

# Equivalent continuum for viscoelastic metamaterials

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## Appendix A. Frequency-dependent effective material properties

In this appendix,  $\xi$  is eliminated first followed by elimination of  $\mathbf{v}$ . Dropping the subscript  ${}^2\boldsymbol{\mu}_M = {}^2\boldsymbol{\mu}$  for clarity, the effective constitutive model for momentum rate can be written by replacing the column with a summation. The first equation (33) become

$$\dot{\boldsymbol{\pi}}_M = \sum_{k=1}^3 \boldsymbol{\mu}_k \cdot \dot{\mathbf{v}}_k + \frac{1}{V} \sum_{j=1}^N \mathbf{a}_j^{(1)} \dot{\xi}_j. \quad (\text{A.1})$$

The first equation (34) is also rewritten with a summation notation for each corner  $k = 1, 2, 3$  and local resonance modes  $j = 1, \dots, N$ . Hence, it reads for each column entry  $i = 1, 2, 3$

$$\boldsymbol{\mu}_i \cdot \dot{\mathbf{u}}_M - \frac{1}{V} \sum_{k=1}^3 \mathbf{M}_{ik}^{(\text{lw})} \cdot \mathbf{v}_k + \frac{1}{V} \sum_{j=1}^N \left( \mathbf{b}_j \dot{\xi}_j - \mathbf{a}_j^{(1)} \xi_j \right) = \mathbf{0}. \quad (\text{A.2})$$

Next, the second equation (34) can be expressed for modes  $j = 1, \dots, N$ . Since the  $\underline{I}^{(\text{lr})}$  and  $\underline{\Lambda}^{(\text{lr})}$  are diagonal each column entry can be written separately

$$\boldsymbol{\alpha}_j \cdot \dot{\mathbf{u}}_M + \sum_{k=1}^3 (\mathbf{b}_{jk} \cdot \dot{\mathbf{v}}_k - \mathbf{a}_{jk} \cdot \mathbf{v}_k) + \dot{\xi}_j - i\omega_j \xi_j = 0. \quad (\text{A.3})$$

Equation (A.3) in the frequency domain reads

$$\xi_j = \frac{-\boldsymbol{\alpha}_j \cdot i\omega \mathbf{u}_M + \sum_{k=1}^3 (-i\omega \mathbf{b}_{jk} + \mathbf{a}_{jk}) \cdot \mathbf{v}_k}{(i\omega - i\omega_j)}, \quad \text{for } j = 1, 2, \dots, N. \quad (\text{A.4})$$

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and this expression is used to eliminate  $\xi_j$  from equations (A.1), leading to

$$\begin{aligned}
\pi_{\text{M}} &= \overbrace{\left[ \frac{1}{V} \sum_{j=1}^N \frac{-\boldsymbol{\alpha}_j \otimes \boldsymbol{\alpha}_j}{(\text{i}\omega - \text{i}\omega_j)} \right]}^{\boldsymbol{\delta}_1(\omega) \equiv} \cdot \text{i}\omega \mathbf{u}_{\text{M}} \\
&\quad + \sum_{k=1}^3 \overbrace{\left[ \boldsymbol{\mu}_k + \frac{1}{V} \sum_{j=1}^N \left( \frac{-\text{i}\omega \boldsymbol{\alpha}_j \otimes \mathbf{b}_{jk} + \boldsymbol{\alpha}_j \otimes \mathbf{a}_{jk}}{\text{i}\omega - \text{i}\omega_j} \right) \right]}^{\text{k-th entry of column } \underline{\boldsymbol{\delta}}_2^{\text{T}}(\omega)} \cdot \mathbf{v}_k \\
&= \boldsymbol{\delta}_1(\omega) \cdot \text{i}\omega \mathbf{u}_{\text{M}} + \underline{\boldsymbol{\delta}}_2^{\text{T}}(\omega) \cdot \underline{\mathbf{y}}
\end{aligned} \tag{A.5}$$

and the elimination of the enrichment variables  $\xi_j$  in the constitutive model (A.2) reads for corners  $i=1,2,3$

$$\mathbf{0} = \overbrace{\left[ \boldsymbol{\mu}_i + \frac{1}{V} \sum_{j=1}^N \left( \frac{-\text{i}\omega \mathbf{b}_{ji} \otimes \boldsymbol{\alpha}_j + \mathbf{a}_{ji} \otimes \boldsymbol{\alpha}_j}{\text{i}\omega - \text{i}\omega_j} \right) \right]}^{\text{i-th entry of column } \underline{\boldsymbol{\delta}}_2(\omega)} \cdot \text{i}\omega \mathbf{u}_{\text{M}} \tag{A.6}$$

$$\begin{aligned}
&\quad - \sum_{k=1}^3 \overbrace{\left[ \frac{1}{V} \mathbf{M}_{ik}^{(\text{lw})} + \frac{1}{V} \sum_{j=1}^N \left( \frac{-\omega^2 \mathbf{b}_{ji} \otimes \mathbf{b}_{jk} - \text{i}\omega (\mathbf{a}_{ji} \otimes \mathbf{b}_{jk} + \mathbf{b}_{ji} \otimes \mathbf{a}_{jk}) + \mathbf{a}_{ji} \otimes \mathbf{a}_{jk}}{\text{i}\omega - \text{i}\omega_j} \right) \right]}^{(i,k)\text{-th entry of matrix } \underline{\boldsymbol{\delta}}_4(\omega)} \cdot \mathbf{v}_k \\
&\tag{A.7}
\end{aligned}$$

or, all together

$$\mathbf{0} = \underline{\boldsymbol{\delta}}_2(\omega) \cdot \text{i}\omega \mathbf{u}_{\text{M}} + \underline{\boldsymbol{\delta}}_4(\omega) \cdot \underline{\mathbf{y}}. \tag{A.8}$$

Finally, eliminating  $\mathbf{v}_k$ , the effective density and effective 4th-order elastic tensor are

$$\pi_{\text{M}} = \overbrace{\left( \boldsymbol{\delta}_1(\omega) + \underline{\boldsymbol{\delta}}_2^{\text{T}}(\omega) \cdot \underline{\boldsymbol{\delta}}_4^{-1}(\omega) \cdot \underline{\boldsymbol{\delta}}_2(\omega) \right)}^{2\rho^{\text{eff}}(\omega) \equiv} \cdot \text{i}\omega \mathbf{u}_{\text{M}} \tag{A.9}$$

$${}^2\boldsymbol{\sigma}_{\text{M}} = \overbrace{\left( {}^4\mathbf{C}_{\text{M}} + \text{i}\omega {}^4\boldsymbol{\eta}_{\text{M}} \right)}^{\mathbf{C}^{\text{eff}}(\omega)} : \boldsymbol{\nabla}_{\text{M}} \mathbf{u}_{\text{M}}. \tag{A.10}$$

This is an alternative expression for the effective material properties given in Liupekevičius et al. [1] and carried out in the scripts in the supporting software dataset [2].

## References

- [1] Liupekevicius, R., Dommelen, J., Geers, M. & Kouznetsova, V. Equivalent continuum for viscoelastic metamaterials. *Computer Methods In Applied Mechanics And Engineering*. **445** pp. 118160 (2025)
- [2] Liupekevicius, R., Van Dommelen, J.A.W., Geers, M.G.D. & Kouznetsova, V.G. MATLAB script and COMSOL models of the article 'Equivalent continuum for viscoelastic metamaterials' [Internet]. 4TU.ResearchData; 2025. Available from: <https://data.4tu.nl/datasets/e1e12991-b957-4ca6-bd21-c59fe9d165b5/1>