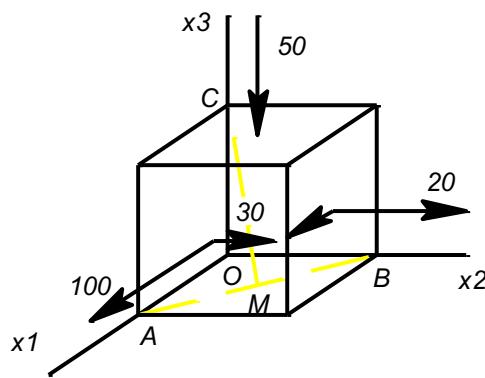


## Exercise V-1

### Problem



Given:

$$E = 200 \text{ GPa} \quad \& \quad \nu = 0.25$$

$$OA = OB = a \quad \& \quad OC = \frac{1}{2}\sqrt{2} \cdot a$$

In this stress-state, the maximal principal stress must not be larger than: 150 MPa.

### Questions:

a)  $\sigma_{ABC}$  &  $\tau_{ABC}$ ,

### Solutions

a)

Stress tensor, from the sketch:  $\sigma = \begin{bmatrix} 100 & 30 & 0 \\ 30 & 20 & 0 \\ 0 & 0 & -50 \end{bmatrix} \text{ MPa}$

Compute the normal to the surface ABC: for example by using the cross-product of two vectors inside this plane.

$$A\vec{C} \times A\vec{B} = \begin{pmatrix} -a \\ 0 \\ \frac{a}{\sqrt{2}} \end{pmatrix} \times \begin{pmatrix} -a \\ a \\ 0 \end{pmatrix} = \frac{-a^2}{\sqrt{2}} \begin{pmatrix} 1 \\ 1 \\ \sqrt{2} \end{pmatrix} = \alpha \begin{pmatrix} 1 \\ 1 \\ \sqrt{2} \end{pmatrix}$$

Normalisation:  $\hat{n}_1^2 + \hat{n}_2^2 + \hat{n}_3^2 = 1$ :  $\alpha^2(1^2 + 1^2 + (\sqrt{2})^2) = 1 \Rightarrow \alpha = \frac{1}{2}$

### Comment

After using the cross-product, with vectors in arbitrary order, one must check/confirm that the normal points out of the plane, away from the cube-backside point O, where the material still exists. The normal should point away from the material. Then choosing  $\alpha$  (in this case) positive, one gets the normal in the right direction; the other solution to normalisation is not valid here.

The stress-vector on surface ABC:  $p_i = \sigma_{ji} \cdot n_j$

$$\rightarrow \begin{bmatrix} p_1 \\ p_2 \\ p_3 \end{bmatrix} = [\sigma] \cdot \begin{bmatrix} \hat{n}_1 \\ \hat{n}_2 \\ \hat{n}_3 \end{bmatrix} = \begin{bmatrix} 100 & 30 & 0 \\ 30 & 20 & 0 \\ 0 & 0 & -50 \end{bmatrix} \cdot \frac{1}{2} \begin{pmatrix} 1 \\ 1 \\ \sqrt{2} \end{pmatrix} = \begin{bmatrix} 65 \\ 25 \\ -25\sqrt{2} \end{bmatrix}$$

Normal-stress:  $\sigma = p^{(n)}$  on ABC:  $\{\sigma\} = \{\hat{n}\}^T \cdot \{p\} = 20 \text{ MPa}$

Shear-stress  $\tau$  on ABC (Pythagoras):

$$\tau^2 = \|\{p\}\|^2 - \sigma^2 = [p_1^2 + p_2^2 + p_3^2] - \sigma^2 = 6100 - 400 = 5700 \text{ MPa} \Rightarrow \tau = 75,5 \text{ MPa}$$

## Exercise V-4

### Problem

Given:

$$E = 2.10^{11} \text{ GPa} \quad \& \quad \nu = 0.25$$

Stress-state in point P:  $\sigma = \begin{bmatrix} 19 & -5 & -\sqrt{6} \\ -5 & 19 & -\sqrt{6} \\ -\sqrt{6} & -\sqrt{6} & 10 \end{bmatrix} \text{ MPa}$

### Questions:

- A) Show that the principal stresses are 8, 16 and 24 MPa. Compute the directional cosines (transformation matrix entries) of the smallest eigen-stress.
- B) Compute the volumetric (isotropic) strain.
- C) What is the largest angle-change (not shear-strain) in P?
- D) Which material property is implicitly used in Hooke's law?

### Solutions

A)

$$\det([\sigma] - \sigma[I]) = \det \begin{bmatrix} \sigma_{11} - \sigma & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \sigma & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - \sigma \end{bmatrix} = 0$$

→ characteristic equation:  $\sigma^3 - 48\sigma^2 + 704\sigma - 3072 = 0 = 0$

From this follow the principal stresses (one can insert them and show that the characteristic equation gets zero for everyone; or one can factorize the equation; or one computes the invariants from the eigen-values and identifies them with the equation):

$$\sigma_1 = 24 \text{ MPa}$$

$$\sigma_2 = 16 \text{ MPa}$$

$$\sigma_3 = 8 \text{ MPa}$$

For the smallest principal stress, compute the eigen-direction:

$$\begin{bmatrix} \sigma_{11} - 8 & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - 8 & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - 8 \end{bmatrix} \cdot \begin{Bmatrix} \hat{n}_1^3 \\ \hat{n}_2^3 \\ \hat{n}_3^3 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \\ 0 \end{Bmatrix}$$

Solving this equation system, for example, yields:

$$\begin{Bmatrix} \hat{n}_1^3 \\ \hat{n}_2^3 \\ \hat{n}_3^3 \end{Bmatrix} = \begin{Bmatrix} 1 \\ 1 \\ \sqrt{6} \end{Bmatrix}$$

which still must be normalized →

$$(\hat{n}_1^3)^2 + (\hat{n}_2^3)^2 + (\hat{n}_3^3)^2 = 1 \quad \Rightarrow \quad (\hat{n}_1^3)^2 = \frac{1}{8} \quad \Rightarrow \quad \hat{n}_1^3 = \frac{\sqrt{2}}{4}$$

which gives the eigen-direction:

$$\begin{Bmatrix} \hat{n}_1^3 \\ \hat{n}_2^3 \\ \hat{n}_3^3 \end{Bmatrix} = \begin{Bmatrix} \frac{1}{4}\sqrt{2} \\ \frac{1}{4}\sqrt{2} \\ \frac{1}{2}\sqrt{3} \end{Bmatrix}$$

which actually are the directional cosines (three entries  $R_{3i}$ ).

B)

$$\text{For the volumetric strain we get: } \varepsilon_V = \varepsilon_1 + \varepsilon_2 + \varepsilon_3 = \left[ \frac{1-2\nu}{E} \right] \cdot \sigma_{kk} = 12 \cdot 10^{-5}$$

C)

$$\text{The largest change of angle is: } \gamma_{\max} = \frac{\tau_{\max}}{G} = \frac{\frac{1}{2}(\sigma_1 - \sigma_3)}{G} = 1 \cdot 10^{-4},$$

where the largest shear strain is just half of that.

D)

Isotropy is intrinsic to using the law of Hooke.

### Solutions of V-12

a) Given was the stress-field in absence of body forces  $f_i = 0$ :

$$\begin{aligned}\sigma_{11}(x_1, x_2) &= \sigma_0 \left[ 20 + \alpha_1 \cdot \frac{x_1}{L} - 10 \cdot \frac{x_2}{L} + \alpha_2 \cdot \left( \frac{x_1}{L} \right)^2 \right] \\ \sigma_{22}(x_1, x_2) &= \sigma_0 \left[ 10 + 8 \cdot \frac{x_1}{L} + \beta_1 \cdot \frac{x_2}{L} + \beta_2 \cdot \left( \frac{x_2}{L} \right)^2 \right] \\ \sigma_{12}(x_1, x_2) &= \sigma_0 \left[ 12 - 10 \cdot \frac{x_1}{L} + 7 \cdot \frac{x_2}{L} - 8 \cdot \frac{x_1}{L} \cdot \frac{x_2}{L} \right]\end{aligned}$$

Using the stress-equilibrium equations, i.e. derivatives with displacement-directions with respect to the coordinate system, one obtains:

$$\begin{aligned}\frac{d}{dx_1} \sigma_{11}(x_1, x_2) + \frac{d}{dx_2} \sigma_{12}(x_1, x_2) &= \sigma_0 \left[ \frac{\alpha_1}{L} + 2\alpha_2 \cdot \frac{x_1}{L^2} \right] + \sigma_0 \left[ \frac{7}{L} - 8 \cdot \frac{x_1}{L^2} \right] = 0 \\ \frac{d}{dx_1} \sigma_{12}(x_1, x_2) + \frac{d}{dx_2} \sigma_{22}(x_1, x_2) &= \sigma_0 \left[ \frac{-10}{L} - 8 \cdot \frac{x_2}{L^2} \right] + \sigma_0 \left[ \frac{\beta_1}{L} + 2\beta_2 \cdot \frac{x_2}{L^2} \right] = 0\end{aligned}$$

From these equations, one obtains the coefficients that solve them:  $\alpha_1 = -7$ ,  $\alpha_2 = 4$ ,  $\beta_1 = 10$ ,  $\beta_2 = 4$

b) The stress Tensor in point  $P = (x_1 = 0, x_2 = 0, x_3 = 0)$  is:  $\begin{bmatrix} \sigma_{ij} \end{bmatrix} = \begin{bmatrix} 20 & 12 & 0 \\ 12 & 10 & 0 \\ 0 & 0 & 0 \end{bmatrix}$  MPa

Using the stress tensor, the characteristic equation can be computed:

$$\sigma^3 - I_1 \sigma^2 + I_2 \sigma - I_3 = 0$$

and from this, knowing that one eigen-value is zero, i.e.  $I_3 = 0$ , the principal stresses can be computed from a second order polynomial as:  $\sigma_I = 28$  MPa,  $\sigma_{II} = 2$  MPa,  $\sigma_{III} = 0$  MPa. This is a plane-stress state with all stresses on the  $x_3$ -surface being equal to zero.

c) And the principal directions can be calculated the usual way, where  $\hat{n}^{(III)} = (0, 0, 1)$  is directly visible from the tensor, due to zero- shear stresses in the  $x_3$ -direciton, while the others require to insert:

Direction of the major stress  $\sigma_I = 28$  MPa

$$\begin{bmatrix} \sigma_{11} - \sigma_I & \sigma_{12} & \sigma_{13} \\ \sigma_{12} & \sigma_{22} - \sigma_I & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & \sigma_{33} - \sigma_I \end{bmatrix} \begin{bmatrix} n_1^{(I)} \\ n_2^{(I)} \\ n_3^{(I)} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \text{ and normalization: } n_1^{(I)} + n_2^{(I)} + n_3^{(I)} = 1$$

$$-8n_1^{(I)} + 12n_2^{(I)} = 0 \Rightarrow n_1^{(I)} = (3/2)n_2^{(I)} \quad \text{and thus: } [(9/4) + 1]n_2^{(I)} = 1 \rightarrow n_2^{(I)} = 2/\sqrt{13}$$

$$\Rightarrow \begin{bmatrix} n_1^{(I)} \\ n_2^{(I)} \\ n_3^{(I)} \end{bmatrix} = \pm \begin{bmatrix} 3/\sqrt{13} \\ 2/\sqrt{13} \\ 0 \end{bmatrix}$$

Direction of the middle (was not asked, for completeness)  $\sigma_{II} = 2 \text{ MPa}$

$$\begin{bmatrix} \sigma_{11} - \sigma_{II} & \sigma_{12} & \sigma_{13} \\ \sigma_{12} & \sigma_{22} - \sigma_{II} & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & \sigma_{33} - \sigma_{II} \end{bmatrix} \begin{bmatrix} n_1^{(II)} \\ n_2^{(II)} \\ n_3^{(II)} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \text{ and normalization: } n_1^{(II)} + n_2^{(II)} + n_3^{(II)} = 1$$

$$18n_1^{(II)} + 12n_2^{(II)} = 0 \rightarrow n_1^{(II)} = -(2/3)n_2^{(II)} \quad \text{and thus: } [(4/9) + 1]n_2^{(II)} = 1 \rightarrow n_2^{(II)} = 3/\sqrt{13}$$

$$\Rightarrow \begin{bmatrix} n_1^{(II)} \\ n_2^{(II)} \\ n_3^{(II)} \end{bmatrix} = \pm \begin{bmatrix} -2/\sqrt{13} \\ 3/\sqrt{13} \\ 0 \end{bmatrix}$$

