

## Nozzle, Steam Nozzle and Steam Turbine

### STAGNATION, SONIC PROPERTIES AND ISENTROPIC EXPANSION IN NOZZLE

The stagnation values are useful reference conditions in a compressible flow. Suppose the properties of a flow (such as  $T$ ,  $p$ ,  $\rho$  etc.) are known at a point. The stagnation properties at a point are defined as those which are to be obtained if the local flow were imagined to cease to zero velocity isentropically. The stagnation values are denoted by a subscript zero. Thus, the stagnation enthalpy is defined as

$$h_0 = h + \frac{1}{2}V^2$$

For a calorically perfect gas, this yields,

$$c_p T_0 = c_p T + \frac{1}{2}V^2 \quad (18.1)$$

which defines the stagnation temperature. It is meaningful to express the ratio of  $(T_0 / T)$  in the form

$$\begin{aligned} \frac{T_0}{T} &= 1 + \frac{V^2}{2c_p T} = 1 + \frac{\gamma - 1}{2} \cdot \frac{V^2}{\gamma R T} \\ \text{or, } \frac{T_0}{T} &= 1 + \frac{\gamma - 1}{2} Ma^2 \end{aligned} \quad (18.2)$$

If we know the local temperature ( $T$ ) and Mach number ( $Ma$ ), we can find out the stagnation temperature  $T_0$ . Consequently, isentropic relations can be used to obtain stagnation pressure and stagnation density as.

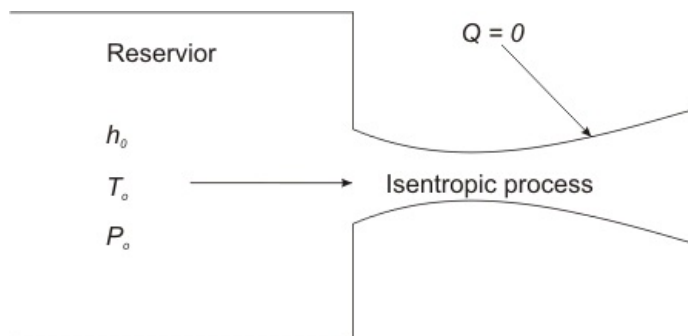
$$\frac{p_0}{p} = \left( \frac{T_0}{T} \right)^{\frac{\gamma}{\gamma-1}} = \left[ 1 + \frac{\gamma-1}{2} Ma^2 \right]^{\frac{\gamma}{\gamma-1}} \quad (18.3)$$

$$\frac{\rho_0}{\rho} = \left( \frac{T_0}{T} \right)^{\frac{1}{\gamma-1}} = \left[ 1 + \frac{\gamma-1}{2} Ma^2 \right]^{\frac{1}{\gamma-1}} \quad (18.4)$$

In general, the stagnation properties can vary throughout the flow field.

However, if the flow is adiabatic, then  $h + \frac{V^2}{2}$  is constant throughout the flow. It follows that the  $h_0, T_0$

and  $a_0$  are constant throughout an adiabatic flow, even in the presence of friction. Here  $a$  is the speed of sound and the suffix signifies the stagnation condition. It is understood that all stagnation properties are constant along an isentropic flow. If such a flow starts from a large reservoir where the fluid is practically at rest, then the properties in the reservoir are equal to the stagnation properties everywhere in the flow (Fig. 18.1).



**Fig 18.1 An isentropic process starting from a reservoir**

There is another set of conditions of comparable usefulness where the flow is sonic,  $Ma=1.0$ . These sonic, or critical properties are denoted by asterisks:  $p^*, \rho^*, a^*$ , and  $T^*$ . These properties are attained if the local fluid is imagined to expand or compress isentropically until it reaches  $Ma=1$ .

We have already discussed that the total enthalpy, hence  $T_0$ , is conserved so long the process is adiabatic, irrespective of frictional effects. In contrast, the stagnation pressure  $p_0$  and density  $\rho_0$  decrease if there is friction.

From Eq.(18.1), we note that

$$\begin{aligned} V^2 &= 2c_p(T_0 - T) \\ \text{or, } V &= \left[ \frac{2\gamma R}{\gamma-1} (T_0 - T) \right]^{\frac{1}{2}} \end{aligned} \quad (18.5a)$$

is the relationship between the fluid velocity and local temperature ( $T$ ), in an adiabatic flow. The flow can attain a maximum velocity of

$$V_{\max} = \left[ \frac{2\gamma RT_0}{\gamma - 1} \right]^{\frac{1}{2}} \quad (18.5b)$$

As it has already been stated, the unity Mach number,  $Ma=1$ , condition is of special significance in compressible flow, and we can now write from Eq.(18.2), (18.3) and (18.4).

$$\frac{T_0}{T^*} = \frac{1+\gamma}{2} \quad (18.6a)$$

$$\frac{p_0}{p^*} = \left( \frac{1+\gamma}{2} \right)^{\frac{\gamma}{\gamma-1}} \quad (18.6b)$$

$$\frac{\rho_0}{\rho^*} = \left( \frac{1+\gamma}{2} \right)^{\frac{\gamma}{\gamma-1}} \quad (18.6c)$$

For diatomic gases, like air  $\gamma=1.4$ , the numerical values are

$$\frac{T^*}{T_0} = 0.8333, \quad \frac{p^*}{p_0} = 0.5282, \quad \text{and} \quad \frac{\rho^*}{\rho_0} = 0.6339$$

The fluid velocity and acoustic speed are equal at sonic condition and is

$$V^* = a^* = [\gamma RT^*]^{\frac{1}{2}} \quad (18.7a)$$

$$\text{or,} \quad V^* = \left[ \frac{2\gamma}{\gamma+1} RT_0 \right]^{\frac{1}{2}} \quad (18.7b)$$

We shall employ both stagnation conditions and critical conditions as reference conditions in a variety of one dimensional compressible flows.