



NORGES TEKNISK- NATURVITENSKAPELIGE UNIVERSITET
INSTITUTT FOR TEKNISK KYBERNETIKK

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Eksamen - TTK 4115 Lineær systemteori

Exam - TTK 4115 Linear system theory

11. desember 2009, 09:00 – 13:00

Hjelpemidler: D - Ingen trykte eller håndskrevne hjelpemidler tillatt. Bestemt, enkel kalkulator tillatt.

Supporting materials: D - No printed or handwritten material allowed. Specific, simple calculator allowed.

Oppgave 1 (20 %)

Gitt

Given:

$$\dot{x} = Ax + bu$$

$$y = Cx + Du$$

a)

La (A, B) ha styrbarhetsmatrisa:

Let (A, B) have controllability matrix:

$$\mathcal{C} = \begin{pmatrix} B & AB & \dots & A^{n-1}B \end{pmatrix}$$

Anta at \mathcal{C} har full rang. Vis at dette impliserer at styrbarhetsmatrisa $\bar{\mathcal{C}}$ til det ekvivalente systemet $(\bar{A} = PAP^{-1}, \bar{B} = PB)$, hvor P er similaritetstransformasjonen, også har full rang.

Assume that \mathcal{C} has full rank. Show that this implies that the controllability matrix $\bar{\mathcal{C}}$ of the equivalent system ($\bar{A} = PAP^{-1}, \bar{B} = PB$), with P being the equivalence transformation, also has full rank.

b)

La:

Let:

$$A = \begin{pmatrix} -1 & -1 \\ -4 & 2 \end{pmatrix}$$

Finn egenverdiene og tilhørende egenvektorer til A .

Find the eigenvalues and the corresponding eigenvectors of A .

c)

La:

Let:

$$B = \begin{pmatrix} 0 \\ 1 \end{pmatrix}, C = \begin{pmatrix} 1 & 0 \end{pmatrix}, D = \begin{pmatrix} 0 & 0 \end{pmatrix}$$

Transformer systemet til diagonalform, ved hjelp av similaritetstransformasjonen $\bar{x} = Px$.

Transform the system to diagonal form, by using the equivalence transformation $\bar{x} = Px$.

d)

Anta konstant pådrag $u \equiv 1$. Hva blir løsningen $y(t)$ for $t = 1$ når $x(0) = x_0$? Unngå integral i svaret.

Assume a constant input $u \equiv 1$. What is the solution $y(t)$ at $t = 1$ when $x(0) = x_0$? Avoid using integrals in the answer.

Oppgave 2 (20 %)

Gitt følgende system:

Given the following system:

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ 0 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} + \begin{pmatrix} 0 \\ 1 \end{pmatrix} u$$

a)

Er systemet BIBO-stabilt? Er systemet styrbart? Forklar!

Is the system BIBO-stable? Is the system controllable? Explain!

b)

La α, β, γ være positive konstanter. Vi ønsker å minimere kostfunksjonen:

Let α, β, γ be positive constants. We wish to minimize the cost function:

$$J = \int_0^{t_e} \alpha x_1^2 + \beta x_2^2 + \gamma u^2 dt, \quad t_e > 0 \quad (1)$$

La $x = (x_1, x_2)^T$. Skriv kostfunksjonen på formen:

Let $x = (x_1, x_2)^T$. Write the cost function on the form:

$$J = \int_0^{t_e} x^T Q x + u^T R u dt, \quad t_e > 0 \quad (2)$$

Hva blir Q ? Hva blir R ? Hvilken effekt har det å øke henholdsvis α , β og γ ?
What is Q ? What is R ? What is the effect of increasing α , β and γ , respectively?

c)

La t_e i (2) være endelig. Blir den resulterende regulatoren fra å løse optimaliseringsproblemet tidsvarierende eller tidsinvariant? Forklar!

Let t_e in (2) be finite. Will the resulting controller from solving the optimization problem be timevarying or timeinvariant? Explain!

d)

La $\alpha = \beta = \gamma = 1$ i (1). Gitt en positiv semidefinit matrise:

Let $\alpha = \beta = \gamma = 1$ in (1). Given a positive semidefinite matrix:

$$P = \begin{pmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{pmatrix}.$$

Finn den stasjonære verdien av P ved å løse Ricatti-likningen:

Find the stationary value of P by solving the Ricatti equation:

$$0 = PA + A^T P + Q - PBR^{-1}B^T P$$

e)

Bruk P fra forrige oppgave til å vise at systemet med tilbakekobling $u = -R^{-1}B^T P x$ er asymptotisk stabilt.

Use P from the previous exercise to show that the system with feedback $u = -R^{-1}B^T P x$ is asymptotically stable.

Oppgave 3 (35 %)

Gitt et signal med autokorrelasjonsfunksjon:

Consider a signal with autocorrelation function:

$$R_s(\tau) = \frac{8}{3} \exp^{-\frac{3}{4}|\tau|}$$

La målinga av signalet være addert med støy med autokorrelasjonsfunksjon:

Let the measurement of the signal be corrupted with additive noise with autocorrelation function:

$$R_n(\tau) = 4\delta(\tau)$$

a)

Vis at systemet kan skrives som:

Show that the system can be written as:

$$\begin{aligned}\dot{x} &= -\frac{3}{4}x + 2u \\ z &= x + v,\end{aligned}$$

hvor u er enhets hvit støy og v er hvit støy med kovariansparameter $R = 4$.

where u is unity white noise and v is white noise with covariance parameter $R = 4$.

b)

Et kontinuerlig Kalman filter skal designes for systemet. Vis at kovariansfeilmatrisen tilfredsstiller:

A continuous Kalman filter is to be designed for the system. Show that the error covariance matrix satisfies:

$$\dot{P} = -\frac{1}{4}P^2 - \frac{3}{2}P + 4$$

c)

La $P(0) = 0$. Bestem $P(t)$. (Avhengig av hvordan du velger å løse oppgaven, kan du finne det nyttig å vite at $a^2 + 6a - 16 = (a + 8)(a - 2)$ eller at $\cos ix = \cosh x = 1/2(e^x + e^{-x})$ og at $-i \sin ix = \sinh x = 1/2(e^x - e^{-x})$).

Let $P(0) = 0$. Find $P(t)$. (Depending on your solution method, you might find it useful to know that $a^2 + 6a - 16 = (a + 8)(a - 2)$ or that $\cos ix = \cosh x = 1/2(e^x + e^{-x})$ and that $-i \sin ix = \sinh x = 1/2(e^x - e^{-x})$).

d)

Hva blir Kalman-forsterkninga K i det stasjonære tilfellet?

What is the Kalman gain K in the stationary case?

Oppgave 4 (25 %)

Gitt følgende system:

Given the following system:

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 \\ -4 & -4 & 0 \\ 2 & 0 & 3 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} + \begin{pmatrix} 0 & 1 \\ 1 & 0 \\ 0 & 0 \end{pmatrix} \begin{pmatrix} u_1 \\ u_2 \end{pmatrix}$$

$$\begin{pmatrix} y_1 \\ y_2 \end{pmatrix} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix}$$

a)

Finn overføringsfunksjonsmatrisa $G(s)$ til systemet.

Find the transfer function matrix $G(s)$ of the system.

b)

Bruk likningene i vedlegget til å finne en annen realisering (A_m, B_m, C_m, D_m) av $G(s)$.

Use the equations in the appendix to find another realization (A_m, B_m, C_m, D_m) of $G(s)$.

c)

Gitt:

Given:

$$A_{m1} = \begin{pmatrix} 0 & 1 \\ -4 & -4 \end{pmatrix}, \quad B_{m1} = \begin{pmatrix} 0 & 1 \\ 1 & 0 \end{pmatrix}, \quad C_{m1} = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}, \quad D_{m1} = \begin{pmatrix} 0 & 0 \\ 0 & 1 \end{pmatrix}$$

Er $(A_{m1}, B_{m1}, C_{m1}, D_{m1})$ også en realisering av $G(s)$? Hvorfor/Hvorfor ikke?

Is $(A_{m1}, B_{m1}, C_{m1}, D_{m1})$ also a realization of $G(s)$? Why/Why not?

Vedlegg til eksamen (noen nyttige formler og uttrykk):

Appendix to the exam (some useful formulas and expressions):

$$\begin{aligned}
 x(t) &= e^{At}x(0) + \int_0^t e^{A(t-\tau)}Bu(\tau)d\tau \\
 x(k) &= A^kx(0) + \sum_{m=0}^{k-1} A^{k-1-m}Bu(m) \\
 A^{-1} &= \frac{adj(A)}{\det(A)} \\
 \det(A) &= \sum_{i=1}^n a_{ij}c_{ij} \\
 adj(A) &= \{c_{ij}\}^T \\
 c_{ij} &= (-1)^{i+j}\det(A_{ij}) \quad (\text{kofaktor}), \quad A_{ij} = \text{submatrix to } A \\
 \mathcal{C} &= (B \ AB \ A^2B \ \dots \ A^{n-1}B) \\
 \mathcal{O} &= \begin{pmatrix} C \\ CA \\ CA^2 \\ \vdots \\ CA^{n-1} \end{pmatrix} \\
 G(s) &= C(sI - A)^{-1}B + D \\
 G(z) &= C(zI - A)^{-1}B + D \\
 \mathbf{G}(\mathbf{s}) &= \mathbf{G}(\infty) + \mathbf{G}_{\text{sp}}(\mathbf{s}) \\
 d(s) &= s^r + \alpha_1 s^{r-1} + \dots + \alpha_{r-1}s + \alpha_r \\
 \mathbf{G}_{\text{sp}}(s) &= \frac{1}{d(s)}[\mathbf{N}_1 s^{r-1} + \mathbf{N}_2 s^{r-2} + \dots + \mathbf{N}_{r-1}s + \mathbf{N}_r] \\
 \dot{\mathbf{x}} &= \begin{bmatrix} -\alpha_1 \mathbf{I}_p & -\alpha_2 \mathbf{I}_p & \dots & -\alpha_{r-1} \mathbf{I}_p & -\alpha_r \mathbf{I}_p \\ \mathbf{I}_p & \mathbf{0} & \dots & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{I}_p & \dots & \mathbf{0} & \mathbf{0} \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ \mathbf{0} & \mathbf{0} & \dots & \mathbf{I}_p & \mathbf{0} \end{bmatrix} \mathbf{x} + \begin{bmatrix} \mathbf{I}_p \\ \mathbf{0} \\ \mathbf{0} \\ \vdots \\ \mathbf{0} \end{bmatrix} \mathbf{u} \\
 \mathbf{y} &= [\mathbf{N}_1 \ \mathbf{N}_2 \ \dots \ \mathbf{N}_{r-1} \ \mathbf{N}_r] \mathbf{x} + \mathbf{G}(\infty) \mathbf{u}
 \end{aligned}$$

Discrete-time Kalman filter:

$$\begin{aligned}
 \mathbf{x}_{k+1} &= \mathbf{\Phi}_k \mathbf{x}_k + \mathbf{w}_k \\
 \mathbf{z}_k &= \mathbf{H}_k \mathbf{x}_k + \mathbf{v}_k \\
 E[\mathbf{w}_k \mathbf{w}_i^T] &= \begin{cases} \mathbf{Q}_k, & i = k \\ 0, & i \neq k \end{cases} \\
 E[\mathbf{v}_k \mathbf{v}_i^T] &= \begin{cases} \mathbf{R}_k, & i = k \\ 0, & i \neq k \end{cases} \\
 E[\mathbf{w}_k \mathbf{v}_i^T] &= 0, \forall i, k \\
 \mathbf{P}_k^- &= E[\mathbf{e}_k^- \mathbf{e}_k^{-T}] \\
 \mathbf{P}_k &= E[\mathbf{e}_k \mathbf{e}_k^T] = (\mathbf{I} - \mathbf{K}_k \mathbf{H}_k) \mathbf{P}_k^- (\mathbf{I} - \mathbf{K}_k \mathbf{H}_k)^T + \mathbf{K}_k \mathbf{R}_k \mathbf{K}_k^T \\
 \mathbf{K}_k &= \mathbf{P}_k^- \mathbf{H}_k^T (\mathbf{H}_k \mathbf{P}_k^- \mathbf{H}_k^T + \mathbf{R}_k)^{-1} \\
 \mathbf{P}_{k+1}^- &= \mathbf{\Phi}_k \mathbf{P}_k \mathbf{\Phi}_k^T + \mathbf{Q}_k
 \end{aligned}$$

Continuous-time Kalman filter:

$$\begin{aligned}
 \dot{\mathbf{x}} &= \mathbf{F}\mathbf{x} + \mathbf{G}\mathbf{u} \\
 \mathbf{z} &= \mathbf{H}\mathbf{x} + \mathbf{v} \\
 E[\mathbf{u}(t)\mathbf{u}(\tau)^T] &= \mathbf{Q}\delta(t - \tau) \\
 E[\mathbf{v}(t)\mathbf{v}(\tau)^T] &= \mathbf{R}\delta(t - \tau) \\
 E[\mathbf{u}(t)\mathbf{v}(\tau)^T] &= 0 \\
 \mathbf{K} &= \mathbf{P}\mathbf{H}^T \mathbf{R}^{-1} \\
 \dot{\mathbf{P}} &= \mathbf{F}\mathbf{P} + \mathbf{P}\mathbf{F}^T - \mathbf{P}\mathbf{H}^T \mathbf{R}^{-1} \mathbf{H}\mathbf{P} + \mathbf{G}\mathbf{Q}\mathbf{G}^T, \quad \mathbf{P}(0) = \mathbf{P}_0
 \end{aligned}$$

Auto-correlation:

$$\begin{aligned}
 R_X(\tau) &= E[X(t)X(t + \tau)] \text{ (Stationary process)} \\
 R_X(t_1, t_2) &= E[X(t_1)X(t_2)] \text{ (Non-stationary process)} \\
 Y(s) &= G(s)U(s) \Rightarrow \\
 R_y(t_1, t_2) &= E[y(t_1)y(t_2)] \\
 &= \int_0^{t_2} \int_0^{t_1} g(\xi)g(\eta) E[u(t_1 - \xi)u(t_2 - \eta)] d\xi d\eta \text{ (Transient analysis)}
 \end{aligned}$$

Laplace transform pairs:

$f(t)$	\Longleftrightarrow	$F(s)$
1	\Longleftrightarrow	$\frac{1}{s}$
e^{-at}	\Longleftrightarrow	$\frac{1}{s+a}$
t	\Longleftrightarrow	$\frac{1}{s^2}$
t^2	\Longleftrightarrow	$\frac{2}{s^3}$
te^{-at}	\Longleftrightarrow	$\frac{1}{(s+a)^2}$
$\sin \omega t$	\Longleftrightarrow	$\frac{\omega}{s^2 + \omega^2}$
$\cos \omega t$	\Longleftrightarrow	$\frac{s}{s^2 + \omega^2}$
