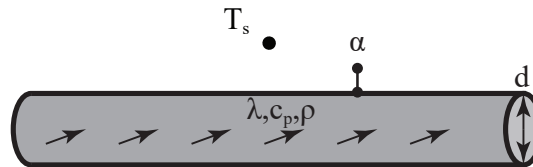


Exercise II.13: (Cooling of a copper rod ★★)

A long copper rod is initially at a uniform temperature T_0 . It is now exposed to an air stream at T_∞ with a heat transfer coefficient α .

**Given parameters:**

- | | |
|-------------------------------------|--|
| • Diameter of the copper rod: | $d = 2 \text{ cm}$ |
| • Initial temperature: | $T_0 = 100 \text{ }^\circ\text{C}$ |
| • Air stream temperature: | $T_\infty = 20 \text{ }^\circ\text{C}$ |
| • Heat transfer coefficient: | $\alpha = 200 \text{ W/m}^2\text{K}$ |
| • Thermal conductivity of copper: | $\lambda = 399 \text{ W/mK}$ |
| • Specific heat capacity of copper: | $c_p = 382 \text{ J/kgK}$ |
| • Density of copper: | $\rho = 8930 \text{ kg/m}^3$ |

Hints:

- Heat radiation can be neglected.
- Setup an energy balance.

Tasks:

- a) Determine how long will it take for the copper rod to cool to a temperature of $T_1 = 25 \text{ }^\circ\text{C}$.
- b) Sketch the temperature profile over the course of time.

Solution II.13: (Cooling of a copper rod ★★)**Task a)**

The temperature profile within the solid body is derived from the conduction equation, considering both spatial and temporal aspects.

In practical scenarios, the temperature profile within the rod is never homogeneous. However, the Biot number is a useful parameter for assessing whether the temperature distribution within the rod can be approximated as homogeneous. If the Biot number allows for such an assumption, the lumped capacity model becomes a viable approach to solving the problem.

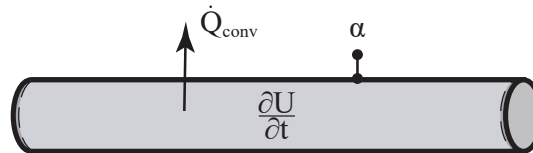
The Biot number is determined by:

$$\begin{aligned} \text{Bi} &= \frac{\alpha V}{\lambda A_s} = \frac{\alpha \cdot d}{4\lambda} = \\ &= \frac{200 \left(\frac{\text{W}}{\text{m}^2\text{K}} \right) \cdot 0.02 \text{ (m)}}{4 \cdot 399 \left(\frac{\text{W}}{\text{mK}} \right)} = 0.025 \text{ (-)}. \end{aligned} \quad (\text{II.13.1})$$

Thus $\text{Bi} \ll 1$, which implies that spatial temperature differences within the copper rod are negligible.

1 Setting up the balance:

Given the significantly low Biot number, temperature variations within the copper rod's body are deemed negligible. Consequently, a global energy balance encompassing the entire rod can be established. Over time, convective losses induce changes in the internal energy of the rod, leading to the rod cooling.



The copper rod is losing heat by convection and therefore the energy balance reads:

$$\underbrace{\frac{\partial U}{\partial t}}_{\text{Temporal change of inner energy}} = - \underbrace{\dot{Q}_{\text{conv}}}_{\text{Convective losses}} \quad (\text{II.13.2})$$

2 Defining the elements within the balance:

The temporal change of internal energy is expressed as:

$$\begin{aligned} \frac{\partial U}{\partial t} &= m c_p \frac{\partial T}{\partial t} \\ &= \rho \frac{\pi d^2}{4} L c_p \cdot \frac{\partial T}{\partial t}, \end{aligned} \quad (\text{II.13.3})$$

and the rate of heat loss by convection

$$\begin{aligned}\dot{Q}_{\text{conv}} &= \alpha A_s \cdot (T(t) - T_\infty) \\ &= \alpha \pi d \cdot L \cdot (T(t) - T_\infty).\end{aligned}\quad (\text{II.13.4})$$

3 Inserting and rearranging:

$$\frac{\partial T}{\partial t} = \frac{4\alpha}{dc_p} \cdot (T(t) - T_\infty). \quad (\text{II.13.5})$$

4 Defining the boundary and/or initial conditions:

To solve the equation, one initial condition must be given. This is described in terms of the initial temperature of the copper rod, which is:

$$T(t = 0) = T_0. \quad (\text{II.13.6})$$

5 Solving the equation:

Before solving, first both sides are multiplied with $\frac{1}{T_\infty - T_0}$:

$$\rho \frac{\pi d^2}{4} L c_p \cdot \frac{1}{T_\infty - T_0} \cdot \frac{\partial T}{\partial t} = -\alpha \pi d \cdot L \cdot \frac{T(t) - T_\infty}{T_\infty - T_0}. \quad (\text{II.13.7})$$

To solve the equation, a dimensionless temporal temperature difference is introduced, which is:

$$\Theta^* = \frac{T(t) - T_0}{T_\infty - T_0}. \quad (\text{II.13.8})$$

Substitution of this parameter and rewriting:

$$\frac{1}{\Theta^* - 1} \frac{\partial \Theta^*}{\partial t} = -\frac{4\alpha}{\rho d c_p}. \quad (\text{II.13.9})$$

Integration gives:

$$\begin{aligned}\ln |\Theta^* - 1| &= -\frac{4\alpha}{\rho d c_p} t + A^* \\ \Rightarrow \Theta^* &= A \cdot \exp\left(-\frac{4\alpha}{\rho d c_p} t\right) + 1.\end{aligned}\quad (\text{II.13.10})$$

To find constant A , the initial condition that has been defined before needs to be used. To do so, the condition must be written in a dimensionless form:

$$\Theta^*(t = 0) = \frac{T_0 - T_0}{T_\infty - T_0} = 0. \quad (\text{II.13.11})$$

Substitution:

$$\begin{aligned}\Theta^*(t = 0) &= A \cdot \exp(0) + 1 = 0 \\ \Rightarrow A &= -1.\end{aligned}\quad (\text{II.13.12})$$

Which yields the function of the dimensionless temporal temperature profile:

$$\Theta^*(t) = -\exp\left(-\frac{4\alpha}{\rho dc_p}t\right) + 1. \quad (\text{II.13.13})$$

At $t = t_1$, the temperature of the rod is equal to $T_1 = 25^\circ\text{C}$. Thus:

$$\begin{aligned} \Theta^*(t = t_1) &= -\exp\left(-\frac{4\alpha}{\rho dc_p}t_1\right) + 1 = \frac{T_1 - T_0}{T_\infty - T_0} \\ \Rightarrow t_1 &= -\ln\left(1 - \frac{T_1 - T_0}{T_\infty - T_0}\right) \frac{\rho dc_p}{4\alpha} \\ &= -\ln\left(1 - \frac{(25 - 100)^\circ\text{C}}{(20 - 100)^\circ\text{C}}\right) \frac{8930 \left(\frac{\text{kg}}{\text{m}^3}\right) \cdot 0.02 \text{ (m)} \cdot 382 \left(\frac{\text{J}}{\text{kgK}}\right)}{4 \cdot 200 \left(\frac{\text{W}}{\text{m}^2\text{K}}\right)} = 236 \text{ (s)}. \end{aligned} \quad (\text{II.13.14})$$

Conclusion

For the copper rod to cool down from 100°C to 25°C takes about 4 min.

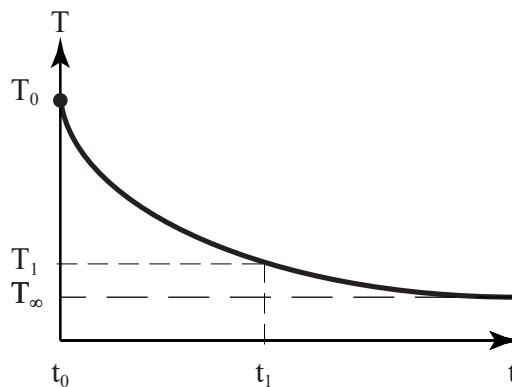
Task b)

Recall Newton's law of cooling:

$$\dot{Q} = \alpha A (T(t) - T_\infty), \quad (\text{II.13.15})$$

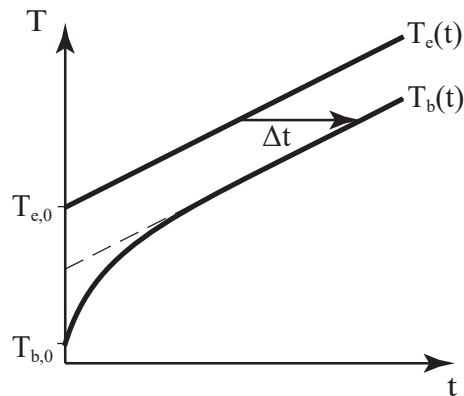
which tells that as the rod cools down, the temperature difference between the body and the ambient will decrease. With this reduction in temperature difference, the rate of heat transfer will also decrease. Consequently, the temperature gradient will decrease until the body temperature matches the ambient temperature, resulting in no further cooling. At this point, a horizontal slope in the temperature profile is observed.

Conclusion



Exercise II.14: (The temperature delay ★★)

A body with a temperature of T_b is located within an environment with the linearly rising temperature T_e and heats up accordingly to the diagram below. As $t \rightarrow \infty$, the temperature of the body follows that of the environment with a constant time delay Δt .

**Given parameters:**

- Heat transfer coefficient of the body: α
- Surface of the body: A
- Mass of the body: m
- Heat capacity of the body: c_p
- Temperature of the environment: $T_e(t)$

Hints:

- The temperature is uniform within the body
- The environment, and its temperature, are not affected by the body.
- Heat radiation can be neglected.
- Setup an energy balance.

Tasks:

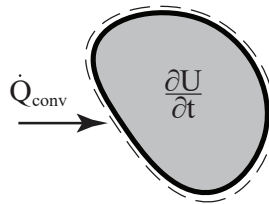
- a) Determine this delay Δt .

Solution II.14: (The temperature delay ★★)**Task a)**

To determine the temperature delay Δt , an energy balance at time instance $t \rightarrow \infty$ must be set.

1 Setting up the balance:

Given that temperature is uniform within the body, temperature variations are negligible. Consequently, a global energy balance encompassing the entire body is established. Over time, convective transport induces changes in the internal energy, heating the body.



The transient energy balance around the body at time instance $t \rightarrow \infty$ reads:

$$\underbrace{\frac{\partial U}{\partial t}}_{\text{Temporal change of inner energy}} = \underbrace{\dot{Q}_{\text{conv}}}_{\text{Convective transport}} \quad (\text{II.14.1})$$

2 Defining the elements within the balance:

Since the temperature is uniform within the body, the change of internal energy over time is expressed as:

$$\frac{\partial U}{\partial t} = mc_p \frac{\partial T}{\partial t}. \quad (\text{II.14.2})$$

Because the energy balance is set at $t \rightarrow \infty$, the temperature increases linearly, and thus within a time instant Δt , the temperature increases by the difference between the body and ambient temperature $\Delta T = (T_e(t \rightarrow \infty) - T_b(t \rightarrow \infty))$. Thus:

$$\frac{\partial T}{\partial t} = \frac{\Delta T}{\Delta t}. \quad (\text{II.14.3})$$

Lastly, the heat transfer rate by convection from the environment to the body is written as,

$$\begin{aligned} \dot{Q}_{\text{conv}} &= \alpha A_s (T_e(t \rightarrow \infty) - T_b(t \rightarrow \infty)) \\ &= \alpha A_s \Delta T. \end{aligned} \quad (\text{II.14.4})$$

3 Inserting and rearranging:

$$\Delta t = \frac{mc_p}{\alpha A_s}. \quad (\text{II.14.5})$$