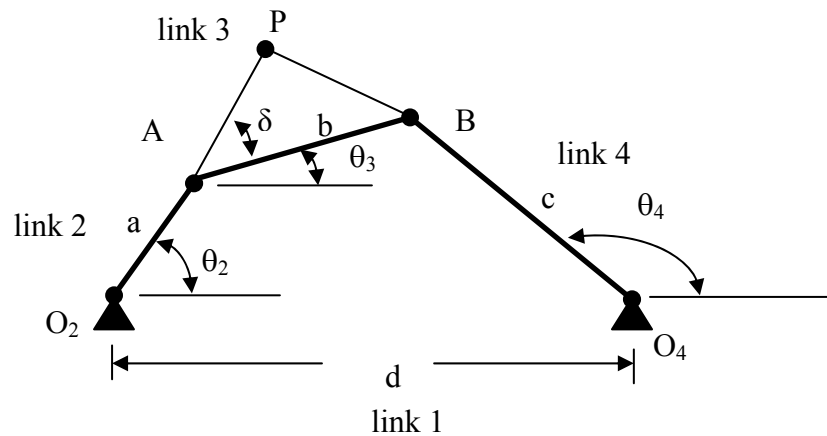


NAME:

PROBLEM 1: Given:

Link 1 = $d = 9\text{in}$	Link 2 = $a = 7\text{in}$	Link 3 = $b = 11\text{in}$	Link 4 = $c = 6\text{in}$
$\theta_2 = 120^\circ$	$\omega_2 = 15 \text{ 1/s}$	$\alpha_2 = -65 \text{ 1/s}^2$	
$r_{pa} = 15\text{in}$	$\delta = 60^\circ$		



Calculate:

$$r_{Ax} = -3.50 \text{ (-3.50)} \quad r_{Ay} = 6.06 \text{ (6.06)} \quad \theta_3 = -1.3 \text{ (-50.4)} \quad \theta_4 = 104.5 \text{ (-156.3)}$$

$$r_{Bx} = 7.50 \text{ (3.51)} \quad r_{By} = 5.81 \text{ (-2.42)} \quad \dot{\theta}_3 = 2.65 \text{ (9.86)} \quad \dot{\theta}_4 = 15.54 \text{ (-3.03)}$$

$$r_{Px} = 4.30 \text{ (11.29)} \quad r_{Py} = 18.88 \text{ (8.56)} \quad \ddot{\theta}_3 = -6.95 \text{ (-26.62)} \quad \ddot{\theta}_4 = -127.3 \text{ (94.2)}$$

$$v_{Ax} = -90.93 \text{ (-90.93)} \quad v_{Ay} = -52.50 \text{ (-52.50)} \quad a_{Ax} = 1181. \text{ (1181)} \quad a_{Ay} = -1136 \text{ (-1136)}$$

$$v_{Bx} = -90.26 \text{ (-7.31)} \quad v_{By} = -23.35 \text{ (16.62)} \quad a_{Bx} = 1102 \text{ (278)} \quad a_{By} = -1211 \text{ (-495)}$$

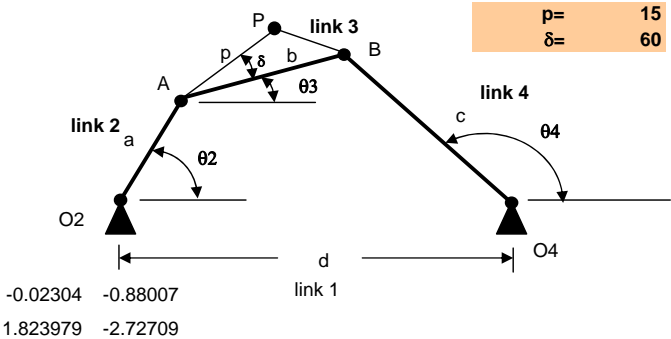
$$v_{Px} = -124.9 \text{ (-115.5)} \quad v_{Py} = -31.8 \text{ (93.4)} \quad a_{Px} = 1216 \text{ (-192)} \quad a_{Py} = -1281 \text{ (-1766)}$$

The crossed solution is in “()”

4-Bar Linkage

a=	7	Link 2
b=	11	Link 3
c=	6	Link 4
d=	9	Link 1
$\theta_2 =$	120	2.094395102
$\dot{\theta}_2 =$	15	$\frac{1}{s}$
$\ddot{\theta}_2 =$	-65	$\frac{1}{s^2}$
By=	5.81	-2.42
Bx=	7.50	3.51
$\theta_3 =$	-1.3	-50.4
$\theta_4 =$	104.5	-156.3
$\dot{\theta}_3 =$	2.6504E+00	9.8626E+00
$\dot{\theta}_4 =$	1.5539E+01	-3.0259E+00
$\ddot{\theta}_3 =$	-6.9538E+00	-2.6177E+01
$\ddot{\theta}_4 =$	-1.2733E+02	9.4202E+01

K1= 4.6800E+00
K2= 4.8497E-01
K3= 3.3923E+00
K4= -1.4036E+01



p= 15
delta= 60

	x comp	y comp	mag	angle	i	j
rO4=	9.00	0.00	9.00	0.0	1.000	0.000
rA=	-3.50	6.06	7.00	120.0	-0.500	0.866
rBA=	11.00	-0.25	11.00	-1.3	1.000	-0.023
rBO4=	-1.50	5.81	6.00	104.5	-0.250	0.968
rB=	7.50	5.81	9.48	37.8	0.790	0.612
rPA=	7.80	12.81	15.00	58.7	0.520	0.854
rP=	4.30	18.88	19.36	77.2	0.222	0.975
vA=	-90.93	-52.50	105.00	-150.0	-0.866	-0.500
vBA=	0.67	29.15	29.15	88.7	0.023	1.000
vB=	-90.26	-23.35	93.23	-165.5	-0.968	-0.250
vPA=	-33.96	20.67	39.76	148.7	-0.854	0.520
vP=	-124.89	-31.83	128.89	-165.7	-0.969	-0.247
aA=	1181.54	-1136.49	1639.41	-43.9	0.721	-0.693
aBA=	-79.01	-74.69	108.73	-136.6	-0.727	-0.687
aB=	1102.53	-1211.18	1637.84	-47.7	0.673	-0.739
aPA=	34.33	-144.23	148.26	-76.6	0.232	-0.973
aP=	1215.88	-1280.72	1765.96	-46.5	0.689	-0.725
ALT	x comp	y comp	mag	angle	i	j
rO4=	9.00	0.00	9.00	0.0	1.000	0.000
rA=	-3.50	6.06	7.00	120.0	-0.500	0.866
rBA=	7.01	-8.48	11.00	-50.4	0.637	-0.771
rBO4=	-5.49	-2.42	6.00	-156.3	-0.915	-0.403
rB=	3.51	-2.42	4.26	-34.6	0.824	-0.567
rPA=	14.79	2.50	15.00	9.6	0.986	0.166
rP=	11.29	8.56	14.17	37.2	0.797	0.604
vA=	-90.93	-52.50	105.00	-150.0	-0.866	-0.500
vBA=	83.62	69.12	108.49	39.6	0.771	0.637
vB=	-7.31	16.62	18.16	113.7	-0.403	0.915
vPA=	-24.61	145.88	147.94	99.6	-0.166	0.986
vP=	-115.54	93.38	148.56	141.1	-0.778	0.629
aA=	1181.54	-1136.49	1639.41	-43.9	FALSE	-0.693
aBA=	-903.63	641.27	1108.04	144.6	-0.816	0.579
aB=	277.92	-495.22	567.88	-60.7	0.489	-0.872
aPA=	-1373.41	-629.90	1510.97	-155.4	-0.909	-0.417
aP=	-191.87	-1766.39	1776.78	-96.2	-0.108	-0.994

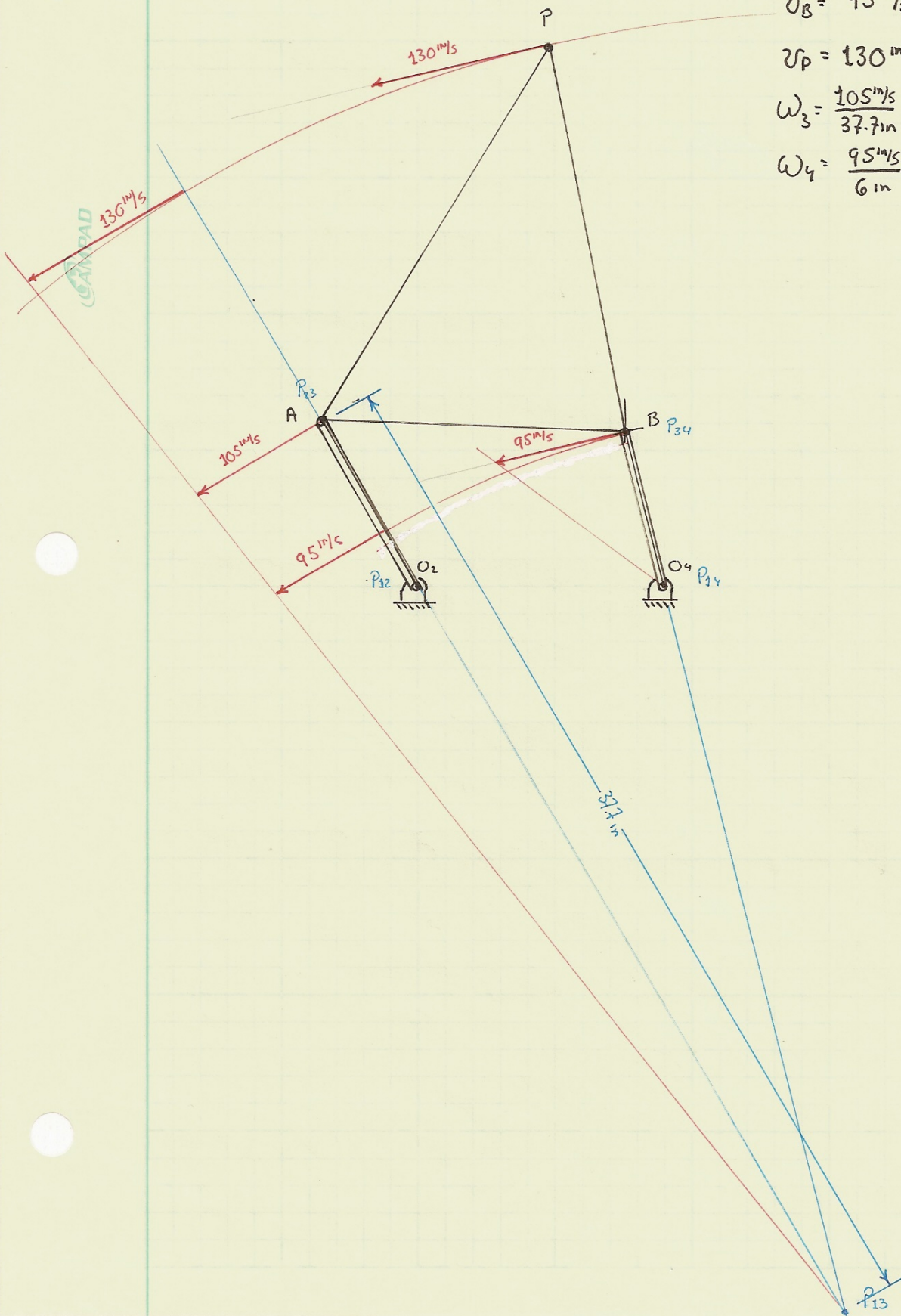
$$v_A = 105 \text{ m/s}$$

$$v_B = 95 \text{ m/s}$$

$$v_P = 130 \text{ m/s}$$

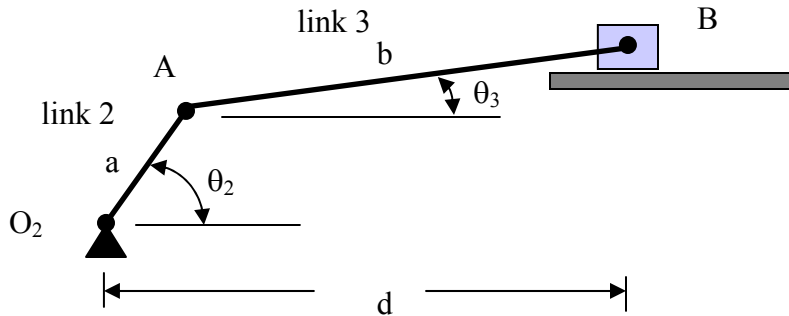
$$\omega_3 = \frac{105 \text{ m/s}}{37.7 \text{ in}} = 2.8 \text{ 1/s}$$

$$\omega_4 = \frac{95 \text{ m/s}}{6 \text{ in}} = 16 \text{ 1/s}$$



PROBLEM 2: Given:

$$\begin{array}{lll} \text{Offset} = 10\text{in} & \text{Link 2} = a = 7\text{in} & \text{Link 3} = b = 25\text{in} \\ \theta_2 = 330^\circ & \omega_2 = 100 \text{ 1/s} & \alpha_2 = 18 \text{ 1/s}^2 \end{array}$$



Calculate:

$$r_{Ax} = 6.06 \text{ (6.06)} \quad r_{Ay} = -3.50 \text{ (-3.50)} \quad \theta_3 = 32.7 \text{ (147.3)} \quad \ddot{\theta}_3 = -1136 \text{ (1136)}$$

$$r_{Bx} = 27.10 \text{ (-14.98)} \quad r_{By} = 10.00 \text{ (10.00)} \quad \dot{\theta}_3 = -28.81 \text{ (28.81)}$$

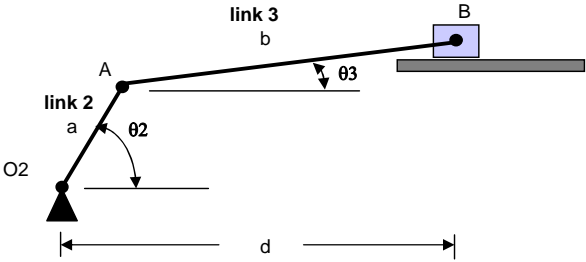
$$v_{Ax} = 350.0 \text{ (350.0)} \quad v_{Ay} = 606.2 \text{ (606.2)} \quad a_{Ax} = -60560 \text{ (-60560)} \quad a_{Ay} = 35110 \text{ (35110)}$$

$$v_{Bx} = 738.9 \text{ (-38.94)} \quad v_{By} = 0 \text{ (0)} \quad a_{Bx} = 62690 \text{ (-58430)} \quad a_{By} = 0 \text{ (0)}$$

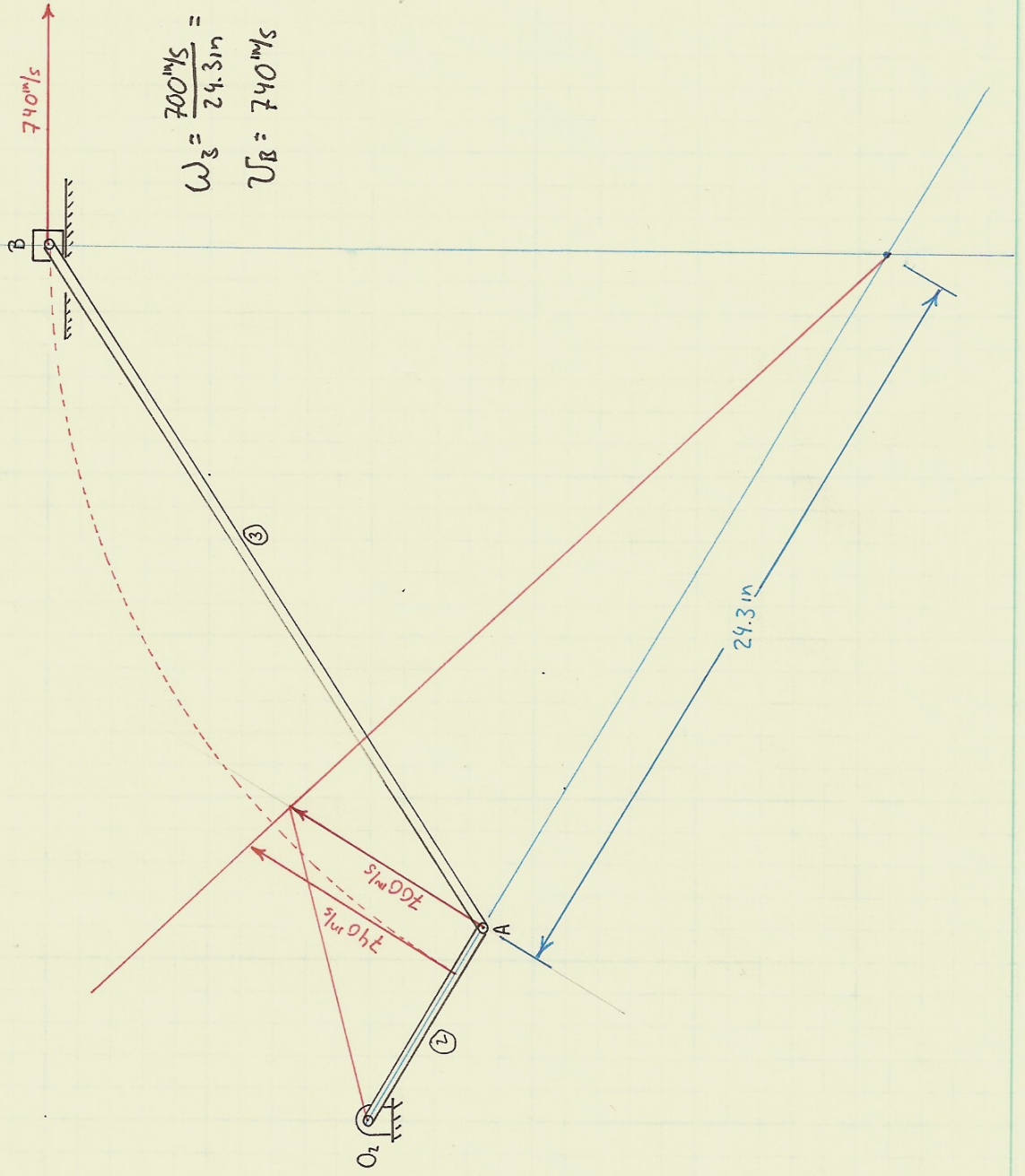
The crossed solution is in “()”

Slider Crank

a=	7	Link 2
b=	25	Link 3
c=	10	Link 1
$\theta_2 =$	330	5.759586532
$\dot{\theta}_2 =$	100	$\frac{1}{s}$
$\ddot{\theta}_2 =$	18	$\frac{1}{s^2}$
By=	10.00	10.00
Bx=	27.10	-14.98
$\theta_3 =$	32.7	147.3
$\dot{\theta}_3 =$	-28.81	28.81
$\ddot{\theta}_3 =$	-1136.01	1136.01
vB=	738.94	-38.94
aB=	-77635.22	-43482.34



	x comp	y comp	mag	angle	i	j
rB=	27.10	10.00	28.89	20.3	0.938	0.346
rA=	6.06	-3.50	7.00	-30.0	0.866	-0.500
rBA=	21.04	13.50	25.00	32.7	0.842	0.540
vB=	738.94	0.00	738.94	0.0	1.000	0.000
vA=	350.00	606.22	700.00	60.0	0.500	0.866
vBA=	388.94	-606.22	720.26	-57.3	0.540	-0.842
aB=	-62687.97	0.00	62687.97	180.0	-1.000	0.000
aA=	-60558.78	35109.12	70000.11	149.9	-0.865	0.502
aBA=	-2129.19	-35109.12	35173.62	-93.5	-0.061	-0.998
alt	x comp	y comp	mag	angle	i	j
rB=	-14.98	10.00	18.01	146.3	-0.832	0.555
rA=	6.06	-3.50	7.00	-30.0	0.866	-0.500
rBA=	-21.04	13.50	25.00	147.3	-0.842	0.540
vB=	-38.94	0.00	38.94	180.0	-1.000	0.000
vA=	350.00	606.22	700.00	60.0	0.500	0.866
vBA=	-388.94	-606.22	720.26	-122.7	-0.540	-0.842
aB=	-58429.59	0.00	58429.59	180.0	-1.000	0.000
aA=	-60558.78	35109.12	70000.11	149.9	-0.865	0.502
aBA=	2129.19	-35109.12	35173.62	-86.5	0.061	-0.998



$$\omega_3 = \frac{740 \text{ m/s}}{24.3 \text{ in}} = 29 \frac{1}{4} \text{ /s}$$

$$v_B = 740 \text{ m/s}$$

PROBLEM 4: Given:

Link 1 = $d = 3\text{in}$

Link 2 = $a = 10\text{in}$

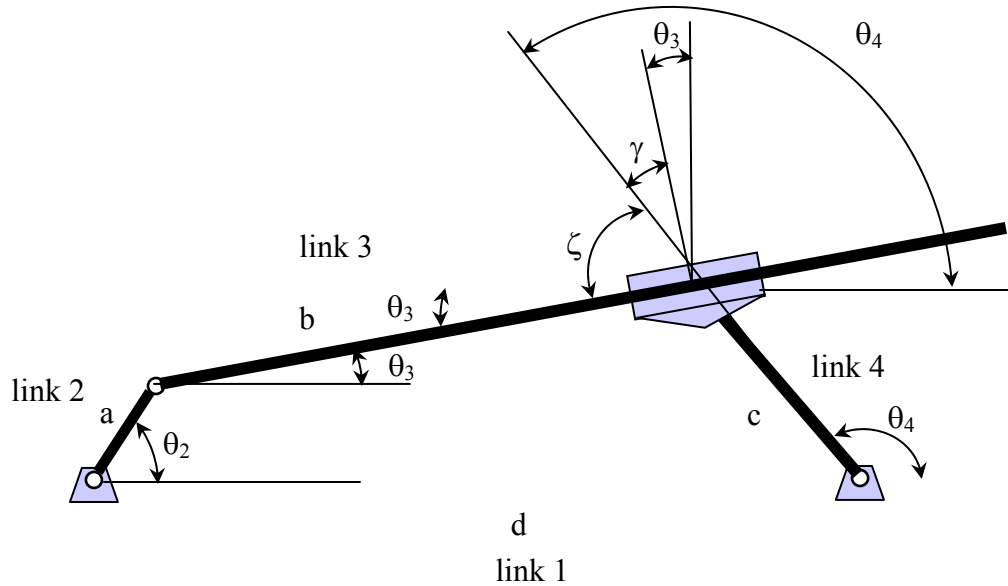
Link 4 = $c = 6\text{in}$

$\theta_2 = 45^\circ$

$\omega_2 = 24 \text{ 1/s}$

$\alpha_2 = 30 \text{ 1/s}^2$

$\gamma = -45^\circ$



Calculate:

$r_{Ax} = 7.07 \text{ (7.07)}$ $r_{Ay} = 7.07 \text{ (7.07)}$ $\theta_3 = -88.6 \text{ (28.7)}$ $\theta_4 = -43.6 \text{ (73.7)}$

$r_{Bx} = 7.35 \text{ (4.68)}$ $r_{By} = -4.14 \text{ (5.76)}$ $\dot{\theta}_3 = 23.75 \text{ (33.06)}$ $\dot{\theta}_4 = 23.75 \text{ (33.06)}$

$\dot{b} = 73.05 \text{ (-73.05)}$ $\ddot{b} = 1079 \text{ (-1079)}$ $\ddot{\theta}_3 = -212.9 \text{ (-217.8)}$ $\ddot{\theta}_4 = -212.9 \text{ (-217.8)}$

$v_{Ax} = -169.7 \text{ (-169.7)}$ $v_{Ay} = 169.7 \text{ (169.7)}$ $a_{Ax} = -4285 \text{ (-4285)}$ $a_{Ay} = -3861 \text{ (-3861)}$

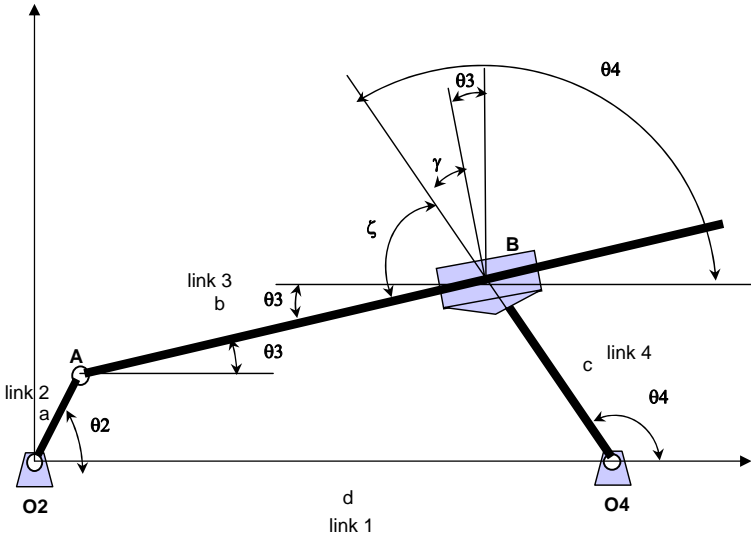
$v_{Bx} = 98.26 \text{ (-190.4)}$ $v_{By} = 103.2 \text{ (55.54)}$ $a_{Bx} = -3331 \text{ (-581.4)}$ $a_{By} = 1408 \text{ (-6661)}$

The crossed solution is in “()”

Inverted Slider Crank

a=	10	Link 2
c=	6	Link 4
d=	3	Link 1
$\theta_2 =$	45	
$\gamma =$	-45	
$\dot{\theta}_2 =$	24	$\frac{1}{s}$
$\ddot{\theta}_2 =$	30	$\frac{1}{s^2}$
b=	11.21	-2.73
$\theta_4 =$	-43.60	73.74
$\theta_3 =$	-88.60	28.74
$\dot{\theta}_4 =$	23.75	33.06
$\dot{\theta}_3 =$	23.75	33.06
b-dot=	73.05	-73.05
$\ddot{\theta}_4 =$	-212.93	-217.83
$\ddot{\theta}_3 =$	-212.93	-217.83
b-dotdot=	1078.84	-1078.84

$\zeta =$ 45
K1= -2.12132034
K2= -7.87867966
K3= 4.242640687

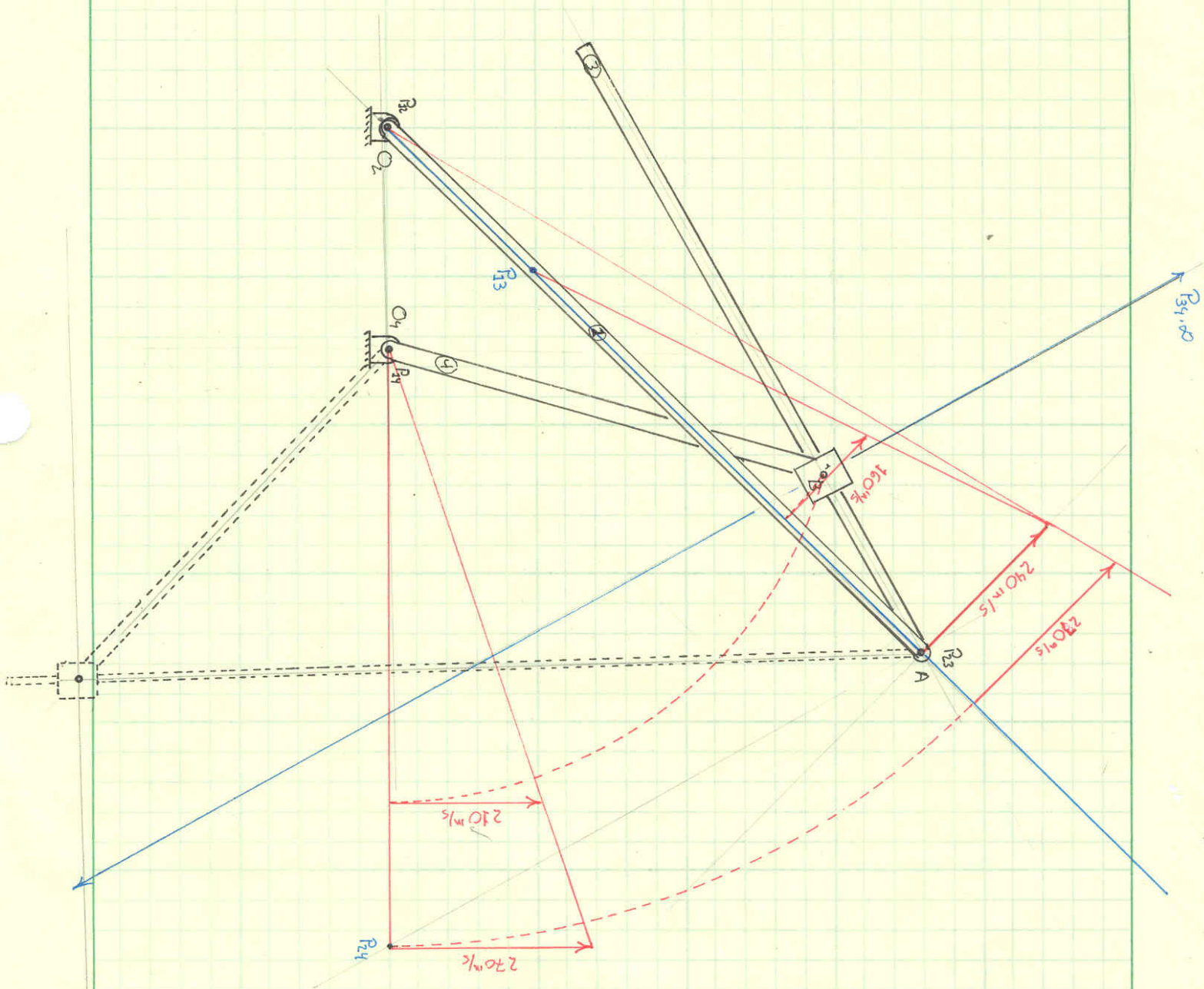


	x comp	y comp	mag	angle	i	j
rO4=	3.00	0.00	3.00	0.0	1.000	0.000
rA=	7.07	7.07	10.00	45.0	0.707	0.707
rBA=	0.27	-11.21	11.21	-88.6	0.024	-1.000
rBO4=	4.35	-4.14	6.00	-43.6	0.724	-0.690
rB=	7.35	-4.14	8.43	-29.4	0.871	-0.491
vA=	-169.71	169.71	240.00	135.0	-0.707	0.707
vBA=	267.97	-66.52	276.10	-13.9	0.971	-0.241
vB=	98.26	103.18	142.49	46.4	0.690	0.724
aA=	-4285.07	-3860.80	5767.81	-138.0	-0.743	-0.669
aBA=	953.67	5269.07	5354.68	79.7	0.178	0.984
aB=	-3331.40	1408.27	3616.83	157.1	-0.921	0.389
alt	x comp	y comp	mag	angle	i	j
rO4=	3.00	0.00	3.00	0.0	1.000	0.000
rA=	7.07	7.07	10.00	45.0	0.707	0.707
rBA=	-2.39	-1.31	2.73	-151.3	-0.877	-0.481
rBO4=	1.68	5.76	6.00	73.7	0.280	0.960
rB=	4.68	5.76	7.42	50.9	0.631	0.776
vA=	-169.71	169.71	240.00	135.0	-0.707	0.707
vBA=	-20.71	-114.16	116.03	-100.3	-0.178	-0.984
vB=	-190.41	55.54	198.35	163.7	-0.960	0.280
aA=	-4285.07	-3860.80	5767.81	-138.0	-0.743	-0.669
aBA=	3703.63	-2799.93	4642.89	-37.1	0.798	-0.603
aB=	-581.44	-6660.74	6686.07	-95.0	-0.087	-0.996

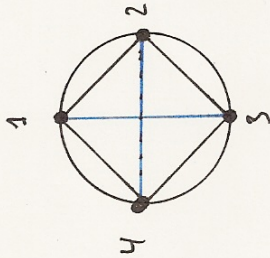
CROSSED SOLUTION

$$\omega_4 = \frac{270 \text{ m/s}}{8.05 \text{ m}} = 33 \text{ 1/s}$$

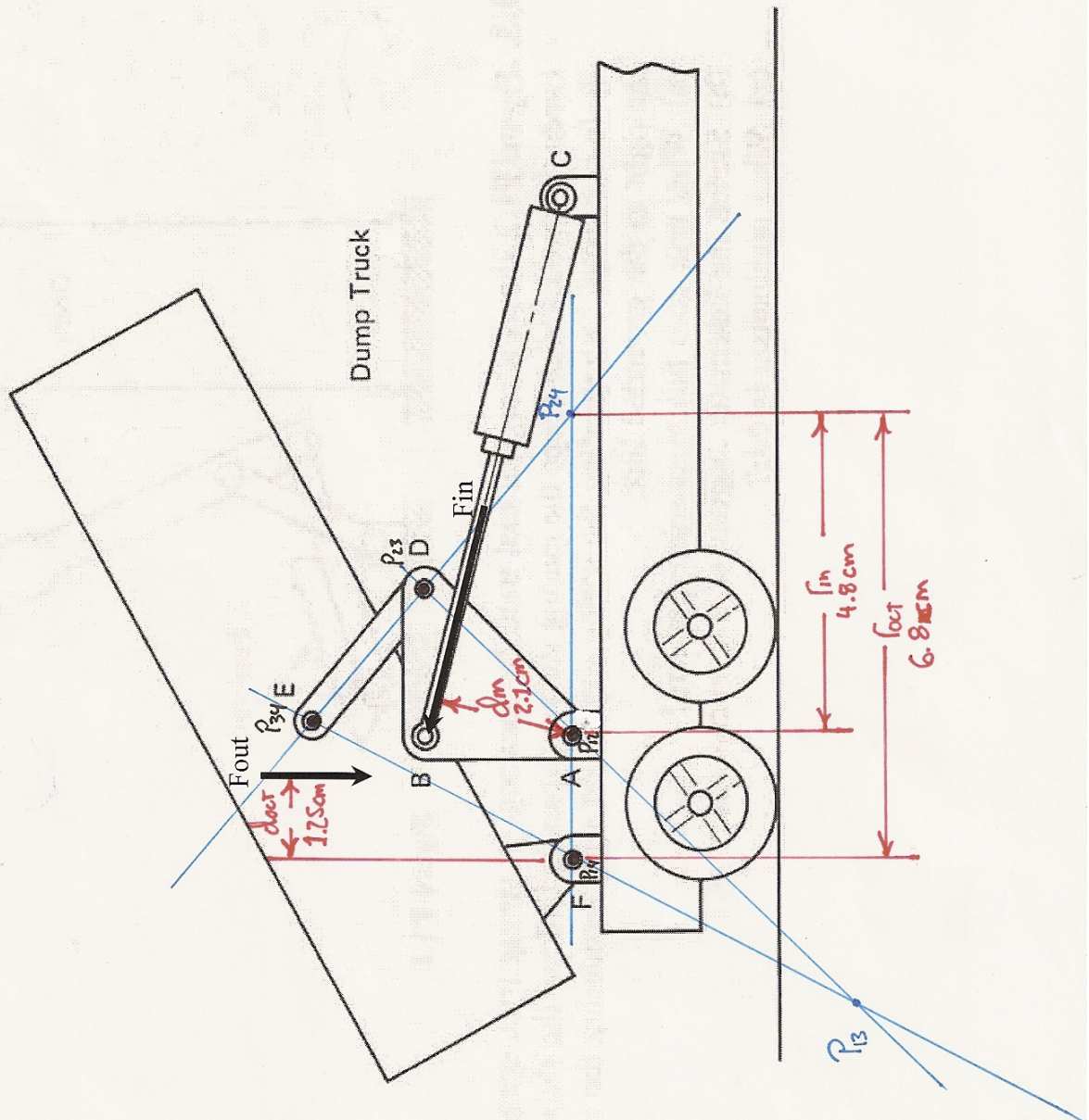
$$\omega_3 = \frac{240 \text{ m/s}}{7.3 \text{ m}} = 33 \text{ 1/s}$$



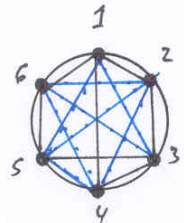
PROBLEM 4: Determine the mechanical advantage of the truck linkage shown.



$$MA = \frac{d_{in}}{d_{out}} \cdot \frac{r_{out}}{r_{in}} = \frac{2.1 \text{ cm}}{1.25 \text{ cm}} \cdot \frac{6.8 \text{ cm}}{4.8 \text{ cm}} = \boxed{2.4}$$



PROBLEM 5: Given: the length of link 2 in 1 inch and it is rotating ccw at 10 1/s
Find: $\omega_3, \omega_5, \omega_6, v_c$

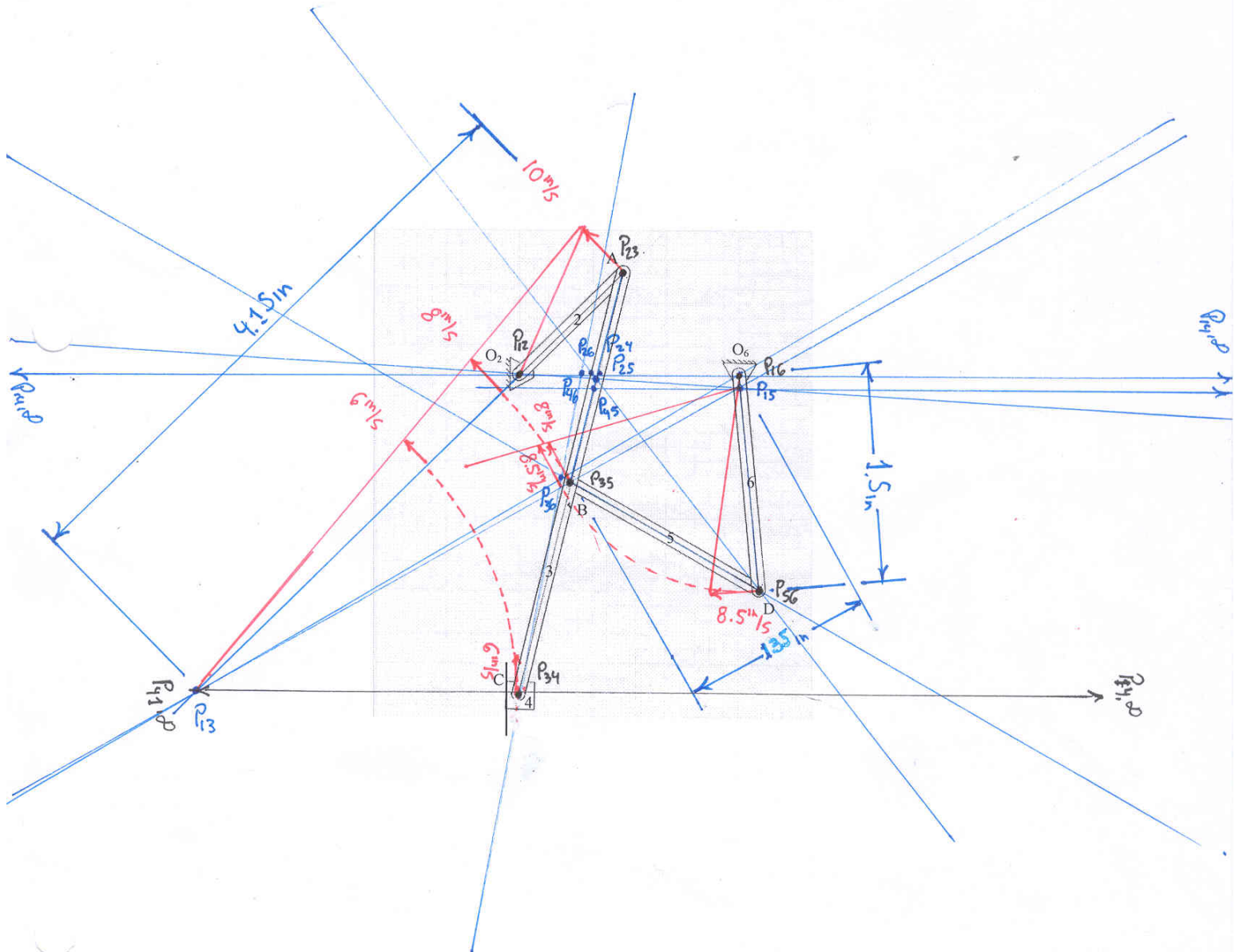


$$\omega_3 = \frac{10 \text{ 1/s}}{4.15 \text{ in}} = \boxed{2.4 \text{ 1/s}}$$

$$\omega_5 = \frac{8 \text{ 1/s}}{1.35 \text{ in}} = \boxed{5.9 \text{ 1/s}}$$

$$\omega_6 = \frac{8.5 \text{ 1/s}}{1.5 \text{ in}} = \boxed{5.7 \text{ 1/s}}$$

$$v_c = \boxed{6 \text{ in/s}}$$



PROBLEM 6: Two segment cam.

Segment 1: Constant velocity of 10 in/s for 0.5s.
Follower position starts at 0 in.

Segment 2: Return the follower to the initial conditions. For 0.5s

SEGMENT 1 $0 \leq \theta \leq \pi$

THE BOUNDARY CONDITIONS ARE

$$\begin{aligned} S(0) &= 0 \\ V(0) &= 10 \text{ in/s} & V(\pi) &= 10 \text{ in/s} \\ A(0) &= 0 \text{ in/s}^2 \end{aligned}$$

THE APPROPRIATE POLYNOMIAL FOR THE
CONSTANT VELOCITY CONSTRAINT

$$\begin{aligned} S(\theta) &= C_0 + C_1 \left(\frac{\theta}{\pi} \right) \\ S(0) &= 0 = C_0 \Rightarrow \underline{S(\theta) = C_1 \left(\frac{\theta}{\pi} \right)} \end{aligned}$$

THE VELOCITY MUST BE CONVERTED FROM
in/s TO in/rad

$$\omega = 1 \frac{\text{REV}}{\text{s}} \cdot \frac{2\pi \text{ RAD}}{\text{REV}} = 6.283 \frac{\text{RAD}}{\text{s}}$$

$$V = 10 \frac{\text{in}}{\text{s}} \cdot \frac{1}{6.283 \frac{\text{RAD}}{\text{s}}} = 1.592 \frac{\text{in}}{\text{RAD}}$$

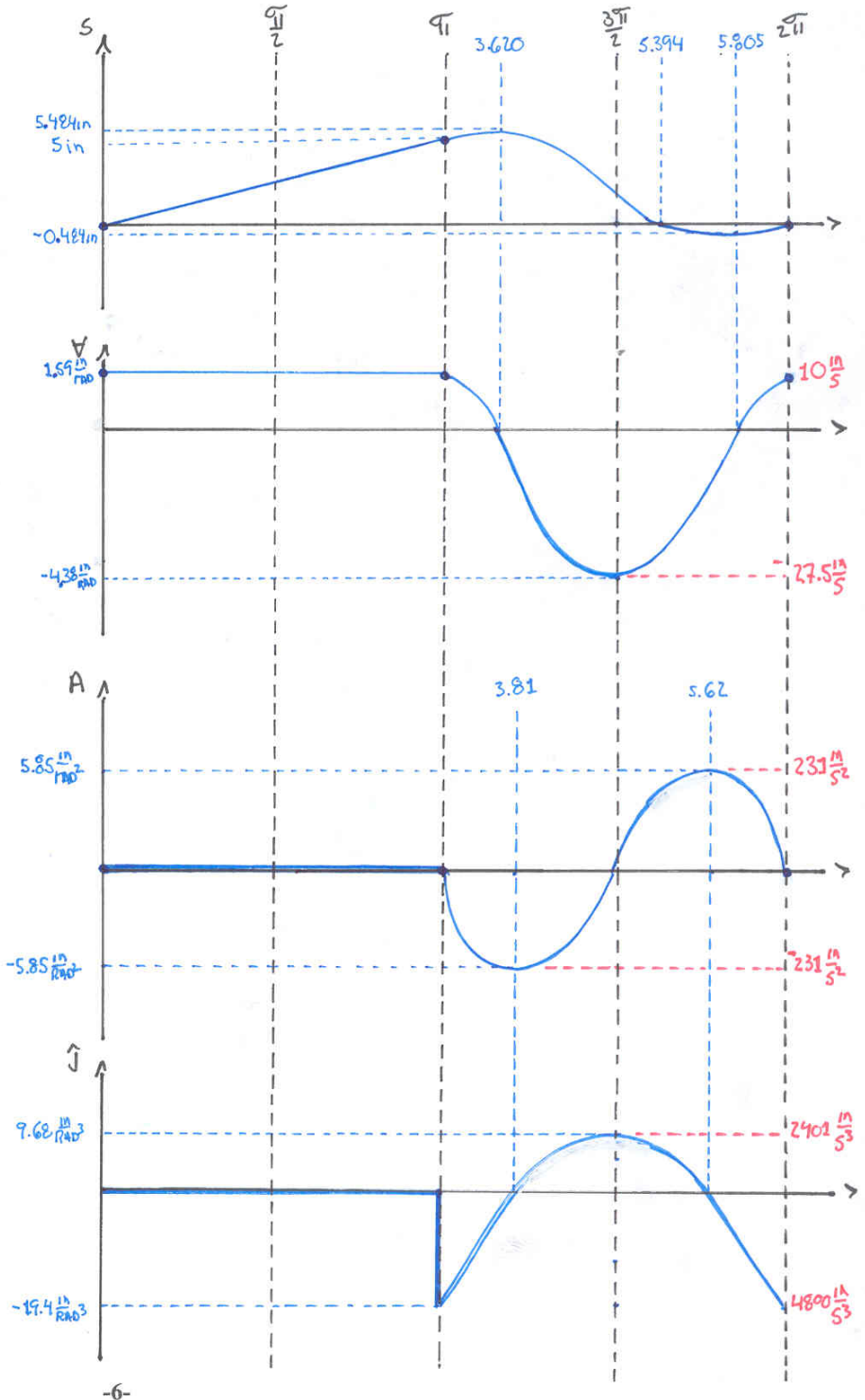
$$\begin{aligned} V(\theta) &= \frac{C_1}{\pi} \\ V(0) &= 1.592 \frac{\text{in}}{\text{RAD}} = \frac{C_1}{\pi} \\ \Rightarrow C_1 &= 5.00 \text{ in} \end{aligned}$$

$$\begin{aligned} S(\theta) &= 5.00 \text{ in} \left(\frac{\theta}{\pi} \right) \\ V(\theta) &= \frac{5.00 \text{ in}}{\pi \text{ RAD}} = 1.592 \frac{\text{in}}{\text{RAD}} \\ A(\theta) &= 0 \\ \delta(\theta) &= 0 \end{aligned}$$

$$S(0) = 0 \text{ in}$$

$$S(\pi) = 5.00 \text{ in}$$

$$V(0) = V(\pi) = 1.592 \frac{\text{in}}{\text{RAD}}$$



SEGMENT 2

$$\pi \leq \theta \leq 2\pi \Rightarrow \theta^* = \theta - \pi \Rightarrow 0 \leq \theta^* \leq \pi, \quad \beta = \pi$$

FOR THE SEGMENT THERE ARE SIX BOUNDARY CONDITIONS THAT MUST BE SATISFIED

$$\begin{aligned} S(0) &= 5\text{in} & V(0) &= 1.591 \text{ in/rad} & A(0) &= 0 \text{ in/rad}^2 \\ S(\pi) &= 0\text{in} & V(\pi) &= 1.591 \text{ in/rad} & A(\pi) &= 0 \text{ in/rad}^2 \end{aligned}$$

THE APPROPRIATE POLYNOMIAL OF SIX BOUNDARY CONDITIONS IS

$$S = C_0 + C_1 \left(\frac{\theta^*}{\pi}\right) + C_2 \left(\frac{\theta^*}{\pi}\right)^2 + C_3 \left(\frac{\theta^*}{\pi}\right)^3 + C_4 \left(\frac{\theta^*}{\pi}\right)^4 + C_5 \left(\frac{\theta^*}{\pi}\right)^5$$

$$S_0 = \underline{S_{in} = C_0} \Rightarrow S(\theta^*) = 5\text{in} + C_1 \left(\frac{\theta^*}{\pi}\right) + C_2 \left(\frac{\theta^*}{\pi}\right)^2 + C_3 \left(\frac{\theta^*}{\pi}\right)^3 + C_4 \left(\frac{\theta^*}{\pi}\right)^4 + C_5 \left(\frac{\theta^*}{\pi}\right)^5$$

$$V(\theta^*) = \frac{C_1}{\pi} + \frac{2 \cdot C_2}{\pi^2} \cdot \theta^* + \frac{3 \cdot C_3}{\pi^3} \cdot \theta^{*2} + \frac{4 \cdot C_4}{\pi^4} \cdot \theta^{*3} + \frac{5 \cdot C_5}{\pi^5} \cdot \theta^{*4}$$

$$\underline{V(0) = 1.591 \text{ in/rad} = \frac{C_1}{\pi}} \Rightarrow C_1 = 5.00 \text{ in}$$

$$S(\theta^*) = 5\text{in} + 5\text{in} \left(\frac{\theta^*}{\pi}\right) + C_2 \left(\frac{\theta^*}{\pi}\right)^2 + C_3 \left(\frac{\theta^*}{\pi}\right)^3 + C_4 \left(\frac{\theta^*}{\pi}\right)^4 + C_5 \left(\frac{\theta^*}{\pi}\right)^5$$

$$V(\theta^*) = \frac{5\text{in}}{\pi} + \frac{2 \cdot C_2}{\pi^2} \cdot \theta^* + \frac{3 \cdot C_3}{\pi^3} \cdot \theta^{*2} + \frac{4 \cdot C_4}{\pi^4} \cdot \theta^{*3} + \frac{5 \cdot C_5}{\pi^5} \cdot \theta^{*4}$$

$$A(\theta^*) = \frac{2 \cdot C_2}{\pi^2} + \frac{6 \cdot C_3}{\pi^3} \cdot \theta^* + \frac{12 \cdot C_4}{\pi^4} \cdot \theta^{*2} + \frac{20 \cdot C_5}{\pi^5} \cdot \theta^{*3}$$

$$\underline{A(0) = 0 \text{ in/rad}^2 = \frac{2 \cdot C_2}{\pi^2}} \Rightarrow C_2 = 0$$

$$S(\theta^*) = 5\text{in} + 5\text{in} \left(\frac{\theta^*}{\pi}\right) + C_3 \left(\frac{\theta^*}{\pi}\right)^3 + C_4 \left(\frac{\theta^*}{\pi}\right)^4 + C_5 \left(\frac{\theta^*}{\pi}\right)^5$$

$$V(\theta^*) = \frac{5\text{in}}{\pi} + \frac{3 \cdot C_3}{\pi^3} \cdot \theta^{*2} + \frac{4 \cdot C_4}{\pi^4} \cdot \theta^{*3} + \frac{5 \cdot C_5}{\pi^5} \cdot \theta^{*4}$$

$$A(\theta^*) = \frac{6 \cdot C_3}{\pi^3} \cdot \theta^* + \frac{12 \cdot C_4}{\pi^4} \cdot \theta^{*2} + \frac{20 \cdot C_5}{\pi^5} \cdot \theta^{*3}$$

THREE MORE BOUNDARY CONDITIONS EXIST AT THE END OF THE SEGMENT THAT CAN NOW BE APPLIED

$$S(\pi) = 0\text{in} = 5\text{in} + 5\text{in} + C_3 + C_4 + C_5 \Rightarrow \underline{-10\text{in} = C_3 + C_4 + C_5}$$

$$V(\pi) = 1.591 \text{ in/rad} = \frac{5\text{in}}{\pi} + \frac{3 \cdot C_3}{\pi^3} \cdot \pi^3 + \frac{4 \cdot C_4}{\pi^4} \cdot \pi^4 + \frac{5 \cdot C_5}{\pi^5} \cdot \pi^5$$

$$\Rightarrow \underline{0 = 3 \cdot C_3 + 4 \cdot C_4 + 5 \cdot C_5}$$

$$A(\pi) = 0 \text{ in/rad}^2 = \frac{6 \cdot C_3}{\pi^3} \cdot \pi^3 + \frac{12 \cdot C_4}{\pi^4} \cdot \pi^4 + \frac{20 \cdot C_5}{\pi^5} \cdot \pi^5 \Rightarrow \underline{0 = 6 \cdot C_3 + 12 \cdot C_4 + 20 \cdot C_5}$$

$$\begin{bmatrix} 1 & 1 & 1 \\ 3 & 4 & 5 \\ 6 & 12 & 20 \end{bmatrix} \begin{Bmatrix} C_3 \\ C_4 \\ C_5 \end{Bmatrix} = \begin{Bmatrix} -10\text{in} \\ 0 \\ 0 \end{Bmatrix} \Rightarrow \begin{Bmatrix} C_3 \\ C_4 \\ C_5 \end{Bmatrix} = \begin{Bmatrix} -100 \\ 150 \\ -60 \end{Bmatrix} \text{ [in]} \quad -7-$$

THE EQUATIONS FOR SEGMENT 2 CAN NOW BE WRITTEN

$$S(\theta^*) = 5\text{in} + 1.592 \frac{\text{in}}{\text{rad}} \cdot \theta^* - 3.225 \frac{\text{in}}{\text{rad}^3} \cdot \theta^{*3} + 1.540 \frac{\text{in}}{\text{rad}^4} \cdot \theta^{*4} - 0.1961 \frac{\text{in}}{\text{rad}^5} \cdot \theta^{*5}$$

$$V(\theta^*) = 1.592 \frac{\text{in}}{\text{rad}} - 9.675 \frac{\text{in}}{\text{rad}^3} \cdot \theta^{*2} + 6.160 \frac{\text{in}}{\text{rad}^4} \cdot \theta^{*3} - 0.9803 \theta^{*4}$$

$$a(\theta^*) = -19.35 \frac{\text{in}}{\text{rad}^3} \cdot \theta^* + 12.48 \frac{\text{in}}{\text{rad}^4} \cdot \theta^{*2} - 3.921 \frac{\text{in}}{\text{rad}^5} \cdot \theta^{*3}$$

$$j(\theta^*) = 36.96 \frac{\text{in}}{\text{rad}^4} \cdot \theta^* - 11.76 \frac{\text{in}}{\text{rad}^5} \cdot \theta^{*2} - 19.35 \frac{\text{in}}{\text{rad}^6}$$

DETERMINING THE ROOTS OF THE ABOVE EQUATIONS SO THAT MAX AND MIN'S CAN BE COMPUTED (ONLY THE REAL ROOTS ARE SHOWN AND ONLY THE ROOTS IN THE INTERVAL)

FOR DISPLACEMENT : 2.252 , 3.1416(π)

FOR VELOCITY : 0.4784 , 2.6632

FOR ACCELERATION : 0.0 , 1.5708, 3.1416(π)

FOR JERK : 0.6639 , 2.4777

FOR THE DERIVATIVE OF THE JERK: 1.5708

NOW VALUES FOR EACH OF THE FUNCTIONS CAN BE FOUND AT CRITICAL POINTS

$$S(0) = 5.000\text{in} \quad S(0.4784) = 5.484\text{in} \quad S(2.6632) = -0.4840\text{in} \quad S(\pi) = 0.000\text{in}$$

$$V(0) = 1.592 \frac{\text{in}}{\text{rad}} \quad V\left(\frac{\pi}{2}\right) = -4.377 \frac{\text{in}}{\text{rad}} \quad V(\pi) = 1.592 \frac{\text{in}}{\text{rad}}$$

$$a(0) = 0 \quad a(0.6639) = -5.850 \frac{\text{in}}{\text{rad}^2} \quad a(2.4777) = 5.850 \frac{\text{in}}{\text{rad}^2} \quad a(\pi) = 0$$

$$j(0) = -19.35 \quad j\left(\frac{\pi}{2}\right) = 9.68 \quad j(\pi) = -19.35$$