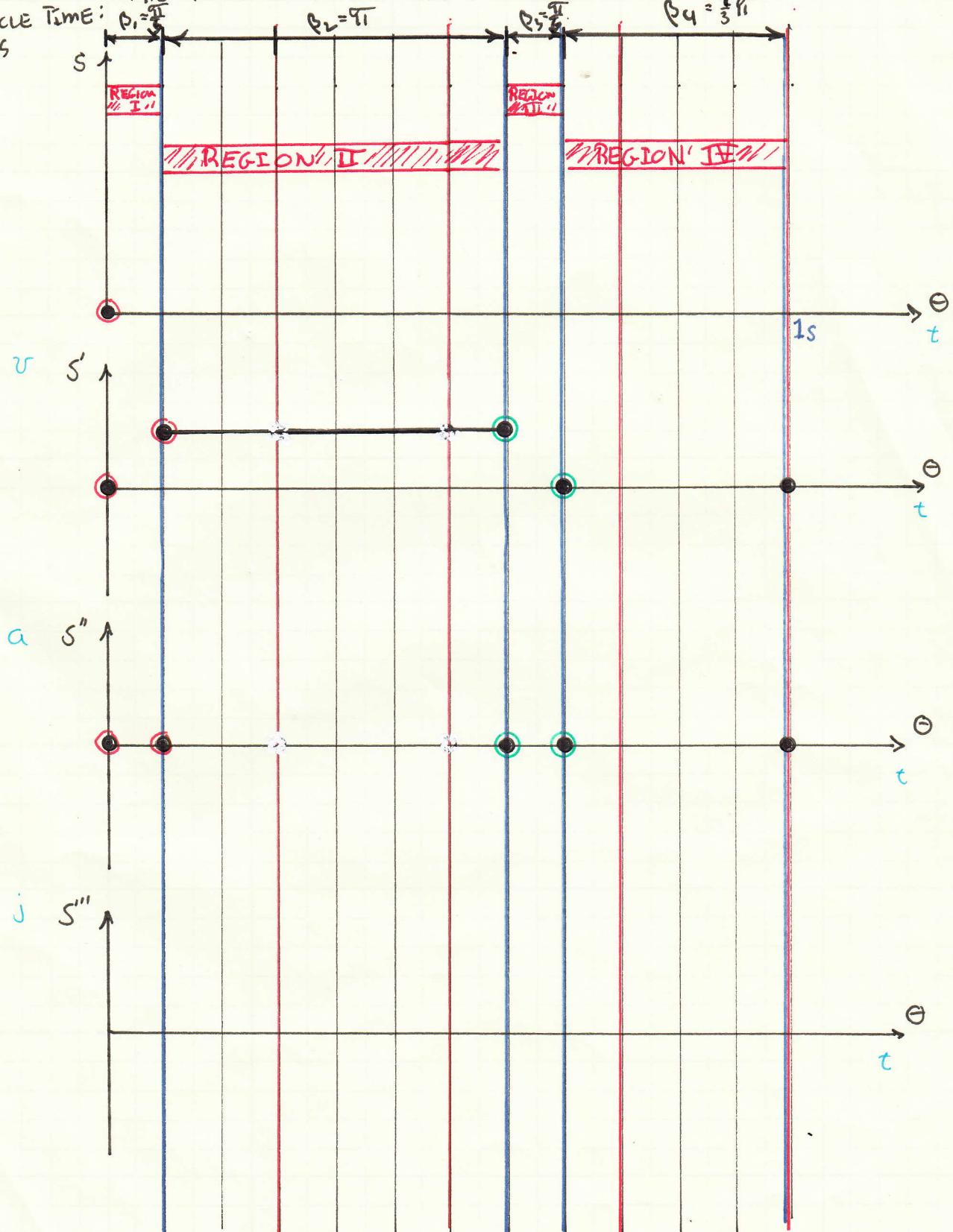


ACCELERATE: THE FOLLOWER TO 10 in/s  
 MAINTAIN: A CONSTANT VELOCITY OF 10 in/s FOR 0.5 s  
 DECELERATE: THE FOLLOWER TO ZERO VELOCITY  
 RETURN: THE FOLLOWER TO THE START POSITION.  
 CYCLE TIME:  $t_1 = \frac{\pi}{2}$   $t_2 = \pi$   $t_3 = \frac{\pi}{2}$   $t_4 = \frac{1}{3}\pi$



$$\omega = \frac{1 \text{ rev.}}{\text{sec}} \cdot \frac{2\pi \text{ rad}}{\text{rev}} = \underline{\underline{\frac{2\pi \text{ rad}}{\text{s}}}} \quad ①$$

$$\theta = \omega \cdot t \quad ②$$

$$s = h \quad ③$$

$$v = \dot{s} = \frac{ds}{dt} = \frac{ds}{d\theta} \cdot \frac{d\theta}{dt} = \frac{ds}{d\theta} \cdot \omega = s' \cdot \omega \Rightarrow \dot{s} = \underline{\underline{\frac{s'}{\omega}}} \quad ④$$

$$a = \ddot{s} = \frac{d^2s}{dt^2} = \frac{d\dot{s}}{dt} = \frac{d\dot{s}}{d\theta} \cdot \frac{d\theta}{dt} = \frac{d\dot{s}}{d\theta} \cdot \omega = \frac{d\dot{s}}{d\theta} \cdot \frac{ds}{d\theta} \cdot \omega \\ = s'' \cdot \omega^2 \Rightarrow \underline{\underline{s'' = \frac{a}{\omega^2}}} \quad ⑤$$

$$j = \ddot{s} = \frac{d^3s}{dt^3} = \frac{da}{dt} = \frac{d^2a}{dt^2} = \frac{d^3s}{dt^3} = \frac{d(s'' \cdot \omega^3)}{dt} = \frac{ds''}{dt} \cdot \omega^2 = \frac{ds''}{d\theta} \cdot \frac{d\theta}{dt} \cdot \omega^2 \\ = s''' \cdot \omega^3 \Rightarrow \underline{\underline{s''' = \frac{j}{\omega^3}}} \quad ⑥$$

IN REGION I:  $0 \leq \theta \leq \beta_1 = \frac{\pi}{3} = 60^\circ, 0 \leq \theta_1 \leq \frac{\pi}{3}$

THE BOUNDARY CONDITIONS FOR THIS REGION ARE

$$\theta_1 = 0: \quad s = 0, \quad v = 0, \quad a = 0 \quad ⑦, ⑧, ⑨$$

$$\theta_1 = \frac{\pi}{6}: \quad v = 10 \frac{m}{s} \cdot \frac{1}{2\pi \frac{\text{rad}}{\text{s}}} = \frac{5}{\pi} \frac{m}{\text{rad}} \quad a = 0 \frac{m}{\text{rad}^2} \quad ⑩, ⑪$$

THE FIVE BOUNDARY CONDITIONS WILL REQUIRE FIVE CONSTANTS

$$s_1 = C_0 + C_1 \left(\frac{\theta_1}{\beta_1}\right) + C_2 \left(\frac{\theta_1}{\beta_1}\right)^2 + C_3 \left(\frac{\theta_1}{\beta_1}\right)^3 + C_4 \left(\frac{\theta_1}{\beta_1}\right)^4 \quad ⑫$$

$$v_1 = \frac{C_1}{\beta_1} + 2 \cdot C_2 \cdot \left(\frac{\theta_1}{\beta_1}\right) + 3 \cdot C_3 \left(\frac{\theta_1}{\beta_1}\right)^2 + 4 \cdot C_4 \left(\frac{\theta_1}{\beta_1}\right)^3 \quad ⑬$$

$$a_1 = \frac{2 \cdot C_2}{\beta_1^2} + 6 \cdot C_3 \left(\frac{\theta_1}{\beta_1}\right) + 12 \cdot C_4 \left(\frac{\theta_1}{\beta_1}\right)^2 \quad ⑭$$

$$j_1 = \frac{6 \cdot C_3}{\beta_1^3} + 24 \cdot C_4 \left(\frac{\theta_1}{\beta_1}\right) \quad ⑮$$

(3)

$$S_1 = C_3 \cdot \left(\frac{\Theta_1}{\beta_1}\right)^3 + C_4 \left(\frac{\Theta_1}{\beta_1}\right)^4 \quad (12)$$

$$v_1 = \frac{3 \cdot C_3}{\beta_1} \cdot \left(\frac{\Theta_1}{\beta_1}\right)^2 + \frac{4 \cdot C_4}{\beta_1} \left(\frac{\Theta_1}{\beta_1}\right)^3 \quad (13)$$

$$a_1 = \frac{6 \cdot C_3}{\beta_1^2} \cdot \left(\frac{\Theta_1}{\beta_1}\right) + 12 \frac{C_4}{\beta_1^2} \left(\frac{\Theta_1}{\beta_1}\right)^2 \quad (14)$$

$$j = \frac{6 \cdot C_3}{\beta_1^3} + 24 \frac{C_4}{\beta_1^3} \left(\frac{\Theta_1}{\beta_1}\right) \quad (15)$$

SUBSTITUTING IN THE REMAINING ACCELERATION BOUNDARY CONDITION

$$a\left(\frac{\pi}{3}\right) = 0 \Rightarrow \frac{6 \cdot C_3}{\beta_1^2} + 12 \frac{C_4}{\beta_1^2}$$

$$\Rightarrow C_3 = -\frac{12}{6} C_4 = -2 \cdot C_4 \quad (16)$$

SUBSTITUTING THE REMAINING VELOCITY BOUNDARY CONDITION

$$v\left(\frac{\pi}{3}\right) = \frac{5}{\pi/3} m = -\frac{3 \cdot 2 \cdot C_4}{\pi/3} + \frac{4 \cdot C_4}{\pi/3} = -\frac{2 \cdot C_4}{\pi/3}$$

$$\Rightarrow C_4 = -\frac{5}{6} m \quad (17)$$

$$\Rightarrow \underline{\underline{C_3 = \frac{10}{6} m = \frac{5}{3} m}} \quad (18)$$

REWRITING THE FUNCTIONS

$$S_1 = \frac{5}{3} m \left(\frac{\Theta_1}{\beta_1}\right)^3 - \frac{5}{6} m \left(\frac{\Theta_1}{\beta_1}\right)^4 \quad (19)$$

$$v_1 = \frac{3 \cdot \frac{5}{3} m}{\pi/3} \left(\frac{\Theta_1}{\beta_1}\right)^2 - \frac{4 \cdot \frac{5}{6} m}{\pi/3} \left(\frac{\Theta_1}{\beta_1}\right)^3 = \frac{15}{\pi/3} m \left(\frac{\Theta_1}{\beta_1}\right)^2 - \frac{10}{\pi/3} m \left(\frac{\Theta_1}{\beta_1}\right)^3 \quad (20)$$

$$a_1 = \frac{6 \cdot \frac{5}{3} m}{\pi/3^2} \cdot \left(\frac{\Theta_1}{\beta_1}\right) - \frac{12 \cdot \frac{5}{6} m}{\pi/3^2} \left(\frac{\Theta_1}{\beta_1}\right)^2 = \frac{90}{\pi/3^2} m \left(\frac{\Theta_1}{\beta_1}\right) - \frac{90}{\pi/3^2} m \left(\frac{\Theta_1}{\beta_1}\right)^2 \quad (21)$$

$$j_1 = \frac{6 \cdot \frac{5}{3} m}{\pi/3^3/27} - \frac{24 \cdot \frac{5}{6} m}{\pi/3^3/27} \left(\frac{\Theta_1}{\beta_1}\right) = \frac{270}{\pi/3^3} m - \frac{540}{\pi/3^3} m \left(\frac{\Theta_1}{\beta_1}\right) \quad (22)$$

CHECKING THE VALUES OF ⑯ - ⑰ AT  $\theta_1 = 0$

$$S_1(0) = 0 \quad a_1(c) = c$$

$$V_1(0) = 0 \quad j_1(c) = \frac{27c}{\pi^3} \text{ in}$$

CHECKING THE VALUES AT  $\theta_1 = \frac{\pi}{3}$

$$S(\frac{\pi}{3}) = \frac{5}{3} \text{ in} - \frac{5}{6} \text{ in} = \frac{5}{6} \text{ in}$$

$$V(\frac{\pi}{3}) = \frac{15}{\pi^3} \text{ in} - \frac{10}{\pi^3} \text{ in} = \frac{5}{\pi^3} \text{ in} \quad (\text{THIS IS THE BC})$$

$$a(\frac{\pi}{3}) = 0$$

$$j(\frac{\pi}{3}) = \frac{27c}{\pi^3} \text{ in}$$

⑯, ⑰ AND ⑲ ESTABLISH BC FOR THE NEXT REGION

IN THE NEXT REGION IT IS DESIRED TO MAINTAIN A CONSTANT VELOCITY OF  $\frac{s}{\pi} \text{ in}$ . IF THE VELOCITY IS CONSTANT THEN THE DISPLACEMENT IS LINEAR. THUS THE POLYNOMIAL FUNCTIONS THAT MAKE UP REGION 2 ARE

REGION 2:  $\frac{\pi}{3} \leq \theta \leq \frac{4\pi}{3}$ ,  $0 \leq \theta_2 \leq \pi$ ,  $\beta_2 = \pi$

$$S_2 = C_0 + C_1 \left( \frac{\theta^2}{\beta_2} \right)$$

$$V_2 = \frac{C_1}{\beta_2}$$

$$a = 0$$

$$j = 0$$

THE BOUNDARY CONDITIONS FOR THIS REGION ARE

$$S_2(0) = \frac{s}{6} \text{ in}$$

$$V_2(0) = \frac{s}{\pi} \text{ in}$$

$a_2(c) = 0$  IS IDENTICALLY SATISFIED BY ⑳

SUBSTITUTING ⑳ INTO ⑲

$$V(c) = \frac{s}{\pi} \text{ in} = \frac{C_1}{\pi} \Rightarrow \underline{\underline{C_1 = 5 \text{ in}}}$$

SUBSTITUTING ⑳ AND ⑳ INTO ⑯

$$\underline{\underline{S(c) = \frac{s}{6} \text{ in} = C_0}}$$

(26) - (25) CAN NOW BE REWRITTEN

$$S_2 = \frac{5}{6}m + \sin\left(\frac{\theta_2}{\pi}\right)$$

$$U_2 = \frac{5m}{\pi}$$

$$A_2 = C$$

$$J_2 = 0$$

(26)

(27)

NOW CONSIDER THESE THE VALUES OF THESE FUNCTIONS AT  $\theta_2 = 0$

$$S_2(0) = \frac{5}{6}m + \sin(0) = \frac{5}{6}m$$

$$U_2(0) = \frac{5m}{\pi}$$

$$A_2(0) = C$$

$$J_2(0) = 0$$

NOW CONSIDER THE VALUES OF THESE FUNCTIONS AT  $\theta_2 = \pi$

$$S_2(\pi) = \frac{5}{6}m + \sin = \frac{35}{6}m$$

$$U_2(\pi) = \frac{5m}{\pi}$$

$$A_2 = 0$$

$$J_2 = 0$$

(28)

(29)

(28) AND (29) ARE THE BOUNDARY CONDITIONS FOR THE NEXT REGION.

REGION 3:  $4\pi/3 \leq \theta \leq 5\pi/3, 0 \leq \theta_3 \leq \pi/3, S_3 = \pi/3$

THE BOUNDARY CONDITIONS FOR THIS REGION ARE

$$S_3(0) = \frac{35}{6}m \quad (30)$$

$$U_3(0) = \frac{5m}{\pi} \quad (31)$$

$$U_4(\pi/3) = 0 \quad (32)$$

$$A_3(0) = 0 \quad (33)$$

THESE FOUR BOUNDARY CONDITIONS IMPLY A THIRD ORDER POLYNOMIAL THAT WILL HAVE FOUR CONSTANTS

$$S_3 = C_0 + C_1 \cdot \left(\frac{\Theta_3}{\beta_3}\right) + C_2 \cdot \cancel{\left(\frac{\Theta_3}{\beta_3}\right)^2} + C_3 \cdot \left(\frac{\Theta_3}{\beta_3}\right)^3 \quad (34)$$

$$U_3 = \frac{C_1}{\beta_3} + 2 \cdot \cancel{\frac{C_2}{\beta_3}} \left(\frac{\Theta_3}{\beta_3}\right) + \cancel{3 \cdot C_3} \left(\frac{\Theta_3}{\beta_3}\right)^2 \quad (35)$$

$$a_3 = \cancel{\frac{2 \cdot C_2}{\beta_3^2}} + \frac{6 \cdot C_3}{\beta_3^2} \left(\frac{\Theta_3}{\beta_3}\right) \quad (36)$$

$$j = \frac{6 \cdot C_3}{\beta_3^3} \quad (37)$$

THE CONSTANTS CAN BE DETERMINED BY CONSIDERING THE BOUNDARY CONDITIONS (30) - (33).

$$(30) \rightarrow S(0) = \frac{35}{6}in = C_0 \quad (38)$$

$$(31) \rightarrow U(0) = \frac{5in}{\pi} = \frac{C_1}{\pi/3} \Rightarrow C_1 = \frac{5}{3}in \quad (39)$$

$$(32) \rightarrow a(0) = 0 = \frac{2 \cdot C_2}{\beta_3^2} \Rightarrow C_2 = 0 \quad (40)$$

$$(33) \rightarrow (38) + (39) + (40) \rightarrow U(\pi/3) = 0 = \frac{5in}{\pi/3} + 3 \frac{C_3}{\pi/3} \\ \Rightarrow C_3 = -\frac{5}{9}in \quad (41)$$

Now (34) - (37) CAN BE REWRITTEN

$$S_3 = \frac{35}{6}in + \frac{5}{3}in \left(\frac{\Theta_3}{\pi/3}\right) - \frac{5}{9}in \left(\frac{\Theta_3}{\pi/3}\right)^3 \quad (42)$$

$$U_3 = \frac{5in}{\pi/3} + \frac{3 \cdot (-\frac{5}{9}in)}{\pi/3} \cdot \left(\frac{\Theta_3}{\pi/3}\right)^2 = \frac{5}{\pi}in - \frac{5}{\pi}in \left(\frac{\Theta_3}{\pi/3}\right)^2 \quad (43)$$

$$a_3 = \frac{6 \cdot (-\frac{5}{9}in)}{\pi^2/9} \left(\frac{\Theta_3}{\pi/3}\right) = -\frac{30}{\pi^2}in \left(\frac{\Theta_3}{\pi/3}\right) \quad (44)$$

$$j_3 = \frac{6 \cdot (-\frac{5}{9}in)}{\pi^3/27} = \frac{90}{\pi^3}in \quad (45)$$

INITIAL THE VALUES OF THESE FUNCTIONS NOW NEED TO BE CALCULATED

$$S_3(0) = \frac{35}{6}in \quad (\text{CHECKS WITH PREVIOUS SEGMENT'S END CONDITION})$$

$$U_3(0) = \frac{5}{\pi}in \quad (\text{CHECKS WITH PREVIOUS SEGMENT'S END CONDITION})$$

$$a_3(0) = 0 \quad (\text{CHECKS WITH PREVIOUS REGIONS EIN CONDITION})$$

$$j_3(c) = \frac{9c}{\pi^3} \text{ in}$$

THE END VALUES OF THESE FUNCTIONS FOR THIS REGION NEED TO BE CALCULATED. THE RESULTS ARE USED AS INITIAL CONDITIONS FOR THE FINAL REGION.

$$S_3\left(\frac{\pi}{3}\right) = \frac{35}{6} \text{ in} + \frac{5}{3} \text{ in} - \frac{5}{9} \text{ in} = \frac{105}{18} \text{ in} + \frac{30}{18} \text{ in} - \frac{10}{18} \text{ in} = \frac{125}{18} \text{ in} \quad (46)$$

$$U_3\left(\frac{\pi}{3}\right) = 0 \quad (47)$$

$$a_3\left(\frac{\pi}{3}\right) = -\frac{30}{\pi^2} \text{ in/rad}^2 \quad (48)$$

$$j_3\left(\frac{\pi}{3}\right) = \frac{9c}{\pi^3} \text{ in/rad}^3 \quad (49)$$

REGION 4:  $\frac{\pi}{3} \leq \theta \leq \pi$ ,  $0 \leq \theta \leq \frac{\pi}{3}$ ,  $\beta_4 = \frac{\pi}{3}$

THE FOLLOWING BOUNDARY CONDITIONS FOR REGION 4 RESULT FROM THE NEED FOR CONTINUITY WITH REGIONS 3 AND 1

$$S_4(0) = \frac{125}{18} \text{ in} \quad (50) \quad S_4\left(\frac{\pi}{3}\right) = 0 \quad (53)$$

$$U_4(0) = 0 \quad (51) \quad U_4\left(\frac{\pi}{3}\right) = 0 \quad (54)$$

$$a_4(0) = -\frac{30}{\pi^2} \text{ in/rad}^2 \quad (52) \quad a_4\left(\frac{\pi}{3}\right) = 0 \quad (55)$$

THESE SIX BOUNDARY CONDITIONS IMPLY A POLYNOMIAL OF DEGREE 5

$$S_4 = C_0 + C_1 \left(\frac{\theta_4}{\beta_4}\right)^0 + C_2 \left(\frac{\theta_4}{\beta_4}\right)^1 + C_3 \left(\frac{\theta_4}{\beta_4}\right)^2 + C_4 \left(\frac{\theta_4}{\beta_4}\right)^3 + C_5 \left(\frac{\theta_4}{\beta_4}\right)^4 + C_6 \left(\frac{\theta_4}{\beta_4}\right)^5 \quad (56)$$

$$U_4 = \frac{C_1}{\beta_4} + 2 \cdot \frac{C_2}{\beta_4} \cdot \left(\frac{\theta_4}{\beta_4}\right) + 3 \cdot \frac{C_3}{\beta_4} \cdot \left(\frac{\theta_4}{\beta_4}\right)^2 + 4 \cdot \frac{C_4}{\beta_4} \cdot \left(\frac{\theta_4}{\beta_4}\right)^3 + 5 \cdot \frac{C_5}{\beta_4} \cdot \left(\frac{\theta_4}{\beta_4}\right)^4 \quad (57)$$

$$a_4 = 2 \cdot \frac{C_2}{\beta_4^2} + 6 \cdot \frac{C_3}{\beta_4^3} \cdot \left(\frac{\theta_4}{\beta_4}\right) + 12 \cdot \frac{C_4}{\beta_4^4} \cdot \left(\frac{\theta_4}{\beta_4}\right)^2 + 20 \cdot \frac{C_5}{\beta_4^5} \cdot \left(\frac{\theta_4}{\beta_4}\right)^3 \quad (58)$$

$$j_4 = 6 \cdot \frac{C_3}{\beta_4^3} + 24 \cdot \frac{C_4}{\beta_4^4} \cdot \left(\frac{\theta_4}{\beta_4}\right) + 60 \cdot \frac{C_5}{\beta_4^5} \cdot \left(\frac{\theta_4}{\beta_4}\right)^2 \quad (59)$$

APPLYING THE BOUNDARY CONDITIONS IN ORDER TO SOLVE FOR THE CONSTANTS

$$(50) \rightarrow (56) \Rightarrow S_4(0) = \frac{125}{18} \text{ in} = C_0 \quad (60)$$

$$(51) \rightarrow (57) \Rightarrow U_4(0) = 0 = \frac{C_1}{\beta_4} \Rightarrow \underline{\underline{C_1 = 0}} \quad (61)$$

$$\begin{aligned} \textcircled{52} \Rightarrow \textcircled{52} &\Rightarrow a_4(0) = a_3\left(\frac{\pi}{3}\right) \Rightarrow -\frac{30}{\pi^2} m = \frac{2 \cdot C_2}{\beta_4^2} \\ &\Rightarrow C_2 = -\frac{30m}{\pi^2} \cdot \frac{\beta_4^2}{2} = -\frac{30m}{\pi^2} \cdot \frac{\left(\frac{\pi}{3}\right)^2}{2} = -\frac{15m}{9} = C_2 \quad \textcircled{62} \end{aligned}$$

THE FUNCTIONS  $\textcircled{56}$  -  $\textcircled{59}$  NEED TO BE REWRITTEN WITH  $\textcircled{60}$  -  $\textcircled{62}$  SUBSTITUTED IN FOR  $C_0, C_1$  &  $C_2$  BEFORE THE REMAINING BOUNDARY CONDITIONS CAN BE SOLVED FOR

$$S_4 = \frac{125}{18} m - \frac{15}{9} m \left(\frac{\theta_4}{\beta_4}\right)^2 + C_3 \cdot \left(\frac{\theta_4}{\beta_4}\right)^3 + C_4 \cdot \left(\frac{\theta_4}{\beta_4}\right)^4 + C_5 \cdot \left(\frac{\theta_4}{\beta_4}\right)^5 \quad \textcircled{63}$$

$$U_4 = -\frac{30m}{9\beta_4} \left(\frac{\theta_4}{\beta_4}\right) + 3 \cdot \frac{C_3}{\beta_4} \cdot \left(\frac{\theta_4}{\beta_4}\right)^2 + 4 \cdot \frac{C_4}{\beta_4} \cdot \left(\frac{\theta_4}{\beta_4}\right)^3 + 5 \cdot \frac{C_5}{\beta_4} \cdot \left(\frac{\theta_4}{\beta_4}\right)^4 \quad \textcircled{64}$$

$$a_4 = -\frac{30m}{9 \cdot \beta_4^2} + 6 \cdot \frac{C_3}{\beta_4^2} \cdot \left(\frac{\theta_4}{\beta_4}\right) + 12 \cdot \frac{C_4}{\beta_4^2} \cdot \left(\frac{\theta_4}{\beta_4}\right)^2 + 20 \cdot \frac{C_5}{\beta_4^2} \cdot \left(\frac{\theta_4}{\beta_4}\right)^3 \quad \textcircled{65}$$

$$j_4 = 6 \cdot \frac{C_3}{\beta_4^3} + 24 \cdot \frac{C_4}{\beta_4^3} \cdot \left(\frac{\theta_4}{\beta_4}\right) + 60 \cdot \frac{C_5}{\beta_4^3} \cdot \left(\frac{\theta_4}{\beta_4}\right)^2 \quad \textcircled{66}$$

NOW THE BOUNDARY CONDITIONS IN  $\textcircled{53}$  -  $\textcircled{55}$  CAN BE USED TO DETERMINE  $C_3, C_4$ , &  $C_5$ .  $\theta_4/\beta_4 = 1$

$$\begin{aligned} \textcircled{53} \Rightarrow \textcircled{63} &\Rightarrow S_4\left(\frac{\pi}{3}\right) = 0 = \frac{125}{18} m - \frac{15m}{9} + C_3 + C_4 + C_5 \\ &\underline{- \frac{95}{18} m = C_3 + C_4 + C_5} \quad \textcircled{67} \end{aligned}$$

$$\begin{aligned} \textcircled{54} \Rightarrow \textcircled{64} &\Rightarrow U_4\left(\frac{\pi}{3}\right) = 0 = -\frac{30m}{9\beta_4} + 3 \cdot \frac{C_3}{\beta_4} + 4 \cdot \frac{C_4}{\beta_4} + 5 \cdot \frac{C_5}{\beta_4} \\ &\underline{\frac{30m}{9} = 3 \cdot C_3 + 4 \cdot C_4 + 5 \cdot C_5} \quad \textcircled{68} \end{aligned}$$

$$\begin{aligned} \textcircled{55} \Rightarrow \textcircled{65} &\Rightarrow a_4\left(\frac{\pi}{3}\right) = 0 = -\frac{30m}{9\beta_4^2} + 6 \cdot \frac{C_3}{\beta_4^2} + 12 \cdot \frac{C_4}{\beta_4^2} + 20 \cdot \frac{C_5}{\beta_4^2} \\ &\underline{\frac{30m}{9} = 6 \cdot C_3 + 12 \cdot C_4 + 20 \cdot C_5} \quad \textcircled{69} \end{aligned}$$

Now  $\textcircled{67}$  -  $\textcircled{69}$  CAN BE SOLVED SIMULTANEOUSLY USING EXCEL TO FIND VALUES FOR THE CONSTANTS  $C_3, C_4$ , &  $C_5$ .

$$\left[ \begin{array}{ccc} 1 & 1 & 1 \\ 3 & 4 & 5 \\ 6 & 12 & 20 \end{array} \right] \left\{ \begin{array}{c} C_3 \\ C_4 \\ C_5 \end{array} \right\} = \left\{ \begin{array}{c} -5.27778 \\ 3.333333 \\ 3.333333 \end{array} \right\}$$

$$\left[ \begin{array}{ccc} 10 & -4 & 0.5 \\ -15 & 7 & -1 \\ 6 & -3 & 0.5 \end{array} \right] \left\{ \begin{array}{c} -5.27778 \\ 3.333333 \\ 3.333333 \end{array} \right\} = \left\{ \begin{array}{c} C_3 \\ C_4 \\ C_5 \end{array} \right\}$$

$$= \left\{ \begin{array}{c} -64.4444 \\ 99.16667 \\ -40 \end{array} \right\}$$

(63) - (66) CAN NOW BE REWRITTEN

$$S_4 = \frac{125}{18}m - \frac{15}{9}m\left(\frac{\theta_4}{\beta_4}\right)^2 - 64.44m\left(\frac{\theta_4}{\beta_4}\right)^3 + 99.267m\left(\frac{\theta_4}{\beta_4}\right)^4 - 40m\left(\frac{\theta_4}{\beta_4}\right)^5 \quad (70)$$

$$\gamma_4 = -\frac{30m}{9\cdot\beta_4}\cdot\left(\frac{\theta_4}{\beta_4}\right) - \frac{193.33m}{\beta_4}\left(\frac{\theta_4}{\beta_4}\right)^2 + \frac{396.67m}{\beta_4}\left(\frac{\theta_4}{\beta_4}\right)^3 + \frac{200m}{\beta_4}\left(\frac{\theta_4}{\beta_4}\right)^4 \quad (71)$$

$$a_4 = -\frac{30m}{9\cdot\beta_4^2} - \frac{386.7m}{\beta_4^2}\cdot\left(\frac{\theta_4}{\beta_4}\right) + \frac{1190m}{\beta_4^2}\left(\frac{\theta_4}{\beta_4}\right)^2 - \frac{800m}{\beta_4^2}\left(\frac{\theta_4}{\beta_4}\right)^3 \quad (72)$$

$$j_4 = -\frac{386.7m}{\beta_4^3} + \frac{2380m}{\beta_4^3}\left(\frac{\theta_4}{\beta_4}\right) - \frac{2400m}{\beta_4^3}\left(\frac{\theta_4}{\beta_4}\right)^2 \quad (73)$$

ON THE FOLLOWING PAGES THE FOUR REGIONS ARE PROGRAMMED INTO EXCEL AND THE CHM PROFILE PLOTTED.

θ Deg		β <sub>n</sub> Deg		c <sub>0</sub> in		c <sub>1</sub> in		c <sub>2</sub> in		c <sub>3</sub> in		c <sub>4</sub> in		c <sub>5</sub> in		θ <sub>n</sub> Deg		θ <sub>n</sub> /β <sub>n</sub> Rad		s in		v in/rad		a in/rad <sup>2</sup>		J in/rad <sup>3</sup>	
0	=RADIAN(A6)	=DEGREES(E6)	=PI() / 3	0	0	0	0	1.666666666666667	-0.833333333333333	0	0	1.666666666666667	-0.833333333333333	0	0	=RADIAN(N6)	=O6/E6	=G6+H6*P6+I6*P6*2+ =(H6/E6)*(2*I6/E6)*P =(2*I6/E6*2)+(G*J6/E1=(6*I6/E6^3)+(24^K6)	=G7+H7*P7+I7*P7*2+ =(H7/E7)*(2*I7/E7)*P =(2*I7/E7*2)+(G*J7/E =(6*I7/E7^3)+(24^K7)	=G8+H8*P8+I8*P8*2+ =(H8/E8)*(2*I8/E8)*P =(2*I8/E8*2)+(G*J8/E8^3)+(24^K8/	=G9+H9*P9+I9*P9*2+ =(H9/E9)*(2*I9/E9)*P =(2*I9/E9*2)+(G*J9/E1=(6*I9/E9^3)+(24^K9)	=G10+H10*P10+I10*P10*2+ =(H10/E10)*(2*I10/E10)+(2*I10/E10^2)+(6*I10/E10^3)+(24^K10)					
1	=RADIAN(A7)	=DEGREES(E7)	=PI() / 3	0	0	0	0	1.666666666666667	-0.833333333333333	0	1	=RADIAN(N7)	=O7/E7														
2	=RADIAN(A8)	=DEGREES(E8)	=PI() / 3	0	0	0	0	1.666666666666667	-0.833333333333333	0	2	=RADIAN(N8)	=O8/E8														
3	=RADIAN(A9)	=DEGREES(E9)	=PI() / 3	0	0	0	0	1.666666666666667	-0.833333333333333	0	3	=RADIAN(N9)	=O9/E9														
4	=RADIAN(A10)	=DEGREES(E10)	=PI() / 3	0	0	0	0	1.666666666666667	-0.833333333333333	0	4	=RADIAN(N10)	=O10/E10														

$\theta$	$\beta_n$	$C_0$	$C_1$	$C_2$	$C_3$	$C_4$	$C_5$	$\theta_n$	$\theta_n/\beta_n$	s	v	a	J					
Deg	Rad	Deg	Rad	in	in	in	in	Deg	Rad	in	in/rad	in/rad <sup>2</sup>	in/rad <sup>3</sup>					
0	0	60	1.047198	0	0	0	1.666667	-0.83333	0	0	0	0	8.707914					
1	0.017453	60	1.047198	0	0	0	1.666667	-0.83333	0	1	0.017453	0.016667	7.65E-06					
2	0.034907	60	1.047198	0	0	0	1.666667	-0.83333	0	2	0.034907	0.033333	6.07E-05					
3	0.05236	60	1.047198	0	0	0	1.666667	-0.83333	0	3	0.05236	0.05	0.000203					
4	0.069813	60	1.047198	0	0	0	1.666667	-0.83333	0	4	0.069813	0.066667	0.000477					
5	0.087266	60	1.047198	0	0	0	1.666667	-0.83333	0	5	0.087266	0.083333	0.000924					
6	0.10472	60	1.047198	0	0	0	1.666667	-0.83333	0	6	0.10472	0.1	0.001583					
7	0.122173	60	1.047198	0	0	0	1.666667	-0.83333	0	7	0.122173	0.116667	0.002492					
8	0.139626	60	1.047198	0	0	0	1.666667	-0.83333	0	8	0.139626	0.133333	0.003687					
9	0.15708	60	1.047198	0	0	0	1.666667	-0.83333	0	9	0.15708	0.15	0.005203					
10	0.174533	60	1.047198	0	0	0	1.666667	-0.83333	0	10	0.174533	0.166667	0.007073					
11	0.191986	60	1.047198	0	0	0	1.666667	-0.83333	0	11	0.191986	0.183333	0.009329					
12	0.20944	60	1.047198	0	0	0	1.666667	-0.83333	0	12	0.20944	0.2	0.012					
13	0.226893	60	1.047198	0	0	0	1.666667	-0.83333	0	13	0.226893	0.216667	0.015116					
14	0.244346	60	1.047198	0	0	0	1.666667	-0.83333	0	14	0.244346	0.233333	0.018703					
15	0.261799	60	1.047198	0	0	0	1.666667	-0.83333	0	15	0.261799	0.25	0.022786					
16	0.279253	60	1.047198	0	0	0	1.666667	-0.83333	0	16	0.279253	0.266667	0.027391					
17	0.296706	60	1.047198	0	0	0	1.666667	-0.83333	0	17	0.296706	0.283333	0.032599					
18	0.314159	60	1.047198	0	0	0	1.666667	-0.83333	0	18	0.314159	0.3	0.03825					
19	0.331613	60	1.047198	0	0	0	1.666667	-0.83333	0	19	0.331613	0.316667	0.044545					
20	0.349066	60	1.047198	0	0	0	1.666667	-0.83333	0	20	0.349066	0.333333	0.05144					
21	0.366519	60	1.047198	0	0	0	1.666667	-0.83333	0	21	0.366519	0.35	0.058953					
22	0.383972	60	1.047198	0	0	0	1.666667	-0.83333	0	22	0.383972	0.366667	0.067098					
23	0.401426	60	1.047198	0	0	0	1.666667	-0.83333	0	23	0.401426	0.383333	0.075887					
24	0.418879	60	1.047198	0	0	0	1.666667	-0.83333	0	24	0.418879	0.4	0.085333					
25	0.436332	60	1.047198	0	0	0	1.666667	-0.83333	0	25	0.436332	0.416667	0.095446					
26	0.453786	60	1.047198	0	0	0	1.666667	-0.83333	0	26	0.453786	0.433333	0.106234					
27	0.471239	60	1.047198	0	0	0	1.666667	-0.83333	0	27	0.471239	0.45	0.117703					
28	0.488692	60	1.047198	0	0	0	1.666667	-0.83333	0	28	0.488692	0.466667	0.12986					
29	0.506145	60	1.047198	0	0	0	1.666667	-0.83333	0	29	0.506145	0.483333	0.142708					
30	0.523599	60	1.047198	0	0	0	1.666667	-0.83333	0	30	0.523599	0.5	0.15625					
31	0.541052	60	1.047198	0	0	0	1.666667	-0.83333	0	31	0.541052	0.516667	0.170486					
32	0.558505	60	1.047198	0	0	0	1.666667	-0.83333	0	32	0.558505	0.533333	0.185416					
33	0.575959	60	1.047198	0	0	0	1.666667	-0.83333	0	33	0.575959	0.55	0.201036					
34	0.593412	60	1.047198	0	0	0	1.666667	-0.83333	0	34	0.593412	0.566667	0.217345					
35	0.610865	60	1.047198	0	0	0	1.666667	-0.83333	0	35	0.610865	0.583333	0.234335					
36	0.628319	60	1.047198	0	0	0	1.666667	-0.83333	0	36	0.628319	0.6	0.252					
37	0.645772	60	1.047198	0	0	0	1.666667	-0.83333	0	37	0.645772	0.616667	0.270332					
38	0.663225	60	1.047198	0	0	0	1.666667	-0.83333	0	38	0.663225	0.633333	0.28932					
39	0.680678	60	1.047198	0	0	0	1.666667	-0.83333	0	39	0.680678	0.65	0.308953					
40	0.698132	60	1.047198	0	0	0	1.666667	-0.83333	0	40	0.698132	0.666667	0.329218					
41	0.715585	60	1.047198	0	0	0	1.666667	-0.83333	0	41	0.715585	0.683333	0.3501					
42	0.733038	60	1.047198	0	0	0	1.666667	-0.83333	0	42	0.733038	0.7	0.371583					
43	0.750549	60	1.047198	0	0	0	1.666667	-0.83333	0	43	0.750549	0.716667	0.39365					
44	0.767945	60	1.047198	0	0	0	1.666667	-0.83333	0	44	0.767945	0.733333	0.41628					
45	0.785398	60	1.047198	0	0	0	1.666667	-0.83333	0	45	0.785398	0.75	0.439453					
46	0.802851	60	1.047198	0	0	0	1.666667	-0.83333	0	46	0.802851	0.766667	0.463147					
47	0.820305	60	1.047198	0	0	0	1.666667	-0.83333	0	47	0.820305	0.783333	0.487338					
48	0.837758	60	1.047198	0	0	0	1.666667	-0.83333	0	48	0.837758	0.8	0.512					
49	0.855211	60	1.047198	0	0	0	1.666667	-0.83333	0	49	0.855211	0.816667	0.537106					
50	0.872665	60	1.047198	0	0	0	1.666667	-0.83333	0	50	0.872665	0.833333	0.562629					
51	0.890118	60	1.047198	0	0	0	1.666667	-0.83333	0	51	0.890118	0.85	0.588536					
52	0.907571	60	1.047198	0	0	0	1.666667	-0.83333	0	52	0.907571	0.866667	0.614798					
53	0.925025	60	1.047198	0	0	0	1.666667	-0.83333	0	53	0.925025	0.883333	0.641381					
54	0.942478	60	1.047198	0	0	0	1.666667	-0.83333	0	54	0.942478	0.9	0.66825					
55	0.959931	60	1.047198	0	0	0	1.666667	-0.83333	0	55	0.959931	0.916667	0.695369					
56	0.977384	60	1.047198	0	0	0	1.666667	-0.83333	0	56	0.977384	0.933333	0.7227					
57	0.994838	60	1.047198	0	0	0	1.666667	-0.83333	0	57	0.994838	0.95	0.750203					
58	1.012291	60	1.047198	0	0	0	1.666667	-0.83333	0	58	1.012291	0.966667	0.777838					
59	1.029744	60	1.047198	0	0	0	1.666667	-0.83333	0	59	1.029744	0.983333	0.805563					
60	1.047198	180	3.141593	0.8333333	5	0	0	0	0	60	1.047198	1	0.833333					
61	1.064651	180	3.141593	0.8333333	5	0	0	0	0	61	1.064651	1	1.591549	0	0			
62	1.082104	180	3.141593	0.8333333	5	0	0	0	0	62	1.082104	2	0.034907	0.011111	0.888889	1.591549	0	0
63	1.099557	180	3.141593	0.8333333	5	0	0	0	0	63	1.099557	3	0.05236	0.016667	0.916667	1.591549	0	0
64	1.117011	180	3.141593	0.8333333	5	0	0	0	0	64	1.117011	4	0.069813	0.022222	0.944444	1.591549	0	0
65	1.134464	180	3.141593	0.8333333	5	0	0	0	0	65	1.134464	5	0.087266	0.027778	0.972222	1.591549	0	0
66	1.151917	180	3.141593	0.8333333	5	0	0	0	0	66	1.151917	6	0.10472	0.033333	1	1.591549	0	0
67	1.169371	180	3.141593	0.8333333	5	0	0	0	0	67	1.169371	7	0.122173	0.038889	1.027778	1.591549	0	0
68	1.186824	180	3.141593	0.8333333	5	0	0	0	0	68	1.186824	8	0.139626	0.044444	1.055556	1.591549	0	0
69	1.204277	180	3.141593	0.8333333	5	0	0	0	0	69	1.204277	9	0.15708	0.05	1.083333	1.591549	0	0
70	1.22173	180	3.141593	0.8333333	5	0	0	0	0	70	1.22173	10	0.174533	0.055556	1.111111	1.591549	0	0
71	1.239184	180	3.141593	0.8333333	5	0	0	0	0	71	1.239184	11	0.191986	0.061111	1.138889	1.591549	0	0
72	1.256637	180	3.141593	0.8333333	5	0	0	0	0	72	1.256637	12	0.20944	0.066667	1.166667	1.591549	0	0
73	1.27409	180	3.141593	0.8333333	5	0	0	0	0	73	1.27409	13	0.226893	0.072222	1.194444	1.591549	0	0
74	1.291544	180	3.141593	0.8333333	5	0	0	0	0	74</								

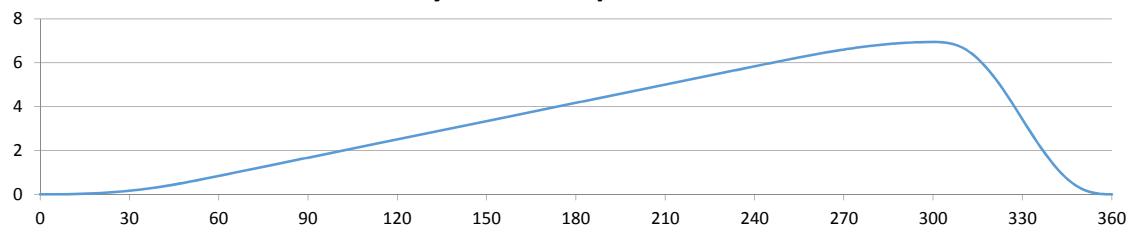
83	1.448623	180	3.141593	0.8333333	5	0	0	0	0	23	0.401426	0.127778	1.472222	1.591549	0	0
84	1.466077	180	3.141593	0.8333333	5	0	0	0	0	24	0.418879	0.133333	1.5	1.591549	0	0
85	1.48353	180	3.141593	0.8333333	5	0	0	0	0	25	0.436332	0.138889	1.527778	1.591549	0	0
86	1.500983	180	3.141593	0.8333333	5	0	0	0	0	26	0.453786	0.144444	1.555556	1.591549	0	0
87	1.518436	180	3.141593	0.8333333	5	0	0	0	0	27	0.471239	0.15	1.583333	1.591549	0	0
88	1.53589	180	3.141593	0.8333333	5	0	0	0	0	28	0.488692	0.155556	1.611111	1.591549	0	0
89	1.553343	180	3.141593	0.8333333	5	0	0	0	0	29	0.506145	0.161111	1.638889	1.591549	0	0
90	1.570796	180	3.141593	0.8333333	5	0	0	0	0	30	0.523599	0.166667	1.666667	1.591549	0	0
91	1.58825	180	3.141593	0.8333333	5	0	0	0	0	31	0.541052	0.172222	1.694444	1.591549	0	0
92	1.605703	180	3.141593	0.8333333	5	0	0	0	0	32	0.558505	0.177778	1.722222	1.591549	0	0
93	1.623156	180	3.141593	0.8333333	5	0	0	0	0	33	0.575959	0.183333	1.75	1.591549	0	0
94	1.640609	180	3.141593	0.8333333	5	0	0	0	0	34	0.593412	0.188889	1.777778	1.591549	0	0
95	1.658063	180	3.141593	0.8333333	5	0	0	0	0	35	0.610865	0.194444	1.805556	1.591549	0	0
96	1.675516	180	3.141593	0.8333333	5	0	0	0	0	36	0.628319	0.2	1.833333	1.591549	0	0
97	1.692969	180	3.141593	0.8333333	5	0	0	0	0	37	0.645772	0.205556	1.861111	1.591549	0	0
98	1.710423	180	3.141593	0.8333333	5	0	0	0	0	38	0.663225	0.211111	1.888889	1.591549	0	0
99	1.727876	180	3.141593	0.8333333	5	0	0	0	0	39	0.680678	0.216667	1.916667	1.591549	0	0
100	1.745329	180	3.141593	0.8333333	5	0	0	0	0	40	0.698132	0.222222	1.944444	1.591549	0	0
101	1.762783	180	3.141593	0.8333333	5	0	0	0	0	41	0.715585	0.227778	1.972222	1.591549	0	0
102	1.780236	180	3.141593	0.8333333	5	0	0	0	0	42	0.730308	0.233333	2	1.591549	0	0
103	1.797689	180	3.141593	0.8333333	5	0	0	0	0	43	0.750492	0.238889	2.027778	1.591549	0	0
104	1.815142	180	3.141593	0.8333333	5	0	0	0	0	44	0.767945	0.244444	2.055556	1.591549	0	0
105	1.832596	180	3.141593	0.8333333	5	0	0	0	0	45	0.785398	0.25	2.083333	1.591549	0	0
106	1.850049	180	3.141593	0.8333333	5	0	0	0	0	46	0.802851	0.255556	2.111111	1.591549	0	0
107	1.867502	180	3.141593	0.8333333	5	0	0	0	0	47	0.820303	0.261111	2.138889	1.591549	0	0
108	1.884956	180	3.141593	0.8333333	5	0	0	0	0	48	0.837758	0.266667	2.166667	1.591549	0	0
109	1.902409	180	3.141593	0.8333333	5	0	0	0	0	49	0.852511	0.272222	2.194444	1.591549	0	0
110	1.919862	180	3.141593	0.8333333	5	0	0	0	0	50	0.872665	0.277778	2.222222	1.591549	0	0
111	1.937315	180	3.141593	0.8333333	5	0	0	0	0	51	0.890118	0.283333	2.25	1.591549	0	0
112	1.954769	180	3.141593	0.8333333	5	0	0	0	0	52	0.907571	0.288889	2.277778	1.591549	0	0
113	1.972222	180	3.141593	0.8333333	5	0	0	0	0	53	0.925025	0.294444	2.305556	1.591549	0	0
114	1.989675	180	3.141593	0.8333333	5	0	0	0	0	54	0.942478	0.3	2.333333	1.591549	0	0
115	2.007129	180	3.141593	0.8333333	5	0	0	0	0	55	0.959931	0.305556	2.361111	1.591549	0	0
116	2.024582	180	3.141593	0.8333333	5	0	0	0	0	56	0.977934	0.311111	2.388889	1.591549	0	0
117	2.042035	180	3.141593	0.8333333	5	0	0	0	0	57	0.994838	0.316667	2.416667	1.591549	0	0
118	2.059489	180	3.141593	0.8333333	5	0	0	0	0	58	0.102291	0.322222	2.444444	1.591549	0	0
119	2.076942	180	3.141593	0.8333333	5	0	0	0	0	59	0.1029744	0.327778	2.472222	1.591549	0	0
120	2.094395	180	3.141593	0.8333333	5	0	0	0	0	60	0.1047198	0.333333	2.5	1.591549	0	0
121	2.111848	180	3.141593	0.8333333	5	0	0	0	0	61	0.1064651	0.338889	2.527778	1.591549	0	0
122	2.129302	180	3.141593	0.8333333	5	0	0	0	0	62	0.1082104	0.344444	2.555556	1.591549	0	0
123	2.146755	180	3.141593	0.8333333	5	0	0	0	0	63	0.1099557	0.35	2.583333	1.591549	0	0
124	2.164208	180	3.141593	0.8333333	5	0	0	0	0	64	0.117011	0.355556	2.611111	1.591549	0	0
125	2.181662	180	3.141593	0.8333333	5	0	0	0	0	65	0.134464	0.361111	2.638889	1.591549	0	0
126	2.199115	180	3.141593	0.8333333	5	0	0	0	0	66	0.151917	0.366667	2.666667	1.591549	0	0
127	2.216568	180	3.141593	0.8333333	5	0	0	0	0	67	0.169371	0.372222	2.694444	1.591549	0	0
128	2.234021	180	3.141593	0.8333333	5	0	0	0	0	68	0.186824	0.377778	2.722222	1.591549	0	0
129	2.251475	180	3.141593	0.8333333	5	0	0	0	0	69	0.204277	0.383333	2.75	1.591549	0	0
130	2.268928	180	3.141593	0.8333333	5	0	0	0	0	70	0.221713	0.388889	2.777778	1.591549	0	0
131	2.286381	180	3.141593	0.8333333	5	0	0	0	0	71	0.239184	0.394444	2.805556	1.591549	0	0
132	2.303835	180	3.141593	0.8333333	5	0	0	0	0	72	0.256637	0.4	2.833333	1.591549	0	0
133	2.321288	180	3.141593	0.8333333	5	0	0	0	0	73	0.27409	0.405556	2.861111	1.591549	0	0
134	2.338741	180	3.141593	0.8333333	5	0	0	0	0	74	0.291544	0.411111	2.888889	1.591549	0	0
135	2.356194	180	3.141593	0.8333333	5	0	0	0	0	75	0.308997	0.416667	2.916667	1.591549	0	0
136	2.373648	180	3.141593	0.8333333	5	0	0	0	0	76	0.32645	0.422222	2.944444	1.591549	0	0
137	2.391101	180	3.141593	0.8333333	5	0	0	0	0	77	0.343904	0.427778	2.972222	1.591549	0	0
138	2.408554	180	3.141593	0.8333333	5	0	0	0	0	78	0.361357	0.433333	3	1.591549	0	0
139	2.426008	180	3.141593	0.8333333	5	0	0	0	0	79	0.37881	0.438889	3.027778	1.591549	0	0
140	2.443461	180	3.141593	0.8333333	5	0	0	0	0	80	0.396263	0.444444	3.055556	1.591549	0	0
141	2.460914	180	3.141593	0.8333333	5	0	0	0	0	81	0.413717	0.45	3.083333	1.591549	0	0
142	2.478368	180	3.141593	0.8333333	5	0	0	0	0	82	0.43117	0.455556	3.111111	1.591549	0	0
143	2.495821	180	3.141593	0.8333333	5	0	0	0	0	83	0.448623	0.461111	3.138889	1.591549	0	0
144	2.513274	180	3.141593	0.8333333	5	0	0	0	0	84	0.466077	0.466667	3.166667	1.591549	0	0
145	2.530727	180	3.141593	0.8333333	5	0	0	0	0	85	0.48353	0.472222	3.194444	1.591549	0	0
146	2.548181	180	3.141593	0.8333333	5	0	0	0	0	86	0.500983	0.477778	3.222222	1.591549	0	0
147	2.565634	180	3.141593	0.8333333	5	0	0	0	0	87	0.518436	0.483333	3.25	1.591549	0	0
148	2.583087	180	3.141593	0.8333333	5	0	0	0	0	88	0.53589	0.488889	3.277778	1.591549	0	0
149	2.600541	180	3.141593	0.8333333	5	0	0	0	0	89	0.553343	0.494444	3.305556	1.591549	0	0
150	2.617994	180	3.141593	0.8333333	5	0	0	0	0	90	0.570796	0.5	3.333333	1.591549	0	0
151	2.635447	180	3.141593	0.8333333	5	0	0	0	0	91	0.58825	0.505556	3.361111	1.591549	0	0</td

170	2.96706	180	3.141593	0.8333333	5	0	0	0	0	110	1.919862	0.611111	3.888889	1.591549	0	0
171	2.984513	180	3.141593	0.8333333	5	0	0	0	0	111	1.937315	0.616667	3.916667	1.591549	0	0
172	3.001966	180	3.141593	0.8333333	5	0	0	0	0	112	1.954769	0.622222	3.944444	1.591549	0	0
173	3.01942	180	3.141593	0.8333333	5	0	0	0	0	113	1.972222	0.627778	3.972222	1.591549	0	0
174	3.036873	180	3.141593	0.8333333	5	0	0	0	0	114	1.989675	0.633333	4	1.591549	0	0
175	3.054326	180	3.141593	0.8333333	5	0	0	0	0	115	2.007129	0.638889	4.027778	1.591549	0	0
176	3.071779	180	3.141593	0.8333333	5	0	0	0	0	116	2.024582	0.644444	4.055556	1.591549	0	0
177	3.089233	180	3.141593	0.8333333	5	0	0	0	0	117	2.042035	0.65	4.083333	1.591549	0	0
178	3.106686	180	3.141593	0.8333333	5	0	0	0	0	118	2.059489	0.655556	4.111111	1.591549	0	0
179	3.124139	180	3.141593	0.8333333	5	0	0	0	0	119	2.076942	0.661111	4.138889	1.591549	0	0
180	3.141593	180	3.141593	0.8333333	5	0	0	0	0	120	2.094395	0.666667	4.166667	1.591549	0	0
181	3.159046	180	3.141593	0.8333333	5	0	0	0	0	121	2.111848	0.672222	4.194444	1.591549	0	0
182	3.176499	180	3.141593	0.8333333	5	0	0	0	0	122	2.129302	0.677778	4.222222	1.591549	0	0
183	3.193953	180	3.141593	0.8333333	5	0	0	0	0	123	2.146755	0.683333	4.25	1.591549	0	0
184	3.211406	180	3.141593	0.8333333	5	0	0	0	0	124	2.164208	0.688889	4.277778	1.591549	0	0
185	3.228859	180	3.141593	0.8333333	5	0	0	0	0	125	2.181662	0.694444	4.305556	1.591549	0	0
186	3.246312	180	3.141593	0.8333333	5	0	0	0	0	126	2.199115	0.7	4.333333	1.591549	0	0
187	3.263766	180	3.141593	0.8333333	5	0	0	0	0	127	2.216568	0.705556	4.361111	1.591549	0	0
188	3.281219	180	3.141593	0.8333333	5	0	0	0	0	128	2.234021	0.711111	4.388889	1.591549	0	0
189	3.298672	180	3.141593	0.8333333	5	0	0	0	0	129	2.251475	0.716667	4.416667	1.591549	0	0
190	3.316126	180	3.141593	0.8333333	5	0	0	0	0	130	2.268928	0.722222	4.444444	1.591549	0	0
191	3.333579	180	3.141593	0.8333333	5	0	0	0	0	131	2.286381	0.727778	4.472222	1.591549	0	0
192	3.351032	180	3.141593	0.8333333	5	0	0	0	0	132	2.303835	0.733333	4.5	1.591549	0	0
193	3.368485	180	3.141593	0.8333333	5	0	0	0	0	133	2.321288	0.738889	4.527778	1.591549	0	0
194	3.385939	180	3.141593	0.8333333	5	0	0	0	0	134	2.338741	0.744444	4.555556	1.591549	0	0
195	3.403392	180	3.141593	0.8333333	5	0	0	0	0	135	2.356194	0.75	4.583333	1.591549	0	0
196	3.420845	180	3.141593	0.8333333	5	0	0	0	0	136	2.373648	0.755556	4.611111	1.591549	0	0
197	3.438299	180	3.141593	0.8333333	5	0	0	0	0	137	2.391101	0.761111	4.638889	1.591549	0	0
198	3.455752	180	3.141593	0.8333333	5	0	0	0	0	138	2.408554	0.766667	4.666667	1.591549	0	0
199	3.473205	180	3.141593	0.8333333	5	0	0	0	0	139	2.426008	0.772222	4.694444	1.591549	0	0
200	3.490659	180	3.141593	0.8333333	5	0	0	0	0	140	2.443461	0.777778	4.722222	1.591549	0	0
201	3.508112	180	3.141593	0.8333333	5	0	0	0	0	141	2.460914	0.783333	4.75	1.591549	0	0
202	3.525565	180	3.141593	0.8333333	5	0	0	0	0	142	2.478368	0.788889	4.777778	1.591549	0	0
203	3.543018	180	3.141593	0.8333333	5	0	0	0	0	143	2.495821	0.794444	4.805556	1.591549	0	0
204	3.560472	180	3.141593	0.8333333	5	0	0	0	0	144	2.513274	0.8	4.833333	1.591549	0	0
205	3.577925	180	3.141593	0.8333333	5	0	0	0	0	145	2.530727	0.805556	4.861111	1.591549	0	0
206	3.595378	180	3.141593	0.8333333	5	0	0	0	0	146	2.548181	0.811111	4.888889	1.591549	0	0
207	3.612832	180	3.141593	0.8333333	5	0	0	0	0	147	2.565634	0.816667	4.916667	1.591549	0	0
208	3.630285	180	3.141593	0.8333333	5	0	0	0	0	148	2.583087	0.822222	4.944444	1.591549	0	0
209	3.647738	180	3.141593	0.8333333	5	0	0	0	0	149	2.600541	0.827778	4.972222	1.591549	0	0
210	3.665191	180	3.141593	0.8333333	5	0	0	0	0	150	2.617994	0.833333	5	1.591549	0	0
211	3.682645	180	3.141593	0.8333333	5	0	0	0	0	151	2.635447	0.838889	5.027778	1.591549	0	0
212	3.700098	180	3.141593	0.8333333	5	0	0	0	0	152	2.6529	0.844444	5.055556	1.591549	0	0
213	3.717551	180	3.141593	0.8333333	5	0	0	0	0	153	2.670354	0.85	5.083333	1.591549	0	0
214	3.735005	180	3.141593	0.8333333	5	0	0	0	0	154	2.687807	0.855556	5.111111	1.591549	0	0
215	3.752458	180	3.141593	0.8333333	5	0	0	0	0	155	2.70526	0.861111	5.138889	1.591549	0	0
216	3.769911	180	3.141593	0.8333333	5	0	0	0	0	156	2.722714	0.866667	5.166667	1.591549	0	0
217	3.787364	180	3.141593	0.8333333	5	0	0	0	0	157	2.740167	0.872222	5.194444	1.591549	0	0
218	3.804818	180	3.141593	0.8333333	5	0	0	0	0	158	2.75762	0.877778	5.222222	1.591549	0	0
219	3.822271	180	3.141593	0.8333333	5	0	0	0	0	159	2.775074	0.883333	5.25	1.591549	0	0
220	3.839724	180	3.141593	0.8333333	5	0	0	0	0	160	2.792527	0.888889	5.277778	1.591549	0	0
221	3.857178	180	3.141593	0.8333333	5	0	0	0	0	161	2.80998	0.894444	5.305556	1.591549	0	0
222	3.874631	180	3.141593	0.8333333	5	0	0	0	0	162	2.827433	0.9	5.333333	1.591549	0	0
223	3.892084	180	3.141593	0.8333333	5	0	0	0	0	163	2.844887	0.905556	5.361111	1.591549	0	0
224	3.909538	180	3.141593	0.8333333	5	0	0	0	0	164	2.86234	0.911111	5.388889	1.591549	0	0
225	3.926991	180	3.141593	0.8333333	5	0	0	0	0	165	2.879793	0.916667	5.416667	1.591549	0	0
226	3.944444	180	3.141593	0.8333333	5	0	0	0	0	166	2.897247	0.922222	5.444444	1.591549	0	0
227	3.961897	180	3.141593	0.8333333	5	0	0	0	0	167	2.9147	0.927778	5.472222	1.591549	0	0
228	3.979351	180	3.141593	0.8333333	5	0	0	0	0	168	2.932153	0.933333	5.5	1.591549	0	0
229	3.996804	180	3.141593	0.8333333	5	0	0	0	0	169	2.949606	0.938889	5.527778	1.591549	0	0
230	4.014257	180	3.141593	0.8333333	5	0	0	0	0	170	2.96706	0.944444	5.555556	1.591549	0	0
231	4.031711	180	3.141593	0.8333333	5	0	0	0	0	171	2.984513	0.95	5.583333	1.591549	0	0
232	4.049164	180	3.141593	0.8333333	5	0	0	0	0	172	3.001966	0.955556	5.611111	1.591549	0	0
233	4.066617	180	3.141593	0.8333333	5	0	0	0	0	173	3.01942	0.961111	5.638889	1.591549	0	0
234	4.084087	180	3.141593	0.8333333	5	0	0	0	0	174	3.036873	0.966667	5.666667	1.591549	0	0
235	4.101524	180	3.141593	0.8333333	5	0	0	0	0	175	3.054326	0.972222	5.694444	1.591549	0	0
236	4.118977	180	3.141593	0.8333333	5	0	0	0	0	176	3.071779	0.977778	5.722222	1.591549	0	0
237	4.13643	180	3.141593	0.8333333	5	0	0	0	0	177	3.089233	0.983333	5.75	1.591549	0	0
238	4.153884	180	3.141593	0.8333333	5	0	0									

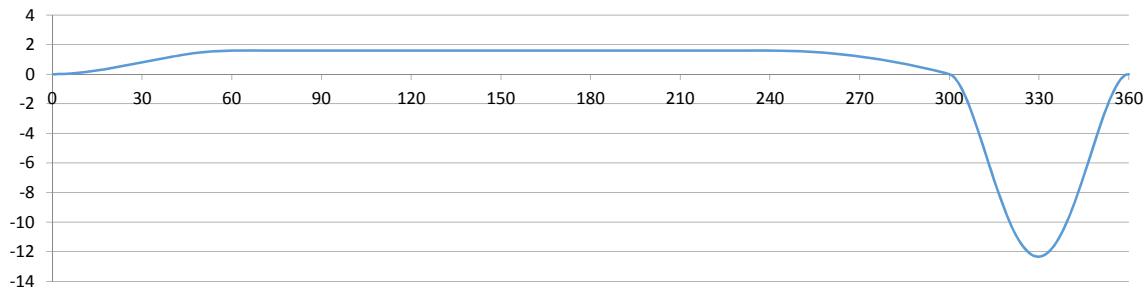
256	4.468043	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	16	0.279253	0.266667	6.267243	1.478373	-0.81057	-2.90264	
257	4.485496	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	17	0.296706	0.283333	6.292919	1.463783	-0.86123	-2.90264	
258	4.502949	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	18	0.314159	0.3	6.318333	1.44831	-0.91189	-2.90264	
259	4.520403	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	19	0.331613	0.316667	6.34347	1.431952	-0.96255	-2.90264	
260	4.537856	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	20	0.349066	0.333333	6.368313	1.414711	-1.01321	-2.90264	
261	4.555309	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	21	0.366519	0.35	6.392847	1.396585	-1.06387	-2.90264	
262	4.572763	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	22	0.383972	0.366667	6.417058	1.377574	-1.11453	-2.90264	
263	4.590216	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	23	0.401426	0.383333	6.440928	1.35768	-1.16519	-2.90264	
264	4.607669	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	24	0.418879	0.4	6.464444	1.336902	-1.21585	-2.90264	
265	4.625123	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	25	0.436332	0.416667	6.48759	1.315239	-1.26651	-2.90264	
266	4.642576	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	26	0.453786	0.433333	6.51035	1.292692	-1.31718	-2.90264	
267	4.660029	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	27	0.471239	0.45	6.532708	1.269261	-1.36784	-2.90264	
268	4.677482	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	28	0.488692	0.466667	6.55465	1.244945	-1.4185	-2.90264	
269	4.694936	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	29	0.506145	0.483333	6.57616	1.219746	-1.46916	-2.90264	
270	4.712389	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	30	0.523599	0.5	6.597222	1.193662	-1.51982	-2.90264	
271	4.729842	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	31	0.541052	0.516667	6.617822	1.166694	-1.57048	-2.90264	
272	4.747296	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	32	0.558505	0.533333	6.637942	1.138842	-1.62114	-2.90264	
273	4.764749	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	33	0.575959	0.55	6.657569	1.110106	-1.6718	-2.90264	
274	4.782202	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	34	0.593412	0.566667	6.676687	1.080485	-1.72246	-2.90264	
275	4.799655	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	35	0.610865	0.583333	6.69528	1.049981	-1.77312	-2.90264	
276	4.817109	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	36	0.628319	0.6	6.713333	1.018592	-1.82378	-2.90264	
277	4.834562	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	37	0.645772	0.616667	6.730831	0.986319	-1.87444	-2.90264	
278	4.852015	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	38	0.663225	0.633333	6.747757	0.953161	-1.9251	-2.90264	
279	4.869469	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	39	0.680678	0.65	6.764097	0.91912	-1.97576	-2.90264	
280	4.886922	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	40	0.698132	0.666667	6.779835	0.884194	-2.02642	-2.90264	
281	4.904375	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	41	0.715585	0.683333	6.794956	0.848384	-2.07708	-2.90264	
282	4.921282	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	42	0.730308	0.7	6.809444	0.81169	-2.12774	-2.90264	
283	4.939282	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	43	0.750492	0.716667	6.823284	0.774112	-2.17841	-2.90264	
284	4.956735	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	44	0.767945	0.733333	6.836461	0.73565	-2.22907	-2.90264	
285	4.974188	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	45	0.785398	0.75	6.848958	0.696303	-2.27973	-2.90264	
286	4.991642	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	46	0.802851	0.766667	6.860761	0.656072	-2.33039	-2.90264	
287	5.009095	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	47	0.820305	0.783333	6.871854	0.614957	-2.38105	-2.90264	
288	5.026548	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	48	0.837758	0.8	6.882222	0.572958	-2.43171	-2.90264	
289	5.044002	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	49	0.852511	0.816667	6.891849	0.530074	-2.48237	-2.90264	
290	5.061455	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	50	0.872665	0.833333	6.90072	0.486307	-2.53303	-2.90264	
291	5.078908	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	51	0.890118	0.85	6.908819	0.441655	-2.58369	-2.90264	
292	5.096361	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	52	0.907571	0.866667	6.916132	0.396119	-2.63435	-2.90264	
293	5.113815	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	53	0.925025	0.883333	6.922641	0.349699	-2.68501	-2.90264	
294	5.131268	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	54	0.942478	0.9	6.928333	0.302394	-2.73567	-2.90264	
295	5.148721	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	55	0.959931	0.916667	6.933192	0.254206	-2.78633	-2.90264	
296	5.166175	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	56	0.977384	0.933333	6.937202	0.205133	-2.83699	-2.90264	
297	5.183628	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	57	0.994838	0.95	6.940347	0.155176	-2.88765	-2.90264	
298	5.201081	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	58	1.012291	0.966667	6.942613	0.104335	-2.93831	-2.90264	
299	5.218534	60	1.047198	5.8333333	1.666667	0	-0.55556	0	0	59	1.029744	0.983333	6.943984	0.05261	-2.98897	-2.90264	
300	5.235988	60	1.047198	5.8444444	0	-1.66667	-64.4444	99.16667	-40	0	0	0	0	6.944444	0	-3.03964	-336.706
301	5.253441	60	1.047198	5.9444444	0	-1.66667	-64.4444	99.16667	-40	1	0.017453	0.016667	6.943691	-0.1026	-8.61821	-302.745	
302	5.270894	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	2	0.034907	0.033333	6.940327	-0.29744	-13.6142	-269.945	
303	5.288348	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	3	0.05236	0.05	6.93283	-0.57455	-18.0478	-238.307	
304	5.305801	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	4	0.069813	0.066667	6.919849	-0.92428	-21.9394	-207.829	
305	5.323254	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	5	0.087266	0.083333	6.900198	-1.33734	-25.3092	-178.512	
306	5.340708	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	6	0.10472	0.1	6.87285	-1.80482	-28.1774	-150.357	
307	5.358161	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	7	0.122173	0.116667	6.836931	-2.31812	-30.5644	-123.362	
308	5.375614	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	8	0.139626	0.133333	6.791714	-2.86903	-32.4903	-97.5286	
309	5.393067	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	9	0.15708	0.15	6.73661	-3.44968	-33.9755	-72.8562	
310	5.410521	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	10	0.174533	0.166667	6.671168	-4.05256	-35.0402	-49.3448	
311	5.427974	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	11	0.191986	0.183333	6.595062	-4.67049	-35.7047	-26.9945	
312	5.445427	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	12	0.20944	0.2	6.508089	-5.29668	-35.9893	-8.0525	
313	5.462881	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	13	0.226893	0.216667	6.410162	-5.92466	-35.9141	14.22295	
314	5.480334	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	14	0.244346	0.233333	6.301304	-6.54834	-35.4996	33.0901	
315	5.497787	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40								

342	5.969026	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	42	0.73038	0.7	1.110452	-8.62301	31.64262	89.98181
343	5.986479	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	43	0.750492	0.716667	0.964848	-8.05777	33.08561	75.17835
344	6.003933	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	44	0.767945	0.733333	0.829315	-7.46966	34.26009	59.21385
345	6.021386	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	45	0.785398	0.75	0.704212	-6.86355	35.14581	42.08828
346	6.038839	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	46	0.802851	0.766667	0.589807	-6.24464	35.72249	23.80166
347	6.056293	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	47	0.820305	0.783333	0.486275	-5.61851	35.96989	4.353986
348	6.073746	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	48	0.837758	0.8	0.393691	-4.99109	35.86772	-16.2547
349	6.091199	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	49	0.85211	0.816667	0.312024	-4.36865	35.39573	-38.0245
350	6.108652	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	50	0.872665	0.833333	0.241129	-3.75782	34.53366	-60.9554
351	6.126106	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	51	0.890118	0.85	0.180744	-3.16558	33.26123	-85.0473
352	6.143559	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	52	0.907571	0.866667	0.130479	-2.59928	31.5582	-110.3
353	6.161012	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	53	0.925025	0.883333	0.089816	-2.06662	29.40428	-136.714
354	6.178466	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	54	0.942478	0.9	0.058098	-1.57562	26.77921	-164.289
355	6.195919	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	55	0.959931	0.916667	0.034525	-1.1347	23.66274	-193.025
356	6.213372	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	56	0.977384	0.933333	0.018147	-0.75261	20.0346	-222.923
357	6.230825	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	57	0.994838	0.95	0.007859	-0.43846	15.87452	-253.981
358	6.248279	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	58	1.012291	0.966667	0.002392	-0.2017	11.16224	-286.2
359	6.265732	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	59	1.029744	0.983333	0.000311	-0.05215	5.8775	-319.58
360	6.283185	60	1.047198	6.9444444	0	-1.66667	-64.4444	99.16667	-40	60	1.047198	1	4.78E-06	1.4E-05	2.8E-05	-354.122

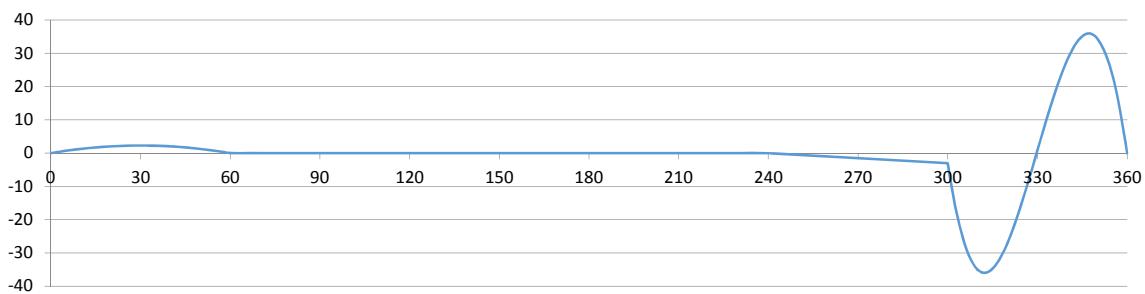
### **Polynomial Displacement**



### **Polynomial Velocity**



### **Polynomial Acceleration**



### **Polynomial Jerk**

