

$M_0$  IS A REDUNDANT LOAD THAT RESULTS FROM A REDUNDANT CONSTRAINT AT THE WALL.

TO USE CASTIGLIANO'S METHOD ALL LOADS NEED TO BE KNOWN, THUS  $M_0$  NEEDS TO BE SOLVED FOR FIRST.

SYMMETRY IS USED TO SIMPLIFY THIS PROBLEM.

ONLY BENDING AND TORSION ARE CONSIDERED.

FROM (C)

$$M_{mn} = \frac{P_y}{2}$$

$$T_{mn} = m_0$$

FROM (F)

$$M_{lm} = -M_0 + \frac{P_x}{2} = \frac{P_x}{2} - M_0$$

THE TOTAL STRAIN ENERGY THAT RESULTS FROM THESE LOADS (TAKING SYMMETRY INTO ACCOUNT)

$$U = 2 \cdot \int_0^{b/2} \frac{M_{lm}^2}{2EI} dx + 2 \cdot \int_0^a \frac{M_{mn}^2}{2EI} dy + 2 \cdot \frac{T_{mn}^2 \cdot a}{2GK}$$

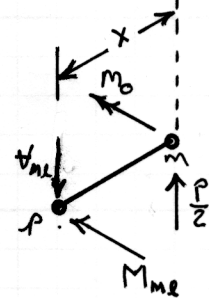
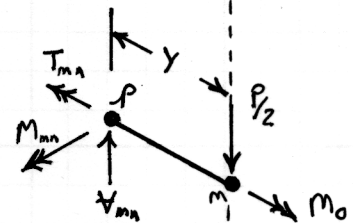
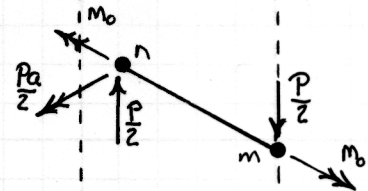
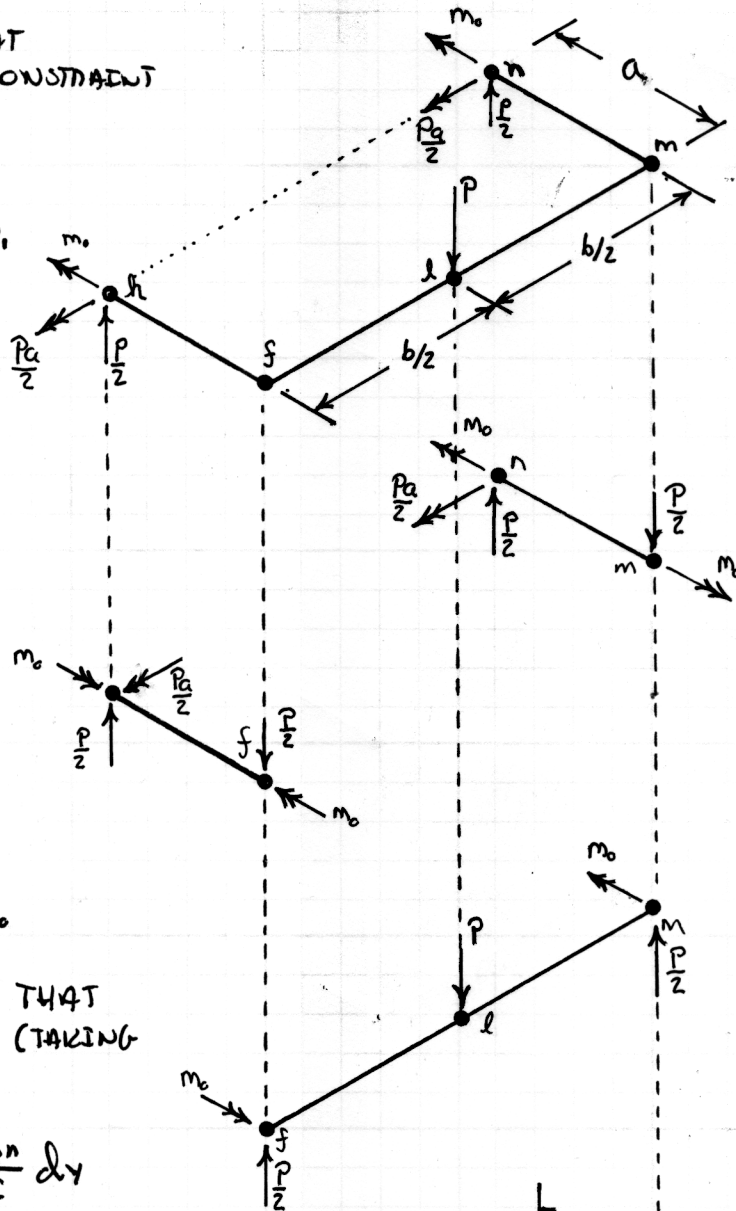
$$= \int_0^{b/2} \left( \frac{P_x}{2} - M_0 \right)^2 dx + \int_0^a \frac{P_y^2}{4EI} dy + \frac{M_0^2 \cdot a}{GK}$$

$$= \frac{1}{EI} \int_0^{b/2} \left( \frac{P_x^2}{4} - M_0 \cdot P_x + M_0^2 \right) dx + \frac{P_y^2}{4EI} \int_0^a dy + \frac{M_0^2 \cdot a}{GK}$$

$$= \frac{1}{EI} \left[ \frac{P_x^2 x^2}{4} - M_0 \cdot P_x x + M_0^2 x \right]_0^{b/2} + \frac{P_y^2}{4EI} \frac{y^3}{3} \Big|_0^a + \frac{M_0^2 a}{GK}$$

$$= \frac{1}{EI} \left[ \frac{P_x^2 b^3}{96} - \frac{M_0 \cdot P_x \cdot b^2}{8} + \frac{M_0^2 \cdot b}{2} \right] + \frac{P_y^2 a^3}{12EI} + \frac{M_0^2 a}{GK}$$

$$= \frac{1}{EI} \left[ \frac{P_x^2 b^3}{96} - \frac{M_0 \cdot P_x \cdot b^2}{8} + \frac{M_0^2 \cdot b}{2} \right] + \frac{P_y^2 a^3}{12EI} + \frac{M_0^2 a}{GK}$$



$$U = \frac{P^2 b^3}{96EI} - \frac{m_o \cdot P \cdot b^2}{8EI} + \frac{m_o^2 \cdot b}{2EI} + \frac{P \cdot a^3}{12EI} + \frac{m_o^2 \cdot a}{GK}$$
$$= \left( \frac{b}{2EI} + \frac{a}{GK} \right) \cdot m_o^2 - \frac{P b^2}{8EI} \cdot m_o + \frac{a^2}{12EI} \cdot P^2$$

THE ROTATIONAL DEFLECTION DUE TO  $m_o$  CAN NOW BE FOUND AND SET TO 0

$$\delta_{m_o} = 0 = \frac{\partial U}{\partial m_o} = 2 \cdot \left( \frac{b}{2EI} + \frac{a}{GK} \right) \cdot m_o - \frac{P \cdot b^2}{8EI}$$

$$m_o = \frac{\frac{P \cdot b^2}{8EI}}{2 \left( \frac{b}{2EI} + \frac{a}{GK} \right)} = \frac{P \cdot b^2}{16EI} \left( \frac{1}{\frac{bGK + 2aEI}{2EI \cdot GK}} \right) = \frac{P \cdot b^2}{16EI} \cdot \frac{2EI \cdot GK}{(bGK + 2aEI)}$$

$$\delta_{m_o} = \frac{b^2 \cdot G \cdot K}{8(bGK + 2a \cdot EI)} \cdot P = A \cdot P \quad \text{WHERE } A = \frac{b^2 \cdot G \cdot K}{8(bGK + 2a \cdot EI)}$$

SUBSTITUTING THIS RESULT FOR  $m_o$  INTO THE TOTAL ENERGY EXPRESSION

$$U = \left( \frac{b}{2EI} + \frac{a}{GK} \right) \cdot A^2 \cdot P^2 - \frac{P \cdot b^2 \cdot A}{8EI} + \frac{a^2}{12EI} \cdot P^2$$
$$= \left( \frac{b \cdot A^2}{2EI} + \frac{a \cdot A^2}{GK} - \frac{b^2 \cdot A}{8EI} + \frac{a^2}{12EI} \right) P^2$$

THE DEFLECTION THAT RESULTS FROM  $P$ , AT THE LOCATION OF  $P$ , AND IN THE DIRECTION OF  $P$  CAN NOW BE FOUND BY TAKING THE DERIVATIVE OF THE STRAIN ENERGY WITH RESPECT TO  $P$

$$\frac{\partial U}{\partial P} = \delta_P = 2 \left( \frac{b \cdot A^2}{2EI} + \frac{a \cdot A^2}{GK} - \frac{b^2 \cdot A}{8EI} + \frac{a^2}{12EI} \right) P$$
$$= \left( \frac{b \cdot A^2}{EI} - \frac{b^2 \cdot A}{4EI} + \frac{a^2}{6EI} + 2 \cdot \frac{a \cdot A^2}{GK} \right) P$$