PROBLEM 1 a. GIVEN THE EXPRESSIONS FOR STRAIN INTERMS OF STRESS

$$e_x = \frac{1}{E} \left[\sigma_x - \nu (\sigma_y + \sigma_z) \right]$$
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$$E_{\gamma} = \frac{1}{E} \left[\sigma_{\gamma} - \nu (\sigma_{x} + \sigma_{z}) \right]$$

$$\epsilon_{z} = \frac{1}{\epsilon} \left[\left[\sigma_{z} - \nu (\sigma_{x} + \sigma_{y}) \right] \right] \tag{3}$$

DERIVE THE EXPRESSIONS FOR STRESS INTERMS OF STRAIN.

b. DERIVE THE EXPRESSIONS FOR THE STRAIN IN TERMS OF STRESS FOR THE CASE OF PLANE STRESS AND PLANE STRAIM.

C. DERIVE THE EXPRESSION FOR THE STRESS IN TERMS OF STRAIN FOR THE CASE OF PLANE STRESS AND PLANE STRAIN

GIVEN:

CONSTRAINTS 1. J., Ty, Tz, E, V Assemptions

1. THE MATERIAL IS CINEAR CLUSTIC

I. Gx (Ex. Ex, Ez)

2. (Cx, Ex, Ez) 3. (Cx, Ex, Ez)

SOLUTION

(4)

0

JU = E.E, + V (Jx + Jt)

(5)

Jz = E.Ez + V (Tx + Tv)

(6)

$$\mathcal{T}_{X} \cdot (1 - 2 \cdot \nu^{2}) = \mathbb{E} \cdot \mathcal{E}_{X} + \nu \left[\mathbb{E} \cdot \mathcal{E}_{Y} + \mathbb{E} \cdot \mathcal{E}_{Z} + \nu \left(\mathcal{T}_{Y} + \mathcal{T}_{Z} \right) \right]$$

(7)

From 9

 (\mathfrak{I})

(10)

(11)

SOBSTENDING (8) INTO (7)
$$\int_{X} \cdot (1 - 2 \cdot \nu^{2}) = E \cdot e_{x} + \nu [E \cdot e_{y} + E \cdot e_{z} + \sigma_{x} - E \cdot e_{x}]$$

$$\int_{X} \cdot (1 - 2 \nu^{2} - \nu) = E \cdot e_{x} - E \cdot \nu \cdot e_{x} + E \cdot \nu (e_{y} + e_{z})$$

$$\underbrace{(1 - \nu - 2 \nu^{2})}_{E} \quad \sigma_{x} = (1 - \nu) e_{x} + \nu (e_{y} + e_{z})$$

$$\underbrace{\sigma_{x} = \frac{E}{(1 - \nu - 2 \nu^{2})} \cdot [(1 - \nu) \cdot e_{x} + \nu \cdot (e_{y} + e_{z})]}_{=(1 - \nu)(1 - 2 \nu)} [(1 - \nu) \cdot e_{x} + \nu \cdot (e_{y} + e_{z})]$$

To FIND
$$G_{y}(E_{x}, E_{y}, E_{z})$$
, G AND G ARE SUBSTITUTED INTO G

$$G_{y} = E \cdot E_{y} + V \left[E \cdot \mathbf{e}_{x} + V G_{y} + V G_{z} + E \cdot E_{z} + V \cdot G_{x} + V G_{y} \right]$$

$$= E \cdot E_{y} + V \left[E \cdot E_{x} + E \cdot E_{z} + 2 \cdot V G_{y} + V \cdot G_{z} + V G_{y} \right]$$

$$G_{y}(1 - 2 \cdot V^{2}) = E \cdot E_{y} + V \left[E \cdot E_{x} + E \cdot E_{z} + V \cdot G_{z} + G_{x} \right]$$

From (8)

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$$\frac{\sigma_y (1-z\cdot v^2)}{\varepsilon} = \varepsilon \cdot \varepsilon_y + v \left[\varepsilon \cdot \varepsilon_x + \varepsilon \cdot \varepsilon_z + \sigma_y - \varepsilon \cdot \varepsilon_y \right] \\
\frac{\sigma_y (1-v-2v^2)}{\varepsilon} = (1-v)\varepsilon_y + v \left(\varepsilon_x + \varepsilon_z\right)$$

$$\overline{(1-\nu-2\nu)^2} \cdot \left[(1-\nu) \cdot \epsilon_{\gamma} + \nu \cdot (\epsilon_{x} + \epsilon_{z}) \right] = \frac{\epsilon}{(1-\nu)(1-2\nu)} \cdot \left[(1-\nu) \cdot \epsilon_{x} + \nu (\epsilon_{y} + \epsilon_{z}) \right]$$

To FIND $T_{\overline{z}}(E_{\lambda_1}, E_{\gamma_2}, E_{\overline{z}})$, G AND G ARE SUBSTITUTED INTO G $T_{\overline{z}} = E \cdot E_{\overline{z}} + V \left(E \cdot E_{x} + V \cdot T_{y} + V \cdot T_{\overline{z}} + E \cdot E_{y} + V \cdot T_{x} + V \cdot T_{\overline{z}} \right)$ $= E \cdot E_{\overline{z}} + V \left(E \cdot E_{x} + E \cdot E_{y} + 2V \cdot T_{z} + V \cdot T_{y} + V \cdot T_{x} \right)$ $T_{\overline{z}}(1 - 2 \cdot V^{2}) = E \cdot E_{\overline{z}} + V \left(E \cdot E_{x} + E \cdot E_{y} + V \cdot T_{x} + V \cdot T_{x} \right)$

FROM (6)

(12)

(13)

(14)

(15)

SUBSTITUTING (12) INTO (11)

$$\mathcal{T}_{\mathbf{z}}(1-2\cdot \nu^2) = E \cdot \epsilon_{\mathbf{z}} + \nu \left(E \cdot \epsilon_{\mathbf{x}} + E \cdot \epsilon_{\mathbf{y}} + \mathcal{T}_{\mathbf{z}} - E \cdot \epsilon_{\mathbf{z}}\right)$$

(1-V-2.V2) = E. Ez (1-V) + E.V (Ex+Ex)

$$\mathcal{J}_{\mathcal{E}} = \frac{E}{(1-\nu-2\nu^2)} \left[\varepsilon_{\mathcal{E}}(1-\nu) + \nu(\varepsilon_{\times} + \varepsilon_{1}) \right] = \frac{E}{(1+\nu)(1-2\nu)} \cdot \left[(1-\nu) \cdot \varepsilon_{\mathbf{z}} + \nu(\varepsilon_{\mathbf{x}} + \varepsilon_{\mathbf{y}}) \right]$$

IN SOMMARY

$$\mathcal{E}_{x} = \frac{1}{E} \left[\mathcal{T}_{x} - \mathcal{V} \left(\mathcal{T}_{y} + \mathcal{T}_{z} \right) \right] \oplus \mathcal{T}_{x} = \frac{E}{(1+\mathcal{V})(1-2\mathcal{V})} \cdot \left[(1-\mathcal{V}) \cdot \mathcal{E}_{x} + \mathcal{V} \cdot \left(\mathcal{E}_{y} + \mathcal{E}_{z} \right) \right]$$

$$\varepsilon_{y} = \frac{1}{\varepsilon} \left[\overline{U_{y}} - V(\overline{U_{x}} + \overline{U_{\varepsilon}}) \right] \bigcirc \overline{U_{y}} = \frac{\varepsilon}{(1+V)(1-2V)} \cdot \left[(1-V) \cdot \varepsilon_{y} + V \cdot (\varepsilon_{x} + \varepsilon_{\varepsilon}) \right]$$

$$\mathcal{E}_{\xi} = \frac{1}{E} \left[\mathcal{T}_{\xi} - \mathcal{V} \left(\mathcal{T}_{\chi} + \mathcal{T}_{\gamma} \right) \right] \otimes \mathcal{T}_{\xi} = \frac{E}{(1+\mathcal{V})(1-2\mathcal{V})} \cdot \left[(1-\mathcal{V}) \cdot \mathcal{E}_{\xi} + \mathcal{V} \left(\mathcal{E}_{\chi} + \mathcal{E}_{\gamma} \right) \right]$$

THE CASE OF "PLANE STRESS" THE THERO DIMENSION IS WERE SMALL (OR THIN). AS A RESULT IT IS ASSOMED THAT (GIVEN Z" IS THE CHIRD DIMENSION)

(16)

SUBSTITUTING TO INTO D-3

PLANE STRESS

(18)

SINCE THE "2" DIMENSION IS SMALL TO BEGIN WITH, CHANGES IN THE "2" DIMENSION WILL DE EXTREMELY SMALL AND ARE ASSOMED ZEND, THERE ARE MANY ASSOMPTIONS THAT ARE ASSOCIATED WITH PLANE STRESS THE RESULT IN (1) AND (12) BEING APPROXIMATIONS. WHY THIS IS IMPORTANT IS IN FIND AN EXPRESSION FOR UX AND UX IN TERMS OF EX AND GY, (1) AND (12) NEED TO BE SOLVES SIMULTAMICOSCY. STARTING FROM (3) (3) AEQUINES IN ASSOCIATION OF ASSOCIATIONS

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STARTING WITH (13)

$$E \cdot E_x = \mathcal{T}_x - \mathcal{V} \cdot \mathcal{T}_Y$$

From (18)

SCESTERLILING (20) INTO (19)

$$E \cdot E_X + V \cdot E \cdot E_Y = \mathcal{T}_X (1 - V^2) = \sum_{x = 1 - Y^2} \left(E_X + V \cdot E_Y \right)$$

NOW STRATER WITH (18)

FROM (17)

$$E \cdot E_X = \mathcal{O}_X - \mathcal{V} \cdot \mathcal{O}_Y \Rightarrow \mathcal{O}_X = E \cdot E_X + \mathcal{V} \cdot \mathcal{O}_Y$$

SUBSTITUTION THIS RESULT INTO THE ABOVE EQUATION

$$\nabla_{y} = \frac{E}{1-v^{2}} (E_{y} + v \cdot E_{x})$$

IN SUMMARY

$$\overline{O_X} = \frac{E}{1 - V^2} (E_X + V \cdot E_Y)$$

$$\overline{O_Y} = \frac{E}{1 - V^2} (E_Y + V \cdot E_X)$$

$$\overline{G}_{y} = \frac{E}{1-V^{2}} (E_{y} + V \cdot E_{x})$$

PLANE STRESS

NOW LET'S CONSIDER THE CASE OF "PLANE STRUIN." FOR THE PLANE STRAIN CONDITION THE THIRD PIMENSION (& DIRECTION HERE) OF THE STRUCTURE IS CONSIDERED TO BE HERY THICK OR CONSTRAINED FROM DEFORMATION. THIS KESOLTS IN

(20)

(21)

(25)

(26)

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$$O = \mathcal{T}_{z} - \mathcal{V}(\mathcal{T}_{x} + \mathcal{T}_{y}) \implies \mathcal{T}_{z} = \mathcal{V}(\mathcal{T}_{x} + \mathcal{T}_{y})$$

D DINI (25) BUILITEBUS

$$\begin{aligned} & \in_{\mathsf{X}} = \frac{1}{E} \left[(\mathsf{T}_{\mathsf{X}} - \mathsf{V}(\mathsf{T}_{\mathsf{Y}} + \mathsf{V} \cdot \mathsf{T}_{\mathsf{X}} + \mathsf{V} \cdot \mathsf{T}_{\mathsf{Y}}) \right] = \frac{1}{E} \left[(\mathsf{T}_{\mathsf{X}} - \mathsf{V} \cdot \mathsf{T}_{\mathsf{Y}} - \mathsf{V}^{2} \cdot \mathsf{T}_{\mathsf{X}} - \mathsf{V}^{2} \cdot \mathsf{T}_{\mathsf{Y}}) \right] \\ & = \frac{1}{E} \left[(\mathsf{T}_{\mathsf{X}} (\mathsf{1} - \mathsf{V}^{2}) - \mathsf{V} \cdot \mathsf{T}_{\mathsf{Y}} (\mathsf{1} + \mathsf{V})) \right] = \frac{1}{E} \left[(\mathsf{T}_{\mathsf{X}} (\mathsf{1} + \mathsf{V}) (\mathsf{1} - \mathsf{V}) - \mathsf{V} \cdot \mathsf{T}_{\mathsf{Y}} (\mathsf{1} + \mathsf{V})) \right] \\ & = \frac{1}{E} \left[(\mathsf{T}_{\mathsf{X}} (\mathsf{1} - \mathsf{V}) - \mathsf{V} \cdot \mathsf{T}_{\mathsf{Y}}) \right] = \frac{1}{E} \left[(\mathsf{T}_{\mathsf{X}} (\mathsf{1} - \mathsf{V}) - (\mathsf{1} - \mathsf{V}) - \mathsf{V} \cdot \mathsf{T}_{\mathsf{Y}}) \right] \\ & = \frac{(\mathsf{1} + \mathsf{V})(\mathsf{1} - \mathsf{V})}{E} \left[(\mathsf{T}_{\mathsf{X}} - \mathsf{1}^{\mathsf{X}} + \mathsf{V} \cdot \mathsf{T}_{\mathsf{Y}}) \right] = \frac{(\mathsf{1} - \mathsf{V}^{2})}{E} \left[(\mathsf{T}_{\mathsf{X}} - \mathsf{1}^{\mathsf{X}} + \mathsf{V} \cdot \mathsf{T}_{\mathsf{Y}}) \right] \end{aligned}$$

SCBSTSTUTENG (25) INTO (2)

$$\begin{aligned}
& \in_{Y} = \frac{1}{E} \left[(\sigma_{Y} - \nu)(\sigma_{X} + \sigma_{Z}) \right] = \frac{1}{E} \left[(\sigma_{Y} - \nu)(\sigma_{X} + \nu)\sigma_{X} + \nu)\sigma_{Y} \right] \\
& = \frac{1}{E} \left[(\sigma_{Y} - \nu)(\sigma_{X} + \sigma_{Z}) \right] = \frac{1}{E} \left[(\sigma_{Y} + \nu)(\sigma_{X} + \nu)\sigma_{Y} \right] \\
& = \frac{1}{E} \left[(\sigma_{Y} - \nu)(\sigma_{X} + \sigma_{Z}) \right] = \frac{1}{E} \left[(\sigma_{Y} + \nu)(\sigma_{X} + \nu)(\sigma_{X} + \nu)(\sigma_{Y} + \nu)(\sigma_{Y} - \nu)(\sigma_{X} + \nu)(\sigma_{Y} + \nu)(\sigma_$$

IN SUMMARY

$$\epsilon_{x} = \frac{1-y^{2}}{\epsilon} \cdot \left[\sigma_{x} - \frac{y}{1-y} \cdot \sigma_{y} \right]$$

$$\epsilon_{y} = \frac{1-y^{2}}{\epsilon} \cdot \left[\sigma_{y} - \frac{y}{1-y} \cdot \sigma_{x} \right]$$

PLANE STRAIN

SUBSTINITING (29) INTO (13)

$$\overline{\mathbb{J}_{\mathsf{X}}} = \frac{E}{(1+\nu)(1-2\nu)} \cdot \left[(1-\nu) \cdot \mathcal{E}_{\mathsf{X}} + \nu \cdot (\mathcal{E}_{\mathsf{Y}} + \mathcal{E}_{\mathsf{Z}}) \right] = \frac{E}{(1+\nu)(1-2\nu)} \cdot \left[(1-\nu) \cdot \mathcal{E}_{\mathsf{X}} + \nu \cdot \mathcal{E}_{\mathsf{Y}} \right]$$

$$\mathcal{J}_{x} = \frac{E \cdot (1 - \nu)}{(1 + \nu)(1 - 2\nu)} \left[\mathcal{E}_{x} + \frac{\nu}{1 - \nu} \mathcal{E}_{y} \right]$$

HOMEWORK SOLUTION MERBY OF MATERIALS

SUBSTITUTE 29 INTO (19)

$$\begin{aligned}
\overline{J}_{\gamma} &= \frac{E}{(1+\nu)(1-2\nu)} \cdot \left[(1-\nu) \cdot E_{\gamma} + \nu \cdot (E_{x} + Z_{z}) \right] &= \frac{E}{(1+\nu)(1-2\nu)} \cdot \left[(1-\nu) \cdot E_{\gamma} \cdot \nu E_{\gamma} \right] \\
&= \frac{(1-\nu) \cdot E}{(1+\nu) \cdot (4-2\nu)} \cdot \left[E_{\gamma} + \frac{\nu}{1-\nu} \cdot E_{\gamma} \right]
\end{aligned}$$

SCESTITUTING (29) INTO (15)

$$\mathbb{Q}_{\xi} = \frac{\mathbb{E}}{(1+\nu)(1-2\nu)} \cdot \left[(1-\nu) \cdot \mathbb{E}_{\xi}^{2} + \nu \cdot (\mathbb{E}_{x} + \mathbb{E}_{y}) \right] = \frac{\nu \cdot \mathbb{E}}{(1+\nu)(1-2\nu)} \cdot (\mathbb{E}_{x} + \mathbb{E}_{y}) \quad (\mathbb{E}_{x} + \mathbb{E}_{y})$$

IN SUMMARY

$$\mathcal{O}_{x} = \frac{(1-\nu)}{(1+\nu)\cdot(1-2\nu)} \cdot E \cdot \left[\mathcal{E}_{x} + \frac{\nu}{1-\nu} \cdot \mathcal{E}_{x} \right] \\
\mathcal{O}_{y} = \frac{(1-\nu)}{(1+\nu)\cdot(1-2\nu)} \cdot E \cdot \left[\mathcal{E}_{y} + \frac{\nu}{1-\nu} \cdot \mathcal{E}_{x} \right] \\
\mathcal{O}_{z} = \frac{(1-\nu)}{(1+\nu)\cdot(1-2\nu)} \cdot E \cdot \left(\mathcal{O}_{x} + \mathcal{O}_{y} \right)$$

PLANE STRAIN

SUMMARY:

FROM THE DEVELOPMENT IT IS CLEAR THAT THE STATE OF PLANE STRESS IS AN APPROXIMATION AND THE STATE OF PLANE STRAIN IS AN EXACT SOLUTION. ALSO NOTE THAT EVEN THOUGH THERE IS NO STRAIN IN THE THIRD DIMENSION (2) FOR THE CASE OF PLANE STRAIN, THERE IS STICL STRESS IN THE THIRD DIMENSION.