HOMEWORK SOLUTION
MER311: ADVANCED MECHANICS

PROB 5.33 PG 1 OF Y BUDYNAS 2ND

PROBLEM 5.33 IF BENDING IS ABOUT THE Z-AXIS FOR THE CROSS-SECTION GHOWN, DETERMINE THE LOCATION OF THE SHEAR CENTER FROM THE CENTER OF THE VERTICAL WALL. ALL DIMENSIONS ARE IN INCHES AND, WHERE APPROPRIATE, ARE FROM THE WALL CENTERS.

### GIYEN:

- 1 MOMENT ABOUT THE 2-AXIS
- Z. CROSS SECTION SHOWN

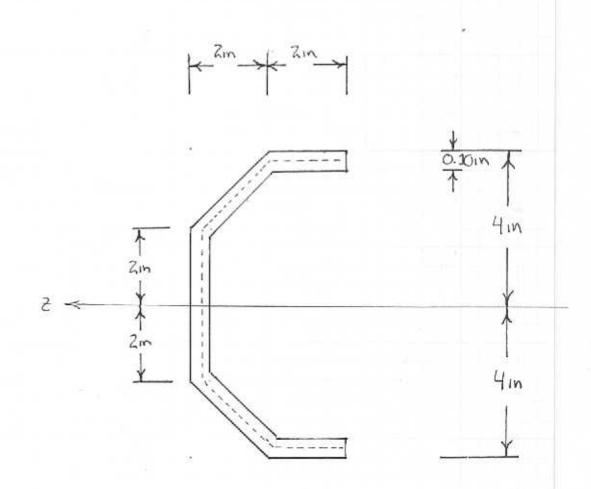
#### Assumptions:

- 1. SMALL DEFORMATIONS
- 2. LINEAR ELASTIC RESPONSE

### FIND:

1. LOCATION OF THE SHEAR CENTER.

### FIGURES:

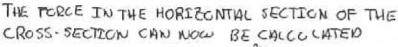


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PROB 5.33 PG 20F 4
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## SOLUTION:

IN THE HORIZONTAL SECTION



$$F_{4} = \int \mathcal{C}_{1} \cdot t \cdot ds = \int_{1}^{2m} \frac{4m \cdot \forall}{\pi} \cdot s \cdot (0.1m) ds$$

$$= \frac{\forall}{\mathbf{I}} \cdot (0.4m^{2}) \cdot \frac{s^{2}}{2} \int_{0}^{2m} = \frac{\forall}{\mathbf{I}} \cdot (0.2m^{2}) (2m)^{2} = \underbrace{0.8m^{4} \cdot \frac{\forall}{\mathbf{I}}}_{1} \quad (3)$$

IN THE DIAGONAL SECTION OF THE CROSS-SECTION

$$\frac{1}{1} = \frac{4}{1} = \frac{1}{1} \left[ \frac{1}{1} + \frac{1}{1} - \frac{1}{1} \cdot \frac{1}{1} + \frac{1}{1} \cdot \frac{1}{1} \cdot \frac{1}{1} \cdot \frac{1}{1} \right] + \frac{1}{1} \cdot \frac{1}{1} \cdot$$

THE FORCE GENERATED IN THE

DEAGONAL SECTION AS A RESULT OF THE SHEAR STRENS CAN NOW BE CALCULATED

$$F_{2} = \int 7 \cdot t \cdot ds = \frac{1}{2} (0.1 \text{ m}) \int [8 \text{ m}^{2} + 4 \text{ m} \cdot 5 - 0.3536 \cdot 5^{2}] ds$$

$$= \frac{1}{2} \cdot (0.1 \text{ m}) \left[ 8 \text{ m}^{2} (2.828 \text{ m}) + \frac{4 \text{ m}}{2} \cdot (2.828 \text{ m})^{2} - \frac{0.3536}{3} (2.828 \text{ m})^{3} \right]$$

$$= 3.595 \cdot 10^{4} \cdot \frac{1}{2} \quad (4)$$

IN THE HORIZONTAL SECTION OF THE CROSS-SECTION

-SECTION
$$Y_{3} = \frac{\forall Q}{\text{IE}}$$

$$= \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(2.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(2.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.828 \text{ in}) \cdot t\} = \frac{\forall \{(4_{1}n)(2_{1}n) \cdot t\}}{\{(4_{1}n)(2_{1}n) \cdot t\}} + (3.0 \text{ in})(3.8$$

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THE FORCE GENERATED IN THE HERTICAL LEG OF THE CROSS-SECTION CAN NOW BE CALCULATED.

$$F_{3} = \int \mathcal{L} \cdot t \cdot ds = \stackrel{?}{\pm} (0.1 \text{ in}) \int_{10.484 \text{ in}^{2}}^{2 \text{ in}} + 2 \text{ in} \cdot s - \frac{s^{2}}{2} \right] ds$$

$$= (0.1 \text{ in}) \stackrel{?}{\pm} \left[ 36.484 \text{ in}^{2} \cdot s + \frac{s^{2}}{2} s^{2} - \frac{s^{2}}{23} \right]^{2 \text{ in}} = (0.1 \text{ in}) \stackrel{?}{\pm} \cdot \left[ 16.484 \text{ in}^{2} \cdot 2 \text{ in} + 1 \text{ in} \cdot (2 \text{ in})^{2} - \frac{(2 \text{ in})^{2}}{2} \right]$$

$$= 3.563 \text{ in}^{4} \cdot \stackrel{?}{\pm} \qquad \boxed{6}$$

EQUATIONS (2), (4), AND (6) WILL BE USED IN THE CALCULATION OF THE SHELL CENTER AND EACH CONTAINS THE CROSS-SECTION MOMENT OF INGRITIR. THE CROSS-SECTION MOMENT OF INENTIA MUST NOW BE CALCULATED.

$$I = Z \cdot I_1 + 2 \cdot I_2 + I_3$$
  $(7)$ 

I1 = 1. (2in) (0.1m) + (2in) (0.1in) (4in)2 = 3.200 in 4

In = 17 (0.11m) (41m)3 = 0. 5333 m4

THE CALCULATION OF I3 = I322 STARTS WITH THE CALCULATION OF I32'2' AND I3x'x'

I 32'2 = 12. (0.1m)(2.828m)3 = 0.18848m4

I3XX = 12 (2.828in) (0.1m) = 0.000 2357in4

TRANSFORM ING THESE TO THE X-2 COCRDINATE SYSTEM USING MOHR'S CINCLE GIVES

$$I_{22} = 0.09436 \text{ in}^4 + (0.5 \text{ in})(2.828 \text{ in})(3 \text{ in})^2$$
  
= 2.6\$0 \text{in}^4 = I\_2

THE TOTAL MOMENT OF INERTIA FOR THIS CROSS-SECTION CAN NOW BE CALCULATED USING (7)

= 12, Z17 my

THE PORCES CAN NOW BE RE WRITTEN

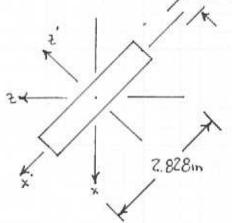
$$F_1 = \frac{0.8 \text{ in}^4}{12.212 \text{ m}^4} \cdot \forall = 0.06551 \cdot \forall$$

$$F_3 = \frac{3.563 \text{ in}^4}{12.212 \text{ m}^4} \cdot \forall = 0.2917 \cdot \forall$$

$$F_2 = \frac{3.595}{17.212} \cdot \text{m}^4 \cdot \text{V} = 0.2944 \cdot \text{V}$$

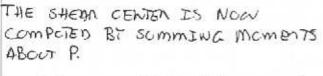
0.000236.4

0.09436in4



0. 12248114

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EMyen=0=2.(4in).(006551.∀) -2: (3in) (.7071) (0.2944-4) + 2. (1m) (.7c71) (0.2944.V) + C. ¥

e = 1.357m

# SUMMARY

THE PROBLEM STANTS WITHER THE DETERMINATION OF THE SHEAR STAESS DISTRIBUTION IN THE CROSS- SECTION. THE SHEAR STRESS IN EACH LEG IS THEN INTEGRATED TO DETERMINE THE FORCE IN THAT LEG. THE MOMENT OF INDITIA

IS CALCULATED BECAUSE IT APPEDANS IN EACH FORCE, BUT NOT IN THE SHEAR LOAD APPLIED TO THE OTHER END OF THE DIFFERENTIAL ELEMENT. FINDLEY MOMENTS ARE

SCHMED ABOUT P TO DETERMINE C.

