

Solution Suggestion  
Exam - TTK4115 Linear System Theory  
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EIG (2009-12-14)

**Problem 1**

- a) The proof is similar to the proof of Theorem 6.2 in Chen. The controllability matrix of  $\bar{\mathcal{C}}$  of the transformed system is:

$$\begin{aligned}\bar{\mathcal{C}} &= [\bar{B} \quad \bar{A}\bar{B} \quad \dots \quad \bar{A}^{n-1}\bar{B}] \\ &= [PB \quad PAP^{-1}PB \quad \dots \quad (PAP^{-1})^{n-1}PB] \\ &= [PB \quad PAP^{-1}PB \quad \dots \quad PA^{n-1}P^{-1}PB] \\ &= P[B \quad AB \quad \dots \quad A^{n-1}B] \\ &= PC\end{aligned}$$

Since the rank of a matrix will not change after pre- or postmultiplication by a nonsingular matrix, and  $P$  is nonsingular, the rank of  $\bar{\mathcal{C}}$  is equal to the rank of  $\mathcal{C}$ . Since  $\mathcal{C}$  was assumed to have full rank, so will  $\bar{\mathcal{C}}$ .

- b) To find the eigenvalues of  $A$ , we solve the equation  $\det(\lambda I - A) = 0$ . We find that

$$\begin{aligned}\det(\lambda I - A) &= \begin{vmatrix} \lambda + 1 & 1 \\ 4 & \lambda - 2 \end{vmatrix} \\ &= \lambda^2 - \lambda - 6 \\ &= (\lambda + 2)(\lambda - 3)\end{aligned}$$

The eigenvalues are therefore  $\lambda_1 = -2$  and  $\lambda_2 = 3$ . The eigenvector  $q_1 = (q_{11}, q_{12})^\top$  corresponding to  $\lambda_1$  is found by solving  $(A - \lambda_1 I)q_1 = 0$ . Since

$$\begin{bmatrix} 1 & -1 \\ -4 & 4 \end{bmatrix} \begin{bmatrix} q_{11} \\ q_{12} \end{bmatrix} = \begin{bmatrix} q_{11} - q_{12} \\ -4q_{11} + 4q_{12} \end{bmatrix},$$

we can pick  $q_1 = (1, 1)^\top$ . In a similar manner we find the eigenvector  $q_2 = (1/4, -1)^\top$ , corresponding to  $\lambda_2$ .

- c) As announced on the exam  $D$  should be taken as  $D = 0$ . The transformed system can be written as

$$\begin{aligned}\dot{\bar{x}} &= \bar{A}\bar{x} + \bar{B}u \\ y &= \bar{C}\bar{x} + \bar{D}u\end{aligned}$$

where  $\bar{A} = PAP^{-1}$ ,  $\bar{B} = PB$ ,  $\bar{C} = CP^{-1}$  and  $\bar{D} = D$ . We define  $Q := [q_1 \quad q_2]$  and take  $P = Q^{-1}$ . We find that

$$P = \begin{bmatrix} \frac{4}{5} & \frac{1}{5} \\ \frac{4}{5} & -\frac{4}{5} \end{bmatrix}.$$

Performing the matrix calculations gives

$$\begin{aligned}\dot{\bar{x}} &= \begin{bmatrix} -2 & 0 \\ 0 & 3 \end{bmatrix} \bar{x} + \begin{bmatrix} 1/5 \\ -4/5 \end{bmatrix} u \\ y &= \begin{bmatrix} 1 & 1/4 \end{bmatrix} \bar{x}\end{aligned}$$

d) Using the formula in the appendix, we find that

$$\begin{aligned}\bar{x}(t) &= \begin{bmatrix} e^{-2t} & 0 \\ 0 & e^{3t} \end{bmatrix} \bar{x}(0) + \int_0^t \begin{bmatrix} e^{-2(t-\tau)} & 0 \\ 0 & e^{3(t-\tau)} \end{bmatrix} \begin{bmatrix} 1/5 \\ -4/5 \end{bmatrix} u(\tau) d\tau \\ &= \begin{bmatrix} \bar{x}_1(0) e^{-2t} \\ \bar{x}_2(0) e^{3t} \end{bmatrix} + \int_0^t \begin{bmatrix} 1/5 e^{-2(t-\tau)} \\ -4/5 e^{3(t-\tau)} \end{bmatrix} u(\tau) d\tau\end{aligned}$$

Since  $y(t) = (1, 1/4) \bar{x}(t)$ , and  $u \equiv 1$ , we get that for  $x_0 = (x_{10}, x_{20})^\top$ ,

$$\begin{aligned}y(1) &= \bar{x}_1(0) e^{-2} + 1/4 \bar{x}_2(0) e^3 + \frac{1}{5} \int_0^1 e^{-2(1-\tau)} d\tau - \frac{1}{5} \int_0^1 e^{3(1-\tau)} d\tau \\ &= \bar{x}_1(0) e^{-2} + \frac{1}{4} \bar{x}_2(0) e^3 + \frac{1}{5} \int_0^1 e^{-2(1-\tau)} d\tau - \frac{1}{5} \int_0^1 e^{3(1-\tau)} d\tau \\ &= \left( \frac{4}{5} x_{10} + \frac{1}{5} x_{20} \right) e^{-2} + \frac{1}{4} \left( \frac{4}{5} x_{10} - \frac{4}{5} x_{20} \right) e^3 + \frac{1}{5} \left( \frac{1}{2} - \frac{1}{2} e^{-2} \right) - \frac{1}{5} \left( \frac{1}{3} e^3 - \frac{1}{3} \right) \\ &= \left( \frac{4}{5} e^{-2} + \frac{1}{5} e^3 \right) x_{10} + \frac{1}{5} (e^{-2} - e^3) x_{20} - \frac{1}{10} e^{-2} - \frac{1}{15} e^3 + \frac{1}{6}\end{aligned}$$

## Problem 2

a) With output  $y = x_1$ , the system has transferfunction

$$G(s) = \frac{1}{s^2},$$

that is, two poles in the origin. By Theorem 5.3 in Chen, the system is not BIBO stable. The system is controllable, since the controllability matrix

$$\mathcal{C} = [B \quad AB] = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}$$

has full rank.

b) By comparing the terms we find that

$$Q = \begin{bmatrix} \alpha & 0 \\ 0 & \beta \end{bmatrix}, \quad R = \gamma.$$

Increasing  $\alpha$  and  $\beta$  penalizes the state variables  $x_1$  and  $x_2$ , respectively. Increasing  $\gamma$  penalizes the control efforts.

c) The resulting controll will be timevarying, since  $t_e$  is finite.

d) We find that

$$A = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \quad R = 1, \quad Q = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

Inserting into the Ricatti equation, we find that.

$$\begin{bmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{bmatrix} \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} + \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}^T \begin{bmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} - \begin{bmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix}^T \begin{bmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{bmatrix}$$

$$\begin{bmatrix} 0 & p_{11} \\ 0 & p_{12} \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ p_{11} & p_{12} \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} - \begin{bmatrix} p_{12}^2 & p_{12}p_{22} \\ p_{12}p_{22} & p_{22}^2 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$

or

$$\begin{bmatrix} 1 - p_{12}^2 & p_{11} - p_{12}p_{22} \\ p_{11} - p_{12}p_{22} & -p_{22}^2 + 2p_{12} + 1 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}.$$

We have the following equation

$$\begin{aligned} 1 - p_{12}^2 &= 0 \\ -p_{22}^2 + 2p_{12} + 1 &= 0 \\ p_{11} - p_{12}p_{22} &= 0 \end{aligned}$$

The first equation implies that  $p_{12} = \pm 1$ . If  $p_{12} = -1$ , we find from the second equation that  $p_{22} = \pm i$ . We are only interested in real solutions, so  $p_{12} = 1$ . Inserting  $p_{12} = 1$  into the second equation, we find that  $p_{22} = \pm\sqrt{3}$ . For  $p_{22} = \sqrt{3}$ , we get from the last equation that  $p_{11} = \sqrt{3}$ , were as for  $p_{22} = -\sqrt{3}$ , we get that  $p_{11} = -\sqrt{3}$ . Possible solutions are therefore

$$P = \begin{bmatrix} \sqrt{3} & 1 \\ 1 & \sqrt{3} \end{bmatrix} \quad \text{or} \quad P = \begin{bmatrix} -\sqrt{3} & 1 \\ 1 & -\sqrt{3} \end{bmatrix}.$$

We are only interested in the positive (semi-) definite solution, so

$$P = \begin{bmatrix} \sqrt{3} & 1 \\ 1 & \sqrt{3} \end{bmatrix}$$

e) The optimal control is

$$u = - \begin{bmatrix} 1 & \sqrt{3} \end{bmatrix} x.$$

The closed-loop system is

$$\begin{aligned} \dot{x} &= \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} x - \begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} 1 & \sqrt{3} \end{bmatrix} x \\ &= \begin{bmatrix} 0 & 1 \\ -1 & -\sqrt{3} \end{bmatrix} x \end{aligned}$$

The characteristic polynomial of the closed-loop system is  $\Delta(\lambda) = \lambda(\lambda + \sqrt{3}) + 1$ . By solving  $\Delta(\lambda) = 0$ , we find that  $\lambda = -\frac{1}{2}\sqrt{3} \pm \frac{1}{2}i$ . The eigenvalues are in the left hand plane, and therefore the system is asymptotically stable.

## Problem 3

a) Realizing that the process signal is on the form

$$R_s(\tau) = \sigma^2 e^{-\beta|\tau|}$$

with mean-square value  $\sigma^2 = 8/3$  and time constant  $1/\beta = 4/3$ , we recognize the process as a Gauss-Markov process, which power spectral desity function is

$$S_s(s) = \frac{2\sigma^2\beta}{-s^2 + \beta^2}.$$

The noise signal should be recognized as white noise, with spectral amplitude  $A = 4$ . The corresponding power spectral function is

$$S_n(s) = A.$$

Spectral factorization gives

$$\begin{aligned} S_s(s) &= S^+(s) \cdot S^-(s) \\ &= \frac{\sqrt{2\frac{8}{3}\frac{3}{4}}}{s + \frac{3}{4}} \cdot \frac{\sqrt{2\frac{8}{3}\frac{3}{4}}}{-s + \frac{3}{4}} \\ &= \frac{2}{s + \frac{3}{4}} \cdot \frac{2}{-s + \frac{3}{4}} \end{aligned}$$

$S^+(s)$  is the shaping filter from the unity white noise input  $u$  to the state  $x$ , so

$$\frac{X(s)}{U(s)} = \frac{2}{s + \frac{3}{4}}$$

or

$$X\left(s + \frac{3}{4}\right) = 2U,$$

which in time-domain becomes

$$\dot{x} = -\frac{3}{4}x + 2u$$

Since the additive measurement is white, no augmentation of the state vector is required, and the measurement is

$$z = x + v.$$

Since  $u$  is unity white noise,  $Q = 1$  and since  $v$  is white noise of amplitude 4,  $R = 4$ .

- b) Comparing the state model with the model in the appendix, we recognize that  $G = 2$ ,  $H = 1$  and  $F = -\frac{3}{4}$ . Inserting for  $H, F, Q$  and  $R$  into the differential Riccati equation gives:

$$\dot{P} = -\frac{1}{4}P^2 - \frac{3}{2}P + 4.$$

- c) We rewrite

$$\begin{aligned} \dot{P} &= -\frac{1}{4}(P^2 + 6P - 16) \\ &= -\frac{1}{4}(P + 8)(P - 2). \end{aligned}$$

We write  $\dot{P} = dP/dt$ , and separate the variables:

$$\frac{dP}{(P + 8)(P - 2)} = -\frac{1}{4}dt, \tag{1}$$

Note that,

$$\begin{aligned} \frac{dP}{(P + 8)(P - 2)} &= \frac{1}{10} \left( \frac{dP(P + 8)}{(P + 8)(P - 2)} - \frac{dP(P - 2)}{(P + 8)(P - 2)} \right) \\ &= \frac{1}{10} \left( \frac{dP}{(P - 2)} - \frac{dP}{(P + 8)} \right) \end{aligned}$$

Inserting into (1), rearranging terms and taking the integral of both sides, gives

$$\int_{P(t_0)}^{P(t)} \frac{dP}{(P-2)} - \int_{P(t_0)}^{P(t)} \frac{dP}{(P+8)} = -\frac{5}{2} \int_{t_0}^t 1dt$$

Calculating the integrals, gives

$$\begin{aligned} \ln(P(t) - 2) - \ln(P(t_0) - 2) - \ln(P(t) + 8) + \ln(P(t_0) + 8) &= -\frac{5}{2}(t - t_0), \\ \implies \ln \frac{P(t) - 2}{P(t) + 8} \frac{P(t_0) + 8}{P(t_0) - 2} &= -\frac{5}{2}(t - t_0), \\ \implies \frac{P(t) - 2}{P(t) + 8} \frac{P(t_0) + 8}{P(t_0) - 2} &= e^{-\frac{5}{2}(t-t_0)}. \end{aligned}$$

Solving for  $P(t)$  gives.

$$P(t) = \frac{2 \left( \frac{P(t_0)+8}{P(t_0)-2} + 4e^{-\frac{5}{2}(t-t_0)} \right)}{\frac{P(t_0)+8}{P(t_0)-2} - e^{-\frac{5}{2}(t-t_0)}}$$

Inserting  $P(t_0) = P(0) = 0$ , gives

$$\begin{aligned} P(t) &= \frac{2 \left( -4 + 4e^{-\frac{5}{2}t} \right)}{-4 - e^{-\frac{5}{2}t}} \\ &= 8 \frac{\left( 1 - e^{-\frac{5}{2}t} \right)}{4 + e^{-\frac{5}{2}t}}. \end{aligned} \tag{2}$$

Another possibility is to transform the nonlinear differential Ricatti equation into a system of linear equations. Assume that  $P$  can be written on product form  $P = XZ^{-1}$  with  $Z(0) = I$ . Then the  $X$  and  $Z$  satisfy

$$\begin{aligned} \dot{X} &= FX + GQG^T Z, & X(0) &= P_0 \\ \dot{Z} &= H^T R^{-1} H X - F^T Z, & Z(0) &= I. \end{aligned}$$

Inserting for  $F, G, Q, H$  and  $R$  we get

$$\begin{aligned} \dot{X} &= -\frac{3}{4}X + 4Z \\ \dot{Z} &= \frac{1}{4}X + \frac{3}{4}Z \end{aligned}$$

or by Laplace transform

$$\begin{aligned} X(s) \cdot s - P_0 + \frac{3}{4}X(s) &= 4Z(s) \implies X(s) = \frac{4Z(s) + P_0}{s + \frac{3}{4}} \\ Z(s) \cdot s - 1 - \frac{3}{4}Z(s) &= \frac{1}{4}X(s) \implies Z(s) = \frac{1 + \frac{1}{4}X(s)}{s - \frac{3}{4}} \end{aligned}$$

Solving for  $X(s)$  and  $Z(s)$ , we get after some intermediate calculations that:

$$\begin{aligned} X(s) &= \frac{P_0 s + 4 - P_0 \frac{3}{4}}{s^2 - \left(\frac{5}{4}\right)^2} \\ Z(s) &= \frac{s + \frac{1}{4}(P_0 + 3)}{s^2 - \left(\frac{5}{4}\right)^2} \end{aligned}$$

To use the Laplace table in the appendix we rewrite

$$\begin{aligned} X(s) &= \frac{P_0 s + \frac{5i}{4} \frac{4}{5i} (4 - P_0 \frac{3}{4})}{s^2 + (\frac{5}{4}i)^2} \\ Z(s) &= \frac{s + \frac{5}{4i} \frac{4}{20i} (P_0 + 3)}{(s^2 + (\frac{5}{4}i)^2)} \end{aligned}$$

and find that

$$\begin{aligned} x(t) &= P_0 \cos \frac{5}{4}it + \frac{4}{5i} \left(4 - P_0 \frac{3}{4}\right) \sin \frac{5}{4}it \\ &= \frac{P_0}{2} (e^{\frac{5}{4}t} + e^{-\frac{5}{4}t}) + \frac{2}{5} \left(4 - P_0 \frac{3}{4}\right) (e^{\frac{5}{4}t} - e^{-\frac{5}{4}t}) \\ &= \frac{1}{20} e^{\frac{5}{4}t} (4P_0 + 32) + \frac{1}{5} e^{-\frac{5}{4}t} (4P_0 - 8) \end{aligned}$$

and that

$$\begin{aligned} z(t) &= \cos \frac{5}{4}it + \frac{4}{20i} (P_0 + 3) \sin \frac{5}{4}it \\ &= \frac{1}{2} (e^{\frac{5}{4}t} + e^{-\frac{5}{4}t}) + \frac{1}{10} (P_0 + 3) (e^{\frac{5}{4}t} - e^{-\frac{5}{4}t}) \\ &= \frac{1}{10} (P_0 + 8) e^{\frac{5}{4}t} - \frac{1}{10} (P_0 - 2) e^{-\frac{5}{4}t} \end{aligned}$$

Using that  $P = XZ^{-1}$ , and  $P(0) = 0$ , we get that

$$\begin{aligned} P(t) &= \frac{\frac{1}{20} e^{\frac{5}{4}t} (4P_0 + 32) + \frac{1}{5} e^{-\frac{5}{4}t} (4P_0 - 8)}{\frac{1}{10} (P_0 + 8) e^{\frac{5}{4}t} - \frac{1}{10} (P_0 - 2) e^{-\frac{5}{4}t}} \\ &= \frac{8 (e^{\frac{5}{4}t} - e^{-\frac{5}{4}t}) e^{-\frac{5}{4}t}}{(4e^{\frac{5}{4}t} + e^{-\frac{5}{4}t}) e^{-\frac{5}{4}t}} \\ &= \frac{8 (1 - e^{-\frac{5}{2}t})}{(4 + e^{-\frac{5}{2}t})} \end{aligned}$$

(The introduction of  $\exp(-5/4t) / \exp(5/4t)$  in the second to last equation were made to get  $P(t)$  at the same form as in (2).

- d) The Kalman gain in the stationary case is  $K_\infty = P_\infty H^\top R^{-1}$ , where  $P_\infty = \lim_{t \rightarrow \infty} P(t)$  is found using the answer in the previous exercise or by solving the algebraic Ricatti equation:

$$0 = -\frac{1}{4} (P_\infty + 8) (P_\infty - 2).$$

The positive solution  $P_\infty = 2$ , gives  $K_\infty = 1/2$ .

## Problem 4

- a) The transfer function matrix is given as

$$G(s) = C \underbrace{(sI - A)^{-1}}_{\Omega} B + D.$$

Since  $D$  is the zero matrix, and since most of the elements of  $B$  and  $C$  are zero, we only need to calculate some of the elements of  $\Omega$  to find  $G(s)$ :

$$\begin{aligned} G(s) &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} \omega_{11} & \omega_{12} & \omega_{13} \\ \omega_{21} & \omega_{22} & \omega_{23} \\ \omega_{31} & \omega_{32} & \omega_{33} \end{bmatrix} \begin{bmatrix} 0 & 1 \\ 1 & 0 \\ 0 & 0 \end{bmatrix} \\ &= \begin{bmatrix} \omega_{12} & \omega_{11} \\ \omega_{22} & \omega_{21} \end{bmatrix} \end{aligned}$$

Using the formula in the appendix

$$\omega_{ij} = \frac{c_{ji}}{\det(sI - A)} = \frac{(-1)^{i+j} \det[sI - A]_{ji}}{|(sI - A)|}$$

where  $[sI - A]_{ji}$  is the submatrix you get by removing row  $j$  and column  $i$  of  $sI - A$ . First we find that

$$\begin{aligned} sI - A &= \begin{bmatrix} s & 0 & 0 \\ 0 & s & 0 \\ 0 & 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 1 & 0 \\ -4 & -4 & 0 \\ 2 & 0 & 3 \end{bmatrix} \\ &= \begin{bmatrix} s & -1 & 0 \\ 4 & s+4 & 0 \\ -2 & 0 & s-3 \end{bmatrix} \end{aligned}$$

and that  $\det(sI - A) = s(s+4)(s-3) + 4(s-3) = (s-3)(s+2)^2$ . Furthermore,

$$\begin{aligned} \omega_{12} &= \frac{(-1)^3 \begin{vmatrix} -1 & 0 \\ 0 & s-3 \end{vmatrix}}{(s-3)(s+2)^2} \\ &= \frac{s-3}{(s-3)(s+2)^2} \\ &= \frac{1}{(s+2)^2}, \end{aligned}$$

$$\begin{aligned} \omega_{11} &= \frac{(-1)^2 \begin{vmatrix} s+4 & 0 \\ 0 & s-3 \end{vmatrix}}{(s-3)(s+2)^2} \\ &= \frac{s+4}{(s+2)^2} \end{aligned}$$

$$\begin{aligned} \omega_{22} &= \frac{(-1)^4 \begin{vmatrix} s & 0 \\ -2 & s-3 \end{vmatrix}}{(s-3)(s+2)^2} \\ &= \frac{s}{(s+2)^2} \end{aligned}$$

$$\begin{aligned} \omega_{21} &= \frac{(-1)^3 \begin{vmatrix} 4 & 0 \\ -2 & s-3 \end{vmatrix}}{(s-3)(s+2)^2} \\ &= \frac{-4}{(s+2)^2} \end{aligned}$$

Hence,

$$G(s) = \frac{1}{(s+2)^2} \begin{bmatrix} 1 & s+4 \\ s & -4 \end{bmatrix}$$

b) To keep the notation consistent with the one in the appendix, we define  $\hat{G}(s) = G(s)$ . We find that

$$d(s) = (s+2)^2 = s^2 + 4s + 4.$$

Comparing with the expression in the appendix,  $d(s) = s^r + \alpha_1 s^{r-1} + \dots + \alpha_{r-1} s + \alpha_r$ , we find that  $r = 2$ ,  $\alpha_1 = 4$  and  $\alpha_2 = 4$ .  $\hat{G}(s)$  is strictly proper, hence  $\hat{G}_\infty(s) = 0$ , and  $\hat{G}_{sp}(s) = \hat{G}(s)$ . We can express  $\hat{G}_{sp}(s)$  as

$$\hat{G}_{sp}(s) = \frac{1}{d(s)} \left[ \underbrace{\begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}}_{N_1} s + \underbrace{\begin{bmatrix} 1 & 4 \\ 0 & -4 \end{bmatrix}}_{N_2} \right].$$

We end up with the following realization using the equations in the appendix:

$$\begin{aligned} \dot{x} &= \begin{bmatrix} -4 & 0 & -4 & 0 \\ 0 & -4 & 0 & -4 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} x + \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} u \\ y &= \begin{bmatrix} 0 & 1 & 1 & 4 \\ 1 & 0 & 0 & -4 \end{bmatrix} x \end{aligned}$$

c) No,  $(A_{m_1}, B_{m_1}, C_{m_1}, D_{m_1})$  is no realization of  $G(s)$ , which can be seen from these calculations:

$$\begin{aligned} G_{m_1}(s) &= C_{m_1}(sI - A_{m_1})^{-1} B_{m_1} + D_{m_1} \\ &= \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} s & -1 \\ 4 & s+4 \end{bmatrix}^{-1} \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix} \\ &= \frac{1}{s^2 + 4s + 4} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} s+4 & 1 \\ 4 & s \end{bmatrix} \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix} \\ &= \frac{1}{s^2 + 4s + 4} \begin{bmatrix} 1 & s+4 \\ s & 4 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix} \\ &= G(s) + \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix} \\ &\neq G(s) \end{aligned}$$