

Supporting Information: Improvements and limitations of Mie λ -6 potential for prediction of saturated and compressed liquid viscosity

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SI.I. Input files

We provide example input files for simulating 2,2,4-trimethylhexane at 293 K with the Potoff force field in GROMACS (see attached .gro, .top, and .mdp files). Additionally, all files necessary to generate the results from this study can be found at www.github.com/ramess101/IFPSC_10.

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SI.II. MCMC from scoring function

The Potoff CH and C parameters are optimized using a scoring function (S) that weights the deviations for several different properties and their derivatives. MCMC requires an expression for the likelihood function (L), in particular, the log of the likelihood function ($\log_{10}(L)$). Standard least squares minimization is mathematically equivalent to maximizing the likelihood function of a normal distribution

$$L(D|\theta) = \frac{1}{\sqrt{2\pi^n\sigma^{2n}}} \exp \left[\frac{-1}{2\sigma^2} \left(\sum_i (y(\theta) - D_i)^2 \right) \right] \quad (1)$$

where D are the data, θ are the model parameters, n is the number of data points, σ is the standard deviation, and $\sum (y(\theta) - D_i)^2$ is the sum-squared-error (SSE).

$$\begin{aligned} L(D|\theta) &= \frac{1}{\sqrt{2\pi^n\sigma^{2n}}} \exp \left[\frac{-1}{2\sigma^2} \left(\sum_i (y(\theta) - D_i)^2 \right) \right] \\ &= \frac{1}{\sqrt{2\pi^n\sigma^{2n}}} \exp \left(\frac{-SSE(\theta)}{2\sigma^2} \right) \end{aligned} \quad (2)$$

In MCMC, assuming a uniform prior, the probability of accepting a new parameter set is

$$\alpha = \frac{L(D|\theta_{\text{new}})}{L(D|\theta_{\text{old}})} \quad (3)$$

In MCMC, the probability of accepting a new parameter set only depends on the log-likelihood (assuming a uniform prior), which for Equation 1

$$\log_{10}(L(D|\theta)) \propto - \sum (y(\theta) - D_i)^2 \propto -SSE(\theta) \quad (4)$$

In MCMC, the probability of accepting a new parameter set is equal to the difference between $\log_{10}(L(D|\theta_{\text{new}}))$ and $\log_{10}(L(D|\theta_{\text{old}}))$ (assuming a uniform prior). All terms in Equation 1 that do not depend on θ cancel. Therefore, the acceptance probability (α) is equal to

$$\alpha = \sum (y(\theta_{\text{old}}) - D_i)^2 - \sum (y(\theta_{\text{new}}) - D_i)^2 = SSE_{\text{old}} - SSE_{\text{new}} \quad (5)$$

$$\alpha = \log_{10}(L(D|\theta_{\text{new}})) - \log_{10}(L(D|\theta_{\text{old}})) = \sum (y(\theta_{\text{old}}) - D_i)^2 - \sum (y(\theta_{\text{new}}) - D_i)^2 = SSE_{\text{old}} - SSE_{\text{new}} \quad (6)$$

note that the order of “new” and “old” changes due to the negative sign in Equation 1.

Because Potoff’s scoring function (S) is not simply the sum-squared-error, minimizing S is not equivalent to maximizing the likelihood of a normal distribution. However, we can still apply the maximum likelihood criterion by substituting S for SSE in Equation 1. Again, because the terms that do not depend on θ cancel when taking the difference of logarithms, the acceptance probability is just

$$\alpha = S_{\text{old}} - S_{\text{new}} \quad (7)$$

$$\log_{10}(L(D|\theta)) \propto -S(\theta) \quad (8)$$

$$\log_{10}(L(D|\theta)) \propto -SSE(\theta) \quad (9)$$

The MCMC sampling was performed by interpolating the raw scoring function values over the two-dimensional grids of $\epsilon_{\text{CH}}\text{-}\sigma_{\text{CH}}$ and $\epsilon_{\text{C}}\text{-}\sigma_{\text{C}}$. The values of S were obtained through private communication with Potoff’s group. We utilize the scoring function from the “long” CH and C parameters. Using the “generalized” or “short” scoring function values would result in a different MCMC sampling.

The optimal “long” CH parameter is on the boundary of the grid tested by Mick et al. Therefore, we did not have any scoring function values for $\epsilon_{\text{CH}} < 14$ K. A similar problem is faced for $\epsilon_{\text{C}} < 0.8$ K and $\sigma_{\text{C}} > 0.63$ nm, but these regions are rarely sampled by the MCMC algorithm. To overcome the challenge of extrapolating outside of the domain where $S(\theta)$ is available, we fit $\log_{10}(S(\theta))$ to a multi-variate normal distribution. This approach works well for the CH parameters because the CH scoring function has a fairly normal shape. While the assumption of normality is worse for S of C, this does not significantly affect our results because of the infrequent sampling of this extrapolation region.

SI.III. MCMC validation

This section validates the combined bootstrap re-sampling and MCMC approach. Specifically, we compare the MCMC-nb 95 % confidence intervals obtained in two different manners. First, where a single replicate simulation is performed for each MCMC-nb parameter set, which are pooled together for bootstrap re-sampling. Second, where 40 replicate simulations are performed for each set of MCMC-nb parameters, and bootstrap re-sampling is performed independently for each set of 40 replicates. Due to the large amount of simulations required for this comparison, we perform this analysis on a simpler system, namely, ethane at saturation conditions. Figure [SI.1](#) demonstrates that the 95 % confidence intervals are nearly indistinguishable for the two methods. This provides empirical evidence that performing a single simulation with each parameter set is the same as performing numerous simulations with each parameter set.

Figure SI.1:

SI.IV. A_s distribution

In this section, we demonstrate how we develop the skewed distribution for A_s , where the lower and upper 95 % confidence intervals correspond to -15 % and +40 % of the maximum torsional barrier. The viscosity values obtained with Potoff are considerably higher than those obtained with AUA4. Therefore, it is feasible, especially at higher pressures, that the optimal value of A_s is negative, i.e., the viscosity may be too high and, thus, decreasing the torsional barriers might improve the viscosity estimates. For this reason, we consider $A_s < 0$.

To determine the appropriate scaling of the torsional barriers, Figure SI.2 presents a sensitivity analysis of η with respect to A_s . The viscosities in Figure SI.2 are computed at 293 K and atmospheric pressure. Also depicted is the only available experimental viscosity value.

Figure SI.2:

Figure SI.2 demonstrates that quantitative agreement with the experimental viscosity point necessitates an A_s value that is 80 % the maximum torsional barrier. Fearing some unforeseen consequences, we do not feel that obtaining quantitative agreement with this single experimental value merits such a dramatic increase in the torsional barriers. For this reason, we adopt the same percent increase as that proposed by Nieto-Draghi et al., i.e., 40 %.

SI.V. Green-Kubo integrals

Figure [SI.3](#) presents the average Green-Kubo integral for all thirteen state points. Note that much longer simulations are required for high pressures/viscosities.

Figure SI.3:

References

References