

Simulations of stratified rotating turbulence and comparison with oceanic wave turbulence

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Abstract

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Chapter 1

Inertial and Gravity Waves

1.1 Introduction

1.1.1 Navier-Stokes Equations

We will study the system defined by the Navier-Stokes equations eq. (1.1) and eq. (1.2).

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{u}) = 0 \quad (1.1)$$

$$\frac{\partial \vec{u}}{\partial t} + \left(\vec{u} \cdot \vec{\nabla} \right) \vec{u} = -\frac{1}{\rho} \vec{\nabla} p + \vec{g} + \nu \Delta \vec{u} - 2\vec{\Omega} \times \vec{u} \quad (1.2)$$

Where ρ is the fluid density, \vec{u} is the velocity vector (of the fluid), $\vec{\Omega}$ is the rotation vector (which in our case will be aligned with \hat{e}_z), p is the pressure, ν is the kinematic viscosity and $\vec{g} = -g\hat{e}_z$ is the gravitational acceleration.

Let us quickly describe and name each term of eq. (1.2).

Local acceleration $\frac{\partial \vec{u}}{\partial t}$ is simply the local acceleration of a fluid particle.

Advection term $\left(\vec{u} \cdot \vec{\nabla} \right) \vec{u}$ is the non linear term representing the acceleration due to the fluid itself.

Pressure gradient term $-\frac{1}{\rho} \vec{\nabla} p$ represents the effects of the pressure on the fluid.

Gravitational term \vec{g} is the force acting on the fluid due to gravity.

Coriolis term $2\vec{\Omega} \times \vec{u}$ is an apparent force arising from the rotation of our reference frame.

Viscous term $\nu \Delta \vec{u}$ is the diffusion of the momentum due to fluid viscosity.



1.1.2 Wave propagation conditions

A system needs a restoring force in order to allow the propagation of waves. In our case, it will be the gravitational acceleration of the system as well as the Coriolis acceleration. Both forces doesn't act on the same movements, gravity being vertical only, it will act as the restoring force of the vertical displacements, also called the buoyancy force, whereas Coriolis will provide the restoring force of horizontal displacements. Wave frequencies will then depend on two parameters :

The Coriolis parameter (f) which depends on the latitude and represent the influence of Earth rotation.

The Brunt-Väisälä frequency (N) which characterize the buoyancy effect.

We will describe more precisely those parameters in section 1.2, respectively section 1.3.

1.1.3 Wave interaction conditions

In order for wave to interact, there must be spatial and temporal resonance such as

$$\vec{k}_0 + \vec{k}_1 + \vec{k}_2 = 0 \qquad \omega_0 + \omega_1 + \omega_2 = 0$$

Which yields conservation of the energy and the pseudo-momentum (see [SS02]). An easy conclusion that we can find from those relations is that $\omega(\vec{k})$ must be a convex function¹.

1.1.4 Dimensionless Numbers

We will use a set of dimensionless numbers to describe our problem. To find the expression of those numbers, we will rewrite our equations in characteristic scales of each variables: Characteristic velocity U , pressure P , length L , height H and time τ . The rotation ω , the kinematic viscosity ν and the gravity g don't need characterization. Any derivatives, either time or space derivatives, will simply be replaced by the inverse of the characteristic variables associated, *i.e.* $\partial_t \propto 1/\tau$, $\partial_{x,y} \propto 1/L$ and $\partial_z \propto 1/H$ ².

We can now rewrite Navier-Stokes equations, especially eq. (1.2) in the *characteristic space*

$$\frac{U}{\tau} + \frac{U^2}{L} = \frac{P}{\rho} + g + \frac{\nu U}{L^2} - 2\Omega U \quad (1.3)$$

The expression of each dimensionless number will be the ratio of two terms of eq. (1.3).

Reynolds Number $Re = \frac{UL}{\nu}$ is the ratio between the advection and viscous terms. It describes how turbulent a flow is.

¹A function is convex if $f(tx_1 + (1-t)x_2) \leq tf(x_1) + (1-t)f(x_2)$, *i.e.* any line between two point on the curve is above the function and doesn't cross it.

²In the whole paper, spatial derivatives $\frac{\partial}{\partial x,y,z}$ will be written $\partial_{x,y,z}$ and time derivatives $\frac{\partial}{\partial t}$ written as ∂_t



Rossby Number $Ro = \frac{U}{L\Omega}$ is the ratio between the advection and Coriolis terms. It describes how the flow is affected by the rotation of the frame of reference.

Ekman Number $Ek = \frac{\nu}{\Omega L^2}$ is the ratio between the diffusion and Coriolis terms. It describes how well the disturbance due to Coriolis can propagate before being diffused.

Froude Number $Fr^2 = \frac{U^2}{gH}$ is the ratio between the advection and gravitational terms. It describes the comparison between flow speed and wave speed.

Burger Number $Bu = \left(\frac{Ro}{Fr}\right)^2$ describes the impacts of density stratification compared to those of the rotation of the reference frame.

1.2 Inertial Waves

1.2.1 Equations and Approximations

For the inertial wave, we will focus on the Coriolis effect due to a rotation along the z-axis. For that, we will consider a system with no gravitational acceleration, *i.e.* $g = 0$, and a constant and uniform density throughout the flow. We will also consider $Ro \ll 1$ and $Ek \ll 1$ meaning that we can neglect the advection and the viscous terms in eq. (1.2). This means that we are left with the following system

$$\vec{\nabla} \cdot \vec{u} = 0 \qquad \partial_t \vec{u} + 2\vec{\Omega} \times \vec{u} = -\vec{\nabla} \tilde{p} \quad (1.4)$$

where $\tilde{p} = p/\rho$ is the dynamic pressure.

We can now apply the curl operator $\vec{\nabla} \times$ to eq. (1.4).

$$\begin{aligned} \vec{\nabla} \times \partial_t \vec{u} + \vec{\nabla} \times (2\vec{\Omega} \times \vec{u}) &= \vec{\nabla} \times \vec{\nabla} \tilde{p} \\ \partial_t (\vec{\nabla} \times \vec{u}) - 2(\vec{\Omega} \cdot \vec{\nabla}) \vec{u} &= 0 \\ \partial_t^2 (\vec{\nabla} \times \vec{u}) &= 2(\vec{\Omega} \cdot \vec{\nabla}) \partial_t \vec{u} \quad \text{we apply } \partial_t \\ \partial_t^2 (\vec{\nabla} \times (\vec{\nabla} \times \vec{u})) &= 2(\vec{\Omega} \cdot \vec{\nabla}) \partial_t (\vec{\nabla} \times \vec{u}) \quad \text{we apply } \vec{\nabla} \times \\ \partial_t^2 \Delta \vec{u} + 4(\vec{\Omega} \cdot \vec{\nabla})^2 \vec{u} &= \vec{0} \quad \text{we inject the second line} \end{aligned}$$

We have obtained the propagation equation of inertial waves.

$$\partial_t^2 \Delta \vec{u} + 4(\vec{\Omega} \cdot \vec{\nabla})^2 \vec{u} = \vec{0} \quad (1.5)$$



1.2.2 Plane wave and dispersion relation

Now that we have found the propagation equation eq. (1.5) for the inertial waves, we need to find its dispersion relation and its eigenmodes. In order to do that, we will express \vec{u} as $\vec{u} = \hat{u}e^{i(\vec{k}\cdot\vec{r}-\omega t)}$. This expression transforms any temporal derivatives as $\partial_t \vec{u} = -i\omega \vec{u}$ and any spatial derivatives as $\vec{\nabla} \cdot \vec{u} = i\vec{k} \cdot \vec{u}$. We can now inject this into the wave propagation equation.

$$\omega^2 |\vec{k}|^2 = 4\Omega^2 (\hat{e}_z \cdot \vec{k})^2 \quad (1.6)$$

which we can rewrite as

$$\omega = \pm 2\Omega \cos \theta \quad (1.7)$$

where θ is the angle between \vec{k} and the z-axis. This means that ω can only takes value between $[-f, f]$, where $f = 2\Omega$ is the Coriolis parameter.

With the divergence-free condition on the flow we also have

$$\vec{\nabla} \cdot \vec{u} = \vec{k} \cdot \vec{u} = 0$$

Which means that the inertial waves are indeed transverse waves.

Lastly we need to find the group \vec{c}_g and phase \vec{c}_ϕ velocity of the waves.

$$\begin{aligned} \vec{c}_g &= \frac{d\omega}{d\vec{k}} & \vec{c}_\phi &= \frac{\omega}{\vec{k}} \hat{k} \\ \vec{c}_g &= \mp f \frac{k_z}{k^2} & \vec{c}_\phi &= \pm f \frac{k_z}{k^2} \\ \vec{c}_g &= \pm f \frac{\vec{k} \times (\hat{z} \times \vec{k})}{k^3} \end{aligned}$$

With the second expression for the group velocity, we find that the group velocity and the wave vector are perpendicular.

1.3 Gravity Waves

1.3.1 Equations and approximations

In this part we will focus on the effect of the gravity field through the buoyancy term. We will consider a newtonian fluid with no rotation vector $\vec{\Omega} = \vec{0}$. The equations to consider are

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{u}) = 0 \quad (1.8)$$

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \vec{\nabla}) \vec{u} = -\frac{1}{\rho} \vec{\nabla} p + \vec{g} + \nu \Delta \vec{u} \quad (1.9)$$



Boussinesq's approximation

We will now use the Boussinesq's approximation, which consists on ignoring the variation of density except in the buoyancy term³. We will express the density as $\rho = \rho_0 + \rho_b(z) + \delta\rho$ where ρ_0 is the mean fluid density, $\rho_b(z)$ is the vertical density profile, with an uniform stratification, and $\delta\rho$ are density fluctuations which are of first order. The Boussinesq's approximation implies that the fluid is divergence-free, *i.e.* $\vec{\nabla} \cdot \vec{u} = 0$.

We can now inject everything into the Laplacian derivative of ρ

$$\begin{aligned}\partial_t \rho + (\vec{u} \cdot \vec{\nabla}) \rho &= 0 \\ \partial_t \delta\rho + u_z \partial_z \rho_b(z) &= 0\end{aligned}\tag{1.10}$$

We will express the velocity vector as $\vec{u} = \vec{u}_b + \vec{u}$ and consider no mean velocity, $\vec{u}_b = \vec{0}$, and inject both expression of \vec{u} and ρ in the Navier-Stokes equation, with negligible viscosity ν

$$(\rho_0 + \rho_b(z) + \delta\rho) \frac{\partial \vec{u}}{\partial t} + ((\vec{u}) \cdot \vec{\nabla}) (\vec{u}) = -\vec{\nabla} p + (\rho_0 + \rho_b(z) + \delta\rho) \vec{g}$$

We will remove every term with any order above the first.

$$\rho_0 \frac{\partial \vec{u}}{\partial t} = -\vec{\nabla} \tilde{P} + \delta\rho \vec{g}\tag{1.11}$$

Where \tilde{P} is the hydrostatic pressure⁴

We will take the divergence of eq. (1.11) to remove the velocity.

$$\begin{aligned}\vec{\nabla} \cdot \left(\rho_0 \frac{\partial \vec{u}}{\partial t} \right) &= \vec{\nabla} \cdot (-\vec{\nabla} \tilde{P} - \delta\rho \vec{g}) \\ \rho_0 \frac{\partial \vec{\nabla} \cdot (\vec{u})}{\partial t} &= -\Delta \tilde{P} + \vec{\nabla} \cdot (\delta\rho g \hat{e}_z) \\ \Delta \tilde{P} &= -\frac{\partial \delta\rho}{\partial z} g\end{aligned}$$

We will project eq. (1.11) along the z-axis.

$$\begin{aligned}\rho_0 \frac{\partial u_z}{\partial t} &= -\frac{\partial \tilde{P}}{\partial z} - \delta\rho g \\ \rho_0 \frac{\partial \Delta u_z}{\partial t} &= -\frac{\partial}{\partial z} \Delta \tilde{P} - \nabla^2 \delta\rho g \\ \rho_0 \frac{\partial \Delta u_z}{\partial t} &= g \frac{\partial^2 \delta\rho}{\partial z^2} - g \nabla^2 \delta\rho \\ \rho_0 \frac{\partial \Delta u_z}{\partial t} &= -g \nabla_h^2 \delta\rho\end{aligned}$$

³In reality this applies for every terms containing \vec{g} , but in our case, only the buoyancy is to consider

⁴The hydrostatic pressure $\tilde{P} = P + \rho g z$ is the pressure as we know in the Bernoulli equation $P = P_{atm} + \rho g z + \frac{1}{2} \rho u^2$, with a velocity u equal to 0.



We will apply the time derivative and use eq. (1.10) to replace $\delta\rho$.

$$\begin{aligned}\frac{\partial^2}{\partial t^2}\Delta u_z &= -\Delta_h \frac{g}{\rho_0} \frac{\partial \delta\rho}{\partial t} \\ \frac{\partial^2}{\partial t^2}\Delta u_z &= \Delta_h u_z \frac{g}{\rho_0} \frac{\partial \rho_b}{\partial z}\end{aligned}$$

We then define the Brunt-Väisälä frequency [Ped79] N as $N^2 = -\frac{g}{\rho_0} \frac{\partial \rho_b}{\partial z}$, note that its derivative is equal to 0 because we have a uniform stratification $\frac{\partial \rho_b}{\partial z} = d\rho = cst$. We can now further develop our equation to obtain our wave propagation equation for gravity wave.

$$\begin{aligned}\frac{\partial^2}{\partial t^2}\Delta u_z &= -N^2 \Delta_h u_z \\ \frac{\partial^2}{\partial t^2}\Delta u_z + N^2 \Delta_h u_z &= 0\end{aligned}\tag{1.12}$$

1.3.2 Plane wave and dispersion relation

With the same objectives as before, we will express u_z as a plane wave : $u_z = \hat{u}_z e^{i(\vec{k}\cdot\vec{r}-\omega t)}$ making the derivatives follow the same rule as in section 1.2.2. We can now work on eq. (1.12) which becomes

$$\omega^2 k^2 + N^2 k_h^2 = 0$$

Which gives us the dispersion relation of gravity wave

$$\omega = \pm N \frac{k_h}{k} = \pm N \sin \theta\tag{1.13}$$

With θ the same angle as in section 1.2.2. ω is still bounded between $[-N, N]$ with N the Brunt-Väisälä frequency.

We can now compute both the group and phase velocity

$$\begin{aligned}\vec{c}_g &= \frac{d\omega}{d\vec{k}} & \vec{c}_\phi &= \frac{\omega}{k} \hat{k} \\ \vec{c}_g &= \mp N \frac{k_h}{k^2} & \vec{c}_\phi &= \pm N \frac{k_z}{k^2} \\ \vec{c}_g &= \pm N \frac{\vec{k} \times (\hat{k}_h \times \vec{k})}{k^3}\end{aligned}$$

Which again demonstrate that the group velocity and the wave vector are perpendicular.

Chapter 2

Mathematical Decomposition

In order to manipulate the equation more easily, we need to decompose our velocity field. In our case, we will focus on two main decomposition, the **poloidal-toroidal** decomposition and the **geostrophic-ageostrophic** decomposition

2.1 Poloidal-Toroidal decomposition

2.1.1 Definitions

Assuming a solenoidal velocity field¹, we can show that \vec{u} can be decomposed in a unique way into a chosen axis[SW92], in our case the vertical direction

$$\vec{u}(x, y, z) = \vec{\nabla} \times \left(\vec{\nabla} \times (\varphi(x, y, z) \hat{e}_z) \right) + \vec{\nabla} \times (\psi(x, y, z) \hat{e}_z) + u_m(x, y, z) \quad (2.1)$$

$$\vec{u}(x, y, z) = \vec{u}_p(x, y, z) + \vec{u}_t(x, y, z) + \vec{u}_m(x, y, z) \quad (2.2)$$

$\vec{u}_p(x, y, z) = \vec{\nabla} \times (\vec{\nabla} \times \varphi \hat{e}_z)$ is called the poloidal part of \vec{u} , $\vec{u}_t(x, y, z) = \vec{\nabla} \times \psi \hat{e}_z$ is the toroidal part of \vec{u} and \vec{u}_m is the mean flow, which can be equal to zero in certain problems. It is useful to remark that \vec{u}_p being a curl of a curl, it is by definition curl-free, *i.e.* $\vec{\nabla} \times \vec{u}_p = 0$. This means that we can take the curl of any equation on the velocity and we will be left with only its toroidal part assuming no mean flow. This also means that the vorticity is only the curl of the toroidal velocity.

2.1.2 Energy

Kinetic Energy

To compute the kinetic energy under the poloidal-toroidal decomposition, it is easier to demonstrate it in the spectral space where $\vec{\nabla} = i\vec{k}$. We can express the poloidal spectral potential as $\hat{u}_p = i\vec{k} \times i\vec{k} \times \hat{\varphi} \hat{e}_z$

¹a field \vec{u} such as $\vec{\nabla} \cdot \vec{u} = 0$



and the toroidal potential as $\hat{u}_t = i\vec{k} \times \hat{\psi}\hat{e}_z$. We easily find that \hat{u}_t is in the plane perpendicular to the wave vector \vec{k} and that \hat{u}_p is indeed perpendicular to this plane, which means that \hat{u}_p and \hat{u}_t are perpendicular, *i.e.* $\hat{u}_p \cdot \hat{u}_t = 0$.

The kinetic energy E_k ² can be computed as

$$\begin{aligned}
 E_K &= \left\langle \frac{u^2}{2} \right\rangle \\
 &= \frac{1}{2} \int_{\mathbb{R}^3} \vec{u}^2 d^3\vec{r} = \frac{1}{2} \int_{\mathbb{R}^3} [\vec{u}_p + \vec{u}_t]^2 d^3\vec{r} \\
 &= \frac{1}{2} \int_{\mathbb{R}^3} [\vec{u}_p^2 + \vec{u}_t^2 + 2\vec{u}_p \cdot \vec{u}_t] d^3\vec{r} \\
 &= \frac{1}{2} \int_{\mathbb{R}^3} \vec{u}_p^2 d^3\vec{r} + \frac{1}{2} \int_{\mathbb{R}^3} \vec{u}_t^2 d^3\vec{r} \\
 &= \left\langle \frac{u_p^2}{2} \right\rangle + \left\langle \frac{u_t^2}{2} \right\rangle \\
 E_K &= E_P + E_T
 \end{aligned}$$

Potential Energy

In our case, the potential energy will be expressed with the vertical displacement of the fluid particles $\zeta = g \delta\rho / (N^2 \rho_0)$ as in [Aug11]

$$E_\phi = \left\langle \frac{N^2 \zeta^2}{2} \right\rangle$$

Total Energy

The total energy is then the sum of each terms

$$E_{tot} = E_P + E_T + E_\phi \tag{2.3}$$

2.1.3 Numerical expressions

We now want to be able to find both components of this decomposition from a numerical velocity field. The easiest way is to first compute the toroidal part by taking the curl of the velocity, then subtract

²This is in fact the specific energy $E = E/\rho$



it from the velocity to get the poloidal part.

$$\begin{aligned}\vec{\omega} &= \vec{\nabla} \times \vec{u} = \vec{\nabla} \times (\vec{u}_p + \vec{u}_t) \\ \vec{\omega} &= \vec{\nabla} \times \vec{u}_t \\ \vec{\nabla} \times \vec{\omega} &= \vec{\nabla} \left(\vec{\nabla} \cdot \vec{u}_t \right) - \nabla^2 \vec{u}_t \\ \vec{\nabla} \times \vec{\omega} &= -\nabla^2 \vec{u}_t\end{aligned}$$

We have then found the expression of \vec{u}_t in terms of $\vec{\omega}$ the vorticity, which is a simple Poisson equation. We can later compute the poloidal velocity $\vec{u}_p = \vec{u} - \vec{u}_t$.

2.2 Geostrophic-Ageostrophic Decomposition

2.2.1 Definitions

In the context of rotating, stratified flows, the velocity field \vec{u} can be decomposed into a geostrophic component and an ageostrophic component, based on the balance of the Coriolis force and pressure gradient forces. Assuming the flow evolves under the influence of a background rotation with angular velocity $\vec{\Omega} = \Omega \hat{e}_z$, we can express \vec{u} as [HH12]:

$$\vec{u}(x, y, z) = \vec{u}_g(x, y, z) + \vec{u}_a(x, y, z), \quad (2.4)$$

where \vec{u}_g is the geostrophic velocity and \vec{u}_a is the ageostrophic velocity.

Geostrophic Velocity

The geostrophic velocity \vec{u}_g is defined by the geostrophic balance, which states that the Coriolis force balances the pressure gradient:

$$2\Omega \hat{e}_z \times \vec{u}_g = -\frac{1}{\rho_0} \vec{\nabla} p, \quad (2.5)$$

where p is the pressure field and ρ_0 is a reference density. This relationship implies that \vec{u}_g is non-divergent in the horizontal plane:

$$\vec{\nabla}_H \cdot \vec{u}_g = 0,$$

where $\vec{\nabla}_H = (\partial_x, \partial_y)$ is the horizontal gradient operator.



Ageostrophic Velocity

The ageostrophic velocity \vec{u}_a captures the part of the flow that deviates from geostrophic balance. It represents unbalanced motions such as inertia-gravity waves, Ekman flows, or other ageostrophic circulations that are not directly in balance with the Coriolis force. The ageostrophic velocity can be obtained by subtracting the geostrophic component from the total velocity

$$\vec{u}_a = \vec{u} - \vec{u}_g.$$

Physical Interpretation

The geostrophic component \vec{u}_g is typically associated with large-scale, balanced flows that are in approximate equilibrium with the Earth's rotation. It is often dominant in the ocean's interior or in the atmosphere outside of boundary layers. The ageostrophic component \vec{u}_a is linked to unbalanced, transient, or smaller-scale processes, including wave motions or boundary layer effects.

2.3 Energy

Chapter 3

Inertia-Gravity Waves

3.1 Inertia and Gravity coupling

3.1.1 Equations and Approximations

In this part we will now study the Navier-Stokes in its integrity in order to find the wave propagation equation of Inertia-Gravity (IG) wave.

$$\begin{aligned}\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{u}) &= 0 \\ \rho \frac{\partial \vec{u}}{\partial t} + \rho \left(\vec{u} \cdot \vec{\nabla} \right) \vec{u} &= -\vec{\nabla} p + \rho \vec{g} + \mu \Delta \vec{u} - 2\rho \vec{\Omega} \wedge \vec{u}\end{aligned}$$

We will use the Boussinesq's approximation for both equations, meaning that we still have a divergence-free velocity, and that $\rho_b(z)$ and $\delta\rho$ are coupled through the vertical velocity, *i.e.* $\partial_t \delta\rho = -u_z \partial_z \rho_b$. We still consider a uniformly density stratified fluid $\partial_z \rho_b = d\rho$ and we place ourselves in a low Ekman $Ek \ll 1$ and low Rossby number $Ro \ll 1$.

The momentum equation is then written

$$\rho_0 \partial_t \vec{u} = -\vec{\nabla} \tilde{P} + \delta\rho \vec{g} - 2\rho_0 \vec{\Omega} \wedge \vec{u} \quad (3.1)$$

We can rewrite $\partial_t \delta\rho = -u_z \partial_z \rho_b$, which is called the buoyancy equation, while using N the Brunt-Väisälä frequency to obtain $\partial_t \delta\rho = \frac{\rho_0}{g} N^2 u_z$.

This gives us the following set of 5 equations to work with

$$\begin{aligned}\partial_t \vec{u} + f \hat{e}_z \wedge \vec{u} &= -\vec{\nabla} \phi + b \hat{e}_z & \partial_t b + N^2 u_z &= 0 & \vec{\nabla} \cdot \vec{u} &= 0\end{aligned} \quad (3.2)$$

where $b = -\frac{\delta\rho}{\rho} g$ and $\phi = \frac{\tilde{P}}{\rho_0}$.



3.1.2 Plane wave and dispersion relation

This is a five-equations system where we have 5 unknown variables, which means that we can solve this system for a set of plane waves

$$(\tilde{\phi}, \tilde{b}, \tilde{u}_x, \tilde{u}_y, \tilde{u}_z) = (\hat{\phi}, \hat{b}, \hat{u}_x, \hat{u}_y, \hat{u}_z) e^{-i(\vec{k} \cdot \vec{x} - \omega t)}$$

Again, this means with spectral derivatives $\partial_t = i\omega$ and $\partial_{x,y,z} = -ik_{x,y,z}$, we can rewrite the eq. (3.2)

$$\begin{aligned} i\omega u_x - f u_y &= i k_x \phi \\ i\omega u_y + f u_x &= i k_y \phi \\ i\omega u_z &= i k_z \phi + b \\ i\omega b &= -N^2 u_z \\ k_x u_x + k_y u_y + k_z u_z &= 0 \end{aligned}$$

We can replace b and u_z in the third equation by using the fourth and the fifth equations

$$-\left(i\omega + \frac{N^2}{i\omega}\right) \frac{k_x u_x + k_y u_y}{k_z^2} = i\phi$$

Then we inject that expression of ϕ in the first and the second equations

$$\begin{aligned} i\omega u_x - f u_y &= -k_x \left(i\omega + \frac{N^2}{i\omega}\right) \frac{k_x u_x + k_y u_y}{k_z^2} \\ i\omega u_y + f u_x &= -k_y \left(i\omega + \frac{N^2}{i\omega}\right) \frac{k_x u_x + k_y u_y}{k_z^2} \end{aligned}$$

Which we can reorder to express u_x in terms of u_y in both

$$\begin{aligned} \left(-\omega^2 + \frac{k_x^2}{k_z^2} (N^2 - \omega^2)\right) u_x &= \left(i\omega f - \frac{k_x k_y}{k_z^2} (N^2 - \omega^2)\right) u_y \\ \left(-\omega^2 + \frac{k_y^2}{k_z^2} (N^2 - \omega^2)\right) u_y &= \left(-i\omega f - \frac{k_x k_y}{k_z^2} (N^2 - \omega^2)\right) u_x \end{aligned}$$

Which we can regroup in one equation as

$$\begin{aligned} \frac{-i\omega f - k_y k_x (N^2 - \omega^2) / k_z^2}{-\omega^2 + k_y^2 (N^2 - \omega^2) / k_z^2} &= \frac{-\omega^2 + k_x^2 (N^2 - \omega^2) / k_z^2}{i\omega f - k_y k_x (N^2 - \omega^2) / k_z^2} \\ \omega^2 f^2 &= \omega^4 - \omega^2 \frac{k_x^2 + k_y^2}{k_z^2} (N^2 - \omega^2) \\ \omega^2 \left(\omega^2 - \frac{k_x^2 + k_y^2}{k_z^2} (N^2 - \omega^2) - f^2 \right) &= 0 \end{aligned}$$



We found the first trivial solution $\omega_0 = 0$ and two other ω_{\pm} which are given by the second term

$$\omega_{\pm}^2 = \frac{f^2 k_z^2 + N^2 (k_x^2 + k_y^2)}{k_x^2 + k_y^2 + k_z^2} = \frac{f^2 k_z^2 + N^2 k_h^2}{k^2} \quad (3.3)$$

Where $k_h^2 = k_x^2 + k_y^2$ is the horizontal wave vector.

We can easily see that ω_+ is bounded between $[f, N]$ and ω_- between $[-N, -f]$ because we have $N \approx 10 f$.

Appendix A

Vector identities

Divergence of a product

$$\vec{\nabla} \cdot (f \vec{A}) = f \vec{\nabla} \cdot \vec{A} + \vec{A} \cdot \vec{\nabla} f \quad (\text{A.1})$$

Curl of a gradient

$$\vec{\nabla} \wedge \vec{\nabla} f = 0 \quad (\text{A.2})$$

Divergence of a curl

$$\vec{\nabla} \cdot (\vec{\nabla} \wedge \vec{A}) = 0 \quad (\text{A.3})$$

Curl of a curl

$$\vec{\nabla} \wedge (\vec{\nabla} \wedge \vec{A}) = \vec{\nabla} (\vec{\nabla} \cdot \vec{A}) - \Delta \vec{A} \quad (\text{A.4})$$

Divergence of a cross product

$$\vec{\nabla} \cdot (\vec{A} \wedge \vec{B}) = \vec{B} \cdot (\vec{\nabla} \wedge \vec{A}) - \vec{A} \cdot (\vec{\nabla} \wedge \vec{B}) \quad (\text{A.5})$$

Curl of a cross product

$$\vec{\nabla} \wedge (\vec{A} \wedge \vec{B}) = (\vec{B} \cdot \vec{\nabla}) \vec{A} - (\vec{A} \cdot \vec{\nabla}) \vec{B} + \vec{A} (\vec{\nabla} \cdot \vec{B}) - \vec{B} (\vec{\nabla} \cdot \vec{A}) \quad (\text{A.6})$$

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