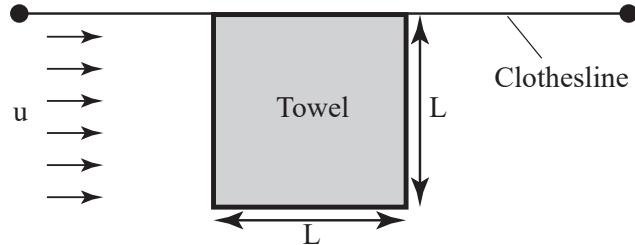


**Exercise V.2:** (Soaked towel ★★)

A square towel (edge length  $L$ ) soaked with water is hung up on a clothesline. The wind is blowing against the towel from the side with a velocity of  $u$ . The air and the towel have the same temperature  $T$  that remains constant over time.



**Given parameters:**

- Temperature of towel and air:  $T = 20 \text{ } ^\circ\text{C}$
- Velocity of the wind:  $u = 1 \text{ m/s}$
- Edge length of the towel:  $L = 0.5 \text{ m}$

**Hints:**

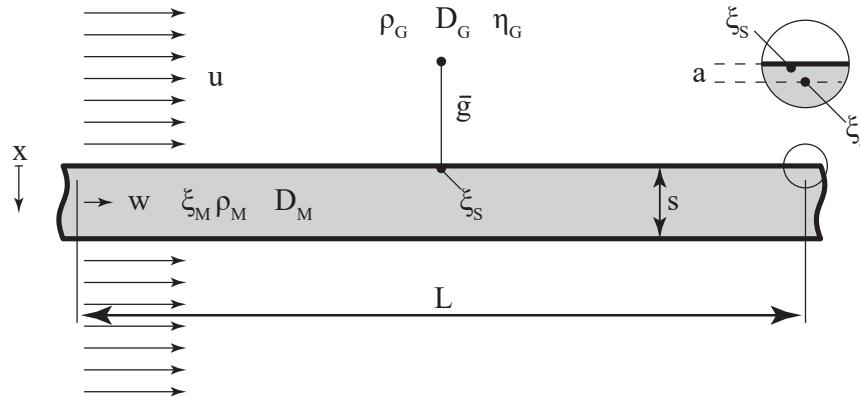
- The influence of radiation on the problem is to be neglected.
- The Lewis relation is valid.

**Tasks:**

- a) Calculate the average mass transfer coefficient  $\bar{g}$ .

**Exercise V.3:** (Metal strap ★★★)

A metal strap (M) with a sheet-thickness  $s$  is pulled at a velocity  $w$  through an oven of length  $L$ . Thereby a CO<sub>2</sub>-containing gas atmosphere (G) flows over the strap with a velocity  $u$ . On entering the furnace, the metal strap has a homogeneous fraction of carbon  $\xi_M$ . Under quasi-steady conditions, a constant fraction of carbon  $\xi_S$  exists just below the surface of the metal strip, while carbon constantly diffuses into its interior.

**Given parameters:**

- Diffusion coefficient of carbon in metal:  $D_M = 5 \cdot 10^{-10} \text{ m}^2/\text{s}$
- Diffusion coefficient of carbon in gas:  $D_G = 1 \cdot 10^{-4} \text{ m}^2/\text{s}$
- Combined density of metal:  $\rho_M = 8 \cdot 10^3 \text{ kg/m}^3$
- Combined density of the gases:  $\rho_G = 0.8 \text{ kg/m}^3$
- Combined viscosity of the gases:  $\eta_G = 5.6 \cdot 10^{-5} \text{ Pa} \cdot \text{s}$
- Flow velocity:  $u = 10 \text{ m/s}$
- Sheet velocity:  $w = 2 \cdot 10^{-2} \text{ m/s}$
- Initial carbon fraction:  $\xi_M = 0.2 \cdot 10^{-4}$
- Surface carbon fraction:  $\xi_S = 1 \cdot 10^{-4}$
- Oven length:  $L = 10 \text{ m}$
- Strap thickness:  $s = 50 \cdot 10^{-3} \text{ m}$
- Layer depth:  $a = 0.2 \cdot 10^{-3} \text{ m}$

**Hints:**

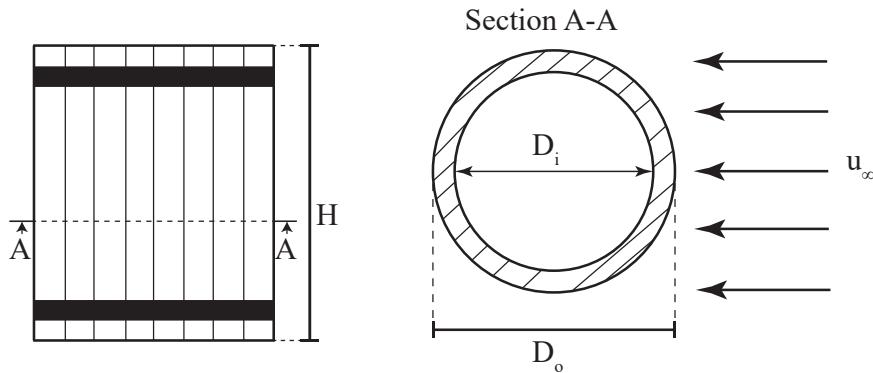
- Use a co-moving coordinate system.
- Neglect diffusion in the direction of the sheet.
- The strap thickness is significantly greater than twice the depth of penetration of the carbon.

**Tasks:**

- a) Calculate the mean mass transfer coefficient  $\bar{g}$  on the strip's surface. Show that the assumption of a constant carbon content of  $\xi_s$  just below the surface is valid.
- b) Provide the differential equation for the carbon transport in the strap as well as the appropriate initial and boundary conditions. For this, provide a suitable equation for the carbon content in the strap  $\xi(x,t)$ .
- c) Calculate the carbon content of  $\xi_a$  which is established at the end of the furnace at a depth  $a$  from the strap's surface. Show that the assumption of a low penetration depth is justified.

**Exercise V.4:** (Whiskey barrel ★★)

Deep in the cellars of a distillery, Whisky is stored in wooden barrels for its maturation. The whisky is composed of an ethanol-water mixture with an ethanol mass fraction  $\xi_{EW,t0}$  at the initial time  $t_0$  (at the beginning of the storage period). The ventilation system of the cellar provides a continuous flow of fresh air (free of ethanol,  $\xi_{EA,\infty} = 0$ ) to the barrels. During the storage period, the concentration of ethanol in the Whisky falls due to mass transport processes down to a value of  $\xi_{EW,t1}$  (time  $t_1$ , is the end of the storage).



**Hint:** Use the following nomenclature for the indexes:

- $\xi_{EW}$  : Ethanol mass fraction in Whisky
- $\xi_{EW,i}$  : Ethanol mass fraction in Wood, inner side of the barrel
- $\xi_{EW,o}$  : Ethanol mass fraction in Wood, outer surface of the barrel
- $\xi_{EA,o}$  : Ethanol mass fraction in air, at the outer surface of the barrel
- $\xi_{EA,\infty}$  : Ethanol mass fraction in air, at the free flow

**Given parameters:**

- Initial time of the barrel storage:  $t_0$
- End time of the barrel storage:  $t_1$
- Length of the storage time:  $\Delta t = 3 \text{ years}$
- Constant:  $Z = 4.34 \cdot 10^{-7} \text{ kg/s}$
- Outer diameter:  $D_o = 0.56 \text{ m}$
- Inner diameter:  $D_i = 0.50 \text{ m}$
- Height:  $H = 0.9 \text{ m}$
- Density of the wood:  $\rho_{Wo} = 500 \text{ kg/m}^3$
- Diffusion coefficient of ethanol in wood:  $D_{EWo} = 1 \cdot 10^{-11} \text{ m}^2/\text{s}$
- Density of the whisky:  $\rho_W = 870 \text{ kg/m}^3$
- Dynamic viscosity of the whisky:  $\eta_W = 1 \cdot 10^{-3} \text{ Pa} \cdot \text{s}$
- Mass fraction of ethanol at initial time  $t_0$ :  $\xi_{EW,t0} = 0.54$
- Flow velocity:  $u_\infty = 0.1 \text{ m/s}$

- Density of the air:  $\rho_A = 1.18 \text{ kg/m}^3$
- Diffusion coefficient of ethanol in air:  $D_{EA} = 1.47 \cdot 10^{-5} \text{ m}^2/\text{s}$
- Dynamic viscosity of the air:  $\eta_A = 1.81 \cdot 10^{-5} \text{ Pa} \cdot \text{s}$

**Hints:**

- Due to the high relative humidity in the cellar, Whisky only loses ethanol.
- There is no mass transport resistance at the inner surface of the barrel.
- Ignore the Stefan flow.
- The overall density of the Whisky, the wood and the air do **not** change due to mass transport processes.
- The Whisky barrels are cylindrical and ethanol diffuses **only** through the lateral surfaces, neglecting the effect of the metal rings around the barrel.
- The Whisky is ideally mixed inside the barrel.
- All given material properties are constant.
- Jumps in concentrations are only due to density differences.

**Tasks:**

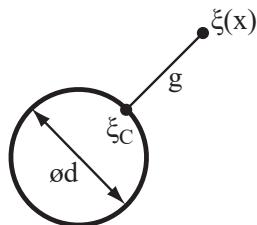
**Hint:** For the sub-problems a) to c) the system is in a (quasi-) stationary state and the concentration  $\xi_{EW}$  is known at each point in time

- a) Sketch (qualitatively) the radial concentration profile of ethanol  $\xi_{EW}$  in the Whisky at any time  $t$  within the time interval  $t_0 < t < t_1$ .
- b) Determine an expression for the ethanol mass flow rate taking place due to mass diffusion through the wood barrel ( $\dot{m}_D$ ) and another for the mass flow produced by the convection process ( $\dot{m}_K$ ) occurring at the external surface of the barrel. Additionally, calculate the mass transfer coefficient  $g$ . To do this use the known ethanol concentrations at the interfaces.
- c) Determine the unknown ethanol concentrations  $\xi_{EW,i}$ ,  $\xi_{EW,o}$ ,  $\xi_{EA,o}$  and  $\xi_{EA,\infty}$ , and give an expression for the ethanol mass flow rate  $\dot{m}_E$ .
- d) By means of an instationary mass balance upon the whisky, calculate the ethanol concentration  $\xi_{EW,t1}$  in the barrel, which is attained after a storage time of  $\Delta t = 3$  years in the barrel. Use the simplified expression of the ethanol mass flow given by  $\dot{m}_E = Z \cdot \xi_{EW}$  with  $Z = 4.34 \cdot 10^{-7} \frac{\text{kg}}{\text{s}}$

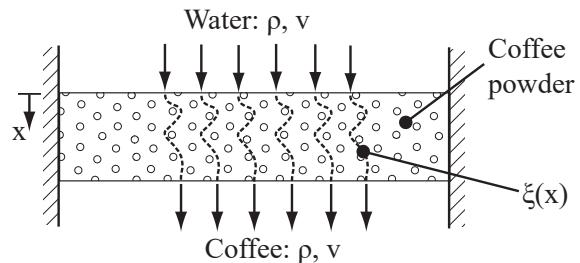
**Exercise V.5:** (Coffee brewing ★★)

Coffee powder consists of many coffee grains, forming a highly concentrated coffee solution during brewing. The flavors come out of the coffee grains ( $\xi_C$ ) through diffusion into the passing water flow ( $\xi(x)$ ). This diffusion process is well described by the mass-transfer coefficient  $g$ .

**a) Idealized coffee grain (sphere)**



**b) Coffee preparation**

**Given parameters:**

- Diffusion coefficient of the flavors in water:  $D$
- Water flow velocity:  $v$
- Total density of flavored water:  $\rho$
- Concentration of highly concentrated coffee solution:  $\xi_C$
- Mass transfer coefficient:  $g$
- Diameter of a coffee grain:  $d$
- Packing density in the coffee powder:  $p$

**Hints:**

- The problem is stationary and the Stefan flow is negligible.
- All coffee grains have the same diameter and are homogeneously distributed in the powder.
- If you cannot solve part a), you may use  $\dot{m}_C''' = \frac{g}{d} \cdot (\xi_C - \xi(x))$ .

**Tasks:**

- a) Determine the mass flow out of the grains per unit volume  $\dot{m}_C'''$ , which is transferred from the coffee grains to the passing water flow.
- b) Derive the differential equation for the mass concentration of flavors  $\xi(x)$  in the passing water flow. Consider the packing density  $p$  of the coffee grains within the ground coffee powder in the source term:  $\dot{m}_C''' = p \cdot \dot{m}_C'''$ .
- c) Write down the required differential equation and the boundary conditions, when diffusion is negligible in the flow direction, and determine the concentration profile of  $\xi(x)$  for this case.
- d) Draw the concentration profiles  $\xi(x)$  for two different grain diameters  $d_1 < d_2$  over the length of the ground coffee powder in the given chart and mark the curves clearly.