

## 7 Background to pull request: direct radiation perpendicular to the cell's surface

Let  $r$  be instantaneous direct radiation perpendicular to Earth's surface.  $dni$  denotes instantaneous surface radiation perpendicular to the beam and is calculated from  $r$  and the solar zenith angle  $\alpha$  as

$$110 \quad dni = \frac{r}{\cos(\alpha)} \quad (21)$$

If the panel points towards the sun, it receives 100% of  $dni$ . If it doesn't, correction factors are needed to account for the difference. The correction can be obtained by evaluating the projections on a horizontal and vertical plane, respectively. Looking at the beam from the side (as opposed to from the top), one can decompose  $dni$  into a component parallel to the ground

$$dni_{||} = dni \cdot \cos(h), \quad (22)$$

115 where  $h$  is solar altitude and one perpendicular to the ground

$$dni_{\perp} = dni \cdot \sin(h). \quad (23)$$

The component perpendicular to the ground is independent of the azimuth angle (because the effective area doesn't change when rotating the panel along a rotational axis in parallel to the beam).

However, the component parallel to the ground is affected by changes of the azimuth angles:

$$120 \quad I_{||} = \cos(a_p - a_s) dni_{||}, \quad (24)$$

where  $a_p$  ( $a_s$ ) is the panel (sun) azimuth angle.

In vector form, we can now write the radiation perpendicular to the plane as

$$I = dni [\cos(h)\cos(a_p - a_s)e_{||} + \sin(h)e_{\perp}] \quad (25)$$

Projecting onto the beam ( $e_{||} = \sin(t)e_I$  and  $e_{\perp} = \cos(t)e_I$ ) yields

$$125 \quad I = dni [\cos(h)\sin(t)\cos(a_p - a_s) + \sin(h)\cos(t)] e_I \quad (26)$$

Only looking at the absolute values yields

$$I = r \frac{1}{\cos(\alpha)} \underbrace{[\cos(h)\sin(t)\cos(a_p - a_s) + \sin(h)\cos(t)]}_g, \quad (27)$$

where solar zenith  $\alpha = \pi/2 - h$  and  $a_s$  vary in time while tilt and panel azimuth are kept constant unless tracking panels are assumed.

130 We are interested in temporal means of  $I$  rather than its instantaneous values. The mean of  $I$  over a timestep  $\Delta t$  is

$$\langle I \rangle = \frac{1}{\Delta t} \int I(t') dt', \quad (28)$$

where the bounds of the integral are typically centered around the timestep  $[t - \Delta t/2, t + \Delta t/2]$ , forward  $[t, t + \Delta t]$  or backward  $[t - \Delta t, t]$

## 7.1 The initial GSEE way to solve eq. 28

135 A helper variable is defined as

$$t_{\text{help}} = \begin{cases} t + 30 \text{Min} & , \text{ if } t.\text{hour} \text{ is not sunset or sunrise hour} \\ t + N/2 \text{Min} & , \text{ otherwise, where } N \text{ is minutes of sunshine.} \end{cases} \quad (29)$$

Note that this assumes (1) hourly input and (2) considers values to be representative for the following hour (i.e., forward running means).

GSEE evaluates the angles  $\alpha$  and  $a_s$  at  $t_{\text{help}}$ . It then makes three assumptions:

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1.  $\langle r \frac{1}{\cos(\alpha)} g \rangle = \langle r \rangle \langle \frac{1}{\cos(\alpha)} \rangle \langle g \rangle$
  2.  $\langle r \rangle = r \frac{N[\text{Mins}]}{60}$
  3.  $\langle \frac{1}{\cos(\alpha)} \rangle = \frac{1}{\cos(\alpha(t_{\text{help}}))}$

**Assumption 1** would be correct if two of the three terms were reasonably constant during a timestep. This is certainly not correct close to sunrise & sunset where  $\frac{1}{\cos(\alpha)} \rightarrow \infty$  and  $r \rightarrow 0$  such that the entire term is well defined even though the zolar  
145 zenith contributions blows up.

**Assumption 2** might be justified for hourly instantaneous values (i.e. observations) but not for model/reanalysis values. The models account for sub-resolution changes of the solar zenith angle in the calculation of  $r$  such that applying 2 means to account for this effect twice which ultimately implies a systematic underestimation of radiation around sunrise and sunset in GSEE.

150 **Assumption 3** can be very wrong around  $\alpha = \pi/2$ .

## 7.2 Suggested alternative

One can solve eq. 28 by focusing on the highly variable part:

- $r \in [0, 1000 \text{W}/\text{m}^2]$  ( $1300 \text{W}/\text{m}^2$  is ToA flux)  $\Rightarrow$  4 orders of magnitude
- $\frac{1}{\cos(\alpha)} \in [-\infty, \infty]$  (numerically  $[-10^{15}, 10^{15}]$ )  $\Rightarrow$  at least 30 orders of magnitude
- 155 -  $g \in [-1, 1]$ ,  $\Rightarrow$  less than 1 order of magnitude

which is the  $\frac{1}{\cos(\alpha)}$  contribution.

Using the following assumptions

1.  $g$  is reasonably constant per timestep and the angles for  $g$  can be calculated at the center of the timestep.
2.  $r$  is constant until the zenith angle  $\alpha$  reaches a threshold at  $t = t_{\text{thr}}$  and drops to zero afterwards,

160 we can write

$$\langle I \rangle = \langle r \frac{1}{\cos(\alpha)} g \rangle = g(t_{\text{cen}}) \langle r \frac{1}{\cos(\alpha)} \rangle. \quad (30)$$

Exploiting assumption 2, it follows that

$$\langle r \frac{1}{\cos(\alpha)} \rangle = \frac{1}{\Delta t} \left( r \int_{t-\Delta t/2}^{t_{\text{thr}}} \frac{1}{\cos(\alpha)} dt' + 0 \int_{t_{\text{thr}}}^{t+\Delta t/2} \frac{1}{\cos(\alpha)} dt' \right), \quad (31)$$

where  $r$  is constant and taken directly from the reanalysis. (Rescale?)

165 For convenience we define a function

$$s = \begin{cases} \frac{1}{\cos(\alpha)} & , \text{if } t < t_{\text{thr}} \\ 0 & , \text{otherwise,} \end{cases} \quad (32)$$

which finally yields

$$\langle I \rangle = g(t_{\text{cen}}) r \langle s \rangle \quad (33)$$