

$$\text{stage efficiency} = \eta_s = \frac{\text{Work done by the rotor}}{\text{Isentropic enthalpy drop}} \quad (23.1)$$

$$\eta_s = \frac{\dot{m} U \Delta V_w}{\dot{m} (\Delta H)_{isen}} = \frac{\dot{m} U \Delta V_w}{\dot{m} \left(\frac{V_1^2}{2} \right)} \cdot \frac{\dot{m} (V_1^2 / 2)}{\dot{m} (\Delta H)_{isen}} \quad (23.2)$$

or,

$$\text{or, } \eta_s = \eta_b \times \eta_n \quad [\eta_n = \text{Nozzle efficiency}] \quad (23.3)$$

Optimum blade speed of a single stage turbine

$$\begin{aligned} \Delta V_w &= V_{r1} \cos \beta_1 + V_{r2} \cos \beta_2 \\ &= V_{r1} \cos \beta_1 + \left(1 + \frac{V_{r2}}{V_{r1}} \cdot \frac{\cos \beta_2}{\cos \beta_1} \right) \\ &= (V_1 \cos \alpha_1 - U) + (1 + kc) \end{aligned} \quad (23.4)$$

where, $k = (V_{r2} / V_{r1}) = \text{friction coefficient}$

$$\begin{aligned} c &= (\cos \beta_2 / \cos \beta_1) \\ \eta_b &= \frac{2U \Delta V_w}{V_1^2} = 2 \frac{U}{V_1} \left(\cos \alpha_1 - \frac{U}{V_1} \right) (1 + kc) \\ \rho &= \frac{U}{V_1} = \frac{\text{Blade speed}}{\text{Fluid velocity at the blade inlet}} = \text{Blade speed ratio} \quad (23.5) \end{aligned}$$

$$\eta_b \text{ is maximum when } \frac{d\eta_b}{d\rho} = 0 \text{ also } \frac{d^2\eta_b}{d\rho^2} = -4(1 + kc)$$

$$\begin{aligned} \text{or, } \frac{d}{d\rho} \{ 2(\rho \cos \alpha_1 - \rho^2) (1 + kc) \} &= 0 \\ \text{or, } \rho &= \frac{\cos \alpha_1}{2} \quad (23.6) \end{aligned}$$

α_1 is of the order of 18° to 22°

$$\text{Now, } (\rho)_{opt} = \left(\frac{U}{V_1} \right)_{opt} = \frac{\cos \alpha_1}{2} \quad (\text{For single stage impulse turbine})$$

\therefore The maximum value of blade efficiency

$$\begin{aligned} (\eta_b)_{\max} &= 2(\rho \cos \alpha_1 - \rho^2) (1 + kc) \\ &= \frac{\cos^2 \alpha_1}{2} (1 + kc) \end{aligned} \quad (23.7)$$

For equiangular blades,

$$(\eta_b)_{\max} = \frac{\cos^2 \alpha_1}{2} (1 + k) \quad (23.8)$$

If the friction over blade surface is neglected

$$(\eta_b)_{\max} = \cos^2 \alpha_1 \quad (23.9)$$