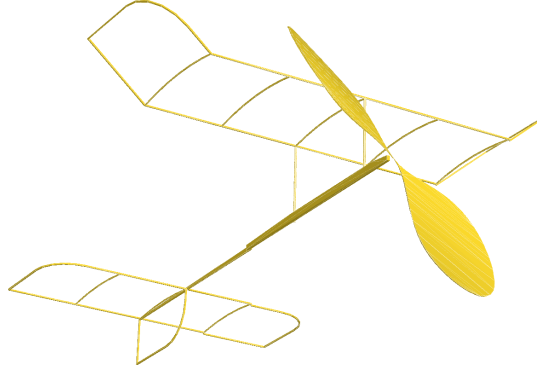


# Parabolized Navier-Stokes SOLution for Axisymmetric Ogive-Cylinder

Roie R. Black

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## 1 Derivation of the Cylindrical Navier Stokes Equations

In this section the system of governing equations given previously will be expanded in a cylindrical coordinate system.

For cylindrical  $(x, r, \phi)$  coordinates, the velocity vector  $\vec{V}$  is given by:

$$\vec{V} = u\hat{e}_x + v\hat{e}_r + w\hat{e}_\phi \quad (1)$$

where  $\hat{e}_x$ ,  $\hat{e}_r$ , and  $\hat{e}_\phi$  are the unit vectors.

The del  $\vec{\nabla}$  operator may be given as:

$$\vec{\nabla} = \hat{e}_x \frac{\partial}{\partial x} + \hat{e}_r \frac{\partial}{\partial r} + \frac{\hat{e}_\phi}{r} \frac{\partial}{\partial \phi} \quad (2)$$

Since the analysis that follows will require taking derivatives of the unit vectors, these expressions will be derived next.

The position vector  $\vec{r}$  may be written in cartesian coordinates as:

$$\begin{aligned} \vec{r} &= x\hat{i} + y\hat{j} + z\hat{k} \\ &= x\hat{i} + r \cos \phi \hat{j} + r \sin \phi \hat{k} \end{aligned} \quad (3)$$

Now the equations for the unit vectors are:

$$\hat{e}_x = \frac{\partial \vec{r}}{\partial x} = \hat{i} \quad (4)$$

$$\hat{e}_r = \frac{\partial \vec{r}}{\partial r} = \cos \phi \hat{j} + \sin \phi \hat{k} \quad (5)$$

$$\hat{e}_\phi = \frac{\partial \vec{r}}{\partial \phi} = -\sin \phi \hat{j} + \cos \phi \hat{k} \quad (6)$$

From these equations, the derivatives of the unit vectors can be found:

$$\frac{\partial \hat{e}_x}{\partial x} = \frac{\partial \hat{e}_x}{\partial r} = \frac{\partial \hat{e}_x}{\partial \phi} = 0 \quad (7)$$

$$\frac{\partial \hat{e}_r}{\partial x} = \frac{\partial \hat{e}_r}{\partial r} = 0 \quad (8)$$

$$\frac{\partial \hat{e}_r}{\partial \phi} = -\sin \phi \hat{j} + \cos \phi \hat{k} = \hat{e}_\phi \quad (9)$$

$$\frac{\partial \hat{e}_\phi}{\partial x} = \frac{\partial \hat{e}_\phi}{\partial r} = 0 \quad (10)$$

$$\frac{\partial \hat{e}_\phi}{\partial \phi} = -\cos \phi \hat{j} - \sin \phi \hat{k} = -\hat{e}_r \quad (11)$$

Using these expressions, the derivatives of a general vector function become:

$$\begin{aligned}
\frac{\partial \vec{F}}{\partial x} &= \frac{\partial F_1}{\partial x} \hat{e}_x + \frac{\partial F_2}{\partial x} \hat{e}_r + \frac{\partial F_3}{\partial x} \hat{e}_\phi \\
\frac{\partial \vec{F}}{\partial r} &= \frac{\partial F_1}{\partial r} \hat{e}_x + \frac{\partial F_2}{\partial r} \hat{e}_r + \frac{\partial F_3}{\partial r} \hat{e}_\phi \\
\frac{\partial \vec{F}}{\partial \phi} &= \frac{\partial F_1}{\partial \phi} \hat{e}_x + \left( \frac{\partial F_2}{\partial \phi} - F_3 \right) \hat{e}_r + \left( \frac{\partial F_3}{\partial \phi} + F_2 \right) \hat{e}_\phi
\end{aligned} \tag{12}$$

where  $F_1$ ,  $F_2$ , and  $F_3$  are the vector components.

### 1.1 Continuity Equation

The continuity equation will be expanded first:

$$\frac{D\rho}{Dt} + \rho \vec{\nabla} \cdot \vec{V} = 0 \tag{13}$$

$$\frac{\partial \rho}{\partial t} + \left( \vec{V} \cdot \vec{\nabla} \rho \right) + \rho \left( \vec{\nabla} \cdot \vec{V} \right) = 0 \tag{14}$$

$$\frac{\partial \rho}{\partial t} + u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial r} + \frac{w}{r} \frac{\partial \rho}{\partial \phi} + \rho \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial r} + \frac{1}{r} \frac{\partial w}{\partial \phi} + \frac{v}{r} \right) = 0 \tag{15}$$

After rearranging and combining terms, we get this form:

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x} (\rho u) + \frac{1}{r} \frac{\partial}{\partial r} (\rho v r) + \frac{1}{r} \frac{\partial}{\partial \phi} (\rho w) = 0 \tag{16}$$

### 1.2 Momentum Equation

Before expanding the momentum equation, it will be convenient to use the following for the shear stress matrix:

$$\vec{\tau} = \vec{\tau}_1 \hat{e}_x + \vec{\tau}_2 \hat{e}_r + \vec{\tau}_3 \hat{e}_\phi \tag{17}$$

Where:

$$\begin{aligned}
\vec{\tau}_1 &= \tau_{xx}\hat{e}_x + \tau_{xr}\hat{e}_r + \tau_{x\phi}\hat{e}_\phi \\
\vec{\tau}_2 &= \tau_{rx}\hat{e}_x + \tau_{rr}\hat{e}_r + \tau_{r\phi}\hat{e}_\phi \\
\vec{\tau}_3 &= \tau_{\phi x}\hat{e}_x + \tau_{\phi r}\hat{e}_r + \tau_{\phi\phi}\hat{e}_\phi
\end{aligned} \tag{18}$$

In this investigation, body forces will be neglected. The momentum equation becomes:

$$\begin{aligned}
\rho \frac{D\vec{V}}{Dt} &= \vec{\nabla} \cdot \vec{\bar{\tau}} \\
\rho \left\{ \frac{\partial \vec{V}}{\partial t} + \vec{V} \vec{\nabla} \vec{V} \right\} &= \vec{\nabla} \cdot \vec{\bar{\tau}}
\end{aligned} \tag{19}$$

or

$$\begin{aligned}
\rho \left\{ \frac{\partial u}{\partial t} \hat{e}_x + \frac{\partial v}{\partial t} \hat{e}_r + \frac{\partial w}{\partial t} \hat{e}_\phi + u \frac{\partial \vec{V}}{\partial t} \hat{e}_x + v \frac{\partial \vec{V}}{\partial r} \hat{e}_r + \frac{w}{r} \frac{\partial \vec{V}}{\partial \phi} \hat{e}_\phi \right\} \\
= \hat{e}_x \cdot \frac{\partial}{\partial x} \{ \vec{\tau}_1 \hat{e}_x + \vec{\tau}_2 \hat{e}_r + \vec{\tau}_3 \hat{e}_\phi \} \\
+ \hat{e}_r \cdot \frac{\partial}{\partial r} \{ \vec{\tau}_1 \hat{e}_x + \vec{\tau}_2 \hat{e}_r + \vec{\tau}_3 \hat{e}_\phi \} \\
+ \frac{\hat{e}_\phi}{r} \cdot \frac{\partial}{\partial \phi} \{ \vec{\tau}_1 \hat{e}_x + \vec{\tau}_2 \hat{e}_r + \vec{\tau}_3 \hat{e}_\phi \} \\
= \frac{\partial \vec{\tau}_1}{\partial x} + \frac{\partial \vec{\tau}_2}{\partial r} + \frac{1}{r} \left\{ \frac{\partial \vec{\tau}_3}{\partial \phi} + \vec{\tau}_2 \right\}
\end{aligned} \tag{20}$$

By expanding this last expression and rearranging terms, the following form results for the momentum equation

$$\begin{aligned}
& \rho \left\{ \frac{\partial u}{\partial t} \hat{e}_x + \frac{\partial v}{\partial t} \hat{e}_r + \frac{\partial w}{\partial t} \hat{e}_\phi + u \frac{\vec{V}}{\partial t} \hat{e}_x + v \frac{\vec{V}}{\partial r} \hat{e}_r + \frac{w}{r} \frac{\vec{V}}{\partial \phi} \hat{e}_\phi \right\} a \\
& + \rho u \left\{ \frac{\partial u}{\partial x} \hat{e}_x + \frac{\partial v}{\partial x} \hat{e}_r + \frac{\partial w}{\partial x} \hat{e}_\phi \right\} \\
& + \rho v \left\{ \frac{\partial u}{\partial r} \hat{e}_x + \frac{\partial v}{\partial r} \hat{e}_r + \frac{\partial w}{\partial r} \hat{e}_\phi \right\} \\
& + \frac{\rho w}{r} \left\{ \frac{\partial u}{\partial \phi} \hat{e}_x + \left( \frac{\partial v}{\partial \phi} - r \right) \hat{e}_r + \left( \frac{\partial w}{\partial \phi} + v \right) \hat{e}_\phi \right\} \\
& = \tau_{xx} \hat{e}_x + \left\{ \tau_{xr} \hat{e}_r + \tau_{x\phi} \hat{e}_\phi \right. \\
& \quad \left. \vec{\tau}_2 = \tau_{rx} \hat{e}_x + \tau_{rr} \hat{e}_r + \tau_{r\phi} \hat{e}_\phi \right. \\
& \quad \left. \vec{\tau}_3 = \tau_{\phi x} \hat{e}_x + \tau_{\phi r} \hat{e}_r + \tau_{\phi\phi} \hat{e}_\phi \right\} \\
& \hspace{15em} (21)
\end{aligned}$$

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## References

- W. Durand. *Aerodynamic Theory*, volume IV. Dover Publications, Inc, 1963.