PROBLEM 11 DETERMINE THE DEPLECTION AND CURTATURE OF POINT C USING THE MOMENT AREA METHOD. COMPARE THESE RESULTS TO TOOR PREVIOUS SOUTHOUS.

GIVEN:

CONSTRUCTS

1. 3.2m LONG BEAM WITH 1.2m HERITCHE EXTENSION AT MED-SPAN

2. SIMPLY SUPPORTED AT ONC END AND AT CENTER SPAN

3. CHBUE ATTIMENED TO THE TOP OF THE MENTICIPLE EXTENSION, TRAVELS OVER A FRICTIONNESS ROWER, AND HOLDS A SAN MASS.

ASSCMPTIONS

1. GRAVETY ACTS IN THE VERTICAL DERECTION

2. MATERIAL IS LINGUILY GLASTIC

3. DEPLECTEONS AND STRAINS ARE SMALL

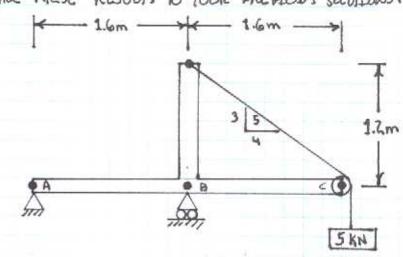
FIND:

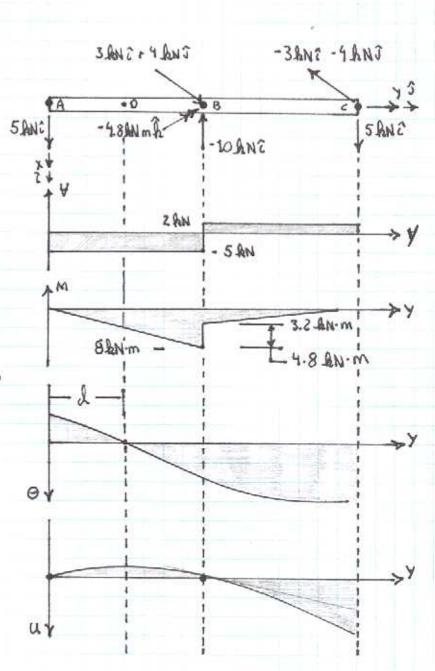
1. THE DEFLECTION OF PLINT C USING THE MOMENT AREA METHOD

## SOLUTION:

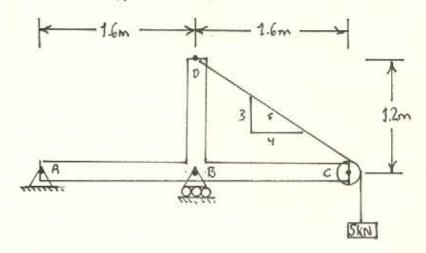
THE FIGURES TO THE RIGHT
SHOW THE ORIGINAL BEAM,
A PREE BODY DIAGRAM OF THE
BEAM, THE SHEAR FORCE, BENDENG
MOMENT, CURVETURE, AWD DEFLECTION
DIAGRAMS.

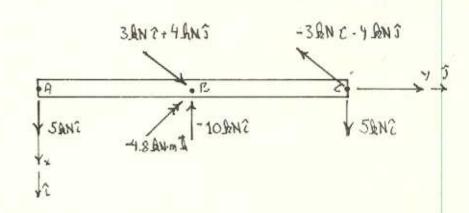
THE NORMAL FORCE DIAGRAM
HAS NO BEGAING ON THE SCUTTON
TO THE PROBLEM ASKED AND
THEREFORE IS NOT SHOWN.





SOCUENCE THE PROBLEM USING SINGULARITY FUNCTIONS





= 5kN<y-0>-1-7kN<y-1.6m>-1-4.8kN·m<y-1.6m>z + 2kN <y-3.2m>-1 1

= [-5kN(y-0)-1+7kN(y-1.6m)-1+4.8kN·m(y-1.6m)-2-2kN(y-3.2m)-1] dy

=-5kN<y-09+7kN<y-1.6m>+4.8kN·m<y-1.6m7-1-ZkN<y-32m> @

= [[-5kN<y-0)+7kN<y-1.6m)+4.8kNm<y-1.6m)-1-2kN</p>

= -5kn<y-051+7kn<y-1.6m)+4.8knm<y-1.6m)-2kn<y-3.2m)1

$$\begin{split} \Theta(s_{1}) &= \frac{1}{ET} \int M \, dy \\ &= \frac{1}{ET} \int \left[ 5.RN \left( y - 0 \right)^{2} - 7.RN \left( y - 1.6m \right)^{2} - 4.8.RN \cdot m \left( y - 1.6m \right)^{2} + 2.RN \left( y - 3.2m \right)^{2} \right] dy \\ &= \frac{5.RN}{2ET} \left( y - 0 \right)^{2} - \frac{7.RN}{2ET} \left( y - 1.6m \right)^{2} - \frac{4.8.RN \cdot m}{ET} \left( y - 1.6m \right)^{2} + \frac{2.RN}{2ET} \left( y - 3.2m \right)^{2} + C_{2} \\ &= \frac{5.RN}{2ET} \left( y - 0 \right)^{2} - \frac{7.RN}{2ET} \left( y - 1.6m \right)^{2} - \frac{4.8.RN \cdot m}{ET} \left( y - 1.6m \right)^{2} + \frac{1.RN}{ET} \left( y - 3.2m \right)^{2} + C_{3} \\ &= \frac{2.5.RN}{ET} \left( y - 0 \right)^{2} - \frac{3.5.RN}{ET} \left( y - 1.6m \right)^{2} - \frac{4.8.RN \cdot m}{ET} \left( y - 1.6m \right)^{2} + \frac{1.RN}{ET} \left( y - 3.2m \right)^{2} + C_{3} \right] G(y) \end{split}$$

$$U(Y) = \int G(Y) dY$$

$$= \int \left[ \frac{2.5 RN}{EI} \langle Y - 0 \rangle^2 - \frac{3.5 RN}{EI} \langle Y - 1.6 m \rangle^2 - \frac{4.8 RN}{EI} \langle Y - 1.6 m \rangle^4 + \frac{1}{EI} \langle Y - 3.2 m \rangle^2 + C_1 \right] dY$$

$$= \frac{2.5 RN}{3 EI} \langle Y - 0 \rangle^3 - \frac{3.5 RN}{3 EI} \langle Y - 1.6 m \rangle^2 - \frac{4.8 LNm}{2 EI} \langle Y - 1.6 m \rangle^2 + \frac{1}{3} \frac{RN}{EI} \langle Y - 3.2 m \rangle^2 + C_1 Y + C_2$$

THE TWO BOUNDARY CONDITIONS FOR THIS PROBLEM ARE

Using (S) AND APPLYING THE FIRST BOUNDART CONSITION, (6)
$$U(0) = 0 = \frac{2.5 \, \text{kn}}{3 \, \text{ET}} (0)^3 + C_1(0) + C_2 \implies C_2 = 0$$
(8)

SUBSTRICTING (8) INTO (5) AND APPLYING THE SECOND BOUNDARY CONDITION (7)

$$\Rightarrow C_1 = -\frac{2.5 \text{ kN}}{3 \text{ EI}} \cdot \frac{(1.6 \text{ m})^3}{(1.6 \text{ m})^3} = -\frac{2.5 \text{ kN}}{3 \text{ E.I}} (1.6 \text{ m})^2 = -\frac{2.133 \text{ kN} \cdot \text{m}^2}{\text{EI}}$$

THEREFORE

$$\begin{split} & (L(Y) = \frac{2.5 \text{ kN}}{3 \text{ ET}} \langle Y - O \rangle^{\frac{3}{2}} \frac{3.5 \text{ kN}}{8 \text{ ET}} \langle Y - 1.6 \text{ m} \rangle^{\frac{3}{2}} - \frac{4.8 \text{ kN} \cdot \text{m}}{2 \cdot \text{E.T}} \langle Y - 1.6 \text{ m} \rangle^{\frac{3}{2}} + \frac{1}{3} \frac{1}{6 \text{ kN}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 1.6 \text{ m} \rangle^{\frac{3}{2}} + \frac{1}{6 \text{ kN}} \langle Y - 1.6 \text{ m} \rangle^{\frac{3}{2}} + \frac{1}{6 \text{ kN}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y - 3.2 \text{ m} \rangle^{\frac{3}{2}} - \frac{2.133 \text{ kN} \cdot \text{m}^2}{6 \text{ ET}} \langle Y$$