

Emnekode / Subject: TTK4115

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$$\text{Let } \ddot{x}_1 = \dot{\varphi}, \quad x_2 = \ddot{\varphi} = \ddot{x}_1$$

Assuming $|\dot{\varphi}|$ is small, we approximate

$$|\dot{\varphi}| \dot{\varphi} = \text{sign}(\dot{\varphi}) |\dot{\varphi}|^2 \approx 0$$

and get

$$\begin{aligned} \ddot{x}_2 &= \ddot{\dot{\varphi}} = -\frac{d}{j} |\dot{\varphi}| \dot{\varphi} - \frac{k}{j} \varphi + \frac{v}{j} u^2 \\ &\approx -\frac{k}{j} x_1 + \frac{v}{j} u^2 \end{aligned}$$

Linearize: ~~around zero~~

$$\frac{d\ddot{x}_2}{du} = \frac{2v}{j} u$$

Which means

$$\begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{k}{j} & 0 \end{bmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} + \begin{pmatrix} 0 \\ \frac{2v}{j} u \end{pmatrix}$$

$$a = \frac{k}{j}, \quad b = \frac{2v}{j}$$

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b) Controllable:

$$\mathcal{E} = \begin{bmatrix} B & AB \end{bmatrix}$$

$$= \begin{bmatrix} 0 & b \\ b & 0 \end{bmatrix}$$

$$\text{Rank}(\mathcal{E}) = 2$$

The system is controllable.

Stable:

$$\det(\lambda I - A) = \begin{vmatrix} +\lambda -1 & \\ & +a +\lambda \end{vmatrix}$$

$$= \lambda^2 + a$$

$$= 0$$

$$\Rightarrow \lambda = \pm i\sqrt{a}$$

It is marginally stable, but not asymptotically
since no eigenvalues are negative (strictly).

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c) It is possible iff it is observable.

Gyro:

$$\Phi_{\text{gyro}} = \begin{pmatrix} 0 & 1 \\ -a & 0 \end{pmatrix}$$

Rank is 2 so it is in principle
possible with gyro.

Incl.:

$$\Phi_{\text{incl.}} = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}$$

Rank is 2 so it is also possible with
inclinometer.

d) Using state feedback $u = -Kx$ ~~MAAALVÅL~~

$$\dot{x} = \begin{pmatrix} 0 & 1 \\ -a & 0 \end{pmatrix}x - \begin{pmatrix} 0 \\ b \end{pmatrix} \cancel{K} \cancel{\dot{x}}$$

$$= \left(\begin{pmatrix} 0 & 1 \\ -a & 0 \end{pmatrix} - \begin{pmatrix} 0 & 0 \\ bK_1 & bK_2 \end{pmatrix} \right) x$$

$$= \begin{pmatrix} 0 & 1 \\ bK_1 - a & -bK_2 \end{pmatrix} x$$

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Denne kolonne er
forbeholdt sensorThis column is for
external examinerWith $a = b = 1$ we have:

$$\dot{\underline{x}} = \begin{pmatrix} 0 & 1 \\ -k_1 - 1 & -k_2 \end{pmatrix} \underline{x}$$

Finding k_1, k_2 :

$$\det(\lambda \mathbb{I} - \begin{pmatrix} 0 & 1 \\ -k_1 - 1 & -k_2 \end{pmatrix}) = (\lambda - \lambda_1)(\lambda - \lambda_2)$$

$$\Leftrightarrow \lambda(\lambda + k_2) + 1 + k_1 = (\lambda + 1)(\lambda + 2)$$

~~ABMVMXARARQX~~

$$\Leftrightarrow \lambda^2 + k_2 \lambda + 1 + k_1 = \lambda^2 + 3\lambda + 2$$

$$\Rightarrow k_2 = 3, k_1 = 1$$

~~Det~~

The input signal $u = -(x_1 + 3x_2)$ places the poles at $-1, -2$.

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e) Luenberger observer:

$$\dot{\hat{x}} = A\hat{x} + Bu + L(y - C_{gyro}\hat{x})$$

$$= \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix} \hat{x} + \begin{pmatrix} 0 \\ b \end{pmatrix} u + \begin{pmatrix} l_1 \\ l_2 \end{pmatrix} (y - \hat{x}_2)$$

Dynamics of observer can be found from the system $\dot{e} = \dot{x} - \dot{\hat{x}}$

$$\dot{e} = Ax + Bu - A\hat{x} - Bu - L(y - C\hat{x})$$

$$= Ae - LCe$$

$$= (A - LC)e$$

$$A - CL = \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix} - \begin{pmatrix} l_1 \\ l_2 \end{pmatrix} \begin{pmatrix} 0 & 1 \\ b & 0 \end{pmatrix}$$

$$= \begin{pmatrix} 0 & 1-l_1 \\ -1 & -l_2 \end{pmatrix}$$

$$\det(\lambda I - (A - CL)) = (\lambda - \lambda'_1)(\lambda - \lambda'_2) = (\lambda + 2)^2$$

$$\Leftrightarrow \begin{vmatrix} \lambda & -1+l_1 \\ 1 & \lambda+l_2 \end{vmatrix} = \lambda^2 + 4\lambda + 4$$

$$\Leftrightarrow \lambda^2 + l_2\lambda + (l_1 + 1) = \lambda^2 + 4\lambda + 4$$

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$$\text{So } L = \underline{L} = \begin{pmatrix} l_1 \\ l_2 \end{pmatrix} = \begin{pmatrix} -3 \\ 4 \end{pmatrix}$$

gives observer poles of $\lambda_1 = \lambda_2 = -2$,

- f) No, since using a stable observer in the loop does not affect the stability of the plant (in theory).

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$$\begin{aligned} g(s) &= \frac{1}{\tilde{\tau}s+1} \begin{pmatrix} 1 \\ \tilde{\tau}s \end{pmatrix} \\ &= \frac{1}{s+\frac{1}{\tilde{\tau}}} \left(\begin{pmatrix} 0 \\ 1 \end{pmatrix} s + \begin{pmatrix} 1/\tilde{\tau} \\ 0 \end{pmatrix} \right) \end{aligned}$$

$$\Rightarrow A = -\frac{1}{\tilde{\tau}}, \quad B = 1$$

$$C = \begin{pmatrix} 0 & 1/\tilde{\tau} \\ 1 & 0 \end{pmatrix}, \quad D = \lim_{s \rightarrow \infty} g(s) = \begin{pmatrix} 0 \\ 1 \end{pmatrix}$$

This gives a minimal realization since the degree of the denominator of $g(s)$ is the same as the number of states,

$$\dot{x} = -\frac{1}{\tilde{\tau}}x + u$$

$$y = \begin{pmatrix} 0 & 1/\tilde{\tau} \\ 1 & 0 \end{pmatrix}x + \begin{pmatrix} 0 \\ 1 \end{pmatrix}u$$

With $y(t) = y_1 + y_2$, we have

$$\begin{aligned} y(s) &= y_1(s) + y_2(s) = \left(\frac{1}{\tilde{\tau}s+1} + \frac{\tilde{\tau}s}{\tilde{\tau}s+1} \right) u(s) \\ &= u(s). \end{aligned}$$

This clearly isn't observable since $C=0$

Problem 3

The system is described in normal state space

as

$$\dot{x} = -x + \begin{pmatrix} 1 & 1 \end{pmatrix} \begin{pmatrix} u_1 \\ u_2 \end{pmatrix}$$

so

$$A = -1, \quad B = \begin{pmatrix} 1 & 1 \end{pmatrix}$$

In the cost function we have $Q = 1, \quad R = \begin{pmatrix} r & 0 \\ 0 & r \end{pmatrix}$.

Computing optimal gain: (note that P is a scalar)

$$A^T P + P A + Q - P B R^{-1} B^T P = 0$$

$$-P - P + 1 - P^2 \begin{pmatrix} 1 & 1 \end{pmatrix} \begin{pmatrix} \frac{1}{r} & 0 \\ 0 & \frac{1}{r} \end{pmatrix} \begin{pmatrix} 1 \\ 1 \end{pmatrix} = 0$$

$$\Rightarrow -P^2 \frac{2}{r} + 2P - 1 = 0$$

$$\Leftrightarrow P^2 + rP - \frac{r}{2} = 0$$

$$\Rightarrow P = \frac{-r \pm \sqrt{r^2 + 4 \frac{r}{2}}}{2} = -\frac{r}{2} \pm \frac{1}{2} \sqrt{r^2 + 2r}$$

$$K = R^{-1} B^T P$$

$$= \begin{pmatrix} \frac{1}{r} & 0 \\ 0 & \frac{1}{r} \end{pmatrix} \begin{pmatrix} 1 \\ 1 \end{pmatrix} P = \begin{pmatrix} \frac{1}{r} \\ \frac{1}{r} \end{pmatrix} P$$

$$= \begin{pmatrix} 1 \\ 1 \end{pmatrix} \left(-\frac{r}{2} \pm \frac{\text{Sign}(r)}{2} \sqrt{1 + \frac{2r}{r}} \right)$$

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Since $r > 0$ and the open loop system is stable we simplify to

$$K = \begin{pmatrix} 1 \\ 1 \end{pmatrix} \left(-\frac{1}{2} + \frac{1}{2} \sqrt{1 + \frac{2}{r}} \right)$$

The inputs are weighed equally since they feed into the system in the same way.

If $r_2 \gg r_1 > 0$ then most of the feedback would go through u_1 . K would look like

~~$\begin{pmatrix} 1 \\ 1 \end{pmatrix}$~~ $K = \begin{pmatrix} \text{(large)} \\ \text{(very small)} \end{pmatrix}$

This is because using input u_2 would be expensive.

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$$\begin{cases} 0 = \alpha \bar{x}_1 - \beta \bar{x}_1 \bar{x}_2 \\ 0 = \delta \bar{x}_1 \bar{x}_2 - \gamma \bar{x}_2 \end{cases}$$

$$\Rightarrow \begin{cases} \bar{x}_1 = \gamma/\delta \\ \bar{x}_2 = \alpha/\beta \end{cases}$$

Non-linear shifted model: $x_1 = \tilde{x}_1 + \frac{\gamma}{\delta}$, $x_2 = \tilde{x}_2 + \frac{\alpha}{\beta}$

$$\begin{aligned} \dot{\tilde{x}}_1 &= \cancel{\alpha} \dot{x}_1 \\ &= \alpha \left(\tilde{x}_1 + \frac{\gamma}{\delta} \right) - \beta \left(\tilde{x}_1 + \frac{\gamma}{\delta} \right) \left(\tilde{x}_2 + \frac{\alpha}{\beta} \right) \\ &= \cancel{\alpha \tilde{x}_1} + \cancel{\frac{\alpha \gamma}{\beta}} - \cancel{\alpha \tilde{x}_1} - \cancel{\frac{\beta \gamma \tilde{x}_2}{\delta}} - \cancel{\beta \tilde{x}_1 \tilde{x}_2} - \cancel{\frac{\alpha \alpha}{\beta}} \\ &= -\frac{\beta \gamma}{\delta} \tilde{x}_2 - \beta \tilde{x}_1 \tilde{x}_2 \end{aligned}$$

$$\begin{aligned} \dot{\tilde{x}}_2 &= \dot{x}_2 \\ &= \delta \left(\tilde{x}_1 + \frac{\gamma}{\delta} \right) \left(\tilde{x}_2 + \frac{\alpha}{\beta} \right) - \gamma \left(\tilde{x}_2 + \frac{\alpha}{\beta} \right) \\ &= \frac{\delta \alpha}{\beta} \tilde{x}_1 + \cancel{\frac{\delta \gamma}{\beta} \tilde{x}_2} + \delta \tilde{x}_1 \tilde{x}_2 + \cancel{\frac{\alpha \gamma}{\beta}} - \cancel{\frac{\alpha \alpha}{\beta}} - \cancel{\frac{\gamma \alpha}{\beta}} - \cancel{\frac{\gamma \gamma}{\beta}} \\ &= \frac{\alpha \delta}{\beta} \tilde{x}_1 + \delta \tilde{x}_1 \tilde{x}_2 \end{aligned}$$

Linearizing around equilibrium:

$$\left. \frac{\partial \dot{x}_1}{\partial x_1} \right|_{\text{equi.}} = -\beta \tilde{x}_2 \Big|_{\tilde{x}_2=0} = 0$$

$$\left. \frac{\partial \dot{x}_1}{\partial x_2} \right|_{\text{equilib.}} = -\frac{\beta \delta}{S} - \cancel{\beta \tilde{x}_1} = -\frac{\beta \delta}{S}$$

$$\left. \frac{\partial \dot{x}_2}{\partial x_1} \right|_{\text{equi.}} = \cancel{\frac{\partial \delta}{\partial S}} + S \tilde{x}_2 \Big|_{\tilde{x}_2=0} = \frac{\partial \delta}{\partial S}$$

$$\left. \frac{\partial \dot{x}_2}{\partial x_2} \right|_{\text{equi.}} = S \tilde{x}_1 \Big|_{\tilde{x}_1=0} = 0$$

Linearized model is then:

$$\dot{\tilde{x}}_1 = -\frac{\beta \delta}{S} \tilde{x}_2$$

$$\dot{\tilde{x}}_2 = \frac{\partial \delta}{\partial S} \tilde{x}_1$$

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b) The system is given by

$$\begin{pmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{pmatrix} = A \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix}, \quad A = \begin{pmatrix} 0 & -\frac{\beta^2}{\delta} \\ \frac{\alpha\delta}{\beta} & 0 \end{pmatrix}$$

Eigenvalues:

$$\det(\lambda I - A) = \begin{vmatrix} \lambda & \frac{\beta^2}{\delta} \\ \frac{\alpha\delta}{\beta} & \lambda \end{vmatrix}$$

$$= \lambda^2 + \alpha\gamma = 0$$

$$\Rightarrow \lambda = \pm i\sqrt{\alpha\gamma}$$

The system is marginally stable since it has no positive eigenvalues.

With $\alpha = \beta = \gamma = \delta = 1$ we have

$$\begin{pmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix} \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix}$$

$$\Leftrightarrow \ddot{x}_1 = \ddot{x}_2 = -\dot{x}_1$$

$$\Leftrightarrow \ddot{x}_1 + \dot{x}_1 = 0$$

This has solutions

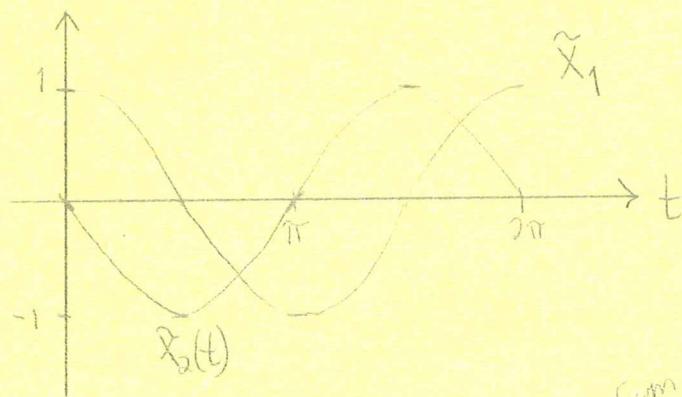
$$\dot{x}_1 = C_1 \cos t + C_2 \sin t$$

$$\dot{x}_2 = C_2 \cos t - C_1 \sin t$$

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Sketch: $C_1 = 1, C_2 = 0$



c) Let \tilde{y} = number of predators, and $\tilde{x} = \begin{pmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{pmatrix}$.
Then

$$\begin{aligned}\tilde{y} &= (0 \ 1) \tilde{x} \\ &= C \tilde{x}.\end{aligned}$$

Observability matrix is then

$$O = \begin{pmatrix} C \\ CA \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ \cancel{\alpha \beta} & 0 \end{pmatrix}$$

which has full rank.

Yes, it is possible since the system is observable.

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d) We now have essentially

$$A = \begin{pmatrix} 0 & -1 \\ 1 & 0 \end{pmatrix} \text{ and } B = \begin{pmatrix} 0 \\ 1 \end{pmatrix}.$$

Controllability:

$$\mathcal{Q}^E = (B \quad AB)$$

$$= \begin{pmatrix} 0 & -1 \\ 1 & 0 \end{pmatrix}$$

It is possible since the system is controllable.

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Problem 5

- a) An antenna that is standing perfectly still
won't move and shouldn't be affected by
disturbances, so

$$\underline{x}[k+1] = \underline{x}[k]$$

$$A = \mathbb{I}$$

$$\underline{\underline{w}} = 0$$

Will use induction on K to show that (8)
holds.

Base case, $K=0$.

$$\begin{aligned}
L[0] &= \cancel{P[0]} C^T (C \cancel{P[0]} C^T + R)^{-1} \\
C = \mathbb{I} \Rightarrow L[0] &= \sigma_v^2 \mathbb{I} \cdot \mathbb{I}^T (\mathbb{I} \sigma_v^2 \mathbb{I} \cdot \mathbb{I}^T + \sigma_v^2 \mathbb{I})^{-1} \\
&= \frac{\mathbb{I}}{2} \\
&= \frac{\mathbb{I}}{0+2} \quad \checkmark
\end{aligned}$$

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$$\begin{aligned}
P[0] &= (\mathbb{I} - L[0]C) P[0] (\mathbb{I} - L[0]C)^T + L[0]RL[0]^T \\
&= \frac{\mathbb{I}}{2} \cdot \sigma_v^2 \cdot \frac{\mathbb{I}^T}{2} + \frac{\mathbb{I}}{2} \sigma_v^2 \frac{\mathbb{I}^T}{2} \\
&= \frac{R}{4} + \frac{R}{4}, \quad (R = \sigma_v^2 \mathbb{I}) \\
&= \frac{R}{0+2} \quad \checkmark
\end{aligned}$$

$$\begin{aligned}
P[0+] &= A P[0] A^T + \cancel{Q_d}, \quad Q_d = 0 \\
&= P[0] \\
&= \frac{R}{0+2} \quad \checkmark
\end{aligned}$$

Assuming (8) holds for $k-1$, we check if it holds for k .

$$\begin{aligned}
L[k] &= P[k-1] C^T (C P[k-1] C^T + R)^{-1} \\
&= \frac{R}{k+1} \left(\frac{R}{k+1} + R \right)^{-1} \\
&= \frac{R}{k+1} \left(\frac{R+(k+1)R}{k+1} \right)^{-1} \\
&= R \left(kR + 2R \right)^{-1} \\
&= \frac{\mathbb{I}}{k+2} \quad \checkmark
\end{aligned}$$

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$$\begin{aligned}
 P[k] &= (I - L[k]C)P[k](I - L[k]C)^T + L[k]R[L[k]]^T \\
 &= \left(I - \frac{I}{k+2}\right) \frac{R}{k+1} \left(I - \frac{I}{k+2}\right)^T + \frac{I}{k+2} R \frac{I}{k+2}^T \\
 &= I \frac{k+1}{k+2} \cdot \frac{R}{k+1} \cdot I \frac{k+1}{k+2} + \frac{R}{(k+2)^2} \\
 &= R \left(\frac{k+1}{(k+2)^2} + \frac{1}{(k+2)^2} \right) \\
 &= \frac{R}{k+2} \quad \checkmark
 \end{aligned}$$

$$\begin{aligned}
 P[k+1] &= A P[k] A^T + Q_d = 0 \\
 &= P[k] \\
 &= \frac{R}{k+2} \quad \checkmark
 \end{aligned}$$

This proves that (8) holds for all $k \geq 0$, III

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b) The original std deviation is given by
 $\bar{P}[0] = R$. At $k=1$ we have halved
it to so $P[1] = \frac{R}{2}$.

It takes 1 measurement.

$$\left\{ \begin{array}{l} \hat{x}[k] = \hat{x}[k] + \frac{y[k] - \hat{x}[k]}{k+2} \\ \quad = \frac{k+1}{k+2} \hat{x}[k] + \frac{1}{k+2} y[k] \\ \hat{x}[k+1] = \hat{x}[k] \end{array} \right.$$

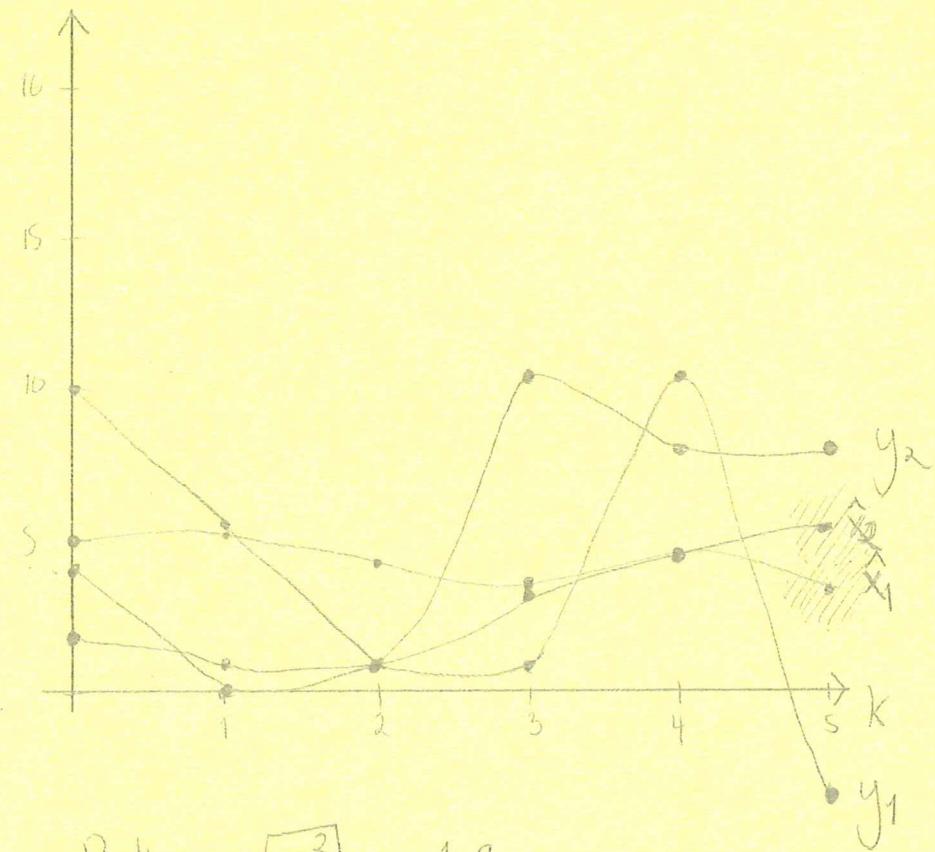
Based on these we compute \hat{x}, \tilde{x} .

$$\hat{x}[0] =$$

K	0	1	2	3	4	5
y_1	10	6	1	1	11	-3
y_2	4	0	1	16	8	8
\hat{x}	(8)	(5)	(5.25)	(4.25)	(3.6)	(4.8)
\tilde{x}	(5)	(1.25)	(4.25)	(3.6)	(4.8)	(3.7)

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$$\text{Radius: } \sqrt{\frac{\sigma_v^2}{s+2}} = 1.9$$