

PROBLEM 7.47 | THE BAR SHOWN IS MACHINED FROM STEEL WITH $S_y = 420 \text{ MPa}$ AND $S_u = 560 \text{ MPa}$. THE AXIAL FORCE OF 50 kN IS COMPLETELY REVERSING. ESTIMATE THE NUMBER OF CYCLES TO FAILURE.

GIVEN:

1. MACHINED STEEL BAR
2. $S_y = 420 \text{ MPa}$, $S_u = 560 \text{ MPa}$
3. 20 mm DIA HOLE IN SECTION OF WIDTH 60 mm
4. RADIUS OF TRANSITION FROM 60 mm TO 40 mm WIDTH IS 4 mm
5. THICKNESS OF BAR 6 mm
6. 50 kN LOADING ON BAR IS COMPLETELY REVERSING.

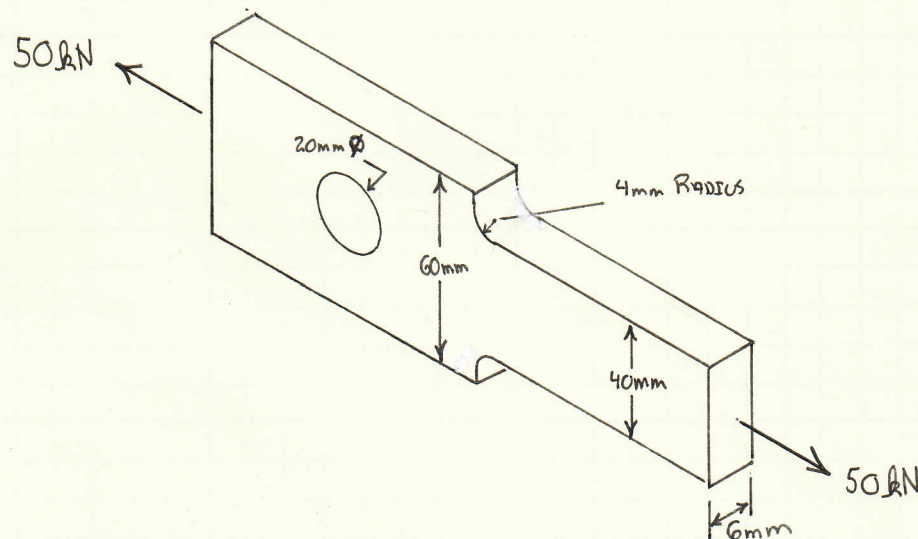
ASSUMPTIONS:

1. LINEAR ELASTIC RESPONSE

FIND:

1. NUMBER OF CYCLES TO FAILURE.

FIGURE:



SOLUTION:

THE AVERAGE STRESS IN THE TWO SECTIONS OF THE BAR ARE

$$\sigma_{60} = \frac{50 \text{ kN}}{(0.06 \text{ m})(0.006 \text{ m})} = 138.9 \text{ MPa} \quad (1)$$

$$\sigma_{40} = \frac{50 \text{ kN}}{(0.04 \text{ m})(0.006 \text{ m})} = 208.3 \text{ MPa} \quad (2)$$

THE AVERAGE STRESS THROUGH THE CENTER OF THE HOLE IN THE 60mm SECTION

$$\sigma_{60,H} = \frac{50 \text{ kN}}{(0.06 \text{ m} - 0.02 \text{ m})(0.006 \text{ m})} = 208.3 \text{ MPa} \quad (3)$$

THE AVERAGE STRESS AT THE HOLE AND IN THE 40mm SECTION ARE THE SAME. THE 208.3 MPa STRESS LEVEL REPRESENTS THE MAXIMUM AVERAGE STRESS IN THE BAR; THEREFORE THE REMAINDER OF THE PROBLEM FOCUSES ON THIS VALUE OF STRESS.

THE S-N CURVE NEEDS TO BE CALCULATED. THE FIRST POINT ON THE S-N CURVE IS

$$0.9 \cdot S_{UT} = 0.9(560 \text{ MPa}) = \underline{504 \text{ MPa @ } 10^3 \text{ CYCLES}} \quad (4)$$

THE SECOND POINT IS S_e @ 10^6 CYCLES. THE VALUE FOR S_e OF THIS BAR MUST BE CALCULATED. FROM LECTURE 15

$$S_e' = 0.5 \cdot S_{UT} = (0.5)(560 \text{ MPa}) = 280 \text{ MPa}$$

$$S_e = k_a \cdot k_b \cdot k_c \cdot k_d \cdot k_e \cdot k_f \cdot S_e' = (0.75)(0.85)(0.4902)(280 \text{ MPa}) = 87.5 \text{ MPa}$$

- $k_a = 0.75$ (machine finish)
- $k_b = 0.85$ (size effect)
- $k_c = 1$ (Reliability)
- $k_d = 1$ (Temperature)
- $k_e = 1/K_{f,H} = 1/2.04 = 0.4902$ $1/K_{f,R} = 1/1.88 = 0.5319$
 - $K_{T,H} = 2.3$ (BODYNAS 2ND APP. F) $d/w = 20 \text{ mm}/60 \text{ mm} = 1/3 = 0.333$
 - $K_{f,H} = 1 + q(K_{T,H} - 1) = 1 + 0.8(2.3 - 1) = 2.04$
 - $q = 0.8$ (LECTURE 15 pg 22)
 - $K_{T,R} = 2.1$ (BODYNAS 2ND APP. F) $P/d = 60/40 = 1.5$ $r/d = 4/40 = 0.1$
 - $K_{f,R} = 1 + q(K_{T,R} - 1) = 1 + 0.8(2.1 - 1) = 1.88$
 - $q = 0.8$ (LECTURE 15 pg 22)

THE PARAMETERS FOR THE S-N CURVE CAN NOW BE CALCULATED

$$m = \frac{1}{3} \cdot \log \frac{0.9 \cdot S_{UT}}{S_e} = \frac{1}{3} \log \frac{0.9(560 \text{ MPa})}{87.5 \text{ MPa}} = 0.2535$$

$$b = \log \frac{(0.9 \cdot S_{UT})^2}{S_e} = \log \frac{(0.9 \cdot 560 \text{ MPa})^2}{87.5 \text{ MPa}} = 3.464 \log \text{ MPa}$$

GIVEN THE REVERSING STRESS OF 208.3 MPa

$$N = \frac{10^{b/m}}{S_f^{1/m}} = \frac{10^{3.464 \log \text{ MPa} / 0.2535}}{(208.3 \text{ MPa})^{1/0.2535}} = \frac{10^{3.464 / 0.2535} 10^{\log \text{ MPa}}}{(208.3 \text{ MPa})^{1/0.2535}}$$

$$= \boxed{33.0(10^3) \text{ CYCLES}}$$

Summary:

THE SN DIAGRAM WAS CONSTRUCTED USING THE CORRECTED ENDURANCE LIMIT THAT ACCOUNTS FOR THE SPECIFIC CONDITIONS OF THE COMPONENT BEING CONSIDERED.