of heat to extract, which may be augmented by heat conduction from surrounding
 geologic layers. In this case, the non-dimensional temperature (Equation 49) is the ratio of
 reservoir production temperature less the reservoir injection temperature to the initial reservoir
 production temperature, less the reservoir injection temperature.

$$\Gamma = \frac{\mathsf{T} - \mathsf{T}_{\mathsf{inj}}}{\mathsf{T}_{\mathsf{initial}} - \mathsf{T}_{\mathsf{inj}}} \tag{49}$$

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Module 07: Well Pattern and Spacing







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