

FOR THE INVENTED SLIPER CRAWK THE FIXED ANGLE & DEPINES THE OFFISET BETWEEN THE SCIDER AND LINK 4. THIS RESOLTS IN A RELATION SHIP BETWEEN G3 AND G4

NOTE THAT I IS A CONSTANT. THE LOCP THAT DEFINES THE RINEMATICS OF THIS PROBLEM CAN BE WILLIEW.

$$\vec{\Gamma}_{z} + \vec{\Gamma}_{\bar{s}} = \vec{\Gamma}_{\bar{s}} + \vec{\Gamma}_{\bar{q}}$$

$$\vec{\Gamma}_{z} = \Gamma_{z} \cdot \hat{\mathcal{C}}_{rz} \ (= \alpha \cdot \hat{\mathcal{C}}_{rz}) = \Gamma_{z} (\cos \theta_{z} \hat{c} + \sin \theta_{z} \hat{s})$$

$$\vec{\Gamma}_{\bar{s}} = \Gamma_{\bar{s}} \cdot \hat{\mathcal{C}}_{rz} \ (= b \cdot \hat{\mathcal{C}}_{rz}) = \Gamma_{\bar{s}} (\cos \theta_{\bar{s}} \hat{c} + \sin \theta_{\bar{s}} \hat{s})$$

$$\vec{\Gamma}_{\bar{s}} = \Gamma_{\bar{s}} \cdot \hat{\mathcal{C}}_{rz} \ (= b \cdot \hat{\mathcal{C}}_{r\bar{s}}) = \Gamma_{\bar{s}} (\cos \theta_{\bar{s}} \hat{c} + \sin \theta_{\bar{s}} \hat{s})$$

$$\vec{\Gamma}_{\bar{q}} = \mathcal{A} \cdot \hat{c}$$

$$\vec{\Gamma}_{\bar{q}} = \Gamma_{\bar{q}} \cdot \hat{\mathcal{C}}_{r\bar{q}} \ (= c \cdot \hat{\mathcal{C}}_{r\bar{q}} \) = \Gamma_{\bar{q}} \cdot (\cos \theta_{\bar{q}} \hat{c} + \sin \theta_{\bar{q}} \hat{s})$$

$$\vec{G}$$

THE LENGTH (3 = b HARJES AS THE LINKAGE MOVES. THUS (3 = b IS
A HARJABLE THAT MUST BE SOLDED FOR. THIS CREATES AN ADDITIONAL
UNKNOWN THAT NEEDS TO BE DETERMINED, O4, O5, G=b. HOWEVER, ① IS A
THIRD EQUATION THAT CAN BE USED TO DETERMINE THESE VANIABLES GIVEN O2, a, c, d.

22-141 50 SHEETS 22-142 100 SHEETS 22-141 200 SHEETS

EAWRAD"

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STARTING WITH THE LOOP EQUATION (2) AND SUBSTITUTING (3)-6
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DOTTING WITH ?

8

DETENG WITH I

(9)

EQUATIONS (1), (8) (9) ARE THREE EQUATIONS THAT CONTAIN THREE CONTROL OF FOR 13

(10)

SUBSTITUTING (10) INTO (8)

SUBSTITUTING (1) INTO (11)

C. sin By cos By cos B + C. sin By · sin By · sin B - a · sin Bz · cos By · cos B - a · sin Bz · sin B

C.cos P. Sin Oy.cos O4 + C.sin P. Sin O4 - a.cos P. Sin Oz.cos O4 - a.sin P. Sin O4 Sin O4 - a.cos O4. Sin O4. cos O4. cos O4. Sin O4. cos O4.

C. cost sinθy cosθ + C. sin f. sin² Θ q - a · cos f. sinθ 2 · cosθ q - a · sin f. sin θ 2 · sin Θ q - c · cosθ q· sinθ q· cos f + c · cos θ q· sin f - d · sinθ q· cos f + d · cos Θ q · sin f + a · cosθ q· sinθ q· cos f - a · cosθ q· cos θ q· sin f = 0

C.sin f. (sin204+cos204)-a. (sin02.cosf+sinf.cos02).cos04 +a. (cos 02.cosf-sin02.sinf).sin 04-d.cosf.sin 04+dsinf.cos04=0

C. sin \$ - a. sin (02+5). cos 64 + a. cos (02+5). sin 64 - d. cos 8. sin 64 + d. sin 8. cos 64 + 0

[a·cos(Oz+))-d·cos]·sinO4+[-a·sin(Oz+))+d·sin]·cosO4+c·sin}=0

$$K_1 \cdot \sin \Theta_1 + K_2 \cdot \cos \Theta_1 + K_3 = 0$$

$$K_1 = \alpha \cdot \cos (\Theta_2 + \beta) - \alpha \cdot \cos \beta$$

$$K_2 = -\alpha \cdot \sin (\Theta_2 + \beta) + \alpha \cdot \sin \beta$$

$$K_3 = C \cdot \sin \beta$$

(12)

(13)

(74)

(15)

USING THE TRIGOMETRIC IDENTITIES

6

$$\cos 2\cdot d = \frac{1 - \tan^2 d}{1 + \tan^2 d}$$
 \Rightarrow $\cos \theta = \frac{1 - \tan^2 \frac{\theta}{2}}{1 + \tan^2 \frac{\theta}{2}}$

(17)

SUBSTITUTING (16) AND (17) INTO (12)

$$K_{1} \cdot \frac{2 \cdot \tan \frac{\Theta_{4}}{2}}{1 + \tan^{2} \frac{\Theta_{4}}{2}} + K_{2} \cdot \frac{1 - \tan^{2} \frac{\Theta_{4}}{2}}{1 + \tan^{2} \frac{\Theta_{4}}{2}} + K_{3} = 0$$

 $2 \cdot K_1 \cdot \tan^2 \theta + K_2 - K_2 \cdot \tan^2 \theta + K_3 + K_3 \cdot \tan^2 \theta = 0$ $(K_3 - K_2) \cdot \tan^2 \theta + 2 \cdot K_1 \cdot \tan^2 \theta + (K_3 + K_2) = 0$

$$\tan^2 \frac{\Theta_4}{z} + \frac{2 \cdot K_1}{K_3 \cdot K_2} \cdot \tan \frac{\Theta_4}{z} + \frac{K_3 + K_2}{K_3 - K_2} = 0$$

$$\tan^{2} \frac{\Theta_{4}}{Z} + \frac{2 \cdot K_{4}}{K_{3} - K_{2}} \cdot \tan^{2} \frac{\Theta_{4}}{Z} + \left(\frac{K_{3}}{K_{3} - K_{2}}\right)^{2} - \left(\frac{K_{3}}{K_{3} - K_{2}}\right)^{2} + \frac{K_{3} + K_{2}}{K_{3} - K_{2}} = 0$$

$$\left(\tan^{2} \frac{\Theta_{4}}{Z} + \frac{K_{4}}{K_{3} - K_{2}}\right)^{2} = \left(\frac{K_{4}}{K_{3} - K_{2}}\right)^{2} - \left(\frac{K_{3} + K_{2}}{K_{3} - K_{2}}\right)$$

$$\tan^{2} \frac{\Theta_{4}}{Z} = -\frac{K_{4}}{K_{3} - K_{2}} + \sqrt{\left(\frac{K_{4}}{K_{5} - K_{2}}\right)^{2} - \left(\frac{K_{3} + K_{2}}{K_{3} - K_{2}}\right)}$$

$$\tan^{2} \frac{\Theta_{4}}{Z} = -\frac{K_{1}}{K_{3} - K_{2}} + \sqrt{\frac{K_{2}^{2} - \left(\frac{K_{3} + K_{2}}{K_{3} - K_{2}}\right) \left(\frac{K_{3} - K_{2}}{K_{3} - K_{2}}\right)}$$

$$\tan^{2} \frac{\Theta_{4}}{Z} = -\frac{K_{1}}{K_{5} - K_{2}} + \sqrt{\frac{K_{2}^{2} - \left(\frac{K_{3}^{2} + K_{2}}{K_{5} - K_{2}}\right) \left(\frac{K_{3} - K_{2}}{K_{3} - K_{2}}\right)}}$$

$$\tan^{2} \frac{\Theta_{4}}{Z} = -\frac{K_{1}}{K_{5} - K_{2}} + \sqrt{\frac{K_{2}^{2} - \left(\frac{K_{3}^{2} - K_{2}}{K_{5} - K_{2}}\right) \left(\frac{K_{3} - K_{2}}{K_{3} - K_{2}}\right)}}{\left(\frac{K_{3} - K_{2}}{K_{3} - K_{2}}\right)}}$$

$$\Theta_{4} = 2 \cdot \tan^{2} \left[\frac{-K_{1} \pm \sqrt{K_{1}^{2} + K_{2}^{2} - K_{3}^{2}}}{K_{3} - K_{2}}\right]$$

$$\Theta_{4} = 2 \cdot \tan^{2} \left[\frac{-K_{1} \pm \sqrt{K_{1}^{2} + K_{2}^{2} - K_{3}^{2}}}{K_{3} - K_{2}}\right]}\right]$$

$$(18)$$

THE SOLUTION OF THE INVERTED SLIDER CRANK LINKAGE STARTS WITH THE DEPENATION OF THE LINKAGE PARAMETERS

GIVEN: a, c, d, O2, & Y

THE PARAMETERS THAT NEED TO BE DETERMINED INCLUDE

FIND: b, O3, & O4

THESE PARAMETERS ARE FECUND USING (1), (10), (13), (14), (13) AND (18)