#### I. INTRODUCTION

### II. CYLINDRICAL RMP RESPONSE MODEL

#### A. Plasma Equilibrium

Consider a large aspect-ratio, low- $\beta$ , tokamak plasma whose magnetic flux surfaces map out (almost) concentric circles in the poloidal plane. Such a plasma is well approximated as a periodic cylinder. Suppose that the minor radius of the plasma is a. Standard cylindrical coordinates  $(r, \theta, z)$  are adopted. The system is assumed to be periodic in the z-direction, with periodicity length  $2\pi R_0$ , where  $R_0 \gg a$  is the simulated plasma major radius. It is convenient to define the simulated toroidal angle  $\phi = z/R_0$ .

The equilibrium magnetic field is written  $\mathbf{B} = [0, B_{\theta}(r), B_{\phi}]$ . The associated equilibrium plasma current density takes the form  $\mathbf{j} = [0, 0, j_{\phi}(r)]$ , where  $\mu_0 j_{\phi} = (1/r) d(r B_{\theta})/dr$ . The so-called safety-factor,  $q(r) = r B_{\phi}/(R_0 B_{\theta})$ , parameterizes the helical pitches of equilibrium magnetic field-lines.

# B. Plasma Response to RMP

Consider the response of the plasma to an externally generated, static, helical, resonant magnetic perturbation (RMP). Suppose that the RMP has m periods in the poloidal direction, and n periods in the toroidal direction. It is convenient to express the perturbed magnetic field and the perturbed plasma current density in terms of a perturbed poloidal magnetic flux,  $\psi(r, \theta, \phi, t)$ . In fact,  $\delta \mathbf{B} = \nabla \psi \times \nabla z$ , and  $\mu_0 \delta \mathbf{j} = -\nabla^2 \psi \nabla z$ , where  $\psi(r, \theta, \phi, t) = \hat{\psi}(r, t) \exp[\mathrm{i} (m \theta - n \phi)]$ , and  $\hat{\psi}$  is real. This particular representation is valid provided that  $m/n \gg a/R_0$ .

The response of the plasma to the RMP is governed by the equations of marginally stable, ideal-MHD everywhere in the plasma, apart from a relatively narrow (in r) region in the vicinity of the so-called *rational surface*, minor radius  $r_s$ , at which  $q(r_s) = m/n$ .<sup>1</sup>

It is convenient to parameterize the RMP in terms of the so-called vacuum magnetic flux,  $\Psi_v(t) = |\Psi_v| e^{-i\varphi_v}$ , which is defined to be the value of  $\hat{\psi}(r,t)$  at radius  $r_s$  in the presence of the RMP, but in the absence of plasma. Here,  $\varphi_v$  is the helical phase of the RMP. Likewise, the response of the plasma in the vicinity of the rational surface is parameterized in terms of

the so-called reconnected magnetic flux,  $\Psi_s(t) = |\Psi_s| e^{i\varphi_s}$ , which is the actual value of  $\hat{\psi}(r,t)$  at radius  $r_s$ . Here,  $\varphi_s$  is the helical phase of the reconnected magnetic flux.

The intrinsic stability of the m, n tearing mode is governed by the dimensionless parameter  $E_{ss} = [d\hat{\psi}_s/d \ln r]_{r_{s-}}^{r_{s+}}$ , where  $\hat{\psi}_s(r)$  is a solution of the marginally stable, ideal-MHD equations, for the case of an m, n helical perturbation, that satisfies physical boundary conditions at r = 0 and r = a, in the absence of the RMP, and is such that  $\hat{\psi}_s(r_s) = 1$ . According to resistive-MHD theory,  $^{2,4}$  if  $E_{ss} > 0$  then the m, n tearing mode spontaneously reconnects magnetic flux at the rational surface to form a helical magnetic island chain. In this paper, it is assumed that  $E_{ss} < 0$ , so that the m, n tearing mode is intrinsically stable. In this case, any magnetic reconnection that takes place at the rational surface is due solely to the action of the RMP.

The ideal-MHD response of the plasma to the RMP is governed by the dimensionless parameter  $E_{sv} = [d\hat{\psi}_v/d \ln r]_{r_{s-}}^{r_{s+}}$ , where  $\hat{\psi}_v(r)$  is a solution of the marginally stable, ideal-MHD equations, for the case of an m, n helical perturbation, that satisfies physical boundary conditions at r = 0 and r = a, in the presence of the RMP, and is such that  $\hat{\psi}_v(r_s) = 0.3$ 

#### C. Linear Response Regime

In the linear response regime, the reconnected magnetic flux induced by the RMP at the rational surface is governed by  $^{1,5,6}$ 

$$\frac{\delta_s}{r_s} \tau_R \left( \frac{d}{dt} + i \,\omega_s \right) \Psi_s = E_{ss} \,\Psi_s + E_{sv} \,\Psi_v, \tag{1}$$

where  $\delta_s$  is the linear layer width,  $\tau_R = \mu_0 \, r_s^2 \, \sigma(r_s)$  the global resistive diffusion timescale, and

$$\omega_s(t) = m \,\Omega_\theta(r_s, t) - n \,\Omega_\phi(r_s, t). \tag{2}$$

Here,  $\sigma(r)$ ,  $\Omega_{\theta}(r,t)$ , and  $\Omega_{\phi}(r,t)$  are the plasma conductivity, poloidal angular velocity, and toroidal angular velocity profiles, respectively. Note that, in this paper, we are assuming that the constant- $\psi$  approximation <sup>2</sup> holds at the rational surface. (It is demonstrated in Ref. 7 that the appropriate linear response regime for an RMP resonant in the pedestal of a typical DIII-D H-mode discharge is the so-called *first semi-collisional regime*, which is indeed a constant- $\psi$  response regime. Moreover, if the appropriate linear response regime

is constant- $\psi$  then so is the appropriate nonlinear response regime, because the constant- $\psi$  constraint is easier to satisfy in the nonlinear regime than in the linear regime.<sup>5,8</sup>)

Equation (1) can be rewritten as an amplitude evolution equation,

$$\frac{\delta_s}{r_s} \tau_R \frac{d|\Psi_s|}{dt} = E_{ss} |\Psi_s| + E_{sv} |\Psi_v| \cos(\varphi_s - \varphi_v), \tag{3}$$

combined with a phase evolution equation,

$$\frac{d\varphi_s}{dt} = \omega_s - \frac{E_{sv}}{\tau_R} \frac{r_s}{\delta_s} \frac{|\Psi_v|}{|\Psi_s|} \sin(\varphi_s - \varphi_v). \tag{4}$$

The final term on the right-hand side of Eq. (4) is termed the *slip frequency*, and is the difference between the helical phase velocity of the reconnected magnetic flux and that expected on the assumption that the flux is convected by the plasma flow at the rational surface (i.e.,  $d\varphi_s/dt = \omega_s$ ). In general, the slip frequency is non-zero because the plasma in the vicinity of the rational surface is capable of diffusing resistively through the linear layer structure.

### D. Nonlinear Response Regime

In the nonlinear response regime, Eq. (3) generalizes to the *Rutherford island width* evolution equation: <sup>4,9</sup>

$$\frac{(\mathcal{I}/2) W_s}{r_s} \tau_R \frac{d|\Psi_s|}{dt} = E_{ss} |\Psi_s| + E_{sv} |\Psi_v| \cos(\varphi_s - \varphi_v), \tag{5}$$

where

$$W_s = 4 \left( \frac{|\Psi_s|}{s_s \, r_s \, B_\theta(r_s)} \right)^{1/2} r_s \tag{6}$$

is the full radial width of the magnetic island chain,  $\mathcal{I} = 0.8227$ ,  $s(r) = d \ln q / d \ln r$ , and  $s_s = s(r_s)$ . The nonlinear regime holds when  $W_s \gg \delta_s$ , whereas the linear regime holds when  $\delta_s \ll W_s$ .

Equation (5) is usually coupled with the so-called no-slip constraint: 1

$$\frac{d\varphi_s}{dt} = \omega_s. \tag{7}$$

The reasoning behind the imposition of this constraint is that the plasma is trapped inside the magnetic separatrix of the magnetic island chain that forms in the vicinity of the rational surface, which forces the chain to co-rotate with the local plasma flow. However, in reality, the plasma is able to diffuse resistively across the separatrix to some extent. Hence, by analogy with Eqs. (3), (4), and (5), and in accordance with Refs. 10 and 11, in this paper we shall modify Eq. (7) such that

$$\frac{d\varphi_s}{dt} = \omega_s - \frac{E_{sv}}{\tau_R} \frac{r_s}{(\mathcal{I}/2) W_s} \frac{|\Psi_v|}{|\Psi_s|} \sin(\varphi_s - \varphi_v). \tag{8}$$

The final term on the right-hand side of the previous equation is the nonlinear slip frequency. In general, we would expect this frequency to be relatively small (because it is generally the case that  $|\omega_s| \tau_R(W_s/r_s) \gg 1$  for fully-developed magnetic islands in high-temperature tokamak plasmas <sup>7,11</sup>). Nevertheless, the nonlinear slip frequency may be non-negligible for developing island chains, which is why we are including it in our analysis. (Note that the nonlinear slip frequency does not appear in rigorous island calculations, such as that described in Ref. 12, and references therein, because such calculations depend crucially on complicated hierarchical ordering assumptions, according to which the nonlinear slip frequency is negligible.)

#### E. Composite Model

We can combine Eqs. (3), (4), (5), and (8) to give the following composite resonant response model that interpolates between the linear and the nonlinear regimes:

$$\left(\frac{(\mathcal{I}/2)W_s + \delta_s}{r_s}\right) \tau_R \frac{d|\Psi_s|}{dt} = E_{ss} |\Psi_s| + E_{sv} |\Psi_v| \cos(\varphi_s - \varphi_v), \tag{9}$$

$$\frac{d\varphi_s}{dt} = \omega_s - \frac{E_{sv}}{\tau_R} \left( \frac{r_s}{(\mathcal{I}/2) W_s + \delta_s} \right) \frac{|\Psi_v|}{|\Psi_s|} \sin(\varphi_s - \varphi_v). \tag{10}$$

If we define  $X_s = |\Psi_s| \cos \varphi_s$ ,  $Y_s = |\Psi_s| \sin \varphi_s$ ,  $X_v = |\Psi_v| \cos \varphi_v$ , and  $Y_v = |\Psi_v| \sin \varphi_v$  then the previous two equations are more conveniently written in the nonsingular (when  $|\Psi_s| = 0$ ) forms:  $^{10,11,13}$ 

$$\left(\frac{(\mathcal{I}/2)W_s + \delta_s}{r_s}\right)\tau_R\left(\frac{dX_s}{dt} + \omega_s Y_s\right) = E_{ss} X_s + E_{sv} X_v, \tag{11}$$

$$\left(\frac{(\mathcal{I}/2)W_s + \delta_s}{r_s}\right)\tau_R\left(\frac{dY_s}{dt} - \omega_s X_s\right) = E_{ss}Y_s + E_{sv}Y_v,$$
(12)

where

$$W_s = 4 \left( \frac{\sqrt{X_s^2 + Y_s^2}}{s_s r_s B_{\theta}(r_s)} \right)^{1/2} r_s.$$
 (13)

With the benefit of hindsight, Eqs. (11) and (12) could have been derived more directly from the following heuristic generalization of Eq. (1): <sup>11</sup>

$$\left(\frac{(\mathcal{I}/2)W_s + \delta_s}{r_s}\right) \tau_R \left(\frac{d}{dt} + i\omega_s\right) \Psi_s = E_{ss} \Psi_s + E_{sv} \Psi_v.$$
(14)

### III. MODIFIED TOROIDAL RMP RESPONSE MODEL

Our toroidal model of the response of a tokamak plasma to a static, externally generated, RMP is described in detail in Ref. 14. In the light of the composite model developed in Sect. II, we shall modify the resonant plasma response component of our toroidal response model; this component is described in Appendix D of Ref. 14.

Equations (D1) and (D2) in Ref. 14 are modified such that

$$\left(\hat{W}_k + \hat{\delta}_k\right) \mathcal{S}_k \frac{d\hat{\Psi}_k}{d\hat{t}} = \sum_{k'=1,K} \hat{E}_{kk'} \hat{\Psi}_{k'} \cos(\varphi_k - \varphi_{k'} - \xi_{kk'}) + \hat{E}_{kk} \hat{\chi}_k \cos(\varphi_k - \zeta_k), \tag{15}$$

$$S_k = \frac{\tau_R(\hat{r}_k)}{\tau_A},\tag{16}$$

respectively. Here,

$$\hat{W}_{k} = \frac{2\mathcal{I}}{\hat{a}\,\hat{r}_{k}} \left(\frac{q}{g\,s}\right)_{\hat{r}_{k}} |\hat{\Psi}_{k}|^{1/2},\tag{17}$$

$$\hat{\delta}_k = \frac{\delta_{\rm SC}(\hat{r}_k)}{R_0 \,\hat{a} \,\hat{r}_k},\tag{18}$$

where  $\delta_{SC}(\hat{r})$  is the semi-collisional linear layer width specified in Ref. 7.

In the previous expressions,  $R_0$  is the major radius of the magnetic axis, r is a magnetic flux surface label with dimensions of length (which, roughly speaking, is the average minor radius of the flux surface), q(r) is the safety-factor profile,  $s(r) = d \ln q / d \ln r$ ,  $g(r) B_0$  is the toroidal magnetic field-strength at major radius  $R_0$ ,  $B_0$  is the vacuum toroidal magnetic field-strength on the magnetic axis, a is the value of r on the last closed magnetic-flux surface,  $r_k$  is the value of r on the kth rational surface (resonant with poloidal mode number  $m_k$ , and toroidal mode number n),  $\hat{a} = a/R_0$ ,  $\hat{r} = r/a$ , and  $\hat{r}_k = r_k/a$ . Furthermore,  $\tau_R(\hat{r}) = \mu_0 r^2 \sigma_{ee} Q_{00}^{ee}$ , where  $\sigma_{ee}$  is the classical plasma parallel electrical conductivity, and  $Q_{00}^{ee}$  describes the corrections to this conductivity due to neoclassical effects and the presence of plasma impurities. Also,  $\tau_A$  is a convenient scale time, and  $\hat{t} = t/\tau_A$ . Finally,  $\Psi_k = B_0 R_0 \hat{\Psi}_k e^{-i\varphi_k}$  is the reconnected magnetic flux at the kth rational surface,

 $\chi_k = B_0 R_0 \hat{\chi}_k e^{-i\zeta_k}$  is a measure of the vacuum magnetic flux at the kth rational surface (in fact,  $\hat{E}_{kk} \chi_k$  is equivalent to  $E_{sv} \Psi_v$  in Sect. II), and  $E_{kk'} = \hat{E}_{kk'} e^{-i\xi_{kk'}}$  is the toroidal tearing stability matrix.<sup>3</sup> Here,  $\hat{\Psi}_k > 0$ ,  $\varphi_k$ ,  $\hat{\chi}_k > 0$ ,  $\zeta_k$ ,  $\hat{E}_{kk'} > 0$ , and  $\xi_{kk'}$  are all real quantities.

Equation (15) represents a minor improvement to Eq. (D1) of Ref. 14 in which the interpolation between the linear and nonlinear regimes is performed in a more systematic manner.

Equation (D6) of Ref. 14 is modified such that

$$\left(\hat{W}_{k} + \hat{\delta}_{k}\right) \mathcal{S}_{k} \left(\frac{d\varphi_{k}}{d\hat{t}} - \hat{\varpi}_{k}\right) = -\sum_{k'=1,K} \hat{E}_{kk'} \hat{\Psi}_{k'} \sin(\varphi_{k} - \varphi_{k'} - \xi_{kk'}) - \hat{E}_{kk} \hat{\chi}_{k} \sin(\varphi_{k} - \zeta_{k}),$$

$$\tag{19}$$

where

$$\hat{\varpi}_k = m_k \,\hat{\Omega}_\theta(\hat{r}_k, \hat{t}) - n \,\hat{\Omega}_\phi(\hat{r}_k, \hat{t}),\tag{20}$$

and  $\hat{\Omega}_{\theta} = \Omega_{\theta} \tau_{A}$ ,  $\hat{\Omega}_{\phi} = \Omega_{\phi} \tau_{A}$ . Equation (19) represents a major improvement to Eq. (D6) that takes into account the finite slip frequencies of the magnetic island chains induced at the various rational surfaces in the plasma.

If we define  $X_k = \hat{\Psi}_k \cos \varphi_k$  and  $Y_k = \hat{\Psi}_k \sin \varphi_k$  then Eqs. (15) and (19) are more conveniently written in the nonsingular (when  $\hat{\Psi}_k = 0$ ) forms

$$\left(\hat{W}_{k} + \hat{\delta}_{k}\right) \mathcal{S}_{k} \left(\frac{dX_{k}}{d\hat{t}} + \hat{\varpi}_{k} Y_{k}\right) = \sum_{k'=1,K} \hat{E}_{kk'} \left(\cos \xi_{kk'} X_{k'} - \sin \xi_{kk'} Y_{k'}\right) + \hat{E}_{kk} \hat{\chi}_{k} \cos \zeta_{k},\tag{21}$$

$$\left(\hat{W}_{k} + \hat{\delta}_{k}\right) \mathcal{S}_{k} \left(\frac{dY_{k}}{d\hat{t}} - \hat{\varpi}_{k} X_{k}\right) = \sum_{k'=1,K} \hat{E}_{kk'} \left(\cos \xi_{kk'} Y_{k'} + \sin \xi_{kk'} X_{k'}\right) + \hat{E}_{kk} \hat{\chi}_{k} \sin \zeta_{k}.$$

$$(22)$$

Equations (15), (19), (21), and (22) are the toroidal generalizations of Eqs. (9), (10), (11), and (12), respectively.

## IV. DISCUSSION AND CONCLUSIONS

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#### DATA AVAILABITY STATEMENT

The data that support the findings of this study are available from the corresponding author upon reasonable request.

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