PROBLEM 5.34 DESIGN A FOORBAR LINKAGE TO CARRY THE BOLT SHOWN BELOW IN THE FLOURE FROM POSITION 1 TO 2 TO 3 WITHOUT RECARD TO THE FIXED PLYOTS SHOWN. THE BOLT IS FEO INTO THE GRIPPER IN THE 2-DIRECTION. THE GRIPPER GRABS THE BOLT, AWD YOUR LIWRINGE MOVES IT TO POSITI POSITION 3 TO BE INSERTED INTO THE HOLE, A SECOND DEGREE OF PREEDOM WITHIN THE GRIPPEN ASSEMBLY (NOT SHOWN PUSHES THE BOLT INTO THE HOLE. EXTEMN THE GRIPPER ASSEMBLY AS NECESSARY TO INCLUDE THE MOUND POHOTS. THE FIXED PIYOTS SHOWN BE ON THE BASE. HINT: TRY GUESS HALLES OF (32=70; B3=140°, 172=5°, 173=47°

## GIVEN!

- 1. THE CONFIGURATION SHOWN IN THE FIGURE
- 2. THE POXED POYETS NEED TO BE

## ASSUMDITIONS:

- 1. ALL COMPONENTS ARE RIGIDO
- 2. ALL JOSHTS ARE FRICTICALESS
- 3. ALL MOTION IS PLANAR
- 4. GRANITY ACTS YENTELALLY DOGWAYND

### FIND:

1) SYNTHESISE A CIMCHUE THAT WELL MOVE THE BOLT AS SPECIFIED. AND HAVE THE GROWN PITCH SHOWN IN 240 gripper all dimensions in mm 183.2 31.7° 301.7° 13 222 272.3° 151.8 400 111.5-200 bolt base workpiece - 111.3-

# Solution:

THIS SOLUTION IS FOR <u>3 POSITIONS WITH FIXED PIYOTS</u>. THIS IS A DEYSATION FROM THE PROBLEM STATED IN THE BOOK.

THE SOLUTION STORTS, AS DED WITH A GRAPHICAL SOLUTION TO THE MECHANISM USING THE 3 ROSITION WITH FIXED PITCIS METHODOLOGY SEEN ON THE NEXT PAGE.

THE GRAPHICAL SCLUTION ON THE NEXT PAGE WILL PROVIDE TWIGHT INTO THE SELECTION OF THE FREE CHOICES FOR THE ANALYTIS CAL SOLUTION.

THE ANALYTICAL SOLUTION STARTS BY LOCATING POINTS P1, P2 & B IN THE PLANE OF THE MECHANISM THAT HAS COORDINATED CENTENED AT P1. FROM THE FIGURE ON THE PREVIOUS PAGE

$$(P_{2x}, P_{2y}) = (99mm, 13mm)$$

THE INPUTS THAT ARE CLASSIFIED AS GIVEN CAN NOW BE COMPUTED.

$$P_{21} = \sqrt{(P_{2x} - P_{3x})^2 + (P_{2y} - P_{3y})^2} = \sqrt{(99mm - 0mn)^2 + (13mm - 0mn)^2} = 99.85mm$$

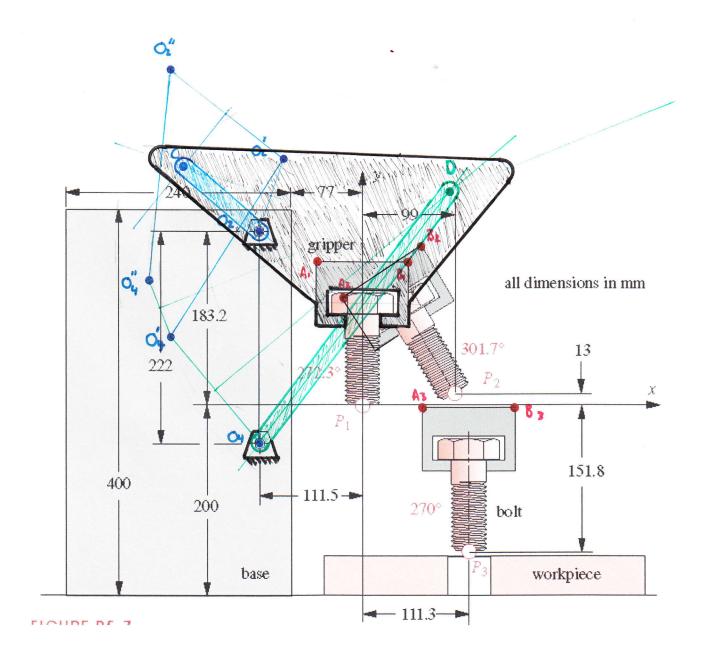
$$P_{31} = \sqrt{(P_{3x} - P_{3x})^2 + (P_{3y} - P_{3y})^2} = \sqrt{(111.3 \text{mm} - 0 \text{mm})^2 + (-151.8 \text{mm} - 0 \text{mm})^2} = 188.23 \text{mm}$$

$$S_z = \tan^3 \frac{R_y - P_{1y}}{P_{2x} - P_{1x}} = \tan^4 \frac{13 \, \text{mm} - 0 \, \text{mm}}{99 \, \text{mm} - 0 \, \text{mm}} = 7.48^{\circ}$$

$$\int_{3} = \tan^{3} \frac{P_{3y} - P_{3y}}{P_{5x} - P_{1x}} = \tan^{3} \frac{-151.8 \, \text{mm} - 0 \, \text{mm}}{111.3 \, \text{mm} - 0 \, \text{mm}} = 306.25^{\circ}$$

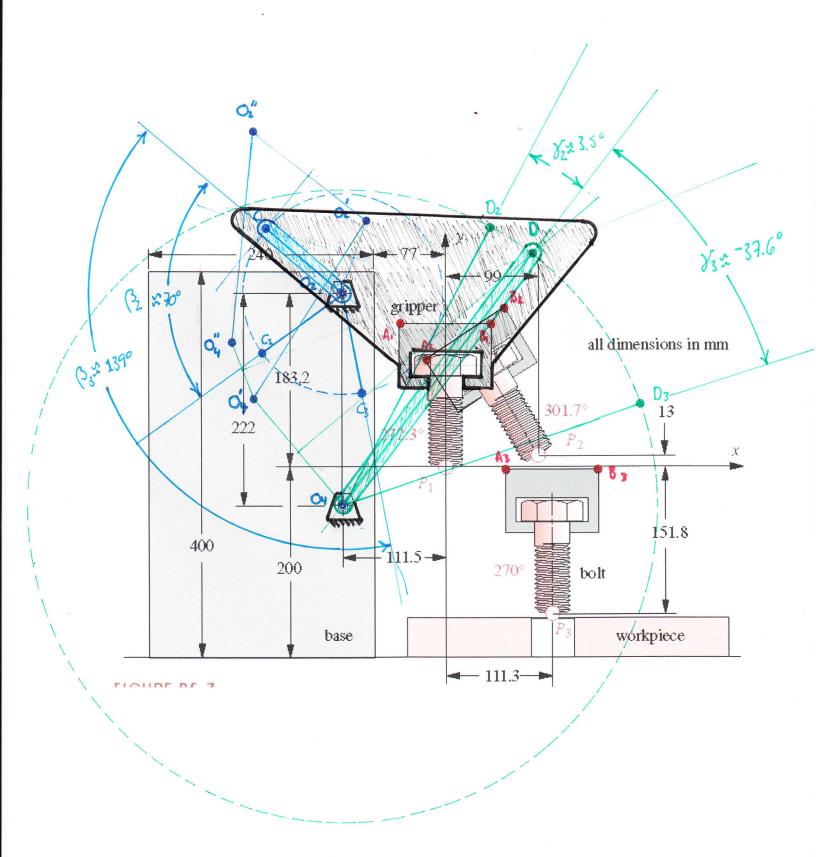
THE FIGURE ON PAGE 4 ILLUSTRATES HOW THE Free CHOICES ARE DETERMINED

$$\beta_2 = 70^{\circ}$$
  $\beta_2 = 3.5^{\circ}$   $\beta_3 = 139^{\circ}$   $\beta_3 = -37.6^{\circ}$ 



HOMEWORK SCUTION
MER 312: ADVANCED DYNAMIUS & KINEMATICS

PROIS 5.34 Pa4 Norton 5TH



### FIRST DYAD

C	CHOSEN:		FIND:				x-coord	y-coord.
99.85 β	32	70.00	w	100.315	02		-111.795	182.07
188.23 β	33	139.00	θ	150.483	A1		-199.091	231.500
7.48			z	305.335	A2		-188.095	116.951
306.25			ф	-49.304	A3		-78.337	87.507
29.40			W1x	-87.295	P1		0.000	0.000
357.70			W1y	49.423	P2		99.000	12.998
			Z1x	199.091	P3		111.302	-151.797
			Z1y	-231.500				
	99.85 ( 188.23 ( 7.48 306.25 29.40	99.85 β2 188.23 β3 7.48 306.25 29.40	99.85 β2 70.00 188.23 β3 139.00 7.48 306.25 29.40 357.70	99.85 β2 70.00 w 188.23 β3 139.00 θ 7.48 z 306.25 φ 29.40 W1x	99.85 β2 70.00 w 100.315 188.23 β3 139.00 θ 150.483 7.48 z 305.335 306.25 φ -49.304 29.40 W1x -87.295 357.70 W1y 49.423 Z1x 199.091	99.85 p2 70.00 w 100.315 O2 188.23 p3 139.00 θ 150.483 A1 7.48 z 305.335 A2 306.25 φ -49.304 A3 29.40 W1x -87.295 P1 357.70 W1y 49.423 P2 Z1x 199.091 P3	99.85 β2 70.00 w 100.315 O2 188.23 β3 139.00 θ 150.483 A1 7.48 z 305.335 A2 306.25 ψ -49.304 A3 29.40 W1x -87.295 P1 357.70 W1y 49.423 P2 Z1x 199.091 P3	99.85 β2 70.00 w 100.315 O2 -111.795 188.23 β3 139.00 θ 150.483 A1 -199.091 7.48 z 305.335 A2 -188.095 306.25 ψ -49.304 A3 -78.337 29.40 W1x -87.295 P1 0.000 357.70 W1y 49.423 P2 99.000 Z1x 199.091 P3 111.302

ı	-0.6580	-0.9397	-0.1288	-0.4909	ſ	W1x	)	ſ	99.0003
	0.9397	-0.6580	0.4909	-0.1288	J	W1y	l _	J	12.9985
	-1.7547	-0.6561	-0.0008	0.0401	)	Z1x	_	)	111.3022
	0.6561	-1.7547	-0.0401	-0.0008	l	Z1y	J	Į	-151.7971

### SECOND DYAD

GIVEN:		CHOSEN:		FIND:			x-coord	y-coord.
P12	99.85	γ2	3.50	u	303.038	04	-115.117	-32.995
P13	188.23	γ3	-37.60	σ	56.747	B1	51.050	220.423
δ2	7.48			S	226.257	B2	35.269	230.095
δ3	306.25			Ψ	-103.040	B3	171.157	66.400
α2	29.40			U1x	166.167	P1	0.000	0.000
α3	357.70			U1y	253.418	P2	99.000	12.998
				S1x	-51.050	P3	111.302	2 -151.797
				S1y	-220.423			

-0.0019	-0.0610	-0.1288	-0.4909		U1x	1	ſ	99.0	0003
0.0610	-0.0019	0.4909	-0.1288	J	U1y	l _	<b>_</b> J	12.9	985
-0.2077	0.6101	-0.0008	0.0401	J	S1x	_	<del>-</del> )	111.3	3022
-0.6101	-0.2077	-0.0401	-0.0008	l	S1v	J	l	-151.7	971