

# Required Instrumentation Information for Interferometrists and Radio Astronomers

Rhodes University RATT Group Introduction Lectures 2014

# Any measurement is a loss in information

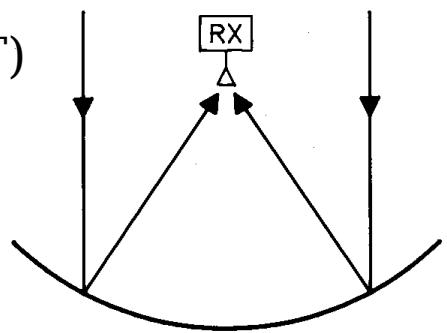
From the sky we can measure infinite frequency bandwidth, frequency resolution, time resolution, across a  $4\pi$  area of the sky.

In reality, our instruments have limits on all these, so we must be selective about which information we retain based on the science goals and engineering limitations.

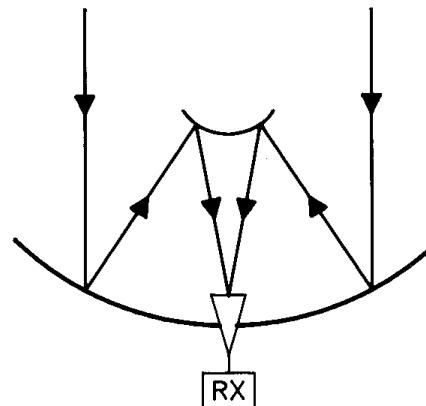
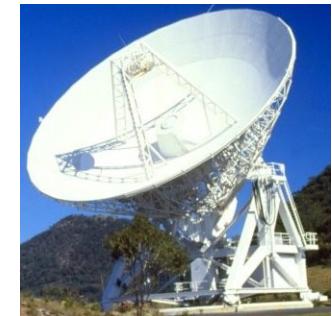
# Primary Beams

## focusing light

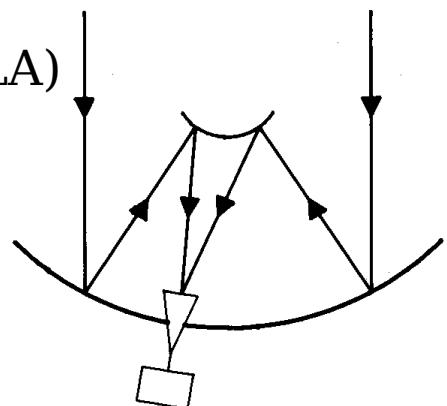
Prime Focus (GMRT)



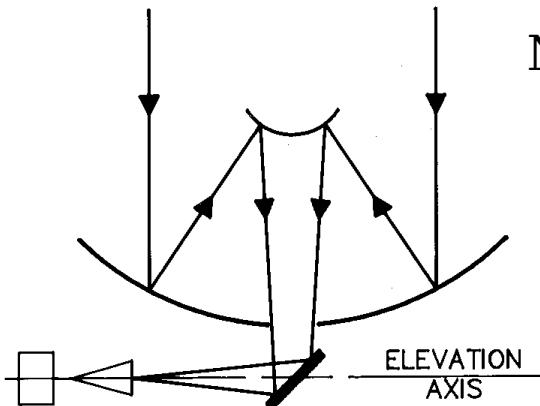
Cassegrain (ATCA)



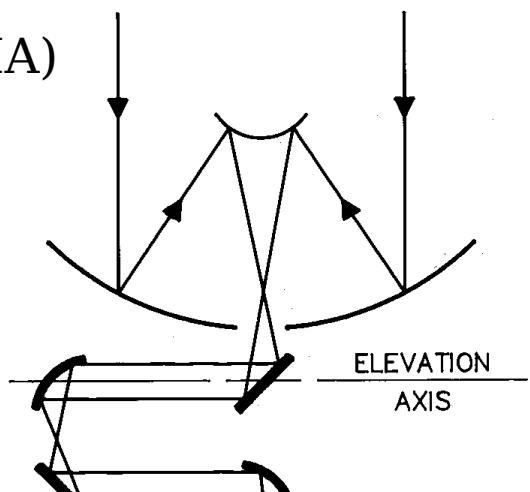
Offset Cassegrain (VLA)



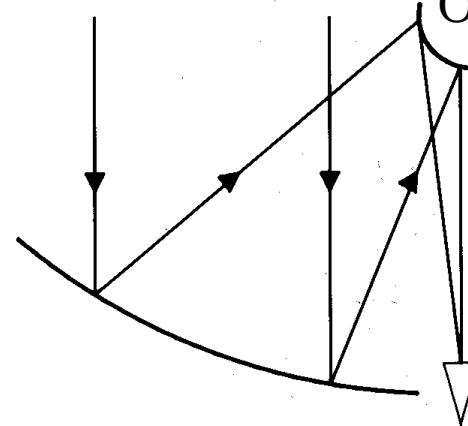
Nasmyth (CARMA)



Bent Nasmyth (SMA)

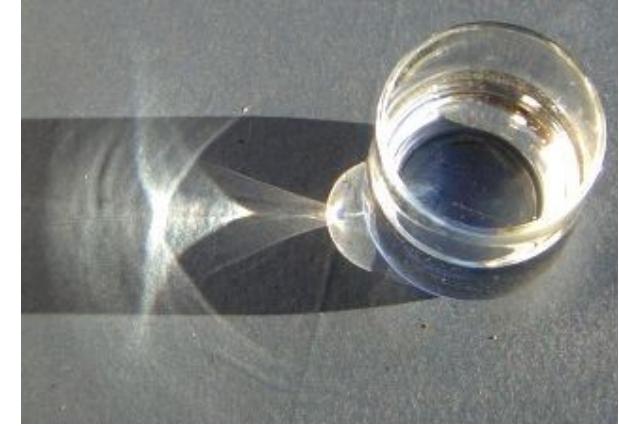


Offset Gregorian (GBT)



$\eta$  : 'aperture' efficiency

$$\eta = \eta_{\text{surface}} \eta_{\text{blockage}} \eta_{\text{spillover}} \eta_{\text{taper}} \dots$$



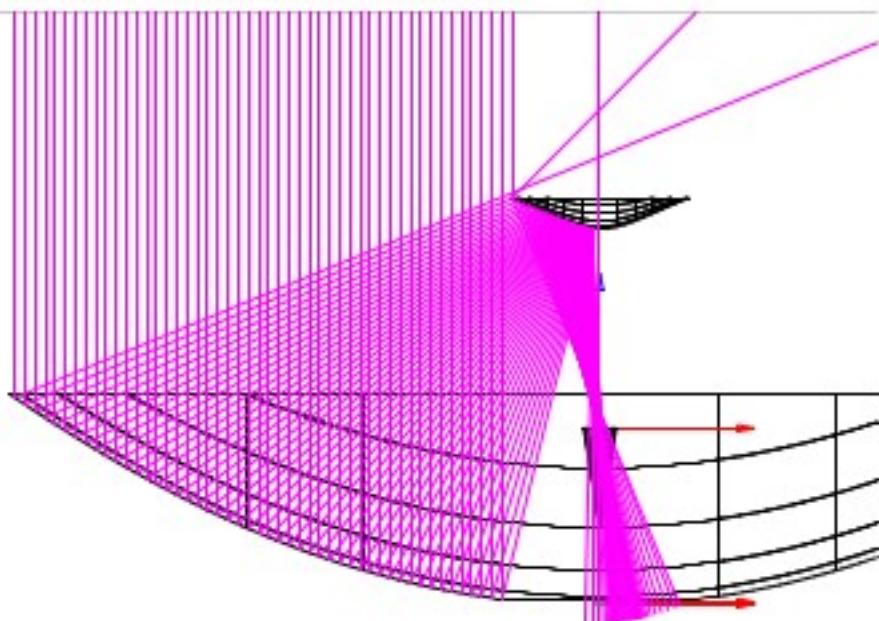
$\eta_{\text{surface}}$  : any surface has reflective loss

$\eta_{\text{blockage}}$  : the structure above the dish block a portion of the light (to 0<sup>th</sup> order)

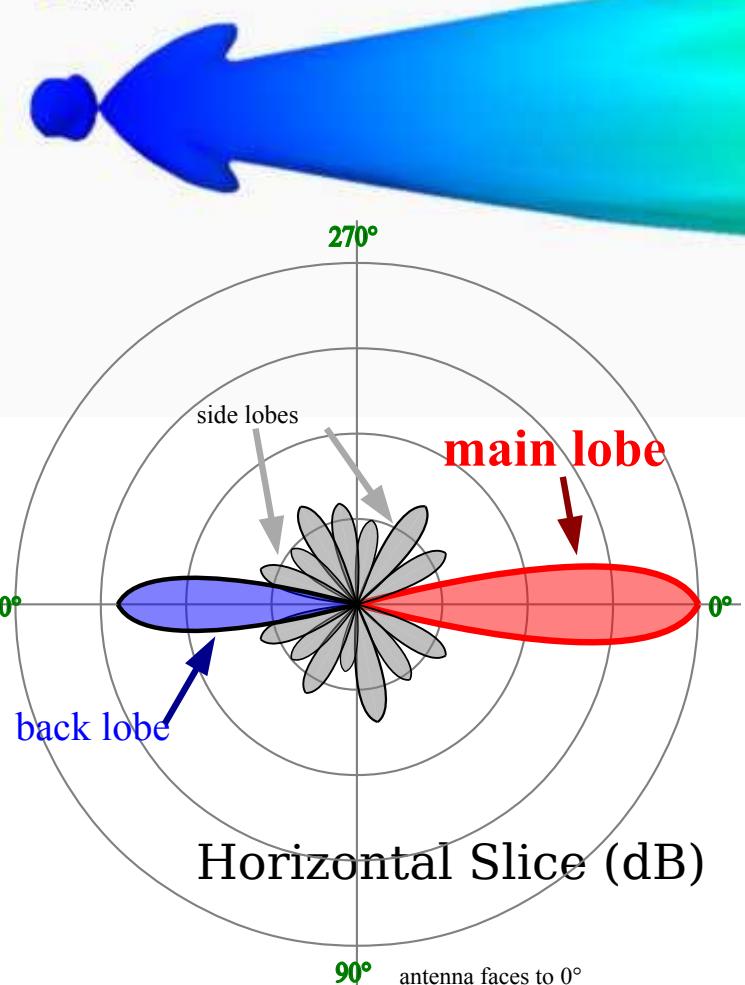
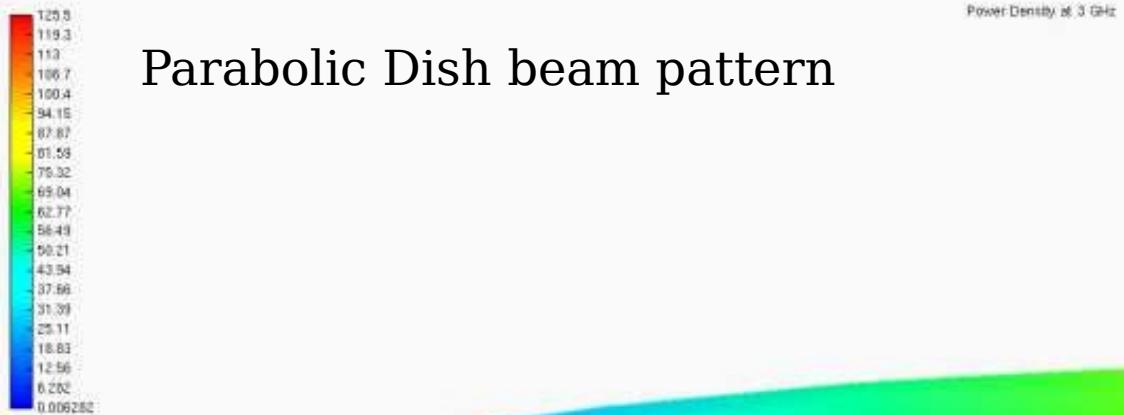
$\eta_{\text{spillover}}$  : loss due to the caustic illumination onto the receiver feed

$\eta_{\text{taper}}$  : there is a radius dependent loss with respect to illumination

These efficiencies are approximate metrics, in reality, a electro-magnetic model of the primary beam provides a more complete description



C. Copley

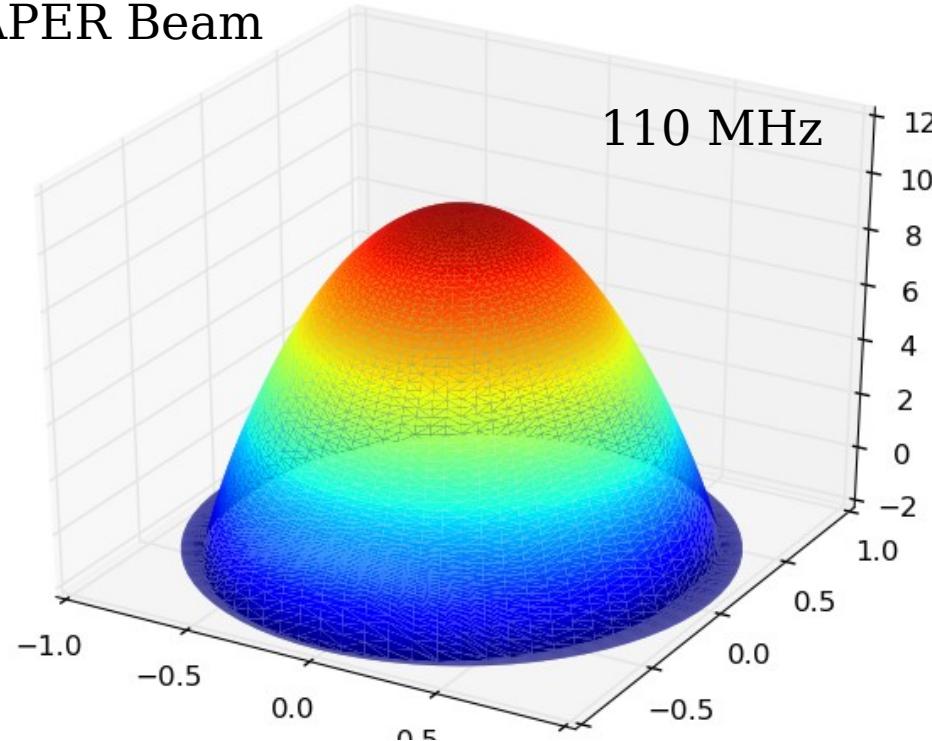


**Directivity:** a figure of merit which is a measurement of an antenna's power in the direction of strongest emission versus an isotropic (all-direction) antenna

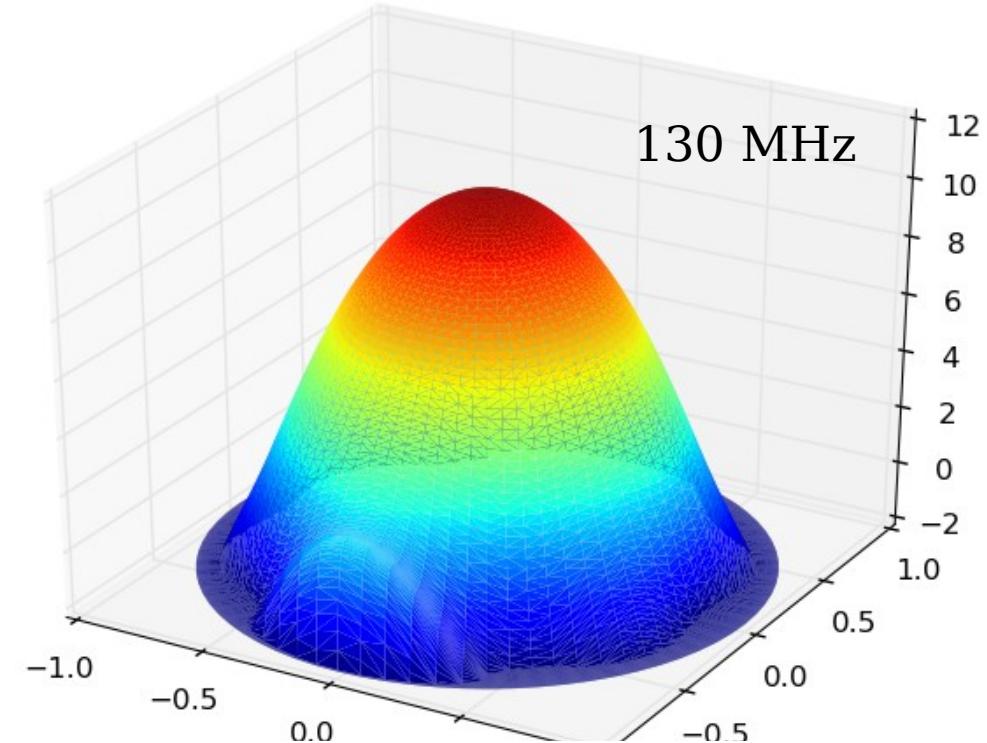
**Electrical efficiency:** efficiency at which a receiving system converts radio power

**Gain:** Combination of the antenna directivity and efficiency

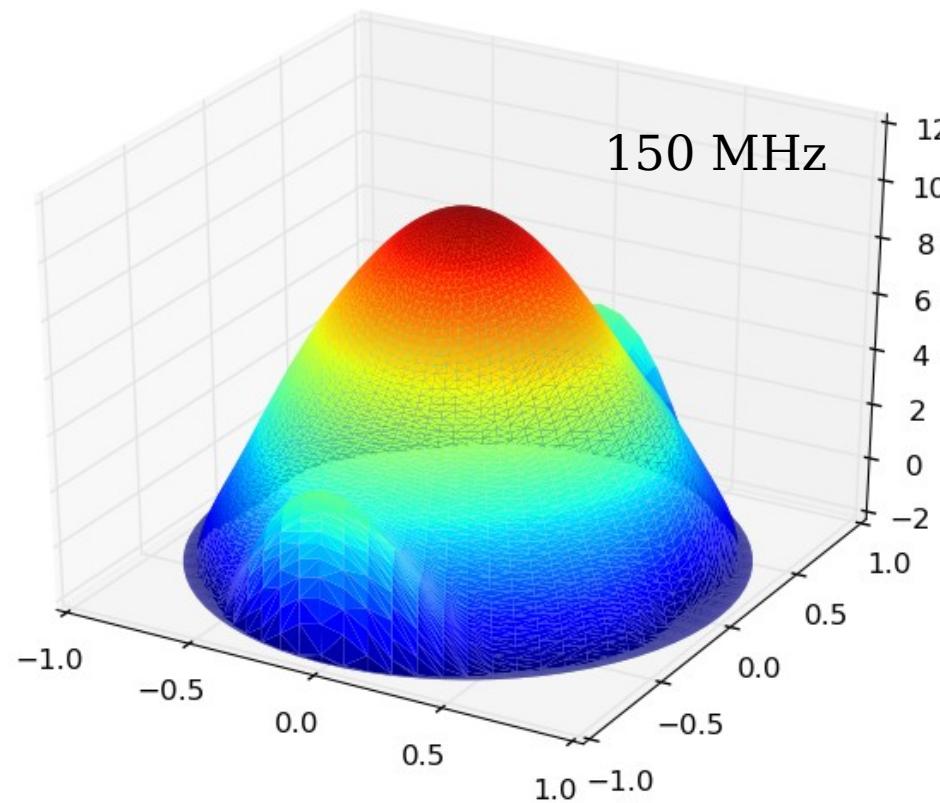
# PAPER Beam



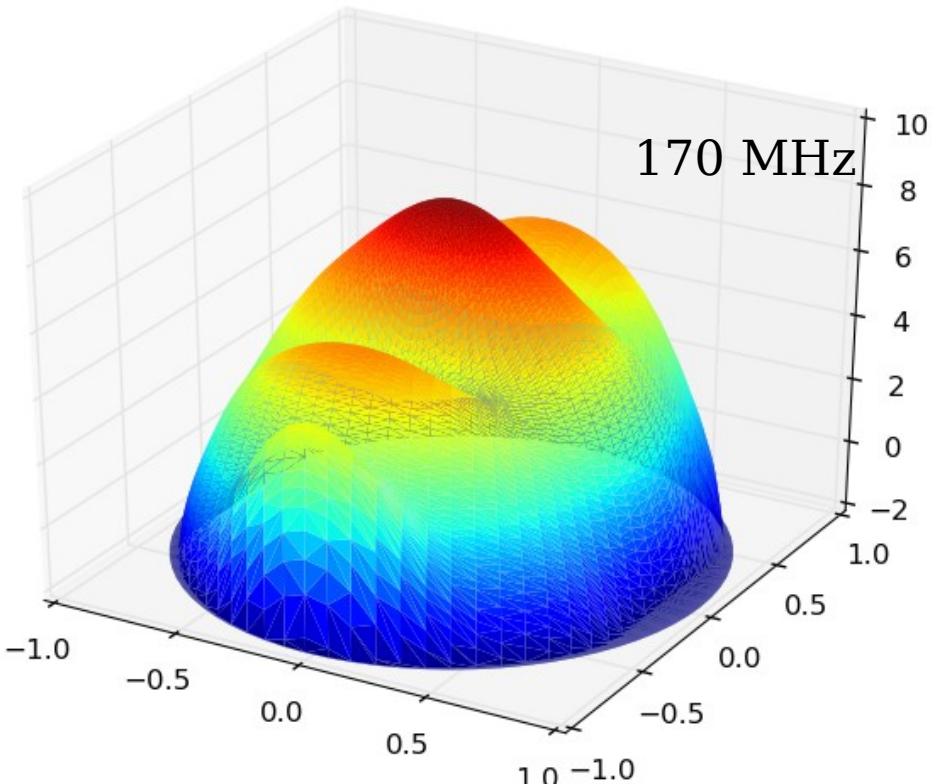
110 MHz



130 MHz



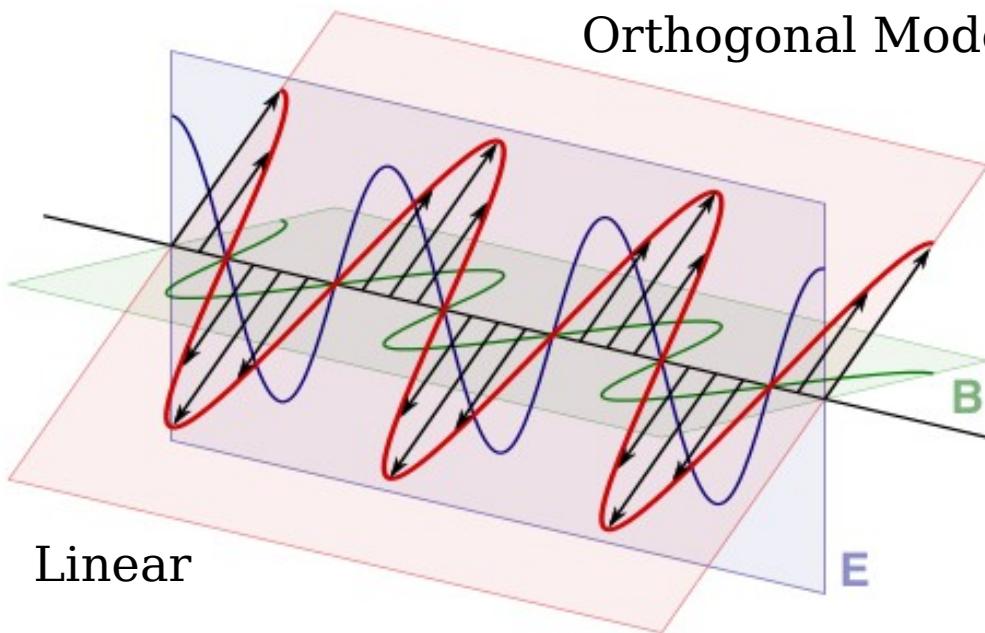
150 MHz



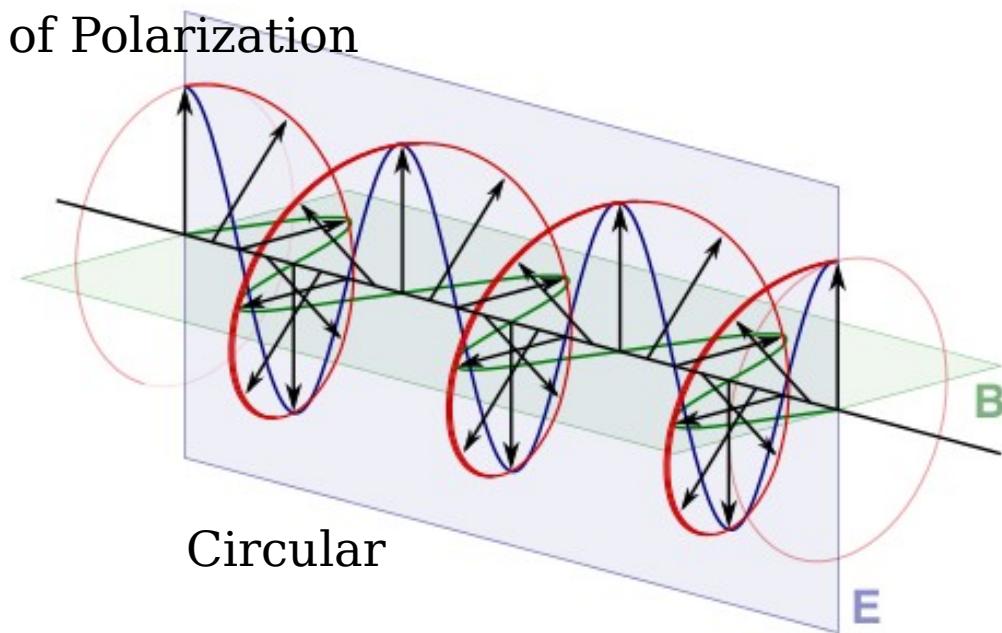
170 MHz



## Orthogonal Modes of Polarization



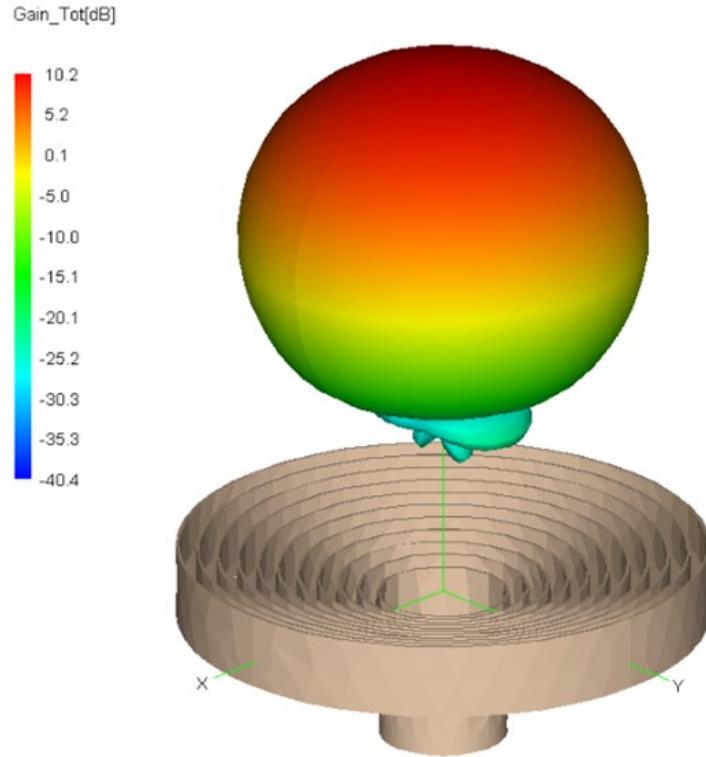
Linear



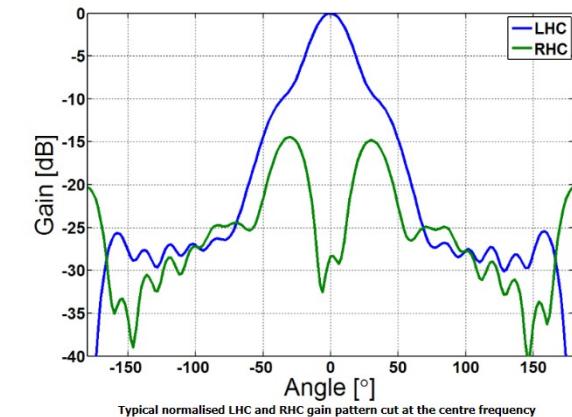
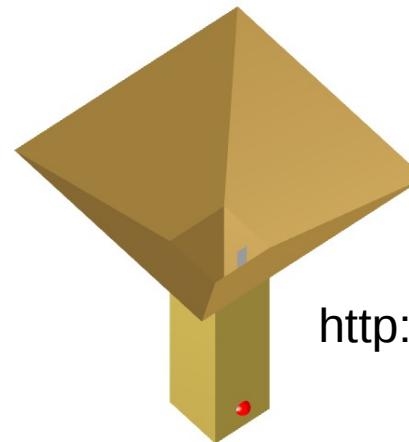
Circular



## Conical Horn

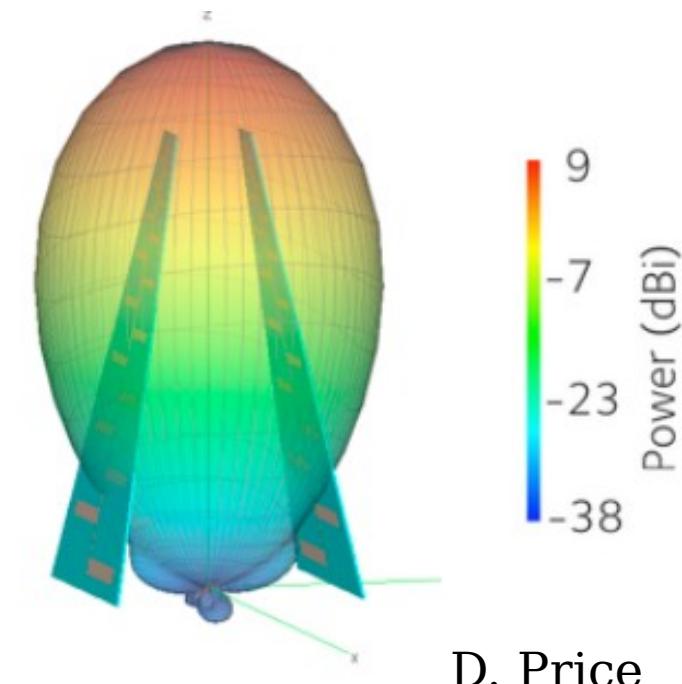
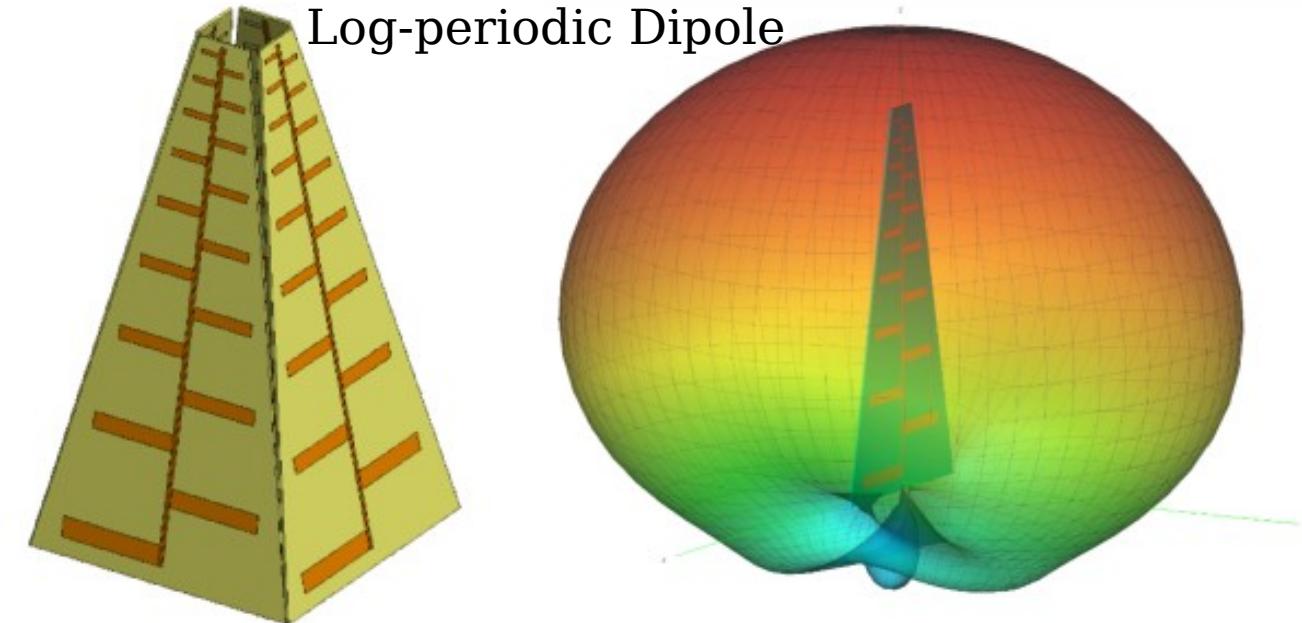


## Square Horn

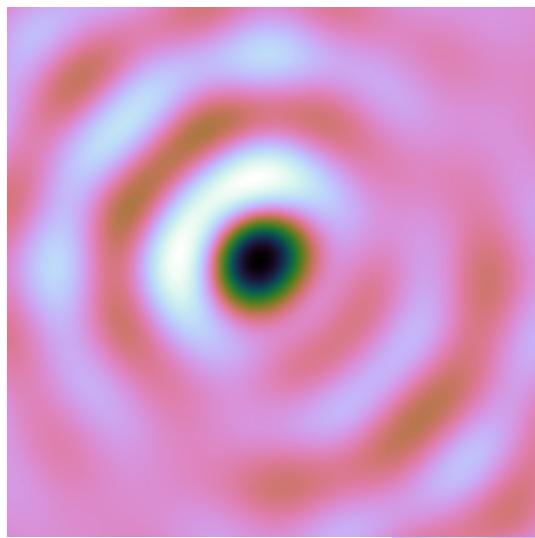


<http://www.antennamagus.com/>

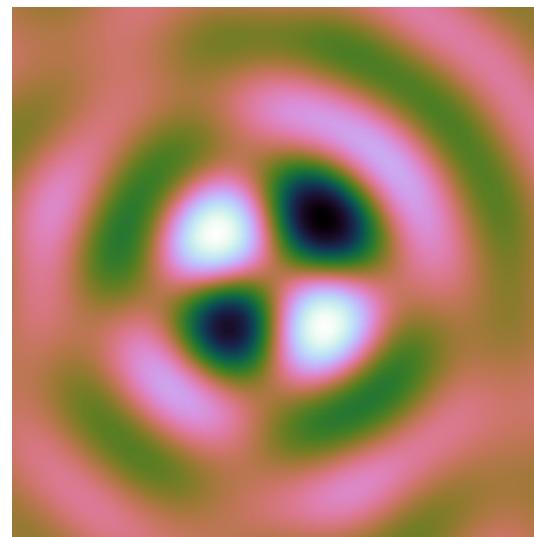
## Log-periodic Dipole



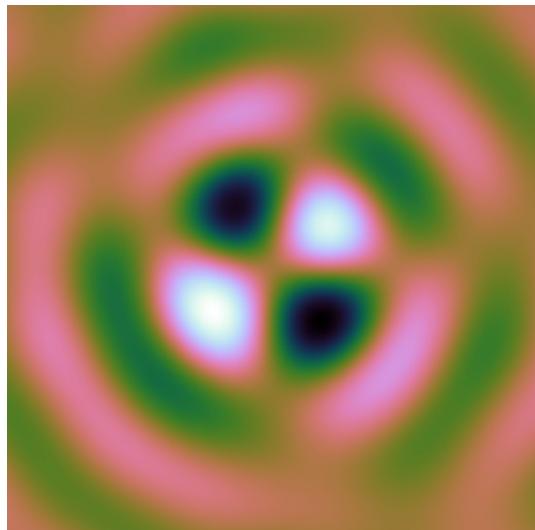
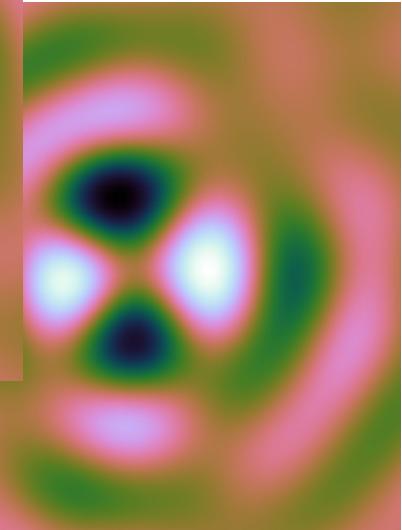
D. Price



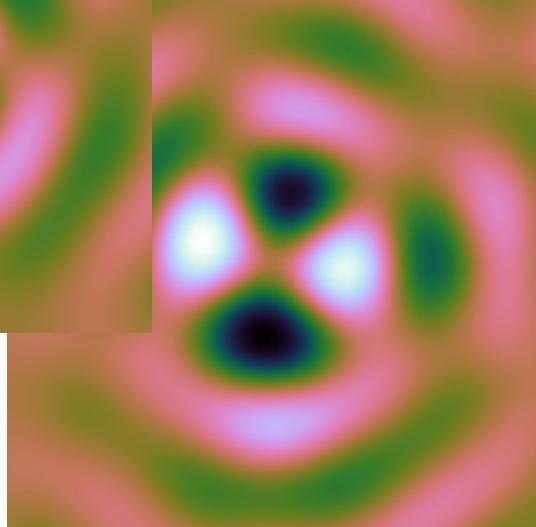
XX



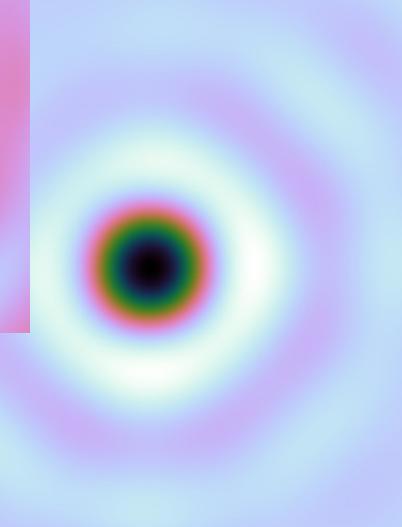
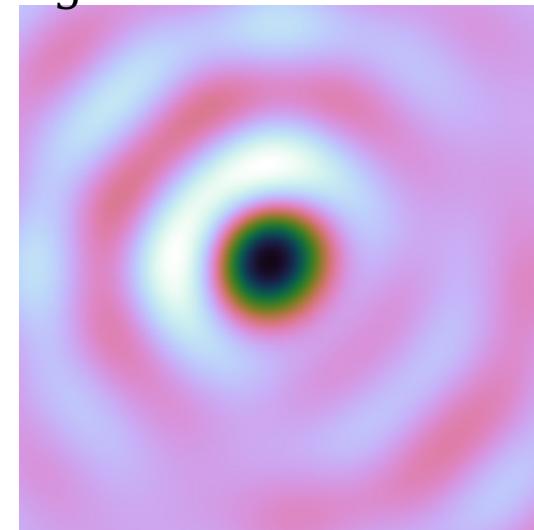
XY



YX



YY



# Conversion between Jones and Mueller (Brightness and Stokes)

$$\mathbf{E} = \begin{pmatrix} E_{xx}(\nu, t, l, m) & E_{xy}(\nu, t, l, m) \\ E_{yx}(\nu, t, l, m) & E_{yy}(\nu, t, l, m) \end{pmatrix}$$

Jones representation of the primary beam,  
 Complex voltage value with frequency and position dependent,  
 and potentially other effects (time, pointing angle, temperature...)

$$\mathbf{M}_{\mathbf{E}} = \mathbf{S}^{-1} (\mathbf{E} \otimes \mathbf{E}^*) \mathbf{S}$$

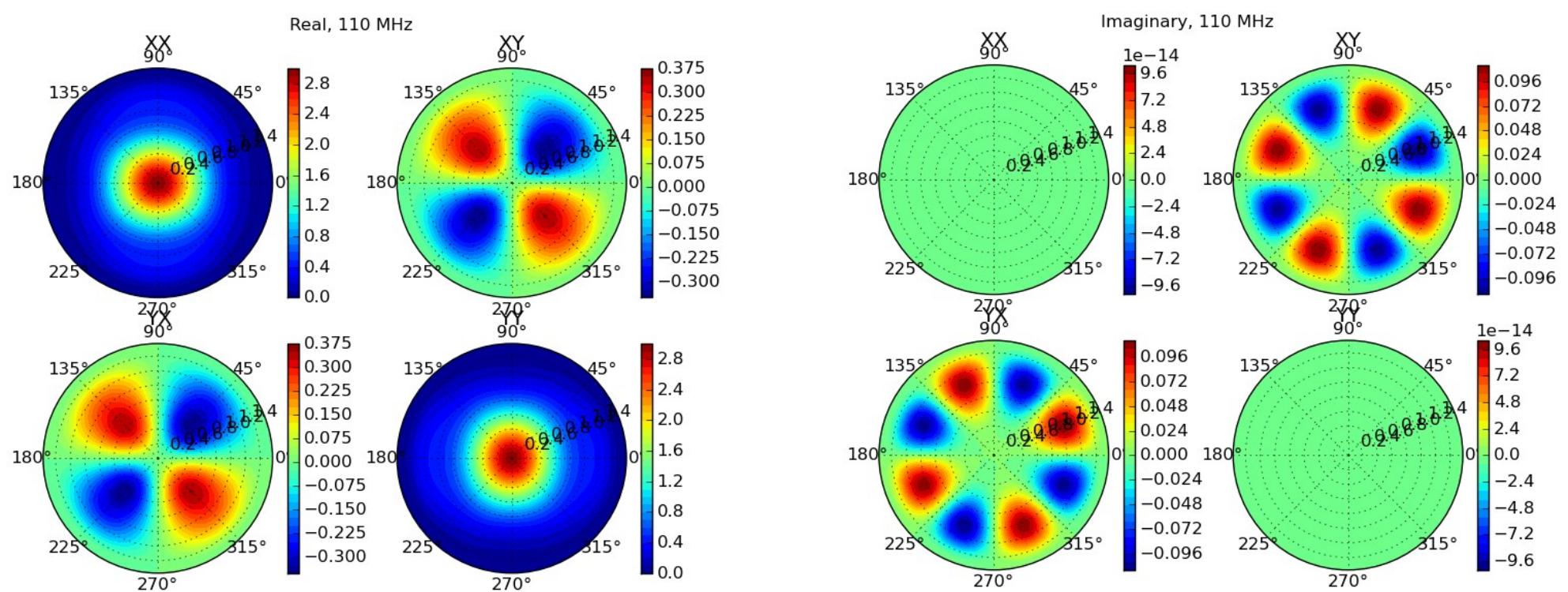
Stokes Mueller matrix representation of the primary beam

$$\mathbf{S} = \frac{1}{2} \begin{pmatrix} 1 & 1 & 0 & 0 \\ 0 & 0 & 1 & i \\ 0 & 0 & 1 & -i \\ 1 & -1 & 0 & 0 \end{pmatrix}$$

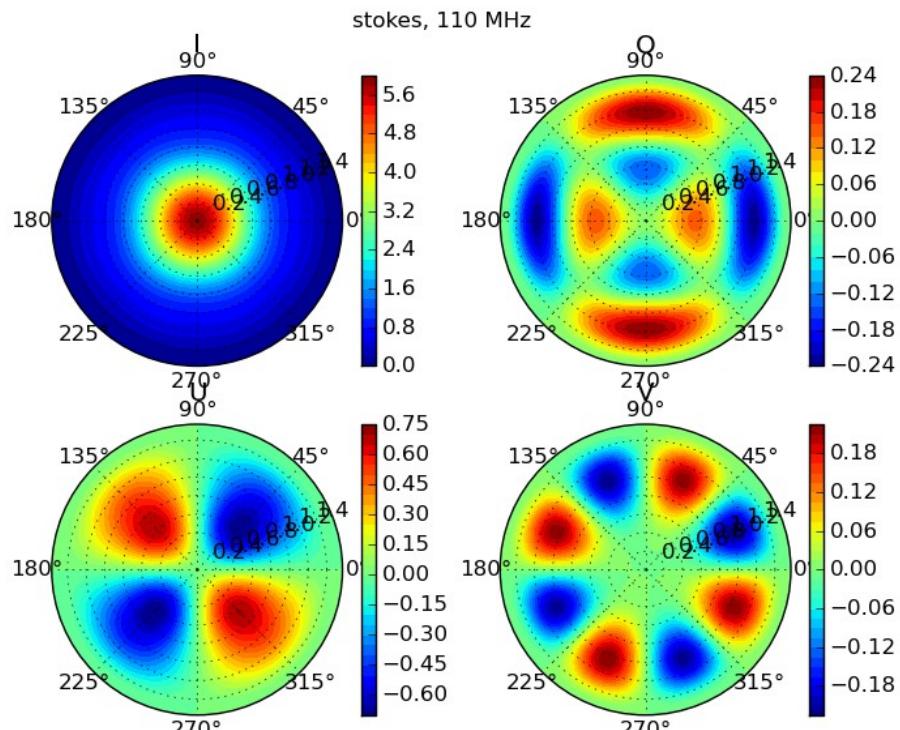
Stokes → Brightness Muller

$$\mathbf{S}^{-1} = \begin{pmatrix} 1 & 0 & 0 & 1 \\ 1 & 0 & 0 & -1 \\ 0 & 1 & 1 & 0 \\ 0 & -i & i & 0 \end{pmatrix}$$

Brightness → Stokes Muller



Jones representation conversion to Stokes Parameters



# Polarization Leakage

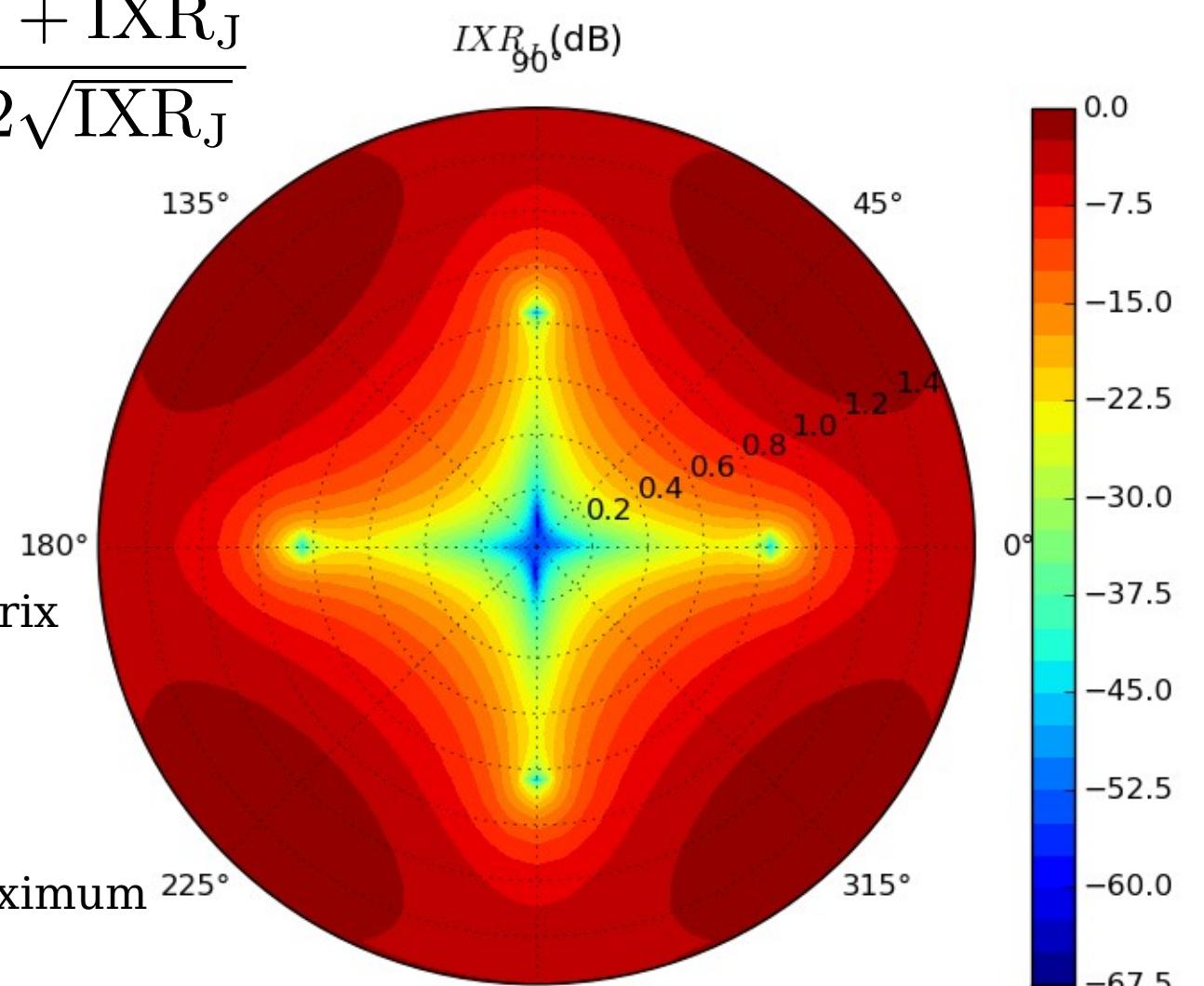
Intrinsic Cross-Polarization Ratio (IXR) [Carozzi & Woan 2011]

$$\text{IXR}_M = \frac{\kappa(M) + 1}{\kappa(M) - 1} = \frac{1 + \text{IXR}_J}{2\sqrt{\text{IXR}_J}}$$

$$\text{IXR}_J = \left( \frac{\kappa(J) + 1}{\kappa(J) - 1} \right)^2$$

$\kappa(M)$  Mueller and Jones matrix  
 $\kappa(J)$  condition numbers

$g_{\min}$  and  $g_{\max}$ : Minimum and maximum values when performing SVD

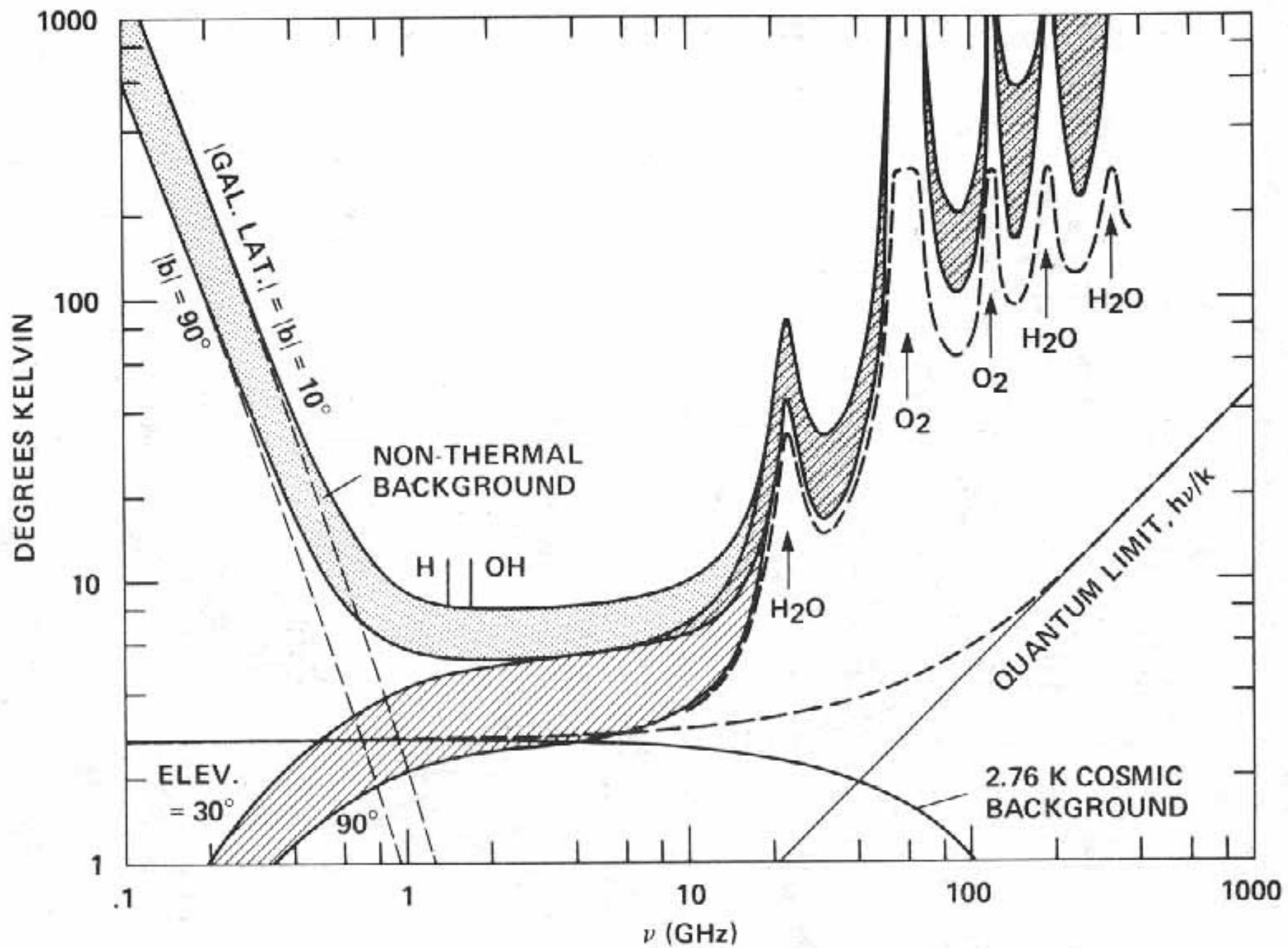


$$J = \frac{g_{\max} + g_{\min}}{2} \begin{pmatrix} 1 & 1/\sqrt{\text{IXR}_J} \\ 1/\sqrt{\text{IXR}_J} & 1 \end{pmatrix}^{270^\circ} \text{ PAPER Beam @ 110 MHz}$$

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Analogue Electronics  
(selectively) converting light to  
voltage

## Simple model of the radio sky



# System Temperature

$$T_{\text{sys}} = T_{\text{sky}} + T_{\text{atmosphere}} + T_{\text{spillover}} + T_{\text{rx}} + \dots$$

$T_{\text{sky}}$ : radio sky background (synchrotron, CMB (2.76K), ...)

$T_{\text{atmosphere}}$ : atmospheric foregrounds (important at mm wavelengths)

$T_{\text{spillover}}$ : pick-up of  $\sim 300\text{K}$  ground in the side and back-lobes

$T_{\text{rx}}$ : receiver temperature from the Friis Cascade Noise Equation

$T_{\text{passive}}$ : passive components (cables, connectors, OMT) before the LNA

$T_{\text{LNA}}$ : Low-Noise Amplifier temperature

$T_{\text{amp}}$ : secondary amplification/attenuation temperature

$G_{\text{LNA}}$ : gain of the LNA

$G_{\text{feed}}$ ,  $G_{\text{passive}}$ : feed and passive 'gain' (related to efficiency)

$$T_{\text{rx}} = T_{\text{feed}} + \frac{T_{\text{passive}}}{G_{\text{feed}}} + \frac{T_{\text{LNA}}}{G_{\text{feed}} G_{\text{passive}}} + \frac{T_{\text{amp}}}{G_{\text{feed}} G_{\text{passive}} G_{\text{LNA}}} + \dots$$

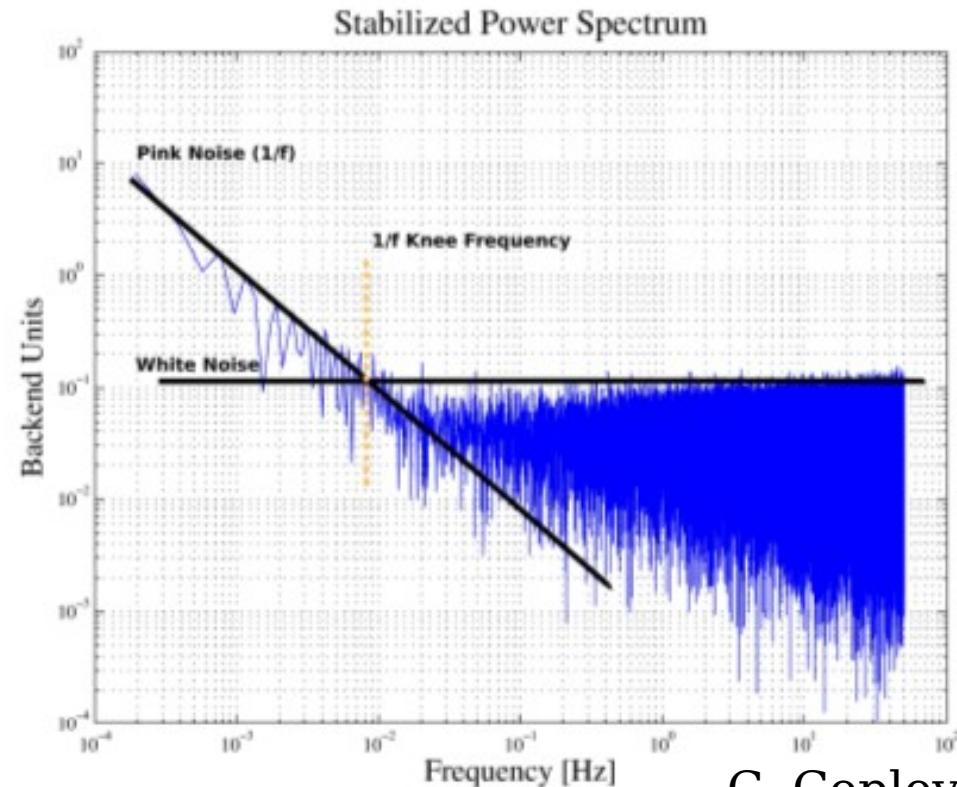
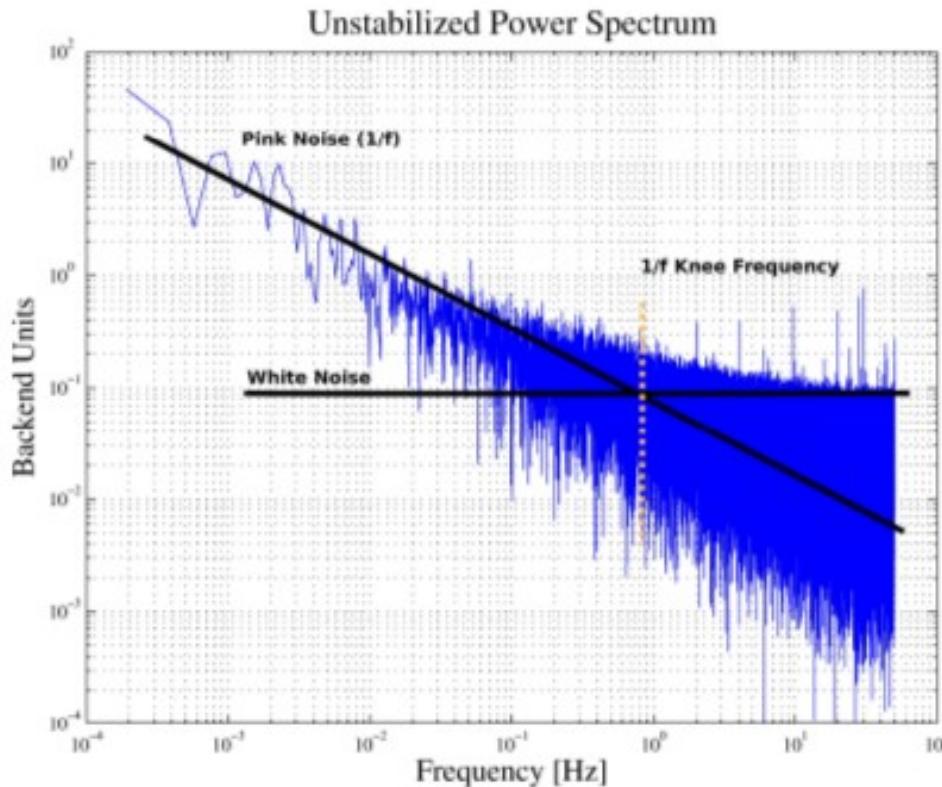
# Radiometer Equation

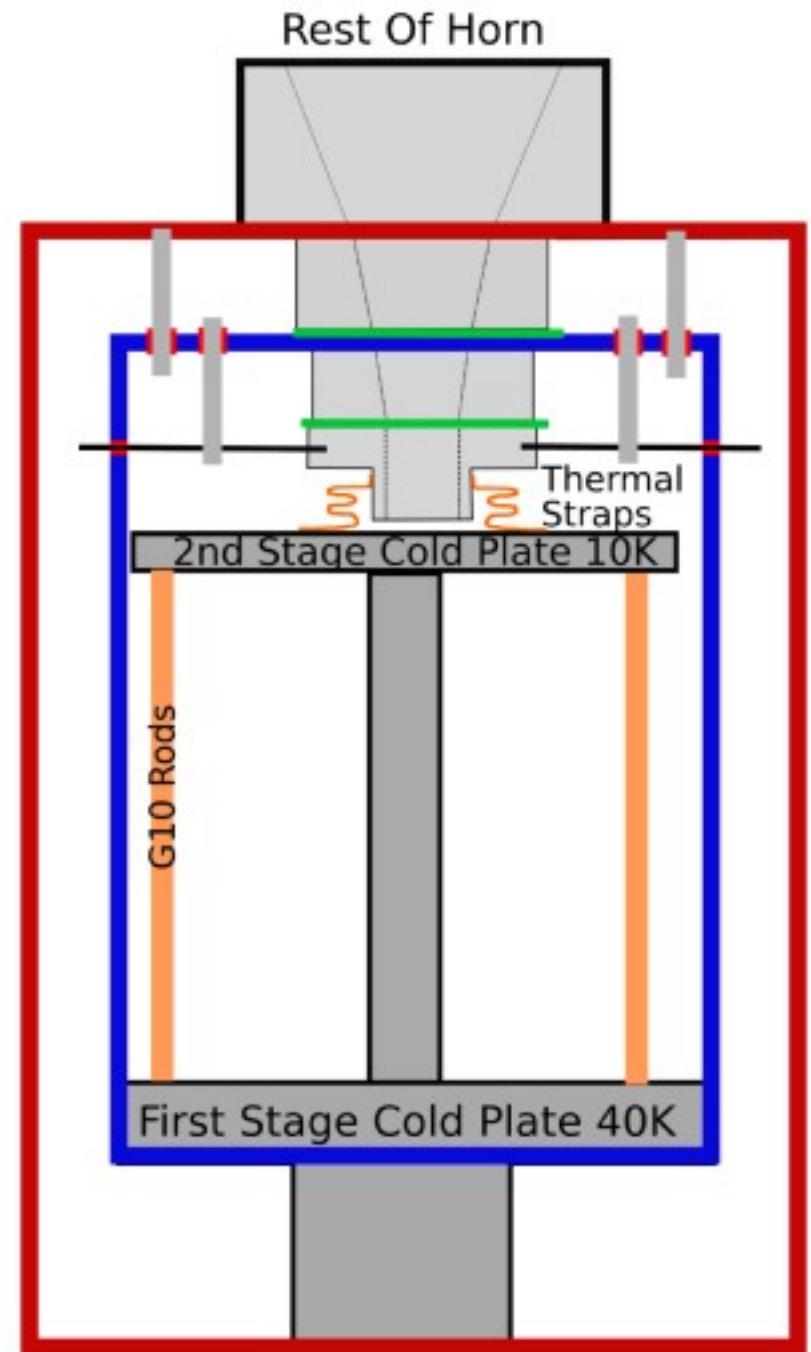
$$\sigma_T = \frac{T_{sys}}{\sqrt{\Delta\nu\tau}}$$

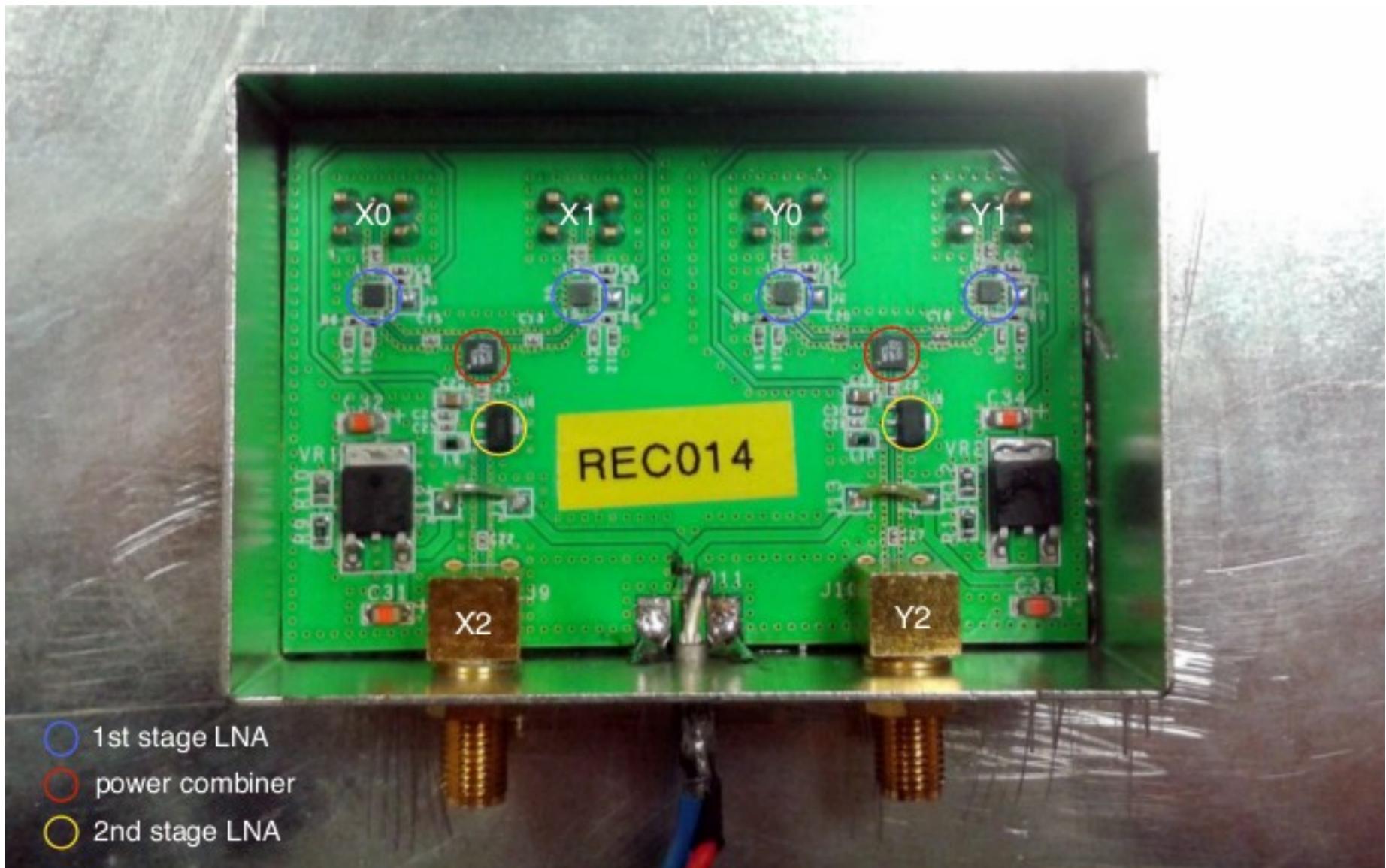
$\sigma_T$ : residual (root-mean-square) in the measurement

$\Delta\nu$ : bandwidth of observation (Hz)  
 $\tau$ : integration time (seconds)

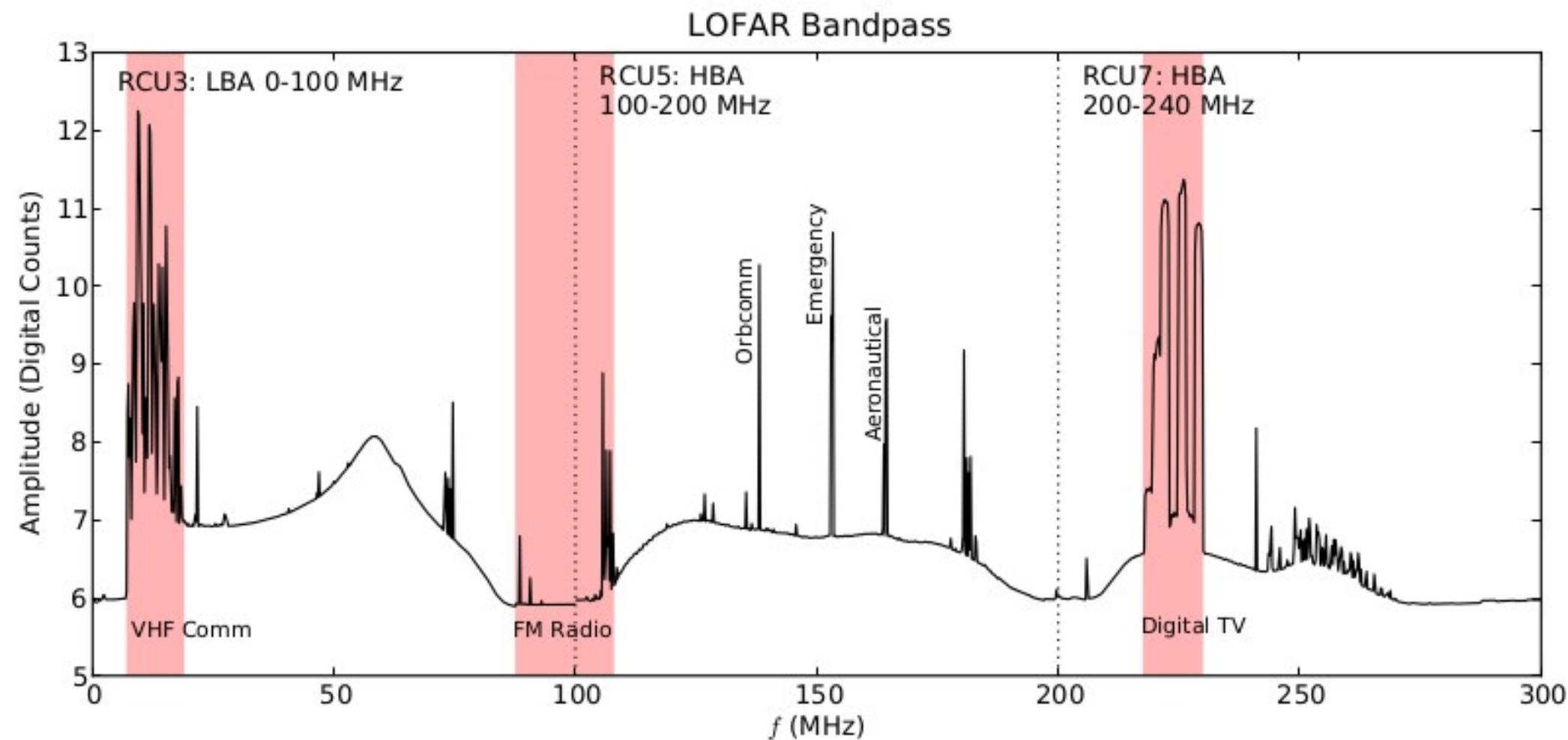
→ the smaller the  $T_{sys}$  the shorter the required observation time



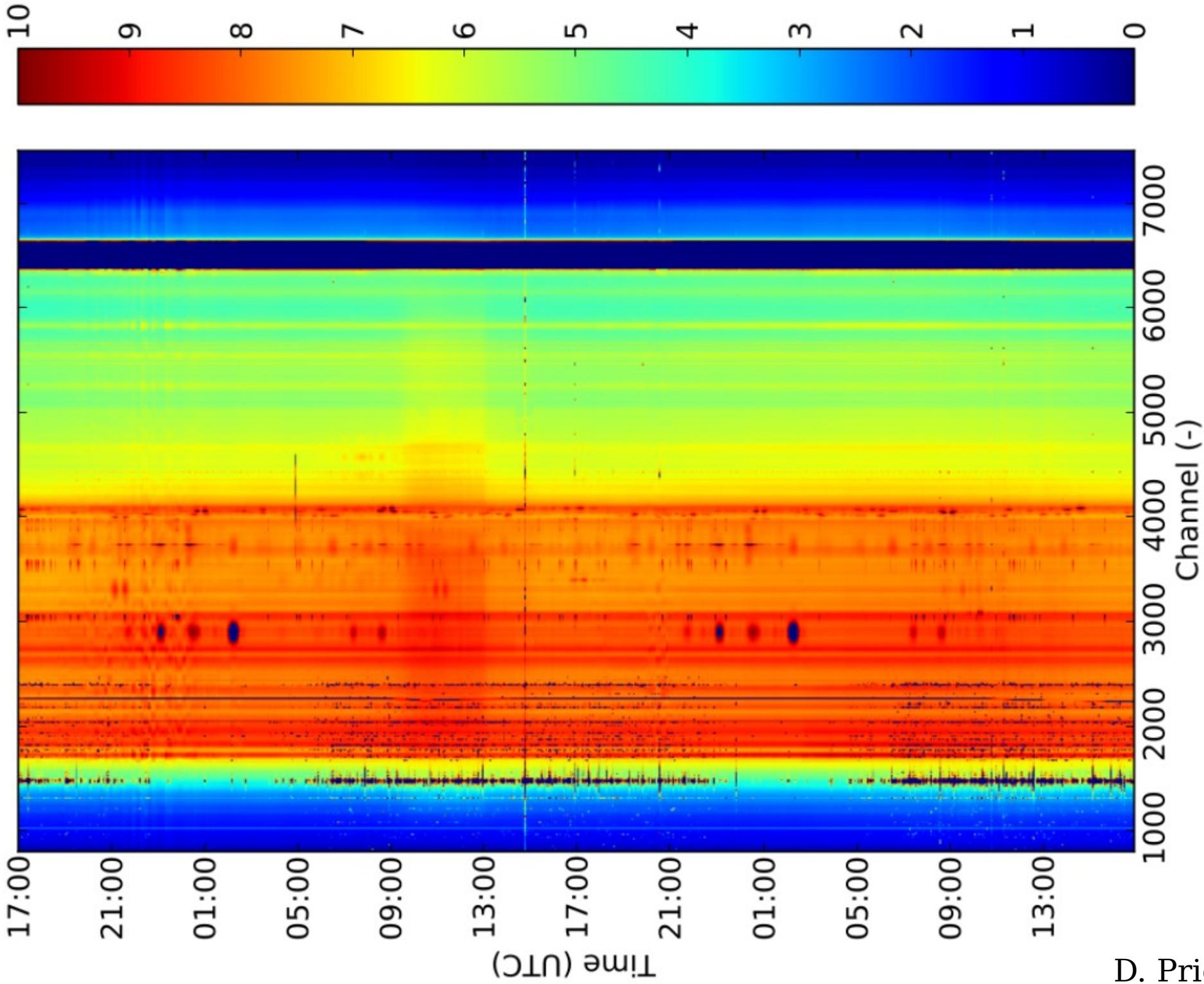




# Radio Frequency Interference (RFI)

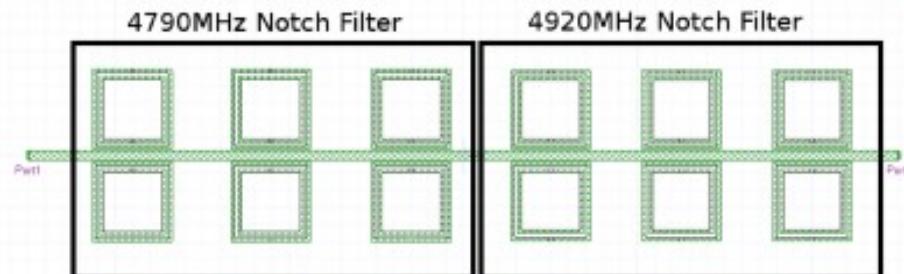


Power (dB)



D. Price

## ■ 4790 4920 Notch Filter ■



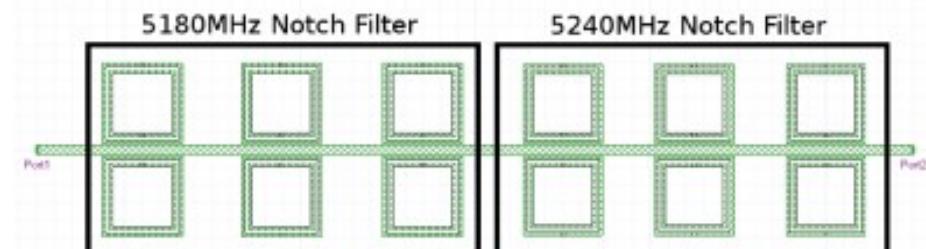
■ Designed for Nominal Fc ■

(a) The 4.79 GHz and 4.92 GHz notch filter



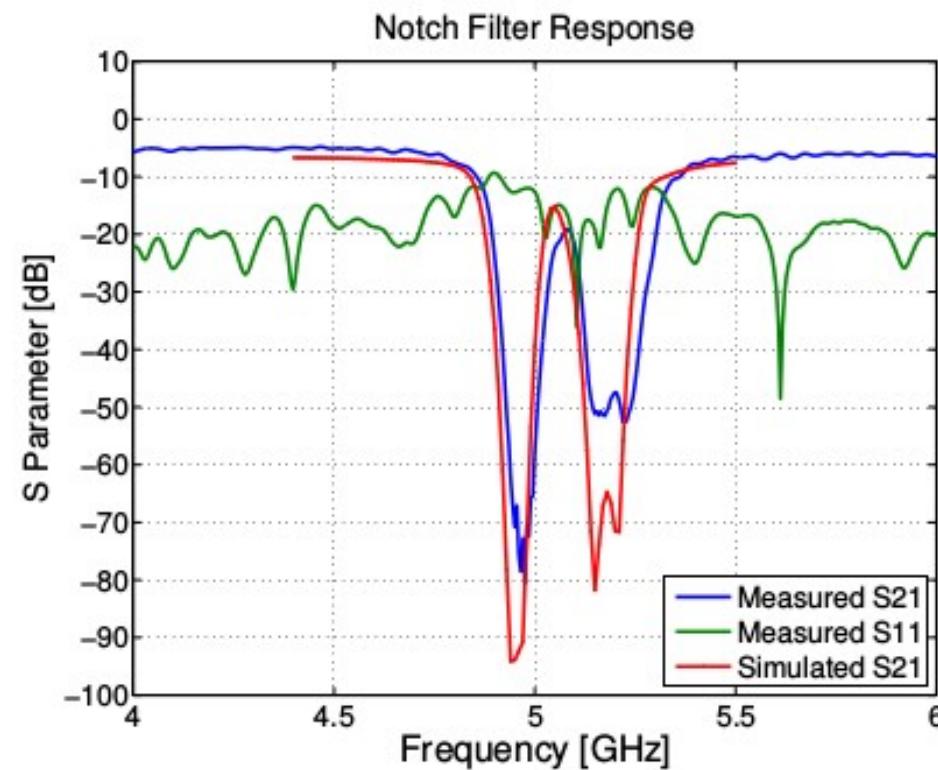
(c) Manufactured notch filter (with 6 dB attenuator to improve input match)

## ■ 5180 5240 Notch Filter ■



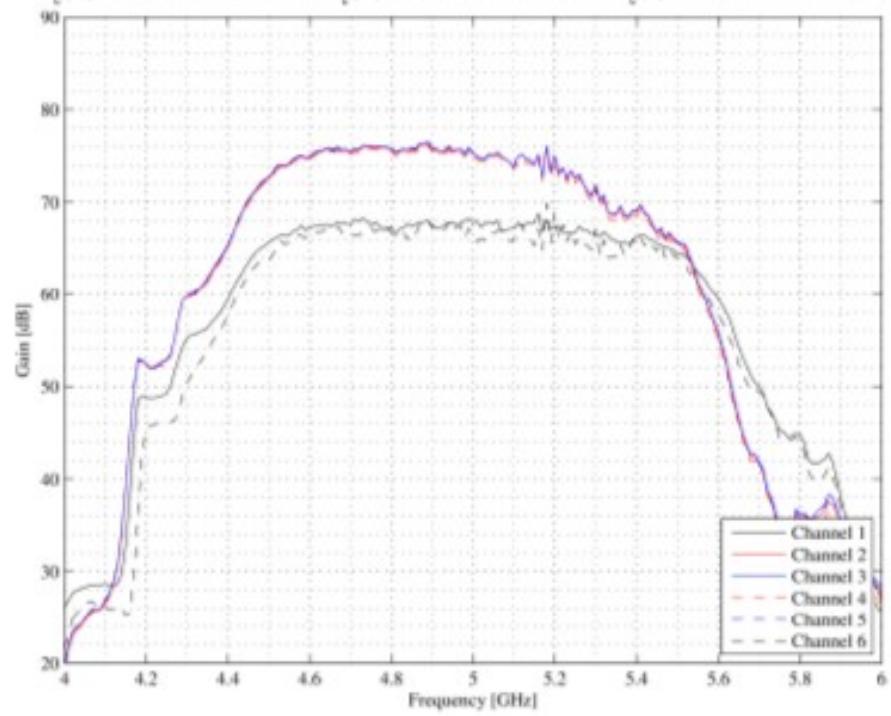
■ Designed for Nominal Fc ■

(b) The 5.18 GHz and 5.24 GHz notch filter

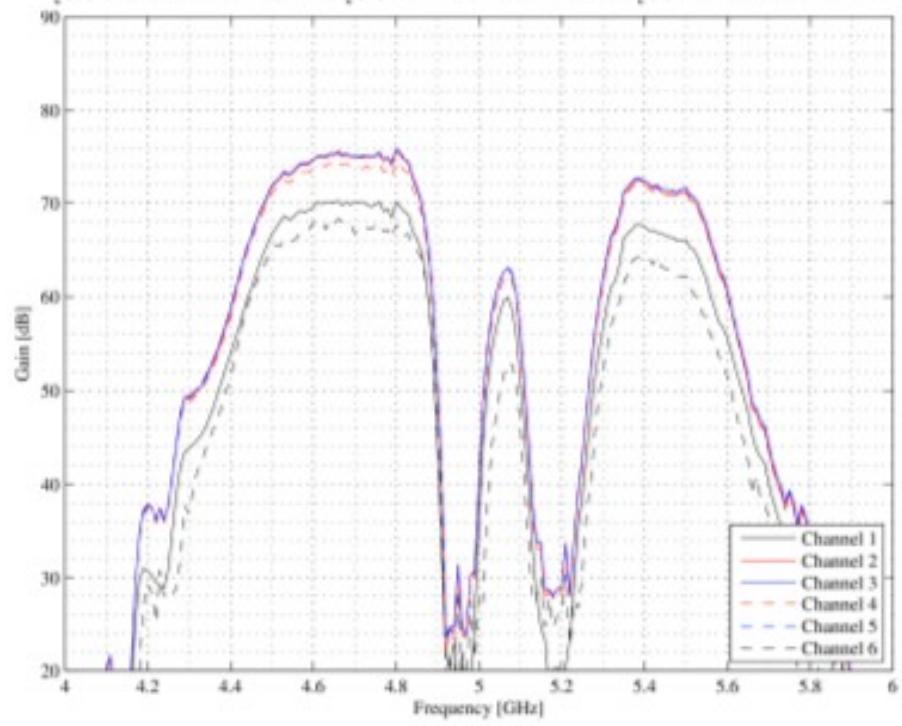


(d) Measured vs Simulated Responses

$f_c [1] = 4.972 \text{ GHz}, \text{BW} = 1.125 \text{ GHz}; f_c [2] = 4.976 \text{ GHz}, \text{BW} = 1.068 \text{ GHz}; f_c [P] = 4.888 \text{ GHz}, \text{BW} = 0.909 \text{ GHz}$



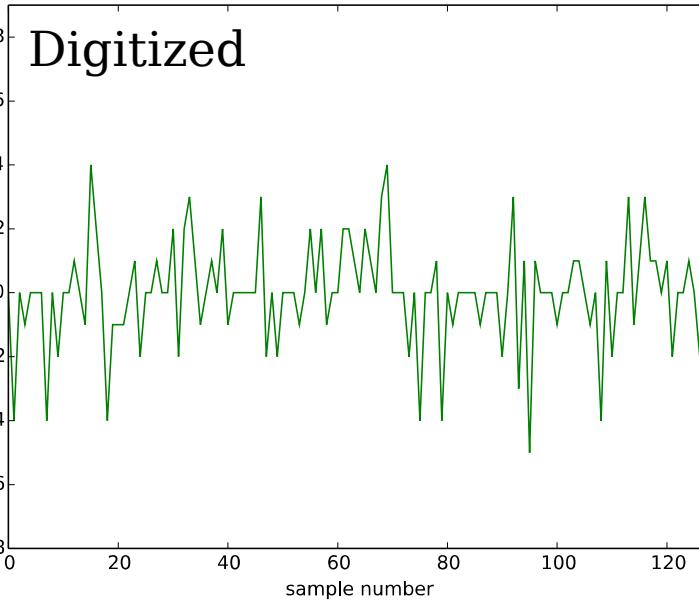
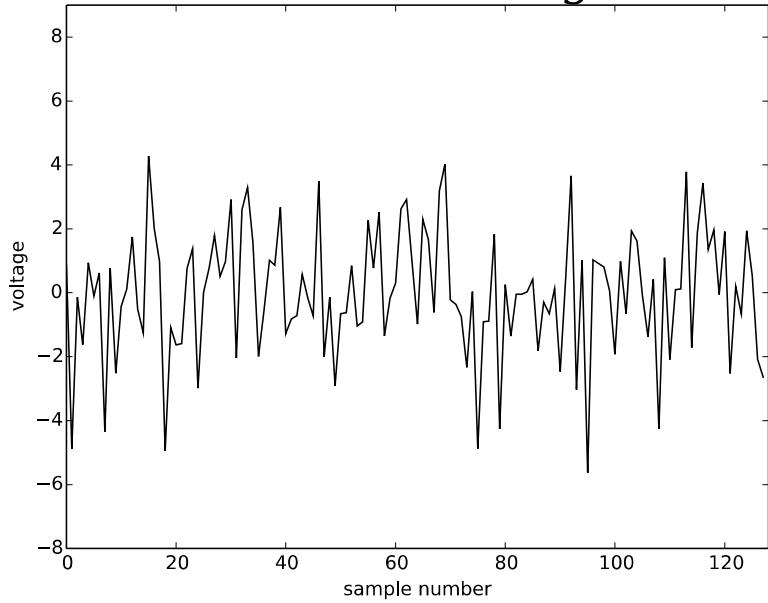
$f_c [1] = 4.849 \text{ GHz}, \text{BW} = 0.573 \text{ GHz}; f_c [2] = 4.804 \text{ GHz}, \text{BW} = 0.537 \text{ GHz}; f_c [P] = 4.845 \text{ GHz}, \text{BW} = 0.564 \text{ GHz}$



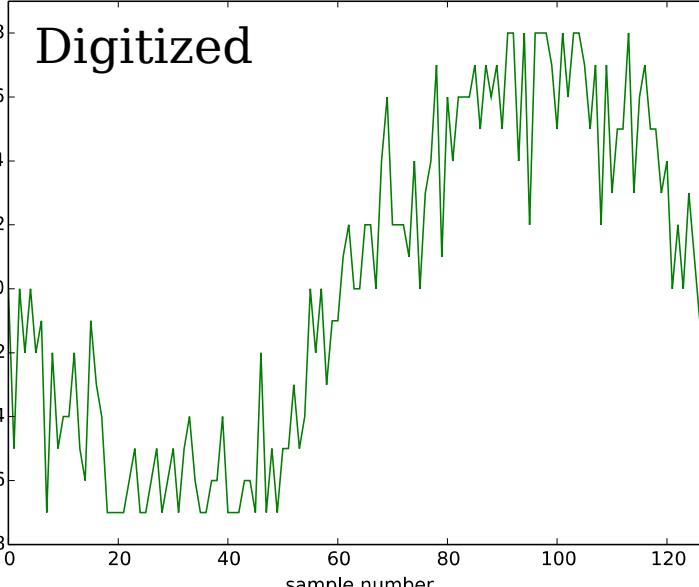
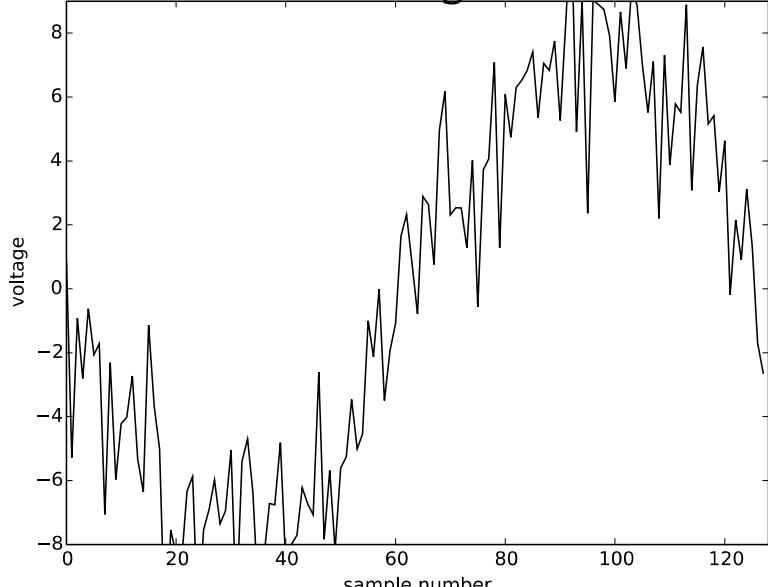
# Analogue to Digital Converter (ADC)

## the last analogue component

Astronomical signal



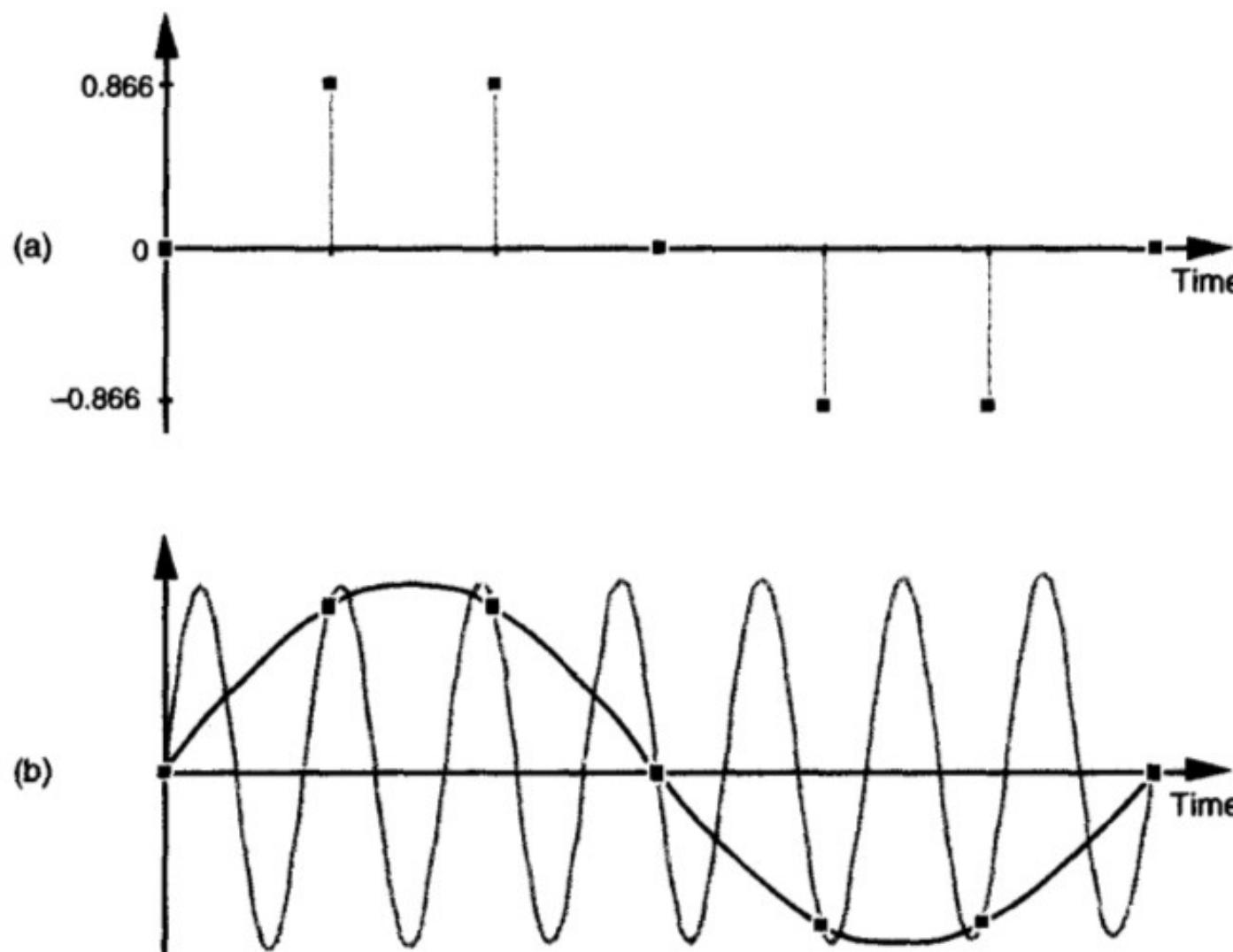
Astronomical signal with RFI



# Digital Electronics

Computing the visibilities

# Ambiguity in the Frequency Domain and the Nyquist Criterion



**Figure 2-1** Frequency ambiguity: (a) discrete-time sequence of values; (b) two different sinewaves that pass through the points of the discrete sequence.

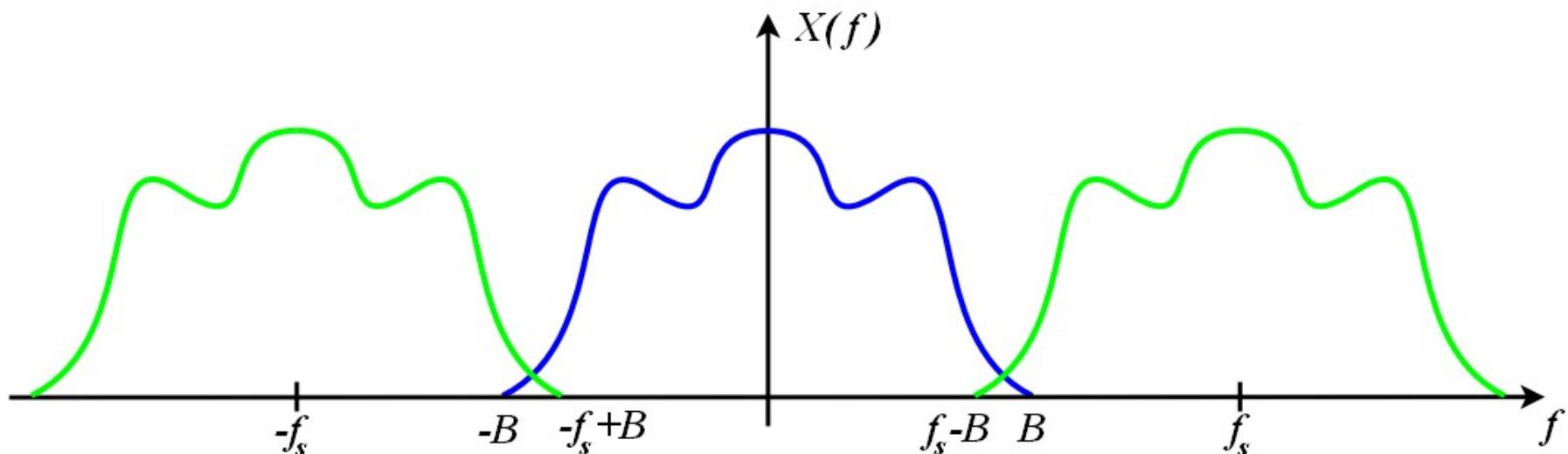
# Ambiguity in the Frequency Domain and the Nyquist Criterion

$f_s$ : frequency sampling rate

Ambiguity: When sampling at a rate of  $f_s$ , for  $k$  any integer, we cannot distinguish between sampled values of a sine wave with frequency  $f_0$  and sine wave of frequency  $f_0 + kf_s$

This puts a limit on the maximum frequency:

$f_{\text{nyquist}} = 0.5 f_s$ , Nyquist frequency, the maximum frequency which can be resolved before aliasing

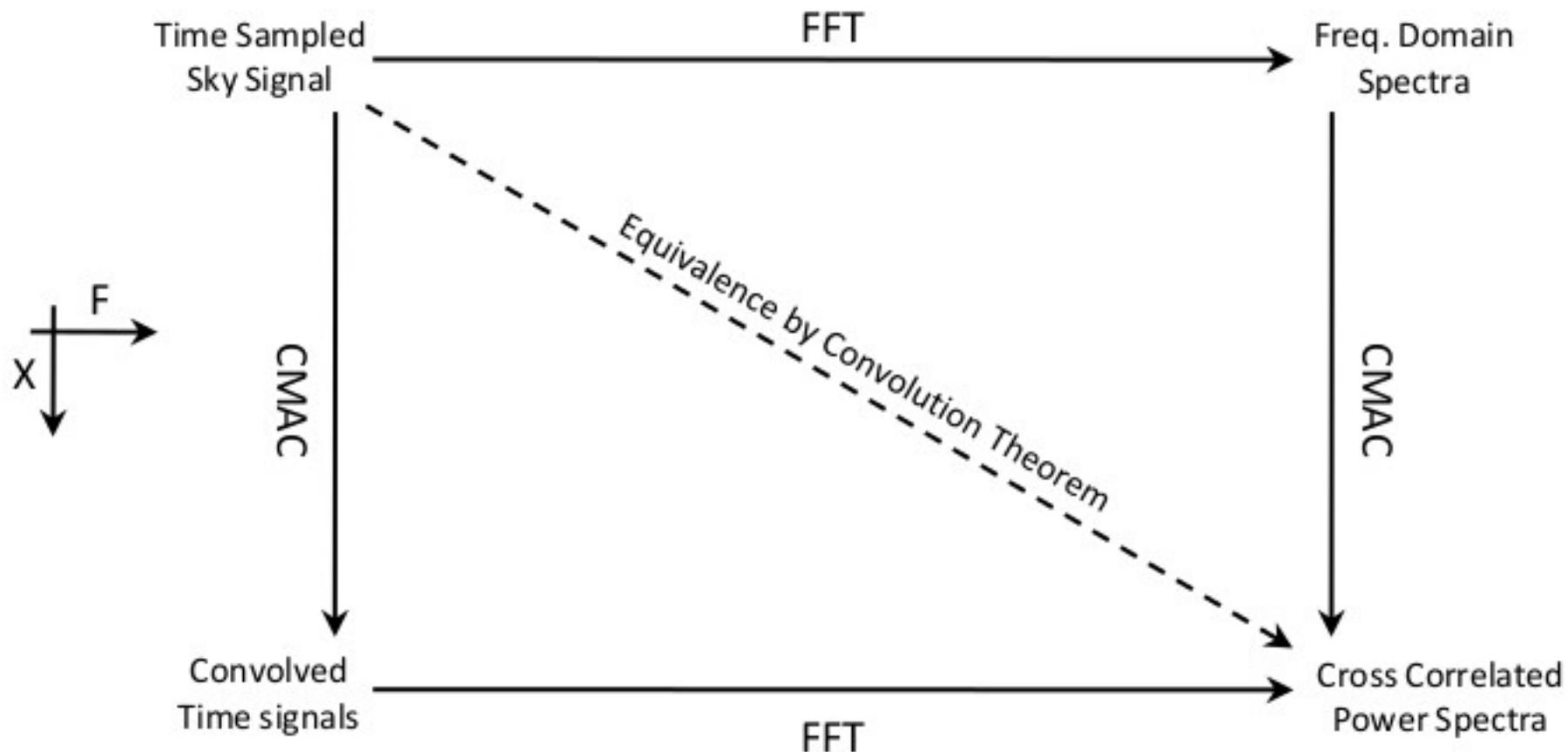


# Convolution Theorem and Correlators

To compute visibilities, we would like to correlate (convolve) for each antenna pair  $(f,g)$

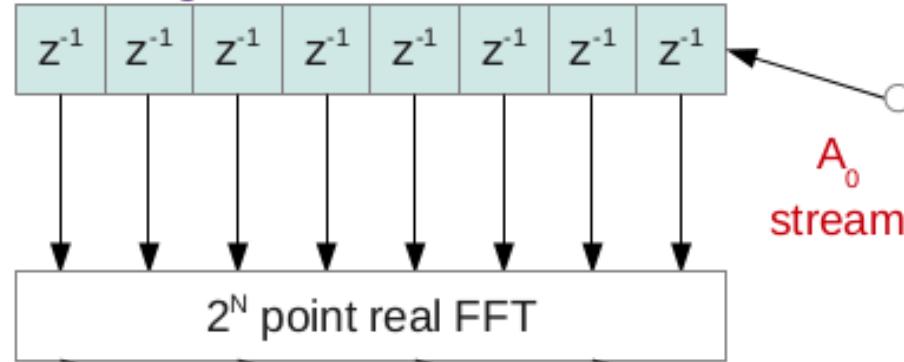
$$\text{Convolution Theorem: } \mathcal{F}\{f * g\} = \mathcal{F}\{f\} \mathcal{F}\{g\}$$

Where the convolution symbol is defined as:  $f * g = \int f(x)g(z-x)dx$

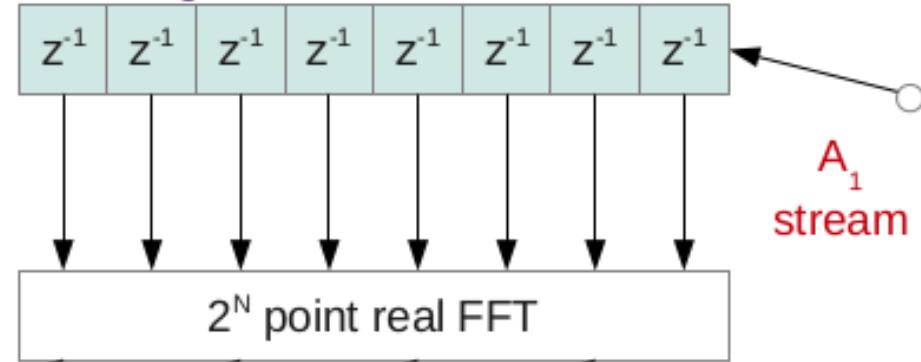


# FX Correlator Design

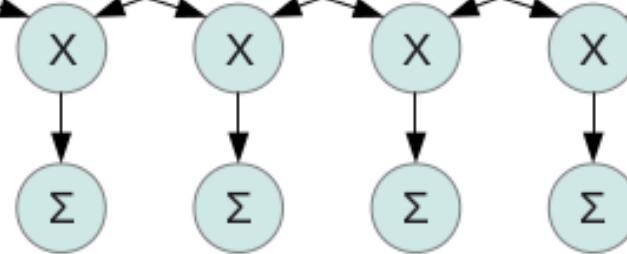
Shift Register



Shift Register



J. Hickish



CROSS POWER SPECTRUM

$$N_{bls} = N_{ant} + \frac{N_{ant}(N_{ant} - 1)}{2}$$

Auto-correlations

Cross-correlations

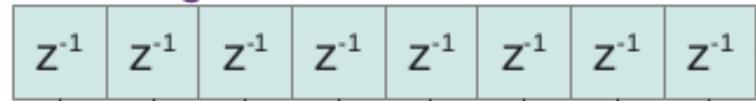
Cost:  $O(NM \log(M) + MN^2)$

M: frequency channels

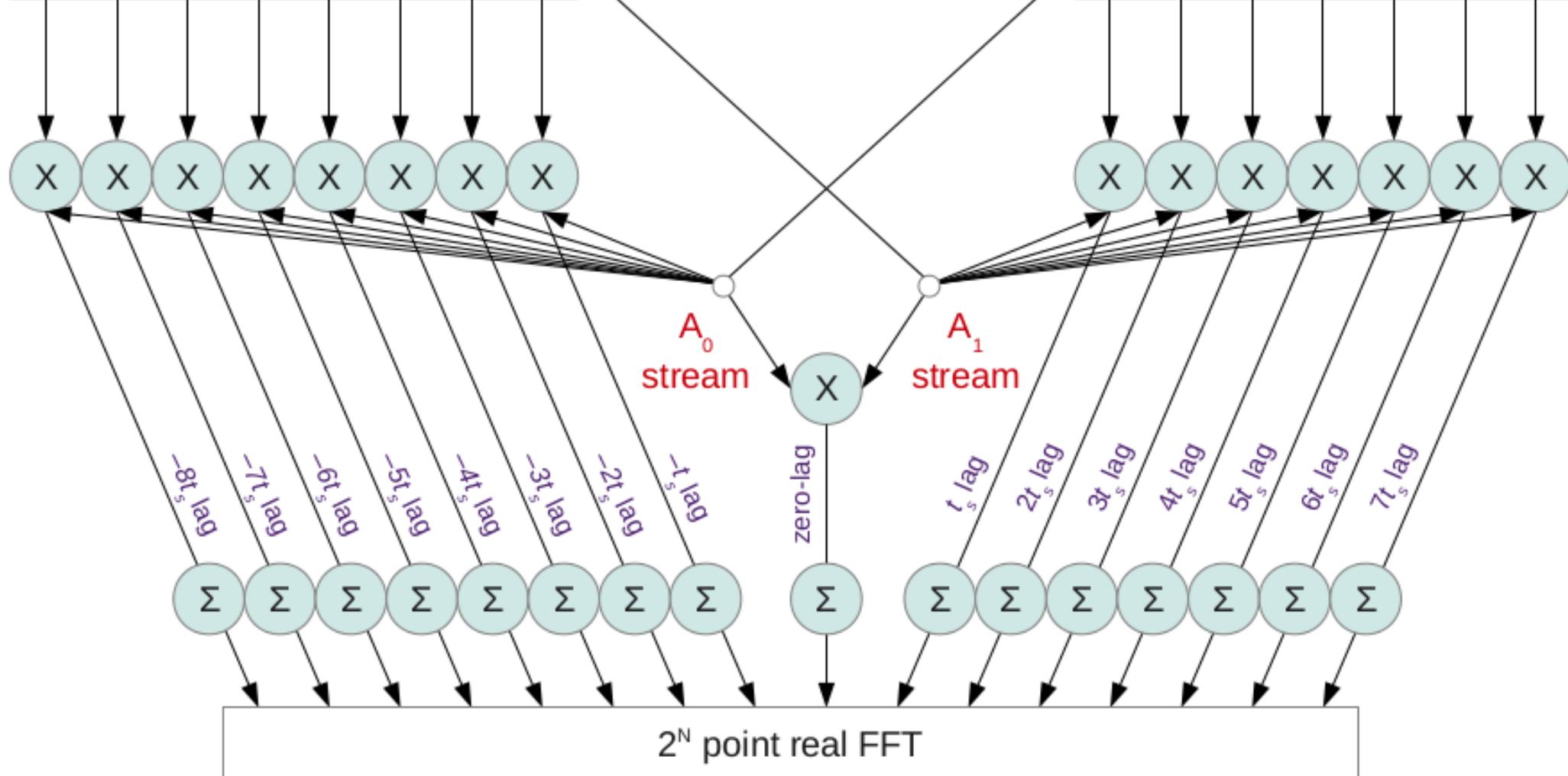
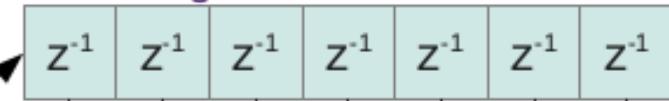
N: number of antennas

# XF Correlator Design

Shift Register



Shift Register



Cost: O(TN<sup>2</sup>)

T: number of lags

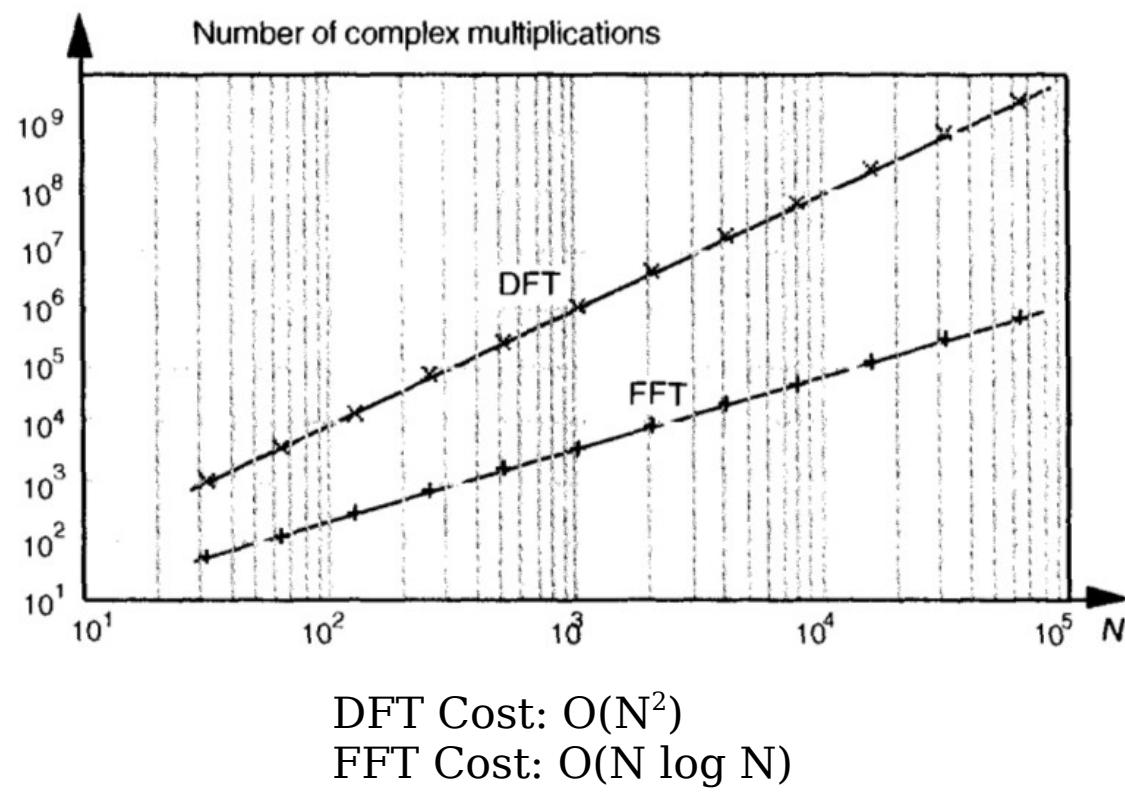
N: number of antennas

CROSS POWER SPECTRUM

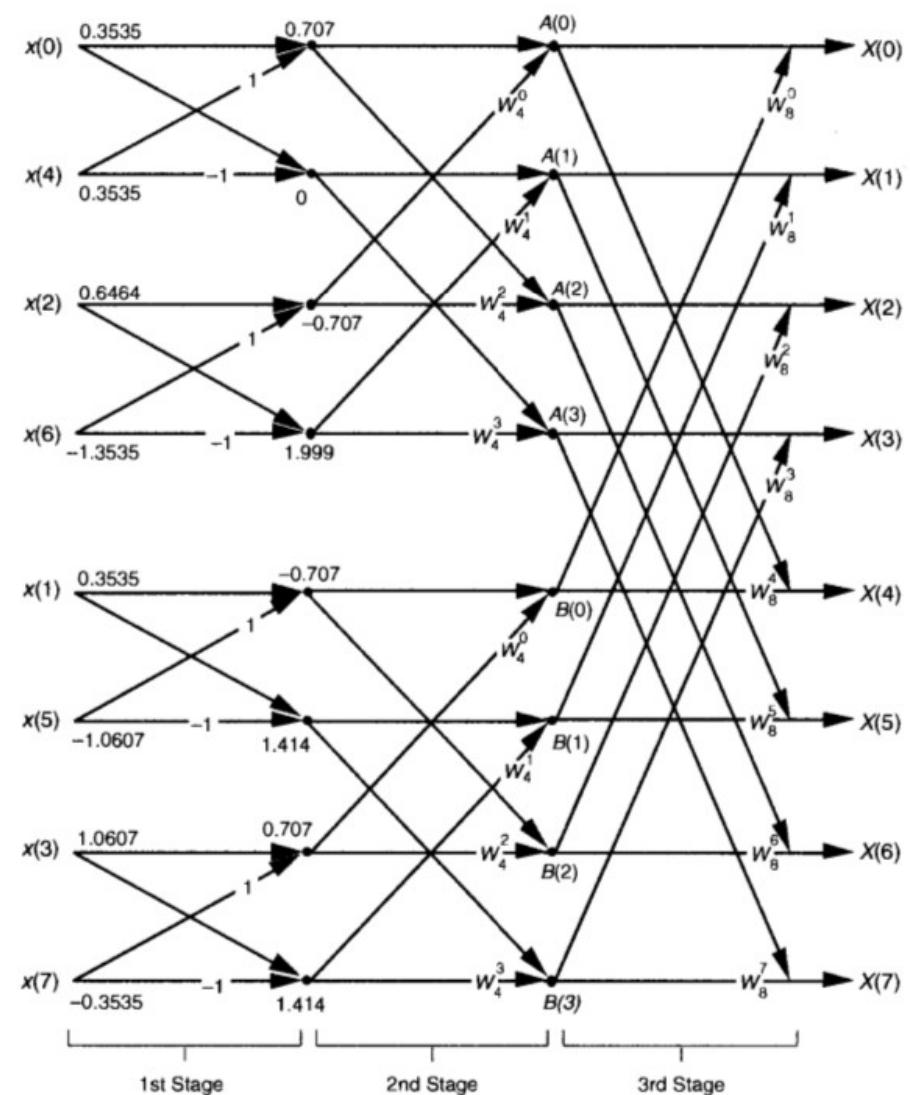
# Fast Fourier Transform (FFT)

$$X_k = \sum_{n=0}^{N-1} x_n e^{\frac{-i2\pi}{N} nk}$$

Discrete Fourier Transform (DFT)



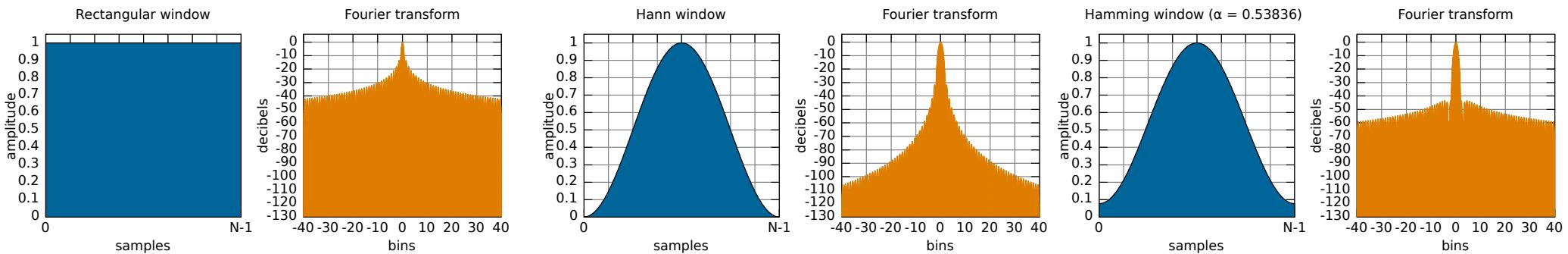
Radix-2 DIT 8-point  
Cooley-Tukey FFT



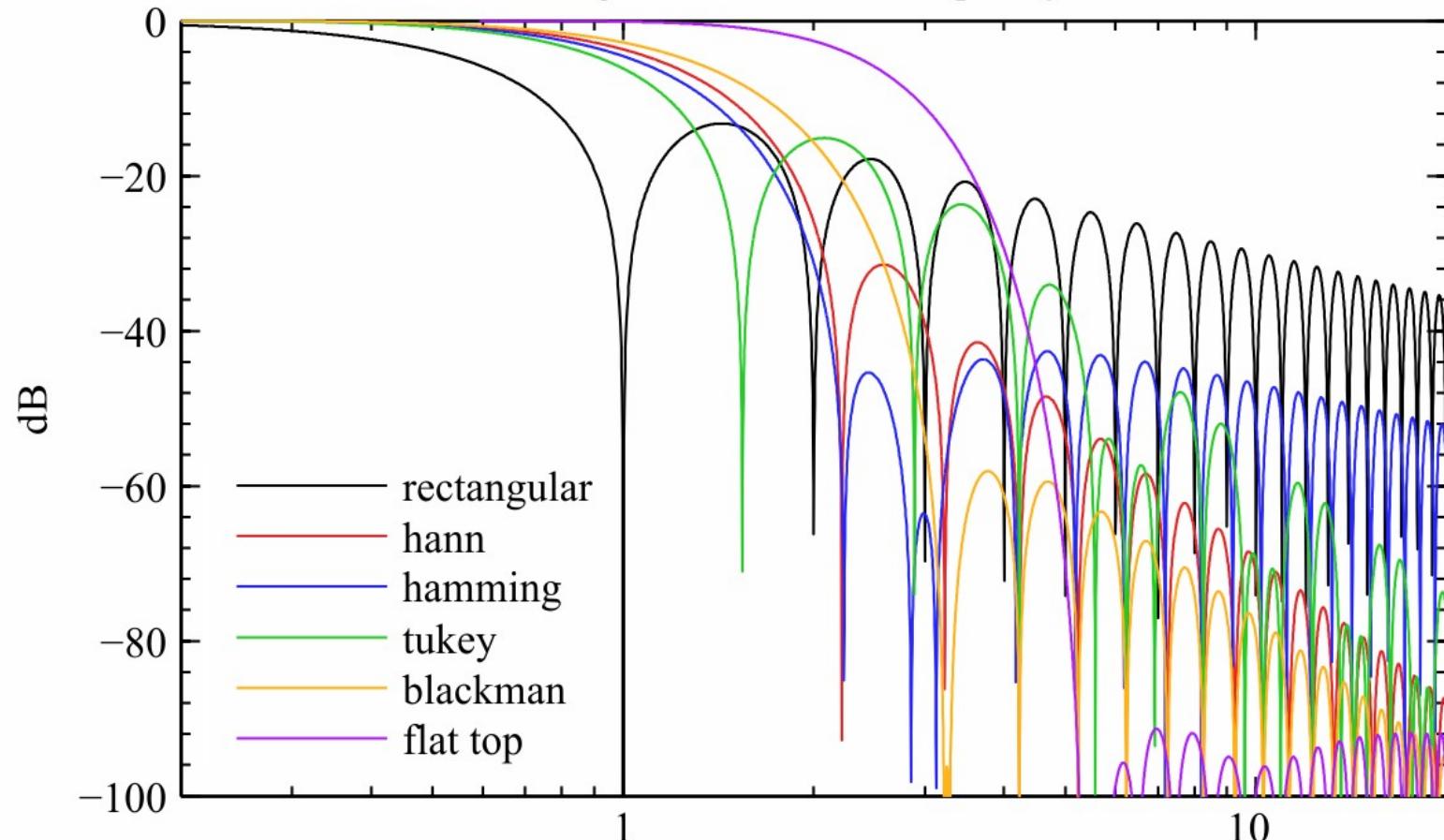
Almost all FFT implementations use a radix-2 system, so FFT of size  $2^N$  are ideal. Try to

32 avoid Fourier transforms of prime number size.

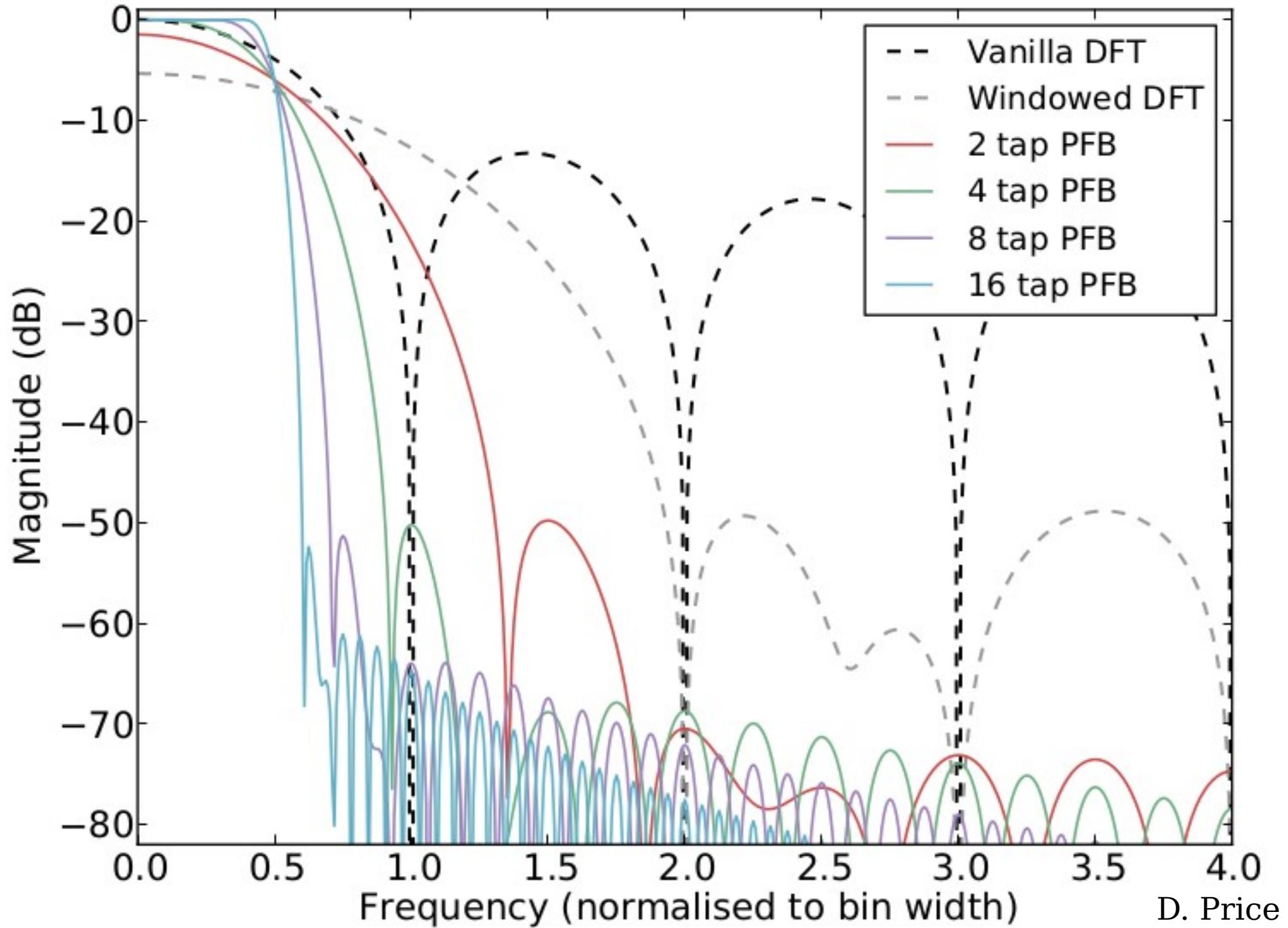
# Windowing Functions

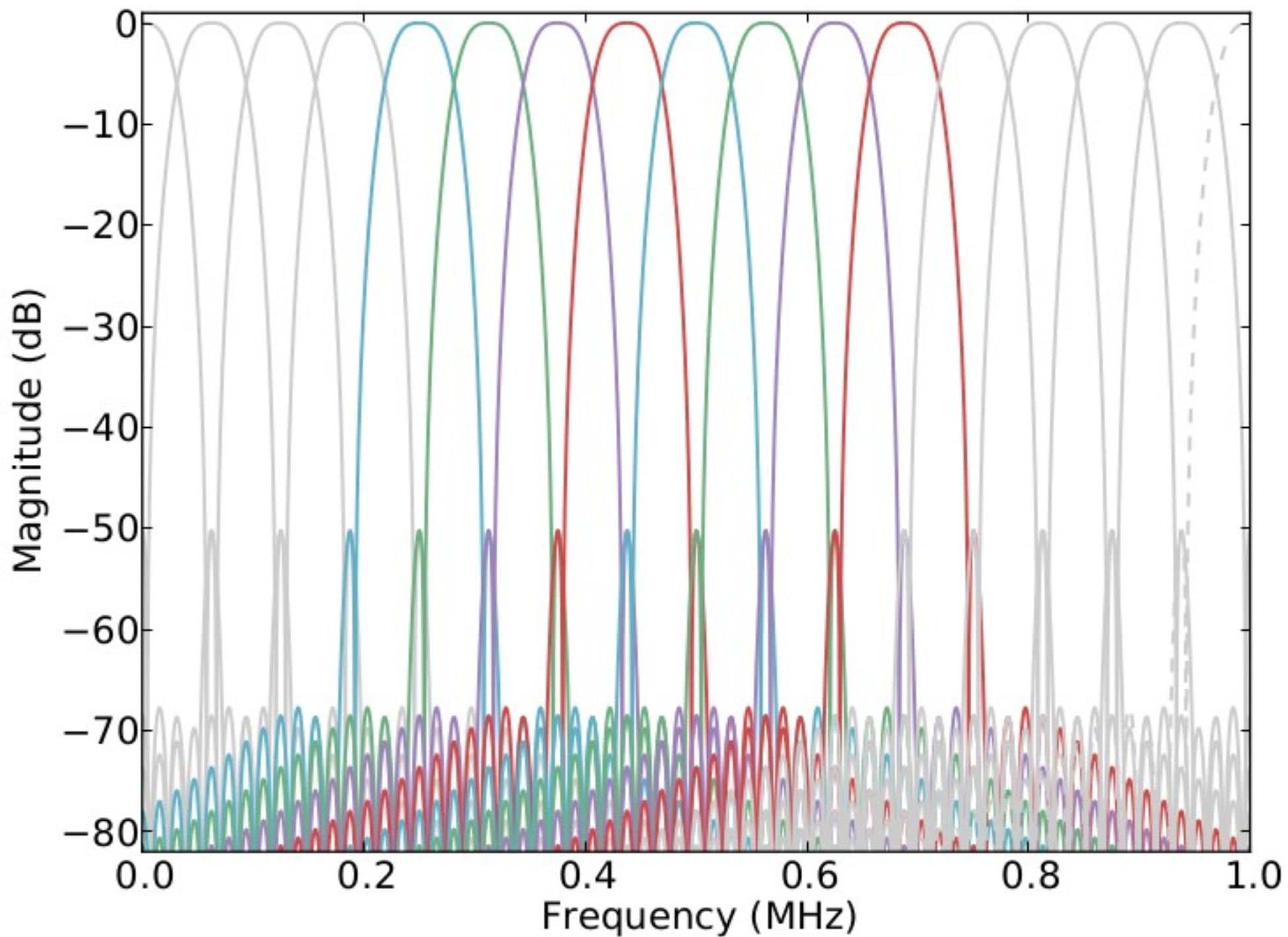


windowing functions in the frequency domain



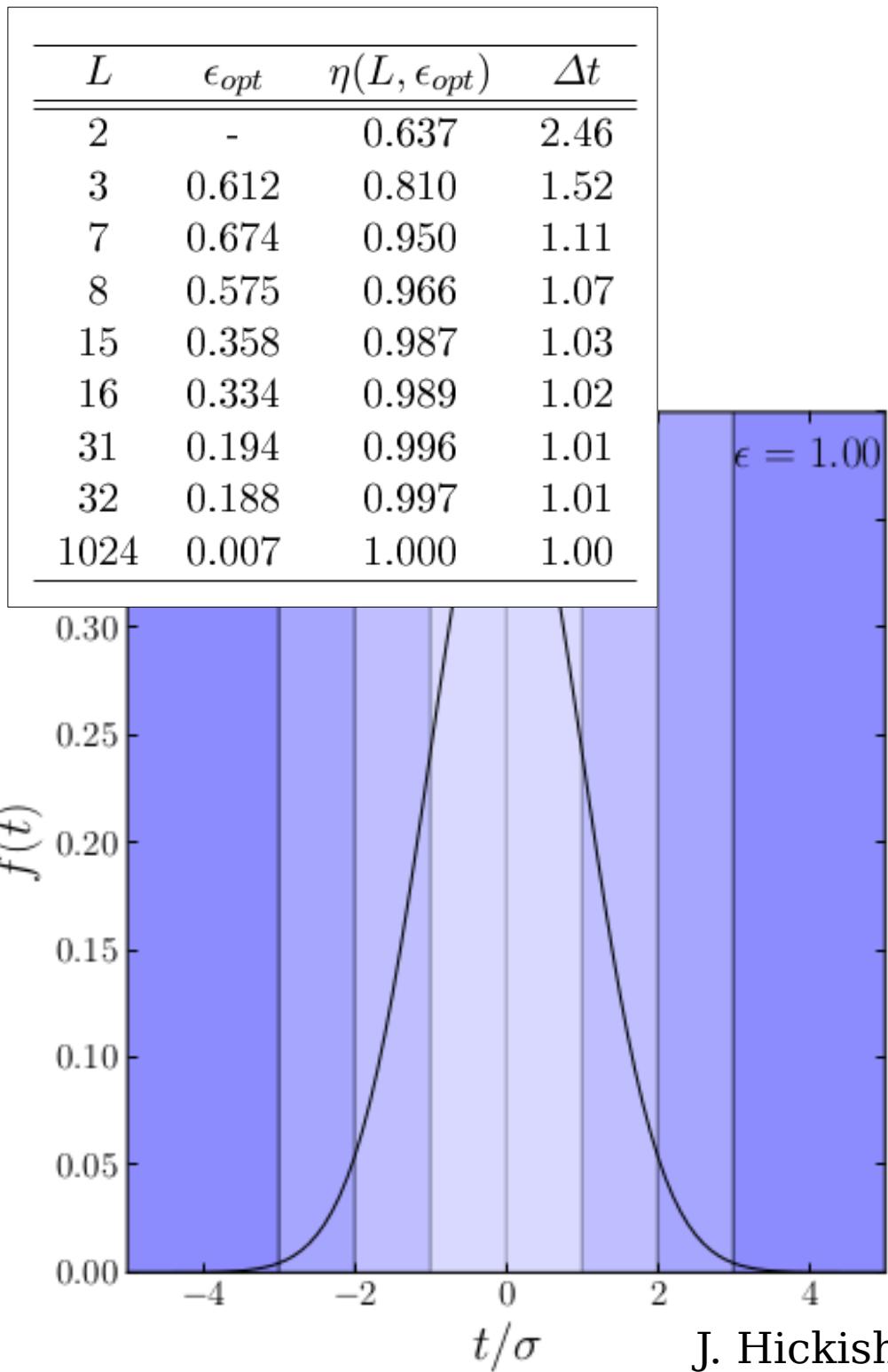
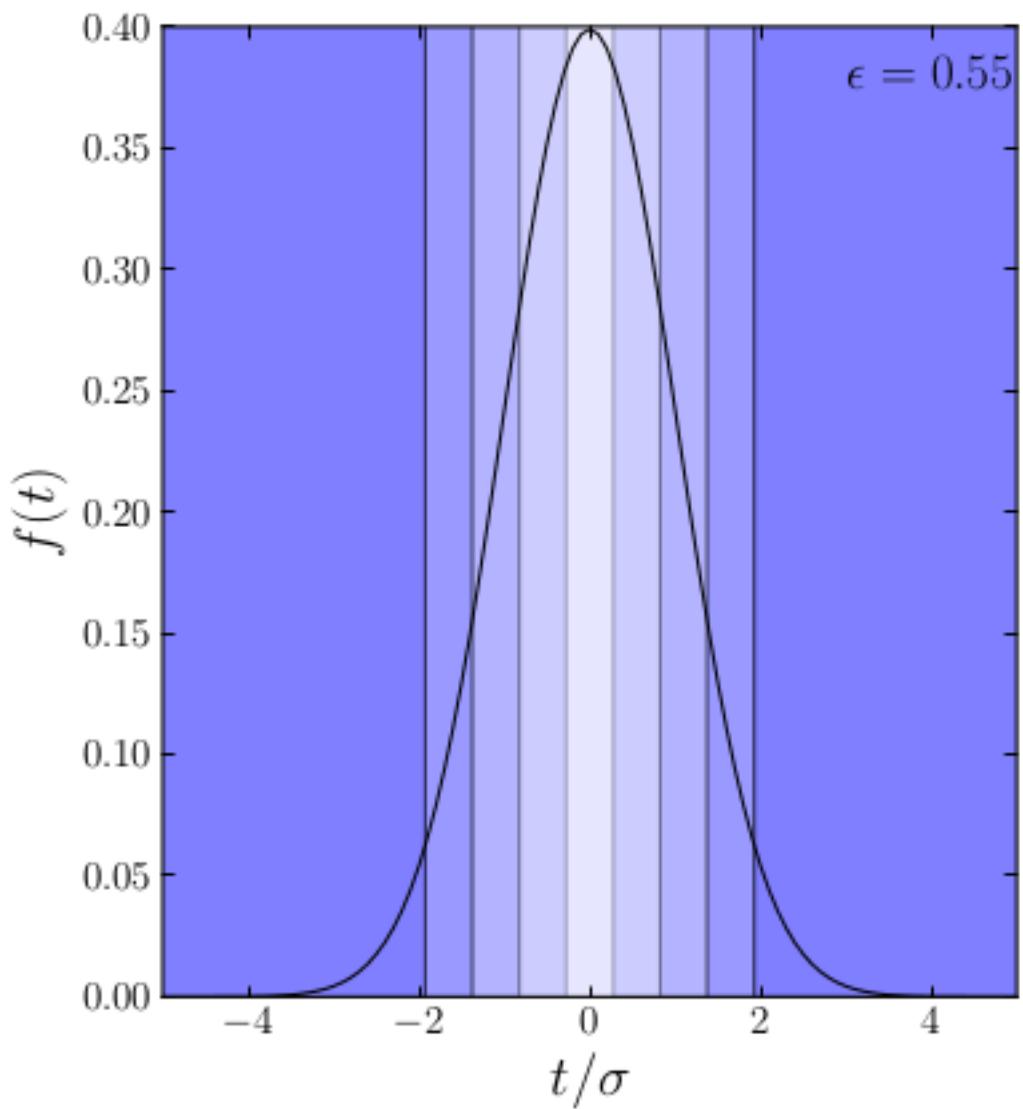
## Polyphase Filter Bank (PFB)



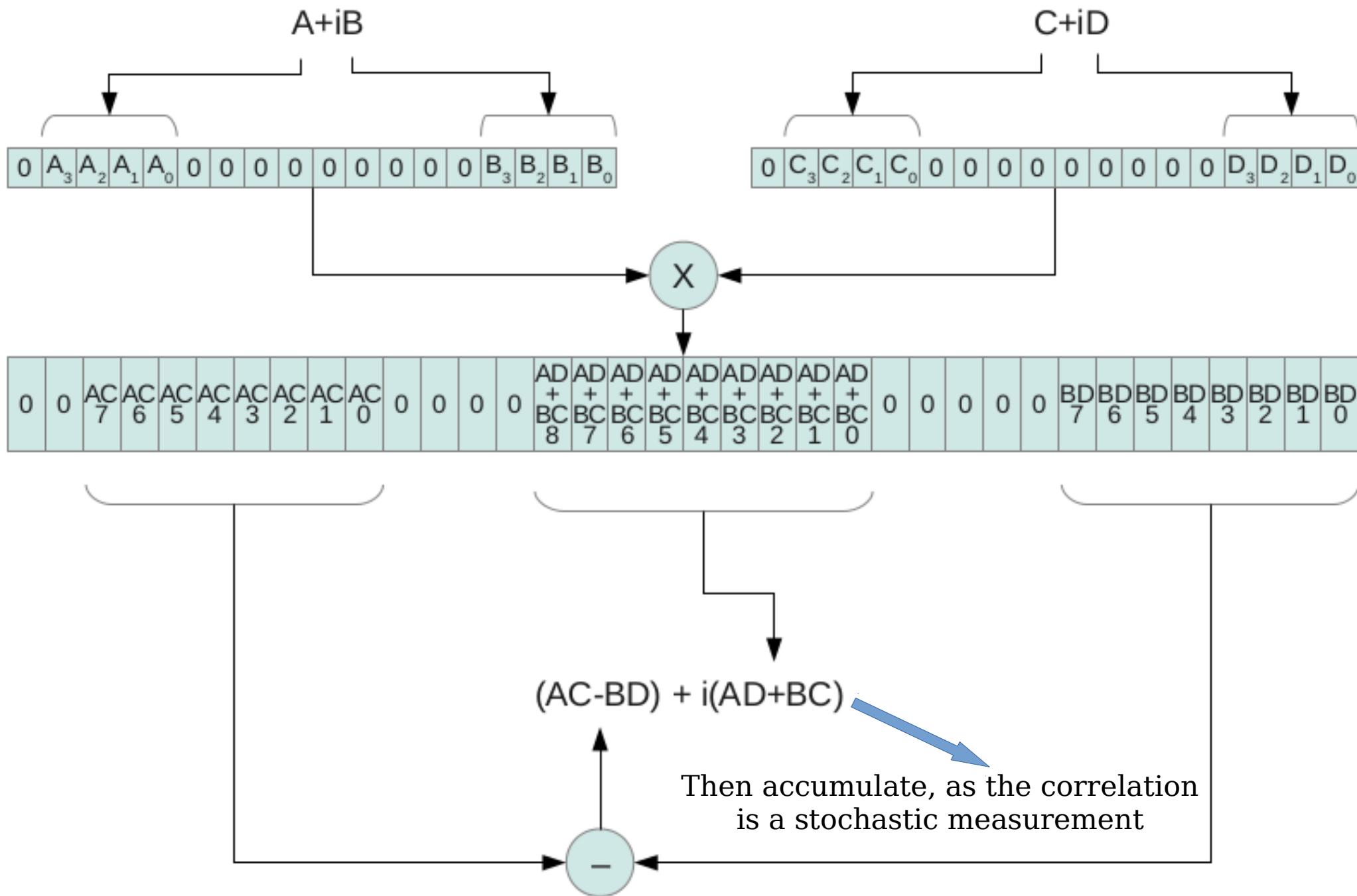


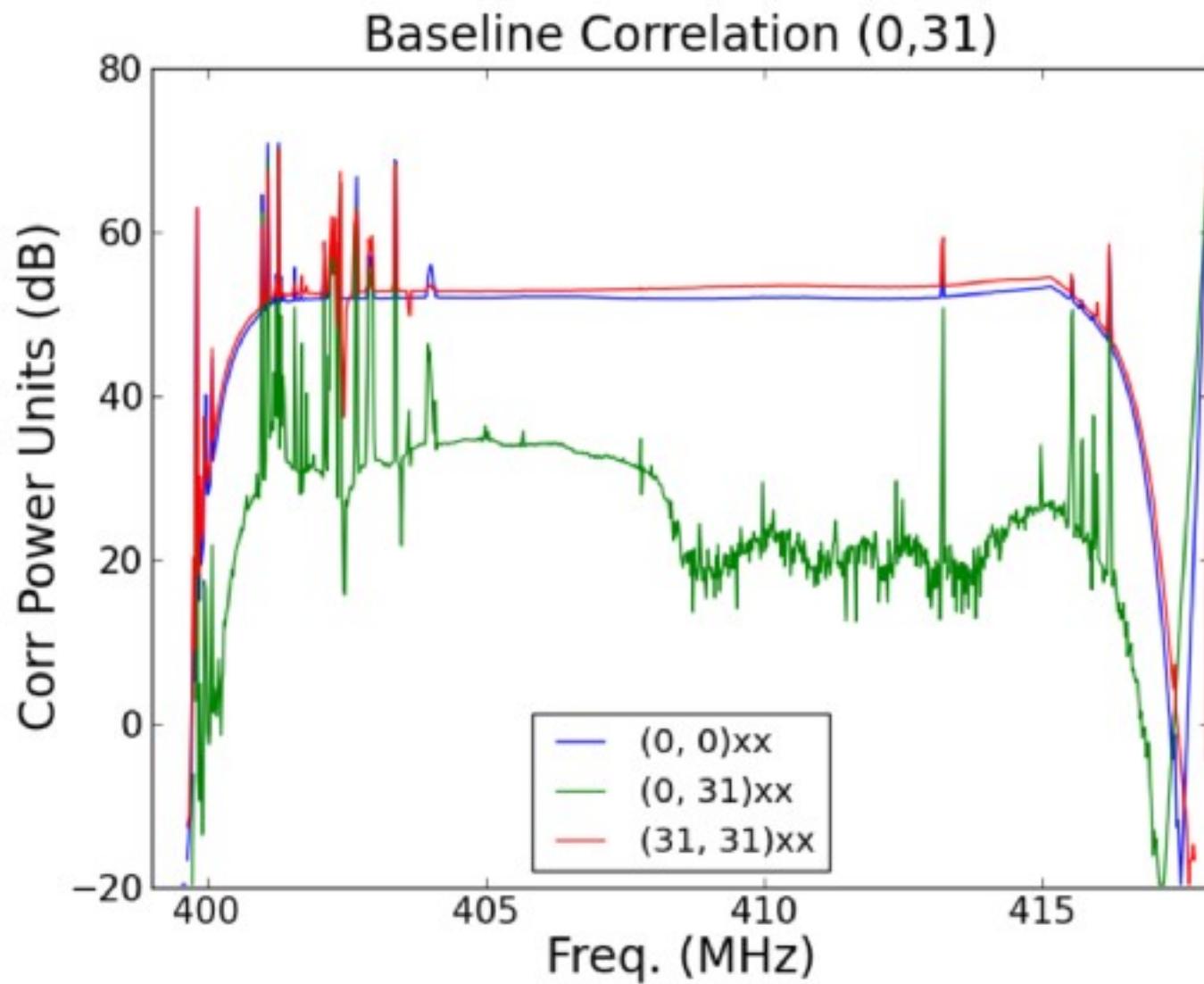
## Low bit resolution quantization and efficiency

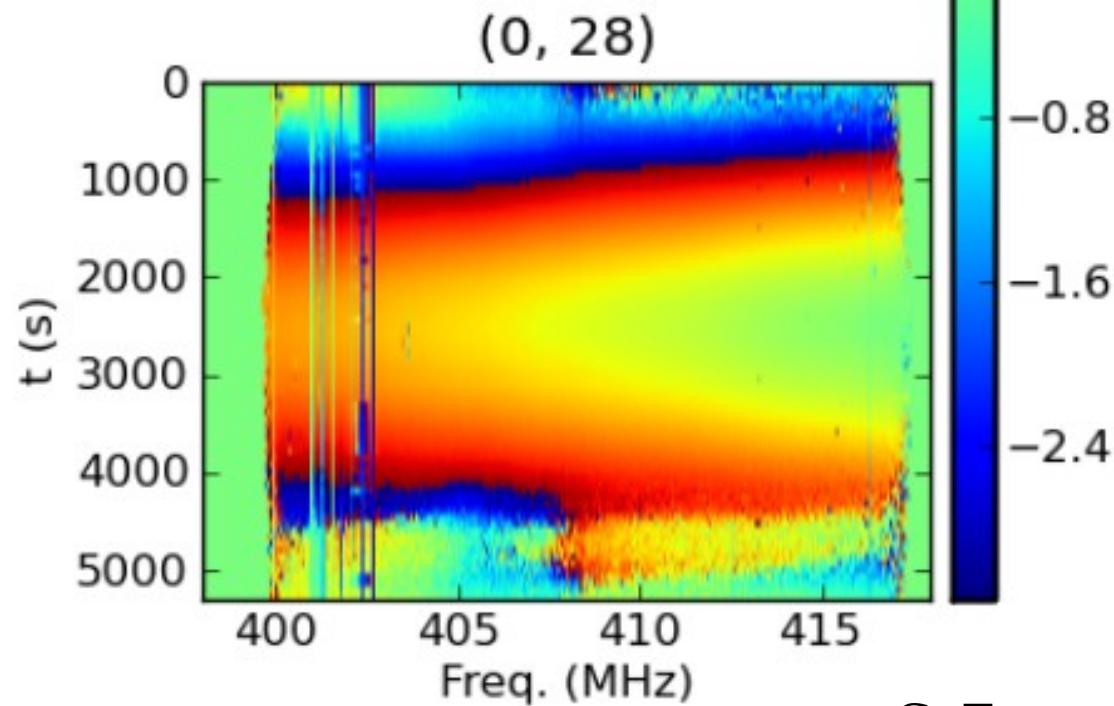
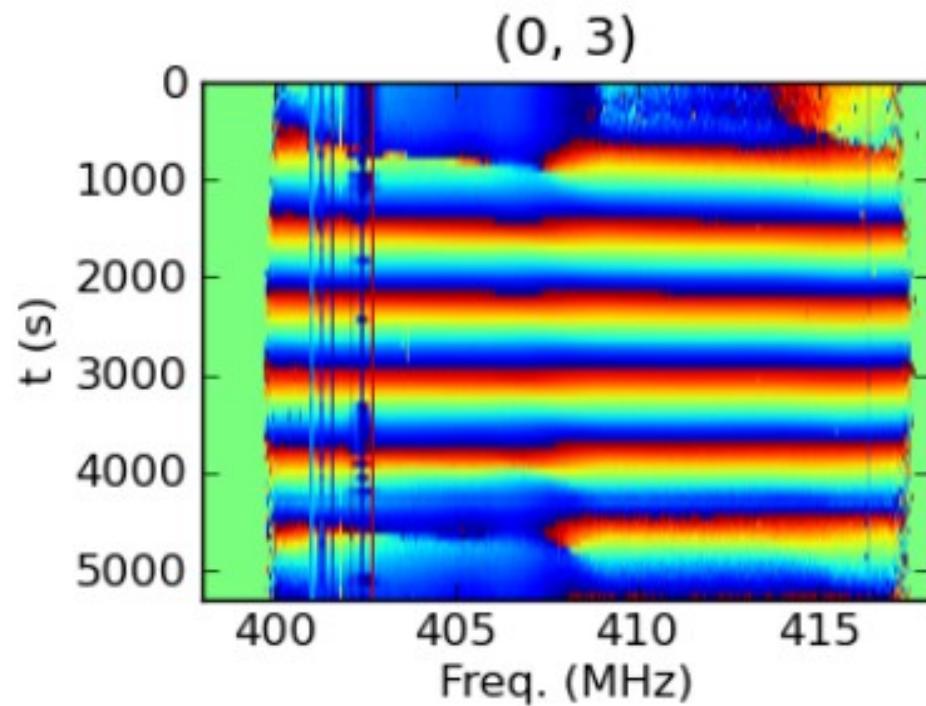
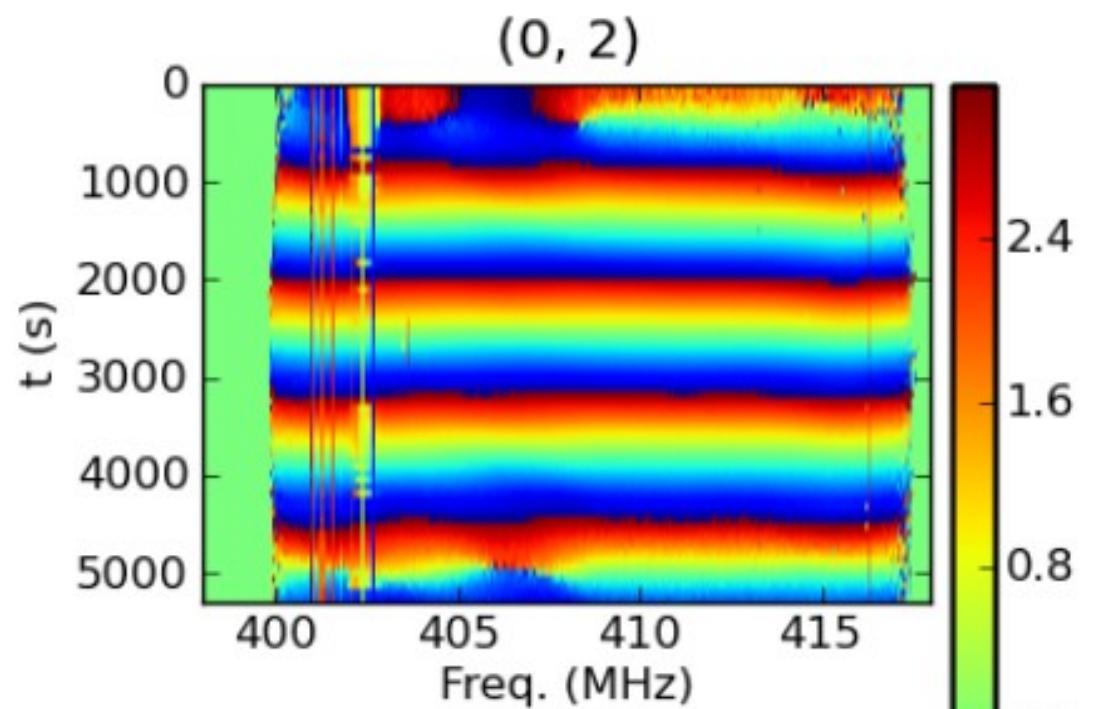
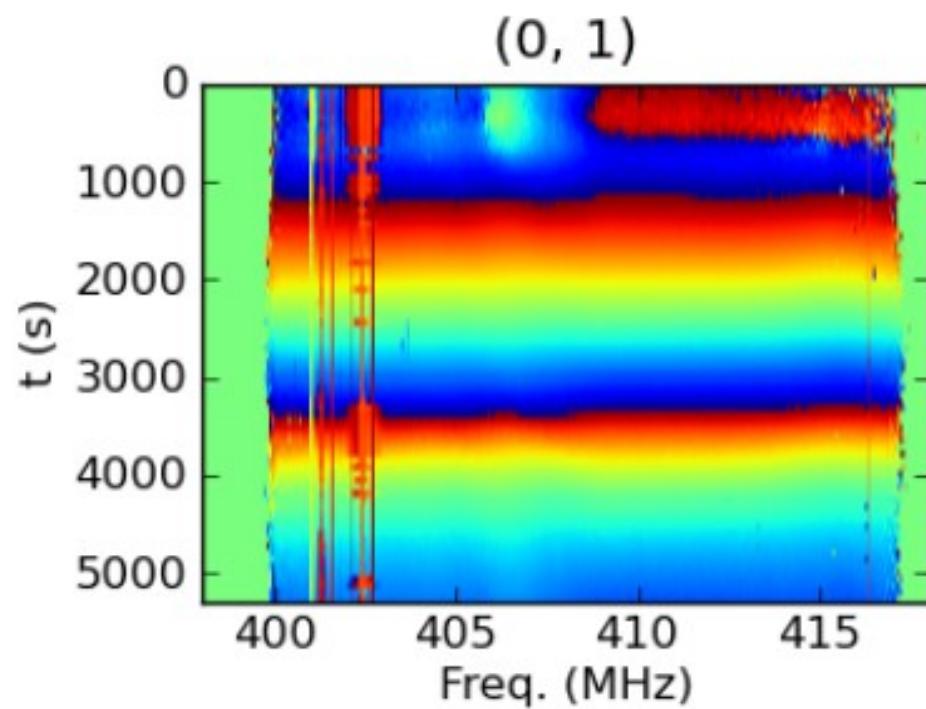
Key point: assuming a Gaussian signal (i.e. Astronomical signals), we only need 4 bits to get 98.9% efficiency



## Efficient 4-bit Multiplication in an FPGA

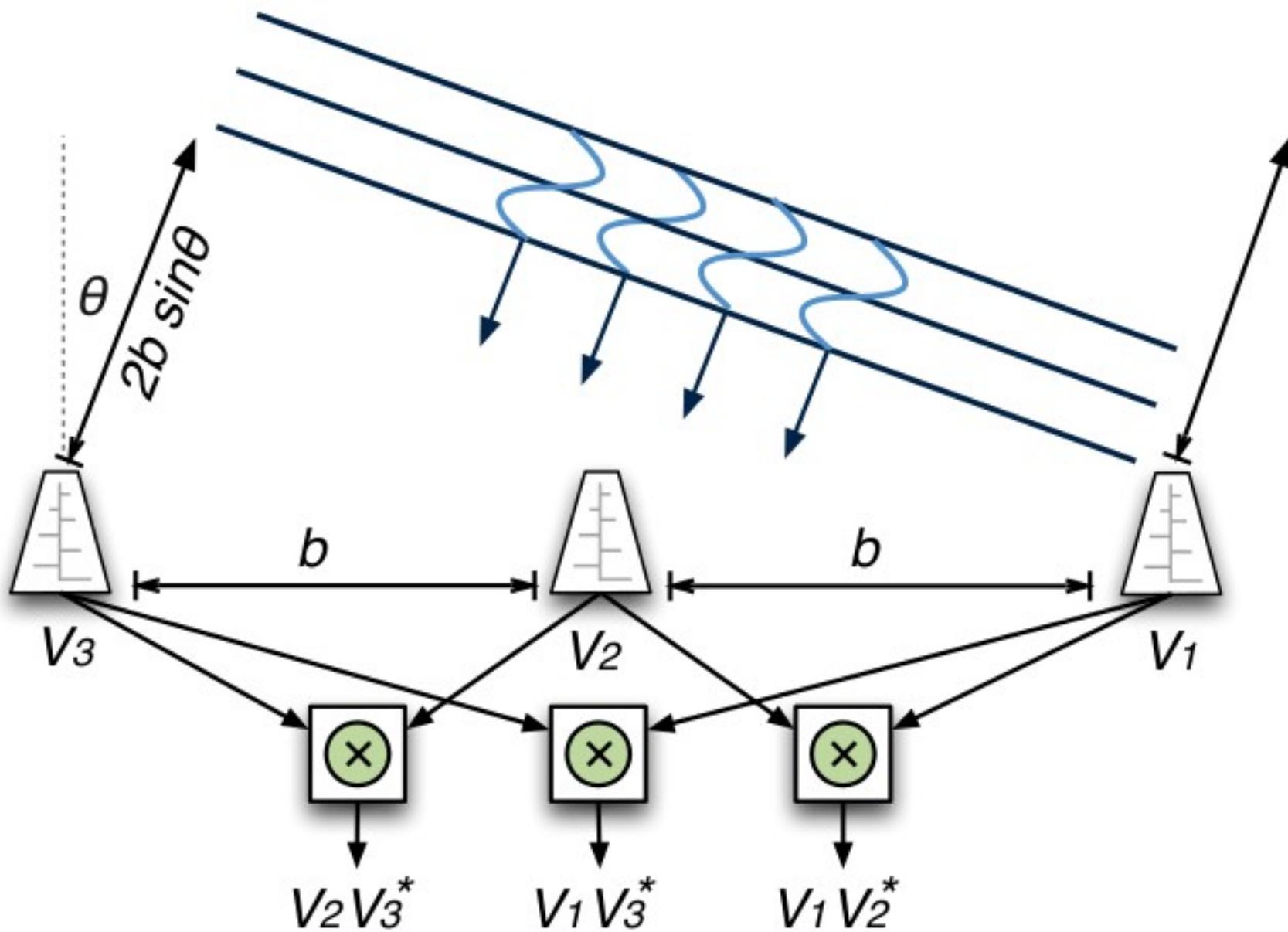




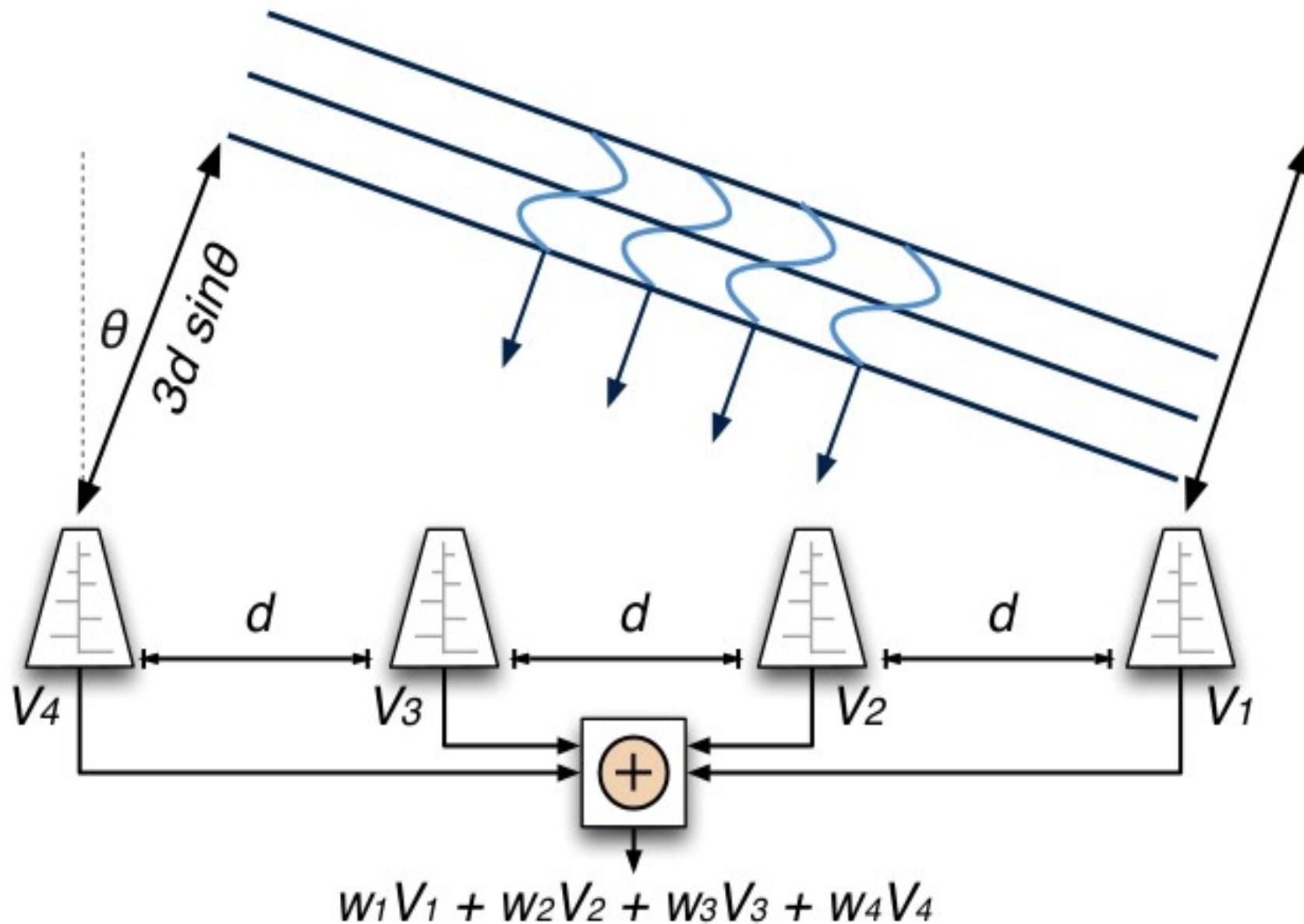


# Transiting Arrays, Aperture Arrays, and Phased Array Feeds

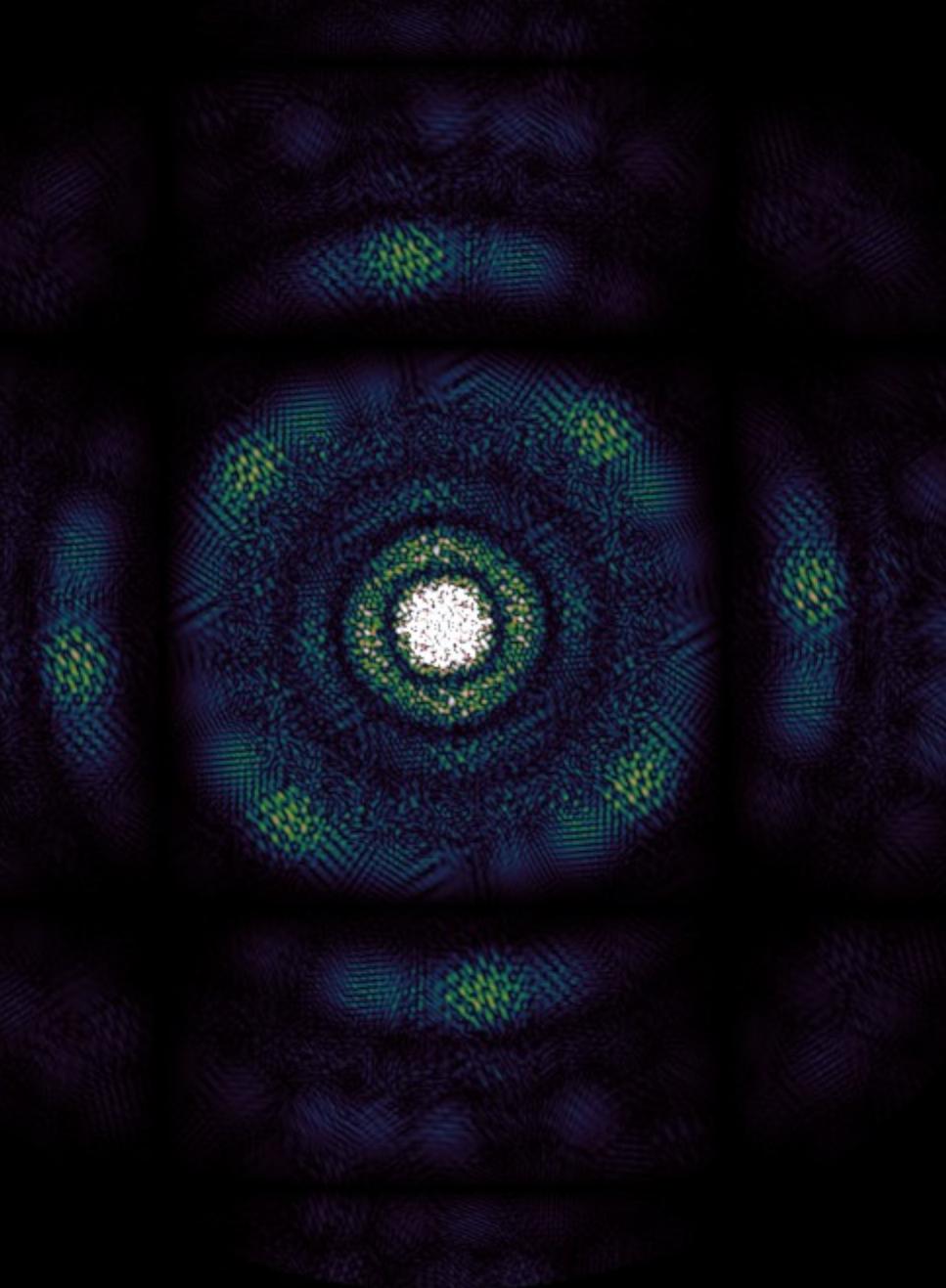
# Simple Interferometer Model



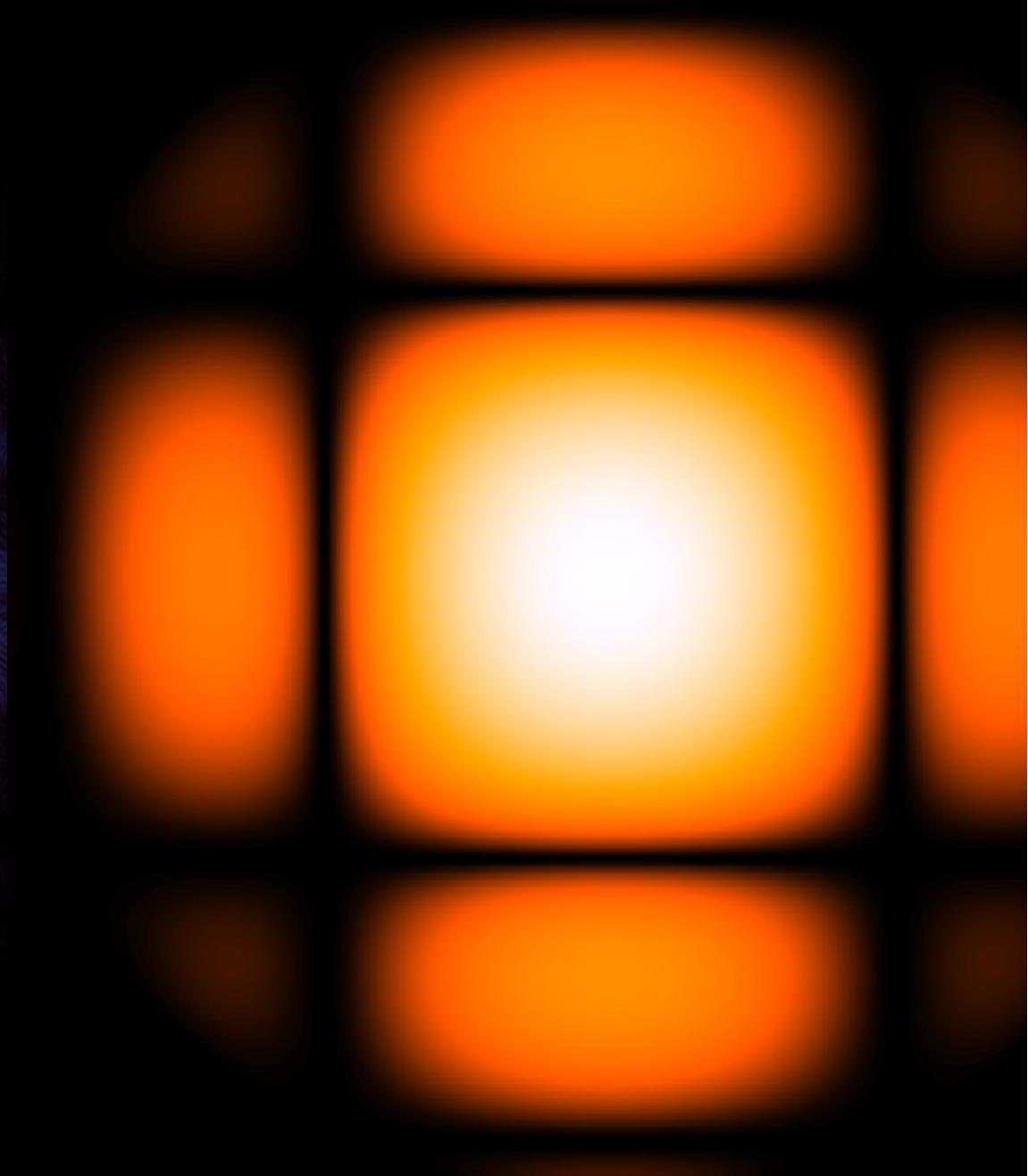
# Simple Beamformer Model



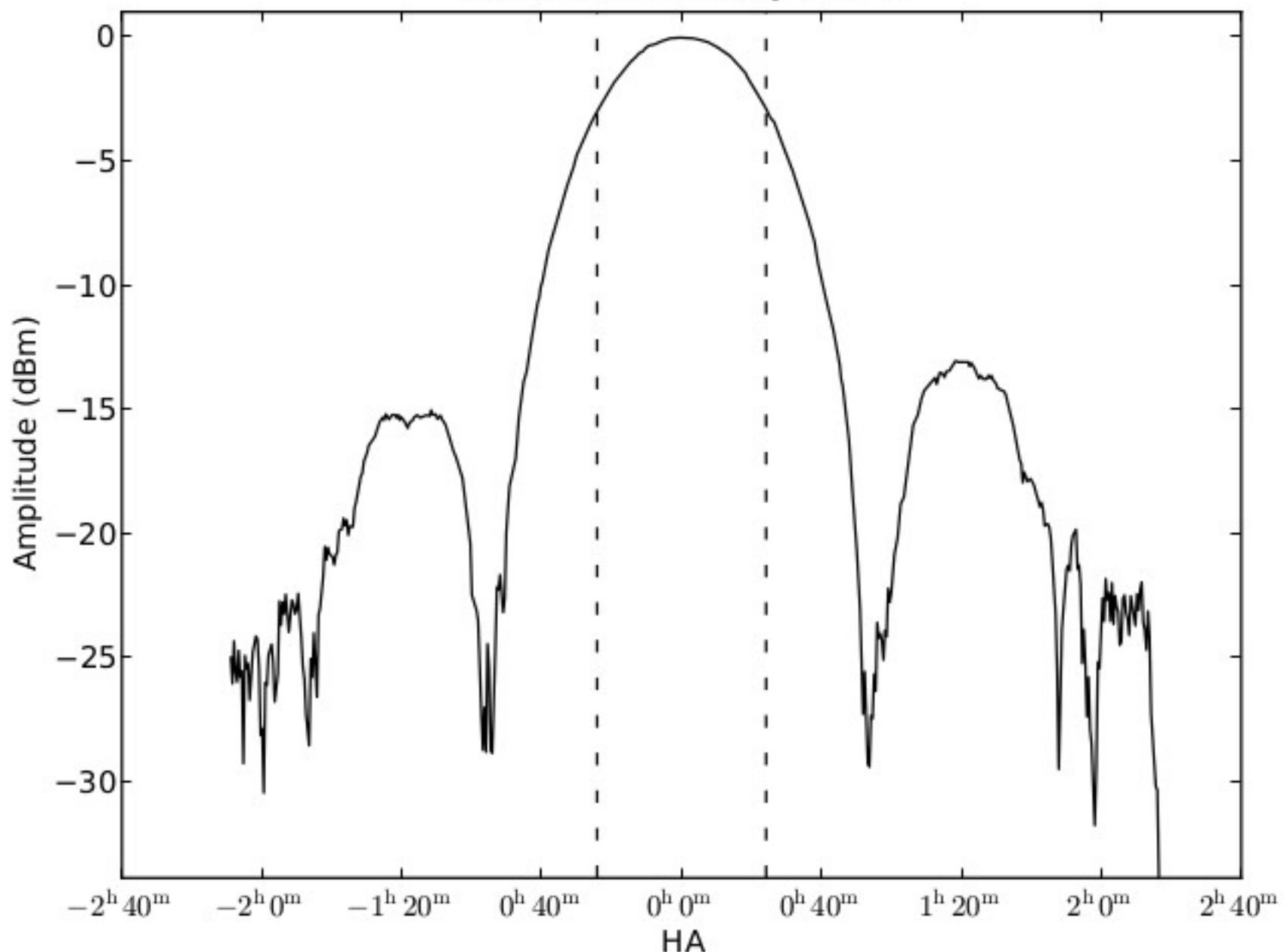
LOFAR Superterp  
HBA 150 MHz

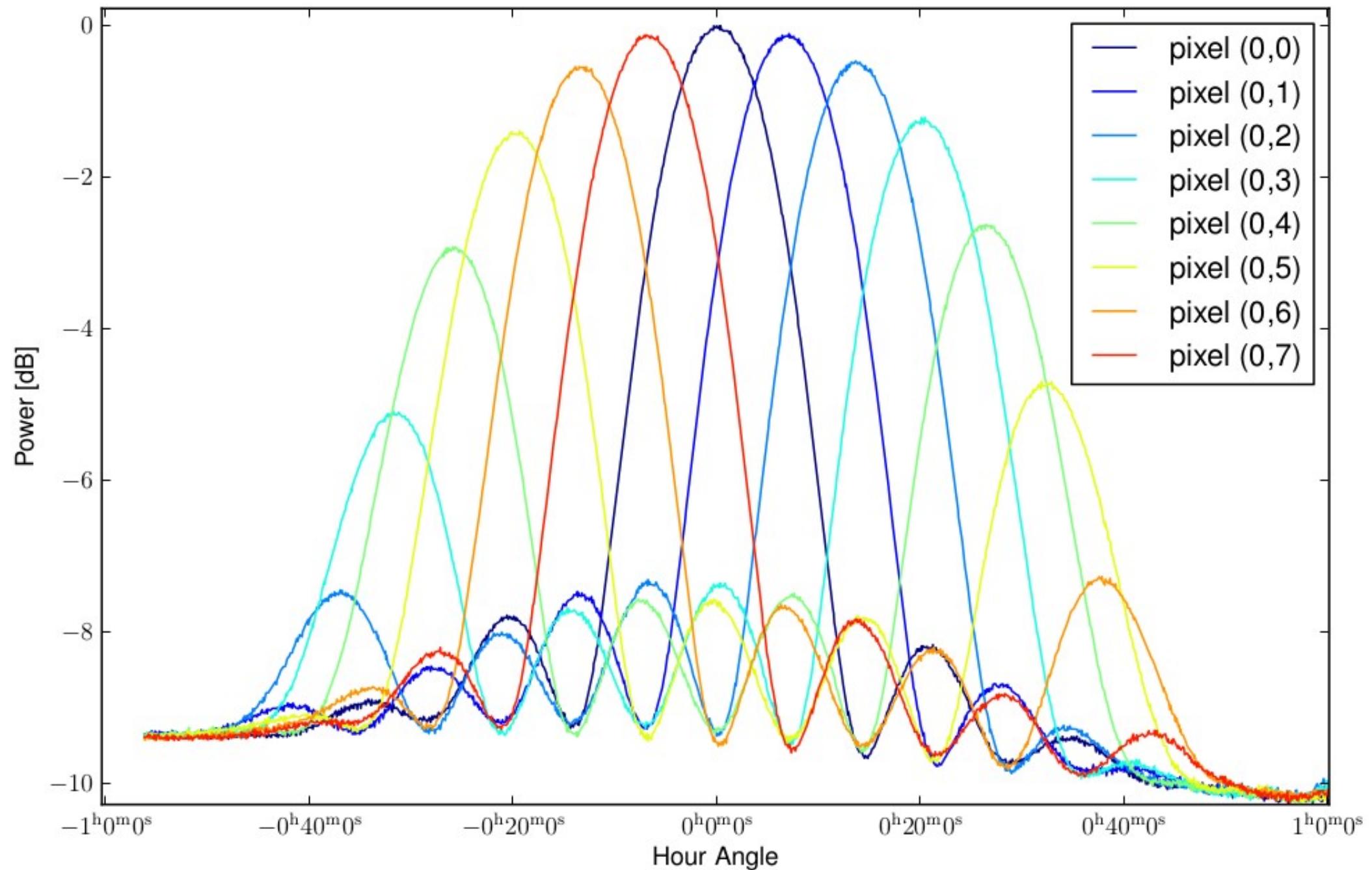


MWA Tile



### Measured Primary Beam





## Phased Array Feeds (PAFs)

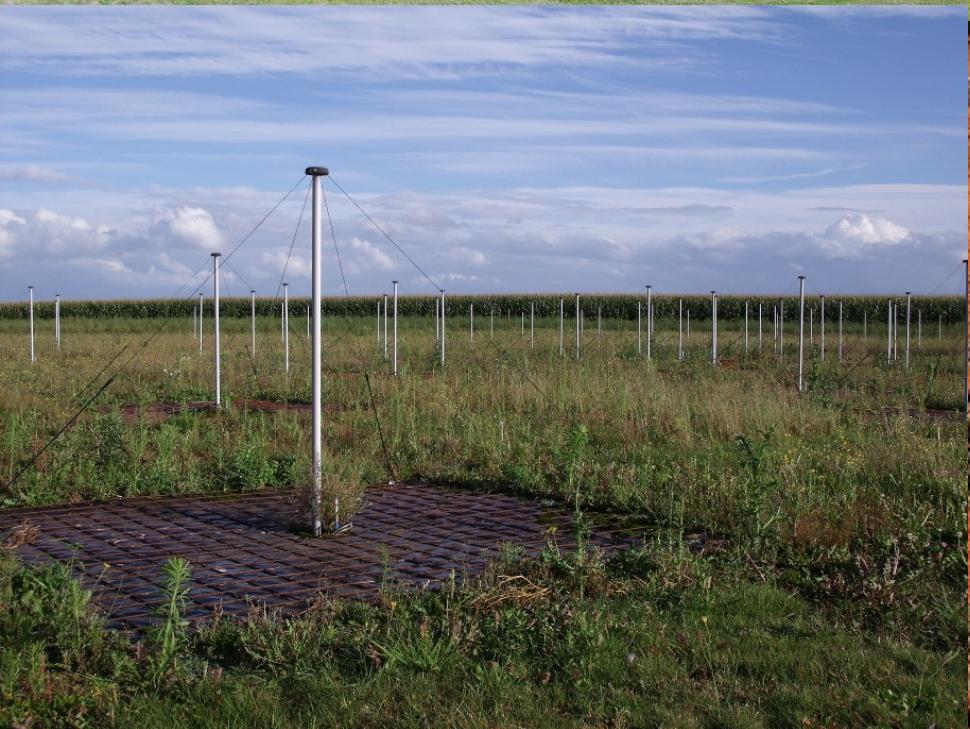


# Transiting Arrays



Aperture Arrays

LOFAR Superterp



# References

**Antennas and Aperture Arrays:**  
*Phased Array Antenna Handbook* : Mailloux  
*Antenna Theory* : Balanis

**Analogue Electronics:**  
*Microwave Engineering* : Pozar

**Digital Signal Processing:**  
*Understanding Digital Signal Processing* : Lyons  
*FFT and Its Applications* : Brigham