

# Applied Wave Optics: Film Waveguides

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All sources and vector graphics are available on the GitHub repository  
[https://github.com/reincas/AWO\\_course](https://github.com/reincas/AWO_course).

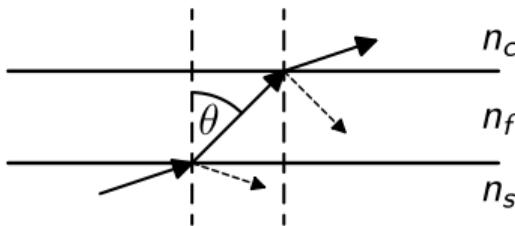
## Film Waveguides

Waveguiding requires at least two interfaces. The film waveguide with two parallel interfaces consisting of three material layers **substrate**, **film** and **cladding** is the simplest kind of dielectric waveguide. Utilisation of total internal reflection requires the highest refractive index for the film layer. We denote the other layers according to

$$n_f > n_s \geq n_c$$

The range of propagation angles  $\theta$  in the film splits into three cases. Small angles result in normal reflection at both interfaces. This is called **free wave**:

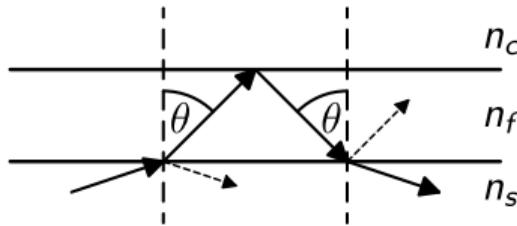
$$\frac{n_s}{n_f} \geq \frac{n_c}{n_f} > \sin \theta$$



## Film Waveguides (cont.)

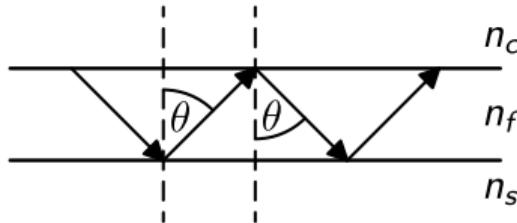
If substrate and cladding have different refractive indices, intermediate angles can result in total internal reflection at the cladding only. This is called **substrate wave**:

$$\frac{n_s}{n_f} > \sin \theta > \frac{n_c}{n_f}$$



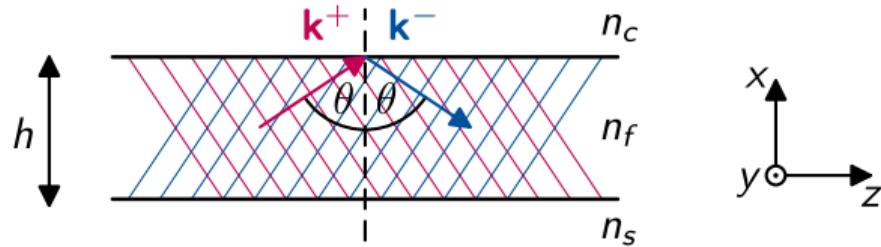
Waveguiding requires total internal reflection at both interfaces. The **film wave** is trapped between both interfaces. It can enter and leave the film only via its end faces:

$$\sin \theta > \frac{n_s}{n_f} \geq \frac{n_c}{n_f}$$



## Reflected Wave

For each guided wave with wave vector  $\mathbf{k}^+ = k(\cos \theta, 0, \sin \theta)$  there is also its reflected counterpart with wave vector  $\mathbf{k}^- = k(-\cos \theta, 0, \sin \theta)$ :



With  $\mathbf{r} = (x, y, z)$  the expressions for these two waves are

$$\mathbf{E}^\pm(t, \mathbf{r}) = \hat{\mathbf{E}} e^{i(\omega t - n_f \mathbf{k}^\pm \cdot \mathbf{r})} = \hat{\mathbf{E}} e^{i[\omega t - kn_f (\pm x \cos \theta + z \sin \theta)]}$$

## Standing Wave

The superposition of both waves results in a sum wave **standing** in  $x$ -direction and **travelling** in  $z$ -direction along the waveguide:

$$\begin{aligned}\mathbf{E}(t, \mathbf{r}) &= \mathbf{E}^+(t, \mathbf{r}) + \mathbf{E}^-(t, \mathbf{r}) \\ &= \hat{\mathbf{E}} \left[ e^{i[\omega t - kn_f(-x \cos \theta + z \sin \theta)]} + e^{i[\omega t - kn_f(x \cos \theta + z \sin \theta)]} \right] \\ &= \hat{\mathbf{E}} \left( e^{ikn_f x \cos \theta} + e^{-ikn_f x \cos \theta} \right) e^{i(\omega t - kn_f z \sin \theta)} \\ &= 2 \hat{\mathbf{E}} \cos(kn_f x \cos \theta) e^{i(\omega t - \beta z)}\end{aligned}$$

with  $\beta = kn_{\text{eff}}$  and the **effective refractive index**  $n_{\text{eff}} = n_f \sin \theta$  of the propagation in  $z$ -direction. The value of this effective refractive index always lies between the film and the surrounding materials:

$$n_f \geq n_{\text{eff}} \geq n_s \geq n_c$$

## Characteristic Equation

Note: The derivation requires **constructive interference** of both waves. The phase delay of a full round trip in  $x$ -direction must sum up to an integer multiple of  $2\pi$ :

$$kn_f h \cos \theta - 2\Phi_c(\theta) + kn_f h \cos \theta - 2\Phi_s(\theta) = m 2\pi \quad \text{with } m = 0, 1, 2, \dots$$

The propagation angle  $\theta$  of a guided wave must satisfy the **characteristic equation**

$$kn_f h \cos \theta - \Phi_c(\theta) - \Phi_s(\theta) = m\pi$$

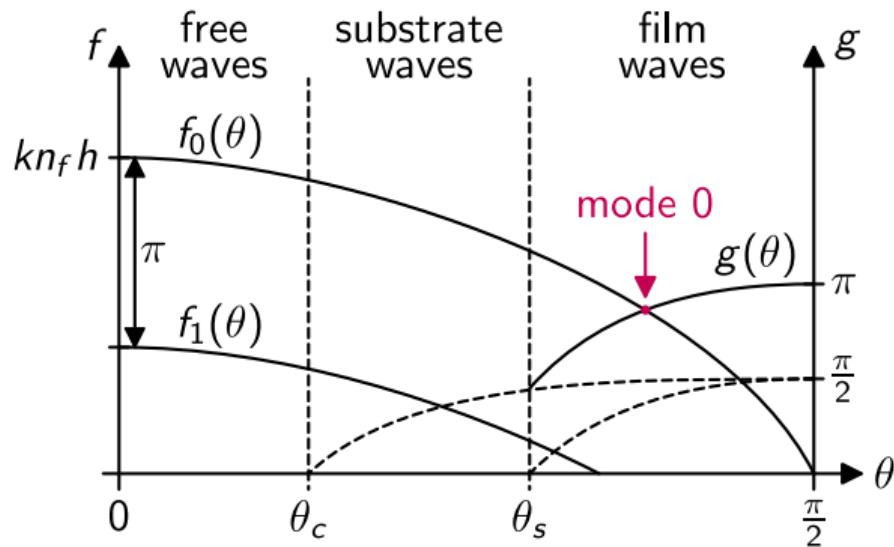
with the polarisation dependent phase shifts of total internal reflection

$$\text{TE: } \tan \Phi_i(\theta) = \sqrt{\frac{n_{\text{eff}}^2(\theta) - n_i^2}{n_f^2 - n_{\text{eff}}^2}} \quad \text{TM: } \tan \Phi_i(\theta) = \frac{n_f^2}{n_i^2} \sqrt{\frac{n_{\text{eff}}^2(\theta) - n_i^2}{n_f^2 - n_{\text{eff}}^2}}$$

with  $i \in [s, c]$ . Such guided waves are called **transversal waveguide modes**.

## Waveguide Modes

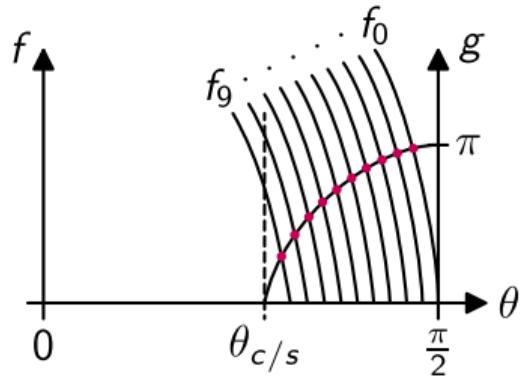
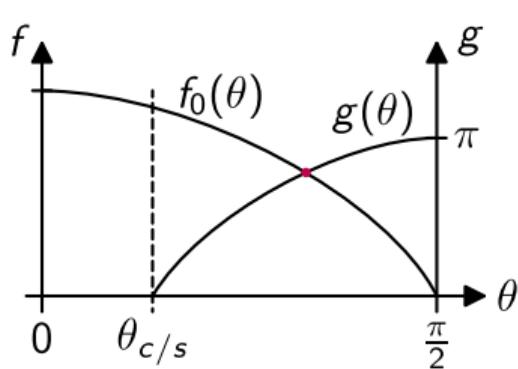
There exists no analytical solution of the characteristic equation. For a graphical solution we split it into two functions  $f_m(\theta) = kn_f h \cos \theta - m\pi$  and  $g(\theta) = \Phi_s(\theta) + \Phi_c(\theta)$ . Guided modes thus correspond to intersections of both functions:



with the critical angles  $\sin \theta_c = n_c/n_f$  and  $\sin \theta_s = n_s/n_f$ .

## Special Cases

**Symmetric waveguides** with  $n_c = n_s$  are always guiding at least one mode:



For thick films with  $h \gg \lambda$  the function  $f_m(\theta)$  becomes very steep, resulting in many intersections. Such waveguides are called **multimode waveguides**.

## Universal Solution

The  $V$ -number as dimensionless **frequency parameter** combines the external input parameters of geometry ( $h$ ), material ( $NA$ ) and signal ( $\lambda$ ) using the definition of the numerical aperture  $NA = \sqrt{n_f^2 - n_s^2}$ :

$$V = kh\sqrt{n_f^2 - n_s^2} = 2\pi \frac{h}{\lambda} NA \in [0, \infty]$$

The **asymmetry parameter**  $\alpha$  is zero for symmetric waveguides with  $n_c = n_s$ . For TE modes it is given by:

$$\alpha_{TE} = \frac{n_s^2 - n_c^2}{n_f^2 - n_s^2} \in [0, \infty]$$

The **phase parameter**  $B_m$  describes a waveguide mode  $m$  based on the propagation angle  $\theta_m$  as output parameter:

$$B_m = \frac{n_{\text{eff}}^2 - n_s^2}{n_f^2 - n_s^2} = \frac{n_f^2 \sin^2 \theta_m - n_s^2}{n_f^2 - n_s^2} \in [0, 1]$$

## Universal Solution (cont.)

With these definitions, the terms of the characteristic equation translate to:

$$kn_f h \cos \theta_m = V \sqrt{1 - B_m} \quad \tan \Phi_{s,TE} = \sqrt{\frac{B_m}{1 - B_m}} \quad \tan \Phi_{c,TE} = \sqrt{\frac{B_m + \alpha_{TE}}{1 - B_m}}$$

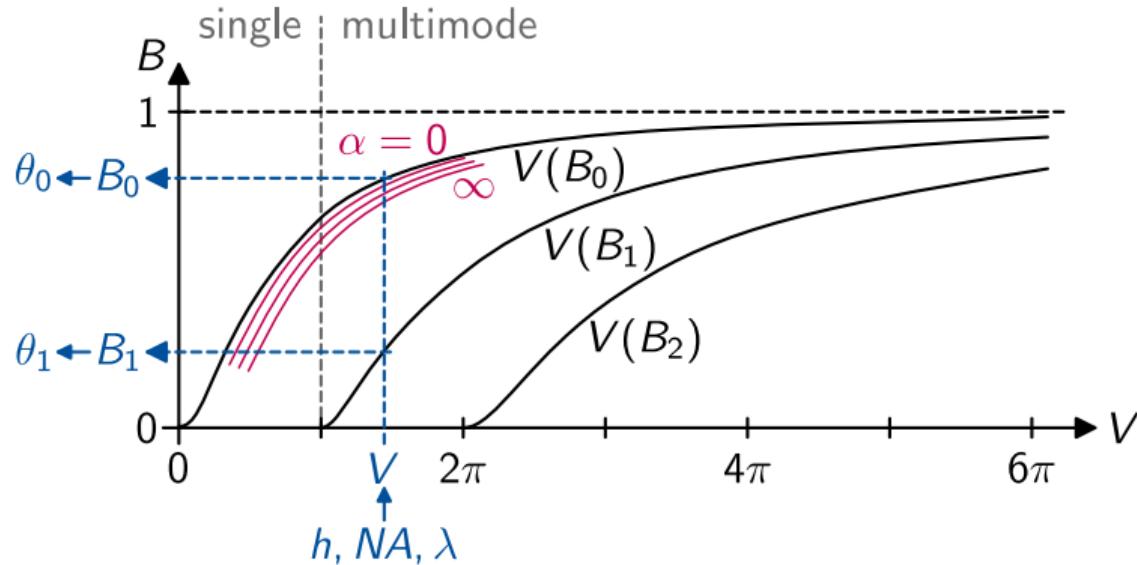
The universal characteristic equation is thus

$$V(B_m) = \frac{1}{\sqrt{1 - B_m}} \left( m\pi + \arctan \sqrt{\frac{B_m}{1 - B_m}} + \arctan \sqrt{\frac{B_m + \alpha_{TE}}{1 - B_m}} \right)$$

There again exists no analytical solution, but  $V$  is a monotonous function of  $B_m$  and has certain properties, which make a numerical inversion simple and straight forward. This is used to determine the phase parameter for each mode.

## Numerical Algorithm

We start with the calculation of the  $V$ -number based on the parameters of the waveguide. Its value determines the number of modes. For each mode  $m$  the phase parameter  $B_m$  between 0 and 1 is found using the bisection method on the monotonous function  $V(B_m)$ . Finally, the mode angle  $\theta_m$  is directly calculated from  $B_m$ .



## Number of Modes

For each mode  $m$  the curve starts at a certain point  $V_m$ , which determines the number of modes for a given  $V$ -number:

$$V_m = V|_{B_m=0} = m\pi + \arctan \sqrt{\alpha_{TE}}$$

Taking into account that each TE mode comes with a respective TM mode, this **number of modes**  $N$  is two times the first integer above  $V/\pi$  in case of a symmetric waveguide with  $\alpha_{TE} = 0$ :

$$N = 2 \operatorname{ceil} \left( \frac{V}{\pi} \right) = 2 \operatorname{ceil} \left( \frac{2h}{\lambda} \sqrt{n_f^2 - n_s^2} \right)$$

## Cut-Off Wavelength

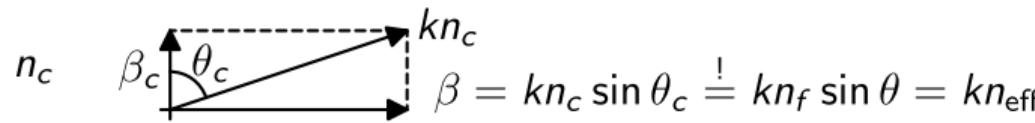
For a given waveguide and a given mode number  $m$  there exists a **cut-off wavelength**  $\lambda_m$ , which is the largest signal wavelength allowed for mode  $m$  to exist:

$$2\pi \frac{h}{\lambda_m} \sqrt{n_f^2 - n_s^2} = m\pi$$
$$\lambda_m = \frac{2h}{m} \sqrt{n_f^2 - n_s^2}$$

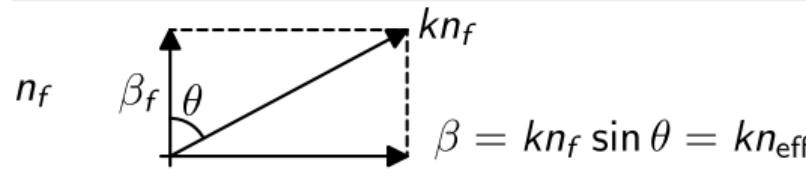
In particular, this means that a given waveguide is **single-mode** for signal wavelengths  $\lambda > \lambda_1$  and the same waveguide is **multimode** for  $\lambda < \lambda_1$ .

## Wave Vectors

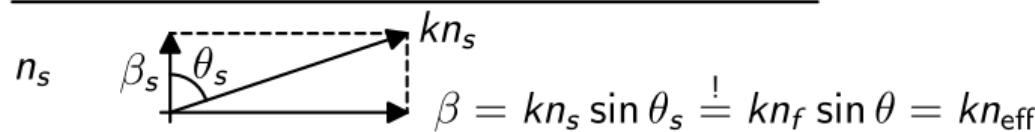
The component  $\beta$  of the wave vector in the direction of the waveguide is the same in all three layers, due to Snell's law:



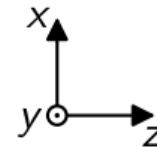
$$\beta = kn_c \sin \theta_c \stackrel{!}{=} kn_f \sin \theta = kn_{\text{eff}}$$



$$\beta = kn_f \sin \theta = kn_{\text{eff}}$$



$$\beta = kn_s \sin \theta_s \stackrel{!}{=} kn_f \sin \theta = kn_{\text{eff}}$$



## Wave Vectors (cont.)

The component  $\beta_i$  perpendicular to the interfaces with  $i \in [s, f, c]$  can be calculated using Pythagoras' theorem:

$$\beta_i = \sqrt{n_i^2 k^2 - \beta^2} = k \sqrt{n_i^2 - n_f^2 \sin^2 \theta}$$

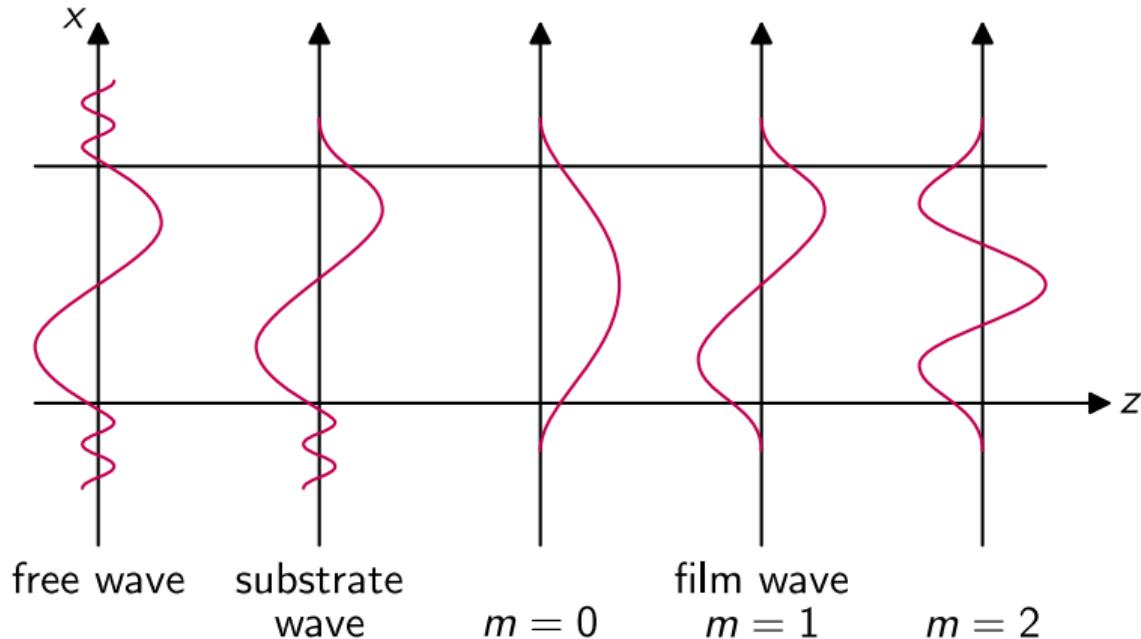
It is related to the **spatial period**  $\Lambda_i$  of the lateral mode shape by  $\beta_i = 2\pi/\Lambda_i$ . In case of total internal reflection, the square root is imaginary in the substrate and/or cladding:

$$\alpha_i = ik \sqrt{n_f^2 \sin^2 \theta - n_i^2}$$

and the mode shape follows an exponential decay instead of a spatial oscillation. This tail of the mode protruding into the substrate and/or cladding is called **evanescent field**.

## Mode Shapes

The lateral shape of the waveguide modes consists of piecewise defined sine and/or exponential functions. The shape as well as its first derivative is continuous at both interfaces. These conditions are fixing the lateral phase offsets in each layer.



## Summary of Mode Calculations

- ▶ The **initial parameters**  $h$ ,  $n_s$ ,  $n_f$ ,  $n_c$ ,  $\lambda$ , and  $E_f$  are given by the waveguide design and the experimental conditions.
- ▶ Fresnel equations determine the amplitudes  $E_s$  and  $E_c$ .
- ▶ Solving the characteristic equation provides the number of modes  $N$  as well as their propagation angles  $\theta_m$ .
- ▶ The propagation angles determine the lateral wave numbers  $\beta_i$  or exponential decay parameters  $\alpha_i$ .
- ▶ Based on the previous results the continuity conditions at the interfaces deliver the lateral phase offset in each material layer.
- ▶ **Result:** Completely defined shape and propagation parameters for all guided and unguided modes.