



Power Quality Compensation for Smart Grids by Model-based Predictive Control

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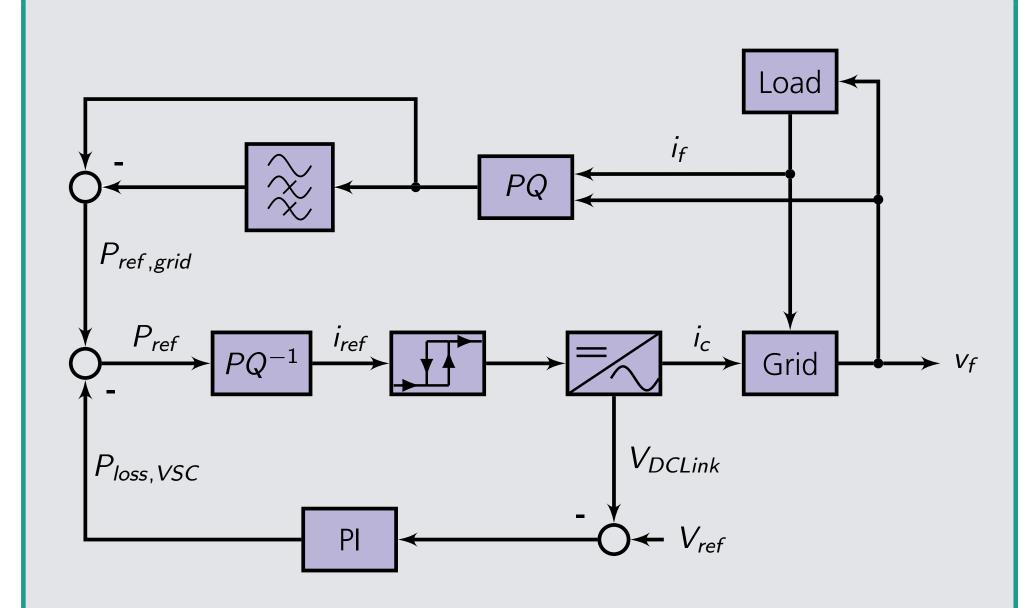
INTRODUCTION

- High order harmonics in the electrical grid introduced by switching converters need to be compensated to avoid damage and energy loss
- Classic active power filter (APF) controllers are capable of compensating harmonics, but are not flexible under variable load scenarios
- A classic well-tested method to compensate harmonics relies on the instantaneous reference frame (IRP) theory
- A novel approach: "Linear State Signal Shaping Model Predictive Control" (LSSS MPC), could be utilized to compensate harmonics using shape classes, without the need to design filters for different load scenarios

APPLICATION PROBLEM

- Could the LSSS MPC controller improve the grid quality compared to a standard IRP APF controller?
- A simulation is set up to evaluate both controller types under different load scenarios

CLASSIC IRP CONTROLLER



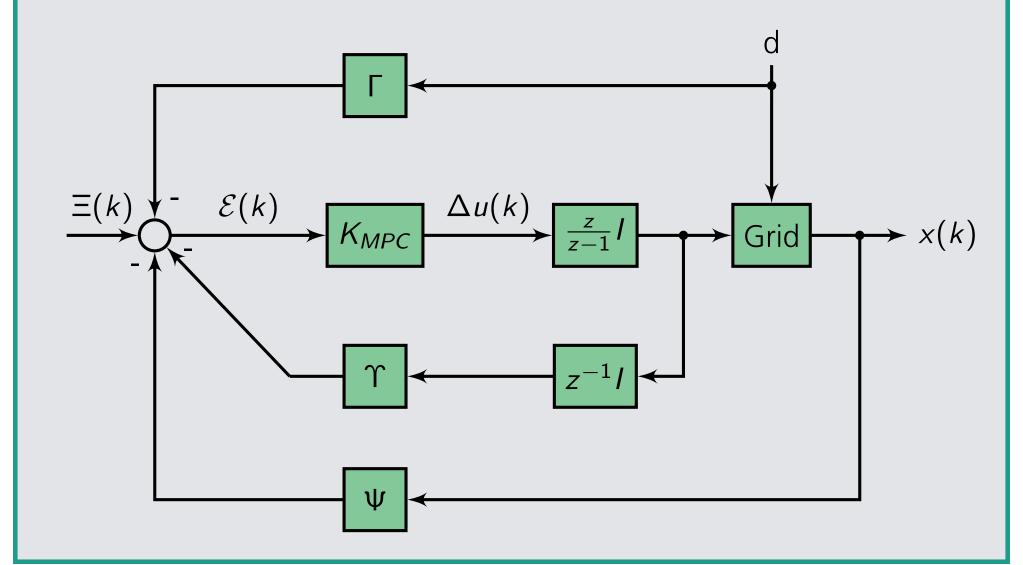
- Clarke and p-q transformation are used
- A high pass filter extracts harmonics
- A hysteresis band controller steers the voltage source converter

PREDICTIVE CONTROLLER

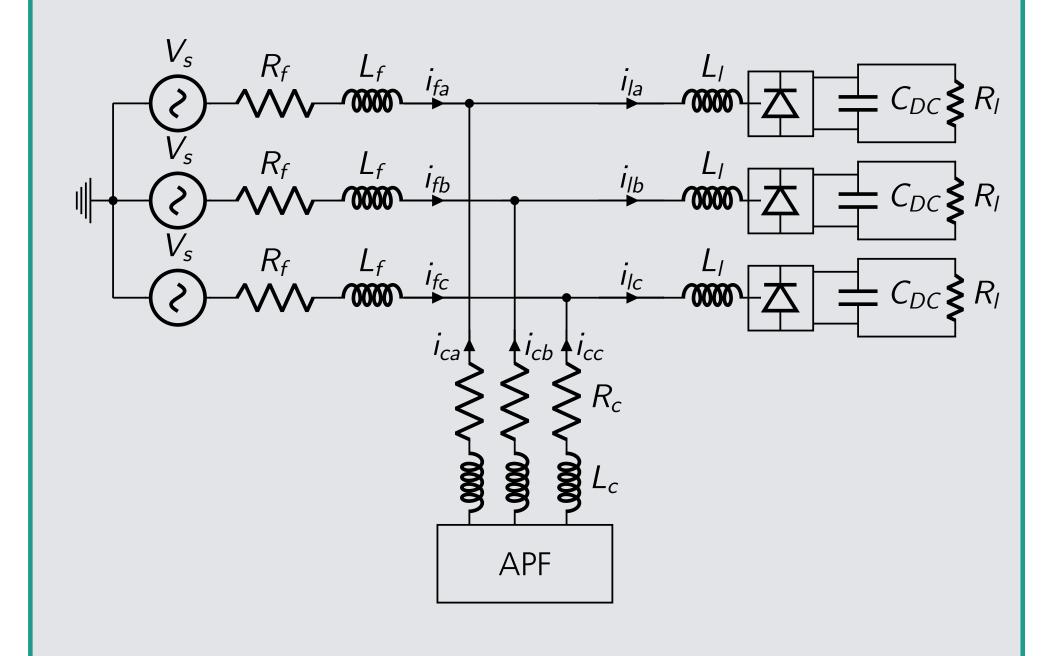
An MPC solves the optimization problem

$$\min_{\Delta U} \|\mathbf{X}(k) - \Xi(k)\|_{\mathbf{Q}}^2 + \|\Delta \mathbf{U}(k)\|_{\mathbf{R}}^2.$$

An internal model enables prediction. The unconstrained solution leads to a linear closed loop behaviour.



3-PHASE GRID MODEL



Active power filter in shunt configuration

 $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{E}\mathbf{d}(t)$

 $\mathbf{x}(t) = \begin{pmatrix} v_I & \frac{di_c}{dt} & \frac{di_l}{dt} \end{pmatrix}^\mathsf{T} \in \mathbb{R}^3 \qquad u(t) = \frac{\mathsf{d}^2 i_c}{\mathsf{d}t^2} \\ d(t) = \frac{\mathsf{d}^2 i_l}{\mathsf{d}t^2}$

WHITE-BOX MODELING

Linear state space model of the grid

LINEAR SHAPE CLASS

The shape of a sine wave is described by the homogeneous ODE

$$\frac{\mathrm{d}^2 x(t)^2}{\mathrm{d}t} + \omega^2 x(t) = 0$$

and approximated in discrete time with

$$\frac{\left(2+\omega^2 t_s^2\right) x(k)-5 x(k+1)+4 x(k+2)-x(k+3)}{t_s^2}=0.$$

From this difference equation the *linear* shape class³ V is given as

$$\mathbf{V} = \frac{1}{t_2^2} \left(2 + (\omega t_s)^2 \quad 5 \quad 4 \quad -1 \right) \in \mathbb{R}^{1 \times 4} .$$

The state error weight matrix Q is built using V by transferring the control goal to the optimization problem

$$\min_{\mathbf{X}(k)} (\mathbf{VX}(k))^2$$
,

where

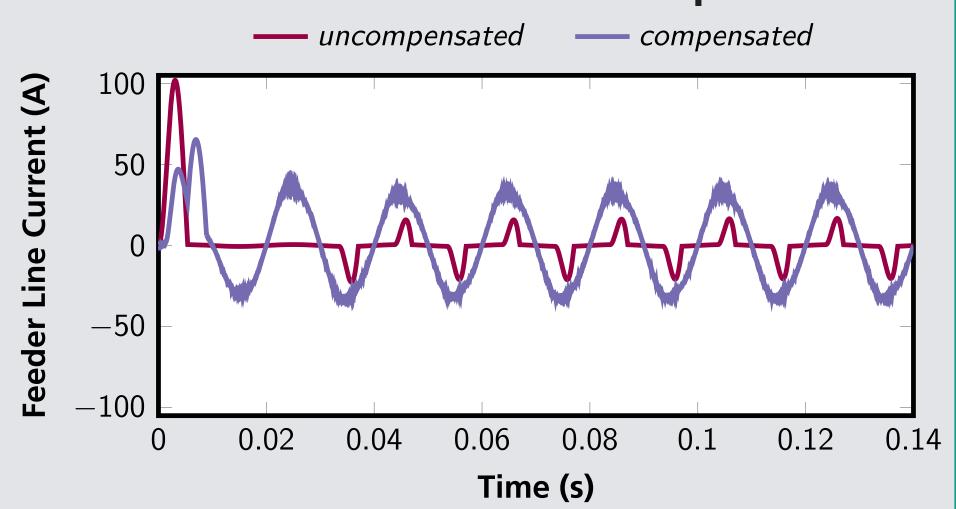
$$X(k) = (x(k) x(k+1) x(k+2) x(k+3))^{T}$$

for all times k.

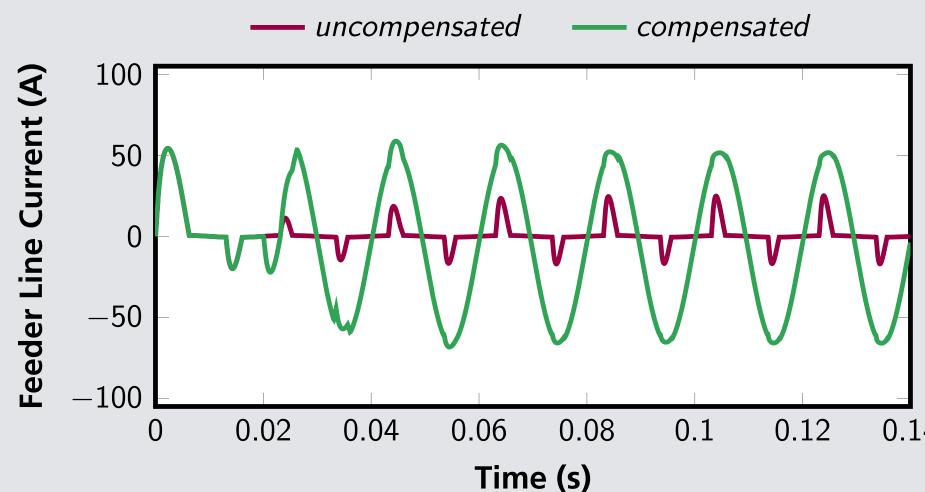
³Cateriano Yáñez, C., Pangalos, G., and Lichtenberg, G. (2018). An approach to linear state signal shaping by quadratic model predictive control. In *European Control Conference (ECC) 2018*

SIMULATION STUDIES

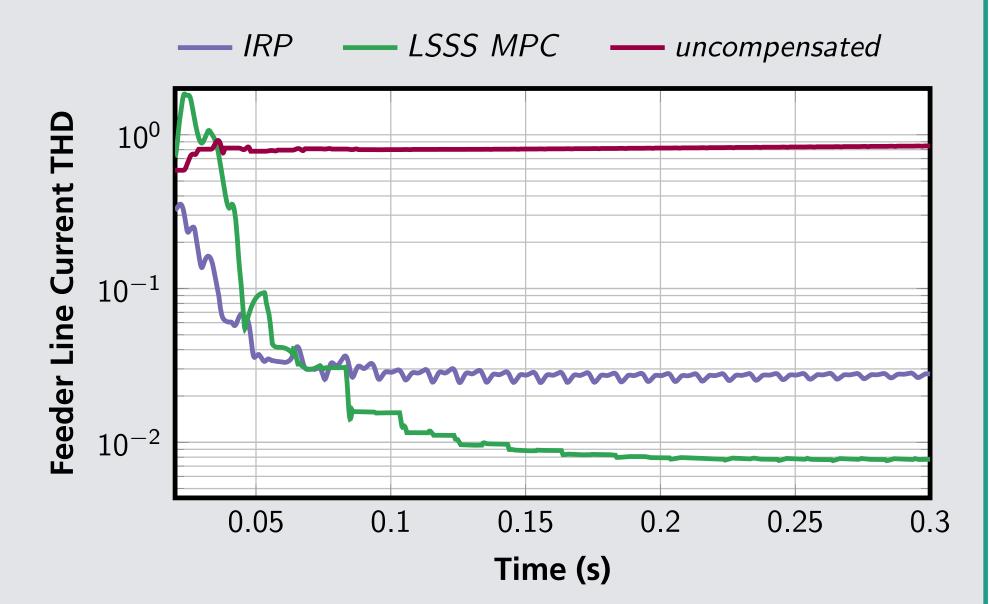
IRP APF harmonic current compensation:



LSSS MPC harmonic current compensation:



Total harmonic distortion (THD):

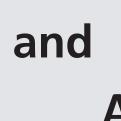


Results for different load scenarios:

Load	THD (v_f)		THD (i _f)	
scenario	IRP	MPC	IRP	MPC
100 Ω	0.65%	0.17%	4.35%	0.78%
9Ω	0.45%	0.35%	0.75%	1.57%
2Ω	1.15%	0.35%	3.75%	1.33%

CONCLUSION

- The LSSS MPC approach has the potential to successfully control an APF
- Classic IRP controllers rely on high pass filter design to achieve good compensation results in a given load scenario
- The LSSS MPC is capable of adapting to a wider variety of load scenarios



where

 $\mathbf{A} \in \mathbb{R}^{3 \times 3}$, $\mathbf{B} \in \mathbb{R}^{3 \times 1}$, $\mathbf{E} \in \mathbb{R}^{3 \times 1}$.