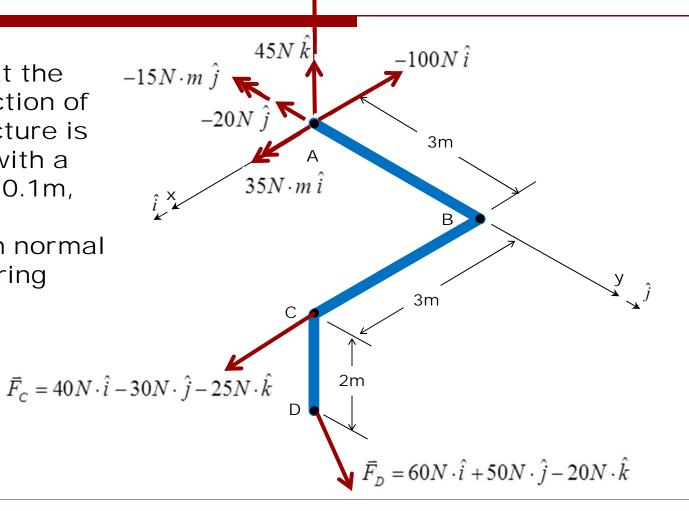
MER311: Advanced Strength of Materials

LECTURE OUTLINE

- State of Stress
- ☐ Stress Tensor
- Equilibrium

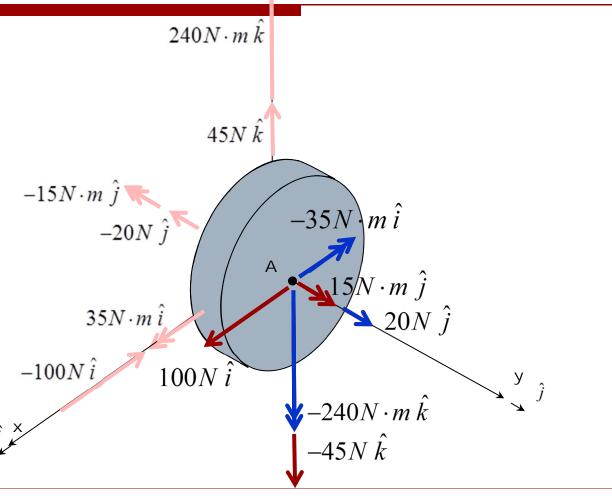
Example Continuation 240N·m k

Given that the cross-section of this structure is circular with a radius of 0.1m, find the maximum normal and shearing stresses.





At the Wall



Calculating the State of Stress Using Strength of Materials

$$\sigma_{y} = \frac{F_{y}}{A_{y}} \pm \frac{M_{x} \cdot z}{I_{xx}} \pm \frac{M_{z} \cdot x}{I_{zz}}$$

$$\tau_{yx} = \frac{V_x \cdot Q}{I_{zz} \cdot t_z}$$

$$\tau_{zx} = \frac{V_z \cdot Q}{I_{xx} \cdot t_x}$$

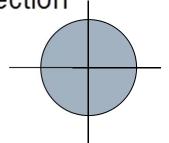
$$\tau_{yr} = \frac{T_y \cdot r}{J}$$

For a Circular Cross-Section

$$A = \pi \cdot r^2$$

$$I = \frac{\pi \cdot r^4}{4} = \frac{\pi \cdot d^4}{64}$$

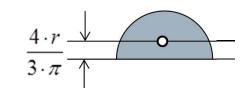
$$J = \frac{\pi \cdot r^4}{2} = \frac{\pi \cdot d^4}{32}$$

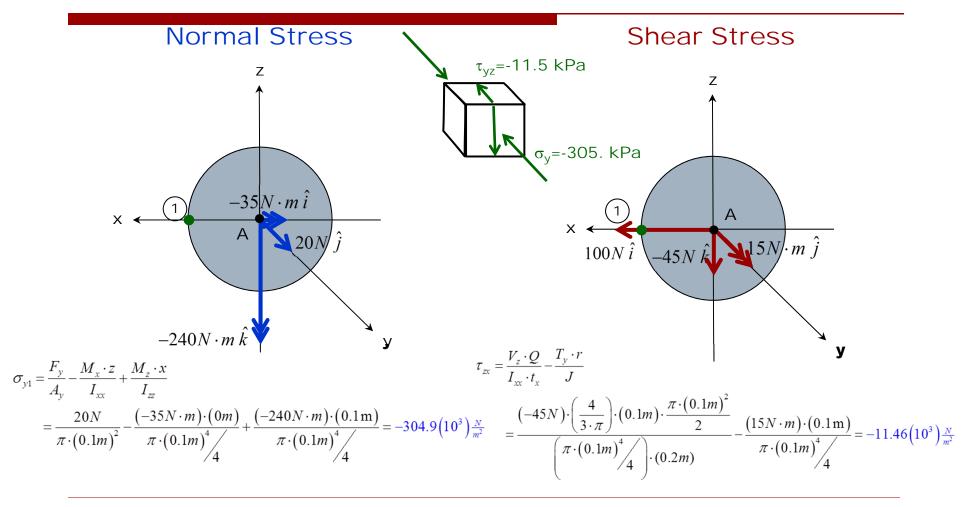


For a Semi-Circular Cross-Section

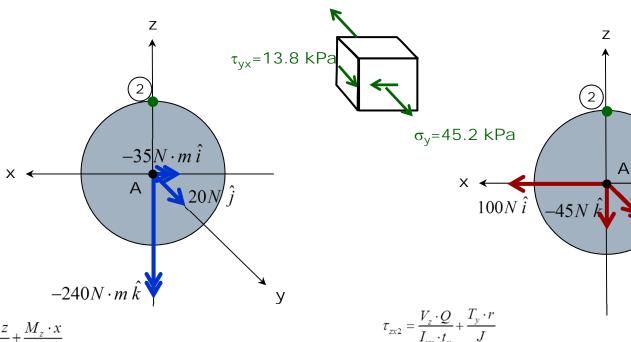
$$A = \frac{\pi \cdot r^2}{2}$$

$$I = 0.110 \cdot r^4$$





Normal Stress

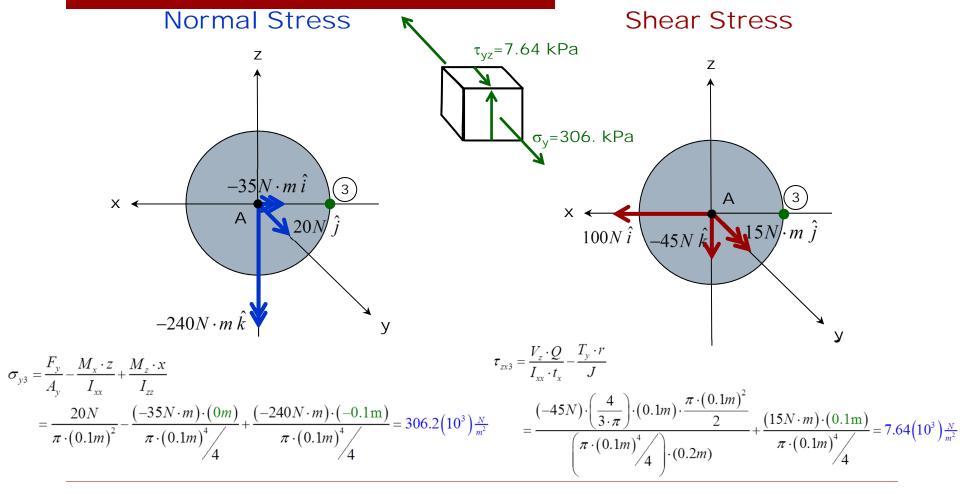


$$\sigma_{y2} = \frac{F_{y}}{A_{y}} - \frac{M_{x} \cdot z}{I_{xx}} + \frac{M_{z} \cdot x}{I_{zz}}$$

$$= \frac{20N}{\pi \cdot (0.1m)^{2}} - \frac{\left(-35N \cdot m\right) \cdot (0.1m)}{\pi \cdot (0.1m)^{4} / 4} + \frac{\left(-240N \cdot m\right) \cdot (0 \cdot m)}{\pi \cdot (0.1m)^{4} / 4} = 45.20 \left(10^{3}\right) \frac{N}{m^{2}}$$

$$= \frac{\left(100N\right) \cdot \left(\frac{4}{3 \cdot \pi}\right) \cdot (0.1m) \cdot \frac{\pi \cdot (0.1m)^{2}}{2}}{\left(\pi \cdot (0.1m)^{4} / 4\right) \cdot (0.2m)} + \frac{\left(15N \cdot m\right) \cdot (0.1m)}{\pi \cdot (0.1m)^{4} / 4}$$

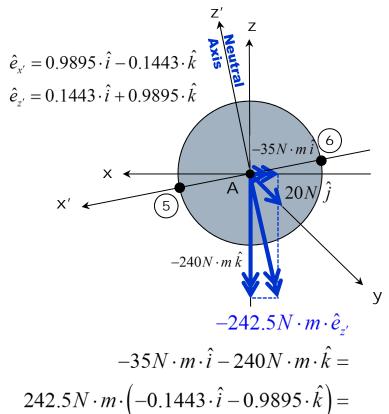
$$= \frac{(100N) \cdot \left(\frac{4}{3 \cdot \pi}\right) \cdot (0.1m) \cdot \frac{\pi \cdot (0.1m)^{2}}{2}}{\left(\pi \cdot (0.1m)^{4}\right) \cdot (0.2m)} + \frac{(15N \cdot m) \cdot (0.1m)}{\pi \cdot (0.1m)^{4}} = 13.79 \left(10^{3}\right) \frac{N}{m^{2}}$$

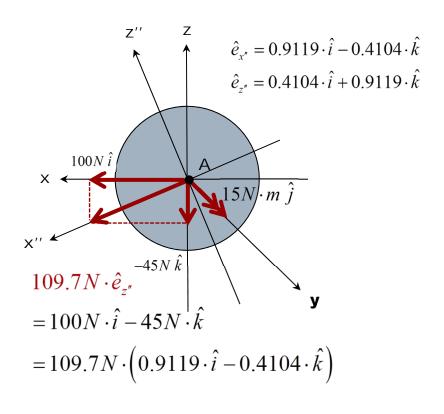


Normal Stress **Shear Stress** σ_v =-43.9 kPa 100Ni $-240N \cdot m \hat{k}$ $\tau_{zx4} = \frac{V_z \cdot Q}{I_{\cdots} \cdot t_{\cdots}} + \frac{T_y \cdot r}{J}$ $\sigma_{y4} = \frac{F_y}{A_y} - \frac{M_x \cdot z}{I_{yy}} + \frac{M_z \cdot x}{I_{zz}}$ $= \frac{20N}{\pi \cdot (0.1m)^{2}} - \frac{\frac{I_{zz}}{(-35N \cdot m) \cdot (-0.1m)}}{\pi \cdot (0.1m)^{4} / 4} + \frac{\frac{(-240N \cdot m) \cdot (0 \cdot m)}{\pi \cdot (0.1m)^{4} / 4}}{\pi \cdot (0.1m)^{4} / 4} = -43.92 (10^{3}) \frac{N}{m^{2}} = \frac{(100N) \cdot \left(\frac{4}{3 \cdot \pi}\right) \cdot (0.1m) \cdot \frac{\pi \cdot (0.1m)}{2}}{\left(\pi \cdot (0.1m)^{4} / 4\right) \cdot (0.2m)} - \frac{(15N \cdot m) \cdot (0.1m)}{\pi \cdot (0.1m)^{4} / 4} = -5.306 (10^{3}) \frac{N}{m^{2}}$

For the Circular X-Section Maximum Stresses

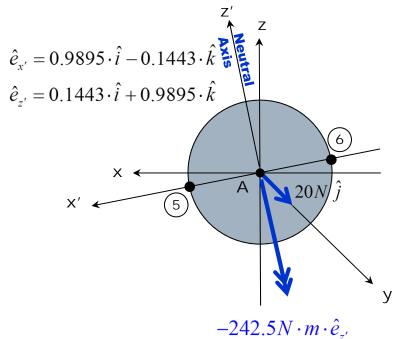
Normal Stress



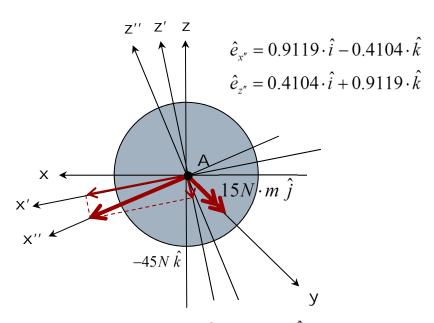


Only a Component of the Shear Stress Important

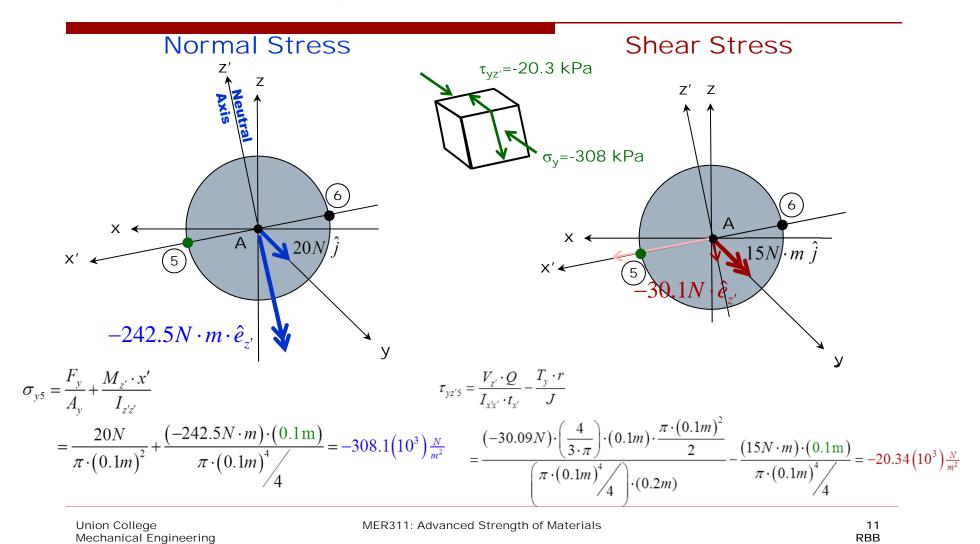
Normal Stress



 $-35N \cdot m \cdot \hat{i} - 240N \cdot m \cdot \hat{k} =$ $242.5N \cdot m \cdot \left(-0.1443 \cdot \hat{i} - 0.9895 \cdot \hat{k}\right) =$



$$109.7N \cdot \hat{e}_{z''} = 100N \cdot \hat{i} - 45N \cdot \hat{k}$$
$$= 105.4N \cdot \hat{e}_{x'} - 30.1N \cdot \hat{e}_{z'}$$

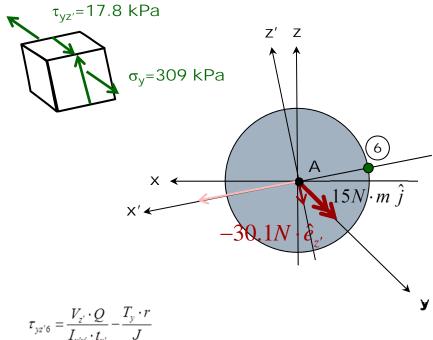


Normal Stress

1 20*N*/ $-242.5N \cdot m \cdot \hat{e}_{z'}$

$$\sigma_{y6} = \frac{F_y}{A_y} + \frac{M_{z'} \cdot x'}{I_{z'z'}}$$

$$= \frac{20N}{\pi \cdot (0.1m)^2} + \frac{(-242.5N \cdot m) \cdot (-0.1m)}{\pi \cdot (0.1m)^4 / 4} = 309.4(10^3) \frac{1}{3}$$



$$= \frac{20N}{\pi \cdot (0.1m)^{2}} + \frac{\left(-242.5N \cdot m\right) \cdot \left(-0.1m\right)}{\pi \cdot (0.1m)^{4} / 4} = 309.4 \left(10^{3}\right) \frac{N}{m^{2}} = \frac{\left(-30.09N\right) \cdot \left(\frac{4}{3 \cdot \pi}\right) \cdot \left(0.1m\right) \cdot \frac{\pi \cdot \left(0.1m\right)^{2}}{2}}{\left(\pi \cdot \left(0.1m\right)^{4} / 4\right) \cdot \left(0.2m\right)} + \frac{\left(15N \cdot m\right) \cdot \left(0.1m\right)}{\pi \cdot \left(0.1m\right)^{4} / 4} = 17.82 \left(10^{3}\right) \frac{N}{m^{2}}$$