

Evolution of a Triad Twisted String Actuator for Controlling a Two Degrees of Freedom Joint to Improve Performance and Allow for Active Transmission Adjustment

Damian Crosby, Joaquin Carrasco *Member, IEEE*, William Heath *Member, IEEE*, and Andrew Weightman

Abstract—

Index Terms—Flexible Robots, Force Control, Tendon/Wire Mechanism, Twisted String Actuator.

I. INTRODUCTION

II. IMPROVEMENTS TO ORIGINAL DESIGN

A. Increasing AUJ Angle Range

The AUJ angle tracking experiments in [1] only had a range of $\pm 14.5^\circ$ in a single axis, and $\pm 6^\circ$ for both axes. This was because one or more twisted string actuator (TSA) would completely “unwind” near that limit and be unable to lengthen further. This limits the practicality of such a mechanism, for example a multi-segment design would have a very large minimum curvature. Increasing f_{\min} does increase the angle range marginally by increasing the TSA motor angle at $\theta = [0 \ 0]^\top$, \approx for the original design, as shown in figure ???. However, this has other effects that are further explained in section II-D that may be undesirable for the application.

In order to increase the angle range significantly, the value of r has to be reduced as shown in figure ??. This can be done by using smaller motors, or by using the same size or larger motors with offset shafts connected by spur gears. Smaller motors were chosen, Micro Metal Gearmotor (50:1), as they were lighter than the existing motors and the mechanism would be less complex. These motors would have a much lower θ_{\max} than the existing motors of only rad s^{-1} compared to rad s^{-1} , but since the original experiments limited the motor velocity to rad s^{-1} to ensure mechanism stability, this is not a concern.

This design change allowed r to be reduced from 13 mm to 7.25 mm. This reduces the TSA stroke range for a given AUJ angle range accordingly, which also reduces the TSA motor angle accordingly, allowing a greater AUJ angle to be reached before one or more TSA unwind.

D. Crosby, and A. Weightman are with the Department of Mechanical, Aerospace and Civil Engineering, School of Engineering, Faculty of Science and Engineering, The University of Manchester, Manchester, United Kingdom.

J. Carrasco and W. Heath are with the Department of Electrical and Electronic Engineering, School of Engineering, Faculty of Science and Engineering, The University of Manchester, Manchester, United Kingdom.

B. Improving AUJ Angle Measurement Accuracy

The original design used a Bosch Sensortec BNO080 9 degree of freedom (DOF) inertial measurement unit (IMU) [2] to measure the AUJ orientation. Originally it was planned for a pair of these IMU to be used, one on the base segment and one on the follower segment, and the orientation of the AUJ to be calculated from the difference between them in any orientation. However, the magnetometer measurements proved to be unreliable inside the laboratory, so only a single IMU was used and the base segment was orientated with the gravity vector parallel to the z axis. This allowed the AUJ orientation to be calculated from only the accelerometer readings, but meant the mechanism could only be controlled when orientated in the vertical axis.

There was also an issue with the IMU resolution as shown in figure ??, which is only only accurate to within 0° . A Savitsky-Golay filter was applied to the results in [1] for data presentation purposes and to more accurately represent the true AUJ angles at that point in time.

In order to allow the mechanism to be controllable for any orientation with respect to gravity, a solution that could directly measure the mechanical angular displacement of the universal joint was needed. Two options were considered, potentiometers and hall effect sensors. A potentiometer would couple a shaft of each universal joint spider axes to a resistive track, changing its resistance depending on AUJ orientation and providing an analog voltage signal to the controller. A hall effect sensor would be similar to the potentiometer solution, but would use a radially bipolar magnet on the end of the shaft with a hall effect sensor beneath it, which would also provide an analog voltage signal or digital data for the axial orientation of the magnet, and therefore the shaft [3]. The potentiometer solution was chosen for easy availability of components and simplicity of control integration, since no programming of the sensor would be required. The potentiometer also has mechanical stops, which make it easier to assure the required AUJ angle range will be able to be measured during assembly. The hall effect sensor is continuous, and the measured voltage overflows every 180° [3], so it would be very important to ensure the magnet was oriented at a value that would encompass both the

maximum and minimum joint limit for each AUJ axis. The Bourns PDB08 was selected as the potentiometer due to its small size and internally threaded shaft, which would allow a captive bolt to be inserted as the spider shaft [4]. As a voltage divider at +5 V, the PDB08 would have a resolution of approximately 40° V^{-1} . With the 12-bit resolution of the onboard analog to digital converter (ADC) for myRIO analog inputs, this gives a theoretical resolution of $\approx 0.048^\circ$. The potentiometer sliding noise (max. 100 mV) will reduce this during AUJ motion, however this can be partially mitigated with filtering.

C. Preventing String Failure

One reoccurring issue with the original experiments were the TSA strings breaking at high values of θ_s , which became more common after a number of twisting and untwisting cycles. Occasionally this was caused by the mechanism operating beyond expected limits for θ_s and f due to a failure of limit monitoring within the control system, but failure would also occur within normal operating conditions.

Analysis of the design and the location of the string failures identified “pinch points” and “bite points”, as shown in figure ??, which could potentially damage the string under high tension, causing it to thin out and lose integrity. By removing these points, by rounding off sharp edges and using an alternative method to secure the string, tying it into a loop instead of using grub screws, eliminated these potential sources of string damage. However, nylon monofilament, as was used for the TSA string, is still susceptible to torsion fatigue [5], [6] which reduces tensile strength [7]. This means the monofilament string will be increasingly susceptible to failure with more twisting and untwisting cycles. Therefore, the SeaKnight BLADE 0.2mm nylon monofilament was exchanged for 0.2mm Dyneema[®] polyfilament string, as used in [8]. Changes to the design of the string clamp allowed for easier installation of string filament, making polyfilament string a practical option.

D. Enabling ATA

Active transmission adjustment (ATA) allows the dynamic properties of the AUJ to change during operation, with a trade off between f_{\max} and \dot{p}_{\max} . With ATA a robot could increase joint force when necessary, such as when lifting a heavy payload, and then return to a faster and more responsive configuration when the payload has been released. As r has been reduced from 0.013 to 0.0725 as shown in table ??, this reduces the TSA stroke range p for a given AUJ angle range. Now the stroke range is smaller, it can be shifted along the curve of the function in equation ?? without exceeding l_{\min} . This is done by simply increasing or decreasing f_{\min} . As shown in figure ??, this changes the range of values of f_{\max} and \dot{p}_{\max} . Namely, f_{\max} decreases and \dot{p}_{\max} increases as f_{\min} increases, which changes the transmission properties of the system.

III. EXPERIMENTAL RESULTS

A. AUJ Angle Tracking

B. Demonstration of the Effects of ATA

As can be seen in figure ??, the effect of increasing f_{\min} is to decrease f_{\max} and increase \dot{p}_{\max} . This has two measurable effects, an increase in total energy consumption for a given follower mass and AUJ angle trajectory, and an increase in the maximum stroke speed for a given θ_{\max} for each motor. Therefore to demonstrate the effects of ATA, two experiments are conducted. The first measures the total energy consumption for a given AUJ angle trajectory at increasing values of f_{\min} . The total energy consumption can then be calculated using

$$\Sigma_j = \int_{t_0}^{t_n} \sum_{i=1}^3 v_s a_i(t) |d_i(t)| dt, \quad (1)$$

where v_s is the motor supply voltage, and a_i and d_i are the current consumption and duty cycle $\in [-1, 1]$ (d_i has a negative duty cycle when the motor is running in reverse) of motor i at time t . Figure 2 shows this increase. The second measures the ability of the AUJ to track a trajectory at a constantly increasing velocity given a constrained θ_{\max} . Since increasing f_{\min} increases \dot{p}_{\max} , a larger value of f_{\min} should allow the AUJ to track the trajectory for a longer period of time before falling behind. Figure ?? shows this effect.

Test.

An experiment was also conducted to assess the performance of the system when f_{\min} is changed while the AUJ is in motion at a non-zero position. The results of this experiment are shown in figure ??, and show minimal disturbance to the AUJ trajectory during the transition.

C. The Effect of Follower Mass on AUJ Angle Tracking

IV. DISCUSSION

V. CONCLUSION

VI. ACKNOWLEDGEMENT

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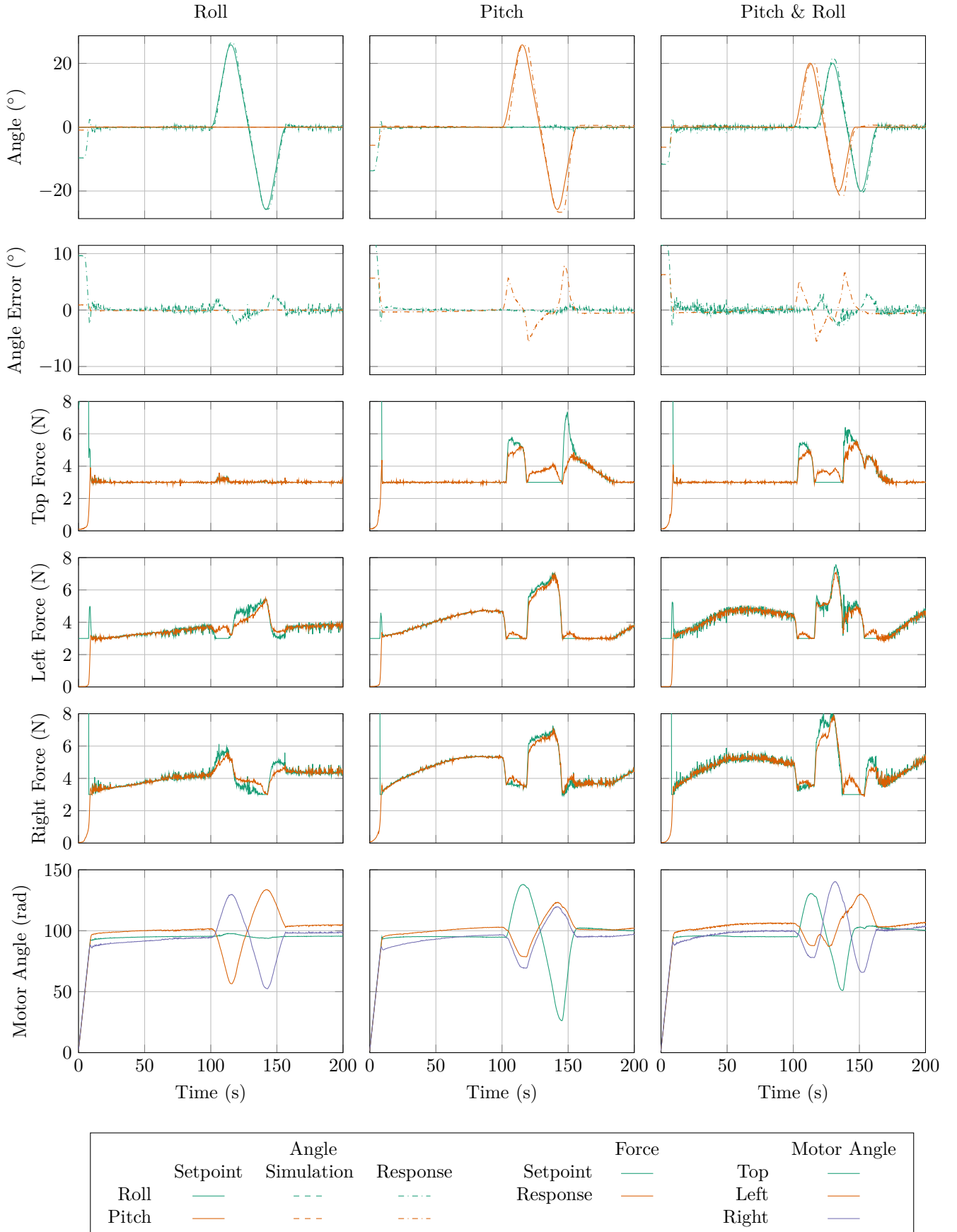


Fig. 1: Plots of the response for three different trajectories, one on only the roll axis θ_1 (column 1), one on only the pitch axis θ_2 (column 2), and one on both axes θ_1 and θ_2 (column 3). Plots include AUJ orientation, forces at the top, left and right TSA, and the motor positions. Note the simulation error is very small, so the plot cannot be seen on the graph.

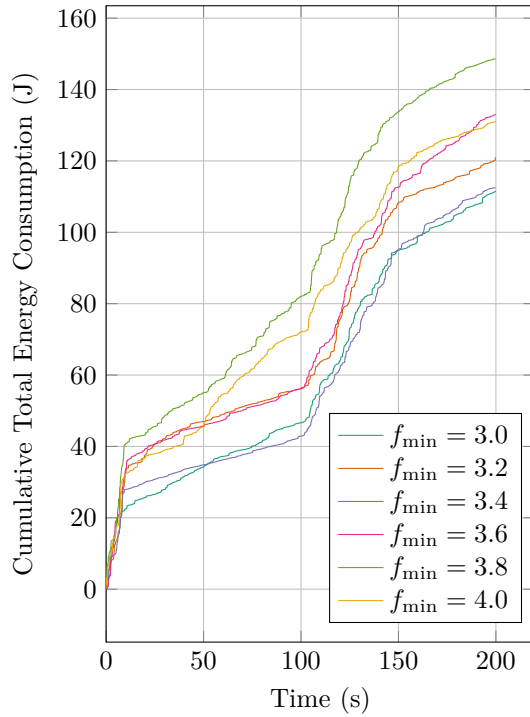


Fig. 2



Dr. Damian J. Crosby is a Post Doctoral Research Associate in the Department of Mechanical, Aerospace and Civil Engineering, University of Manchester, U.K. He received a B.Sc. in Special Effects Development from The University of Bolton, U.K., in 2010, and a M.Res. in Robotics from The University of Plymouth, U.K., in 2012. He worked as a Research Technician in robotic laser welding at The University of Manchester from 2013 to 2017, and then completed his PhD at the same university in 2023, developing a robotic tail for improved robot balance when carrying a payload. He has worked on robotic research in the fields of nuclear energy and advanced manufacturing.

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Dr. Joaquin Carrasco is a Lecturer at the Department of Electrical and Electronic Engineering, University of Manchester, UK. He was born in Abarn, Spain, in 1978. He received the B.Sc. degree in physics and the Ph.D. degree in control engineering from the University of Murcia, Murcia, Spain, in 2004 and 2009, respectively. From 2009 to 2010, he was with the Institute of Measurement and Automatic Control, Leibniz Universitt Hannover, Hannover, Germany. From 2010 to 2011, he was a Research Associate at the Control Systems Centre, School of Electrical and Electronic Engineering, University of Manchester, UK.



Prof. William P. Heath is Chair of Feedback and Control in the Department of Electrical and Electronic Engineering, University of Manchester, U.K. He received the B.A. and M.A. degrees in mathematics from Cambridge University, U.K., in 1987 and 1991, and the M.Sc. and Ph.D. degrees in systems and control from the University of Manchester Institute of Science and Technology, U.K., in 1989 and 1992, respectively. He was with Lucas Automotive from 1995 to 1998 and was a Research Academic at the University of Newcastle, Australia from 1998 to 2004. His research interests include absolute stability, multiplier theory, constrained control, and system identification.



Prof. Andrew Weightman graduated in 2006 with a PhD in Mechanical Engineering from the University of Leeds. Whilst at the University of Leeds he developed rehabilitation robotic technology for improving upper limb function in adults and children with neurological impairment which was successfully utilised in homes, schools and clinical settings. In 2013 he moved to the University of Manchester, Department of Mechanical, Aerospace and Civil Engineering as a Lecturer in Medical Mechatronics. Prof. Weightman has research interests in biomimetic mobile robotics, rehabilitation robotics, robotics for nuclear decommissioning and collaborative robotics.