PAGBLET 12] DETERMINE THE DEFLECTION AND CURVATURE OF POINTS "C"AND"D" ALONG WITH THE LOCATION OF THE MAXIMUM DEPLECTION USING THE MOMENT AREA METHOD.

CONSTRAENTS

- 1. 20 St long beam with simple supports at Both ends
- 2. A DESTRICTED LOAD OF 2013) Mys IS APPLIED ONER FROM THE MID-SPAN TO THE GND OF THE BEAM.
- 3. 9(10) D WAD APPLIED AT QUARTER SPAN

ASSOMMIONS

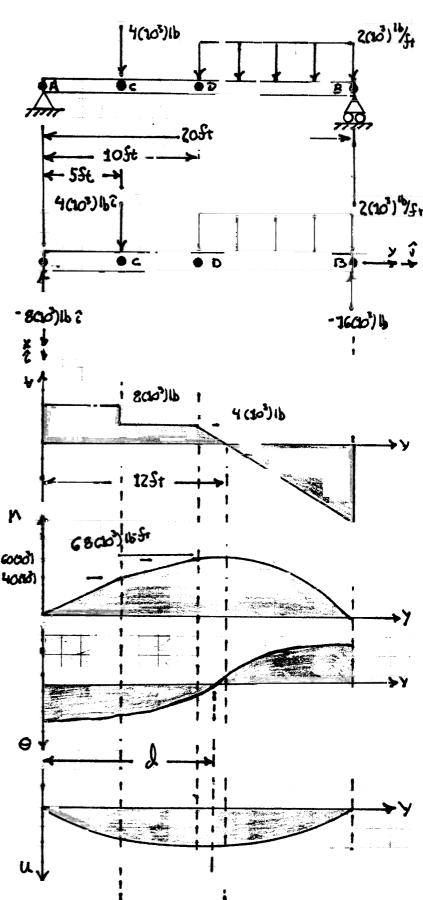
- 1. THE BEAM IS MADE OF LINEAR ELASTIC MATERIAL
- 2. ALL DEPLECTIONS AND STRAINS IN THE BEAM ARE SMALL

EIND:

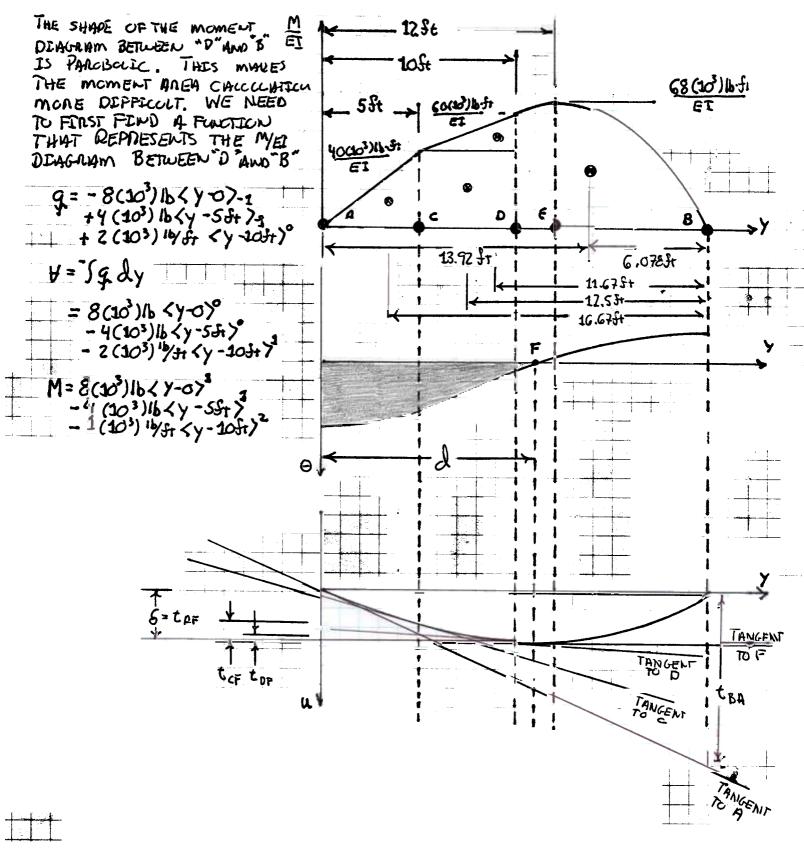
- 4. Determine the Deflection at Points "C"and "D"
- 2. DETERMENE THE CURVATURE AT PURNTS "C" AND "D"

## SOLUTION:

THE FIGURES TO THE RICHT
SHOW THE ORIGIONAL BEAM,
A FREE BODY DIAGRAM OF
THE BEAM, THE SHEAR FORCE
DIAGRAM, BENDING MOMENT
DIAGRAM, AND DEPLECTION
DIAGRAMS WERE DRAWN BY
INSPECTION FROM THE
FREE-BODY DIAGRAM AND
AN UNDERSTANDING OF THE
INTEGRAL RELATIONSHIP
BETWEEN THE FIGURES.



THE SOLUTION NEEDS TO START WITH THE LOCADION OF THE MAXIMOM DEPLECTION OF THE ELASTIC CURVE.



IN THE REGION FROM 10St TO 20St (BETWEEN "D"AND "B")

$$\frac{M^{*}}{EI} = \frac{1}{EI} \left[ 8(30^{3}) lb \cdot y - 4(30^{3}) lb \cdot y + 20(30^{3}) lb \cdot fr \right]$$

$$= \prod_{i=1}^{1} \left[ 24(10^3) \text{ lb·y} - 80(10^3) \text{ lb·ft} - 1(10^3) \frac{16}{5} \text{ ft·y}^2 \right]$$

THE AREA UNDER THE  $\frac{M}{EI}$  DIAGRAM BETWEEN D'AND B'IS CACCUARDO  $A = \int_{EI}^{M^*} dy = \frac{1}{EI} \left( \left[ 24(10^3) \text{ lb·y} - 80(10^3) \text{ lb·ft} - 1(10^3) \frac{1}{10} \cdot y^2 \right] dy$   $= \frac{1}{EI} \left[ 17(10^3) \text{ lb·y}^2 - 80(10^3) \text{ lb·ft} \cdot y - .3333(10^3) \frac{1}{10} \cdot y^3 \right]_{10}^{20}$   $= \frac{466.9(10^3) \text{ lb·ft}^2}{60}$ 

THE CENTROID OF THIS CROSS SECTION WITH RESPECT TO THE ORIGIN

$$\overline{Y} = \frac{\int y \cdot \frac{M^*}{E_I} \cdot dy}{A}$$

 $\int Y \cdot \int_{E_{1}}^{\infty} dy = \int_{E_{1}}^{\infty} \int [24(30^{3})lb \cdot y^{2} - 80(30^{3})lb \cdot f_{1} \cdot y - 1(30^{3})f_{1} \cdot y^{3}] dy$   $= \int_{E_{1}}^{\infty} \left[ 8(30^{3})lb \cdot y^{3} - 40(30^{3})lb \cdot f_{1} \cdot y^{2} - .25(30^{3})f_{1}^{2} \cdot y^{4} \right]_{10}^{\infty}$   $= \underbrace{6.500(30^{6})lb \cdot f_{1}^{3}}_{E_{1}} \underbrace{4.66.9(30^{3})lb \cdot f_{1}^{2}}_{E_{3}} = 13.925t$ 

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Now the can be calculated

t_{BA} = (16.675t) \cdot \frac{1}{2} \cdot (55t) \cdot \frac{40(10^3) \cdot b \cdot f_1}{EI} + (12.55t) \cdot (55t) \cdot (\frac{40(10^3) \cdot b \cdot f_1}{EI}) + (6.6785t) \cdot (\frac{466.9(10^3) \cdot b \cdot f_1^2}{EI})

= \frac{1}{EI} \cdot 7.588(10^6) \cdot b \cdot f_1^3

Now the angle \Theta_A can be calculated using theorem II

\Theta_A \approx \text{Tan }\Theta_A = \frac{7.588(10^6) \cdot b \cdot f_1^3}{EI} = \frac{379.4(10^3) \cdot b \cdot f_1^2}{EI}

Now the angle \Theta_A is calculated with the use of theorem I
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 $\Theta_{A} = \int_{EI}^{EI} dy = \frac{1}{2} \cdot (55t) \cdot (\frac{40(20^{3})16 \cdot 5^{4}}{EI}) + (55t) \cdot (\frac{40(20^{3})16 \cdot 5^{4}}{EI}) + \frac{1}{2} \cdot (55t) \cdot (\frac{50(20^{3})16 \cdot 5^{4}}{EI})$ 

=  $\frac{350.0(10^3) |b.5e^2+\frac{1}{61}}{EI} \left[12(10^3) |b.y^2-80(10^3) |b.f+y-.3333(10^3) |b.y^3|^{d}\right]$ 

= 350.0 (103) lb.fr + = [12(103) lb.d2 - 80(103) lb.fr.d - 3333(103) lb d3

\_ 68.7(103)1b.fe2]

= = [-0.3333(103) ft. d3 + 12(103) lb. d2 - 80(103) lb. ft. d + 283.3(103) lb. ft]

 $0 = 0.3333(10^3) f_t d^3 - 12(10^3) lb d^2 + 80(10^3) lb f_t d + 96.10(10^3) lb f_t^2$   $0 = d^3 - 36 f_t d^2 + 240 f_t^2 d + 288.3 f_t^3$ 

d = -1.04, 10.48, 26.55

THE ONLY ROCT IN THE DOMAIN OF THE PROBLEM IS

d= 10.48

THE DEPLECTEONS AT "C" AND "D" CAN NOW BE CALCULATED

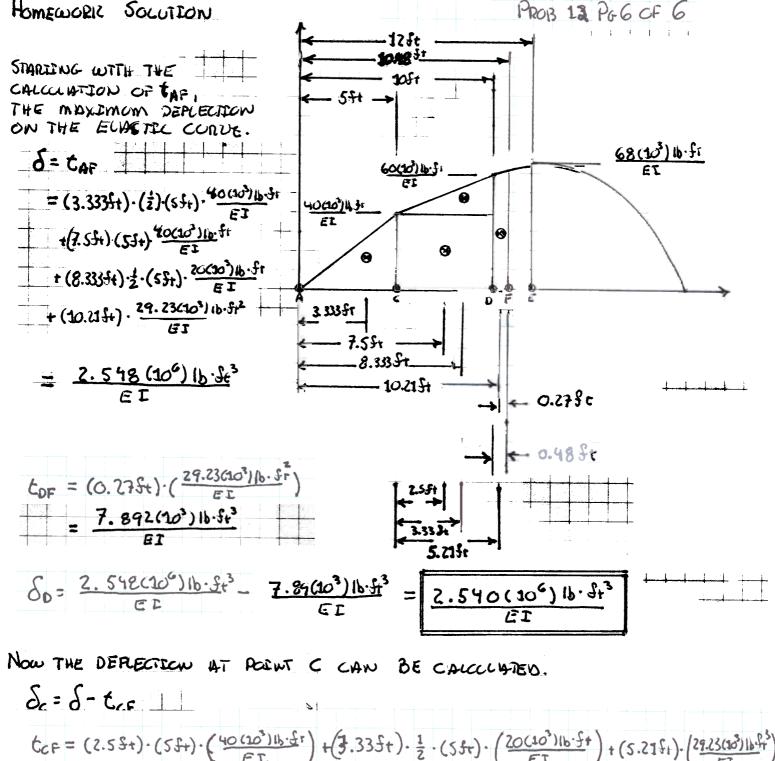
Sp = tar - tor

THE CENTRALD OF SECTION OF NEEDS TO BE CHECKINED.

 $\nabla_{F} = 30 \frac{1}{2} \frac{1}{4} \frac{1}{4}$ 

 $= \frac{1}{6!} \left[ 8(10^3) | \text{lb} \cdot \text{y}^3 - 90 (10^3) | \text{lb} \cdot \text{fr} \cdot \text{y}^2 - .25 (10^3) | \text{fr} \cdot \text{y}^4 \right]_{1057}$   $= \frac{1}{6!} \cdot 299.3 (10^3) | \text{lb} \cdot \text{fr}^3$ 

 $\frac{7}{7} = \frac{299.3(20^{3}) \text{ lb·fs}^{3}}{29.23(10^{3}) \text{ lb·fs}^{2}} = \frac{10.21 \text{ ft}}{10.21 \text{ ft}}$ 



= 818.8 (103) (b.fr3
ET

2510 (251) (337) (251)

$$\delta_{c} = \frac{2.548(10^{6}) \text{ lb.ft}^{3}}{\text{EL}} = \frac{818.8(10^{3}) \text{ lb.ft}^{3}}{\text{EL}} = \frac{1.729(10^{3}) \text{ lb.ft}^{3}}{\text{EL}}$$

Summary: This may have not been the best way to schoe this Anchem.
The distributed load couses a parabolic distribution in the moment that Forces the march and moment aren to be calculated through direct prechara.