

In discussing the steady-state response with regards to a particular input, control engineers use the term "System Type"

System Type

Type O: Fixite corror to a step (position error)

Type 1 : fixite error to a ramp (velocity error)

Type Z ? Fivite error to a parabola (acaleration error)

This system is type I with respect to the reference

post Xx-8

post Xx-8

Ramp input

Parabolic input

To determine system type for a writy feedback connection (no blocks in the feedback loop), you can look at the loop gain or loop transfer function

$$L(s) = D(s) G(s)$$

$$= L_0(s) \qquad n \text{ integrators mean a}$$

$$\overline{S^n} \qquad \overline{System \text{ type of } n}$$

$$E(s) = \frac{1}{1 + L(s)} \qquad R(s) = \frac{k!}{5^{K+1}} \text{ for } r(t) = t^K$$

$$\frac{1.m}{t \to \infty} e(t) = \lim_{S \to 0} S E(s) = \lim_{S \to 0} \frac{1}{1 + L(s)} \cdot S \cdot \frac{K!}{5k+1}$$

$$= \lim_{S \to 0} \frac{1}{1 + \frac{L_0(s)}{5n}} \cdot \frac{K!}{5k}$$

= 11m 5n K! = 0 if n7K

=> n is the system type

To be on the safe side, you can always use the final value theorem to check instead of nemembering a particular formula. The Key thing to understand from this is that system type is related to the number of integrators in the 100p transfer function—the more integrators, the water the system type.

In addition to looking at the reference input; it is also possible to characterize the system type with regards to a disturbance. This gives some measure of the disturbance rejection capability of the system.

 $\frac{E(s)}{W(s)} = \frac{G(s)}{1 + D(s)G(s)} = \frac{1}{ms^2 + bs + K}$

ess = 1 m s for a step change Am pond grade

=> The system is type o with respect to disturbance.

System type does not depend upon the control gaing (in this case, K) chosen. It is instead related to the structure of the plant and controller. If we want to change system type, we need to change the controller structure.

How can we change if to track an accelerating / decelerating vehicle and reject disturbances?

Integral Control

The system is type I with regards to reference reputs.

=> Add an integrator to L(3) = D(3) G(5)

PI controller: D(s) = Kp + KI = Kps + KI

This means U(s) = D(s) E(s) or the sedt

If the initial error is quite large, the integral of the error can be huge, resulting in a large overshoot. This effect is known as integration wind-up and is something to be coneful about when using integral control.

With the integral controller, the loop gain is

 $\frac{E(s)}{R(s)} = \frac{1}{1 + \frac{K\rho S + K_{Z}}{5^{2}(mS + b)}} = \frac{S^{2}(mS + b)}{mS^{3} + bS^{2} + K\rho S + K_{Z}}$

For a ramp, the steady-state error is given by: $E(s) = \frac{1.\text{m}}{s \neq 0} s \cdot \frac{s^2 cms + b}{ms^2 + bs^2 + Kps + K_I} \cdot \frac{1}{s^2} = 0$

So the system will have zero error to a ramp, for a parabola characteristic of an acceleration or decelerating lead vehicle:

 $E(s) = \frac{1}{500} \cdot \frac{s^2(m_5+b)}{m_5^3+b_5^2+Kp_5+Kz} \cdot \frac{z}{5^3} = \frac{b}{K_I}$

KI can be tuned to give acceptable error so the cars don't collède.

For the disturbance:

 $\frac{E(s)}{W(s)} = \frac{s(ms+b)}{1 + \frac{Kps+KI}{s^2(ms+b)}} = \frac{s}{ms^3+bs^2+Kps+KI}$

So for a step change in road grade:

E(s) = 50 5 · ms3+652+Kps+Kz · 5 = 0

This all looks good but remember that the final value theorem is only valed for stable systems. Do we have a stable system? The characteristic equation is:

1 + D(s) G(s) = 0

ms3+652+Kp5+Kz =0

Is it enough to say that m, b, Kp, KI >0? If turns out it isht. We can always solve for the poles and check if they are in the left half plane but there is an analytical way based on the characteristic equation.