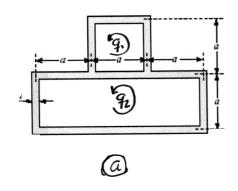
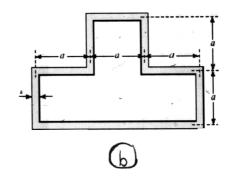
NAME: SOLUTION

Problem 1: For the two beam sections shown, calculate the shear stress in each of the members of both sections given that a torque T is applied to the structures.





FOR

$$Q_{b} = \frac{T}{Z \cdot A} = \frac{T}{Z \cdot (a^{2} + 3a^{2})} = \frac{T}{8a^{2}} \Rightarrow \frac{T}{C_{b} = \frac{q_{b}}{t} = \frac{T}{8 \cdot t \cdot a^{2}}}$$

$$Q_{b} = \frac{(1+\nu) \cdot T \cdot L \cdot 10 \cdot a}{2 \cdot E \cdot (4 \cdot a^{2})^{2} t} = \frac{(1+\nu) \cdot T \cdot L}{E \cdot a^{3} \cdot t} \cdot \frac{5}{16}$$
(2)

FOR @ IT IS NECESSARY TO COMPOTE THE Q'S IN EACH SEGMENT FIRST.
STARTING WITH THE CALCULATION OF THE TORQUE

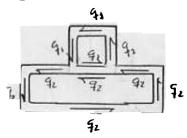
$$T = 2[q_1 \cdot \alpha^2 + q_2 \cdot 3\alpha^2] = 2 \cdot q_1 \cdot \alpha^2 + 6 \cdot q_2 \cdot \alpha^2$$

NOW CALCULATING THE ANGLE OF TWIST FOR EACH SEGMENT

$$\Theta = \frac{(1+\nu)\cdot L}{E \alpha^2} \left[\frac{3\cdot q_1 \cdot \alpha}{t} + \frac{\alpha(q_1 - q_2)}{t} \right]$$

$$\Theta = \frac{(1+\nu)\cdot L}{E \cdot \alpha \cdot t} \left[4\cdot q_1 - q_2 \right]$$

$$\frac{\Theta \cdot E \cdot \alpha \cdot t}{(1+\nu)\cdot L} = 4\cdot q_1 - q_2 = C \qquad (7)$$



$$\frac{(1+\nu)\cdot L}{3Ea^2} \left[\frac{7\cdot q_2\cdot a}{t} + \frac{\alpha(q_2-q_1)}{t} \right] = \frac{(1+\nu)\cdot L}{3E\cdot a\cdot t} \left[8\cdot q_2 - q_1 \right]$$

$$\frac{\bigcirc \cdot \cancel{\xi} \cdot \alpha \cdot t}{(1+\nu) \cdot L} = \frac{992 - 9}{3} = C \qquad \textbf{G}$$

EQUATING (1) 1(6)

$$4q_1-q_2 = 8q_2-q_1 \Rightarrow 2q_1-3q_2=8q_2-q_1 \Rightarrow 13q_1=11q_2$$

 $q_1=\frac{11}{13}q_2$ (6)

$$T = 2 \cdot \frac{11}{13} \cdot q_2 \cdot Q^2 + 6 \cdot q_2 \cdot Q^2 = \left[\frac{22}{13} + \frac{78}{13} \right] q_2 \cdot Q^2 = \frac{100}{13} \cdot q_2 \cdot Q^2$$

$$q_2 = 0.13 \frac{T}{Q^2} \qquad (7)$$

SCBSTITUTING (7) INTO (6)

$$q_1 = \frac{11}{13} \cdot \frac{1^3}{100} \frac{T}{a^2} = 0.11 \frac{T}{a^2}$$

HE ANGLE OF TWIST CAN NOW BE CHLCCLATED FROM (4)

$$\Theta = \frac{(1+\nu)\cdot L}{E\cdot a\cdot t} \left[4\cdot 0.11\frac{T}{a^2} - 0.13\frac{T}{a^2} \right] = 0.31 \cdot \frac{(1+\nu)\cdot L\cdot T}{E\cdot a^3\cdot t}$$

THE SHEAR STRESS IN THE UPPER I SEGMENTS CAN NOW BE

$$\mathcal{C}_1 = \frac{q_1}{t} = 0.11 \frac{T}{\alpha^2 t}$$

THE SHEAR STRESS IN THE LOGER SEGMENTS

$$\mathcal{L}_{i} = \frac{q_{i}}{t} = \begin{bmatrix} 0.13 \frac{T}{a^{2} \cdot t} \end{bmatrix}$$
 (1)

AND THE SHEAR STRESS IN THE INTERSECTING SEGMENT

$$C_{32} = \frac{q_1 - q_2}{t} = (0.11 - 0.13) \frac{T}{a^2 t} = \frac{1}{0.02 a^2 t}$$

Problem 2: Determine the torsional stiffness for both of these cross-sections. Which of the structures is stiffer?

DEFINING THE TORSIONAL STIFFNESS AS K= 0

$$\frac{E \cdot a^{3} \cdot t}{0.31 \cdot (1+V) \cdot L} = 3.226 \frac{E \cdot a^{3} \cdot t}{(1+V) \cdot L}$$

$$\frac{16}{5} \cdot \frac{E \cdot a^{3} t}{(1+\nu) \cdot L} = 3.200 \cdot \frac{E \cdot a^{3} \cdot t}{(1+\nu) \cdot L}$$

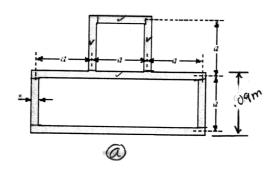
GIVEN G= E Z(1+V)

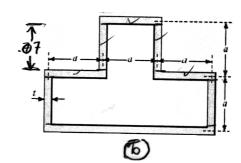
$$K_{A} = 6.452 \frac{G \cdot G^{3} \cdot c}{L}$$

$$K_{13} = 6.400 \frac{6 \cdot a^{3} \cdot t}{L}$$

Problem 3: For the structures given in Problem 1, let a=80mm, t=10mm, G=80GPa, and T=4kN-m. Assume that in addition a horizontal moment is applied through the centroid directed to the right. Draw the stress cube and Mohr's circle for an element on the to segment of each of the cross-sections.







FOR CROSS SECTION @

 $V = \frac{(.07m)(.01m)(.165m) + 2 \cdot (.08m)(.01m)(.13m) + (.25m)(.01m)(.085m) + 2(.07m)(.01m)(.045m)}{(.07m)(.01m) + 2(.08m)(.01m) + (.25)(.01m) + 2 \cdot (.07m)(.01m) + 2 \cdot (.07m)(.01m)}$

0.07029m = 70.29mm

 $I_q = \frac{1}{12} (.09m) (.08m)^3 + (.09m) (.08m) (.13m - .07029m)^2$ $\frac{1}{17}(.07m)(.07m)^3 - (.07m)(.07m)(.125m - .07029m)^2$

 $+\frac{1}{12}(0.25m)(.09m)^3+(0.25m)(.09m)(.045m-.07029m)_3^2$ $-\frac{1}{17}$ (G.23m) (.07m) 3 - (0.23m) (.07m) (.045m - 07029m)

 $= 25.55 (10^{-6}) \text{ m}^4$

FOR CROSS SECTION (b)

 $V_{b} = \frac{(.09m)(.01m)(.165m) + 2 \cdot (.01)(.07m)(.125m) + 2 \cdot (.09m)(.01m)(.085m) + 2 \cdot (.01)(.07)(.045) + (.25m)(.01m)(.025m)}{(09)(.01m) + 2 \cdot (.01m)(.07m) + 2 \cdot (.09m)(.01m) + 2 \cdot (.01)(.07) + (.25m)(.01m)(.07m)(.07m)}$

= 0.06900m = 69.00mm

Ib= 12(.09m)(.08m)3+(.09m)(.08m)(.13m-.0690m)2 -12(.07m)(.08m)3-(.07m)(.08m)(.12m-.0690m)2 + 12 (.25m)(.09m)3+(.25m)(.09m)(.045m-,0690m)2 12(.23m)(.07m)3-(.23m)(.07m)(.045m-.0690m)2 = 25.38(10-6) m4

THE NORMAL STRESS CAN NOW BE CALCULATED IN THE UPDER SEGMENT OF CRUSS-SECTION &

$$\sqrt{E} = \frac{MC}{I} = \frac{200^{3}) \text{ N.m. } (0.170 - 0.07029 \text{ m})}{25.55 (10^{-6}) \text{ m}^{4}} = 7.805 (10^{6}) \frac{N}{m^{2}} = \frac{7.805 \text{ M/a}}{25.55 (10^{-6}) \text{ m}^{4}} = \frac{7.805 \text{ M/a}}{25.55 (10^{-6}) \text{$$

THE SHELD STRESS FOR THIS SECTION CAN ALSO BE CALLCLUTED

$$C_{G} = 11 \cdot \frac{4(40^{3}) \text{ N.m}}{600 \text{ m}} = 6.875(40^{6}) \frac{\text{M}_{2}}{\text{m}_{2}} = 6.875 \text{ MPc}$$
 7.805 mPc
 7.805 mPc
 7.805 mPc
 7.805 mPc

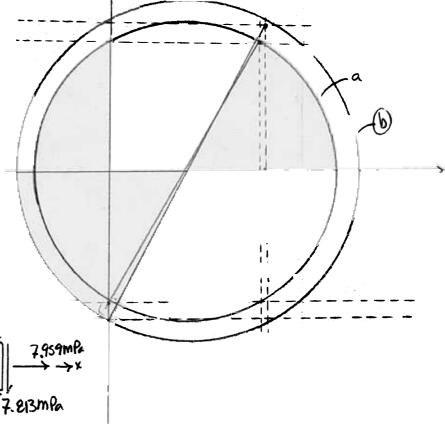
THE NORMAL STRESS IN SECTION B

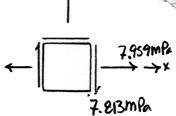
$$T_{B} = \frac{M \cdot C}{T} = \frac{2(10^{3} \text{ N·m} \cdot (0.170\text{m} - 0.0690\text{m})}{25.38(10^{-6})\text{m}^{4}}$$

= 7.959 MPa

THE SHEAR STRESS IN SECTION B

$$V_B = \frac{4(10^3) \text{ N.m}}{8 \cdot (.01 \text{ m}) (.00 \text{ m}^2)^2}$$
7. 813 MPa





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