

Chapter 7. Relative Motion and Rendezvous

WorkerInSpace

Hongseok Kim

Example 7.2

Problem Statement

A space station and spacecraft are in orbits with the following parameters

	Space station	Spacecraft
Perigee \times apogee(altitude)	300km circular	318.5×515.51 km
Period (computed using above data)	1.508 hr	1.548 hr
True anomaly, θ	60°	349.65°
Inclination, i	40°	40.130°
RA, Ω	20°	19.819°
Argument of perigee, ω	0° (arbitrary)	70.662°

Compute the total delta-v required for an eight-hour, two-impulse rendezvous trajectory.

Solution

We use the given data in Algorithm 4.1 to obtain the state vectors of the two spacecraft in the geocentric equatorial frame.

Space station:

$$\mathbf{r}_0 = 1622.39\hat{\mathbf{I}} + 5305.10\hat{\mathbf{J}} + 3717.44\hat{\mathbf{K}} \text{ (km)}$$

$$\mathbf{v}_0 = -7.29977\hat{\mathbf{I}} + 0.492357\hat{\mathbf{J}} + 2.48318\hat{\mathbf{K}} \text{ (km/s)}$$

Spacecraft:

$$\mathbf{r} = 1612.75\hat{\mathbf{I}} + 5310.19\hat{\mathbf{J}} + 3750.33\hat{\mathbf{K}} \text{ (km)}$$

$$\mathbf{v} = -7.35521\hat{\mathbf{I}} + 0.463856\hat{\mathbf{J}} + 2.46920\hat{\mathbf{K}} \text{ (km/s)}$$

The space station reference frame unit vectors (at this instant) are, by definition

$$\hat{\mathbf{i}} = \frac{\mathbf{r}_0}{|\mathbf{r}_0|} = 0.242945\hat{\mathbf{I}} + 0.794415\hat{\mathbf{J}} + 0.556670\hat{\mathbf{K}}$$

$$\hat{\mathbf{j}} = \frac{\mathbf{v}_0}{|\mathbf{v}_0|} = -0.944799\hat{\mathbf{I}} + 0.063725\hat{\mathbf{J}} + 0.321392\hat{\mathbf{K}}$$

$$\hat{\mathbf{k}} = \hat{\mathbf{i}} \times \hat{\mathbf{j}} = 0.219846\hat{\mathbf{I}} - 0.604023\hat{\mathbf{J}} + 0.766044\hat{\mathbf{K}}$$

Therefore, the transformation matrix from the geocentric equatorial frame into space station frame is (at this instant)

$$[Q]_{XX} = \begin{bmatrix} 0.242945 & 0.794415 & 0.556670 \\ -0.944799 & 0.063725 & 0.321394 \\ 0.219846 & -0.604023 & 0.766044 \end{bmatrix}$$

The position vector of the spacecraft relative to the space station (in the geocentric equatorial frame) is

$$\delta \mathbf{r} = \mathbf{r} - \mathbf{r}_0 = -9.63980\hat{\mathbf{I}} + 5.08240\hat{\mathbf{J}} + 32.8821\hat{\mathbf{K}} \text{ (km)}$$

The relative velocity is given by the formula

$$\mathbf{v} = \mathbf{v}_0 + \Omega_{\text{space station}} \times \mathbf{r}_{\text{rel}} + \mathbf{v}_{\text{rel}}$$

$$\mathbf{r}_{\text{rel}} = \delta \mathbf{r}, \mathbf{v}_{\text{rel}} = \delta \mathbf{v}$$

$$\delta \mathbf{v} = \mathbf{v} - \mathbf{v}_0 - \Omega_{\text{space station}} \times \delta \mathbf{r}$$

where $\Omega_{\text{space station}} = n\hat{\mathbf{k}}$ and n , the mean motion of the space station, is

$$n = \frac{v_0}{r_0} = \frac{7.72627}{6678} = 0.00115697 \text{ rad/s}$$

Thus,

$$\begin{aligned} \delta \mathbf{v} &= \mathbf{v} - \mathbf{v}_0 - \Omega_{\text{space station}} \times \delta \mathbf{r} = \mathbf{v} - \mathbf{v}_0 - n\hat{\mathbf{k}} \times \delta \mathbf{r} \\ &= -7.35521\hat{\mathbf{I}} + 0.463856\hat{\mathbf{J}} + 2.46920\hat{\mathbf{K}} - (-7.29977\hat{\mathbf{I}} + 0.492357\hat{\mathbf{J}} + 2.48318\hat{\mathbf{K}}) \\ &\quad - 0.00115697 \cdot (0.219846\hat{\mathbf{I}} - 0.604023\hat{\mathbf{J}} + 0.766044\hat{\mathbf{K}}) \times (9.63980\hat{\mathbf{I}} + 5.08240\hat{\mathbf{J}} + 32.8821\hat{\mathbf{K}}) \\ &= -0.024854\hat{\mathbf{I}} - 0.01159370\hat{\mathbf{J}} - 0.00853577\hat{\mathbf{K}} \text{ (km/s)} \end{aligned}$$

In space station coordinates, the relative position vector $\delta \mathbf{r}_0$ at the beginning of the rendezvous maneuver is

$$\begin{aligned} [\delta \mathbf{r}_0] &= [Q]_{XX} \delta \mathbf{r} = \begin{bmatrix} 0.242945 & 0.794415 & 0.556670 \\ -0.944799 & 0.063725 & 0.321394 \\ 0.219846 & -0.604023 & 0.766044 \end{bmatrix} \begin{bmatrix} -9.63980 \\ 5.08240 \\ 32.8821 \end{bmatrix} \\ &= \begin{bmatrix} 20 \\ 20 \\ 20 \end{bmatrix} \text{ (km)} \end{aligned}$$

Likewise, the relative velocity $\delta \mathbf{v}_0^-$ just before launch into the rendezvous trajectory is

$$\begin{aligned} [\delta \mathbf{v}_0^-] &= [\mathbf{Q}]_{\text{xx}}[\delta \mathbf{v}] = \begin{bmatrix} 0.242945 & 0.794415 & 0.556670 \\ -0.944799 & 0.063725 & 0.321394 \\ 0.219846 & -0.604023 & 0.766044 \end{bmatrix} \begin{bmatrix} -0.024854 \\ -0.0115937 \\ -0.00853577 \end{bmatrix} \\ &= \begin{bmatrix} -0.02000 \\ 0.02000 \\ -0.005000 \end{bmatrix} (\text{km/s}) \end{aligned}$$

The Clohessy-Wiltshire matrices, for $t = t_f = 8\text{hr} = 28800\text{s}$ and $n = 0.00115697\text{rad/s}$, are

$$[\delta \mathbf{r}(t)] = [\Phi_{\text{rr}}(t)][\delta \mathbf{r}_0] + [\Phi_{\text{rv}}(t)][\delta \mathbf{v}_0]$$

$$[\delta \mathbf{v}(t)] = [\Phi_{\text{vr}}(t)][\delta \mathbf{r}_0] + [\Phi_{\text{vv}}(t)][\delta \mathbf{v}_0]$$

$$\begin{aligned} [\Phi_{\text{rr}}(t)] &= \begin{bmatrix} 4 - 3\cos nt & 0 & 0 \\ 6(\sin nt - nt) & 1 & 0 \\ 0 & 0 & \cos nt \end{bmatrix} = \begin{bmatrix} 4.98383 & 0 & 0 \\ -194.257 & 1 & 0 \\ 0 & 0 & -0.327942 \end{bmatrix} \\ [\Phi_{\text{rv}}(t)] &= \begin{bmatrix} \frac{\sin nt}{n} & \frac{2}{n}(1 - \cos nt) & 0 \\ \frac{2}{n}(\cos nt - 1) & \frac{4}{n}\sin nt - 3t & 0 \\ 0 & 0 & \frac{1}{n}\sin nt \end{bmatrix} = \begin{bmatrix} 816.525 & 2295.54 & 0 \\ -2205.54 & -83133.9 & 0 \\ 0 & 0 & 816.525 \end{bmatrix} \\ [\Phi_{\text{vr}}(t)] &= \begin{bmatrix} 3n \sin nt & 0 & 0 \\ 6n(\cos nt - 1) & 0 & 0 \\ 0 & 0 & -n \sin nt \end{bmatrix} = \begin{bmatrix} 0.00327897 & 0 & 0 \\ -0.00921837 & 0 & 0 \\ 0 & 0 & -0.00109299 \end{bmatrix} \\ [\Phi_{\text{vv}}(t)] &= \begin{bmatrix} \cos nt & 2 \sin nt & 0 \\ -2 \sin nt & 4 \cos nt - 3 & 0 \\ 0 & 0 & \cos nt \end{bmatrix} = \begin{bmatrix} -0.327942 & 1.88940 & 0 \\ -1.88940 & -4.31177 & 0 \\ 0 & 0 & -0.327942 \end{bmatrix} \end{aligned}$$

From equation $[\delta \mathbf{v}_0^+] = -[\Phi_{\text{rv}}(t_f)]^{-1}[\Phi_{\text{rr}}(t_f)][\delta \mathbf{r}_0]$, we find $\delta \mathbf{v}_0^+$

$$\begin{aligned} \begin{bmatrix} \delta u_0^+ \\ \delta v_0^+ \\ \delta w_0^+ \end{bmatrix} &= -\begin{bmatrix} 816.525 & 2295.54 & 0 \\ -2205.54 & -83133.9 & 0 \\ 0 & 0 & 816.525 \end{bmatrix}^{-1} \begin{bmatrix} 4.98383 & 0 & 0 \\ -194.257 & 1 & 0 \\ 0 & 0 & -0.327942 \end{bmatrix} \begin{bmatrix} 20 \\ 20 \\ 20 \end{bmatrix} \\ &= -\begin{bmatrix} 816.525 & 2295.54 & 0 \\ -2205.54 & -83133.9 & 0 \\ 0 & 0 & 816.525 \end{bmatrix}^{-1} \begin{bmatrix} 99.6765 \\ -3865.14 \\ -6.55884 \end{bmatrix} \\ &= \begin{bmatrix} 0.00936084 \\ -0.0467514 \\ 0.00803263 \end{bmatrix} (\text{km/s}) \end{aligned}$$

From equation $[\delta \mathbf{v}_f^-] = [\Phi_{vr}(t_f)][\delta \mathbf{r}_0] + [\Phi_{vv}(t_f)][\delta \mathbf{v}_0^+]$

$$\begin{bmatrix} \delta u_f^- \\ \delta v_f^- \\ \delta w_f^- \end{bmatrix} = \begin{bmatrix} 0.00327897 & 0 & 0 \\ -0.00921837 & 0 & 0 \\ 0 & 0 & -0.00109299 \end{bmatrix} \begin{bmatrix} 20 \\ 20 \\ 20 \end{bmatrix} + \begin{bmatrix} -0.327942 & 1.88940 & 0 \\ -1.88940 & -4.31177 & 0 \\ 0 & 0 & -0.327942 \end{bmatrix} \begin{bmatrix} 0.00936084 \\ -0.0467514 \\ 0.00803263 \end{bmatrix}$$

$$= \begin{bmatrix} -0.2528223 \\ -0.000472444 \\ -0.0222449 \end{bmatrix} (\text{km/s})$$

Delta-v at the beginning of the rendezvous maneuver is found as

$$[\Delta \mathbf{v}_0] = [\delta \mathbf{v}_0^+] - [\delta \mathbf{v}_0^-] = \begin{bmatrix} 0.00936084 \\ -0.0467514 \\ 0.00803263 \end{bmatrix} - \begin{bmatrix} -0.02000 \\ 0.02000 \\ -0.005000 \end{bmatrix} = \begin{bmatrix} 0.0293608 \\ -0.0667514 \\ 0.0130326 \end{bmatrix}$$

Delta-v at the conclusion of the maneuver is

$$[\Delta \mathbf{v}_f] = [\delta \mathbf{v}_f^+] - [\delta \mathbf{v}_f^-] = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} - \begin{bmatrix} -0.2528223 \\ -0.000472444 \\ -0.0222449 \end{bmatrix} = \begin{bmatrix} 0.2528223 \\ 0.000472444 \\ 0.0222449 \end{bmatrix} (\text{km/s})$$

The total delta-v requirement is

$$\Delta v_{\text{total}} = |\Delta \mathbf{v}_0| + |\Delta \mathbf{v}_f| = 0.0740787 + 0.03559465 = 0.109673 \text{ km/s} = 109.7 \text{ m/s}$$

From equation $[\delta \mathbf{r}(t)] = [\Phi_{rr}(t)][\delta \mathbf{r}_0] + [\Phi_{rv}(t)][\delta \mathbf{v}_0]$, we have, for $0 < t < t_f$,

$$\begin{bmatrix} \delta x(t) \\ \delta y(t) \\ \delta z(t) \end{bmatrix} = \begin{bmatrix} 4 - 3\cos nt & 0 & 0 \\ 6(\sin nt - nt) & 1 & 0 \\ 0 & 0 & \cos nt \end{bmatrix} \begin{bmatrix} 20 \\ 20 \\ 20 \end{bmatrix} + \begin{bmatrix} \frac{\sin nt}{n} & \frac{2}{n}(1 - \cos nt) & 0 \\ \frac{2}{n}(\cos nt - 1) & \frac{4}{n}\sin nt - 3t & 0 \\ 0 & 0 & \frac{1}{n}\sin nt \end{bmatrix} \begin{bmatrix} 0.00936084 \\ -0.0467514 \\ 0.00803263 \end{bmatrix}$$

Substituting $n = 0.00115697 \text{ rad/s}$, we obtain the relative position vector as a function of time.

Example 7.3

Problem statement

A target and a chase vehicle are in the same 300km circular earth orbit. The chaser is 2km behind the target when the chaser initiates a two-impulse rendezvous maneuver so as to rendezvous with the target in 1.49 hours. Find the total delta-v requirement.

Solution:

For the circular orbit

$$v = \sqrt{\frac{\mu}{r}} = \sqrt{\frac{398600}{6378 + 300}} = 7.726 \text{ km/s}$$

So that the mean motion is

$$n = \frac{v}{r} = \frac{7.726}{6678} = 0.0011569 \text{ rad/s}$$

For this mean motion and the rendezvous trajectory time $t = 1.49 \text{ hr} = 5364 \text{ s}$, the Clohessy-Wiltshire matrices are

$$\begin{aligned} [\Phi_{rr}(t)] &= \begin{bmatrix} 4 - 3\cos nt & 0 & 0 \\ 6(\sin nt - nt) & 1 & 0 \\ 0 & 0 & \cos nt \end{bmatrix} = \begin{bmatrix} 1.0090 & 0 & 0 \\ -37.699 & 1 & 0 \\ 0 & 0 & 0.99700 \end{bmatrix} \\ [\Phi_{rv}(t)] &= \begin{bmatrix} \frac{\sin nt}{n} & \frac{2}{n}(1 - \cos nt) & 0 \\ \frac{2}{n}(\cos nt - 1) & \frac{4}{n}\sin nt - 3t & 0 \\ 0 & 0 & \frac{1}{n}\sin nt \end{bmatrix} = \begin{bmatrix} -66.946 & 5.1928 & 0 \\ -5.1928 & -16360 & 0 \\ 0 & 0 & -66.946 \end{bmatrix} \\ [\Phi_{vr}(t)] &= \begin{bmatrix} 3n \sin nt & 0 & 0 \\ 6n(\cos nt - 1) & 0 & 0 \\ 0 & 0 & -n \sin nt \end{bmatrix} = \begin{bmatrix} -2.6881 \times 10^{-4} & 0 & 0 \\ -2.0851 \times 10^{-5} & 0 & 0 \\ 0 & 0 & 8.9603 \times 10^{-5} \end{bmatrix} \\ [\Phi_{vv}(t)] &= \begin{bmatrix} \cos nt & 2 \sin nt & 0 \\ -2 \sin nt & 4 \cos nt - 3 & 0 \\ 0 & 0 & \cos nt \end{bmatrix} = \begin{bmatrix} 0.99700 & -0.15490 & 0 \\ 0.15490 & 0.98798 & 0 \\ 0 & 0 & 0.99700 \end{bmatrix} \end{aligned}$$

The initial and final positions of the chaser in the CW frame are

$$[\delta \mathbf{r}_0] = \begin{bmatrix} 0 \\ -2 \\ 0 \end{bmatrix} (\text{km}) \quad [\delta \mathbf{r}_f] = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

Thus, solving the first CW equation, $[\delta \mathbf{r}_f] = [\Phi_{rr}(t_f)][\delta \mathbf{r}_0] + [\Phi_{rv}(t_f)][\delta \mathbf{v}_0^+]$, for $[\delta \mathbf{v}_0^+]$, we get

$$\begin{aligned} [\delta \mathbf{v}_0^+] &= - \begin{bmatrix} -66.946 & 5.1928 & 0 \\ -5.1928 & -16360 & 0 \\ 0 & 0 & -66.946 \end{bmatrix}^{-1} \begin{bmatrix} 1.0090 & 0 & 0 \\ -37.699 & 1 & 0 \\ 0 & 0 & 0.99700 \end{bmatrix} \begin{bmatrix} 0 \\ -2 \\ 0 \end{bmatrix} \\ &= \begin{bmatrix} -9.4824 \times 10^{-6} \\ -1.2225 \times 10^{-4} \\ 0 \end{bmatrix} (\text{km/s}) \end{aligned}$$

Therefore, the second CW equation, $[\delta \mathbf{v}_f^-] = [\Phi_{vr}(t)][\delta \mathbf{r}_0] + [\Phi_{vv}(t)][\delta \mathbf{v}_0^+]$

$$\begin{aligned} [\delta \mathbf{v}_f^-] &= \begin{bmatrix} -2.6881 \times 10^{-4} & 0 & 0 \\ -2.0851 \times 10^{-5} & 0 & 0 \\ 0 & 0 & 8.9603 \times 10^{-5} \end{bmatrix} \begin{bmatrix} 0 \\ -2 \\ 0 \end{bmatrix} + \begin{bmatrix} 0.99700 & -0.15490 & 0 \\ 0.15490 & 0.98798 & 0 \\ 0 & 0 & 0.99700 \end{bmatrix} \begin{bmatrix} -9.4824 \times 10^{-6} \\ -1.2225 \times 10^{-4} \\ 0 \end{bmatrix} \\ &= \begin{bmatrix} -2.839 \times 10^{-5} \\ 1.1193 \times 10^{-4} \\ 0 \end{bmatrix} (\text{km/s}) \end{aligned}$$

Since the chaser is in the same circular orbit as the target, its relative velocity is initially zero, i.e., $[\delta \mathbf{v}_0^-] = [0]$. Thus,

$$[\Delta \mathbf{v}_0] = [\delta \mathbf{v}_0^+] - [\delta \mathbf{v}_0^-] = \begin{bmatrix} -9.4824 \times 10^{-6} \\ -1.2225 \times 10^{-4} \\ 0 \end{bmatrix} - \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} -9.4824 \times 10^{-6} \\ -1.2225 \times 10^{-4} \\ 0 \end{bmatrix} (\text{km/s})$$

Which implies

$$|\Delta \mathbf{v}_0| = 0.1226 \text{ m/s}$$

At the end of the rendezvous maneuver, $[\delta \mathbf{v}_f^+] = [0]$, so that

$$[\Delta \mathbf{v}_f] = [\delta \mathbf{v}_f^+] - [\delta \mathbf{v}_f^-] = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} - \begin{bmatrix} -2.839 \times 10^{-5} \\ 1.1193 \times 10^{-4} \\ 0 \end{bmatrix} = \begin{bmatrix} 2.839 \times 10^{-5} \\ -1.1193 \times 10^{-4} \\ 0 \end{bmatrix} (\text{km/s})$$

Therefore,

$$|\Delta \mathbf{v}_f| = 0.1226 m/s$$

The total delta-v required is

$$\Delta v_{\text{total}} = |\Delta \mathbf{v}_0| + |\Delta \mathbf{v}_f| = 0.2452 m/s$$

Observe that in this case the motion takes place entirely in the plane of the target orbit. There is no motion normal to the plane (in the z direction). The coplanar rendezvous trajectory relative to the CW frame is sketched.