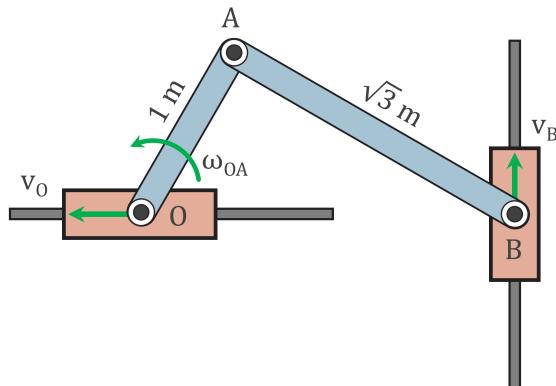


Two DOF Planar Manipulator



The two degree of freedom manipulator is driven by two linear actuators (O and B). The lines from O to A and from B to A are perpendicular to each other in the given situation. The length of the arms OA and AB are 1 m and $\sqrt{3}$ m respectively. Calculate the velocity of actuator B in m/s , if the velocity of actuator O is known to be $v_O = \frac{3}{2}\sqrt{3}$ m/s and the angular velocity of arm OA is $\omega_{OA} = \frac{5}{4}$ rad/s.

Using known expressions:

$$\mathbf{v}_A = \mathbf{v}_O + \boldsymbol{\omega}_{OA} \times \mathbf{r}_{A/O} + \mathbf{v}_{\text{rel}} \quad (1)$$

$$\mathbf{v}_A = \mathbf{v}_B + \boldsymbol{\omega}_{AB} \times \mathbf{r}_{A/B} + \mathbf{v}_{\text{rel}} \quad (2)$$

Given:

Length of OA: $L_{OA} = 1$ m

Length of AB: $L_{AB} = \sqrt{3}$ m

Velocity of O: $v_O = \frac{3}{2}\sqrt{3}$ m/s

Angular velocity arm OA: $\omega_{OA} = \frac{5}{4}$ rad/s

Angle \angle OAB: 90°

Solution:

Using trigonometry it can be seen that $\angle BOA = 60^\circ$, since it is given that $L_{OA} = 1$, $L_{AB} = \sqrt{3}$ and $\angle OAB = 90^\circ$ (triangle $\triangle OAB$ is a $30 - 60 - 90$ triangle). For the derivations we use θ for the $\angle BOA$. Inserting the known values (with $v_{rel} = 0$) in Equation 1 gives:

$$\mathbf{v}_A = \begin{pmatrix} -v_O \\ 0 \\ 0 \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ \omega_{OA} \end{pmatrix} \times \begin{pmatrix} \cos \theta \\ \sin \theta \\ 0 \end{pmatrix} L_{OA} + \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} \quad (3)$$

$$\mathbf{v}_A = \begin{pmatrix} -v_O \\ 0 \\ 0 \end{pmatrix} + \begin{pmatrix} -\sin \theta \\ \cos \theta \\ 0 \end{pmatrix} L_{OA} \cdot \omega_{OA} = \begin{pmatrix} -v_O - \sin \theta \cdot L_{OA} \cdot \omega_{OA} \\ \cos \theta \cdot L_{OA} \cdot \omega_{OA} \\ 0 \end{pmatrix} \quad (4)$$

Inserting the known values (with $v_{rel} = 0$) in Equation 2 gives:

$$\mathbf{v}_A = \begin{pmatrix} 0 \\ v_B \\ 0 \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ \omega_{AB} \end{pmatrix} \times \begin{pmatrix} -\sin \theta \\ \cos \theta \\ 0 \end{pmatrix} L_{AB} + \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} \quad (5)$$

$$\mathbf{v}_A = \begin{pmatrix} 0 \\ v_B \\ 0 \end{pmatrix} + \begin{pmatrix} -\sin \theta \\ -\cos \theta \\ 0 \end{pmatrix} \cdot L_{AB} \cdot \omega_{AB} = \begin{pmatrix} -\cos \theta \cdot L_{AB} \cdot \omega_{AB} \\ v_B - \sin \theta \cdot L_{AB} \cdot \omega_{AB} \\ 0 \end{pmatrix} \quad (6)$$

We now have two equations (Equations 4 and 6) for v_A that must be equal to each other. This follows.

$$\begin{pmatrix} -v_O - \sin \theta \cdot L_{OA} \cdot \omega_{OA} \\ \cos \theta \cdot L_{OA} \cdot \omega_{OA} \\ 0 \end{pmatrix} = \begin{pmatrix} -\cos \theta \cdot L_{AB} \cdot \omega_{AB} \\ v_B - \sin \theta \cdot L_{AB} \cdot \omega_{AB} \\ 0 \end{pmatrix} \quad (7)$$

This gives us two equations with two unknowns, ω_{AB} and v_B , thus it is possible to solve for v_B . First we solve for $-L_{AB} \cdot \omega_{AB}$ using the top equation, as we can use this in the second equation to solve for v_B :

$$-v_O - \sin \theta \cdot L_{OA} \cdot \omega_{OA} = -\cos \theta \cdot L_{AB} \cdot \omega_{AB} \quad (8)$$

$$-L_{AB} \cdot \omega_{AB} = \frac{-v_O - \sin \theta \cdot L_{OA} \cdot \omega_{OA}}{\cos \theta} \quad (9)$$

Inserting this in the second equation gives us a solution for v_B .

$$\cos \theta \cdot L_{OA} \cdot \omega_{OA} = v_B - \sin \theta \cdot L_{AB} \cdot \omega_{AB} \quad (10)$$

$$\cos \theta \cdot L_{OA} \cdot \omega_{OA} = v_B + \sin \theta \cdot (-L_{AB} \cdot \omega_{AB}) \quad (11)$$

$$\cos \theta \cdot L_{OA} \cdot \omega_{OA} = v_B + \sin \theta \cdot \left(\frac{-v_O - \sin \theta \cdot L_{OA} \cdot \omega_{OA}}{\cos \theta} \right) \quad (12)$$

$$v_B = \cos \theta \cdot L_{OA} \cdot \omega_{OA} - \sin \theta \cdot \left(\frac{-v_O - \sin \theta \cdot L_{OA} \cdot \omega_{OA}}{\cos \theta} \right) \quad (13)$$

$$v_B = \cos \theta \cdot L_{OA} \cdot \omega_{OA} + \sin \theta \cdot \left(\frac{v_O + \sin \theta \cdot L_{OA} \cdot \omega_{OA}}{\cos \theta} \right) \quad (14)$$

$$v_B = \cos \theta \cdot L_{OA} \cdot \omega_{OA} + (v_O + \sin \theta \cdot L_{OA} \cdot \omega_{OA}) \cdot \frac{\sin \theta}{\cos \theta} \quad (15)$$

$$v_B = \cos \theta \cdot L_{OA} \cdot \omega_{OA} + (v_O + \sin \theta \cdot L_{OA} \cdot \omega_{OA}) \cdot \tan \theta \quad (16)$$

Inserting the values for $\theta, L_{OA}, \omega_{OA}, v_O$ gives:

$$v_B = \cos(60^\circ) \cdot 1 \cdot \frac{5}{4} + \left(\frac{3}{2}\sqrt{3} + \sin(60^\circ) \cdot 1 \cdot \frac{5}{4} \right) \cdot \tan(60^\circ) \quad (17)$$

$$v_B = \frac{1}{2} \cdot \frac{5}{4} + \left(\frac{3}{2}\sqrt{3} + \frac{1}{2}\sqrt{3} \cdot \frac{5}{4} \right) \cdot \sqrt{3} = \frac{5}{8} + \frac{9}{2} + \frac{15}{8} = 7 \text{ m/s} \quad (18)$$