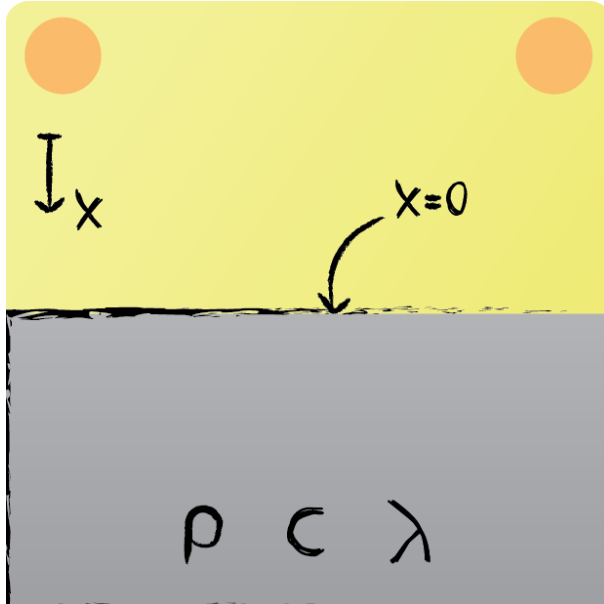


## Exam Preparation - Conduction 1



A large body is suddenly imposed to a new temperature at its surface  $T(x = 0, t > 0) = 500$  K. The body has an initial homogeneous temperature  $T(x, t = 0) = 298$  K. Determine  $T(x_1, t_1)$ , for  $t_1 = 18$  s at depth  $x_1 = 3$  mm.

Problem type:

One-dimensional, unsteady-state heat conduction inside a semi-infinite plate with negligible heat transfer resistance.

Temperature profile inside a semi-infinite plate with negligible heat transfer resistance:

$$\Theta^* = \frac{T - T_0}{T_a - T_0} = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right)$$



Determining the Fourier number:

$$\text{Fo} = \frac{\lambda \cdot t}{\rho \cdot c \cdot x^2} = 0.7178$$

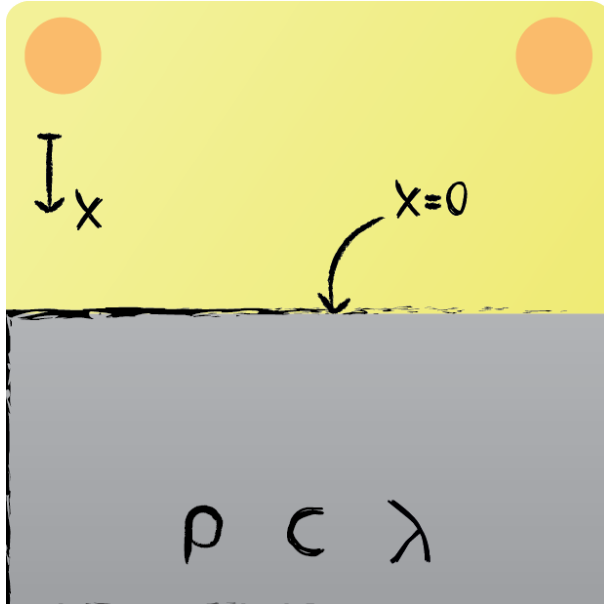
Determining  $\Theta^*$ :

$$\Theta^* = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right) = 0.4039$$

Rearranging  $\Theta^*$  and filling in:

$$T = \Theta^* \cdot (T_a - T_0) + T_0 = 380 \text{ K}$$

## Exam Preparation - Conduction 2



A large body is suddenly imposed to a new temperature at its surface  $T(x = 0, t > 0) = 500$  K. The body has an initial homogeneous temperature  $T(x, t = 0) = 298$  K. Determine  $T(x_1, t_1)$ , for  $t_1 = 18$  s at depth  $x_1 = 3$  mm.

Problem type:

One-dimensional, unsteady-state heat conduction inside a semi-infinite plate with negligible heat transfer resistance.

Temperature profile inside a semi-infinite plate with negligible heat transfer resistance:

$$\Theta^* = \frac{T - T_0}{T_a - T_0} = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right)$$



Determining the Fourier number:

$$\text{Fo} = \frac{\lambda \cdot t}{\rho \cdot c \cdot x^2} = 0.2771$$

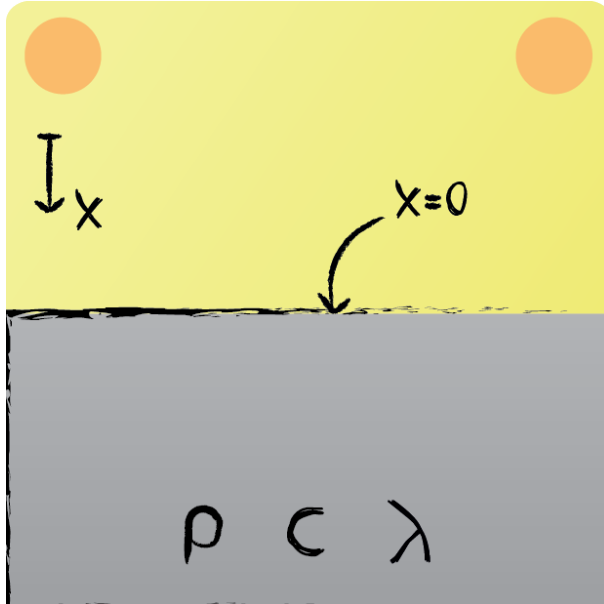
Determining  $\Theta^*$ :

$$\Theta^* = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right) = 0.1792$$

Rearranging  $\Theta^*$  and filling in:

$$T = \Theta^* \cdot (T_a - T_0) + T_0 = 334 \text{ K}$$

## Exam Preparation - Conduction 3



A large body is suddenly imposed to a new temperature at its surface  $T(x = 0, t > 0) = 500$  K. The body has an initial homogeneous temperature  $T(x, t = 0) = 298$  K. Determine  $T(x_1, t_1)$ , for  $t_1 = 18$  s at depth  $x_1 = 3$  mm.

Problem type:

One-dimensional, unsteady-state heat conduction inside a semi-infinite plate with negligible heat transfer resistance.

Temperature profile inside a semi-infinite plate with negligible heat transfer resistance:

$$\Theta^* = \frac{T - T_0}{T_a - T_0} = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right)$$



Determining the Fourier number:

$$\text{Fo} = \frac{\lambda \cdot t}{\rho \cdot c \cdot x^2} = 0.4450$$

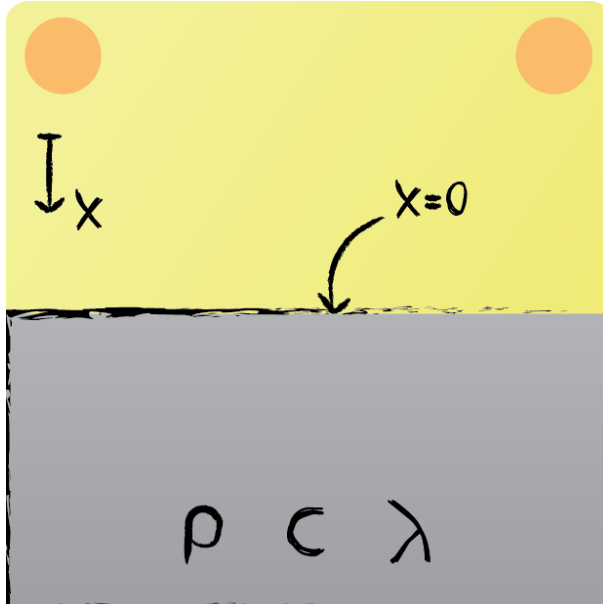
Determining  $\Theta^*$ :

$$\Theta^* = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right) = 0.2891$$

Rearranging  $\Theta^*$  and filling in:

$$T = \Theta^* \cdot (T_a - T_0) + T_0 = 356 \text{ K}$$

## Exam Preparation - Conduction 4



A large body is suddenly imposed to a new temperature at its surface  $T(x = 0, t > 0) = 500$  K. The body has an initial homogeneous temperature  $T(x, t = 0) = 298$  K. Determine  $T(x_1, t_1)$ , for  $t_1 = 18$  s at depth  $x_1 = 3$  mm.

Problem type:

One-dimensional, unsteady-state heat conduction inside a semi-infinite plate with negligible heat transfer resistance.

Temperature profile inside a semi-infinite plate with negligible heat transfer resistance:

$$\Theta^* = \frac{T - T_0}{T_a - T_0} = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right)$$



Determining the Fourier number:

$$\text{Fo} = \frac{\lambda \cdot t}{\rho \cdot c \cdot x^2} = 0.1162$$

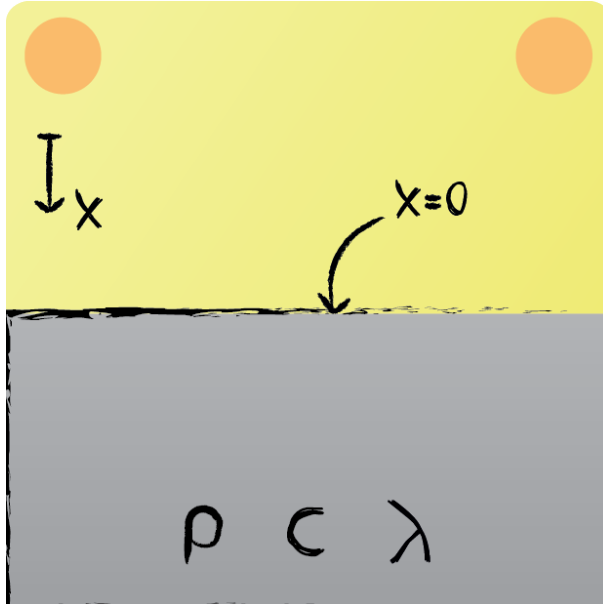
Determining  $\Theta^*$ :

$$\Theta^* = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right) = 0.0380$$

Rearranging  $\Theta^*$  and filling in:

$$T = \Theta^* \cdot (T_a - T_0) + T_0 = 306 \text{ K}$$

## Exam Preparation - Conduction 5



A large body is suddenly imposed to a new temperature at its surface  $T(x = 0, t > 0) = 500$  K. The body has an initial homogeneous temperature  $T(x, t = 0) = 298$  K. Determine  $T(x_1, t_1)$ , for  $t_1 = 18$  s at depth  $x_1 = 3$  mm.

Problem type:

One-dimensional, unsteady-state heat conduction inside a semi-infinite plate with negligible heat transfer resistance.

Temperature profile inside a semi-infinite plate with negligible heat transfer resistance:

$$\Theta^* = \frac{T - T_0}{T_a - T_0} = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right)$$



Determining the Fourier number:

$$\text{Fo} = \frac{\lambda \cdot t}{\rho \cdot c \cdot x^2} = 2.6923$$

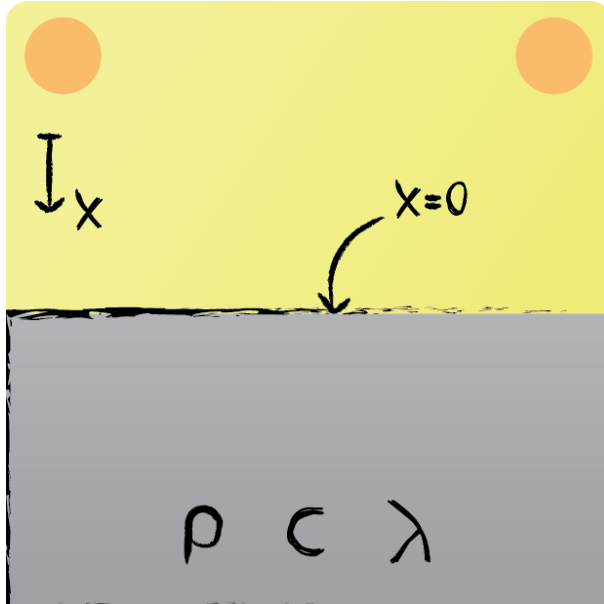
Determining  $\Theta^*$ :

$$\Theta^* = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right) = 0.6666$$

Rearranging  $\Theta^*$  and filling in:

$$T = \Theta^* \cdot (T_a - T_0) + T_0 = 433 \text{ K}$$

## Exam Preparation - Conduction 6



A large body is suddenly imposed to a new temperature at its surface  $T(x = 0, t > 0) = 500$  K. The body has an initial homogeneous temperature  $T(x, t = 0) = 298$  K. Determine  $T(x_1, t_1)$ , for  $t_1 = 18$  s at depth  $x_1 = 3$  mm.

Problem type:

One-dimensional, unsteady-state heat conduction inside a semi-infinite plate with negligible heat transfer resistance.

Temperature profile inside a semi-infinite plate with negligible heat transfer resistance:

$$\Theta^* = \frac{T - T_0}{T_a - T_0} = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right)$$



Determining the Fourier number:

$$\text{Fo} = \frac{\lambda \cdot t}{\rho \cdot c \cdot x^2} = 233.9312$$

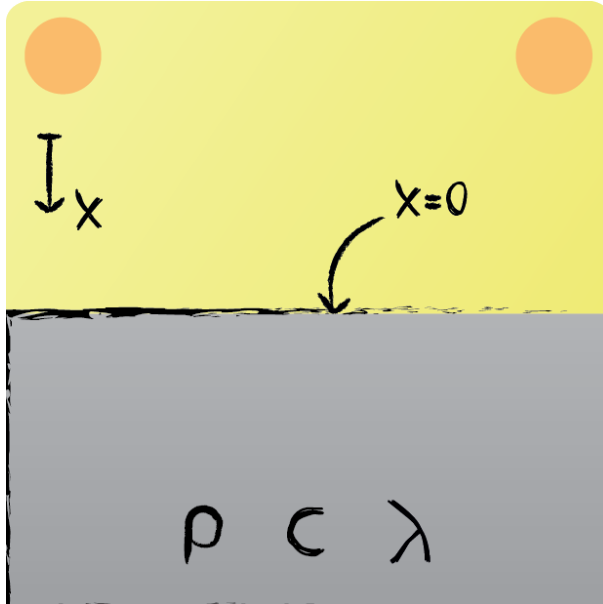
Determining  $\Theta^*$ :

$$\Theta^* = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right) = 0.9631$$

Rearranging  $\Theta^*$  and filling in:

$$T = \Theta^* \cdot (T_a - T_0) + T_0 = 493 \text{ K}$$

## Exam Preparation - Conduction 7



A large body is suddenly imposed to a new temperature at its surface  $T(x = 0, t > 0) = 500$  K. The body has an initial homogeneous temperature  $T(x, t = 0) = 298$  K. Determine  $T(x_1, t_1)$ , for  $t_1 = 18$  s at depth  $x_1 = 3$  mm.

Problem type:

One-dimensional, unsteady-state heat conduction inside a semi-infinite plate with negligible heat transfer resistance.

Temperature profile inside a semi-infinite plate with negligible heat transfer resistance:

$$\Theta^* = \frac{T - T_0}{T_a - T_0} = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right)$$



Determining the Fourier number:

$$\text{Fo} = \frac{\lambda \cdot t}{\rho \cdot c \cdot x^2} = 0.2296$$

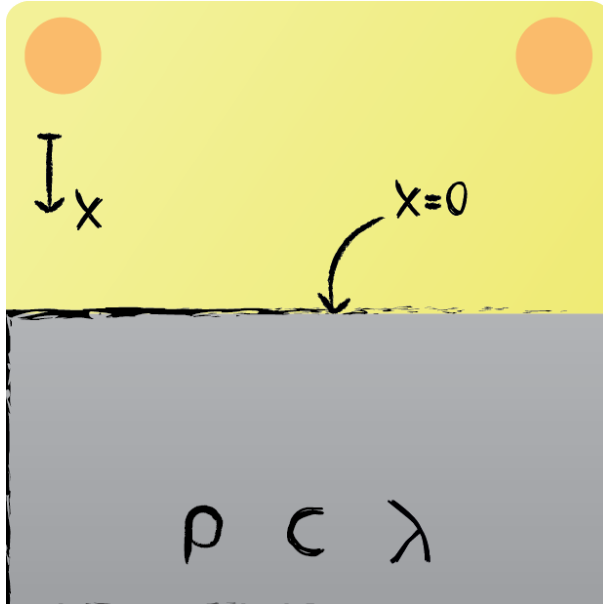
Determining  $\Theta^*$ :

$$\Theta^* = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right) = 0.1400$$

Rearranging  $\Theta^*$  and filling in:

$$T = \Theta^* \cdot (T_a - T_0) + T_0 = 326 \text{ K}$$

## Exam Preparation - Conduction 8



A large body is suddenly imposed to a new temperature at its surface  $T(x = 0, t > 0) = 500$  K. The body has an initial homogeneous temperature  $T(x, t = 0) = 298$  K. Determine  $T(x_1, t_1)$ , for  $t_1 = 18$  s at depth  $x_1 = 3$  mm.

Problem type:

One-dimensional, unsteady-state heat conduction inside a semi-infinite plate with negligible heat transfer resistance.

Temperature profile inside a semi-infinite plate with negligible heat transfer resistance:

$$\Theta^* = \frac{T - T_0}{T_a - T_0} = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right)$$



Determining the Fourier number:

$$\text{Fo} = \frac{\lambda \cdot t}{\rho \cdot c \cdot x^2} = 47.8515$$

Determining  $\Theta^*$ :

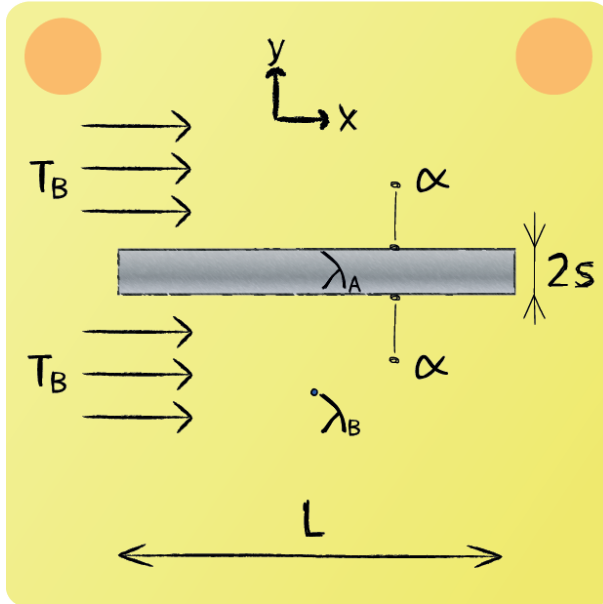
$$\Theta^* = 1 - \operatorname{erf}\left(\frac{1}{\sqrt{4 \cdot \text{Fo}}}\right) = 0.9186$$

Rearranging  $\Theta^*$  and filling in:

$$T = \Theta^* \cdot (T_a - T_0) + T_0 = 484 \text{ K}$$



## Exam Preparation - Conduction 9



Choose the right equation to determine the heat transfer coefficient  $\alpha$  for a plate of thickness  $2s$  and a thermal conductivity  $\lambda_A$  for a given problem specific Biot number  $Bi$ .

Heat transfer happens in the  $y$ -direction. Therefore the conductive inside and convective resistance outside the body in  $y$ -direction have to be brought into relation. Resulting in:

$$Bi_s = \frac{\alpha \cdot L}{\lambda_A}$$

Note that  $L$  is the characteristic length, which is the ratio  $\frac{V}{A}$ . Resulting in:



$$L = \frac{2s \cdot A_s}{2 \cdot A_s} = s$$

Where  $A_s$  is the surface area where the fluid is flowing over.

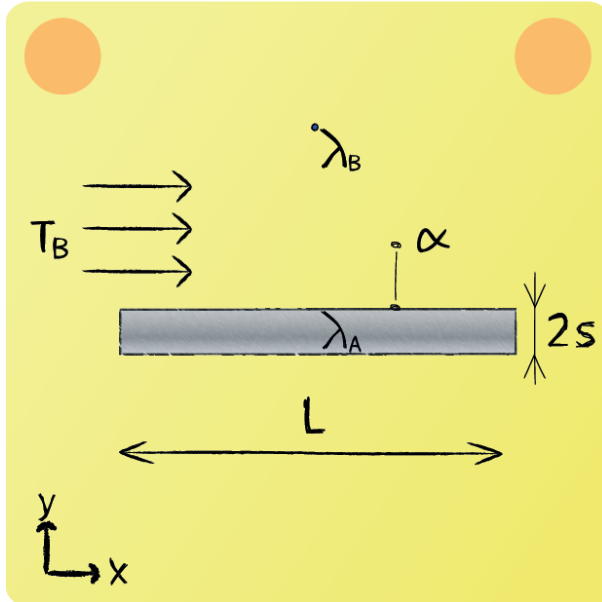
Therefore:

$$Bi_s = \frac{\alpha \cdot s}{\lambda_A}$$

And thus:

$$\rightarrow \alpha = \frac{Bi \cdot \lambda_A}{s}$$

## Exam Preparation - Conduction 10



Choose the right equation to determine the heat transfer coefficient  $\alpha$  for a given problem-specific Nusselt number,  $Nu$  and given the fluid properties.

The Nusselt number  $Nu$  can be described as:

$$Nu_L = \frac{\alpha \cdot L}{\lambda_B}$$

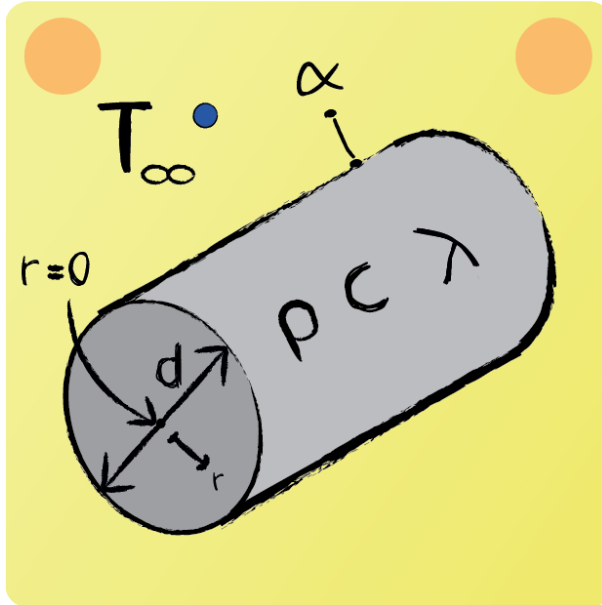


Where  $L$  is the length of the flat plate where the fluid is flowing over and  $\lambda_B$  is the thermal conductivity of the fluid.

Therefore:

$$\rightarrow \alpha = \frac{Nu_L \cdot \lambda_B}{L}$$

## Exam Preparation - Conduction 11



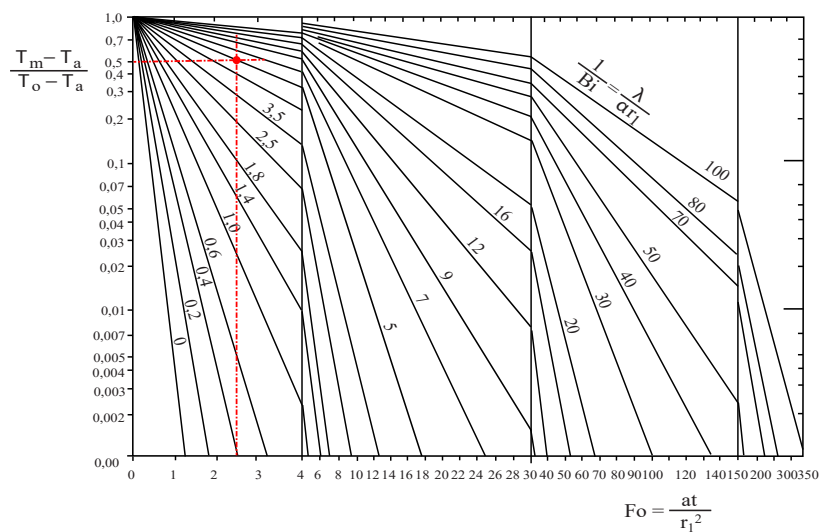
A cylinder of diameter  $d = 0.5$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 323$  K is reached.

Problem type:

One-dimensional, unsteady heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot r_1} = 5$$

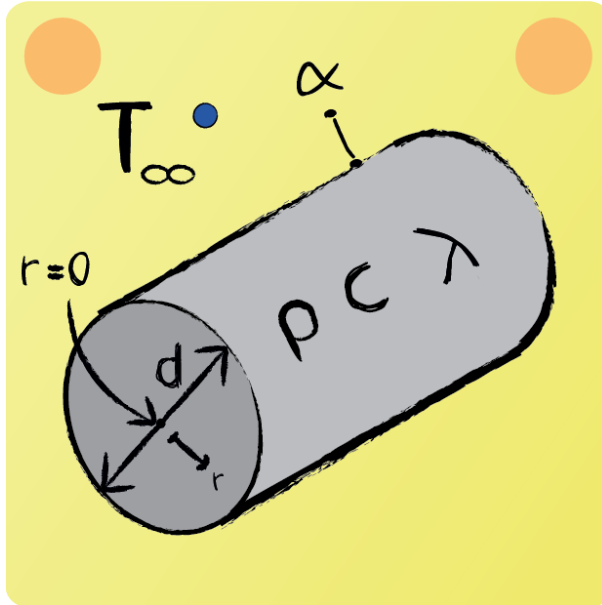
$$\frac{T_m - T_a}{T_o - T_a} = 0.5$$



$$\rightarrow Fo = 2.50$$

$$t = 7026.67 \text{ s}$$

## Exam Preparation - Conduction 12



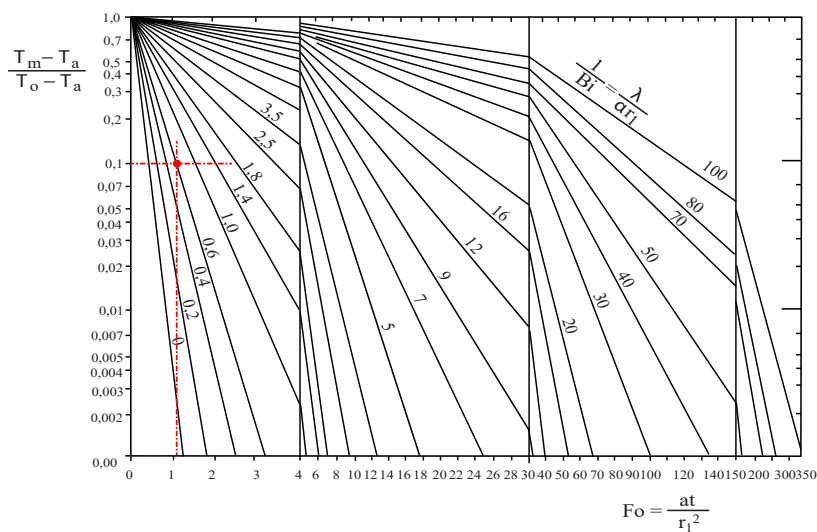
A cylinder of diameter  $d = 0.5$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 347$  K is reached.

Problem type:

One-dimensional, unsteady heat conduction that does penetrate.

$$\frac{1}{\text{Bi}} = \frac{\lambda}{\alpha \cdot r_1} = 0.6087$$

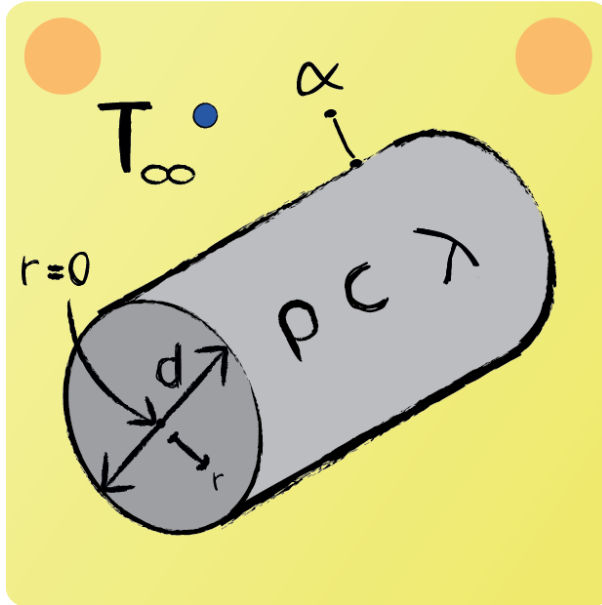
$$\frac{T_m - T_a}{T_o - T_a} = 0.1$$



$$\rightarrow \text{Fo} = 1.08$$

$$t = 1876.66 \text{ s}$$

## Exam Preparation - Conduction 13



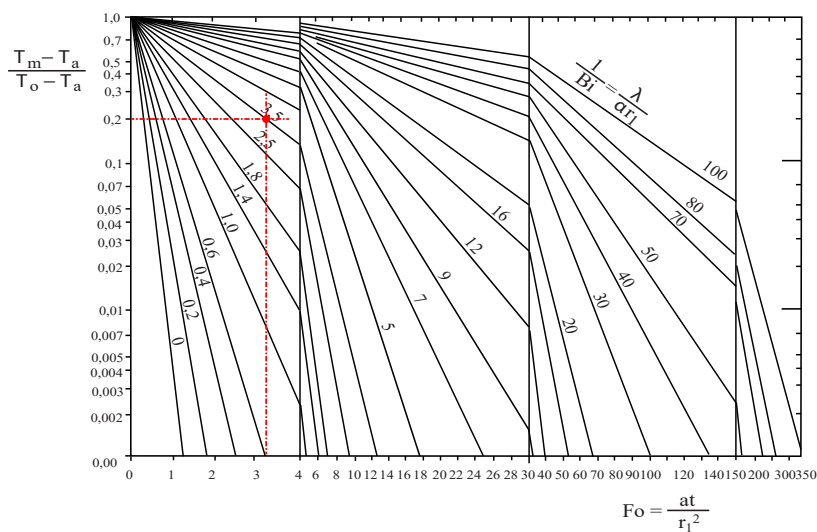
A cylinder of diameter  $d = 0.5$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 341$  K is reached.

Problem type:

One-dimensional, unsteady heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot r_1} = 3.50$$

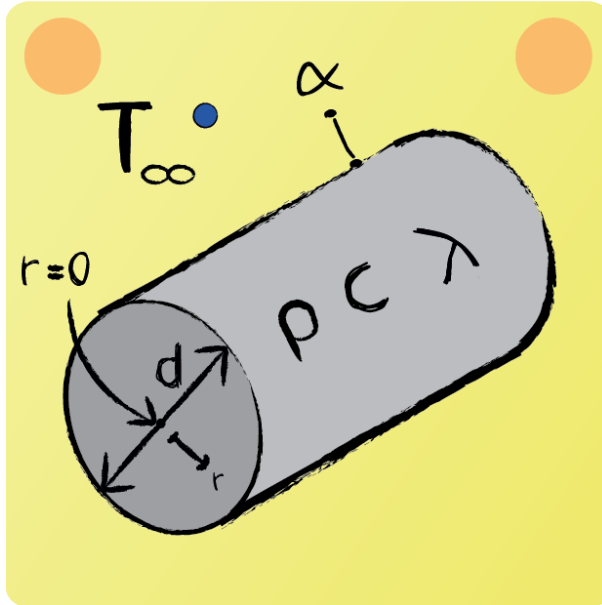
$$\frac{T_m - T_a}{T_o - T_a} = 0.2$$



$$\rightarrow Fo = 3.27$$

$$t = 14730.19 \text{ s}$$

## Exam Preparation - Conduction 14



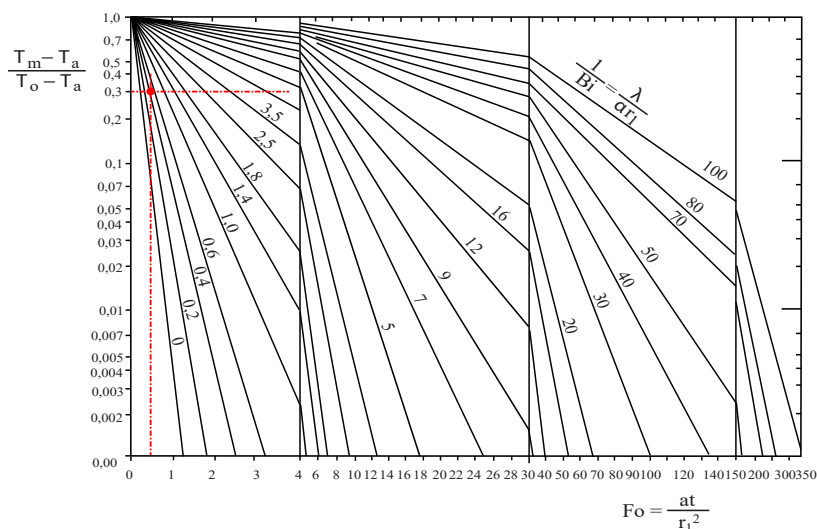
A cylinder of diameter  $d = 0.5$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 335$  K is reached.

Problem type:

One-dimensional, unsteady heat conduction that does penetrate.

$$\frac{1}{\text{Bi}} = \frac{\lambda}{\alpha \cdot r_1} = 0.41$$

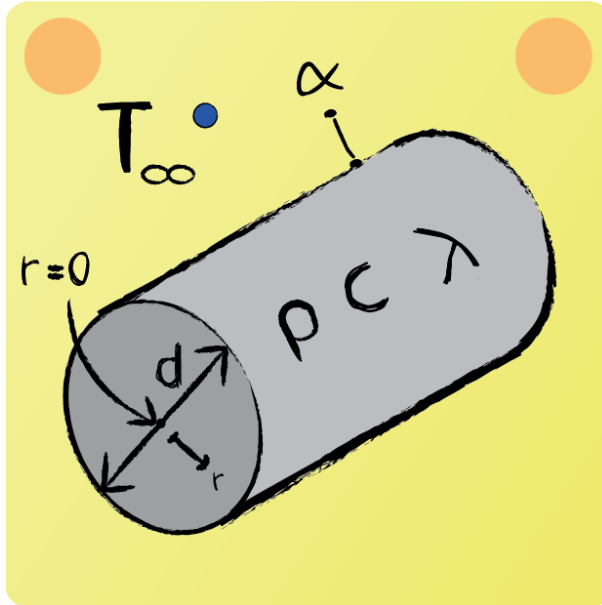
$$\frac{T_m - T_a}{T_o - T_a} = 0.3$$



$$\rightarrow \text{Fo} = 0.46$$

$$t = 4977.02 \text{ s}$$

## Exam Preparation - Conduction 15



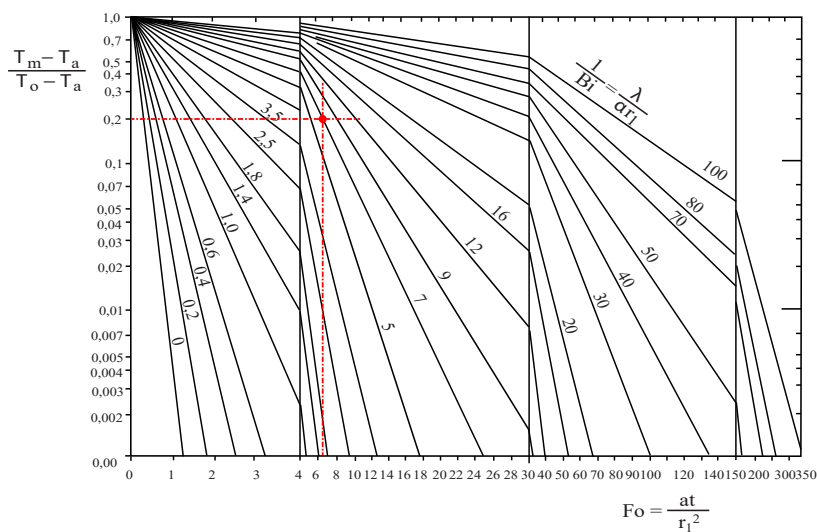
A cylinder of diameter  $d = 0.5$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 341$  K is reached.

Problem type:

One-dimensional, unsteady heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot r_1} = 7$$

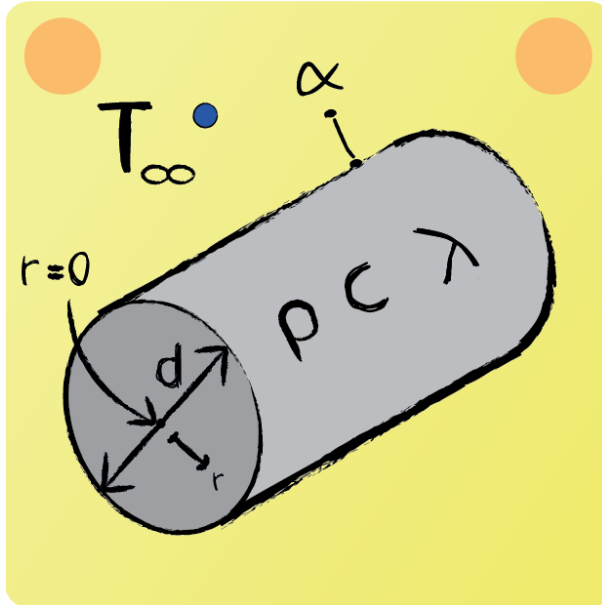
$$\frac{T_m - T_a}{T_o - T_a} = 0.2$$



$$\rightarrow Fo = 6.51$$

$$t = 3021.11 \text{ s}$$

## Exam Preparation - Conduction 16



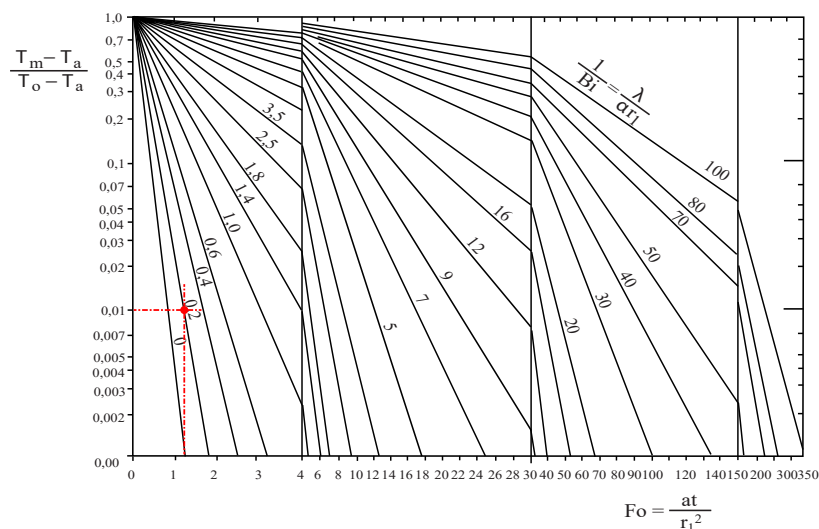
A cylinder of diameter  $d = 0.5$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 352.4$  K is reached.

Problem type:

One-dimensional, unsteady heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot r_1} = 0.2$$

$$\frac{T_m - T_a}{T_o - T_a} = 0.01$$

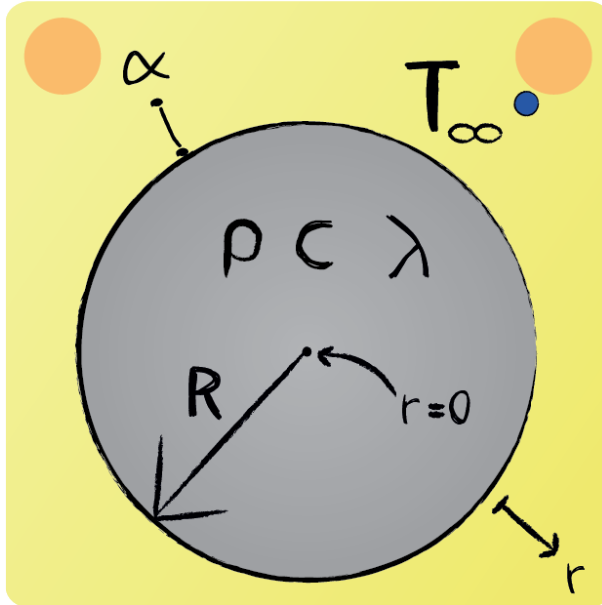


$$\rightarrow Fo = 1.21$$

$$t = 6596.16 \text{ s}$$



## Exam Preparation - Conduction 17



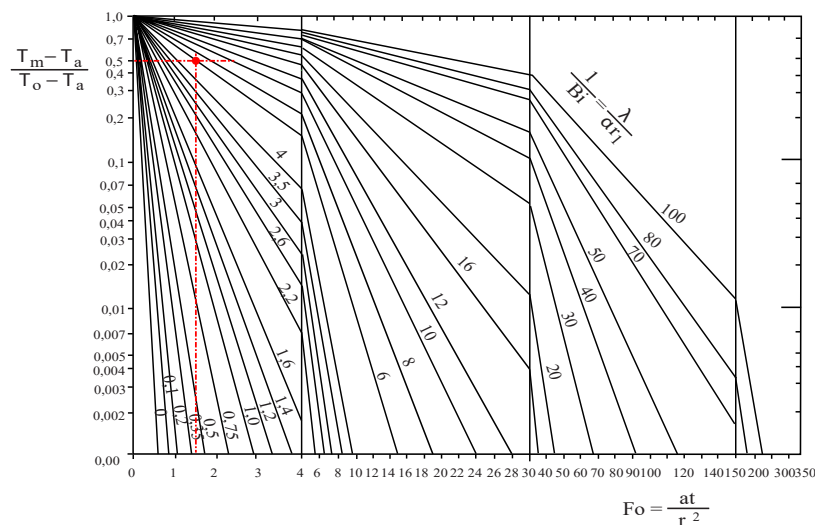
A sphere with radius  $R = 1$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 323$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot r_1} = 6$$

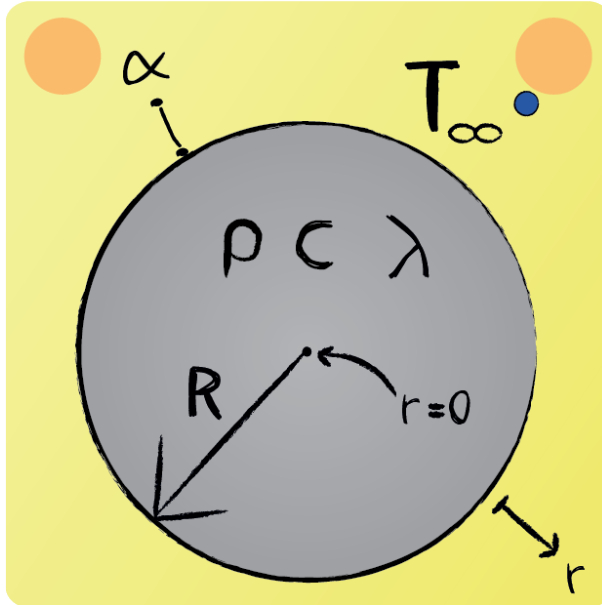
$$\frac{T_m - T_a}{T_o - T_a} = 0.5$$



$$\rightarrow Fo = 1.49$$

$$t = 668.44 \text{ s}$$

## Exam Preparation - Conduction 18



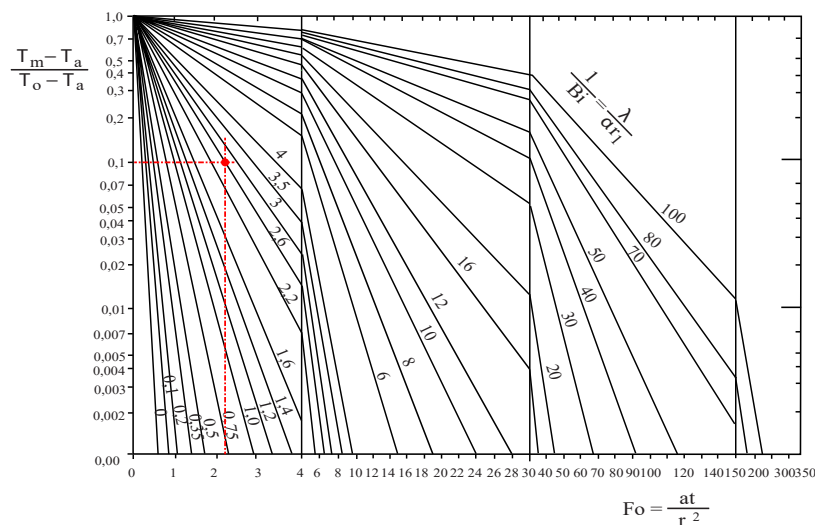
A sphere with radius  $R = 1$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 347$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{\text{Bi}} = \frac{\lambda}{\alpha \cdot r_1} = 2.60$$

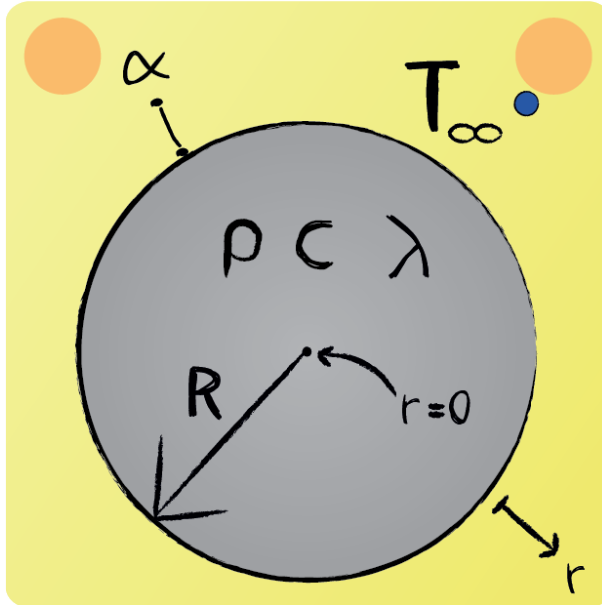
$$\frac{T_m - T_a}{T_o - T_a} = 0.1$$



$$\rightarrow \text{Fo} = 2.21$$

$$t = 615.32 \text{ s}$$

## Exam Preparation - Conduction 19



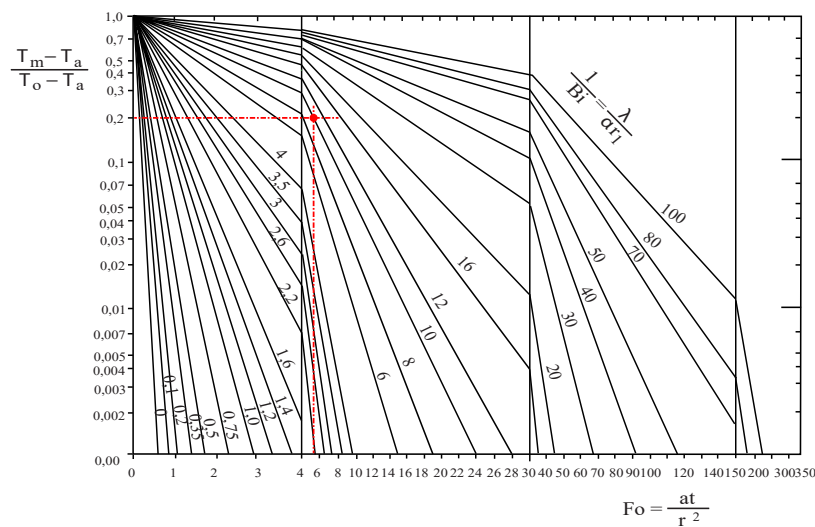
A sphere with radius  $R = 1$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 341$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot r_1} = 10$$

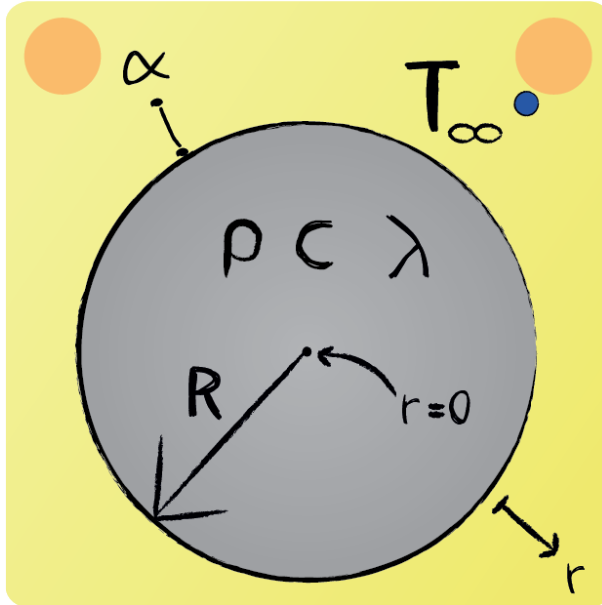
$$\frac{T_m - T_a}{T_o - T_a} = 0.2$$



$$\rightarrow Fo = 5.35$$

$$t = 3862.46 \text{ s}$$

## Exam Preparation - Conduction 20



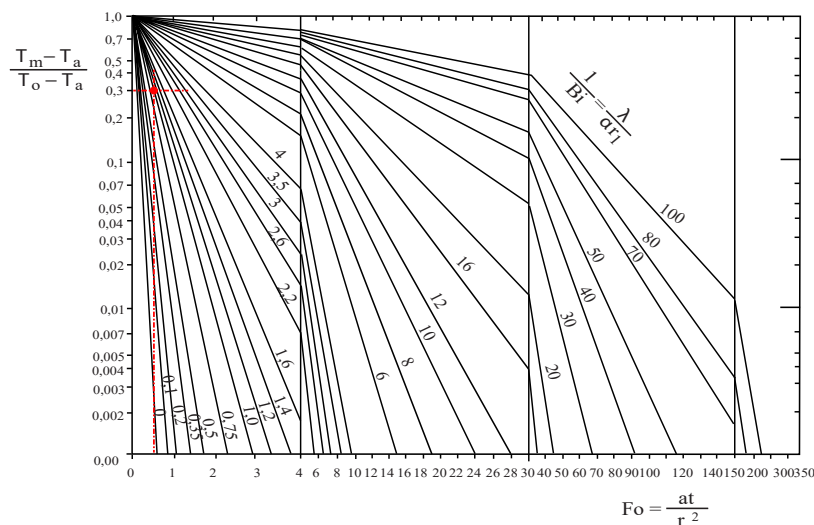
A sphere with radius  $R = 1$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 335$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot r_1} = 1.02$$

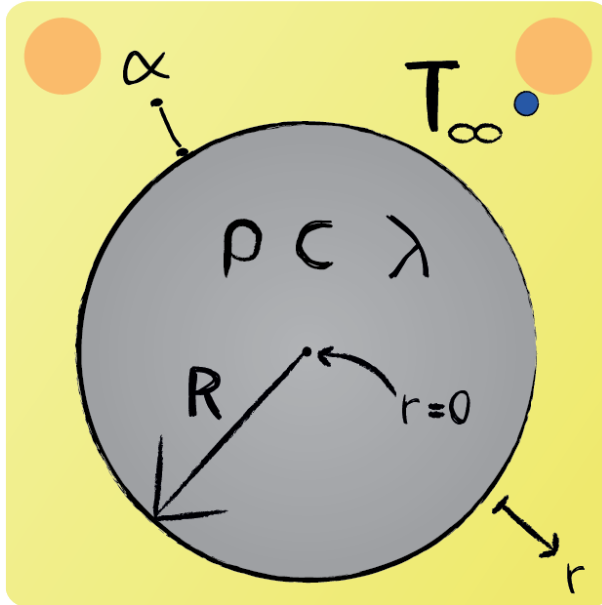
$$\frac{T_m - T_a}{T_o - T_a} = 0.3$$



$$\rightarrow Fo = 0.51$$

$$t = 880.13 \text{ s}$$

## Exam Preparation - Conduction 21



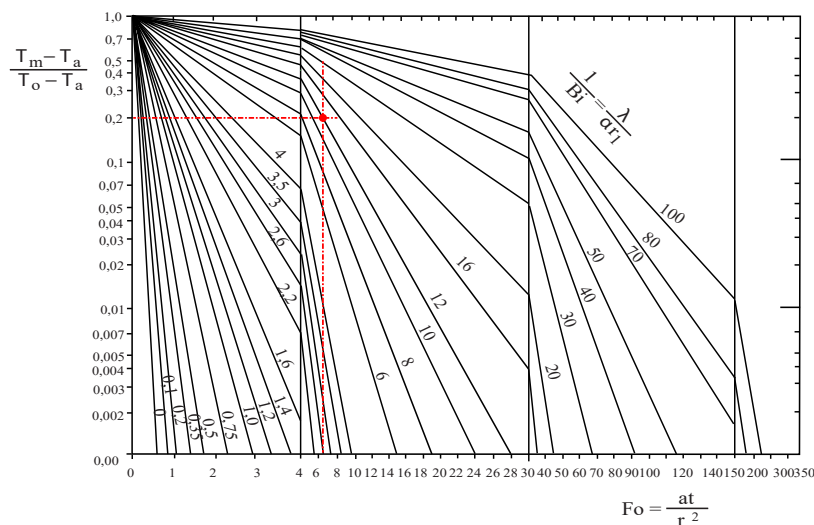
A sphere with radius  $R = 1$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 341$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot r_1} = 12$$

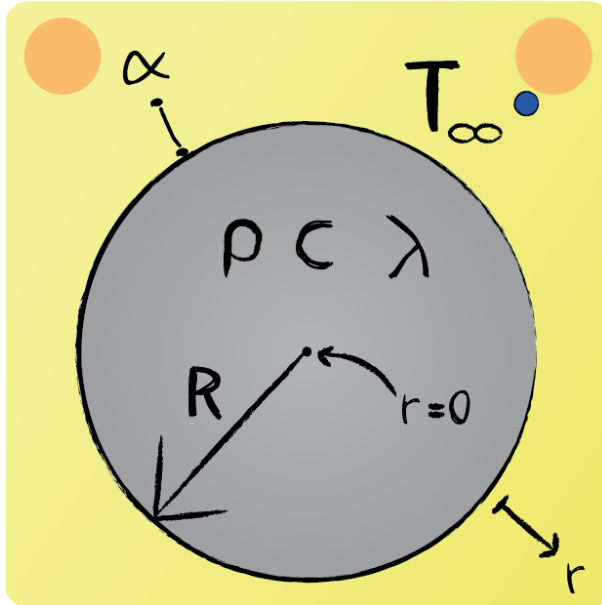
$$\frac{T_m - T_a}{T_o - T_a} = 0.2$$



$$\rightarrow Fo = 6.48$$

$$t = 481.08 \text{ s}$$

## Exam Preparation - Conduction 22



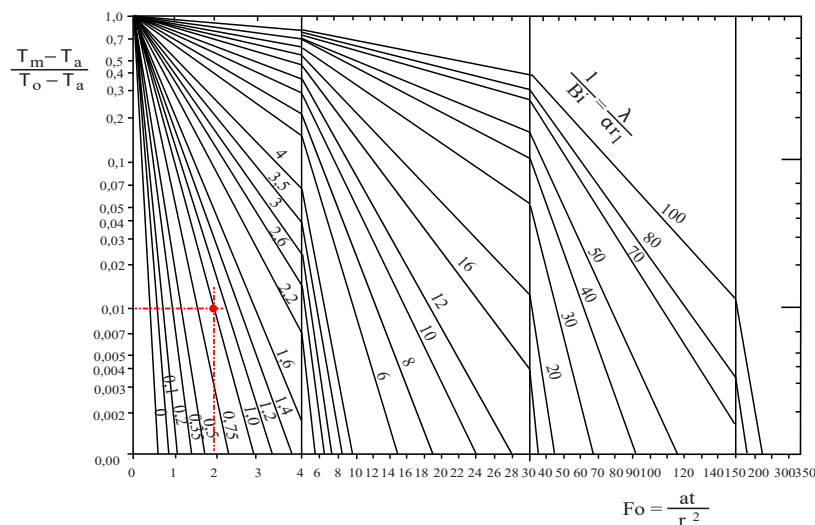
A sphere with radius  $R = 1$  cm with initial homogeneous temperature  $T(r, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(r = 0, t_1) = 352.4$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot r_1} = 1$$

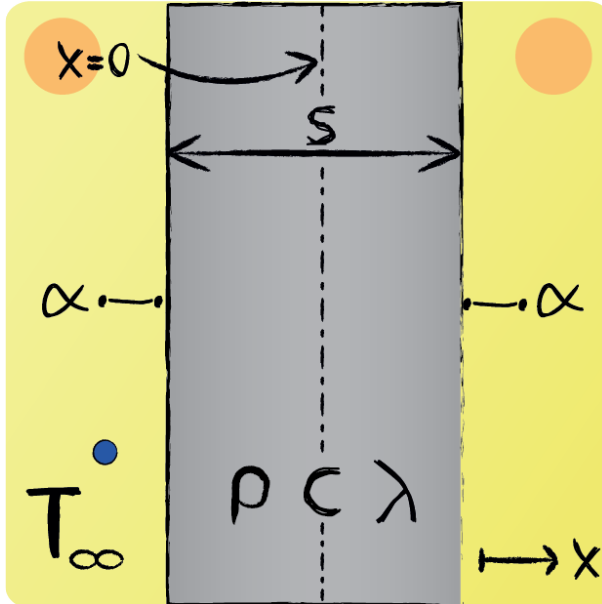
$$\frac{T_m - T_a}{T_o - T_a} = 0.01$$



$$\rightarrow Fo = 1.92$$

$$t = 1675.65 \text{ s}$$

## Exam Preparation - Conduction 23



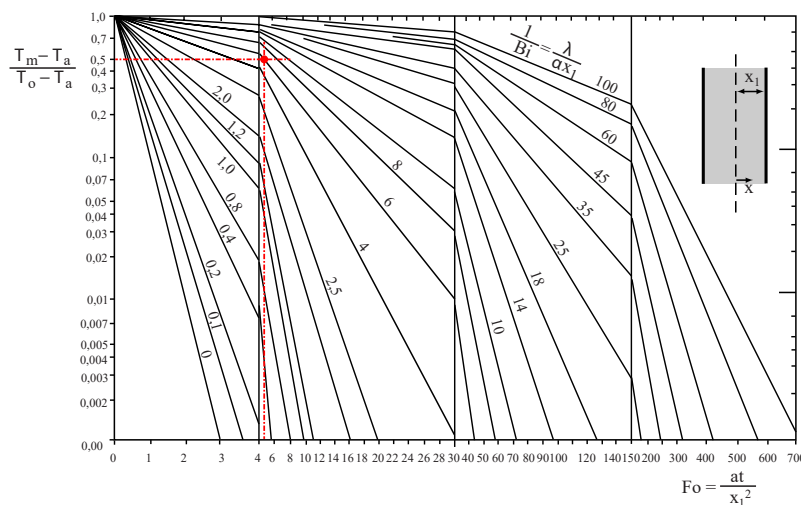
A plate with thickness  $x = 2$  cm with initial homogeneous temperature  $T(x, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(x = 0, t_1) = 323$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot x_1} = 6$$

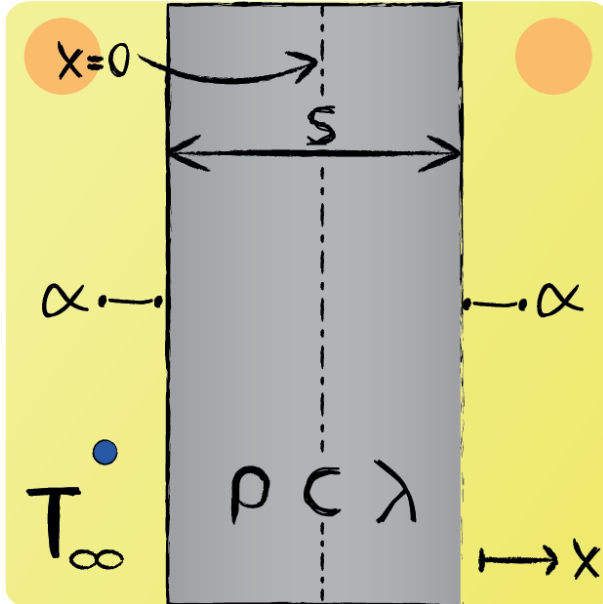
$$\frac{T_m - T_a}{T_o - T_a} = 0.5$$



$$\rightarrow Fo = 4.69$$

$$t = 2108.11 \text{ s}$$

## Exam Preparation - Conduction 24



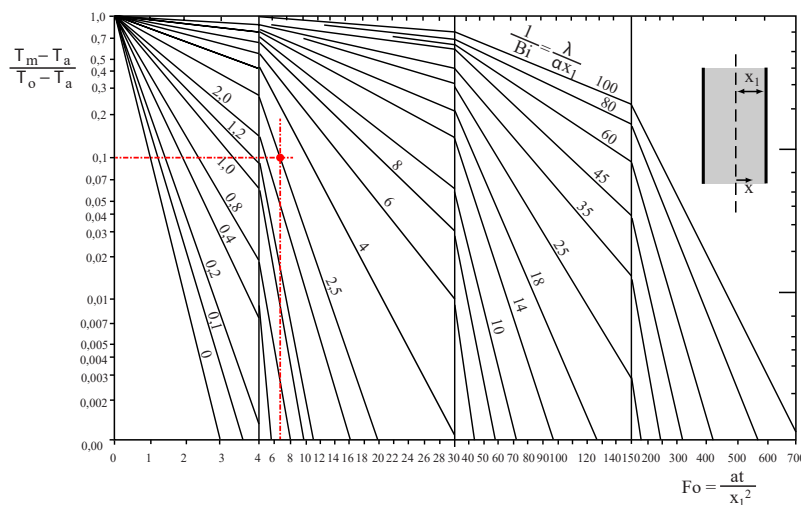
A plate with thickness  $x = 2$  cm with initial homogeneous temperature  $T(x, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(x = 0, t_1) = 347$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot x_1} = 2.5$$

$$\frac{T_m - T_a}{T_o - T_a} = 0.1$$

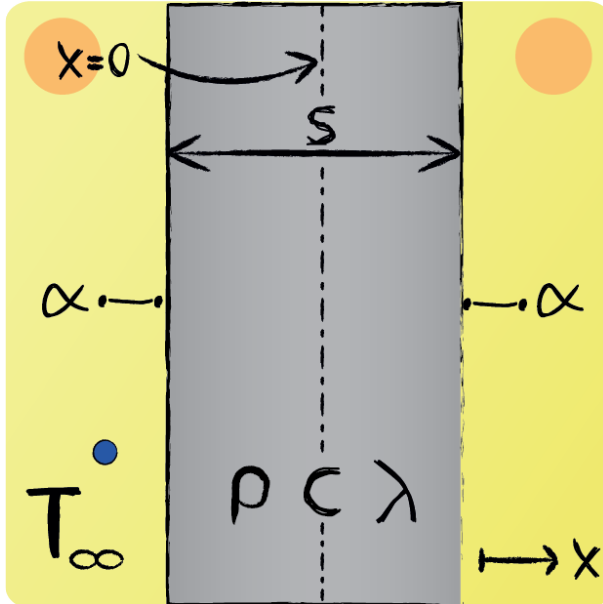


$$\rightarrow Fo = 6.74$$

$$t = 1876.60 \text{ s}$$



## Exam Preparation - Conduction 25



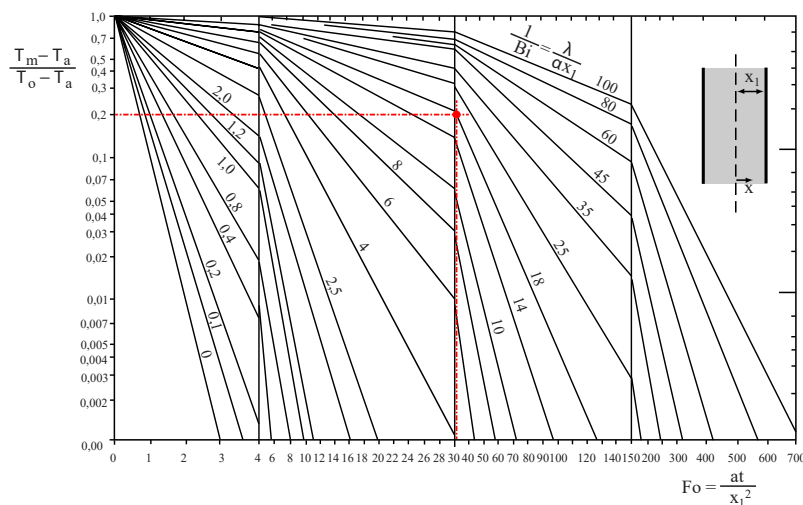
A plate with thickness  $x = 2$  cm with initial homogeneous temperature  $T(x, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(x = 0, t_1) = 341$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot x_1} = 18.01$$

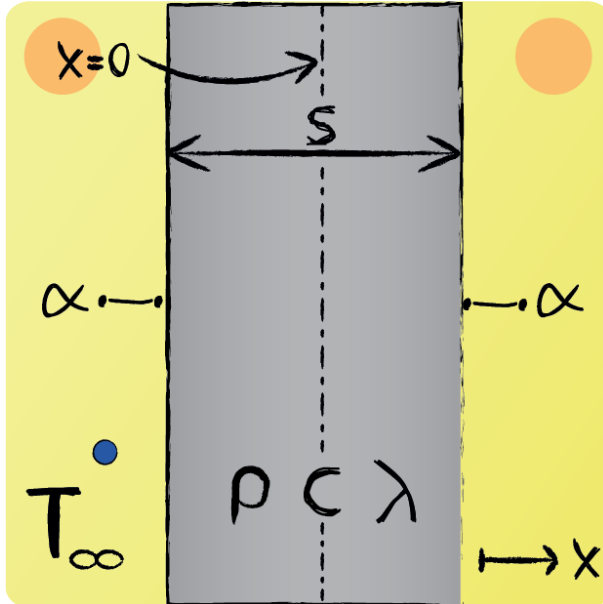
$$\frac{T_m - T_a}{T_o - T_a} = 0.2$$



$$\rightarrow Fo = 31.31$$

$$t = 2326.00 \text{ s}$$

## Exam Preparation - Conduction 26



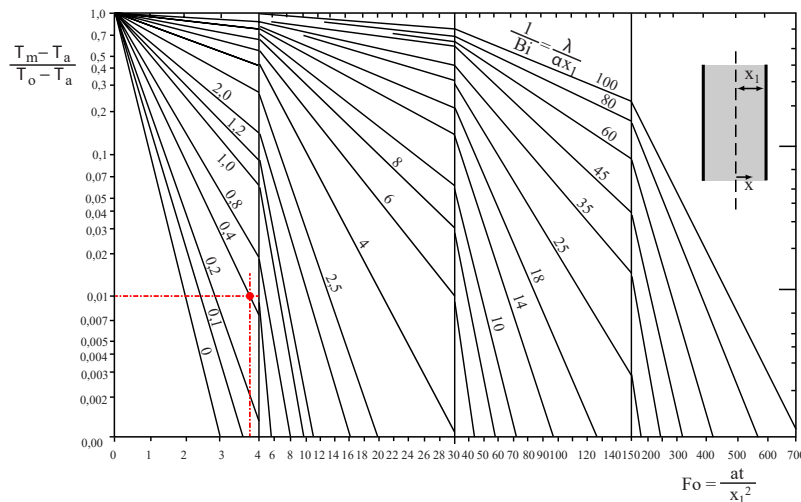
A plate with thickness  $x = 2$  cm with initial homogeneous temperature  $T(x, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(x = 0, t_1) = 352.4$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot x_1} = 0.4$$

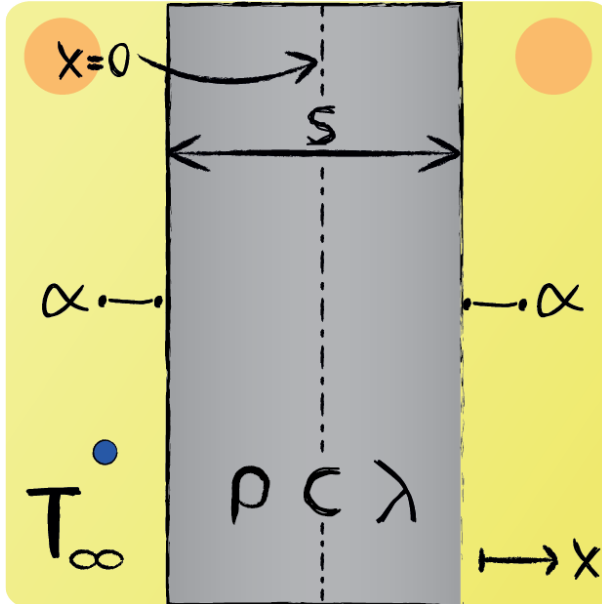
$$\frac{T_m - T_a}{T_o - T_a} = 0.01$$



$$\rightarrow Fo = 3.77$$

$$t = 3283.95 \text{ s}$$

## Exam Preparation - Conduction 27



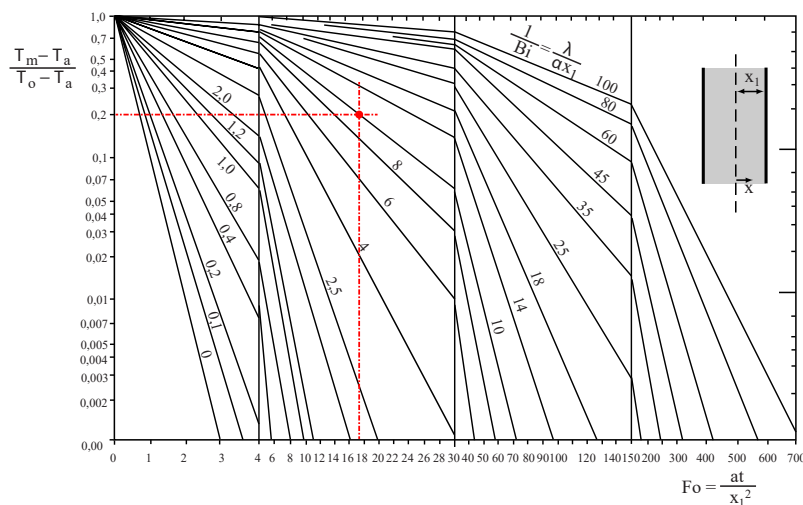
A plate with thickness  $x = 2$  cm with initial homogeneous temperature  $T(x, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(x = 0, t_1) = 341$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot x_1} = 10$$

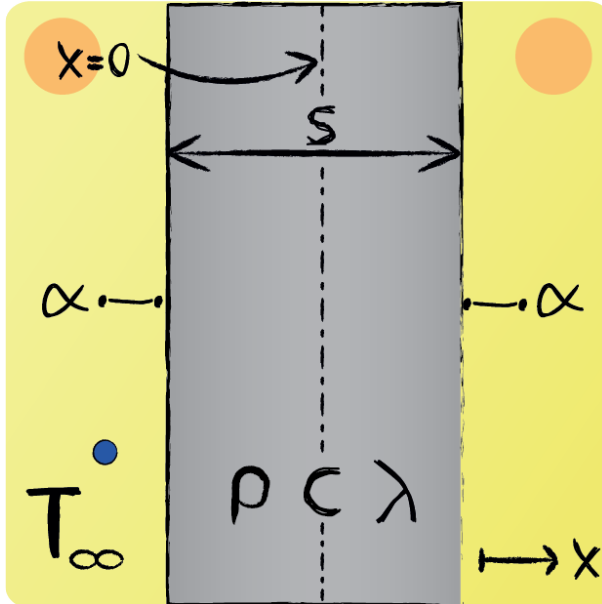
$$\frac{T_m - T_a}{T_o - T_a} = 0.2$$



$$\rightarrow Fo = 17.33$$

$$t = 12507.77 \text{ s}$$

## Exam Preparation - Conduction 28



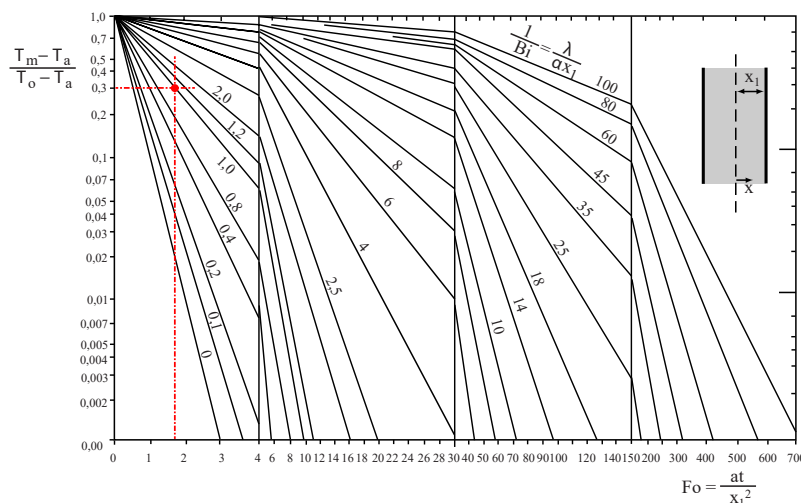
A plate with thickness  $x = 2$  cm with initial homogeneous temperature  $T(x, t = 0) = 293$  K, is suddenly exposed to a medium of temperature  $T_A = 353$  K. Determine the time  $t_1$  at which  $T(x = 0, t_1) = 335$  K is reached.

Problem type:

One-dimensional, unsteady-state heat conduction that does penetrate.

$$\frac{1}{Bi} = \frac{\lambda}{\alpha \cdot x_1} = 1.02$$

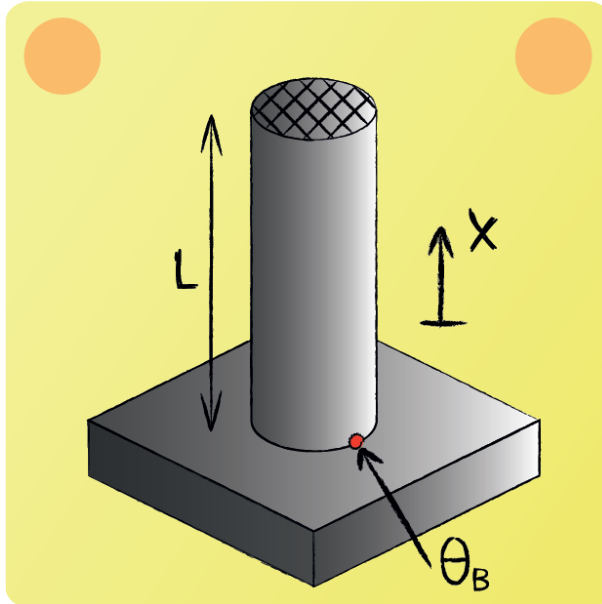
$$\frac{T_m - T_a}{T_o - T_a} = 0.3$$



$$\rightarrow Fo = 1.68$$

$$t = 2884.73 \text{ s}$$

## Conduction Fins 01



Choose the right boundary conditions for a fin with an adiabatic fin head!

Temperature difference:

$$\theta(x) = T(x) - T_A$$

Boundary conditions:

$$T(x = 0) = T_B$$

$$-\lambda \cdot A \cdot \left. \frac{dT}{dx} \right|_{x=L} = 0$$

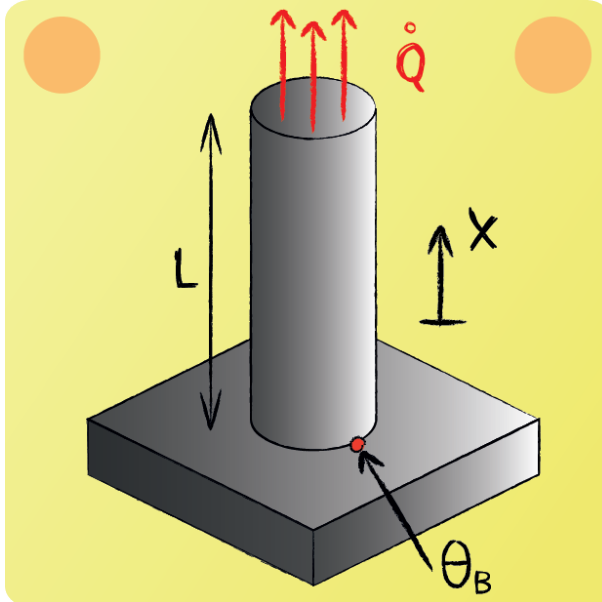


Combining the temperature difference and the boundary conditions results in:

$$\theta(x = 0) = T_B - T_A = \theta_B$$

$$\lambda \cdot \left. \frac{d\theta}{dx} \right|_{x=L} = 0$$

## Conduction Fins 02



Choose the right boundary conditions for a fin with transferring heat at the fin head!

Temperature difference:

$$\theta(x) = T(x) - T_A$$

Boundary conditions:

$$T(x = 0) = T_B$$



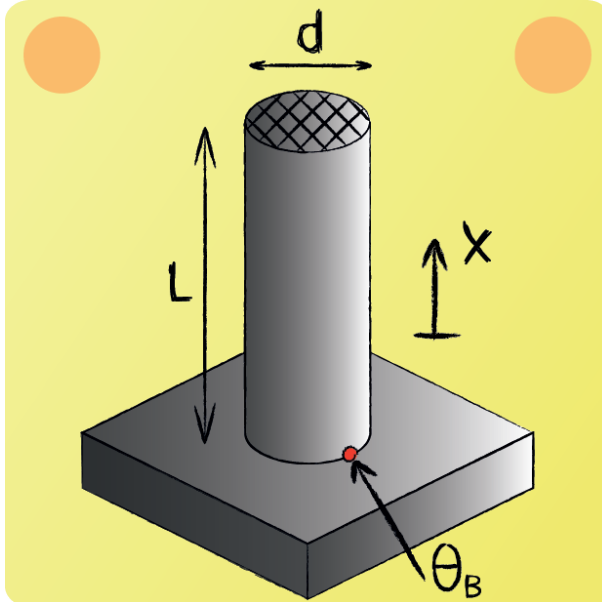
$$-\lambda \cdot A \cdot \left. \frac{dT}{dx} \right|_{x=L} = \alpha \cdot A \cdot (T(x = L) - T_A)$$

Combining the temperature difference and the boundary conditions results in:

$$\theta(x = 0) = T_B - T_A = \theta_B$$

$$-\lambda \cdot \left. \frac{d\theta}{dx} \right|_{x=L} = \alpha \cdot \theta(x = L)$$

## Conduction Fins 03



Calculate the transferred heat for the given fin with an adiabatic head!

Boundary conditions:

$$\theta(x = 0) = \theta_B$$

$$-\lambda \cdot \frac{d\theta}{dx} \Big|_{x=L} = 0$$

Heat flow through the fin:

$$\dot{Q} = \lambda \cdot A_c \cdot m \cdot \theta_B \cdot \tanh(m \cdot L)$$



Where:

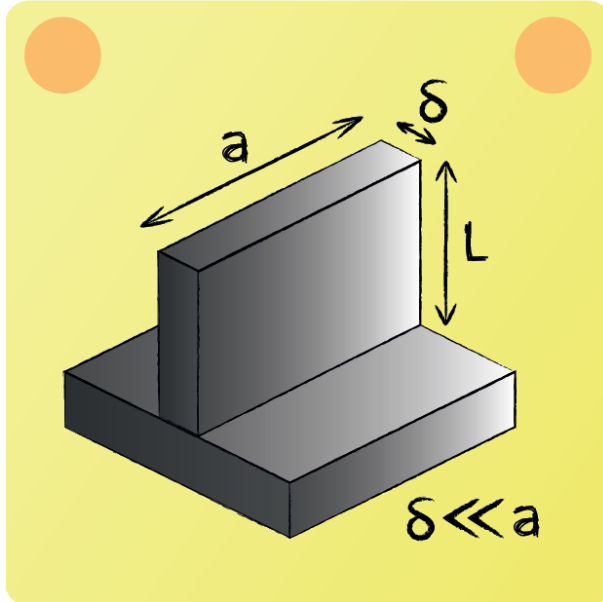
$$m = \sqrt{\frac{4 \cdot \alpha}{\lambda \cdot d}}$$

$$A_c = \frac{1}{4} \pi d^2$$

And thus:

$$\dot{Q} = \lambda \cdot A_c = \frac{1}{4} \pi d^2 \cdot \sqrt{\frac{4 \cdot \alpha}{\lambda \cdot d}} \cdot \theta_B \cdot \tanh\left(\sqrt{\frac{4 \cdot \alpha}{\lambda \cdot d}} \cdot L\right)$$

## Conduction Fins 04



Determine the fin parameter  $m$  for the shown fin geometry.

$$m^2 = \frac{\alpha \cdot U}{\lambda \cdot A_c} = \frac{\alpha \cdot 2 \cdot (\delta + a)}{\lambda \cdot \delta \cdot a} = \frac{2 \cdot \alpha}{\lambda} \cdot \left( \frac{1}{\delta} + \frac{1}{a} \right)$$



Where:

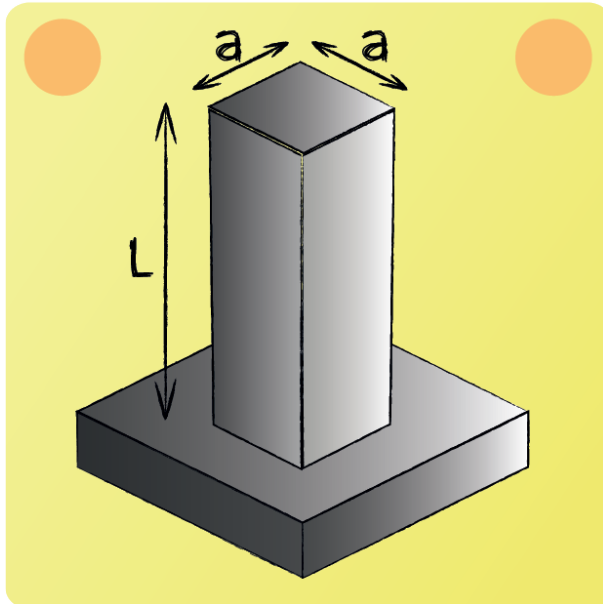
$$\frac{1}{\delta} \gg \frac{1}{a}$$

And thus:

$$m \approx \sqrt{\frac{2 \cdot \alpha}{\lambda \cdot \delta}}$$



## Conduction Fins 05



Determine the fin parameter  $m$  for the shown fin geometry.

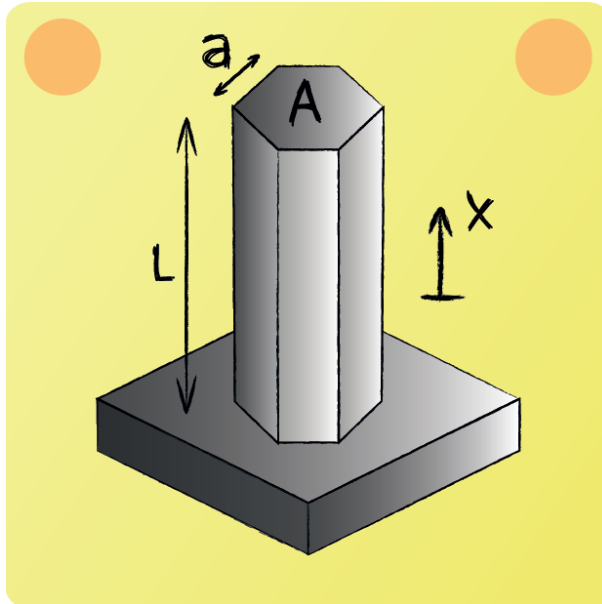


And thus:

$$m^2 = \frac{\alpha \cdot U}{\lambda \cdot A_c} = \frac{\alpha \cdot 4 \cdot a}{\lambda \cdot a^2} = \frac{4 \cdot \alpha}{\lambda \cdot a}$$

$$m = \sqrt{\frac{4 \cdot \alpha}{\lambda \cdot a}}$$

## Conduction Fins 06



Determine the fin parameter  $m$  for the shown fin geometry.

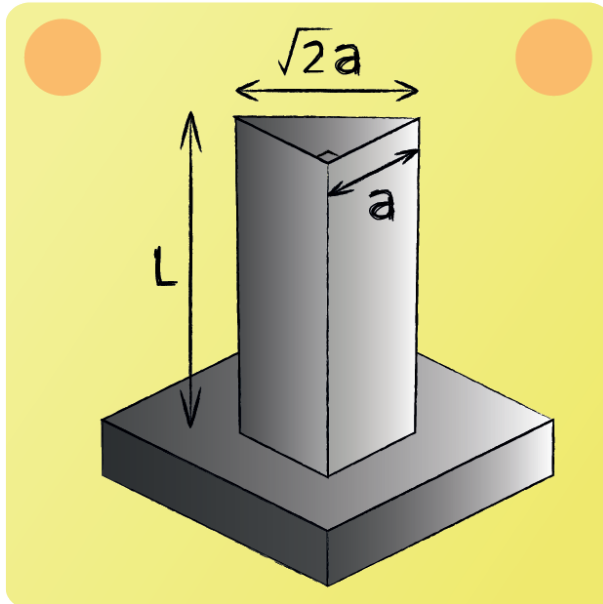


And thus:

$$m^2 = \frac{\alpha \cdot U}{\lambda \cdot A_c} = \frac{\alpha \cdot 6 \cdot a}{\lambda \cdot A_c}$$

$$m = \sqrt{\frac{6 \cdot \alpha \cdot a}{\lambda \cdot A_c}}$$

## Conduction Fins 07



Determine the fin parameter  $m$  for the shown fin geometry.

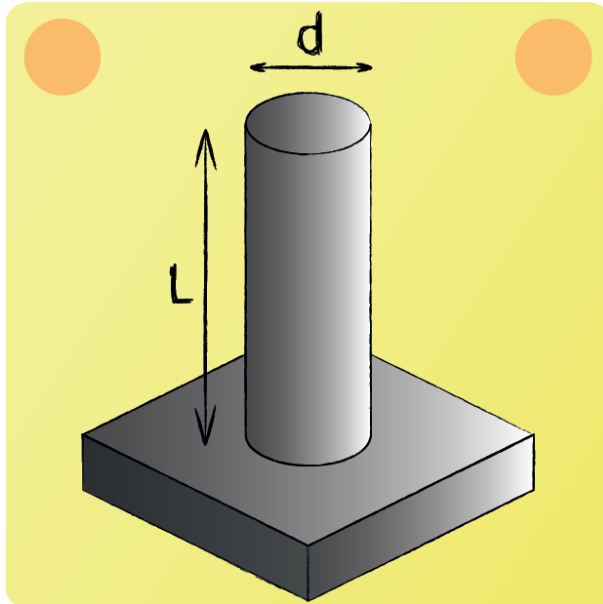


And thus:

$$m^2 = \frac{\alpha \cdot U}{\lambda \cdot A_c} = \frac{\alpha \cdot a \cdot (2 + \sqrt{2})}{\lambda \cdot \frac{1}{2} \cdot a^2}$$

$$m = \sqrt{\frac{\alpha \cdot (4 + 2\sqrt{2})}{\lambda \cdot a}}$$

## Conduction Fins 08



Determine the fin parameter  $m$  for the shown fin geometry.

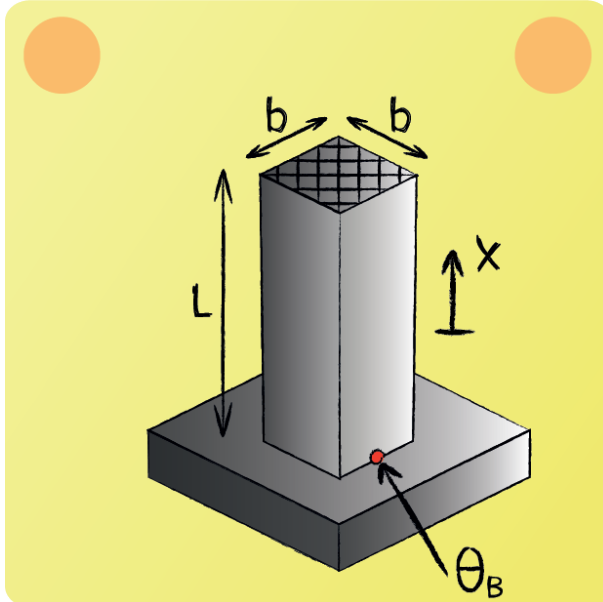


And thus:

$$m^2 = \frac{\alpha \cdot U}{\lambda \cdot A_c} = \frac{\alpha \cdot d \cdot \pi}{\lambda \cdot \frac{1}{4}\pi d^2}$$

$$m = \sqrt{\frac{4 \cdot \alpha}{\lambda \cdot d}}$$

## Conduction Fins 09



Calculate the transferred heat for the given fin with an adiabatic head!

Boundary conditions:

$$\theta(x = 0) = \theta_B$$

$$-\lambda \cdot \frac{d\theta}{dx} \Big|_{x=L} = 0$$

Heat flow through the fin:

$$\dot{Q} = \lambda \cdot A_c \cdot m \cdot \theta_B \cdot \tanh(m \cdot L)$$



Where:

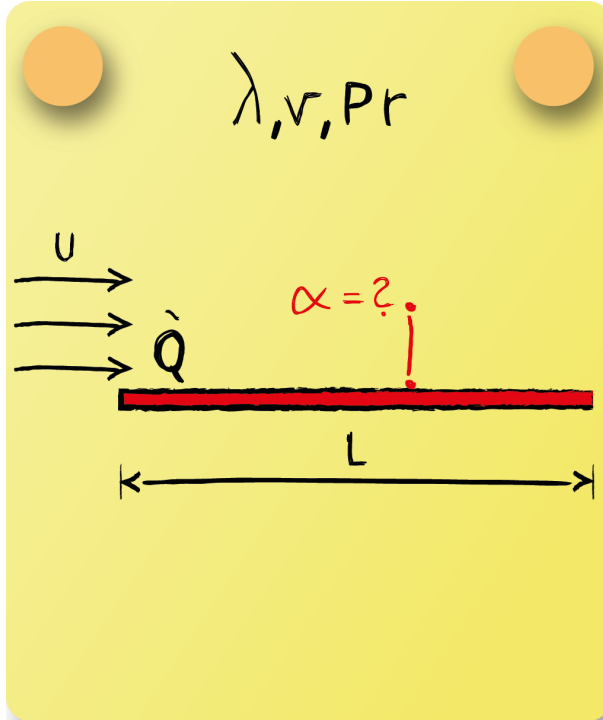
$$m = \sqrt{\frac{4 \cdot \alpha}{\lambda \cdot b}}$$

$$A_c = b^2$$

And thus:

$$\dot{Q} = \lambda \cdot b^2 \cdot \sqrt{\frac{4 \cdot \alpha}{\lambda \cdot b}} \cdot \theta_B \cdot \tanh\left(\sqrt{\frac{4 \cdot \alpha}{\lambda \cdot b}} \cdot L\right)$$

## Heat Transfer Correlation 2.1



A fluid streams over a flat plate.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_L = \frac{u \cdot L}{\nu} = 6.51 \cdot 10^4$$



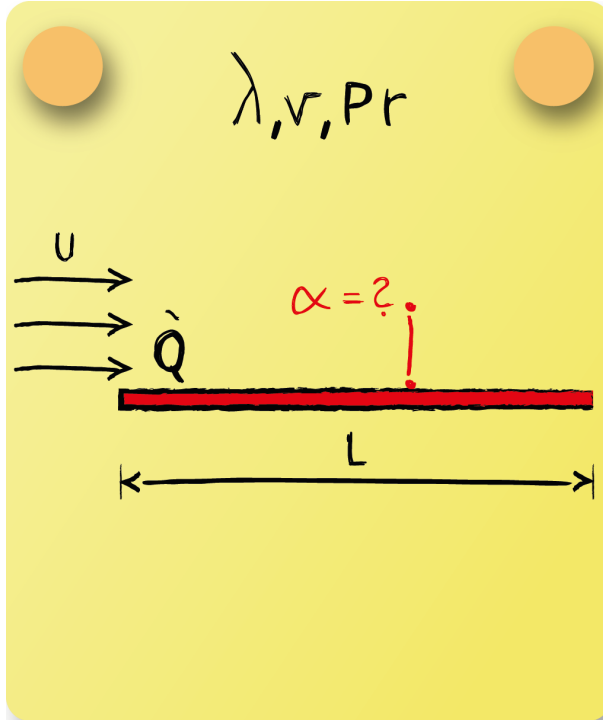
Nusselt number:

$$\overline{Nu}_L = 0.664 \cdot Re_L^{\frac{1}{2}} \cdot Pr^{\frac{1}{3}} = 151.53$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_L \cdot \lambda_f}{L} = 0.78 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 2.2



A fluid streams over a flat plate.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_L = \frac{u \cdot L}{\nu} = 2.40 \cdot 10^3$$



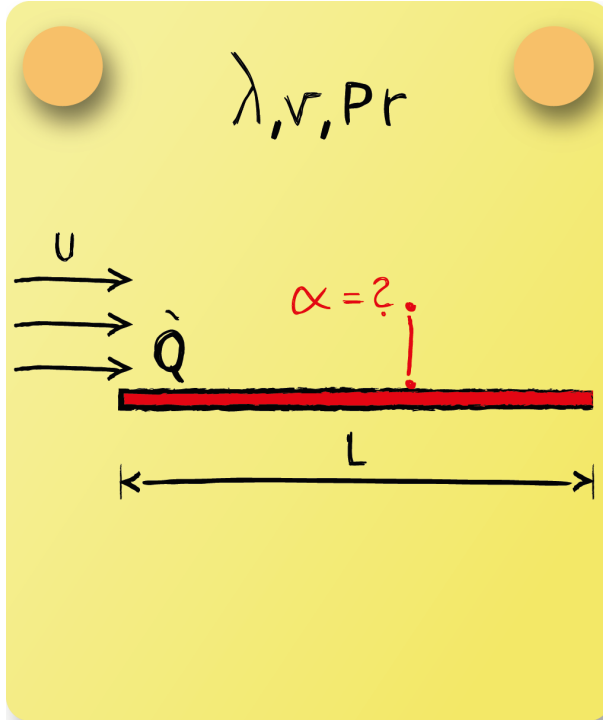
Nusselt number:

$$\overline{Nu}_L = 0.664 \cdot Re_L^{\frac{1}{2}} \cdot Pr^{\frac{1}{3}} = 32.54$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_L \cdot \lambda_f}{L} = 0.163 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 2.3



A fluid streams over a flat plate.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_L = \frac{u \cdot L}{\nu} = 1.52 \cdot 10^4$$



Nusselt number:

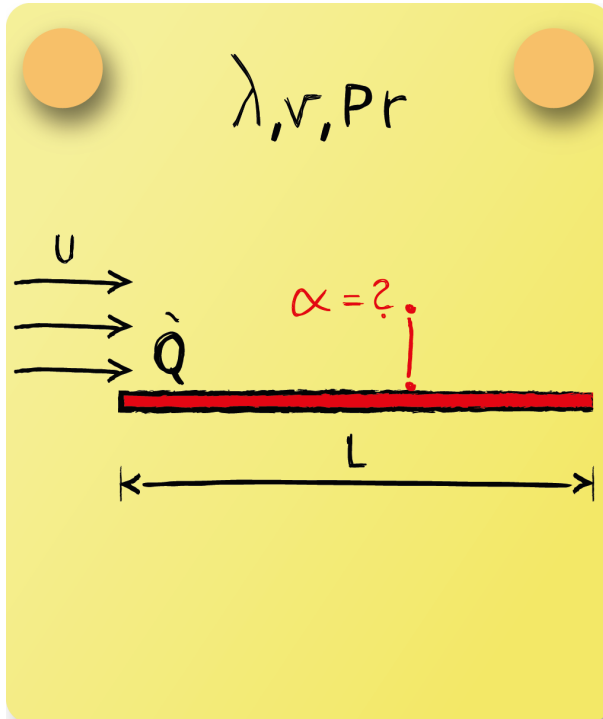
$$\overline{Nu}_L = 0.664 \cdot Re_L^{\frac{1}{2}} \cdot Pr^{\frac{1}{3}} = 133.40$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_L \cdot \lambda_f}{L} = 84.17 \text{ W/m}^2\text{K}$$



## Heat Transfer Correlation 2.4



A fluid streams over a flat plate.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_L = \frac{u \cdot L}{\nu} = 3.38 \cdot 10^4$$



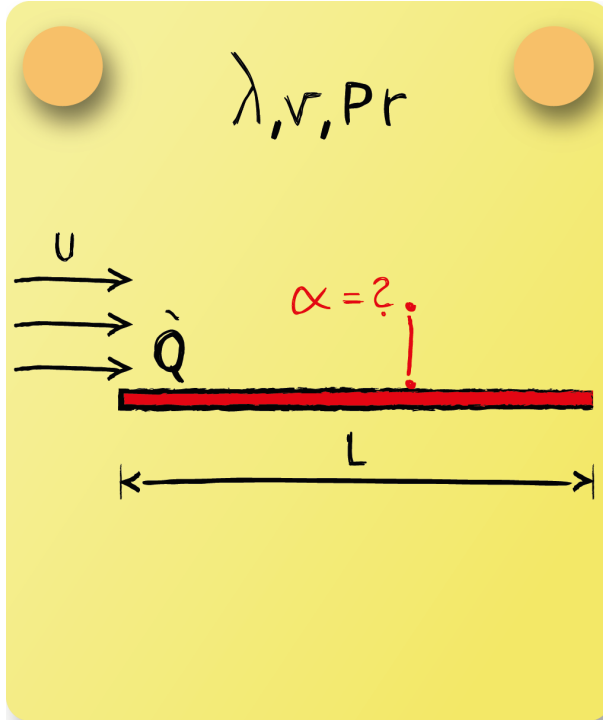
Nusselt number:

$$\overline{Nu}_L = 0.664 \cdot Re_L^{\frac{1}{2}} \cdot Pr^{\frac{1}{3}} = 237.08$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_L \cdot \lambda_f}{L} = 14.60 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 2.5



A fluid streams over a flat plate.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_L = \frac{u \cdot L}{\nu} = 1.85 \cdot 10^3$$



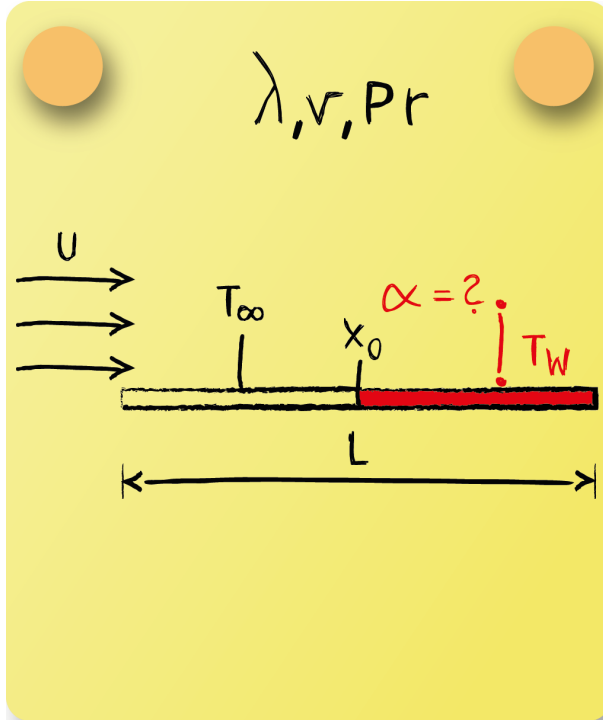
Nusselt number:

$$\overline{Nu}_L = 0.664 \cdot Re_L^{\frac{1}{2}} \cdot Pr^{\frac{1}{3}} = 25.57$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_L \cdot \lambda_f}{L} = 0.247 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 3.1



A fluid streams over a flat plate. The plate is heated from  $x_0$ . Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$\text{Re}_L = \frac{u \cdot L}{\nu} = 2.40 \cdot 10^3$$

Nusselt number:

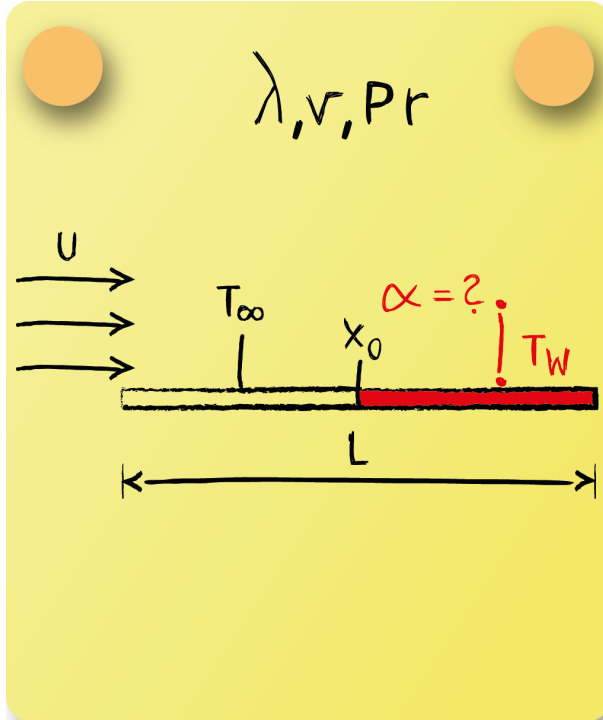


$$\overline{\text{Nu}}_L = 0.664 \cdot \text{Re}_L^{\frac{1}{2}} \cdot \text{Pr}^{\frac{1}{3}} \frac{\left[1 - \left(\frac{x_0}{L}\right)^{\frac{3}{4}}\right]^{\frac{2}{3}}}{\left[1 - \frac{x_0}{L}\right]} = 35.64$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{\text{Nu}}_L \cdot \lambda_f}{L} = 0.18 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 3.2



A fluid streams over a flat plate. The plate is heated from  $x_0$ . Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$\text{Re}_L = \frac{u \cdot L}{\nu} = 1.52 \cdot 10^4$$

Nusselt number:

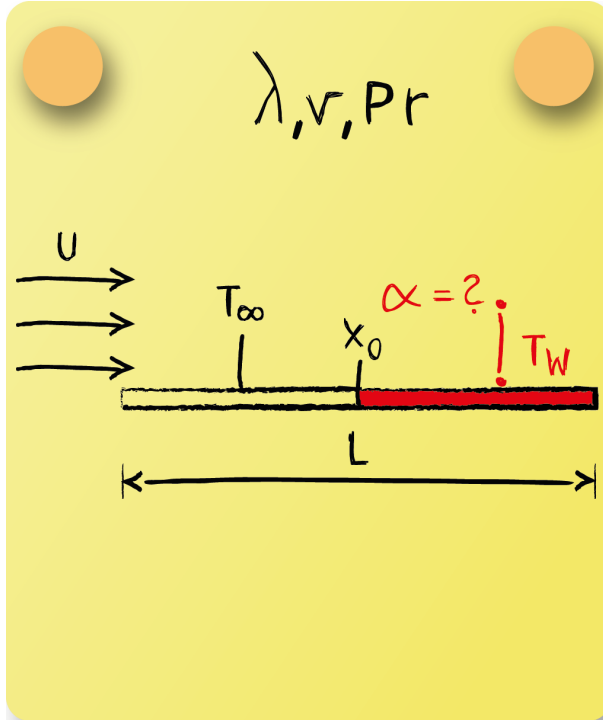


$$\overline{\text{Nu}}_L = 0.664 \cdot \text{Re}_L^{\frac{1}{2}} \cdot \text{Pr}^{\frac{1}{3}} \frac{\left[1 - \left(\frac{x_0}{L}\right)^{\frac{3}{4}}\right]^{\frac{2}{3}}}{\left[1 - \frac{x_0}{L}\right]} = 146.14$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{\text{Nu}}_L \cdot \lambda_f}{L} = 92.21 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 3.3



A fluid streams over a flat plate. The plate is heated from  $x_0$ . Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_L = \frac{u \cdot L}{\nu} = 3.38 \cdot 10^4$$

Nusselt number:

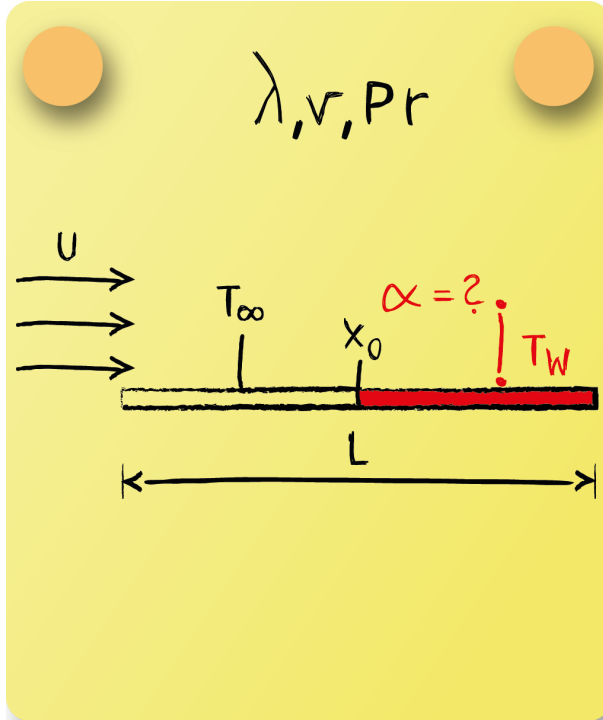


$$\overline{Nu}_L = 0.664 \cdot Re_L^{\frac{1}{2}} \cdot Pr^{\frac{1}{3}} \frac{\left[1 - \left(\frac{x_0}{L}\right)^{\frac{3}{4}}\right]^{\frac{2}{3}}}{\left[1 - \frac{x_0}{L}\right]} = 259.72$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_L \cdot \lambda_f}{L} = 16 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 3.4



A fluid streams over a flat plate. The plate is heated from  $x_0$ . Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_L = \frac{u \cdot L}{\nu} = 1.85 \cdot 10^3$$

Nusselt number:

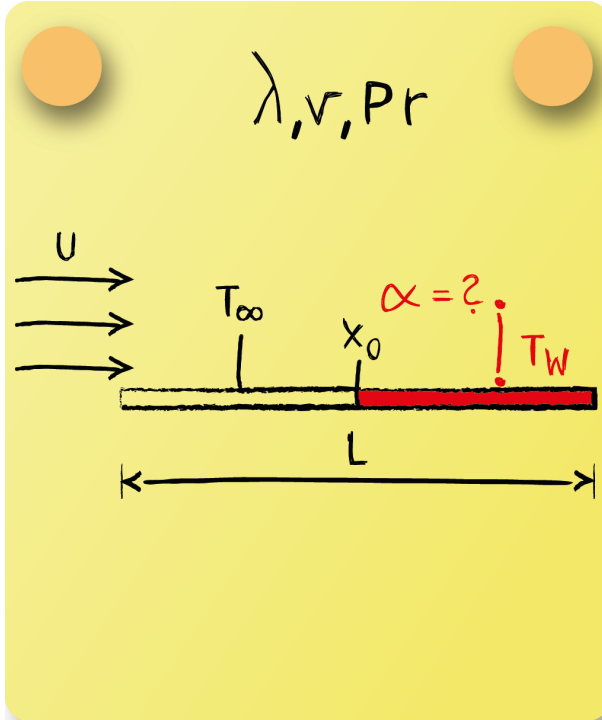


$$\overline{Nu}_L = 0.664 \cdot Re_L^{\frac{1}{2}} \cdot Pr^{\frac{1}{3}} \frac{\left[1 - \left(\frac{x_0}{L}\right)^{\frac{3}{4}}\right]^{\frac{2}{3}}}{\left[1 - \frac{x_0}{L}\right]} = 28.01$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_L \cdot \lambda_f}{L} = 0.27 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 3.5



A fluid streams over a flat plate. The plate is heated from  $x_0$ . Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$\text{Re}_L = \frac{u \cdot L}{\nu} = 6.52 \cdot 10^4$$

Nusselt number:

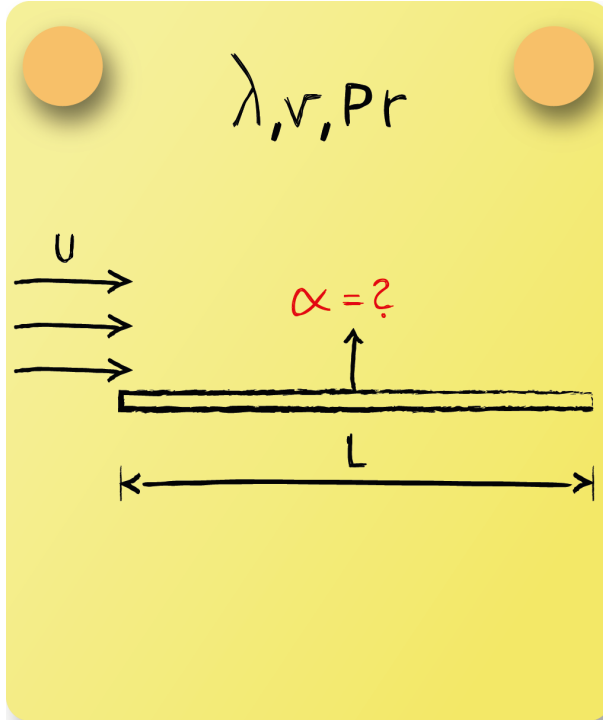


$$\overline{\text{Nu}}_L = 0.664 \cdot \text{Re}_L^{\frac{1}{2}} \cdot \text{Pr}^{\frac{1}{3}} \frac{\left[1 - \left(\frac{x_0}{L}\right)^{\frac{3}{4}}\right]^{\frac{2}{3}}}{\left[1 - \frac{x_0}{L}\right]} = 166.01$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{\text{Nu}}_L \cdot \lambda_f}{L} = 0.85 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 4.1



A fluid streams over a flat plate.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_L = \frac{u \cdot L}{\nu} = 6.52 \cdot 10^5$$



Nusselt number:

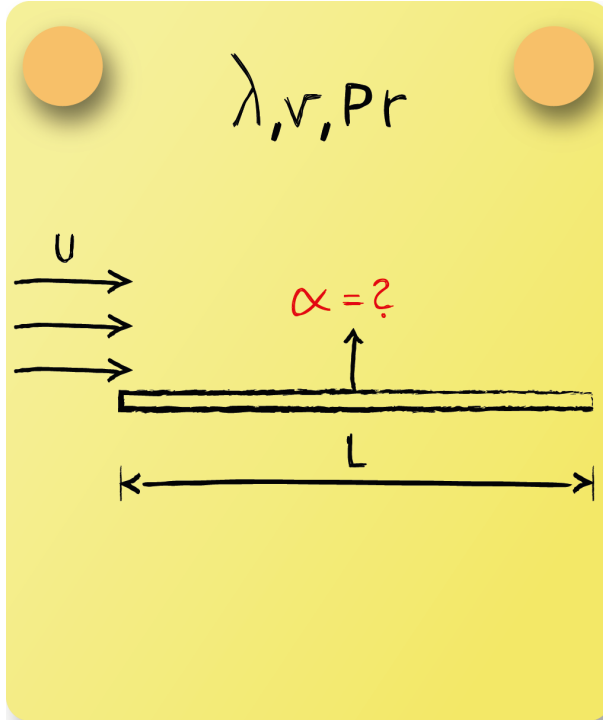
$$\overline{Nu}_L = 0.036 \cdot Pr^{0.43} \cdot (Re_L^{0.8} - 9400) = 1.10 \cdot 10^3$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_L \cdot \lambda_f}{L} = 2.82 \text{ W/m}^2\text{K}$$



## Heat Transfer Correlation 4.2



A fluid streams over a flat plate.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_L = \frac{u \cdot L}{\nu} = 9.61 \cdot 10^5$$



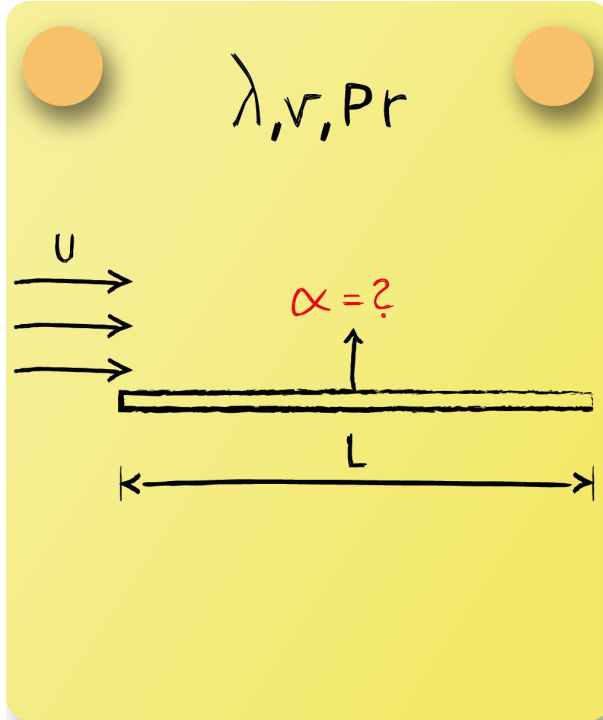
Nusselt number:

$$\overline{Nu}_L = 0.036 \cdot Pr^{0.43} \cdot (Re_L^{0.8} - 9400) = 1.86 \cdot 10^3$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_L \cdot \lambda_f}{L} = 4.67 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 4.3



A fluid streams over a flat plate.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$\text{Re}_L = \frac{u \cdot L}{\nu} = 7.60 \cdot 10^5$$



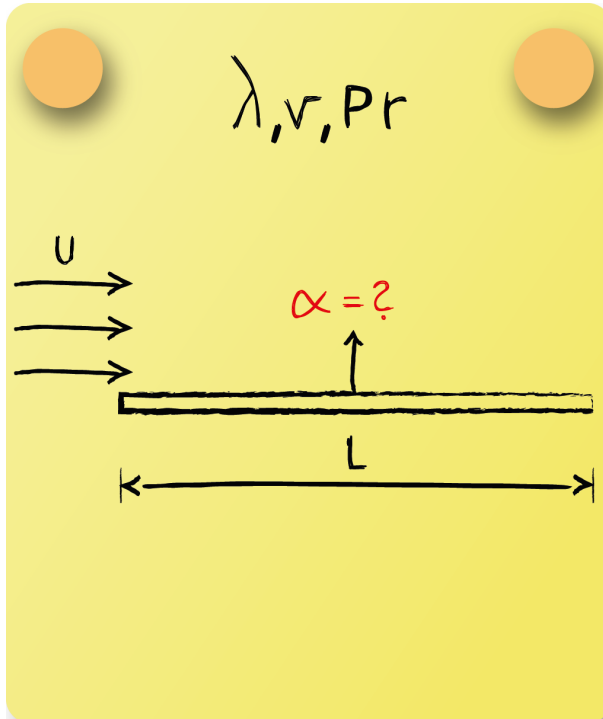
Nusselt number:

$$\overline{\text{Nu}}_L = 0.036 \cdot \text{Pr}^{0.43} \cdot (\text{Re}_L^{0.8} - 9400) = 2.79 \cdot 10^3$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{\text{Nu}}_L \cdot \lambda_f}{L} = 1759 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 4.4



A fluid streams over a flat plate.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_L = \frac{u \cdot L}{\nu} = 7.40 \cdot 10^5$$



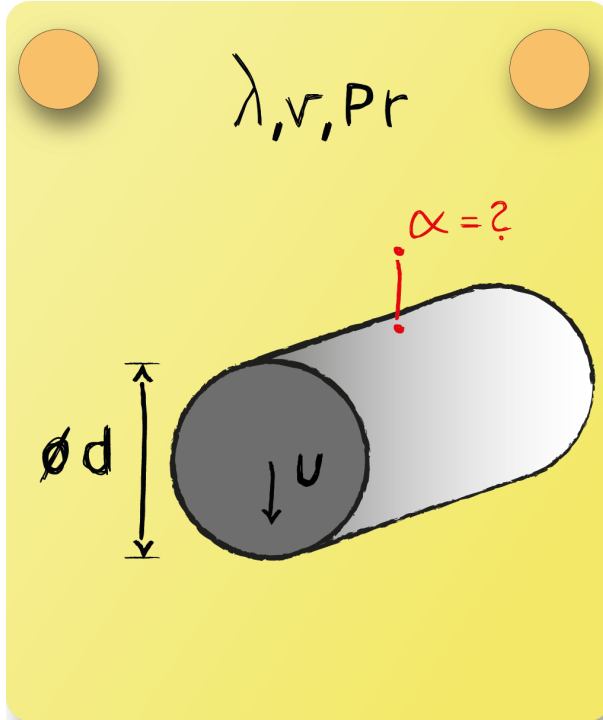
Nusselt number:

$$\overline{Nu}_L = 0.036 \cdot Pr^{0.43} \cdot (Re_L^{0.8} - 9400) = 1.25 \cdot 10^3$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_L \cdot \lambda_f}{L} = 3.03 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 5.1



A cylinder falls through a non-moving fluid. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 6.67 \cdot 10^4$$



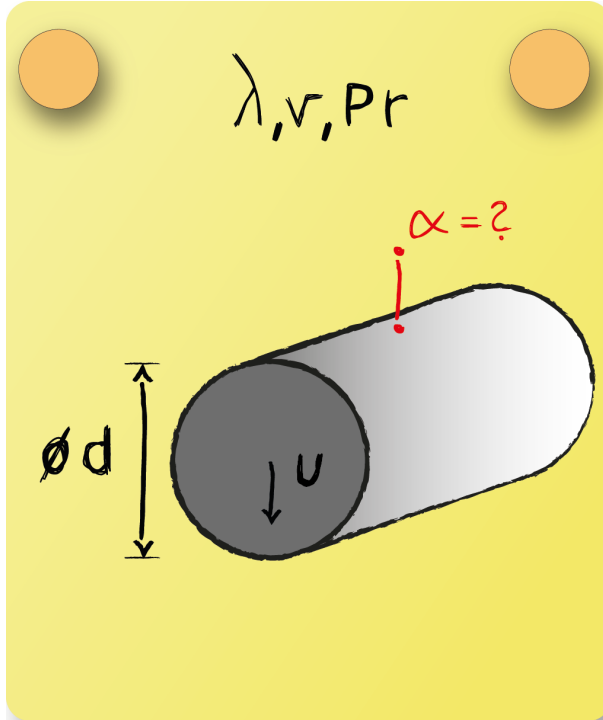
Nusselt number:

$$\overline{Nu}_d = 0.0266 \cdot Re_d^{0.805} \cdot Pr^{0.4} = 177.27$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 23.05 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 5.2



A cylinder falls through a non-moving fluid. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 3.33 \cdot 10^3$$



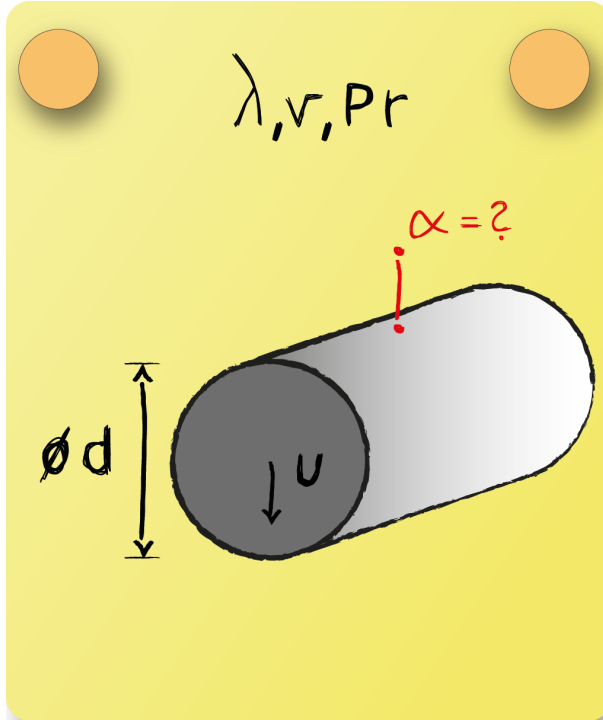
Nusselt number:

$$\overline{Nu}_d = 0.683 \cdot Re_d^{0.466} \cdot Pr^{0.4} = 28.95$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 156.31 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 5.3



A cylinder falls through a non-moving fluid. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 2.94 \cdot 10^4$$



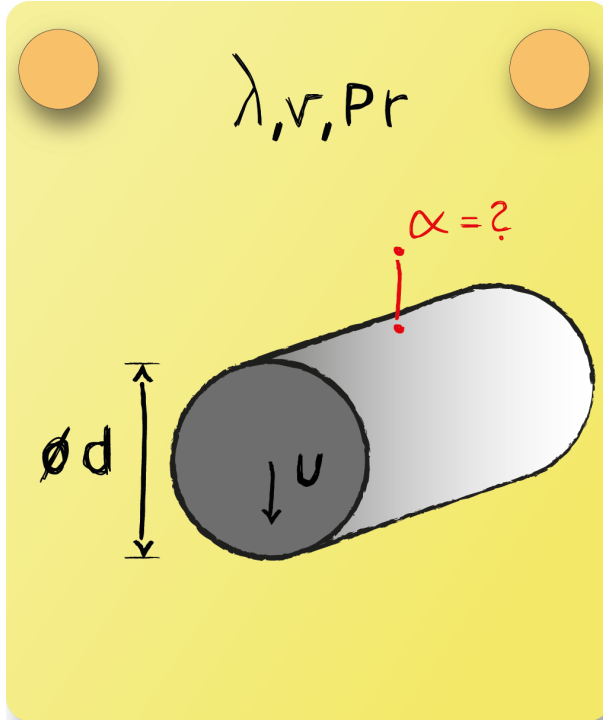
Nusselt number:

$$\overline{Nu}_d = 0.193 \cdot Re_d^{0.618} \cdot Pr^{0.4} = 242.74$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 1238.0 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 5.4



A cylinder falls through a non-moving fluid. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 5.56$$



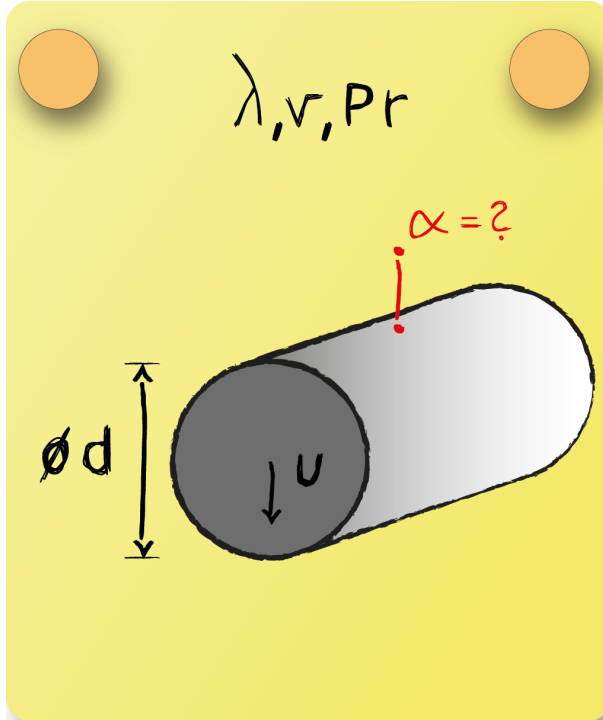
Nusselt number:

$$\overline{Nu_d} = 0.911 \cdot Re_d^{0.385} \cdot Pr^{0.4} = 6.39$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu_d} \cdot \lambda_f}{d} = 70.27 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 5.5



A cylinder falls through a non-moving fluid. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 0.794$$



Nusselt number:

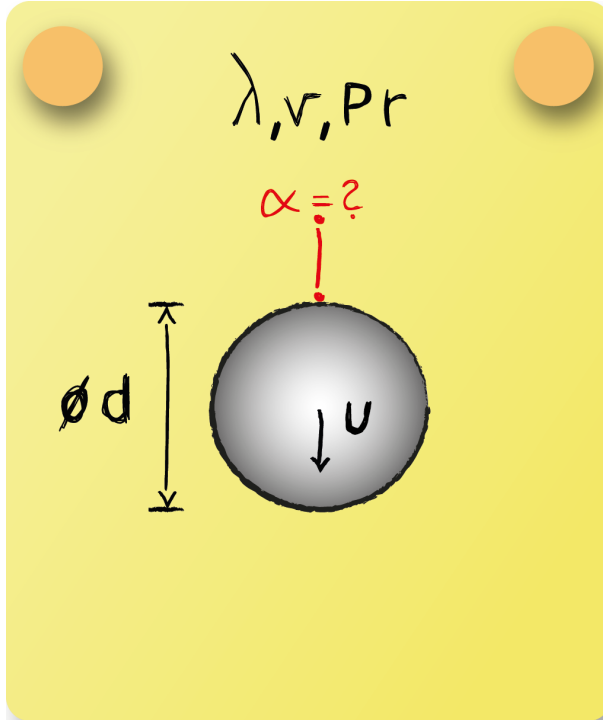
$$\overline{Nu}_d = 0.989 \cdot Re_d^{0.330} \cdot Pr^{0.4} = 0.781$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 15.77 \text{ W/m}^2\text{K}$$



## Heat Transfer Correlation 11.1



A sphere falls through a non-moving fluid. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 6.51 \cdot 10^4$$



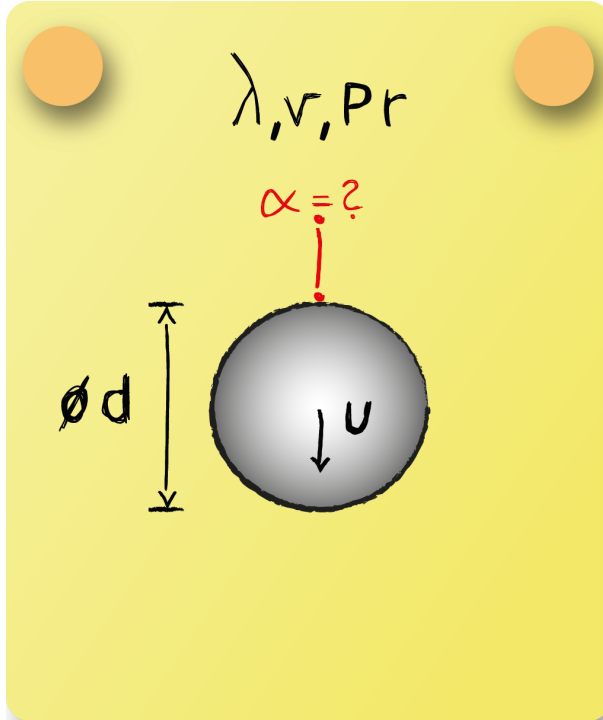
Nusselt number:

$$\overline{Nu_d} = 2 + \left( 0.4 \cdot Re_d^{\frac{1}{2}} + 0.06 \cdot Re_d^{\frac{2}{3}} \right) \cdot Pr^{0.4} \cdot \left( \frac{\eta_{\infty}}{\eta_w} \right)^{\frac{1}{4}} = 176.20$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu_d} \cdot \lambda_f}{d} = 22.55 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 11.2



A sphere falls through a non-moving fluid. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 1.20 \cdot 10^4$$

Nusselt number:

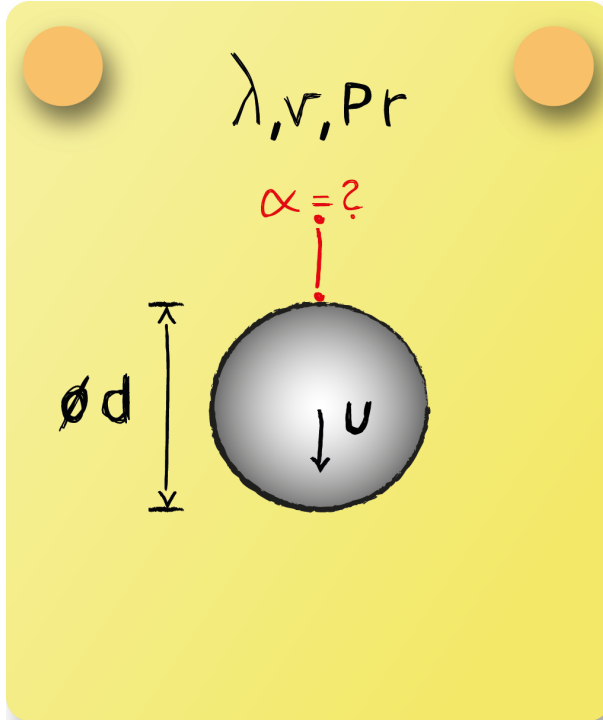


$$\overline{Nu_d} = 2 + \left( 0.4 \cdot Re_d^{\frac{1}{2}} + 0.06 \cdot Re_d^{\frac{2}{3}} \right) \cdot Pr^{0.4} \cdot \left( \frac{\eta_{\infty}}{\eta_w} \right)^{\frac{1}{4}} = 77.28$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu_d} \cdot \lambda_f}{d} = 193.83 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 11.3



A sphere falls through a non-moving fluid. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 2.79 \cdot 10^4$$

Nusselt number:

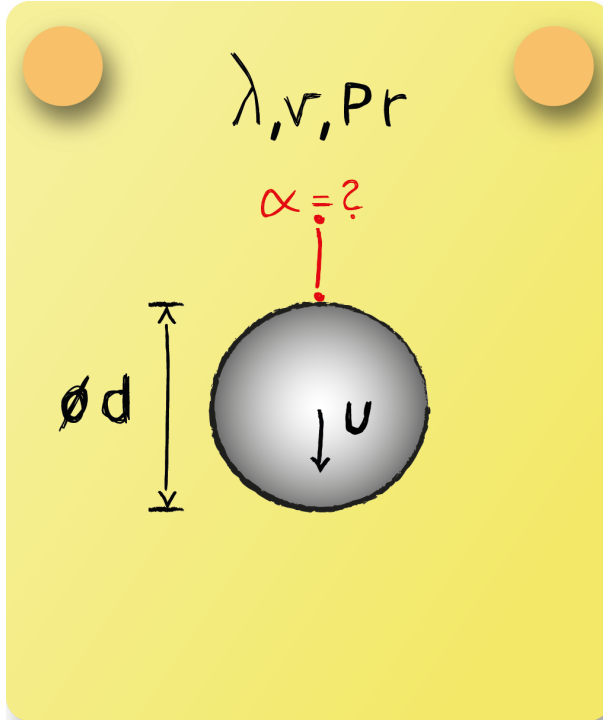


$$\overline{Nu_d} = 2 + \left( 0.4 \cdot Re_d^{\frac{1}{2}} + 0.06 \cdot Re_d^{\frac{2}{3}} \right) \cdot Pr^{0.4} \cdot \left( \frac{\eta_{\infty}}{\eta_w} \right)^{\frac{1}{4}} = 347.25$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu_d} \cdot \lambda_f}{d} = 1948.08 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 11.4



A sphere falls through a non-moving fluid. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 15.20$$

Nusselt number:

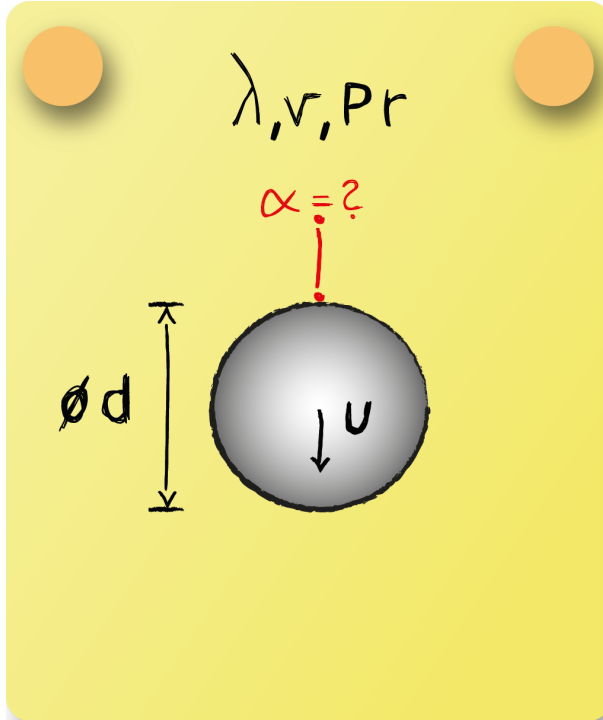


$$\overline{Nu}_d = 2 + \left( 0.4 \cdot Re_d^{\frac{1}{2}} + 0.06 \cdot Re_d^{\frac{2}{3}} \right) \cdot Pr^{0.4} \cdot \left( \frac{\eta_{\infty}}{\eta_w} \right)^{\frac{1}{4}} = 5.46$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 344.74 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 11.5



A sphere falls through a non-moving fluid. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 54.95$$

Nusselt number:

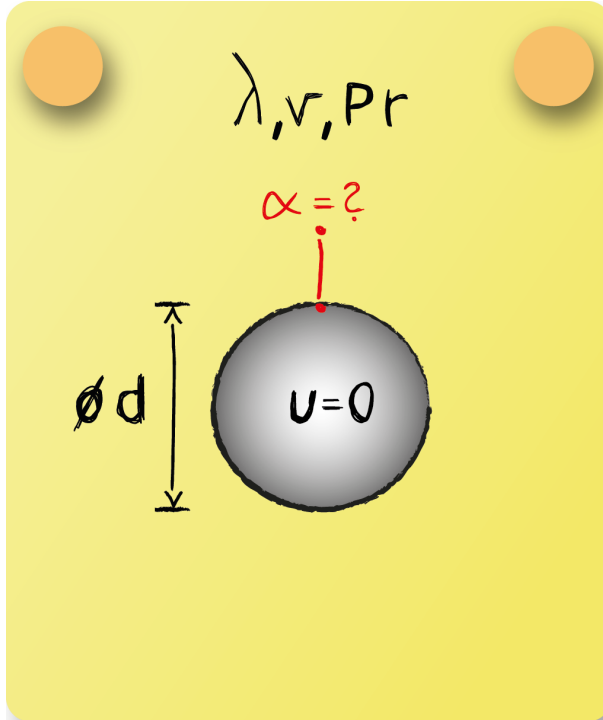


$$\overline{Nu}_d = 2 + \left( 0.4 \cdot Re_d^{\frac{1}{2}} + 0.06 \cdot Re_d^{\frac{2}{3}} \right) \cdot Pr^{0.4} \cdot \left( \frac{\eta_{\infty}}{\eta_w} \right)^{\frac{1}{4}} = 16.04$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 186.08 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 12.1



A sphere is in a non-moving fluid.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 0$$



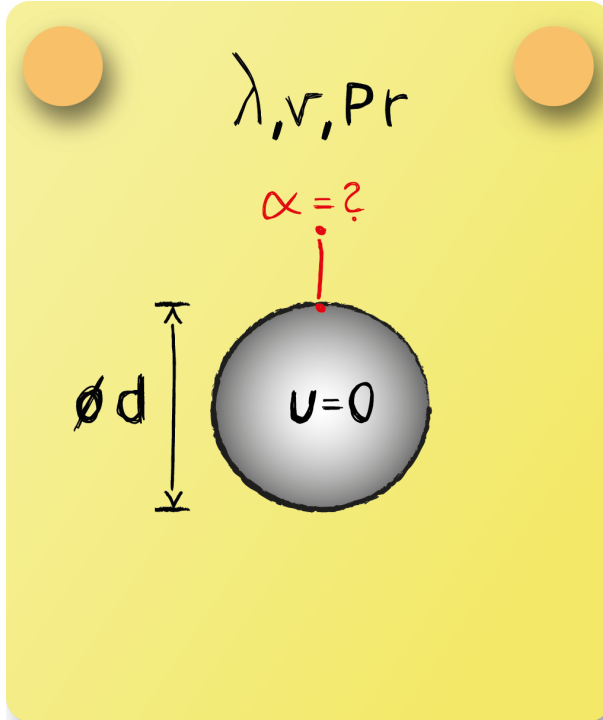
Nusselt number:

$$\overline{Nu}_d = 2 + \left( 0.4 \cdot Re_d^{\frac{1}{2}} + 0.06 \cdot Re_d^{\frac{2}{3}} \right) \cdot Pr^{0.4} \cdot \left( \frac{\eta_{\infty}}{\eta_w} \right)^{\frac{1}{4}} = 2$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 0.256 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 12.2



A sphere is in a non-moving fluid.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 0$$



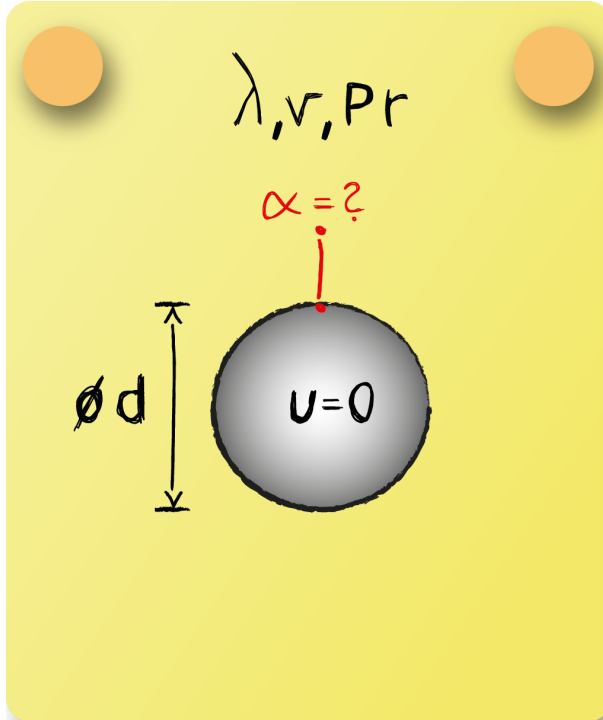
Nusselt number:

$$\overline{Nu}_d = 2 + \left( 0.4 \cdot Re_d^{\frac{1}{2}} + 0.06 \cdot Re_d^{\frac{2}{3}} \right) \cdot Pr^{0.4} \cdot \left( \frac{\eta_{\infty}}{\eta_w} \right)^{\frac{1}{4}} = 2$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 5.02 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 12.3



A sphere is in a non-moving fluid.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 0$$



Nusselt number:

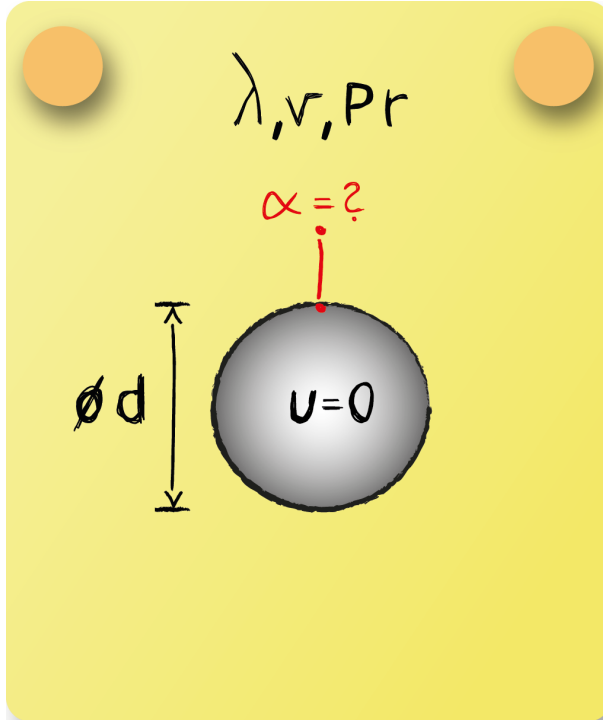
$$\overline{Nu}_d = 2 + \left( 0.4 \cdot Re_d^{\frac{1}{2}} + 0.06 \cdot Re_d^{\frac{2}{3}} \right) \cdot Pr^{0.4} \cdot \left( \frac{\eta_{\infty}}{\eta_w} \right)^{\frac{1}{4}} = 2$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 11.22 \text{ W/m}^2\text{K}$$



## Heat Transfer Correlation 12.4



A sphere is in a non-moving fluid.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 0$$



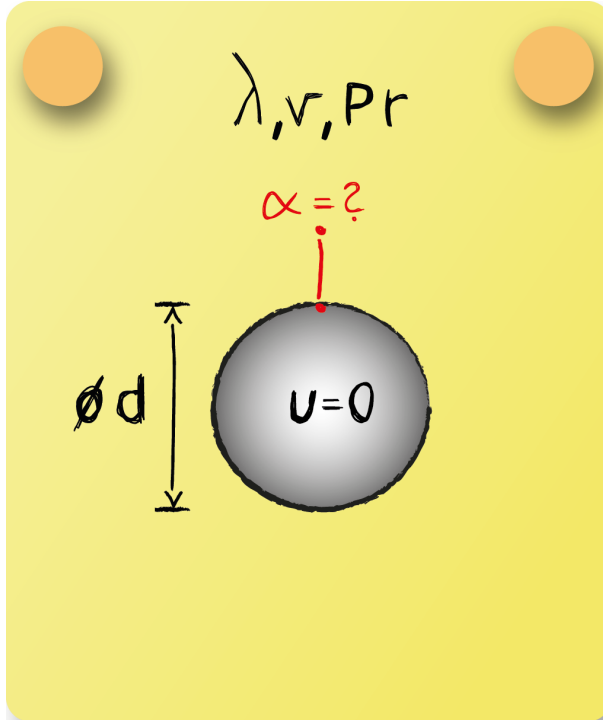
Nusselt number:

$$\overline{Nu}_d = 2 + \left( 0.4 \cdot Re_d^{\frac{1}{2}} + 0.06 \cdot Re_d^{\frac{2}{3}} \right) \cdot Pr^{0.4} \cdot \left( \frac{\eta_{\infty}}{\eta_w} \right)^{\frac{1}{4}} = 2$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 126.2 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 12.5



A sphere is in a non-moving fluid.  
Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 0$$



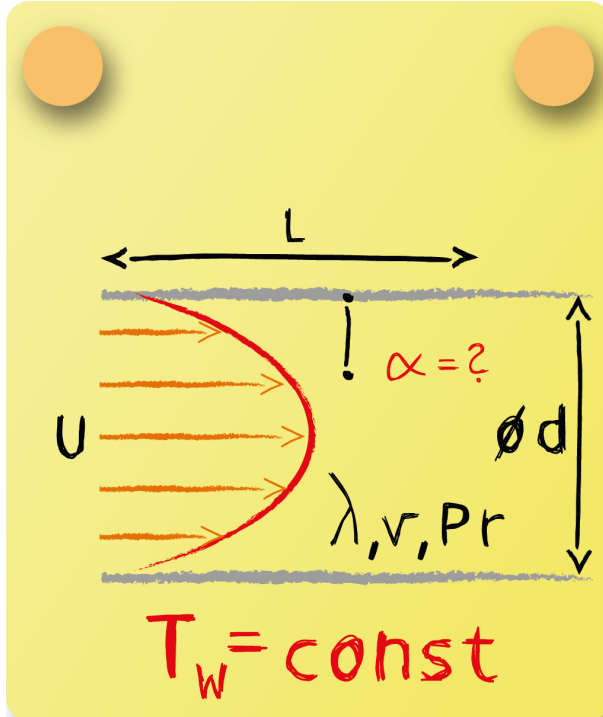
Nusselt number:

$$\overline{Nu}_d = 2 + \left( 0.4 \cdot Re_d^{\frac{1}{2}} + 0.06 \cdot Re_d^{\frac{2}{3}} \right) \cdot Pr^{0.4} \cdot \left( \frac{\eta_{\infty}}{\eta_w} \right)^{\frac{1}{4}} = 2$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 23.2 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 13.1



A fluid flows through a pipe with isothermal surface. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 1400$$

Thermal entry length:

$$L_{th} = 0.05 \cdot Re_d \cdot Pr \cdot d = 4.97 \text{ m} > L$$



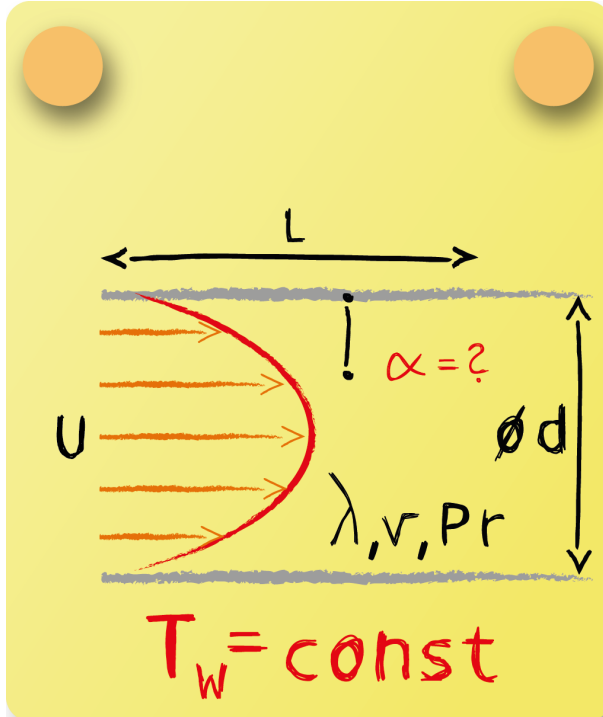
Nusselt number:

$$\overline{Nu_d} = \left( 3.66 + \frac{0.0677 \cdot (Re_d \cdot Pr \cdot \frac{d}{L})^{1.33}}{1 + 0.1 \cdot Pr \cdot (Re_d \cdot \frac{d}{L})^{0.83}} \right) \cdot \left( \frac{\eta}{\eta_w} \right)^{0.14} = 5.72$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu_d} \cdot \lambda_f}{d} = 1.49 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 13.2



A fluid flows through a pipe with isothermal surface. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 1266.67$$

Thermal entry length:

$$L_{th} = 0.05 \cdot Re_d \cdot Pr \cdot d = 0.58 \text{ m} > L$$



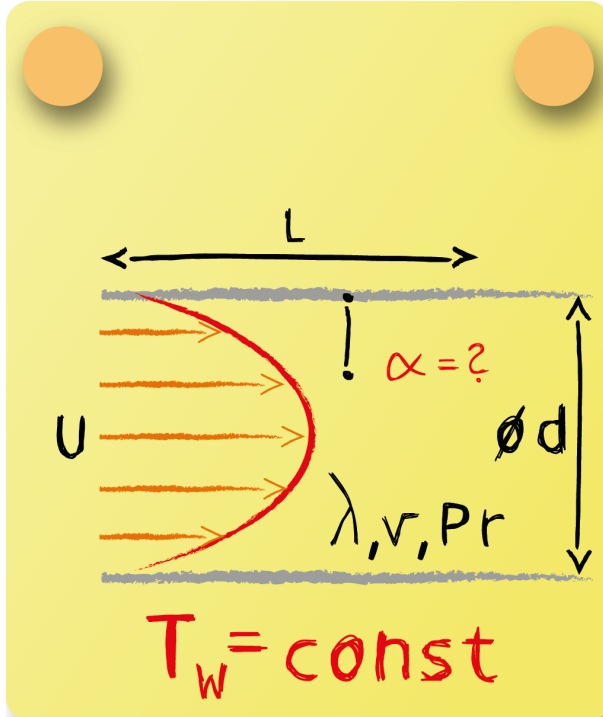
Nusselt number:

$$\overline{Nu}_d = \left( 3.66 + \frac{0.0677 \cdot (Re_d \cdot Pr \cdot \frac{d}{L})^{1.33}}{1 + 0.1 \cdot Pr \cdot (Re_d \cdot \frac{d}{L})^{0.83}} \right) \cdot \left( \frac{\eta}{\eta_w} \right)^{0.14} = 5.56$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu}_d \cdot \lambda_f}{d} = 30.03 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 13.3



Reynolds number:

$$\text{Re}_d = \frac{u \cdot d}{\nu} = 1823.53$$

Thermal entry length:

$$L_{\text{th}} = 0.05 \cdot \text{Re}_d \cdot \text{Pr} \cdot d = 197.85 \text{ m} > L$$



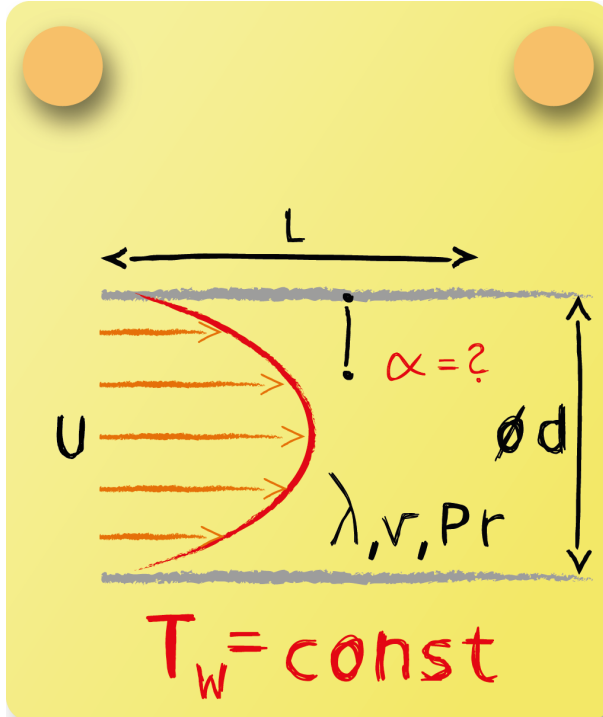
Nusselt number:

$$\overline{\text{Nu}}_d = \left( 3.66 + \frac{0.0677 \cdot (\text{Re}_d \cdot \text{Pr} \cdot \frac{d}{L})^{1.33}}{1 + 0.1 \cdot \text{Pr} \cdot (\text{Re}_d \cdot \frac{d}{L})^{0.83}} \right) \cdot \left( \frac{\eta}{\eta_w} \right)^{0.14} = 7.29$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{\text{Nu}}_d \cdot \lambda_f}{d} = 12.00 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 13.4



A fluid flows through a pipe with isothermal surface. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$\text{Re}_d = \frac{u \cdot d}{\nu} = 1861.11$$

Thermal entry length:

$$L_{\text{th}} = 0.05 \cdot \text{Re}_d \cdot \text{Pr} \cdot d = 155.87 \text{ m} > L$$



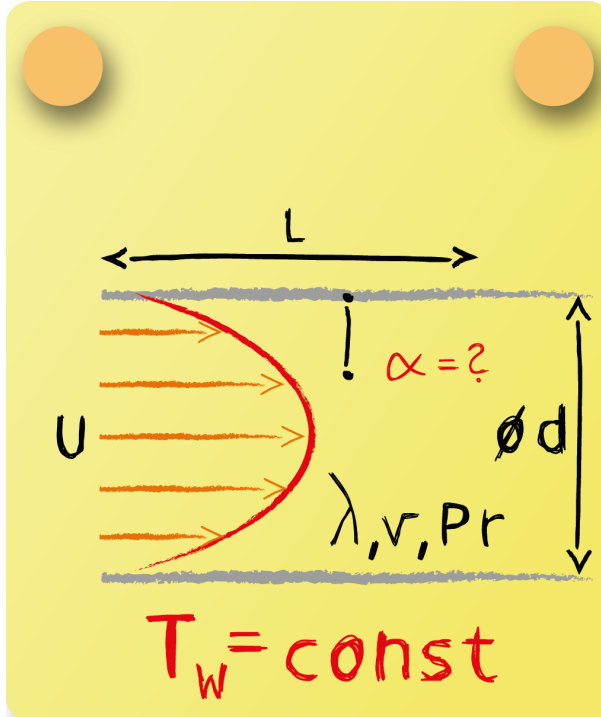
Nusselt number:

$$\overline{\text{Nu}}_d = \left( 3.66 + \frac{0.0677 \cdot (\text{Re}_d \cdot \text{Pr} \cdot \frac{d}{L})^{1.33}}{1 + 0.1 \cdot \text{Pr} \cdot (\text{Re}_d \cdot \frac{d}{L})^{0.83}} \right) \cdot \left( \frac{\eta}{\eta_w} \right)^{0.14} = 4.88$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{\text{Nu}}_d \cdot \lambda_f}{d} = 8.01 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 13.5



A fluid flows through a pipe with isothermal surface. Calculate the mean heat transfer coefficient  $\bar{\alpha}$ .

Reynolds number:

$$Re_d = \frac{u \cdot d}{\nu} = 214.29$$

Thermal entry length:

$$L_{th} = 0.05 \cdot Re_d \cdot Pr \cdot d = 0.065 \text{ m} > L$$



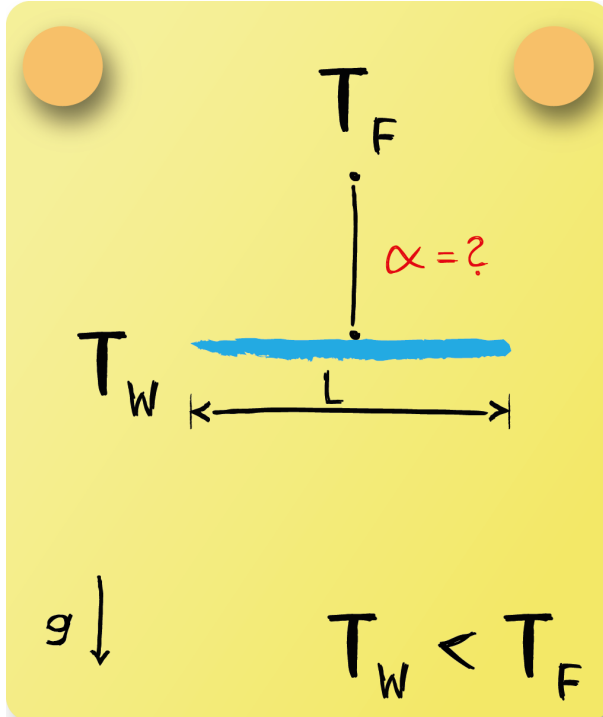
Nusselt number:

$$\overline{Nu_d} = \left( 3.66 + \frac{0.0677 \cdot (Re_d \cdot Pr \cdot \frac{d}{L})^{1.33}}{1 + 0.1 \cdot Pr \cdot (Re_d \cdot \frac{d}{L})^{0.83}} \right) \cdot \left( \frac{\eta}{\eta_w} \right)^{0.14} = 5.80$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{Nu_d} \cdot \lambda_f}{d} = 128.93 \text{ W/m}^2\text{K}$$

## Heat Transfer Correlation 20



A horizontal plate stands in a non-moving ideal gas. Calculate the mean heat transfer coefficient  $\bar{\alpha}$  on the upper surface.

Coefficient of volume expansion for an ideal gas:

$$\beta = \frac{1}{T_F} = 0.0033 \text{ K}^{-1}$$

Grashof number:

$$\text{Gr}_L = \frac{g \cdot \beta \cdot (T_F - T_w) \cdot L^3}{\nu^2} = 4.662 \cdot 10^5$$



And thus  $\text{Gr}_L \cdot \text{Pr} = 3.053 \cdot 10^5$ .

Nusselt number:

$$\overline{\text{Nu}}_L = 0.27 \cdot (\text{Gr}_L \cdot \text{Pr})^{\frac{1}{4}} = 6.35$$

Heat transfer coefficient:

$$\bar{\alpha} = \frac{\overline{\text{Nu}}_L \cdot \lambda_f}{L} = 4.95 \text{ W/m}^2\text{K}$$