



Mecánica de los Sólidos 2019 Profesor Titular Daniel Millán JTP Eduardo Rodríguez

Tensor tensión de Cauchy

$$T^{(n)} = n \cdot \sigma, \qquad T_j^{(n)} = \sigma_{ij} n_i$$

$$(\boldsymbol{\sigma} - \lambda_i \boldsymbol{I}) \, \boldsymbol{n}_i = \boldsymbol{0}, \qquad |\boldsymbol{\sigma} - \lambda \boldsymbol{I}| = 0$$

$$\lambda^3 - I_1 \lambda^2 + I_2 \lambda - I_3 = 0$$

$$I_1 = \sigma_{kk}$$

$$I_2 = \frac{1}{2} (\sigma_{ii}\sigma_{jj} - \sigma_{ij}\sigma_{ji})$$

$$I_3 = \det(\sigma_{ij})$$

$$\sigma' = A\sigma A^T, \qquad \sigma'_{ij} = a_{im}a_{jn}\sigma_{mn}$$

Círculo de Mohr en tensión plana

$$\sigma_{x'} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta,
\sigma_{y'} = \frac{\sigma_x + \sigma_y}{2} - \frac{\sigma_x - \sigma_y}{2} \cos 2\theta - \tau_{xy} \sin 2\theta,
\tau_{x'y'} = - \frac{\sigma_x - \sigma_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta.$$

$$r = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}.$$

Relaciones tensión-deformación-temperatura

$$\frac{\partial \sigma_{ij}}{\partial x_i} = 0, \qquad \varepsilon_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right).$$

$$\sigma_{ij} = 2\mu\varepsilon_{ij} + \lambda\varepsilon_{kk}\delta_{ij} - \left(\lambda + \frac{2}{3}\mu\right)\alpha\Delta T\delta_{ij}$$

$$\varepsilon_{ij} = \frac{1+\nu}{E}\sigma_{ij} - \frac{\nu}{E}\sigma_{kk}\delta_{ij} + \alpha\Delta T\delta_{ij}$$

	E : módulo de Young $ u$: coeficiente de Poisson	K : módulo de compresibilidad G : módulo de rigidez	λ : 1.er coeficiente de Lamé μ : 2º coeficiente de Lamé
(E, ν)		$K = \frac{E}{3(1 - 2\nu)}$ $G = \frac{E}{2(1 + \nu)}$	$\lambda = rac{ u E}{(1+ u)(1-2 u)} onumber \ \mu = rac{E}{2(1+ u)}$
(K,G)	$E=rac{9KG}{3K+G} onumber $		$\lambda = K - \frac{2G}{3}$ $\mu = G$
(λ,μ)	$E = \frac{\mu(3\lambda + 2\mu)}{\lambda + \mu}$ $\nu = \frac{\lambda}{2(\lambda + \mu)}$	$K=\lambda+rac{2\mu}{3}$ $G=\mu$	

Tensión de Von Mises σ_{VM}

$$\sigma_{VM} = \frac{1}{2} \sqrt{(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2},$$

donde $\sigma_1, \sigma_2, \sigma_3$, son la tensiones principales.

Energía de deformación en cuerpos elásticos

$$U = \frac{1}{2} \int_{V} \boldsymbol{\sigma} : \boldsymbol{\varepsilon} \, dV.$$

Sistema lineal-elástico

$$\delta_i = \frac{\partial U}{\partial P_i}, \qquad y \qquad \phi_i = \frac{\partial U}{\partial M_i},$$

Estados planos en coordenadas cartesianas

$$\begin{split} \varepsilon_x &= \frac{1}{\widetilde{E}} (\sigma_x - \widetilde{\nu} \sigma_y), \qquad \sigma_x = \frac{\widetilde{E}}{1 - \widetilde{\nu}^2} (\varepsilon_x - \widetilde{\nu} \varepsilon_y), \\ \varepsilon_y &= \frac{1}{\widetilde{E}} (\sigma_y - \widetilde{\nu} \sigma_x), \qquad \sigma_y = \frac{\widetilde{E}}{1 - \widetilde{\nu}^2} (\varepsilon_y - \widetilde{\nu} \varepsilon_x), \end{split}$$

	Tensión plana	Deformación plana
$\widetilde{\nu}$	ν	$\frac{\nu}{1-\nu}$
\widetilde{E}	E	$\frac{E}{1- u^2}$
σ_z	0	$\frac{\nu E}{1 - \nu^2} (\varepsilon_x - \varepsilon_y)$
ε_z	$-\frac{\nu}{E}(\sigma_x + \sigma_y)$	0

Función de tensiones de Airy

$$\sigma_{xx} = \frac{\partial^2 \phi}{\partial y^2}, \quad \sigma_{yy} = \frac{\partial^2 \phi}{\partial x^2}, \quad \sigma_{xy} = -\frac{\partial^2 \phi}{\partial y \partial x}.$$

$$\nabla^4 \phi = \phi_{.1111} + 2\phi_{.1122} + \phi_{.2222} = 0$$

Estados planos en coordenadas polares

$$\begin{split} \sigma_{r,r} + \frac{1}{r} \tau_{r\theta,\theta} + \frac{\sigma_r - \sigma_\theta}{r} &= 0, \\ \frac{1}{r} \sigma_{\theta,\theta} + \tau_{r\theta,r} + \frac{2\tau_{r\theta}}{r} &= 0. \end{split}$$

$$\varepsilon_r = u_{,r}$$
 $\varepsilon_\theta = \frac{u}{r} + \frac{1}{r}v_{,\theta}$ $\gamma_{r\theta} = \frac{1}{r}u_{,\theta} + v_{,r} - \frac{v}{r}$

Estado plano de tensiones

$$\varepsilon_r = \frac{1}{E}(\sigma_r - \nu \sigma_\theta),$$

$$\varepsilon_\theta = \frac{1}{E}(\sigma_\theta - \nu \sigma_r),$$

$$\gamma_{r\theta} = \frac{1}{G}\tau_{r\theta}.$$

Distribuciones de tensión axisimétricas

$$\begin{split} \phi &= C_1 + C_2 \log r + C_3 r^2 + C_4 r^2 \log r, \\ \sigma_r &= \frac{1}{r} \phi_{,r} = \frac{C_2}{r^2} + 2C_3 + C_4 (2 \log r + 1), \\ \sigma_\theta &= \phi_{,rr} = -\frac{C_2}{r^2} + 2C_3 + C_4 (2 \log r + 3). \end{split}$$

Cilindro de pared gruesa sometido a presión uniforme ${\cal C}_4=0$

$$\sigma_r(r=a) = -p_i, \quad \sigma_r(r=b) = -p_e.$$

$$u = \frac{2(1-\nu)}{E}C_3r - \frac{(1+\nu)}{E}\frac{C_2}{r},$$

$$\sigma_r = \frac{p_ia^2 - p_eb^2}{b^2 - a^2} + \frac{a^2b^2(p_e - p_i)}{r^2(b^2 - a^2)},$$

$$\sigma_\theta = \frac{p_ia^2 - p_eb^2}{b^2 - a^2} - \frac{a^2b^2(p_e - p_i)}{r^2(b^2 - a^2)}.$$

Pequeños agujeros circulares en placas tensionadas

$$\sigma_r = \sigma_{\infty} \left[1 - \left(\frac{R}{r} \right)^2 \right], \quad \sigma_{\theta} = \sigma_{\infty} \left[1 + \left(\frac{R}{r} \right)^2 \right].$$

Discos rotantes, velocidad angular ω

$$\sigma_r = \frac{3+\nu}{8}\rho\,\omega^2 \left(a^2 + b^2 - \frac{a^2b^2}{r^2} - r^2\right),$$

$$\sigma_\theta = \frac{3+\nu}{8}\rho\,\omega^2 \left(a^2 + b^2 + \frac{a^2b^2}{r^2} - \frac{1+3\nu}{3+\nu}r^2\right).$$

Cilindros rotantes, velocidad angular ω

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$$\sigma_\theta = \frac{3+\nu}{8}\rho\,\omega^2 \left(a^2 + b^2 + \frac{a^2b^2}{r^2} - \frac{1+3\nu}{3+\nu}r^2\right)$$

$$u = r\varepsilon_\theta = \frac{r}{E} \left[\sigma_\theta - \nu(\sigma_r + \sigma_z)\right].$$

Deformación plana $\varepsilon_z = 0$

$$\sigma_z = \frac{3 - 2\nu}{4(1 - \nu)} \nu \rho \,\omega^2 \left(a^2 + b^2 - \frac{2r^2}{3 - 2\nu} \right).$$

Deformación plana generalizada $\varepsilon_z=cte$

$$\int_0^{2\pi} \int_a^b \sigma_z \, r \, dr \, d\theta = 0,$$

$$\varepsilon_z = -\frac{\nu\rho\omega^2}{2E}(a^2 + b^2),$$

$$\sigma_z = \frac{\nu\rho\omega^2}{4(1-\nu)}(a^2 + b^2 - 2r^2).$$

Discos rotantes de espesor variable, $h=cr^{-\beta},\,c$ y β constantes.

$$\phi = C_1 r^{q_1} + C_2 r^{q_2} - \frac{3+\nu}{8-(3+\nu)\beta} c \rho \omega^2 r^{3-\beta},$$

$$\sigma_r = \frac{C_1}{c} r^{q_1+\beta-1} + \frac{C_2}{c} r^{q_2+\beta-1} - \frac{(3+\nu)\rho \omega^2 r^2}{8-(3+\nu)\beta},$$

$$\sigma_\theta = \frac{C_1}{c} q_1 r^{q_1+\beta-1} + \frac{C_2}{c} q_2 r^{q_2+\beta-1} - \frac{(1+3\nu)\rho \omega^2 r^2}{8-(3+\nu)\beta}.$$

Discos delgados con temperatura no uniforme

$$\sigma_r = \alpha E \frac{1}{r^2} \left[\frac{r^2 - a^2}{b^2 - a^2} \int_a^b Tr \, dr - \int_a^r Tr \, dr \right],$$

$$\sigma_\theta = \alpha E \frac{1}{r^2} \left[\frac{r^2 + a^2}{b^2 - a^2} \int_a^b Tr \, dr + \int_a^r Tr \, dr - Tr^2 \right].$$

Cilindros largos con temperatura no uniforme

$$\begin{split} \sigma_r &= \frac{\alpha E}{1 - \nu} \frac{1}{r^2} \left[\frac{r^2 - a^2}{b^2 - a^2} \int_a^b Tr \, dr - \int_a^r Tr \, dr \right], \\ \sigma_\theta &= \frac{\alpha E}{1 - \nu} \frac{1}{r^2} \left[\frac{r^2 + a^2}{b^2 - a^2} \int_a^b Tr \, dr + \int_a^r Tr \, dr - Tr^2 \right], \\ u &= r \varepsilon_\theta = \frac{r}{E} \left[\sigma_\theta - \nu (\sigma_r + \sigma_z) \right] + r \alpha T. \end{split}$$

Extremo fijo, $\varepsilon = 0$

$$\sigma_z = \frac{\alpha E}{1-\nu} \left[\frac{2\nu}{b^2-a^2} \int_a^b Tr \, dr - T \right].$$

Extremo libre, $\varepsilon = cte$

$$\begin{split} \varepsilon_z &= \frac{2\alpha}{b^2 - a^2} \int_a^b Tr \, dr, \\ \sigma_z &= \frac{\alpha E}{1 - \nu} \left[\frac{2}{b^2 - a^2} \int_a^b Tr \, dr - T \right]. \end{split}$$

Torsión

Eje sólido circular

$$\begin{split} \sigma_x &= \sigma_y = \sigma_z = \tau_{rz} = \tau_{r\theta} = 0, \quad \tau_{\theta z} = G \gamma_{\theta z} = G r \frac{d\phi}{dz} \\ M_t &= \int_A r(\tau_{\theta z} \ dA) = G \frac{d\phi}{dz} \int_A r^2 \ dA = G \frac{d\phi}{dz} I_z, \\ \text{donde } I_z &= \int_A r^2 \ dA. \\ \frac{d\phi}{dz} &= \frac{M_t}{GI_z}, \quad \phi = \int_L \frac{M_t}{GI_z} dz = \frac{M_t L}{GI_z} \\ \tau_{\theta z} &= \frac{M_t \, r}{I_z} \end{split}$$

Eie hueco circular

$$I_z = \frac{\pi r_0^4}{2} \left(1 - \frac{r_i^4}{r_0^4} \right) = \frac{\pi d_0^4}{32} \left(1 - \frac{d_i^4}{d_0^4} \right)$$

Energía de deformación torsional

$$U = \frac{1}{2} \int_{V} \frac{1}{G} \left(\frac{M_t r}{I_z}\right)^2 dV = \frac{1}{2} \int_{L} \frac{M_t^2}{G I_z^2} dz \int_{A} r^2 dA$$
$$= \frac{1}{2} \int_{L} \frac{M_t^2}{G I_z} dz$$