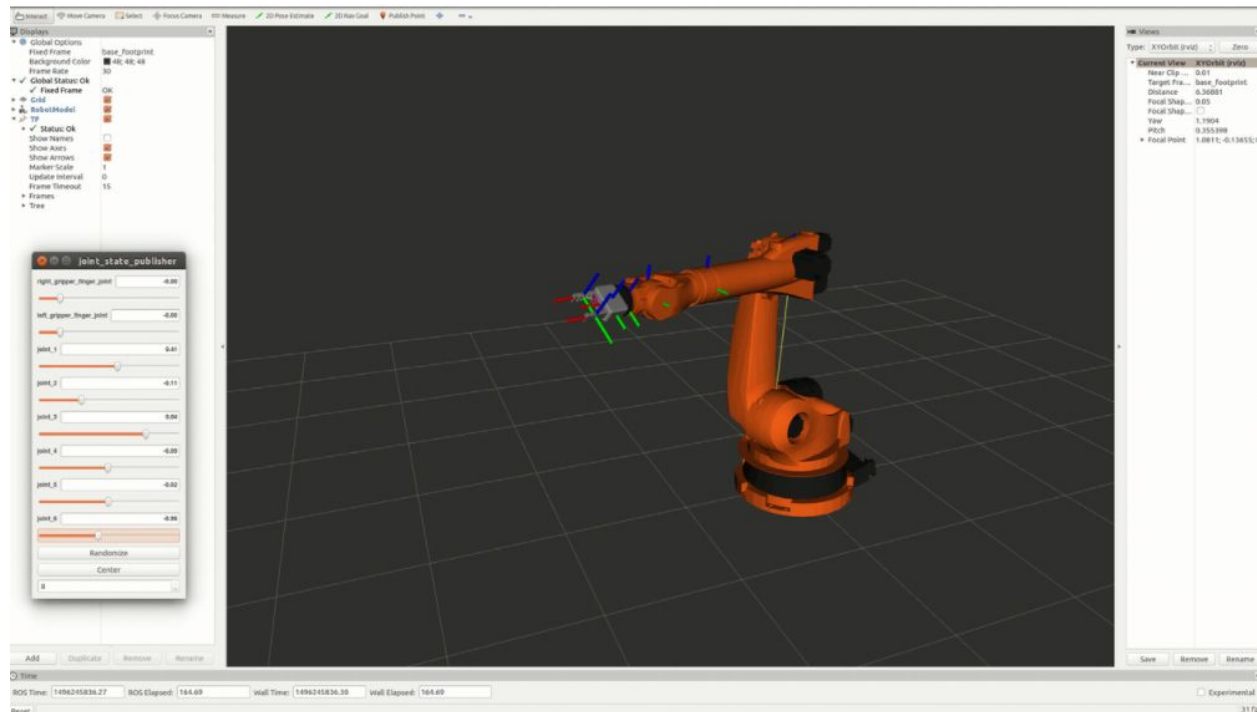


# Kinematic Analysis:

## Kuka KR210 six degree of freedom serial manipulator



## Modified DH-Parameters:

By reading kr210.urdf.xacro files, we could derive its DH parameters as shown in Figure 1. The DH parameters are defined as follows:

- $\alpha_{i-1}$  (twist angle) = angle between  $\hat{Z}_{i-1}$  and  $\hat{Z}_i$  measured about  $\hat{X}_{i-1}$  in a right-hand sense.
- $a_{i-1}$  (link length) = distance from  $\hat{Z}_{i-1}$  to  $\hat{Z}_i$  measured along  $\hat{X}_{i-1}$  where  $\hat{X}_{i-1}$  is perpendicular to both  $\hat{Z}_{i-1}$  to  $\hat{Z}_i$
- $d_i$  (link offset) = signed distance from  $\hat{X}_{i-1}$  to  $\hat{X}_i$  measured along  $\hat{Z}_i$ . Note that this quantity will be a variable in the case of prismatic joints.
- $\theta_i$  (joint angle) = angle between  $\hat{X}_{i-1}$  to  $\hat{X}_i$  measured about  $\hat{Z}_i$  in a right-hand sense. Note that this quantity will be a variable in the case of a revolute joint.

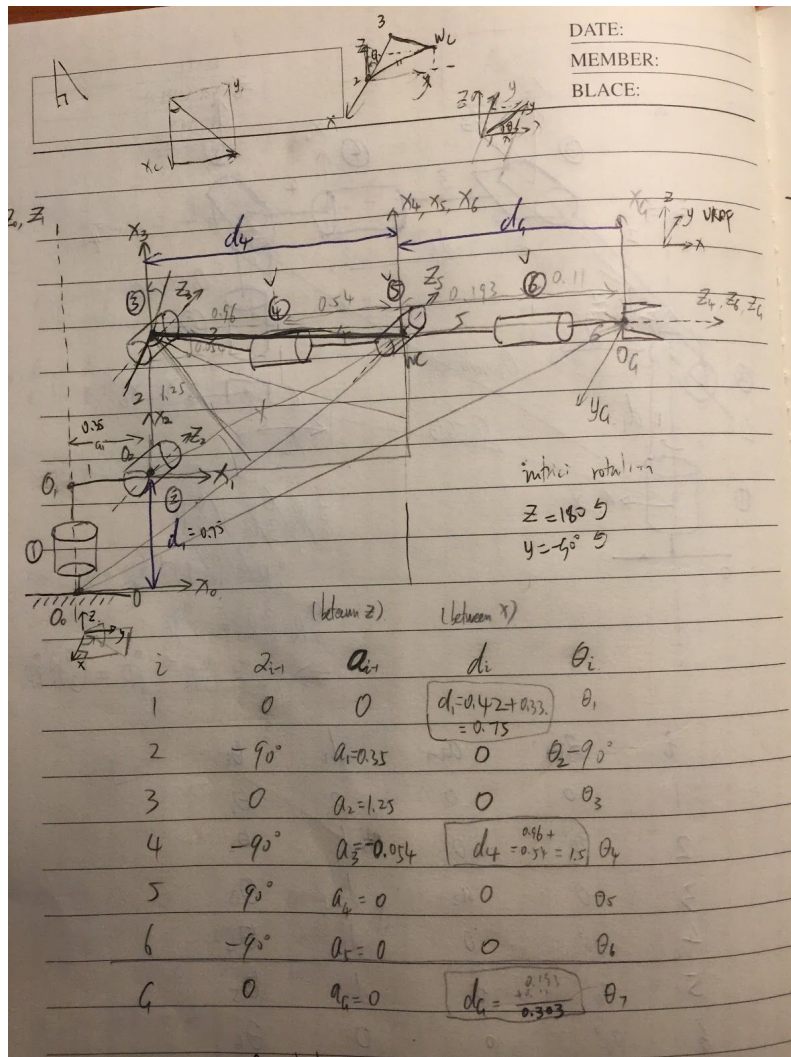


Figure 1. Robot links assignments, joint rotations, and DH parameters table.

## Individual Transformation Matrices About Each Joint

The transformation matrix from frame  $i-1$  to frame  $i$  is given by equation,

$${}^{i-1}_i T = R(x_{i-1}, \alpha_{i-1}) T(x_{i-1}, a_{i-1}) R(z_i, \theta_i) T(z_i, d_i)$$

This individual homogeneous transformation matrix means that we first rotate about  $x[i-1]$  by  $\alpha[i-1]$ . Then, translate along  $x[i-1]$  by  $a[i-1]$ . Next, rotate about resulting axis  $z[i]$  by  $\theta[i]$ . Finally, translate along axis  $z[i]$  by  $d[i]$ . We will use sympy to write out the symbolic transformation matrices about each joint using the DH table shown in Figure 1 and total homogeneous transformation matrix from base\_link to gripper\_linker. The symbolic transform matrix for individual frame is given by,

$${}^{i-1}T_i = \begin{bmatrix} c\theta_i & -s\theta_i & 0 & a_{i-1} \\ s\theta_i c\alpha_{i-1} & c\theta_i c\alpha_{i-1} & -s\alpha_{i-1} & -s\alpha_{i-1}d_i \\ s\theta_i s\alpha_{i-1} & c\theta_i s\alpha_{i-1} & c\alpha_{i-1} & c\alpha_{i-1}d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Therefore, by plugging in corresponding DH parameters, we can get individual transformation matrix as follows:

```
('T0_1 is', Matrix([
[cos(q1), -sin(q1), 0, 0],
[sin(q1), cos(q1), 0, 0],
[0, 0, 1, 0.75],
[0, 0, 0, 1]]))
('T1_2 is', Matrix([
[cos(q2 - 0.5*pi), -sin(q2 - 0.5*pi), 0, 0.35],
[0, 0, 1, 0],
[-sin(q2 - 0.5*pi), -cos(q2 - 0.5*pi), 0, 0],
[0, 0, 0, 1]]))
('T2_3 is', Matrix([
[cos(q3), -sin(q3), 0, 1.25],
[sin(q3), cos(q3), 0, 0],
[0, 0, 1, 0],
[0, 0, 0, 1]]))
('T3_4 is', Matrix([
[cos(q4), -sin(q4), 0, -0.054],
[0, 0, 1, 1.5],
[-sin(q4), -cos(q4), 0, 0],
[0, 0, 0, 1]]))
('T4_5 is', Matrix([
[cos(q5), -sin(q5), 0, 0],
[0, 0, -1, 0],
[sin(q5), cos(q5), 0, 0],
[0, 0, 0, 1]]))
('T5_6 is', Matrix([
[cos(q6), -sin(q6), 0, 0],
[0, 0, 1, 0],
[-sin(q6), -cos(q6), 0, 0],
[0, 0, 0, 1]]))
('T6_EE is', Matrix([
[1, 0, 0, 0],
[0, 1, 0, 0],
[0, 0, 1, 0.303],
[0, 0, 0, 1]]))
('R3_6 is', Matrix([
[-sin(q4)*sin(q6) + cos(q4)*cos(q5)*cos(q6), -sin(q4)*cos(q6) - sin(q6)*cos(q4)*cos(q5), -sin(q5)*cos(q4)],
[ sin(q5)*cos(q6), -sin(q5)*sin(q6), cos(q5)],
[-sin(q4)*cos(q5)*cos(q6) - sin(q6)*cos(q4), sin(q4)*sin(q6)*cos(q5) - cos(q4)*cos(q6), sin(q4)*sin(q5)]])
```

Figure 2: Individual transformation matrix.

In Figure 2, I also include the rotation matrix from joint 3 to joint 6. It will be easy for us to calculate theta4, theta5 and theta6 later on.

The total transformation matrix from base\_link to gripper\_linker is given by:

$$L0\_EE = L0\_1 * L1\_2 * L2\_3 * L3\_4 * L4\_5 * L5\_6 * L6\_EE$$

By plugging in these individual transformation matrix, we can get L0\_EE to be,

$${}^0\mathbf{r}_{WC/0} = {}^0\mathbf{r}_{EE/0} - d \cdot {}^0_6R \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} p_x \\ p_y \\ p_z \end{bmatrix} - d \cdot {}^0_6R \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

From the DH table,  $d$  is  $d_7 = 0.303$ . The end effector position  $[p_x, p_y, p_z]$  is given because it is inverse kinematics problem. We also know the roll, pitch, yaw angle from the base\_link with respect to end effector. The roll, pitch, yaw are extrinsic rotations, so we can build the transformation matrix from the base\_link to end effector. However, we need to pay attention to the difference between the gripper reference frame as defined in the URDF versus the DH parameters, so we have to perform a 180 degree counterclockwise rotation about gripper frame  $z$  axis and then a 90 degree clockwise rotation about the gripper frame  $y$  axis to form the right  $R_{0_6}$  matrix. The error\_rotation matrix performance is shown in Figure 4.

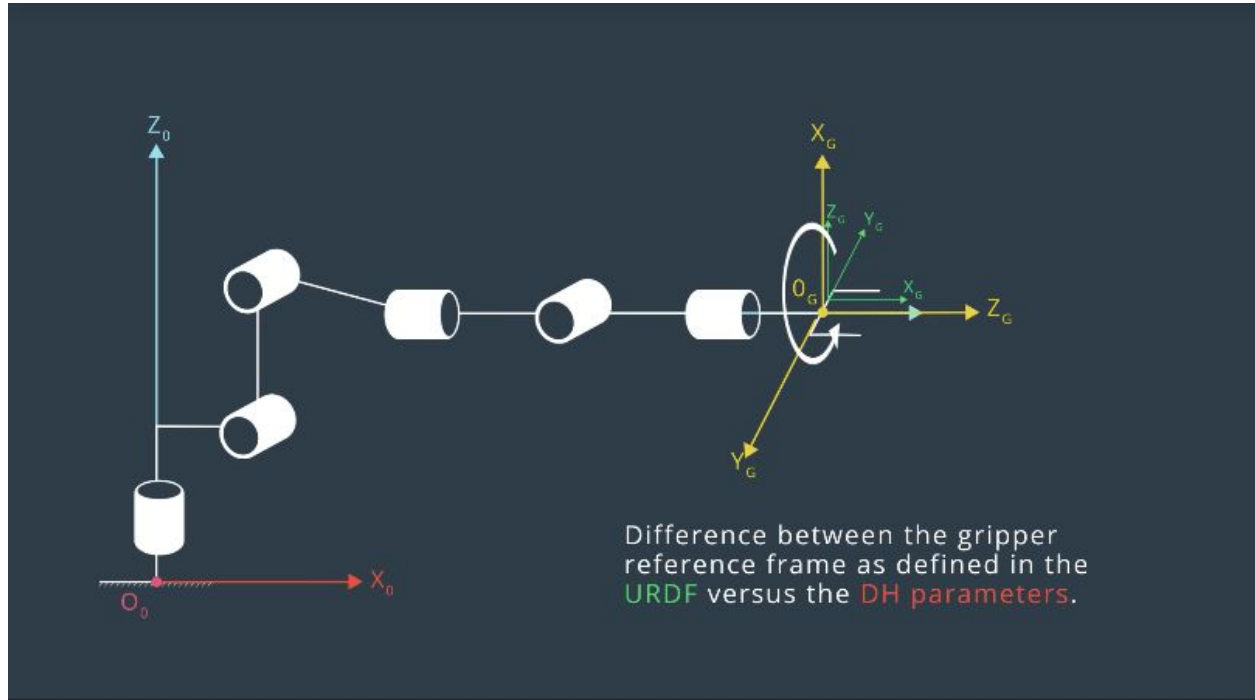


Figure 4: Error correction matrix rotation

Therefore, we first define the roll, pitch, yaw rotation matrix, then do extrinsic rotations wrt base\_link frame. Finally, multiply the extrinsic rotation matrix by the error correction matrix. The procedure is shown in Figure 5.

```
RotRoll_x = Matrix([[1, 0, 0],
                    [0, cos(R), -sin(R)],
                    [0, sin(R), cos(R)]]);
RotPitch_y = Matrix([[cos(P), 0, sin(P)],
                     [0, 1, 0],
                     [-sin(P), 0, cos(P)]]);
RotYaw_z = Matrix([[cos(Y), -sin(Y), 0],
                   [sin(Y), cos(Y), 0],
                   [0, 0, 1]]);
Rot_EE = RotYaw_z * RotPitch_y * RotRoll_x;
Rot_Error = RotYaw_z.subs(Y, radians(180)) * RotPitch_y.subs(P, radians(-90));
Rot_EE = Rot_EE * Rot_Error;
```

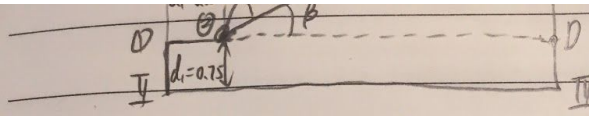
Plug the  $Rot\_EE$ , Euler angles into the above equations, we can find the wrist center position.



The diagram illustrates the projection of a point from a 3D coordinate system onto a 2D plane. The top part shows a 3D coordinate system with axes \$x\$, \$y'\$, and \$z\$. A point is located at coordinates \$(w\_x, w\_y, w\_z)\$, labeled as WC IV. This point is projected onto the \$xy\$-plane (labeled I II III IV) along the \$z\$-axis. The projection is shown as a dashed line. Below the 3D diagram, a double arrow points down to a 2D representation of the \$xy\$-plane. In this 2D view, the point is projected onto the \$x\$-axis at a distance \$a\_i = 0.65\$ from the origin. The \$y\$-coordinate is indicated by a dashed line to the right axis. Other labels include \$A\$, \$B\$, \$C\$, \$E\$, and \$D\$.

The procedures for solving  $\theta_1$ ,  $\theta_2$ ,  $\theta_3$  is shown in Figure 6 and Figure 7.  $\theta_3$  is the trickiest angle to solve. Remember  $\theta_3$  is the angle between  $X_2$  and  $X_3$  measured about

Z3 in a right-hand sense. The direction is negative based on the picture we drew.



After we found wrist center coordinate  $(W_x, W_y, W_z)$ , we can calculate  $\theta_1$ ,  $\theta_2$ , and  $\theta_3$ . First, find the length of A, B, C as follows.

$A = 1.501$ ,  $C = 1.25$  (from DH table).

$$B = \sqrt{(\sqrt{W_x^2 + W_y^2} - 0.135)^2 + (W_z - d_1 = 0.75)^2}$$

Then, by using cos Law, we can get.

$$\alpha = \cos^{-1} \left( \frac{B^2 + C^2 - A^2}{2BC} \right)$$

$$\beta = \cos^{-1} \left( \frac{A^2 + C^2 - B^2}{2AC} \right) \Rightarrow \theta_2 = 90^\circ - \alpha - \beta$$

$$\gamma = \cos^{-1} \left( \frac{A^2 + B^2 - C^2}{2AB} \right)$$

Figure 6: Solving first three joints angles part 1.

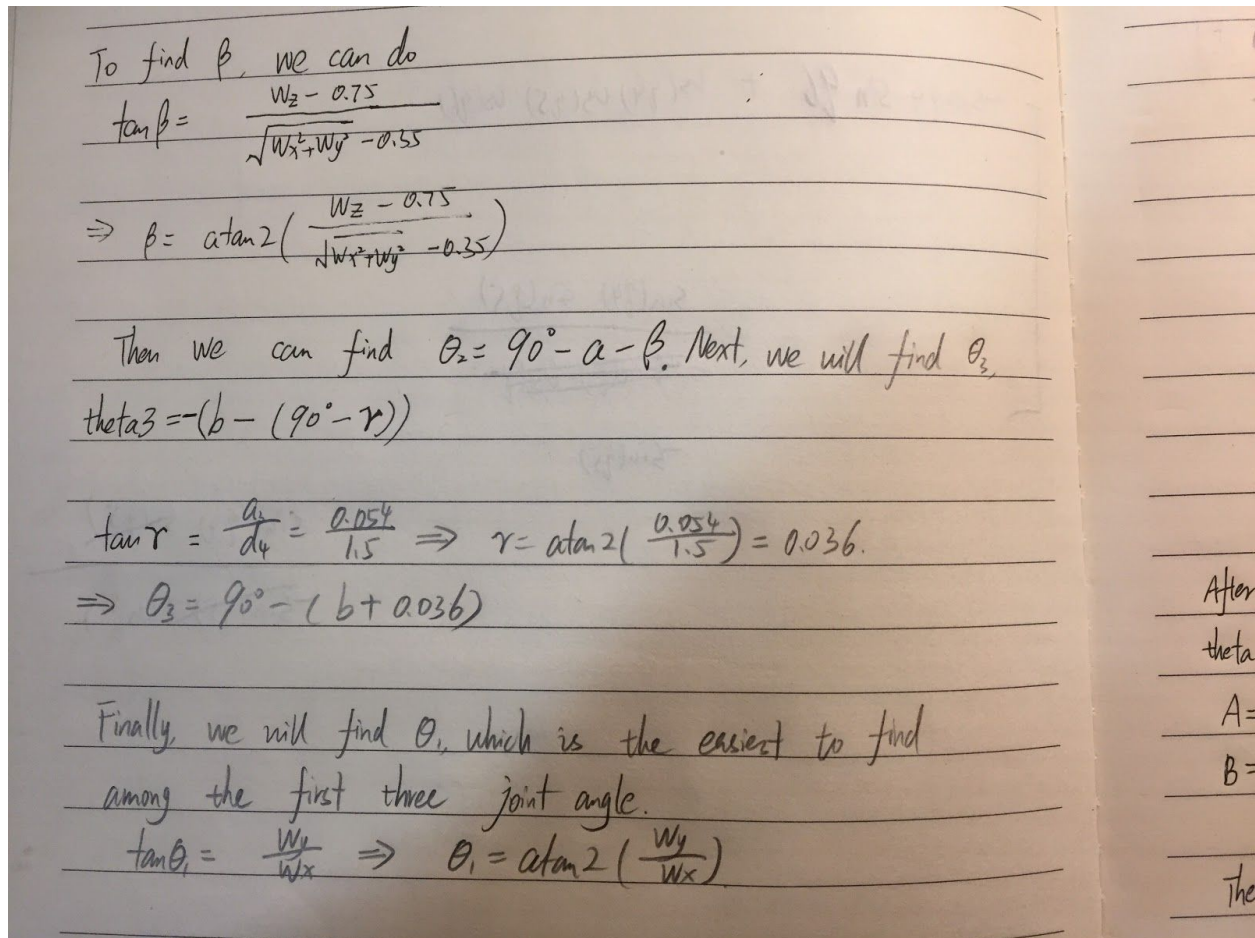


Figure 7: Solving first three joints angles part 2.

Last, let's solve the last three joint angles  $\theta_4$ ,  $\theta_5$  and  $\theta_6$ . First, we need to use  $\theta_1$ ,  $\theta_2$  and  $\theta_3$  that we just calculated to compute  $R_{0\_3}$ . Because we know that  $R_{0\_EE} = \text{Rot\_EE}$ , both side multiple by  $\text{inv}(R_{0\_3})$ , we can get  $R_{3\_6} = \text{inv}(R_{0\_3}) * \text{Rot\_EE}$ . We already have the form of  $R_{3\_6}$  in Figure 2, then we can compute last three joint angle by doing,

```
# Convert the rotation matrix to Euler angles using tf
theta4 = atan2(R3_6[2,2], -R3_6[0,2]);
theta5 = atan2(sqrt(R3_6[0,2]**2 + R3_6[2,2]**2), R3_6[1,2]);
theta6 = atan2(-R3_6[1,1], R3_6[1,0]);
```

## Project Implementation

The code below is the implementation of handling inverse kinematics problem.



```

def handle_calculate_IK(req):
    rospy.loginfo("Received %s eef-poses from the plan" % len(req.poses))
    if len(req.poses) < 1:
        print "No valid poses received"
        return -1
    else:
        ### Your FK code here
        # Create symbols
        q1, q2, q3, q4, q5, q6, q7 = symbols('q1:8');
        d1, d2, d3, d4, d5, d6, d7 = symbols('d1:8');
        a0, a1, a2, a3, a4, a5, a6 = symbols('a0:7');
        alpha0, alpha1, alpha2, alpha3, alpha4, alpha5, alpha6 =
symbols('alpha0:7');
        # Create Modified DH parameters
        s = {
            alpha0: 0, a0: 0, d1: 0.75, q1: q1,
            alpha1: -pi/2., a1: 0.35, d2: 0, q2: -pi/2. + q2,
            alpha2: 0, a2: 1.25, d3: 0, q3: q3,
            alpha3: -pi/2., a3: -0.054, d4: 1.5, q4: q4,
            alpha4: pi/2., a4: 0, d5: 0, q5: q5,
            alpha5: -pi/2., a5: 0, d6: 0, q6: q6,
            alpha6: 0, a6: 0, d7: 0.303, q7: 0
        }
        # Define Modified DH Transformation matrix
        def TF_Matrix(alpha, a, d, q):
            TF = Matrix([[
                cos(q), -sin(q),
0, a,
                [sin(q)*cos(alpha), cos(q)*cos(alpha),
-sin(alpha), -sin(alpha) * d],
                [sin(q)*sin(alpha), cos(q)*sin(alpha),
cos(alpha), cos(alpha) * d],
                [
0, 0, 0,
0, 1]])
            return TF;

        # Create individual transformation matrices
        T0_1 = TF_Matrix(alpha0, a0, d1, q1).subs(s);
        T1_2 = TF_Matrix(alpha1, a1, d2, q2).subs(s);
        T2_3 = TF_Matrix(alpha2, a2, d3, q3).subs(s);
        # T3_4 = TF_Matrix(alpha3, a3, d4, q4).subs(s);
        # T4_5 = TF_Matrix(alpha4, a4, d5, q5).subs(s);
        # T5_6 = TF_Matrix(alpha5, a5, d6, q6).subs(s);
        # T6_EE = TF_Matrix(alpha6, a6, d7, q7).subs(s);

```

```

# T3_6 = T3_4 * T4_5 * T5_6;
# R3_6 = T3_6[0:3, 0:3];
# print(R3_6);

# T0_EE = T0_1 * T1_2 * T2_3 * T3_4 * T4_5 * T5_6 * T6_EE;

R = symbols('R');
Y = symbols('Y');
P = symbols('P');

### Build Rotation Matrix extrinsic

RotRoll_x = Matrix([[1,      0,      0],
                    [0, cos(R), -sin(R)],
                    [0, sin(R), cos(R)]]);
RotPitch_y = Matrix([[cos(P), 0, sin(P)],
                    [0,      1,      0],
                    [-sin(P), 0, cos(P)]]);
RotYaw_z    = Matrix([[cos(Y), -sin(Y), 0],
                    [sin(Y),  cos(Y), 0],
                    [0,      0,      1]]);
Rot_EE = RotYaw_z * RotPitch_y * RotRoll_x;
Rot_Error = RotYaw_z.subs(Y, radians(180)) * RotPitch_y.subs(P,
radians(-90));
Rot_EE = Rot_EE * Rot_Error;
wc_to_ee = 0.303;
###
R0_3 = T0_1[0:3, 0:3] * T1_2[0:3, 0:3] * T2_3[0:3, 0:3]
# Initialize service response
joint_trajectory_list = []
for x in xrange(0, len(req.poses)):
    # IK code starts here
    joint_trajectory_point = JointTrajectoryPoint()

    # Extract end-effector position and orientation from request
    # px,py,pz = end-effector position
    # roll, pitch, yaw = end-effector orientation
    px = req.poses[x].position.x
    py = req.poses[x].position.y
    pz = req.poses[x].position.z

```

```

        (roll, pitch, yaw) = tf.transformations.euler_from_quaternion(
            [req.poses[x].orientation.x, req.poses[x].orientation.y,
             req.poses[x].orientation.z,
             req.poses[x].orientation.w])

    ### Your IK code here

    euler = {R: roll, P: pitch, Y: yaw};
    Rrpy = Rot_EE.subs(euler);
    nx = Rrpy[0,2];
    ny = Rrpy[1,2];
    nz = Rrpy[2,2];

    ### Calculate wrist center
    wx = px - wc_to_ee * nx;
    wy = py - wc_to_ee * ny;
    wz = pz - wc_to_ee * nz;
    # Calculate joint angles using Geometric IK method
    theta1 = atan2(wy, wx);
    # side_a = sqrt(s[a3]**2 + s[d4]**2);
    side_a = 1.501
    side_c = 1.25
    # side_c = s[a2];
    # wcx = wz - s[d1];
    wcx = wz - 0.75;
    # wcy = sqrt(wx**2 + wy**2) - s[a1];
    wcy = sqrt(wx**2 + wy**2) - 0.35;

    side_b = sqrt(wcy**2 + wcx**2);

    angle_a = acos((side_b**2 + side_c**2 -
side_a**2)/(2*side_b*side_c));
    angle_b = acos((side_a**2 + side_c**2 -
side_b**2)/(2*side_a*side_c));
    angle_c = acos((side_a**2 + side_b**2 -
side_c**2)/(2*side_a*side_b));
    theta2 = pi/2 - angle_a - atan2(wcx, wcy);
    theta3 = pi/2 - (angle_b + 0.036);
    ### Clip the joint angle for physical constrain
    theta1 = np.clip(theta1, -3.23, 3.23);
    theta2 = np.clip(theta2, -0.79, 1.48);
    theta3 = np.clip(theta3, -3.67, 1.13);

```

```

R0_3 = R0_3.evalf(subs={q1: theta1, q2: theta2, q3: theta3});
R3_6 = R0_3.inv("LU") * Rrpy;

# Convert the rotation matrix to Euler angles using tf
theta4 = atan2(R3_6[2,2], -R3_6[0,2]);
theta5 = atan2(sqrt(R3_6[0,2]**2 + R3_6[2,2]**2), R3_6[1,2]);
theta6 = atan2(-R3_6[1,1], R3_6[1,0]);
# print("theta4, theta5, theta6", theta4, theta5, theta6);
### Clip the joint angle for physical constrain
theta4 = np.clip(theta4, -6.11, 6.11);
theta5 = np.clip(theta5, -2.18, 2.18);
theta6 = np.clip(theta6, -6.11, 6.11);

# Populate response for the IK request
joint_trajectory_point.positions = [theta1, theta2, theta3,
theta4, theta5, theta6]
joint_trajectory_list.append(joint_trajectory_point)

rospy.loginfo("length of Joint Trajectory List: %s" %
len(joint_trajectory_list))
return CalculateIKResponse(joint_trajectory_list)

```

The images below show the pick and drop processes.





Figure 8: Reaching to the target position

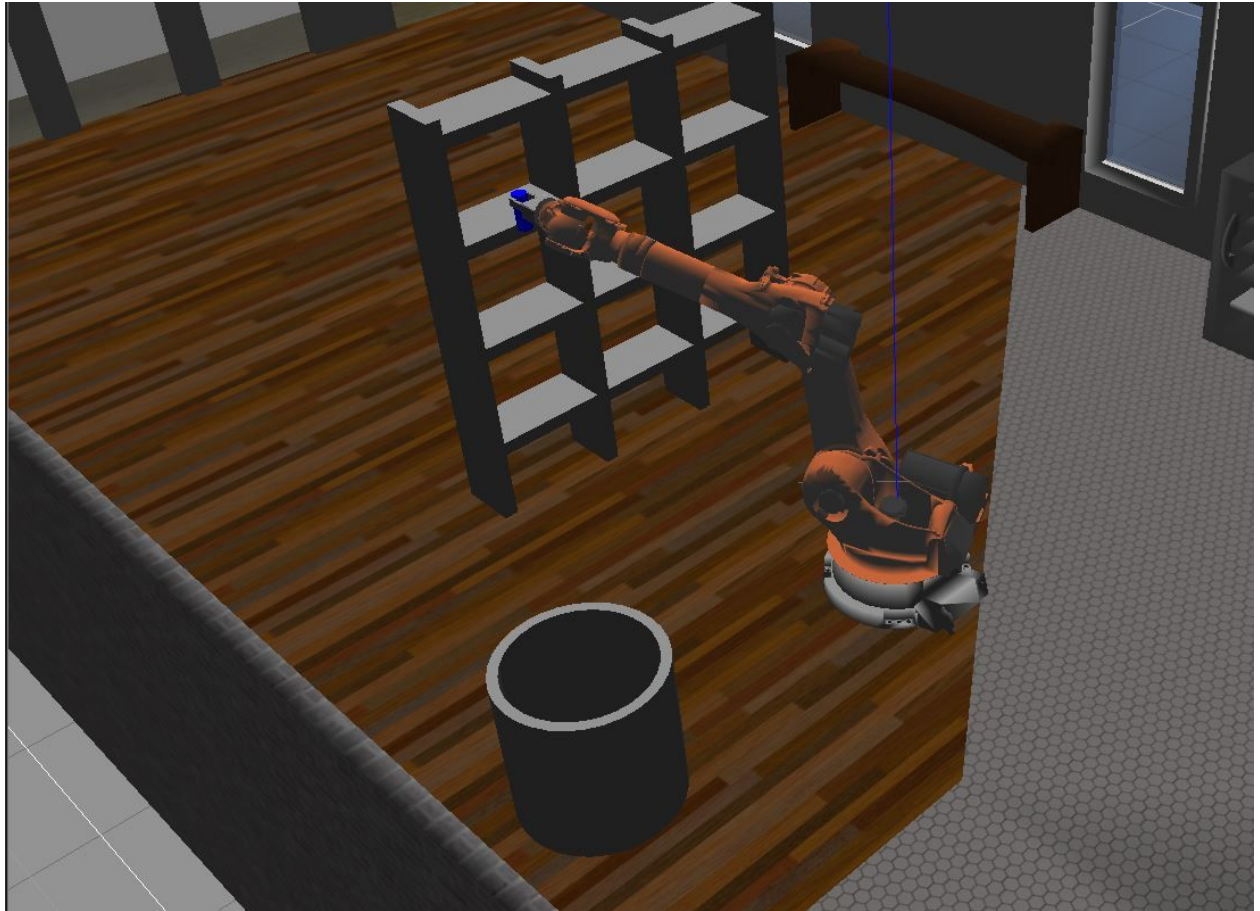


Figure 9: Retrieve the target

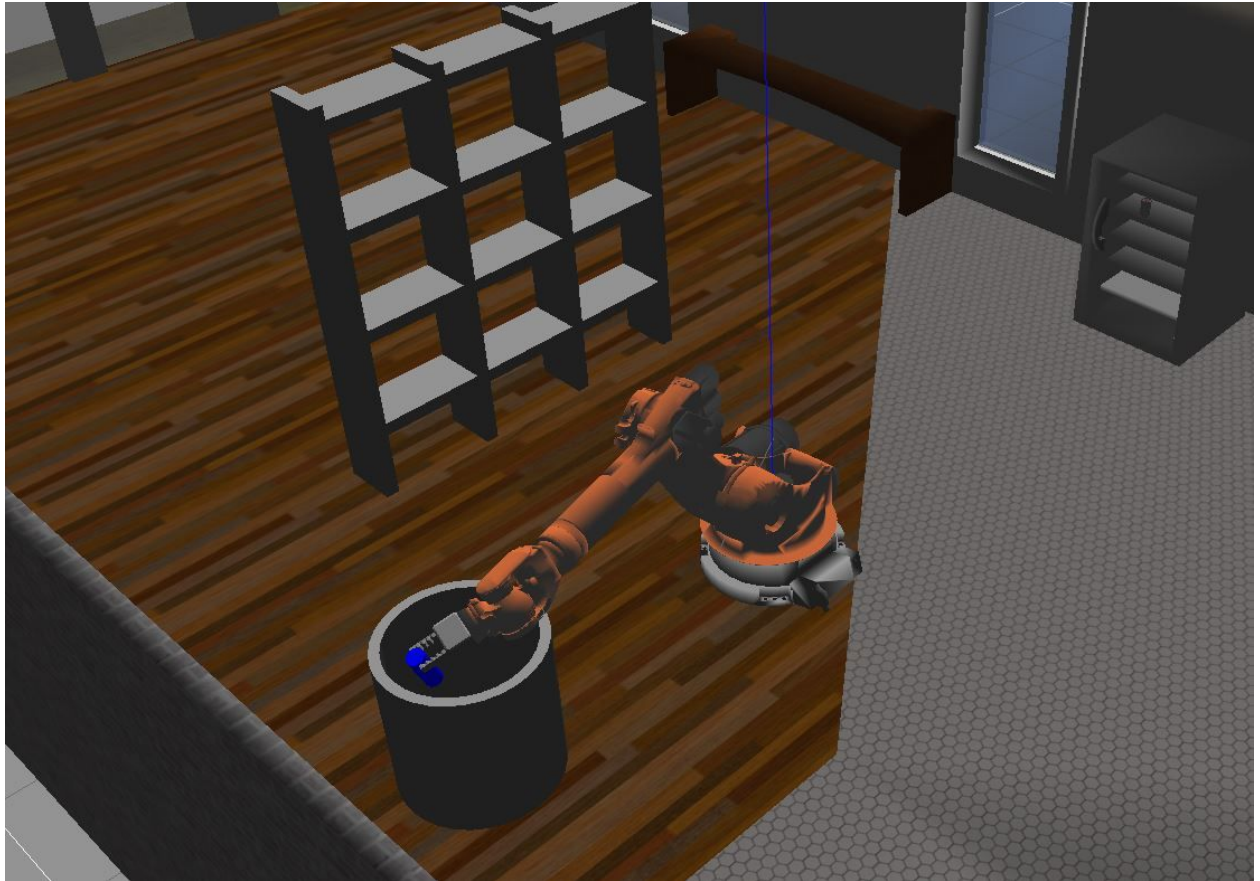


Figure 10: Drop the target