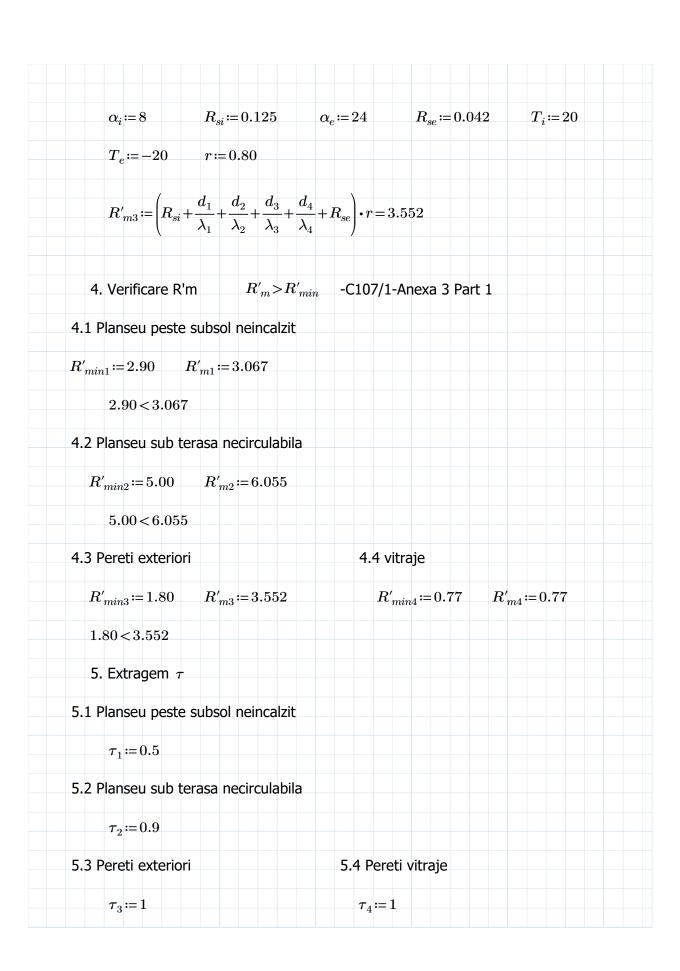
	1.Calculul ariilor elementelor anvelopei incalzite
	1.1 Planseu sub terasa necirculabila
	$A_{pspn}\coloneqq 119.07$ $m{m}^2$
	1.2 Planseu peste subsol neincalzit
	$A_{ppsn}\coloneqq 119.07 extbf{ extit{m}}^2$
	1.3 Pereti exteriori
	Aria totala
1	$_{oetot} := (3 + 5.8 + 1.5 + 2 + 5.3 + 20.175 + 3.6 + 4.9 + 6.1 + 5.475) \cdot (2.72 \cdot 2) = 314.704$ m^2
	Aria vitraje
	etaj:
a	$_{jeetaj} \coloneqq 1.5 \cdot 1.3 + 1.5 \cdot 1.3 + 1.5 \cdot 1.3 + 3 \cdot 1.3 + 3 \cdot 1.3 + 2 \cdot 1.3 + 1.5 \cdot 1.3 + 0.9 \cdot 1.3 + 1.5 \cdot 1.3 = 2.3 \cdot 1.3 + 1.3 \cdot 1.3 + 1.3 \cdot 1.3 = 2.3 \cdot 1.3 + 1.3 \cdot 1.3 + 1.3 \cdot 1.3 = 2.3 \cdot 1.3 + 1.3 \cdot 1.3 $
	parter:
	$A_1 \coloneqq 3 \cdot 1.3 + 2 \cdot 1.3 + 2.5 \cdot 0.6 + 2 \cdot 2.13 + 0.9 \cdot 1.3 + 1.6 \cdot 2.13 = 16.838$
	$A_2 \!\coloneqq\! 3 \cdot 1.3 + 1.5 \cdot 1.3 + 1.7 \cdot 2.13 + 1.15 \cdot 2.2 + 2.905 \cdot 2.13 = 18.189$
ı	$_{nitrajeparter} := A_1 + A_2 = 35.027$
	$A_{vitraje} \coloneqq A_{vitrajeetaj} + A_{vitrajeparter} = 56.347$ $m{m}^2$
	Aria pereti exteriori opaca $A_{peopaca} \coloneqq A_{petot} - A_{vitraje} = 258.357$ m^2
	Calculul volumului spatiului incalzit
	$V_{s.i.} := A_{ppsn} \cdot (2 \cdot 3 + 4 \cdot 0.7) = 1.048 \cdot 10^3$

	Ilul rezistentelor termice				
3.	1. Planseu peste subsol nei	ncalzit			
Strat	ificatie:				
	Parchet laminat	$d_1 \coloneqq 0.02$		\ 0.22	W
	1. Parchet lanning	$a_1 = 0.02$	m	$\lambda_1 = 0.23$	$\overline{m \cdot K}$
	2. Sapa egalizare mortar	$d_2 = 0.04$	m	$\lambda_2 \coloneqq 0.93$	$rac{W}{m \cdot K}$
		W2 0.01		7.2	$m \cdot K$
	3.Polistiren expandat	$d_3 = 0.13$	m	$\lambda_3 = 0.036$	<u>W</u>
					$m \cdot K$
	4.Placa b.a.	$d_4 = 0.13$	m	$\lambda_4 \coloneqq 1.74$	$\frac{W}{m}$
	5. Tencuiala interioara	$d_5\!\coloneqq\!0.02$	m	$\lambda_5 \coloneqq 0.87$	$\frac{W}{m \cdot K}$
					770 22
α_i :=0	$R_{si} = 0.167$	$\alpha_e \coloneqq 12$	$R_{se} = 0.08$	$T_i = 2$	20
T_e :=	$-20 \qquad r := 0.75$				
R'_{m1}	$\coloneqq \left(R_{si} + \frac{d_1}{\lambda_1} + \frac{d_2}{\lambda_2} + \frac{d_3}{\lambda_3} + \frac{d_4}{\lambda_4}\right)$	$+\frac{d_5}{\lambda} + R_{se}$ $\cdot r =$	3.067		
		75 /			
3.	2. Planseu sub terasa neciro	culabila			
	Stratificatie:				
	1. Tencuiala interioara	$d_1 = 0.02$	m	$\lambda_1 = 0.8$	7 <u>W</u>
	I i i i i i i i i i i i i i i i i i i i	ω ₁ σ.σ.	.,,	710.0	$m \cdot K$
	2.Placa b.a	$d_2 = 0.13$	m	$\lambda_2 \coloneqq 1.74$	4 <u>W</u>
					$m \cdot K$
	3. Strat difuzie-folie de polietilena	$d_3 = 0.02$	m	$\lambda_3 = 0.02$	$\frac{W}{m \cdot K}$

5	. Beton de panta $d_{artheta}$	$_{5} \coloneqq 0.04$ m	λ_5 := 1	1.64 $\frac{W}{m \cdot I}$	<u></u>
		0.04			
o	. Sapa egalizare din mortar $d_{ m e}$	$_{3}\coloneqq0.04$ m	$\lambda_6 = 0$	$0.93 \frac{W}{m \cdot l}$	K
7	. Hidroizolatie-folie PVC $d_{ au}$	$_{7} \coloneqq 0.02$ m	$\lambda_7 := 0$	$0.40 \frac{W}{m \cdot I}$	
8	.Protectie hidroizolatie-nisip d_8	$_{3} \coloneqq 0.01$ m	$\lambda_8 \coloneqq 0$	$0.58 \frac{W}{m \cdot I}$	K
$\alpha_i \coloneqq$	$R_{si} = 0.125$ α_c	$_{e}\coloneqq 12$ R_{se}	e := 0.084	$T_i = 20$	
T_e :=	r = 0.85				
	(d. d. d. d.	d. d. d.	d. \		
R'_{m2}	$\coloneqq \left(R_{si} + \frac{d_1}{\lambda_1} + \frac{d_2}{\lambda_2} + \frac{d_3}{\lambda_3} + \frac{d_4}{\lambda_4} + \cdots\right)$	$\frac{\alpha_5}{\lambda_5} + \frac{\alpha_6}{\lambda_6} + \frac{\alpha_7}{\lambda_7} + \cdots$	$\left.rac{a_8}{\lambda_8}\!+\!R_{se} ight]\!\!\cdot\! r$	=6.055	
3.3. Per	rete exterior				
Si	tratificatie:				
	1. Tencuiala interioara	$d_1 \coloneqq 0.02$	m	$\lambda_1 \coloneqq 0.87$	$\frac{W}{m}$
	2. Perete caramida	$d_2 = 0.30$	m	$\lambda_2 \coloneqq 0.207$	$\frac{W}{m}$
	3.Polistiren expandat	$d_3 = 0.10$	m	$\lambda_3 = 0.036$	и
	5.1 olistileti expandat	<i>a</i> ₃ :=0.10	116	A ₃ .= 0.030	\overline{m}
	4. Tencuiala exterioara	$d_4\!\coloneqq\!0.02$	m	$\lambda_4 \coloneqq 0.87$	$\frac{W}{m}$
					111.



6 0.6					
6. $n = 0.6$		2			
Element	Arie m^2	R'm $\frac{m^2 \cdot K}{W}$	L=A/R'm	au	Lx au
Planseu peste subsol neincalzit	119.07	3.067	38.82229	0.5	19.41114
lanseu sub terasa ecirculabila	119.07	6.055	19.66473	0.9	17.69825
Pereti exteriori opaca	258.357	3.552	72.73564	1	72.73564
Vitraje	56.347	0.77	73.17792	1	73.17792
$\Sigma L \tau \coloneqq 19.41$	114 + 17.69825	6 + 72.73564 + 73	.17792 = 183.02	23	
$V \coloneqq 119.07 \cdot ($	(3+3+0.13) =	729.899	$m{m}^3$ -volun	nul spatiı	ului incalzit
$G \coloneqq \frac{\Sigma L \tau}{V} + r$	$n \cdot 0.34 = 0.455$				
$A_{tot} \coloneqq 119.07$	7+119.07+258	8.357 + 56.347 =	552.844		
$\frac{A_{tot}}{V} = 0.7$	=> (0.794>0.75 =>	→ GN=0.54		
G = 0.455	<u>, </u>				
		G < GN			