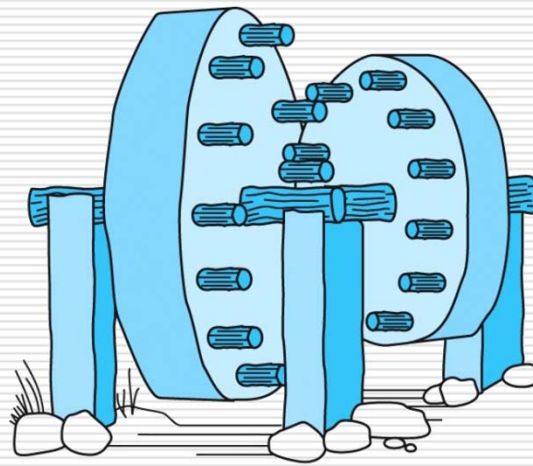
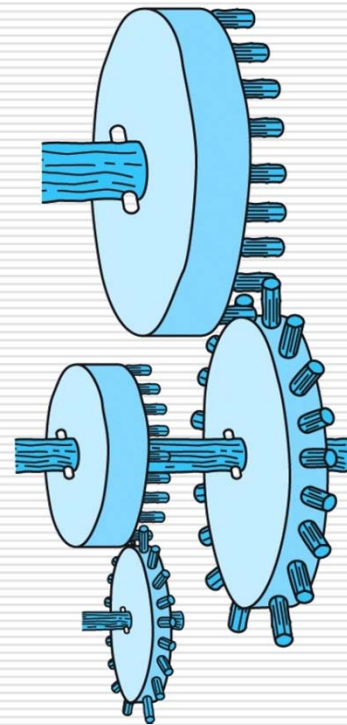


# Introduction to Gears

- Basic Nomenclature
- Conjugate **Action/Involute**



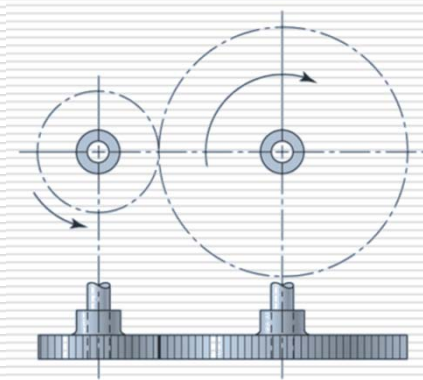
Right-angle gearing



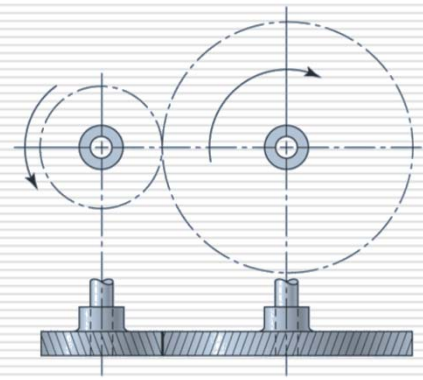
# Gears are Classified into Four Basic Types

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SPUR

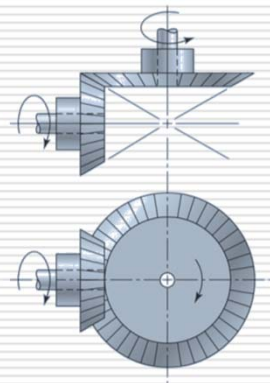


Helical

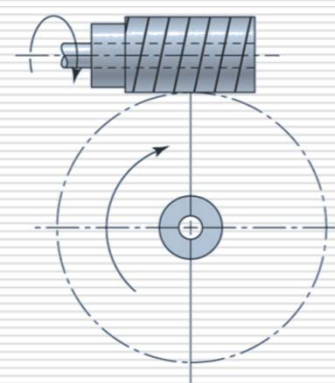


Bevel

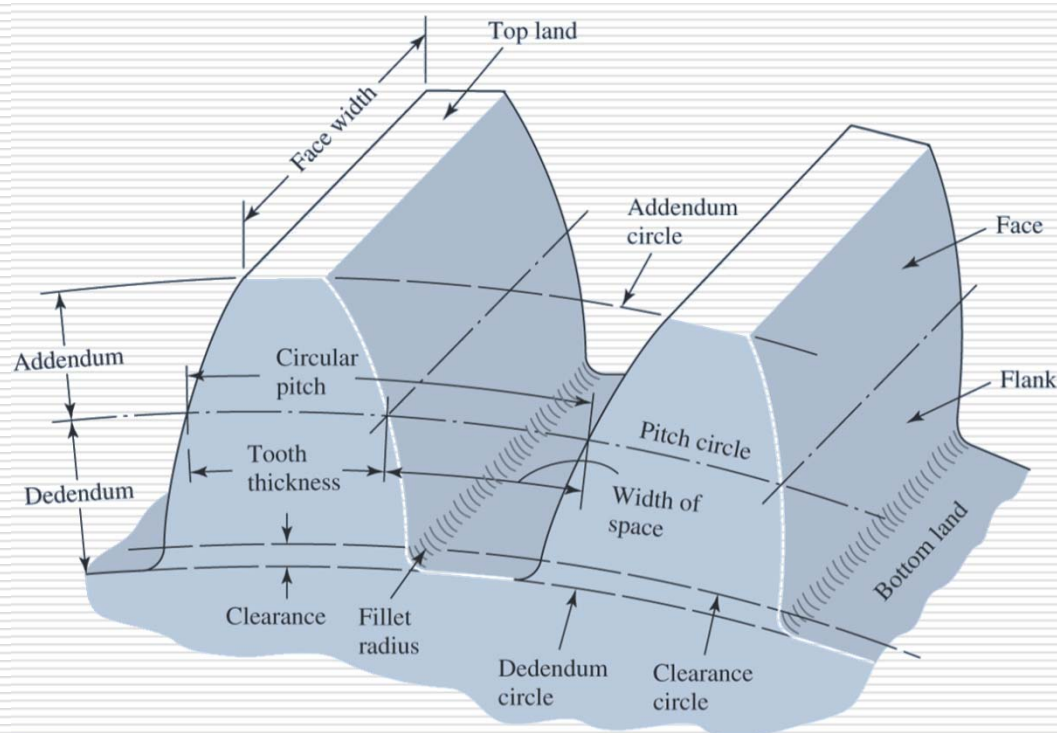
- Straight Tooth
- Spiral
- Hypoid



Worm



# Gear Nomenclature



$$P = \frac{N}{d} \equiv \frac{\text{Diametral}}{\text{Pitch}} \left[ \frac{\text{teeth}}{\text{in}} \right]$$

$$m = \frac{d}{N} \equiv \text{Module [mm]}$$

$$p = \frac{\pi \cdot d}{N} = \pi \cdot m \equiv \frac{\text{Circular}}{\text{Pitch}} \left[ \text{in or mm} \right]$$

$$= \frac{\pi \cdot d}{N} = \frac{\pi}{P}$$

$$p \cdot P = \pi$$

$$d \equiv \text{Pitch Diameter [in or mm]}$$

$$N \equiv \text{Number of Teeth}$$

# General Use Tooth Sizes

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## Diametral Pitch

Coarse	2, $2\frac{1}{4}$ , $2\frac{1}{2}$ , 3, 4, 6, 8, 10, 12, 16
Fine	20, 24, 32, 40, 48, 64, 80, 96, 120, 150, 200

## Modules

Preferred	1, 1.25, 1.5, 2, 2.5, 3, 4, 5, 6, 8, 10, 12, 16, 20, 25, 32, 40, 50
Next Choice	1.125, 1.375, 1.75, 2.25, 2.75, 3.5, 4.5, 5.5, 7, 9, 11, 14, 18, 22, 28, 36, 45

# Standard Tooth Systems for Spur Gears

Tooth System	Pressure Angle $\phi$ , deg	Addendum $a$	Dedendum $b$
Full depth	20	$1/P_d$ or $1m$	$1.25/P_d$ or $1.25m$ $1.35/P_d$ or $1.35m$
	$22\frac{1}{2}$	$1/P_d$ or $1m$	$1.25/P_d$ or $1.25m$ $1.35/P_d$ or $1.35m$
	25	$1/P_d$ or $1m$	$1.25/P_d$ or $1.25m$ $1.35/P_d$ or $1.35m$
Stub	20	$0.8/P_d$ or $0.8m$	$1/P_d$ or $1m$

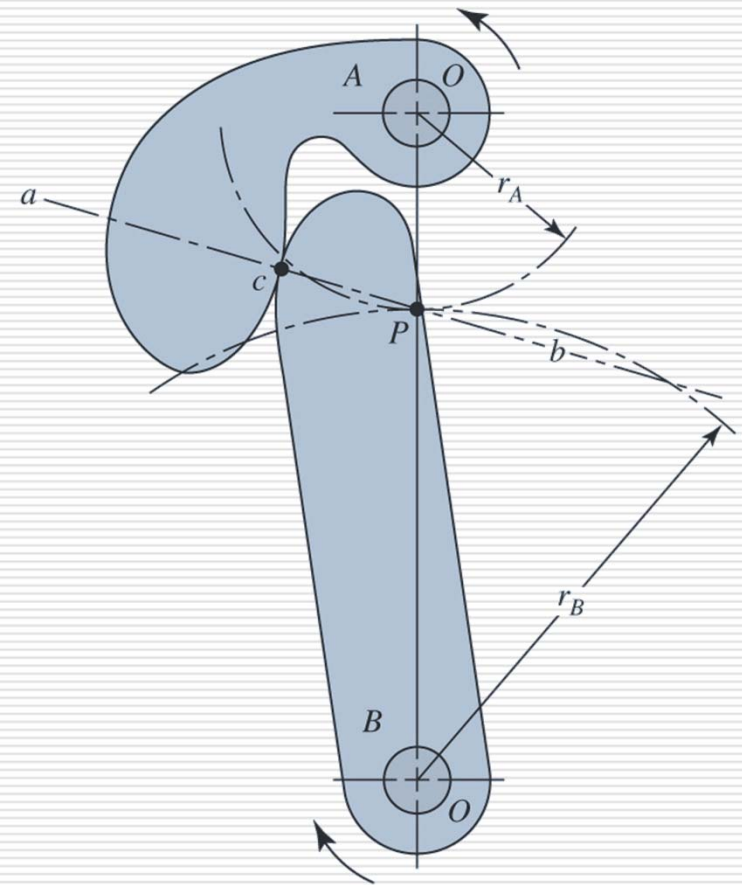
$$3p < F < 5p$$

Common Face Width  $p = \frac{\pi}{P}$

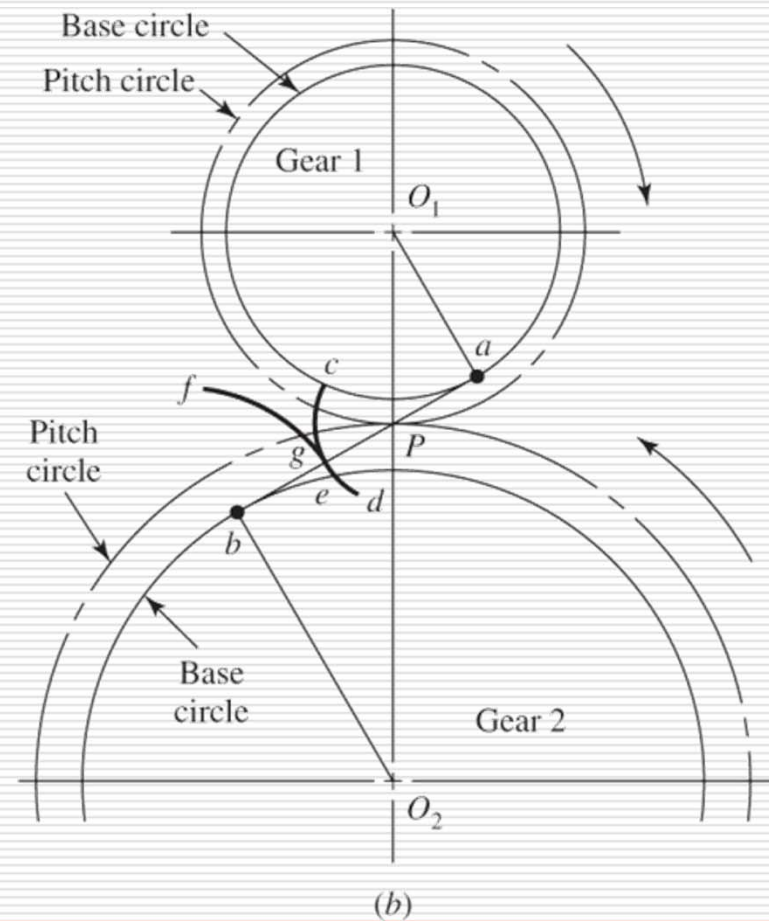
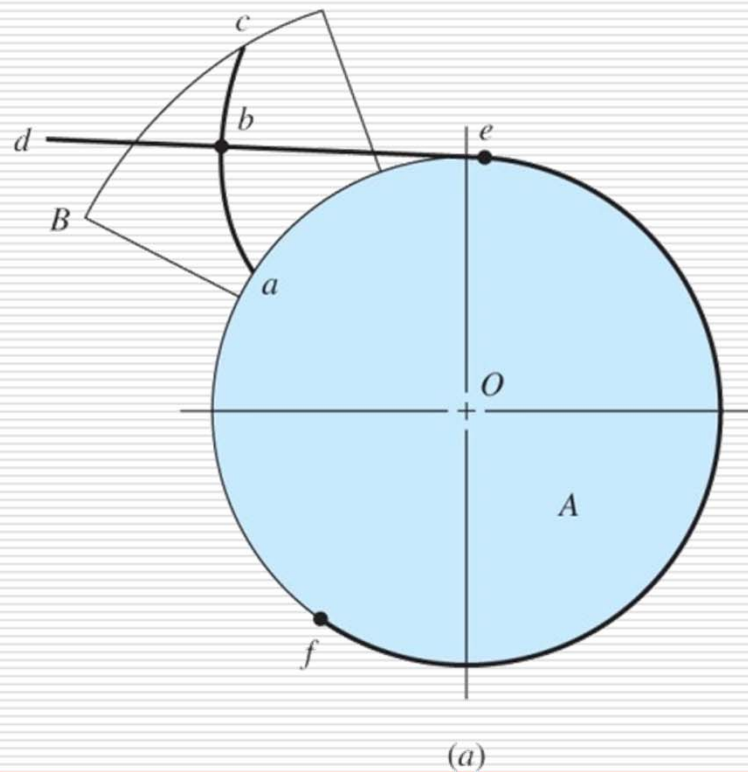
$$\frac{3\pi}{P} < F < \frac{5\pi}{P}$$

# Conjugate Action

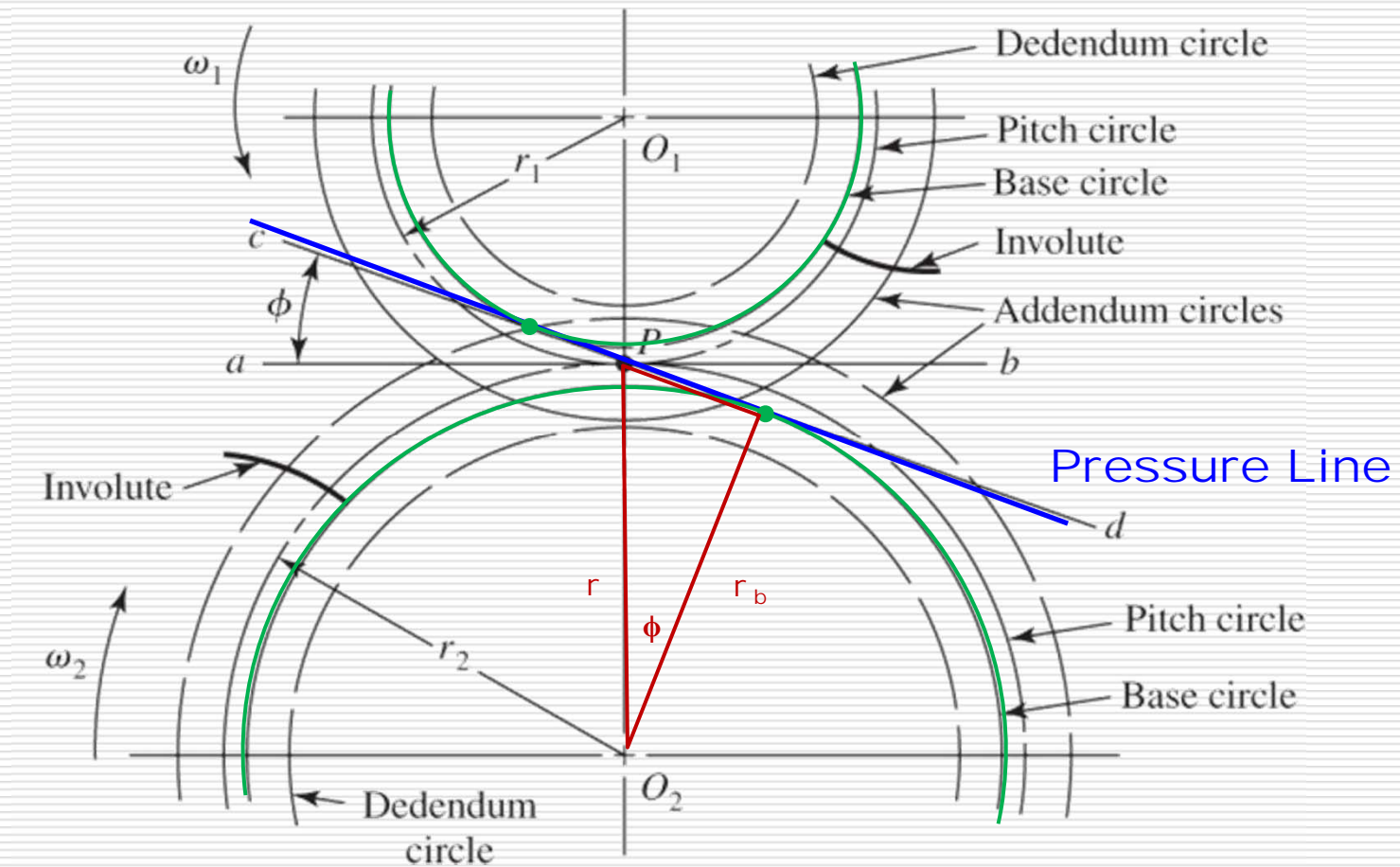
- Conjugate Action
  - Surfaces Roll/Slide Against Each Other
  - Produce Constant Angular Velocity
- Instant Center of Velocity Between Bodies Stationary
  - Between Ground ICs



# Understanding the Importance of the Involute



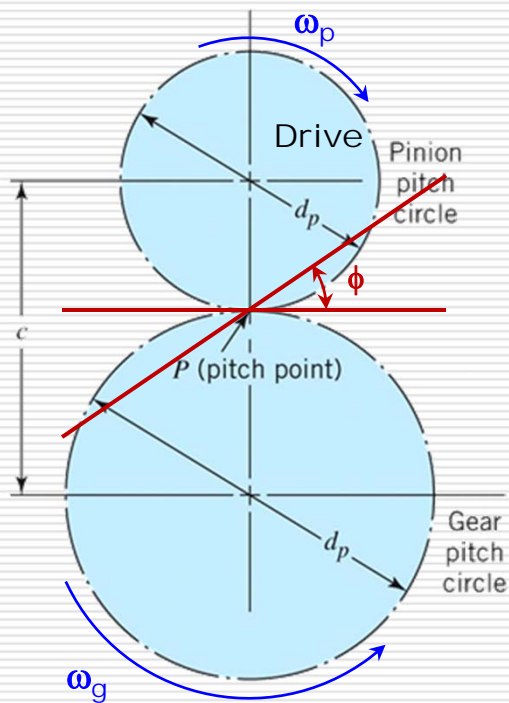
# Circles of a Gear Layout





# Force Analysis

- $F_t \times v$  accounts for power transmission
- $F_r$  does no work



Line of Action  
of the Force



## Torque on Shafts

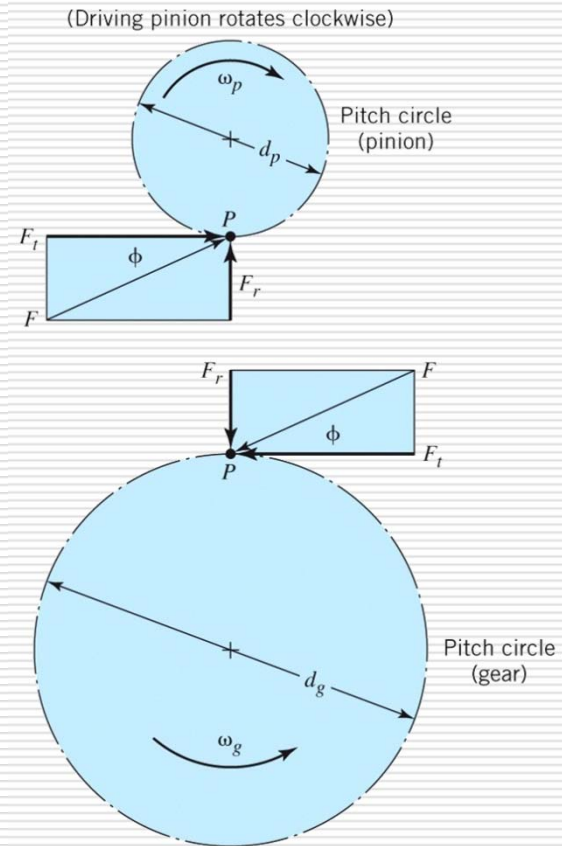
$$T_p = F_{tp} \cdot \frac{d_p}{2} = F_{tp} \cdot r_p$$

$$T_g = F_{tg} \cdot \frac{d_g}{2} = F_{tg} \cdot r_g$$

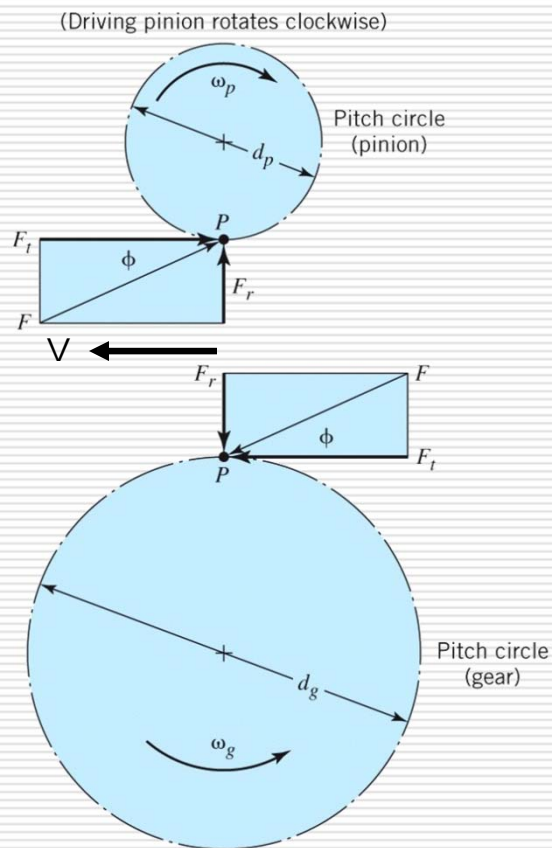
Subscripts: p-pinion, g-gear

$T \equiv$  Torque

$F_t \equiv$  Tangential Force at Pitch Point



# Force Analysis



## Pitch Line Velocity (feet / min)

$$V = r_p \cdot \omega_p = r_g \cdot \omega_g \left[ \frac{rad}{s} \right] \text{ or } \left[ \frac{1}{s} \right]$$

$$= \frac{\pi \cdot d_p \cdot n_p}{12} = \frac{\pi \cdot d_g \cdot n_g}{12} \left[ \frac{ft}{min} \right]$$

Subscripts: p-pinon, g-gear

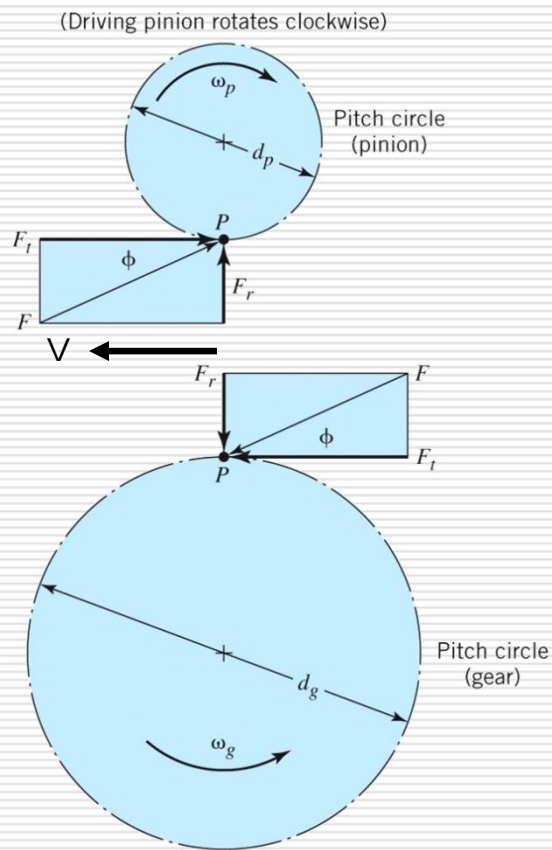
$n \equiv$  speed of the shaft, [rev/min]

$\omega \equiv$  speed of the shaft, [rad/s]

$r \equiv$  pitch radius, [in]

$d \equiv$  pitch diameter, [in]

# Power Transmission



## Transmitted Power in horsepower [hp], Imperial Units

$$H [hp] = \frac{F_t [lb] \cdot V [\frac{ft}{min}]}{33,000 [\frac{ft \cdot lb}{hp \cdot min}]} = \frac{T [lb \cdot in] \cdot n [\frac{rev}{min}]}{63025 \cdot [\frac{lb \cdot in \cdot rev}{min \cdot hp}]}$$

Subscripts: p-pinion, g-gear

$H \equiv$  Power

$F_t \equiv$  Tangential Force at pitch Point

$T \equiv$  Torque

$V \equiv$  pitch line velocity

$n \equiv$  angular velocity

## Transmitted Power in kilo - Watts [kW], SI Units

$$H [kW] = F_t \cdot V$$

Subscripts: p-pinion, g-gear

$H \equiv$  Power, [kW]

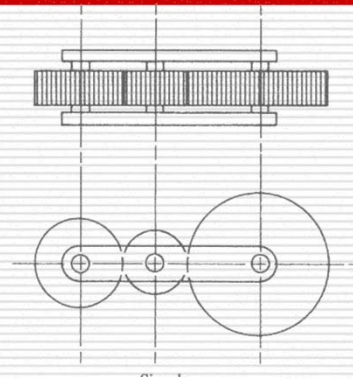
$F_t \equiv$  Tangential Force at pitch Point, [N]

$$V [\frac{m}{s}] \equiv \text{pitch line velocity} = \frac{\pi \cdot d [\text{mm}] \cdot n [\frac{rev}{min}]}{60,000}$$

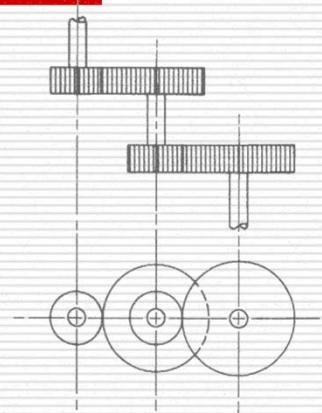
$d \equiv$  pitch diameter

# Gear Trains

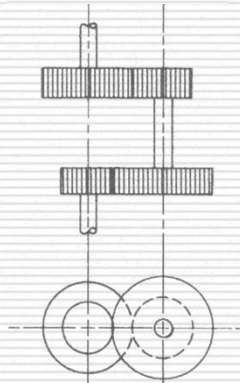
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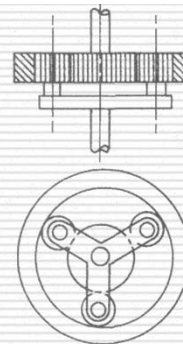
Simple



Compound

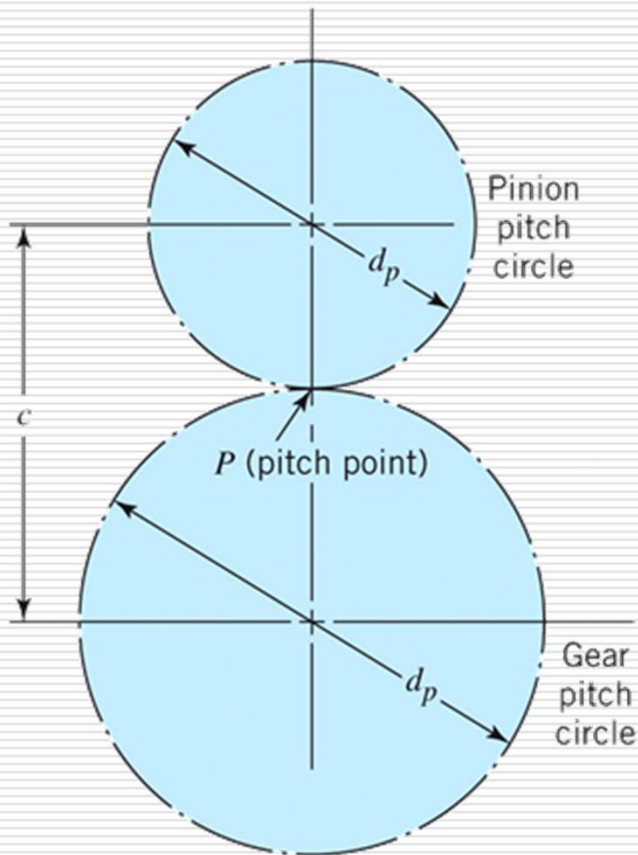


Reverted



Planetary

# Gear Train's Gear Ratio



## Gear Ratio

$$\left| \frac{\omega_p}{\omega_g} \right| = \left| \frac{n_g}{n_p} \right| = \frac{d_g}{d_p} = \frac{N_g}{N_p}$$

Subscripts: p-pinion, g-gear

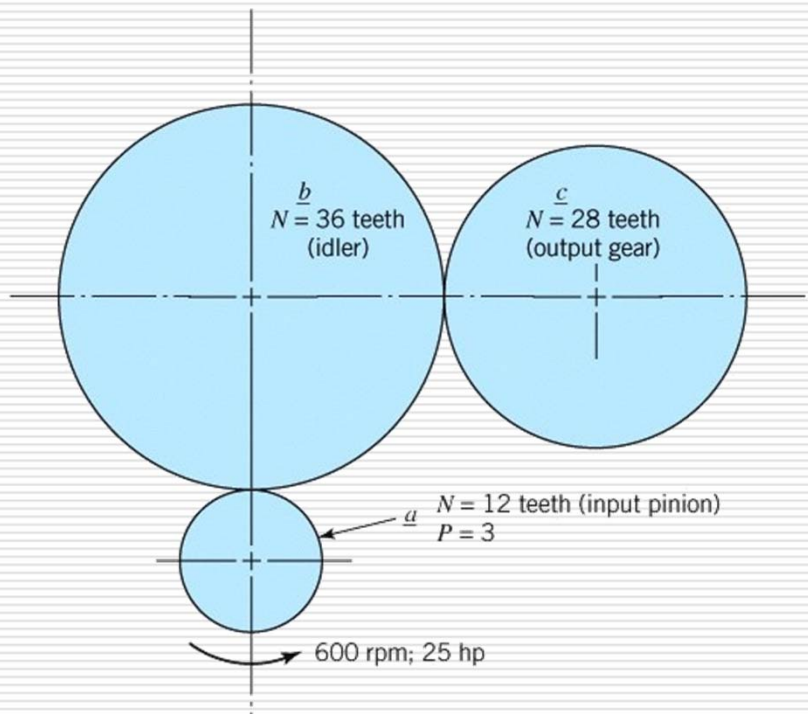
$n \equiv$  speed of the shaft, [rev/min]

$\omega \equiv$  speed of the shaft, [rad/s]

$d \equiv$  pitch diameter, [in]

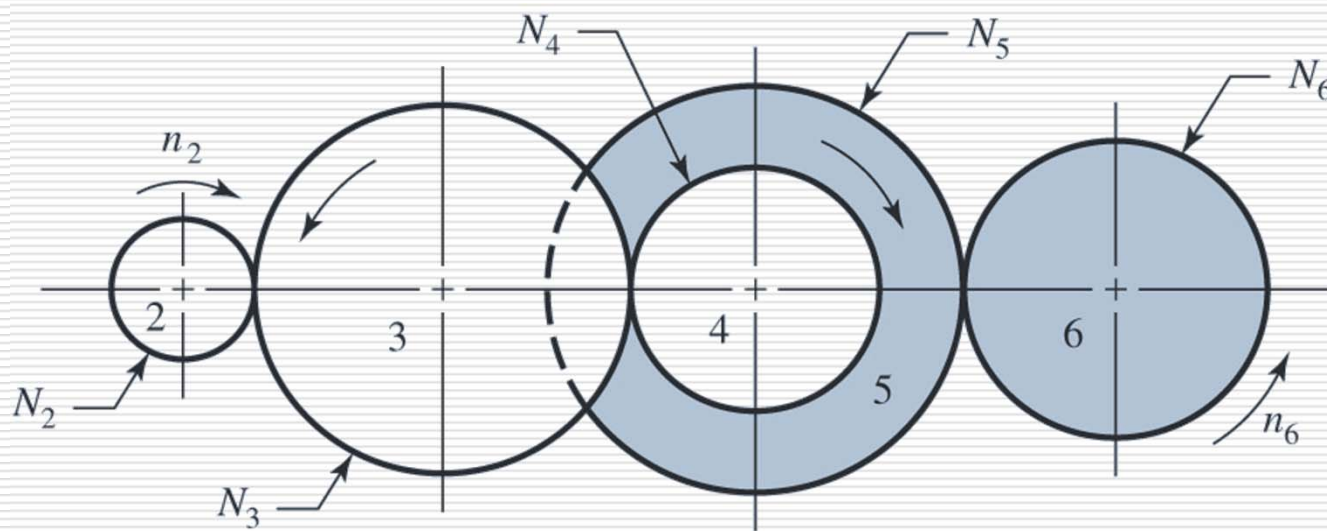
$N \equiv$  teeth

# Example



The three gears shown have a pitch of 3, a pressure angle of  $20^\circ$ . Gear  $a$  is the driving, or input, pinion. It rotates counterclockwise at 600-rpm and transmits 25-hp to the idler gear  $b$ . Output gear  $c$  is attached to a shaft that drives a machine. Nothing is attached to the idler shaft, and friction losses in the bearings and gears can be neglected. Determine the resultant load applied by the idler to its shaft.

# Gear Train: Train Value



$$e \equiv \text{Train Value} = \frac{\text{product of driving tooth numbers}}{\text{product of driven tooth numbers}}$$

# Example

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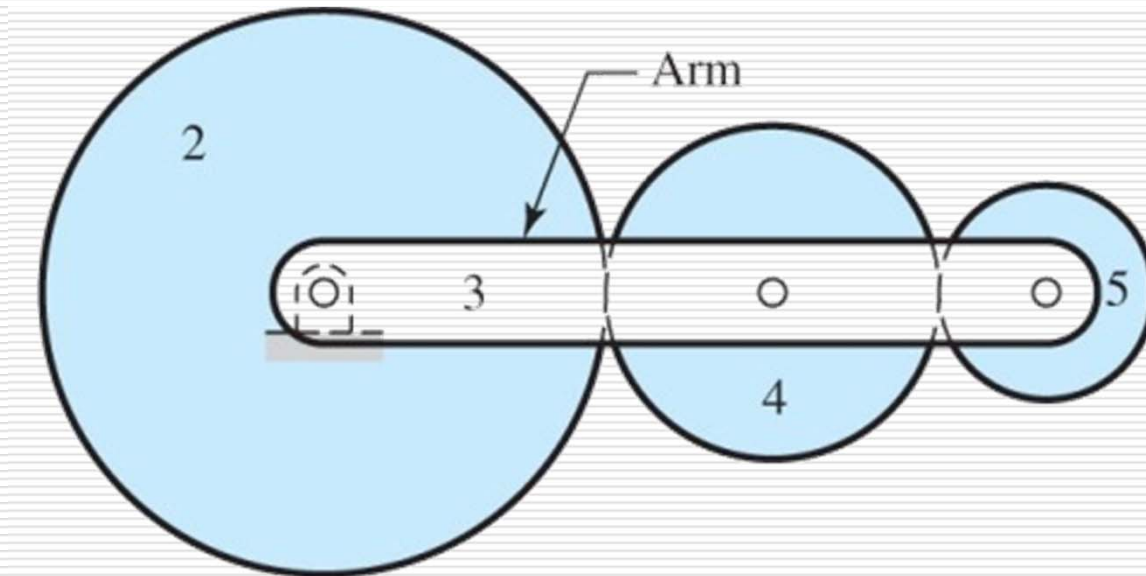
A gearset consists of a 16 tooth pinion driving a 40 tooth gear. The gears are cut using a pressure angle of  $20^\circ$

- a. Compute the addendum and dedendum
- b. Compute the circular pitch, the center distance, and the radii of the base circles
- c. In mounting these gears, the center distance was incorrectly made  $\frac{1}{4}$  in larger. Compute the new values of the pressure angle and the pitch-circle diameters.



# Gear Train on the Arm of a Planetary Gear Train

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# Planetary or Epicyclic Gear Train

