

# Tearing Mode Dynamics in Tokamak Plasmas

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## 1 Fluid Theory

### 1.1 Introduction

The aim of this section is to introduce the fundamental plasma fluid theory that underpins the analysis of tearing mode dynamics in tokamak plasmas.

### 1.2 Fundamental Quantities

Consider an idealized tokamak plasma consisting of an equal number of electrons, with mass  $m_e$  and charge  $-e$  (here,  $e$  denotes the magnitude of the electron charge), and ions, with mass  $m_i$  and charge  $+e$ . We shall employ the symbol

$$T_s = \frac{1}{3} m_s \langle v_s^2 \rangle \quad (1)$$

to denote a *kinetic temperature* measured in units of energy. Here,  $v$  is a particle speed, and the angular brackets denote an ensemble average (Reif 1965). The kinetic temperature of species  $s$  is a measure of the mean kinetic energy of particles of that species. (Here,  $s$  represents either  $e$  for electrons, or  $i$  for ions.) In tokamak plasma physics, kinetic temperature is invariably measured in *electron-volts* (1 joule is equivalent to  $6.24 \times 10^{18}$  eV).

Quasi-neutrality demands that

$$n_i \simeq n_e, \quad (2)$$

where  $n_s$  is the *particle number density* (that is, the number of particles per cubic meter) of species  $s$  (Fitzpatrick 2015).

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We can estimate typical particle speeds in terms of the so-called *thermal speed*,

$$v_{ts} = \left( \frac{2T_s}{m_s} \right)^{1/2}. \quad (3)$$

In a tokamak plasma, the ambient magnetic field,  $\mathbf{B}$ , is strong enough to significantly alter charged particle trajectories. Consequently, tokamak plasmas are highly anisotropic, responding differently to forces that are parallel and perpendicular to the direction of  $\mathbf{B}$ . As is well known, charged particles respond to the Lorentz force by freely streaming in the direction of  $\mathbf{B}$ , while executing circular *gyro-orbits* in the plane perpendicular to  $\mathbf{B}$  (Fitzpatrick 2008). The typical *gyroradius* of a charged particle gyrating in a magnetic field is given by

$$\rho_s = \frac{v_{ts}}{\Omega_s}, \quad (4)$$

where

$$\Omega_s = \frac{eB}{m_s} \quad (5)$$

is the *gyrofrequency* associated with the gyration.

The electron-ion and ion-ion *collision times* are written

$$\tau_e = \frac{6\sqrt{2}\pi^{3/2} \epsilon_0^2 \sqrt{m_e} T_e^{3/2}}{\ln \Lambda_c e^4 n_e}, \quad (6)$$

and

$$\tau_i = \frac{12\pi^{3/2} \epsilon_0^2 \sqrt{m_i} T_i^{3/2}}{\ln \Lambda_c e^4 n_e}, \quad (7)$$

respectively (Fitzpatrick 2015). Here,  $\ln \Lambda_c \simeq 15$  is the *Coulomb logarithm* (Richardson 2019). Note that  $\tau_e$  is the typical time required for the cumulative effect of electron-ion collisions to deviate the path of an electron through  $90^\circ$ . Likewise,  $\tau_i$  is the typical time required for the cumulative effect of ion-ion collisions to deviate the path of an ion through  $90^\circ$ .

### 1.3 Braginskii Equations

The electron and ion fluid equations in a collisional plasma take the form:

$$\frac{dn}{dt} + n \nabla \cdot \mathbf{V}_e = 0, \quad (8)$$

$$m_e n \frac{d\mathbf{V}_e}{dt} + \nabla p_e + \nabla \cdot \boldsymbol{\pi}_e + e n (\mathbf{E} + \mathbf{V}_e \times \mathbf{B}) = \mathbf{F}, \quad (9)$$

$$\frac{3}{2} \frac{dp_e}{dt} + \frac{5}{2} p_e \nabla \cdot \mathbf{V}_e + \boldsymbol{\pi}_e : \nabla \mathbf{V}_e + \nabla \cdot \mathbf{q}_e = w_e, \quad (10)$$

and

$$\frac{dn}{dt} + n \nabla \cdot \mathbf{V}_i = 0, \quad (11)$$

$$m_i n \frac{d\mathbf{V}_i}{dt} + \nabla p_i + \nabla \cdot \boldsymbol{\pi}_i - e n (\mathbf{E} + \mathbf{V}_i \times \mathbf{B}) = -\mathbf{F}, \quad (12)$$

$$\frac{3}{2} \frac{dp_i}{dt} + \frac{5}{2} p_i \nabla \cdot \mathbf{V}_i + \boldsymbol{\pi}_i : \nabla \mathbf{V}_i + \nabla \cdot \mathbf{q}_i = w_i, \quad (13)$$

respectively. Equations (8)–(13) are called the *Braginskii equations*, because they were first obtained in a celebrated article by S.I. Braginskii (Braginskii 1965). Here,  $n$  is the electron number density,  $\mathbf{V}_s$  is the species- $s$  flow velocity,  $p_s = n T_s$  is the species- $s$  scalar pressure,  $\boldsymbol{\pi}_s$  is the species- $s$  viscosity tensor,  $\mathbf{F}$  is the collisional friction force density,  $\mathbf{q}_s$  is the species- $s$  heat flux density,  $w_s$  is the species- $s$  collisional heating rate density, and  $\mathbf{E}$  is the ambient electric field strength. Moreover,  $d/dt \equiv \partial/\partial t + \mathbf{V}_e \cdot \nabla$  in the electron fluid equations, (8)–(10), whereas  $d/dt \equiv \partial/\partial t + \mathbf{V}_i \cdot \nabla$  in the ion fluid equations, (11)–(13).

A tokamak plasma is highly magnetized. In other words,

$$\Omega_i \tau_i, \quad \Omega_e \tau_e \gg 1, \quad (14)$$

which implies that the electron and ion gyroradii are much smaller than the corresponding mean-free-paths between  $90^\circ$  collisional scattering events. In this limit, a standard two-Laguerre-polynomial Chapman-Enskog closure scheme (Chapman & Cowling 1953) yields

$$\mathbf{F} = n e \left( \frac{\mathbf{j}_\parallel}{\sigma_\parallel} + \frac{\mathbf{j}_\perp}{\sigma_\perp} \right) - 0.71 n \nabla_\parallel T_e - \frac{3n}{2\Omega_e \tau_e} \mathbf{b} \times \nabla_\perp T_e, \quad (15)$$

$$w_i = \frac{3m_e n (T_e - T_i)}{m_i \tau_e}, \quad (16)$$

$$w_e = -w_i + \frac{\mathbf{j} \cdot \mathbf{F}}{n e}. \quad (17)$$

Here,  $\mathbf{b} = \mathbf{B}/B$  is a unit vector parallel to the magnetic field, and  $\mathbf{j} = n e (\mathbf{V}_i - \mathbf{V}_e)$  is the net plasma current density. Moreover, the *parallel electrical conductivity*,  $\sigma_\parallel$ , is given by

$$\sigma_\parallel = 1.96 \frac{n e^2 \tau_e}{m_e}. \quad (18)$$

whereas the *perpendicular electrical conductivity*,  $\sigma_\perp$ , takes the form

$$\sigma_\perp = 0.51 \sigma_\parallel = \frac{n e^2 \tau_e}{m_e}. \quad (19)$$

Note that  $\nabla_\parallel(\dots) \equiv [\mathbf{b} \cdot \nabla(\dots)] \mathbf{b}$  denotes a gradient parallel to the magnetic field, whereas  $\nabla_\perp \equiv \nabla - \nabla_\parallel$  denotes a gradient perpendicular to the magnetic field. Likewise,  $\mathbf{j}_\parallel \equiv (\mathbf{b} \cdot \mathbf{j}) \mathbf{b}$  represents the component of the plasma current flowing parallel to the magnetic field, whereas  $\mathbf{j}_\perp \equiv \mathbf{j} - \mathbf{j}_\parallel$  represents the perpendicular component of the plasma current.

In a highly magnetized plasma, the electron and ion heat flux densities are written

$$\mathbf{q}_e = -\kappa_{\parallel}^e \nabla_{\parallel} T_e - \kappa_{\perp}^e \nabla_{\perp} T_e - \kappa_{\times}^e \mathbf{b} \times \nabla_{\perp} T_e - 0.71 \frac{T_e}{e} \mathbf{j}_{\parallel} - \frac{3 T_e}{2 \Omega_e \tau_e} \mathbf{b} \times \mathbf{j}_{\perp}, \quad (20)$$

$$\mathbf{q}_i = -\kappa_{\parallel}^i \nabla_{\parallel} T_i - \kappa_{\perp}^i \nabla_{\perp} T_i + \kappa_{\times}^i \mathbf{b} \times \nabla_{\perp} T_i, \quad (21)$$

respectively. Here, the *parallel thermal conductivities*, which control the diffusion of heat parallel to magnetic field-lines, are given by

$$\kappa_{\parallel}^e = 3.2 \frac{n \tau_e T_e}{m_e}, \quad (22)$$

$$\kappa_{\parallel}^i = 3.9 \frac{n \tau_i T_i}{m_i}, \quad (23)$$

whereas the *perpendicular thermal conductivities*, which control the diffusion of heat perpendicular to magnetic flux-surfaces, take the form

$$\kappa_{\perp}^e = 4.7 \frac{n T_e}{m_e \Omega_e^2 \tau_e}, \quad (24)$$

$$\kappa_{\perp}^i = 2 \frac{n T_i}{m_i \Omega_i^2 \tau_i}. \quad (25)$$

Finally, the *cross thermal conductivities*, which control the flow of heat within magnetic flux-surfaces, are written

$$\kappa_{\times}^e = \frac{5 n T_e}{2 m_e \Omega_e}, \quad (26)$$

$$\kappa_{\times}^i = \frac{5 n T_i}{2 m_i \Omega_i}. \quad (27)$$

In order to describe the viscosity tensor in a magnetized plasma, it is helpful to define the *rate-of-strain tensor*

$$W_{\alpha\beta} = \frac{\partial V_{\alpha}}{\partial r_{\beta}} + \frac{\partial V_{\beta}}{\partial r_{\alpha}} - \frac{2}{3} \nabla \cdot \mathbf{V} \delta_{\alpha\beta}. \quad (28)$$

Obviously, there is a separate rate-of-strain tensor for the electron and ion fluids. It is easily demonstrated that this tensor is zero if the fluid translates, or rotates as a rigid body, or if it undergoes isotropic compression. Thus, the rate-of-strain tensor measures the deformation of fluid volume elements.

In a highly magnetized plasma, the viscosity tensor is best described as the sum of five component tensors,

$$\boldsymbol{\pi} = \sum_{n=0,4} \boldsymbol{\pi}_n, \quad (29)$$

where

$$\boldsymbol{\pi}_0 = -3 \eta_0 \left( \mathbf{b}\mathbf{b} - \frac{1}{3} \mathbf{I} \right) \left( \mathbf{b}\mathbf{b} - \frac{1}{3} \mathbf{I} \right) : \nabla \mathbf{V}, \quad (30)$$

with

$$\boldsymbol{\pi}_1 = -\eta_1 \left[ \mathbf{I}_\perp \cdot \mathbf{W} \cdot \mathbf{I}_\perp + \frac{1}{2} \mathbf{I}_\perp (\mathbf{b} \cdot \mathbf{W} \cdot \mathbf{b}) \right], \quad (31)$$

and

$$\boldsymbol{\pi}_2 = -4\eta_1 (\mathbf{I}_\perp \cdot \mathbf{W} \cdot \mathbf{b}\mathbf{b} + \mathbf{b}\mathbf{b} \cdot \mathbf{W} \cdot \mathbf{I}_\perp). \quad (32)$$

plus

$$\boldsymbol{\pi}_3 = \frac{\eta_3}{2} (\mathbf{b} \times \mathbf{W} \cdot \mathbf{I}_\perp - \mathbf{I}_\perp \cdot \mathbf{W} \times \mathbf{b}), \quad (33)$$

and

$$\boldsymbol{\pi}_4 = 2\eta_3 (\mathbf{b} \times \mathbf{W} \cdot \mathbf{b}\mathbf{b} - \mathbf{b}\mathbf{b} \cdot \mathbf{W} \times \mathbf{b}). \quad (34)$$

Here,  $\mathbf{I}$  is the identity tensor, and  $\mathbf{I}_\perp = \mathbf{I} - \mathbf{b}\mathbf{b}$ . The previous expressions are valid for both electrons and ions.

The tensor  $\boldsymbol{\pi}_0$  describes what is known as *parallel viscosity*. This is a viscosity that controls the variation along magnetic field-lines of the velocity component parallel to field-lines. The parallel viscosity coefficients are given by

$$\eta_0^e = 0.73 n \tau_e T_e, \quad (35)$$

$$\eta_0^i = 0.96 n \tau_i T_i, \quad (36)$$

The tensors  $\boldsymbol{\pi}_1$  and  $\boldsymbol{\pi}_2$  describe what is known as *perpendicular viscosity*. This is a viscosity that controls the variation perpendicular to magnetic field-lines of the velocity components perpendicular to field-lines. The perpendicular viscosity coefficients are given by

$$\eta_1^e = 0.51 \frac{n T_e}{\Omega_e^2 \tau_e}, \quad (37)$$

$$\eta_1^i = \frac{3 n T_i}{10 \Omega_i^2 \tau_i}. \quad (38)$$

Finally, the tensors  $\boldsymbol{\pi}_3$  and  $\boldsymbol{\pi}_4$  describe what is known as *gyroviscosity*. This is not really viscosity at all, because the associated viscous stresses are always perpendicular to the velocity, implying that there is no dissipation (i.e., viscous heating) associated with this effect. The gyroviscosity coefficients are given by

$$\eta_3^e = -\frac{n T_e}{2 \Omega_e}, \quad (39)$$

$$\eta_3^i = \frac{n T_i}{2 \Omega_i}. \quad (40)$$

## 1.4 Normalization of Braginskii Equations

As we have just seen, the Braginskii equations contain terms that describe a very wide range of different physical phenomena. For this reason, they are extremely complicated.

Fortunately, however, it is not generally necessary to retain all of the terms in these equations when investigating tearing mode dynamics in tokamak plasmas. In this section, we shall attempt to construct a systematic normalization scheme for the Braginskii equations that will, hopefully, enable us to determine which terms to keep, and which to discard, when investigating tearing mode dynamics.

It is convenient to split the friction force  $\mathbf{F}$  into a component  $\mathbf{F}_U$  corresponding to resistivity, and a component  $\mathbf{F}_T$  corresponding to the thermal force. Thus,

$$\mathbf{F} = \mathbf{F}_U + \mathbf{F}_T, \quad (41)$$

where

$$\mathbf{F}_U = n e \left( \frac{\mathbf{j}_{\parallel}}{\sigma_{\parallel}} + \frac{\mathbf{j}_{\perp}}{\sigma_{\perp}} \right), \quad (42)$$

$$\mathbf{F}_T = -0.71 n \nabla_{\parallel} T_e - \frac{3 n}{2 \Omega_e \tau_e} \mathbf{b} \times \nabla_{\perp} T_e. \quad (43)$$

Likewise, the electron collisional energy gain term  $w_e$  is split into a component  $-w_i$  corresponding to the energy lost to the ions (in the ion rest frame), a component  $w_U$  corresponding to work done by the friction force  $\mathbf{F}_U$ , and a component  $w_T$  corresponding to work done by the thermal force  $\mathbf{F}_T$ . Thus,

$$w_e = -w_i + w_U + w_T, \quad (44)$$

where

$$w_U = \frac{\mathbf{j} \cdot \mathbf{F}_U}{n e}, \quad (45)$$

$$w_T = \frac{\mathbf{j} \cdot \mathbf{F}_T}{n e}. \quad (46)$$

Finally, it is helpful to split the electron heat flux density  $\mathbf{q}_e$  into a diffusive component  $\mathbf{q}_{Te}$  and a convective component  $\mathbf{q}_{Ue}$ . Thus,

$$\mathbf{q}_e = \mathbf{q}_{Te} + \mathbf{q}_{Ue}, \quad (47)$$

where

$$\mathbf{q}_{Te} = -\kappa_{\parallel}^e \nabla_{\parallel} T_e - \kappa_{\perp}^e \nabla_{\perp} T_e - \kappa_{\times}^e \mathbf{b} \times \nabla_{\perp} T_e, \quad (48)$$

$$\mathbf{q}_{Ue} = 0.71 \frac{T_e}{e} \mathbf{j}_{\parallel} - \frac{3 T_e}{2 \Omega_e \tau_e e} \mathbf{b} \times \mathbf{j}_{\perp}. \quad (49)$$

Let us, first of all, consider the electron fluid equations, which can be written:

$$\frac{dn}{dt} + n \nabla \cdot \mathbf{V}_e = 0, \quad (50)$$

$$m_e n \frac{d\mathbf{V}_e}{dt} + \nabla p_e + \nabla \cdot \boldsymbol{\pi}_e + e n (\mathbf{E} + \mathbf{V}_e \times \mathbf{B}) = \mathbf{F}_U + \mathbf{F}_T, \quad (51)$$

$$\frac{3}{2} \frac{dp_e}{dt} + \frac{5}{2} p_e \nabla \cdot \mathbf{V}_e + \boldsymbol{\pi}_e : \nabla \mathbf{V}_e + \nabla \cdot \mathbf{q}_{Te} + \nabla \cdot \mathbf{q}_{Ue} = -w_i + w_U + w_T. \quad (52)$$

Let  $\bar{n}$ ,  $\bar{v}_e$ ,  $\bar{\tau}_e$ ,  $\bar{l}_e = \bar{v}_e \bar{\tau}_e$ ,  $\bar{B}$ , and  $\bar{\rho}_e = \bar{v}_e / (e\bar{B}/m_e)$ , be typical values of the particle density, the electron thermal velocity, the electron collision time, the electron mean-free-path between collisions, the magnetic field-strength, and the electron gyroradius, respectively. Suppose that the typical spatial variation lengthscale of fluid variables is  $L$ . Let

$$\delta_e = \frac{\bar{\rho}_e}{L}, \quad (53)$$

$$\zeta_e = \frac{\bar{\rho}_e}{\bar{l}_e}, \quad (54)$$

$$\mu = \sqrt{\frac{m_e}{m_i}}. \quad (55)$$

All three of these parameters are assumed to be small compared to unity. Finally, the typical electron flow velocity is assumed to be of order  $\delta_e \bar{v}_e$ . This corresponds to the so-called *drift ordering* in which the flow velocity is comparable to the curvature and grad-B particle drift velocities (Fitzpatrick 2015). The drift ordering is appropriate to tearing modes in tokamak plasmas, which are comparatively slowly growing instabilities.

We define the following normalized quantities:

$$\begin{aligned} \hat{n} &= \frac{n}{\bar{n}}, & \hat{v}_e &= \frac{v_e}{\bar{v}_e}, & \hat{\mathbf{r}} &= \frac{\mathbf{r}}{L}, \\ \hat{\nabla} &= L \nabla, & \hat{t} &= \frac{\delta_e \bar{v}_e t}{L}, & \hat{\mathbf{V}}_e &= \frac{\mathbf{V}_e}{\delta_e \bar{v}_e}, \\ \hat{\mathbf{B}} &= \frac{\mathbf{B}}{\bar{B}}, & \hat{\mathbf{E}} &= \frac{\mathbf{E}}{\delta_e \bar{v}_e \bar{B}}, & \hat{\mathbf{j}} &= \frac{\mathbf{j}}{n e \delta_e \bar{v}_e}, \\ \hat{p}_e &= \frac{p_e}{m_e \bar{n} \bar{v}_e^2}, & \hat{\boldsymbol{\pi}}_e &= \frac{\boldsymbol{\pi}_e}{\delta_e^2 \zeta_e^{-1} m_e \bar{n} \bar{v}_e^2}, & \hat{\mathbf{q}}_{Te} &= \frac{\mathbf{q}_{Te}}{\delta_e \zeta_e^{-1} m_e \bar{n} \bar{v}_e^3}, \\ \hat{\mathbf{q}}_{Ue} &= \frac{\mathbf{q}_{Ue}}{\delta_e m_e \bar{n} \bar{v}_e^3}, & \hat{\mathbf{F}}_U &= \frac{\mathbf{F}_U}{\zeta_e m_e \bar{n} \bar{v}_e^2 / L}, & \hat{\mathbf{F}}_T &= \frac{\mathbf{F}_T}{m_e \bar{n} \bar{v}_e^2 / L}, \\ \hat{w}_i &= \frac{w_i}{\delta_e^{-1} \zeta_e \mu^2 m_e \bar{n} \bar{v}_e^3 / L}, & \hat{w}_U &= \frac{w_U}{\delta_e \zeta_e m_e \bar{n} \bar{v}_e^3 / L}, & \hat{w}_T &= \frac{w_T}{\delta_e m_e \bar{n} \bar{v}_e^3 / L}. \end{aligned}$$

The normalization procedure is designed to make all hatted quantities  $\mathcal{O}(1)$ . The normalization of the electric field is chosen such that the  $\mathbf{E} \times \mathbf{B}$  velocity is of similar magnitude to the electron fluid velocity. Note that the parallel viscosity makes an  $\mathcal{O}(1)$  contribution to  $\hat{\boldsymbol{\pi}}_e$ , whereas the gyroviscosity makes an  $\mathcal{O}(\zeta_e)$  contribution, and the perpendicular viscosity only makes an  $\mathcal{O}(\zeta_e^2)$  contribution. Likewise, the parallel thermal conductivity makes an  $\mathcal{O}(1)$  contribution to  $\hat{\mathbf{q}}_{Te}$ , whereas the cross conductivity makes an  $\mathcal{O}(\zeta_e)$  contribution, and the perpendicular conductivity only makes an  $\mathcal{O}(\zeta_e^2)$  contribution. Similarly, the parallel components of  $\mathbf{F}_T$  and  $\mathbf{q}_{Ue}$  are  $\mathcal{O}(1)$ , whereas the perpendicular components are  $\mathcal{O}(\zeta_e)$ .

The normalized electron fluid equations take the form:

$$\frac{d\hat{n}}{d\hat{t}} + \hat{n} \hat{\nabla} \cdot \hat{\mathbf{V}}_e = 0, \quad (56)$$

$$\hat{n} \frac{d\hat{\mathbf{V}}_e}{d\hat{t}} + \delta_e^{-2} \hat{\nabla} \hat{p}_e + \zeta_e^{-1} \hat{\nabla} \cdot \hat{\boldsymbol{\pi}}_e + \delta_e^{-2} \hat{n} (\hat{\mathbf{E}} + \hat{\mathbf{V}}_e \times \hat{\mathbf{B}}) = \delta_e^{-2} \zeta_e \hat{\mathbf{F}}_U + \delta_e^{-2} \hat{\mathbf{F}}_T, \quad (57)$$

$$\begin{aligned} \frac{3}{2} \frac{d\hat{p}_e}{d\hat{t}} + \frac{5}{2} \hat{p}_e \hat{\nabla} \cdot \hat{\mathbf{V}}_e + \delta_e^2 \zeta_e^{-1} \hat{\boldsymbol{\pi}}_e : \hat{\nabla} \cdot \hat{\mathbf{V}}_e \\ + \zeta_e^{-1} \hat{\nabla} \cdot \hat{\mathbf{q}}_{Te} + \hat{\nabla} \cdot \hat{\mathbf{q}}_{Ue} = -\delta_e^{-2} \zeta_e \mu^2 \hat{w}_i + \zeta_e \hat{w}_U + \hat{w}_T. \end{aligned} \quad (58)$$

The only large or small (compared to unity) quantities in these equations are the parameters  $\delta_e$ ,  $\zeta_e$ , and  $\mu$ . Here,  $d/d\hat{t} \equiv \partial/\partial\hat{t} + \hat{\mathbf{V}}_e \cdot \hat{\nabla}$ . It is assumed that  $T_e \sim T_i$ .

Let us now consider the ion fluid equations, which can be written:

$$\frac{dn}{dt} + n \nabla \cdot \mathbf{V}_i = 0, \quad (59)$$

$$m_i n \frac{d\mathbf{V}_i}{dt} + \nabla p_i + \nabla \cdot \boldsymbol{\pi}_i - e n (\mathbf{E} + \mathbf{V}_i \times \mathbf{B}) = -\mathbf{F}_U - \mathbf{F}_T, \quad (60)$$

$$\frac{3}{2} \frac{dp_i}{dt} + \frac{5}{2} p_i \nabla \cdot \mathbf{V}_i + \boldsymbol{\pi}_i : \nabla \mathbf{V}_i + \nabla \cdot \mathbf{q}_i = w_i. \quad (61)$$

It is convenient to adopt a normalization scheme for the ion equations which is similar to, but independent of, that employed to normalize the electron equations. Let  $\bar{n}$ ,  $\bar{v}_i$ ,  $\bar{l}_i$ ,  $\bar{B}$ , and  $\bar{\rho}_i = \bar{v}_i/(e\bar{B}/m_i)$ , be typical values of the particle density, the ion thermal velocity, the ion mean-free-path between collisions, the magnetic field-strength, and the ion gyroradius, respectively. Suppose that the typical spatial variation lengthscale of fluid quantities is  $L$ . Let

$$\delta_i = \frac{\bar{\rho}_i}{L}, \quad (62)$$

$$\zeta_i = \frac{\bar{\rho}_i}{\bar{l}_i}, \quad (63)$$

$$\mu = \sqrt{\frac{m_e}{m_i}}. \quad (64)$$

All three of these parameters are assumed to be small compared to unity. As before, we adopt the drift ordering in which the typical ion flow velocity is assumed to be of order  $\delta_i \bar{v}_i$ .

We define the following normalized quantities:

$$\begin{aligned} \hat{n} &= \frac{n}{\bar{n}}, & \hat{v}_i &= \frac{v_i}{\bar{v}_i}, & \hat{\mathbf{r}} &= \frac{\mathbf{r}}{L}, \\ \hat{\nabla} &= L \nabla, & \hat{t} &= \frac{\delta_i \bar{v}_i t}{L}, & \hat{\mathbf{V}}_i &= \frac{\mathbf{V}_i}{\delta_i \bar{v}_i}, \end{aligned}$$



$$\begin{aligned}
\widehat{\mathbf{B}} &= \frac{\mathbf{B}}{\bar{B}}, & \widehat{\mathbf{E}} &= \frac{\mathbf{E}}{\delta_i \bar{v}_i \bar{B}}, & \widehat{\mathbf{j}} &= \frac{\mathbf{j}}{n e \delta_i \bar{v}_i}, \\
\widehat{p}_i &= \frac{p_i}{m_i \bar{n} \bar{v}_i^2}, & \widehat{\boldsymbol{\pi}}_i &= \frac{\boldsymbol{\pi}_i}{\delta_i^2 \zeta_i^{-1} m_i \bar{n} \bar{v}_i^2}, & \widehat{\mathbf{q}}_i &= \frac{\mathbf{q}_i}{\delta_i \zeta_i^{-1} m_i \bar{n} \bar{v}_i^3}, \\
\widehat{\mathbf{F}}_U &= \frac{\mathbf{F}_U}{\zeta_i \mu m_i \bar{n} \bar{v}_i^2 / L}, & \widehat{\mathbf{F}}_T &= \frac{\mathbf{F}_T}{m_i \bar{n} \bar{v}_i^2 / L}, & \widehat{w}_i &= \frac{w_i}{\delta_i^{-1} \zeta_i \mu m_i \bar{n} \bar{v}_i^3 / L}.
\end{aligned}$$

As before, the normalization procedure is designed to make all hatted quantities  $\mathcal{O}(1)$ . The normalization of the electric field is chosen such that the  $\mathbf{E} \times \mathbf{B}$  velocity is of similar magnitude to the ion fluid velocity. Note that the parallel viscosity makes an  $\mathcal{O}(1)$  contribution to  $\widehat{\boldsymbol{\pi}}_i$ , whereas the gyroviscosity makes an  $\mathcal{O}(\zeta_i)$  contribution, and the perpendicular viscosity only makes an  $\mathcal{O}(\zeta_i^2)$  contribution. Likewise, the parallel thermal conductivity makes an  $\mathcal{O}(1)$  contribution to  $\widehat{\mathbf{q}}_i$ , whereas the cross conductivity makes an  $\mathcal{O}(\zeta_i)$  contribution, and the perpendicular conductivity only makes an  $\mathcal{O}(\zeta_i^2)$  contribution. Similarly, the parallel component of  $\mathbf{F}_T$  is  $\mathcal{O}(1)$ , whereas the perpendicular component is  $\mathcal{O}(\zeta_i \mu)$ .

The normalized ion fluid equations take the form:

$$\frac{d\hat{n}}{d\hat{t}} + \hat{n} \widehat{\nabla} \cdot \widehat{\mathbf{V}}_i = 0, \quad (65)$$

$$\hat{n} \frac{d\widehat{\mathbf{V}}_i}{d\hat{t}} + \delta_i^{-2} \widehat{\nabla} \widehat{p}_i + \zeta_i^{-1} \widehat{\nabla} \cdot \widehat{\boldsymbol{\pi}}_i - \delta_i^{-2} \hat{n} (\widehat{\mathbf{E}} + \widehat{\mathbf{V}}_i \times \widehat{\mathbf{B}}) = -\delta_i^{-2} \zeta_i \mu \widehat{\mathbf{F}}_U - \delta_i^{-2} \widehat{\mathbf{F}}_T, \quad (66)$$

$$\frac{3}{2} \frac{d\widehat{p}_i}{d\hat{t}} + \frac{5}{2} \widehat{p}_i \widehat{\nabla} \cdot \widehat{\mathbf{V}}_i + \delta_i^2 \zeta_i^{-1} \widehat{\boldsymbol{\pi}}_i : \widehat{\nabla} \cdot \widehat{\mathbf{V}}_i + \zeta_i^{-1} \widehat{\nabla} \cdot \widehat{\mathbf{q}}_i = \delta_i^{-2} \zeta_i \mu \widehat{w}_i. \quad (67)$$

The only large or small (compared to unity) quantities in these equations are the parameters  $\delta_i$ ,  $\zeta_i$ , and  $\mu$ . Here,  $d/d\hat{t} \equiv \partial/\partial\hat{t} + \widehat{\mathbf{V}}_i \cdot \widehat{\nabla}$ .

## 1.5 Lowest-Order Fluid Equations

If we restore dimensions to the Braginskii equations then we can write them in the form

$$\frac{\partial n}{\partial t} + \nabla \cdot (n \mathbf{V}_e) = 0, \quad (68)$$

$$\begin{aligned}
m_e n \frac{\partial \mathbf{V}_e}{\partial t} + m_e n (\mathbf{V}_e \cdot \nabla) \mathbf{V}_e + [\delta_e^{-2}] \nabla p_e + [\zeta_e^{-1}] \nabla \cdot \boldsymbol{\pi}_e \\
+ [\delta_e^{-2}] e n (\mathbf{E} + \mathbf{V}_e \times \mathbf{B}) = [\delta_e^{-2} \zeta_e] \mathbf{F}_U + [\delta_e^{-2}] \mathbf{F}_T,
\end{aligned} \quad (69)$$

$$\begin{aligned}
\frac{3}{2} \frac{\partial p_e}{\partial t} + \frac{3}{2} \mathbf{V}_e \cdot \nabla p_e + \frac{5}{2} p_e \nabla \cdot \mathbf{V}_e + [\delta_e^2 \zeta_e^{-1}] \boldsymbol{\pi}_e : \nabla \mathbf{V}_e \\
+ [\zeta_e^{-1}] \nabla \cdot \mathbf{q}_{Te} + \nabla \cdot \mathbf{q}_{Ue} = -[\delta_e^{-2} \zeta_e \mu^2] w_i + [\zeta_e] w_U + w_T,
\end{aligned} \quad (70)$$

and

$$\frac{\partial n}{\partial t} + \nabla \cdot (n \mathbf{V}_i) = 0, \quad (71)$$

$$m_i n \frac{\partial \mathbf{V}_i}{\partial t} + m_i n (\mathbf{V}_i \cdot \nabla) \mathbf{V}_i + [\delta_i^{-2}] \nabla p_i + [\zeta_i^{-1}] \nabla \cdot \boldsymbol{\pi}_i - [\delta_i^{-2}] e n (\mathbf{E} + \mathbf{V}_i \times \mathbf{B}) = -[\delta_i^{-2} \zeta_i \mu] \mathbf{F}_U - [\delta_i^{-2}] \mathbf{F}_T, \quad (72)$$

$$\frac{3}{2} \frac{\partial p_i}{\partial t} + \frac{3}{2} \mathbf{V}_i \cdot \nabla p_i + \frac{5}{2} p_i \nabla \cdot \mathbf{V}_i + [\delta_i^2 \zeta_i^{-1}] \boldsymbol{\pi}_i : \nabla \mathbf{V}_i + [\zeta_i^{-1}] \nabla \cdot \mathbf{q}_i = [\delta_i^{-2} \zeta_i \mu] w_i. \quad (73)$$

The terms in square brackets are there to remind us that the terms they precede are smaller or larger than the other terms in the equations (by the corresponding terms within the brackets).

If we assume that  $\delta_e \sim \zeta_e \sim \mu \ll 1$  then the dominant terms in the electron energy conservation equation (70) yield

$$\nabla \cdot \mathbf{q}_{T_e} \simeq \nabla \cdot (-\kappa_{\parallel}^e \nabla_{\parallel} T_e) \simeq 0, \quad (74)$$

which implies that

$$\mathbf{B} \cdot \nabla T_e = 0. \quad (75)$$

In other words, the parallel electron heat conductivity in a tokamak plasma is usually sufficiently large that it forces the electron temperature to be constant on magnetic flux-surfaces. Likewise, if we assume that  $\delta_i \sim \zeta_i \sim \mu \ll 1$  then the dominant terms in the ion energy conservation equation (73) yield

$$\nabla \cdot \mathbf{q}_{T_i} \simeq \nabla \cdot (-\kappa_{\parallel}^i \nabla_{\parallel} T_i) \simeq 0, \quad (76)$$

which implies that

$$\mathbf{B} \cdot \nabla T_i = 0. \quad (77)$$

In other words, the parallel ion heat conductivity in a tokamak plasma is usually sufficiently large that it forces the ion temperature to be constant on magnetic flux-surfaces.

The dominant terms in the electron and ion momentum conservation equations, (69) and (72), respectively, yield

$$\nabla p_e + n e (\mathbf{E} + \mathbf{V}_e \times \mathbf{B}) \simeq 0, \quad (78)$$

$$\nabla p_i - n e (\mathbf{E} + \mathbf{V}_i \times \mathbf{B}) \simeq 0. \quad (79)$$

The sum of the preceding two equations gives

$$\mathbf{j} \times \mathbf{B} \simeq \nabla p, \quad (80)$$

where  $p = p_e + p_i$ . In other words, a conventional tokamak plasma exists in a state in which electromagnetic forces exactly balance the total scalar pressure force. It follows from the previous equation that

$$\mathbf{B} \cdot \nabla p \simeq 0. \quad (81)$$

In other words, the pressure in a conventional tokamak plasma is constant on magnetic flux-surfaces. However, given that  $p = n(T_e + T_i)$ , and making use of Eqs. (75) and (77), we deduce that

$$\mathbf{B} \cdot \nabla n \simeq 0. \quad (82)$$

In other words, the electron number density in a conventional tokamak plasma is also constant on magnetic flux-surfaces.

Taking the difference of the electron and ion particle conservation equations, (68) and (71), respectively, we obtain

$$\nabla \cdot \mathbf{j} = 0. \quad (83)$$

Equations (80) and (83) can be combined to give

$$(\mathbf{B} \cdot \nabla) \mathbf{j} - (\mathbf{j} \cdot \nabla) \mathbf{B} \simeq \mathbf{0}. \quad (84)$$

Here, we have made use of the fact that  $\nabla \cdot \mathbf{B} = 0$ .

Finally, Equations (78) and (79) imply that

$$\mathbf{V}_{\perp e} \simeq \mathbf{V}_E + \mathbf{V}_{*e}, \quad (85)$$

$$\mathbf{V}_{\perp i} \simeq \mathbf{V}_E + \mathbf{V}_{*i}, \quad (86)$$

where

$$\mathbf{V}_E = \frac{\mathbf{E} \times \mathbf{B}}{B^2} \quad (87)$$

is the *E-cross-B drift velocity* (otherwise known as the  $\mathbf{E} \times \mathbf{B}$  velocity), and

$$\mathbf{V}_{*e} = \frac{\nabla p_e \times \mathbf{B}}{e n B^2}, \quad (88)$$

$$\mathbf{V}_{*i} = -\frac{\nabla p_i \times \mathbf{B}}{e n B^2}, \quad (89)$$

are termed the *electron diamagnetic velocity* and the *ion diamagnetic velocity*, respectively (Fitzpatrick 2015).

## 2 Cylindrical Tearing Mode Theory

### 2.1 Introduction

The aim of this section is to describe the simplest theory of tearing mode dynamics in tokamak plasmas, according to which the plasma equilibrium is approximated as a periodic cylinder.

## 2.2 Tokamak Equilibrium

Consider a large aspect-ratio, toroidal, tokamak plasma equilibrium whose magnetic flux-surfaces map out (almost) concentric circles in the poloidal plane. Such an equilibrium can be approximated as a periodic cylinder (Wesson 1978). Let us employ a conventional set of right-handed cylindrical coordinates,  $r$ ,  $\theta$ ,  $z$ . The equilibrium magnetic flux-surfaces lie on surfaces of constant  $r$ . The system is assumed to be periodic in the  $z$  ('toroidal') direction, with periodicity length  $2\pi R_0$ , where  $R_0$  is the simulated *major radius* of the plasma. The *safety-factor* profile takes the form

$$q(r) = \frac{r B_z}{R_0 B_\theta(r)}, \quad (90)$$

where  $B_z$  is the constant 'toroidal' magnetic field-strength, and  $B_\theta(r)$  is the poloidal magnetic field-strength. It is assumed that  $q \sim \mathcal{O}(1)$ . The equilibrium 'toroidal' current density satisfies

$$\mu_0 j_z(r) = \frac{(r B_\theta)'}{r}, \quad (91)$$

where  $'$  denotes  $d/dr$ . Finally, the standard large aspect-ratio tokamak orderings,

$$\frac{r}{R_0} \ll 1, \quad \frac{B_\theta}{B_z} \ll 1, \quad (92)$$

are adopted (Fitzpatrick 1993).

## 2.3 Perturbed Magnetic Field

Consider a tearing mode perturbation that has  $m$  periods in the poloidal direction, and  $n$  periods in the toroidal direction, where  $m/n \sim \mathcal{O}(1)$ . We can write the perturbed magnetic field in the form

$$\delta \mathbf{B} \simeq \nabla \times (\psi \mathbf{e}_z), \quad (93)$$

where

$$\psi(r, \theta, \varphi, t) = \psi(r, t) \exp[i(m\theta - n\varphi)]. \quad (94)$$

Here,  $\varphi = z/R_0$  is a simulated toroidal angle. The perturbed current density becomes

$$\mu_0 \delta \mathbf{j} \simeq -\nabla^2 \psi \mathbf{e}_z. \quad (95)$$

It is assumed that  $|\delta \mathbf{B}| \ll |\mathbf{B}|$ .

## 2.4 Cylindrical Tearing Mode Equation

To lowest order, the tearing perturbation is governed by the linearized version of Equation (84), which yields

$$(\delta \mathbf{B} \cdot \nabla) \mathbf{j} + (\mathbf{B} \cdot \nabla) \delta \mathbf{j} - (\delta \mathbf{j} \cdot \nabla) \mathbf{B} - (\mathbf{j} \cdot \nabla) \delta \mathbf{B} \simeq \mathbf{0}. \quad (96)$$

Making use of Equations (90)–(95), the  $z$ -component of the previous equation gives the *cylindrical tearing mode equation* (Fitzpatrick 1993),

$$\frac{\partial^2 \psi}{\partial r^2} + \frac{1}{r} \frac{\partial \psi}{\partial r} - \frac{m^2}{r^2} \psi - \frac{J'_z \psi}{r(1/q - n/m)} \simeq 0, \quad (97)$$

where

$$J_z(r) = \frac{R_0 \mu_0 j_z(r)}{B_z}. \quad (98)$$

## 2.5 Solution in Presence of Perfectly-Conducting Wall

Suppose that the plasma occupies the region  $0 \leq r \leq a$ , where  $a$  is the plasma *minor radius*. It follows that  $J_z(r) = 0$  for  $r > a$ . Let the plasma be surrounded by a concentric perfectly-conducting wall of radius  $r_w > a$ . (By definition,  $a \ll R_0$  in a large aspect-ratio tokamak.) An appropriate physical solution of the cylindrical tearing mode equation takes the form

$$\psi(r, t) = \Psi_s(t) \hat{\psi}_s(r), \quad (99)$$

where the real function  $\hat{\psi}_s(r)$  is a solution of

$$\frac{d^2 \hat{\psi}_s}{dr^2} + \frac{1}{r} \frac{d \hat{\psi}_s}{dr} - \frac{m^2}{r^2} \hat{\psi}_s - \frac{J'_z \hat{\psi}_s}{r(1/q - n/m)} \simeq 0 \quad (100)$$

that satisfies

$$\hat{\psi}_s(0) = 0, \quad (101)$$

$$\hat{\psi}_s(r_s) = 1, \quad (102)$$

$$\hat{\psi}_s(r \geq r_w) = 0. \quad (103)$$

Note that Equation (100) is singular at the so-called *resonant* magnetic flux-surface, radius  $r = r_s$ , at which

$$q(r_s) = \frac{m}{n}. \quad (104)$$

At the resonant surface,  $\mathbf{k} \cdot \mathbf{B} = 0$ , where  $\mathbf{k} = (0, m/r, -n/R_0)$  is the wavevector of the tearing perturbation. The value of  $\psi(r, t)$  at the resonant surface—namely,  $\Psi_s(t)$ —is known as the *reconnected magnetic flux* (Fitzpatrick 1993). Note that  $\Psi_s$  is, in general, a complex quantity. Let  $\rho = (r - r_s)/r_s$ . The solution of Equation (100) in the vicinity of the resonant surface is

$$\hat{\psi}_s(\rho) = 1 + \Delta_{s+} \rho + \alpha_s \rho \ln |\rho| + \mathcal{O}(\rho^2) \quad (105)$$

for  $\rho > 0$ , and

$$\hat{\psi}_s(\rho) = 1 + \Delta_{s-} \rho + \alpha_s \rho \ln |\rho| + \mathcal{O}(\rho^2) \quad (106)$$

for  $\rho < 0$ . Here,

$$\alpha_s = - \left( \frac{r q J'_z}{s} \right)_{r=r_s}, \quad (107)$$

$$s(r) = \frac{r q'}{q}. \quad (108)$$

Moreover, the real parameters  $\Delta_{s+}$  and  $\Delta_{s-}$  are fully determined by Equation (100) and the boundary conditions (101)–(103). Note that, in general,  $\psi$  is continuous across the resonant surface (in accordance with Maxwell's equations), whereas  $\partial\psi/\partial r$  is discontinuous. The discontinuity in  $\partial\psi/\partial r$  implies the presence of a radially thin, helical, current sheet at the resonant surface. This current sheet can only be resolved by retaining more terms in the perturbed plasma equation of motion, (96).

The complex quantity

$$\Delta\Psi_s = \left[ r \frac{\partial\psi}{\partial r} \right]_{r_{s-}}^{r_{s+}} \quad (109)$$

parameterizes the amplitude and phase of the current sheet flowing at the resonant surface. Matching the solutions in the so-called *inner region* (i.e., the region of the plasma in the immediate vicinity of the resonant surface) and the so-called *outer region* (i.e., everywhere in the plasma other than the inner region) with the help of Equations (99), (105), and (106), we obtain

$$\Delta\Psi_s = E_{ss} \Psi_s, \quad (110)$$

where  $E_{ss} = \Delta_{s+} - \Delta_{s-}$  is a real quantity that is known as the *tearing stability index* (Furth, et al., 1963).

## 2.6 Solution in Presence of Resistive Wall

Suppose, now, that the wall at  $r = r_w$  possesses a finite resistivity, but is surrounded by a second perfectly-conducting wall located at radius  $r_c > r_w$ . The solution in the outer region can be written

$$\psi(r, t) = \Psi_s(t) \hat{\psi}_s(r) + \Psi_w(t) \hat{\psi}_w(r), \quad (111)$$

where the real function  $\hat{\psi}_s(r)$  is specified in the previous section, and the real function  $\hat{\psi}_w(r)$  is a solution of

$$\frac{d^2 \hat{\psi}_w}{dr^2} + \frac{1}{r} \frac{d \hat{\psi}_w}{dr} - \frac{m^2}{r^2} \hat{\psi}_w - \frac{J'_z \hat{\psi}_w}{r(1/q - n/m)} \simeq 0 \quad (112)$$

that satisfies

$$\hat{\psi}_w(r \leq r_s) = 0, \quad (113)$$

$$\hat{\psi}_w(r_w) = 1, \quad (114)$$

$$\hat{\psi}_w(r \geq r_c) = 0. \quad (115)$$

It is easily seen that

$$\hat{\psi}_w(r_w < r < r_c) = \frac{(r/r_c)^{-m} - (r/r_c)^m}{(r_w/r_c)^{-m} - (r_w/r_c)^m}. \quad (116)$$

In general,  $\psi$  is continuous across the wall (in accordance with Maxwell's equations), whereas  $\partial\psi/\partial r$  is discontinuous. The discontinuity in  $\partial\psi/\partial r$  is caused by a helical current sheet induced in the wall. The complex quantity  $\Psi_w(t)$  determines the amplitude and phase of the perturbed magnetic flux that penetrates the wall. The complex quantity

$$\Delta\Psi_w = \left[ r \frac{\partial\psi}{\partial r} \right]_{r_w-}^{r_w+} \quad (117)$$

parameterizes the amplitude and phase of the helical current sheet flowing in the wall. Simultaneously matching the outer solution (111) across the resonant surface and the wall yields

$$\Delta\Psi_s = E_{ss}\Psi_s + E_{sw}\Psi_w, \quad (118)$$

$$\Delta\Psi_w = E_{ws}\Psi_s + E_{ww}\Psi_w \quad (119)$$

(Fitzpatrick 1993). Here,

$$E_{ww} = \left[ r \frac{d\hat{\psi}_w}{dr} \right]_{r_w-}^{r_w+}, \quad (120)$$

$$E_{sw} = \left[ r \frac{d\hat{\psi}_w}{dr} \right]_{r=r_{s+}}, \quad (121)$$

$$E_{ws} = - \left[ r \frac{d\hat{\psi}_s}{dr} \right]_{r=r_{w-}} \quad (122)$$

are real quantities determined by the solutions of Equations (100) and (112) in the outer region.

Equations (100) and (112) can be combined to give

$$\frac{d}{dr} \left( \hat{\psi}_s r \frac{d\hat{\psi}_w}{dr} - \hat{\psi}_w r \frac{d\hat{\psi}_s}{dr} \right) = 0. \quad (123)$$

If we integrate the previous equation from  $r = r_{s+}$  to  $r = r_{w-}$ , making use of Equations (102), (103), (113), (114), (121), and (122), then we obtain

$$E_{sw} = E_{ws} \quad (124)$$

(Fitzpatrick 1993).

## 2.7 Resistive Wall Physics

It is clear from Equation (93) that

$$\delta \mathbf{A} \simeq \psi \mathbf{e}_z, \quad (125)$$

where  $\delta \mathbf{A}$  is the perturbed magnetic vector potential. Hence, the perturbed electric field can be written

$$\delta \mathbf{E} \simeq -\nabla \delta \Phi - \frac{\partial \psi}{\partial t} \mathbf{e}_z, \quad (126)$$

where  $\delta \Phi$  is the perturbed electric scalar potential. Assuming that  $|\nabla \delta \Phi| \sim |\partial \psi / \partial t|$ , the  $z$ -component of the previous equation yields

$$\delta E_z \simeq -\frac{\partial \psi}{\partial t}, \quad (127)$$

where use has been made of the large aspect-ratio orderings (92). Within the wall, we can write

$$\delta E_z \simeq -\frac{d\Psi_w}{dt}. \quad (128)$$

Here, we are making use of the so-called *thin wall approximation*, according to which  $\psi$  is assumed to only vary weakly in  $r$  inside the wall. Ohm's law implies that

$$\delta j_z = \frac{\delta E_z}{\eta_w} = -\frac{1}{\eta_w} \frac{d\Psi_w}{dt} \quad (129)$$

within the wall, where  $\eta_w$  is the wall resistivity. Equations (95) and (117) yield

$$\Delta \Psi_w = -\mu_0 \int_{r_{w-}}^{r_{w+}} r \delta j_z dr. \quad (130)$$

Suppose that the radial thickness of the wall is  $\delta_w \ll r_w$ . The previous two equations give

$$\Delta \Psi_w = \tau_w \frac{d\Psi_w}{dt}, \quad (131)$$

where

$$\tau_w = \frac{\mu_0 r_w \delta_w}{\eta_w} \quad (132)$$

is the so-called *time constant* of the wall (Nave & Wesson 1990; Fitzpatrick 1993). The thin wall approximation is valid as long as

$$\frac{r_w}{\delta_w} \gg \tau_w \left| \frac{d \ln \Psi_w}{dt} \right|. \quad (133)$$



## 2.8 Resonant Layer Physics

By analogy with Equation (131), we can write

$$\Delta\Psi_s = \tau_s \left( \frac{d\Psi_s}{dt} + i\varpi_s \Psi_s \right). \quad (134)$$

Here,  $\tau_s$  is the *reconnection time* (i.e., the typical timescale on which magnetic reconnection takes place in the resonant layer surrounding the resonant surface), whereas  $\varpi_s$  is the so-called *natural frequency*. The natural frequency is the phase velocity of the tearing mode when the wall is perfectly conducting. The natural frequency is non-zero because the reconnected flux in the resonant layer is convected by the local plasma flow (Fitzpatrick 1993).

## 2.9 Solution in Presence of External Magnetic Field-Coil

Suppose that the perfectly-conducting wall at  $r = r_c$  is replaced by a magnetic field-coil that carries a helical current possessing  $m$  periods in the poloidal direction, and  $n$  periods in the toroidal direction. Let the current density in the field-coil take the form

$$\delta j_z = \frac{I_c(t)}{r_c} \delta(r - r_c) e^{i(m\theta - n\varphi)}. \quad (135)$$

Here, the complex quantity  $I_c(t)$  parameterizes the amplitude and phase of the helical current flowing in the field-coil.

The solution in the outer region can be written

$$\psi(r, t) = \Psi_s(t) \hat{\psi}_s(r) + \Psi_w(t) \hat{\psi}_w(r) + \Psi_c \hat{\psi}_c(r), \quad (136)$$

where the real functions  $\hat{\psi}_s(r)$  and  $\hat{\psi}_w(r)$  are specified in Sections 2.5 and 2.6, respectively. Moreover, the real function  $\hat{\psi}_c(r)$  is a solution of

$$\frac{d^2 \hat{\psi}_c}{dr^2} + \frac{1}{r} \frac{d\hat{\psi}_c}{dr} - \frac{m^2}{r^2} \hat{\psi}_c \simeq 0 \quad (137)$$

that satisfies

$$\hat{\psi}_c(r \leq r_w) = 0, \quad (138)$$

$$\hat{\psi}_c(r_c) = 1, \quad (139)$$

$$\hat{\psi}_c(\infty) = 0. \quad (140)$$

It is easily seen that

$$\hat{\psi}_c(r \leq r_w) = 0, \quad (141)$$

$$\hat{\psi}_c(r_w < r \leq r_c) = \frac{(r/r_w)^m - (r/r_w)^{-m}}{(r_c/r_w)^m - (r_c/r_w)^{-m}}, \quad (142)$$

$$\hat{\psi}_c(r > r_c) = \left(\frac{r}{r_c}\right)^{-m}. \quad (143)$$

In general,  $\psi$  is continuous across the field-coil (in accordance with Maxwell's equations), whereas  $\partial\psi/\partial r$  is discontinuous. The discontinuity in  $\partial\psi/\partial r$  is caused by the helical currents flowing in the coil. The complex quantity  $\Psi_c(t)$  determines the amplitude and phase of the perturbed magnetic flux at the coil. The complex quantity

$$\Delta\Psi_c = \left[ r \frac{\partial\psi}{\partial r} \right]_{r_{c-}}^{r_{c+}} \quad (144)$$

parameterizes the amplitude and phase of the helical current sheet flowing in the coil. It follows from Equations (94), (95), and (135) that

$$\Delta\Psi_c = -\mu_0 I_c. \quad (145)$$

Simultaneously matching the outer solution across the resonant surface, the wall, and the field-coil, we obtain

$$\Delta\Psi_s = E_{ss} \Psi_s + E_{sw} \Psi_w, \quad (146)$$

$$\Delta\Psi_w = E_{ws} \Psi_s + E_{ww} \Psi_w + E_{wc} \Psi_c, \quad (147)$$

$$\Delta\Psi_c = E_{cw} \Psi_w + E_{cc} \Psi_c. \quad (148)$$

Here,

$$E_{cc} = \left[ r \frac{d\hat{\psi}_c}{dr} \right]_{r_{c-}}^{r_{c+}} = -\frac{2m}{1 - (r_w/r_c)^{2m}}, \quad (149)$$

$$E_{wc} = \left[ r \frac{d\hat{\psi}_c}{dr} \right]_{r_{w+}} = \frac{2m (r_w/r_c)^m}{1 - (r_w/r_c)^{2m}}, \quad (150)$$

$$E_{cw} = - \left[ r \frac{d\hat{\psi}_w}{dr} \right]_{r_{c-}} = \frac{2m (r_w/r_c)^m}{1 - (r_w/r_c)^{2m}}, \quad (151)$$

where use has been made of Equations (116), (142), and (143).

## 2.10 Electromagnetic Torques

The flux-surface integrated poloidal and toroidal electromagnetic torque densities acting on the plasma can be written

$$T_\theta(r) = \langle r \mathbf{j} \times \mathbf{B} \cdot \mathbf{e}_\theta \rangle \quad (152)$$

$$T_\varphi(r) = \langle R_0 \mathbf{j} \times \mathbf{B} \cdot \mathbf{e}_z \rangle, \quad (153)$$

respectively, where

$$\langle \cdots \rangle \equiv \oint \oint r R_0 (\cdots) d\theta d\varphi \quad (154)$$

is a flux-surface integration operator. However, according to Equation (80),

$$\mathbf{j} \times \mathbf{B} \simeq \nabla p. \quad (155)$$

Given that the scalar pressure is a single-valued function of  $\theta$  and  $\varphi$ , it immediately follows that  $T_\theta = T_\varphi = 0$  throughout the plasma (Fitzpatrick 1993). The only exception to this rule occurs in the immediate vicinity of the resonant surface, where Equation (155) breaks down. It follows that we can write

$$T_\theta(r) = T_{\theta s} \delta(r - r_s), \quad (156)$$

$$T_\varphi(r) = T_{\varphi s} \delta(r - r_s), \quad (157)$$

where

$$T_{\theta s} = \frac{1}{4} \int_{r_{s-}}^{r_{s+}} \oint \oint R_0 r^2 (\delta j_z \delta B_r^* + \delta j_z^* \delta B_r) dr d\theta d\varphi, \quad (158)$$

$$T_{\varphi s} = -\frac{1}{4} \int_{r_{s-}}^{r_{s+}} \oint \oint R_0^2 r (\delta j_\theta \delta B_r^* + \delta j_\theta^* \delta B_r) dr d\theta d\varphi \quad (159)$$

are the net poloidal and toroidal torques, respectively, acting at the resonant surface. Note that the zeroth-order (in perturbed quantities) torques are zero because  $B_r = 0$ . Furthermore, the linear (in perturbed quantities) torques average to zero over the flux-surface. Hence, the largest non-zero torques are quadratic in perturbed quantities. According to Equation (83),

$$\nabla \cdot \delta \mathbf{j} = i \left( \frac{m}{r} \delta j_\theta - \frac{n}{R_0} \delta j_z \right) = 0, \quad (160)$$

where  $\delta \mathbf{j}$  is the density of the current sheet flowing at the resonant surface, and we have made use of the fact that  $\delta j_r \simeq 0$ . It follows from the previous three equations that

$$T_{\varphi s} = -\frac{n}{m} T_{\theta s}. \quad (161)$$

Finally, Equations (93), (95), (158), and (161) imply that

$$T_{\theta s} = -\frac{2\pi^2 R_0 m}{\mu_0} \text{Im}(\Delta \Psi_s \Psi_s^*), \quad (162)$$

$$T_{\varphi s} = \frac{2\pi^2 R_0 n}{\mu_0} \text{Im}(\Delta \Psi_s \Psi_s^*) \quad (163)$$

(Fitzpatrick 1993).

By analogy with the previous analysis, the net poloidal and toroidal electromagnetic torques acting on the resistive wall are

$$T_{\theta w} = -\frac{2\pi^2 R_0 m}{\mu_0} \text{Im}(\Delta\Psi_w \Psi_w^*), \quad (164)$$

$$T_{\varphi w} = \frac{2\pi^2 R_0 n}{\mu_0} \text{Im}(\Delta\Psi_w \Psi_w^*), \quad (165)$$

respectively. Finally, the net poloidal and toroidal electromagnetic torques acting on the magnetic field-coil are

$$T_{\theta c} = -\frac{2\pi^2 R_0 m}{\mu_0} \text{Im}(\Delta\Psi_c \Psi_c^*), \quad (166)$$

$$T_{\varphi c} = \frac{2\pi^2 R_0 n}{\mu_0} \text{Im}(\Delta\Psi_c \Psi_c^*), \quad (167)$$

respectively.

It follows from Equations (146)–(148) that

$$\text{Im}(\Delta\Psi_s \Psi_s^*) = E_{sw} \text{Im}(\Psi_w \Psi_s^*), \quad (168)$$

$$\text{Im}(\Delta\Psi_w \Psi_w^*) = E_{ws} \text{Im}(\Psi_s \Psi_w^*) + E_{wc} \text{Im}(\Psi_c \Psi_w^*), \quad (169)$$

$$\text{Im}(\Delta\Psi_c \Psi_c^*) = E_{cw} \text{Im}(\Psi_w \Psi_c^*). \quad (170)$$

Thus,

$$\begin{aligned} \text{Im}(\Delta\Psi_s \Psi_s^*) + \text{Im}(\Delta\Psi_w \Psi_w^*) + \text{Im}(\Delta\Psi_c \Psi_c^*) &= (E_{sw} - E_{ws}) \text{Im}(\Psi_w \Psi_s^*) \\ &\quad + (E_{wc} - E_{cw}) \text{Im}(\Psi_c \Psi_w^*). \end{aligned} \quad (171)$$

However, according to Equations (124), (150), and (151),  $E_{sw} = E_{ws}$  and  $E_{wc} = E_{cw}$ . We deduce that

$$\text{Im}(\Delta\Psi_s \Psi_s^*) + \text{Im}(\Delta\Psi_w \Psi_w^*) + \text{Im}(\Delta\Psi_c \Psi_c^*) = 0. \quad (172)$$

Hence, Equations (162)–(167) yield

$$T_{\theta s} + T_{\theta w} + T_{\theta c} = 0, \quad (173)$$

$$T_{\varphi s} + T_{\varphi w} + T_{\varphi c} = 0. \quad (174)$$

In other words, the plasma/wall/field-coil system exerts zero net poloidal electromagnetic torque, and zero net toroidal electromagnetic torque, on itself.

## 2.11 Plasma Angular Equations of Motion

The sum of the electron fluid equation of motion, (69), and the ion fluid equation of motion, (72), yields the plasma equation of motion,

$$\rho \frac{\partial \mathbf{V}_i}{\partial t} + \rho (\mathbf{V}_i \cdot \nabla) \mathbf{V}_i + [\delta_i^{-2}] \nabla p + [\zeta_i^{-1}] \nabla \cdot \boldsymbol{\pi}_i - [\delta_i^{-2}] \mathbf{j} \times \mathbf{B} = 0, \quad (175)$$

where  $\rho = m_i n$  is the plasma mass density. Here, we have neglected electron inertial terms with respect to ion inertial terms (because the former are order  $m_e/m_i$  smaller than the latter). We have also neglected electron viscosity terms with respect to ion viscosity terms (because the former are order  $\sqrt{m_e/m_i}$  smaller than the latter). (See Sections 1.3 and 1.4.) Recall that the terms in square brackets are there to remind us that the terms they precede are larger than the other terms in the equation (by the corresponding terms within the brackets).

Taking the scalar product of  $r \mathbf{e}_\theta$  with the plasma equation of motion, (175), and integrating around magnetic flux-surfaces, we obtain

$$\left\langle \rho \frac{\partial(r V_{\theta i})}{\partial t} \right\rangle + \left\langle \rho \left[ V_{r i} \frac{\partial(r V_{\theta i})}{\partial r} + V_{z i} \frac{\partial(r V_{\theta i})}{\partial z} \right] \right\rangle + [\zeta_i^{-1}] \langle r \nabla \cdot \boldsymbol{\pi}_i \cdot \mathbf{e}_\theta \rangle = [\delta_i^{-2}] T_{\theta s} \delta(r - r_s), \quad (176)$$

where use has been made of Equations (152) and (156). Note that the dominant  $\nabla p$  term has averaged to zero. Moreover, because  $T_{\theta s}$  is quadratic in perturbed quantities (see Section 2.10), it is plausible that the right-hand side of the previous equation is no longer a dominant term [i.e., it is not  $\mathcal{O}(\delta_i^{-2})$  larger than the other terms in the equation]. To be more exact, if  $|\delta \mathbf{B}|/|\mathbf{B}| \sim \delta_i$  then the right-hand side ceases to be a dominant term in the equation.

The largest contribution to  $\langle r \nabla \cdot \boldsymbol{\pi}_i \cdot \mathbf{e}_\theta \rangle$  comes from the ion parallel viscosity tensor acting on the zeroth-order (in perturbed quantities) ion flow. (See Section 1.3.) However, this contribution averages to zero in a cylindrical plasma in which  $B_z$  is constant on magnetic flux-surfaces. Of course, in reality, in a large aspect-ratio tokamak plasma,  $B_z$  varies slightly around magnetic flux-surfaces, being larger on the inboard side of the torus than on the outboard side (Wesson 2011). This variation gives rise to a residual contribution to  $\langle r \nabla \cdot \boldsymbol{\pi}_i \cdot \mathbf{e}_\theta \rangle$ . It is plausible that this contribution is not a dominant term in Equation (176) [i.e., it is not  $\mathcal{O}(\zeta_i^{-1})$  larger than the other terms in the equation]. To be more exact, if the residual contribution is  $\mathcal{O}(\zeta_i)$  times smaller than the original contribution then  $\langle r \nabla \cdot \boldsymbol{\pi}_i \cdot \mathbf{e}_\theta \rangle$  ceases to be a dominant term in the equation.

According to the previous discussion, it is plausible that all terms appearing in Equation (176) are of approximately equal magnitude when the inertial and viscous terms are evaluated with the zeroth-order ion flow, which can be written

$$\mathbf{V}_i = r \Omega_\theta(r, t) \mathbf{e}_\theta + R_0 \Omega_\varphi(r, t) \mathbf{e}_z. \quad (177)$$

Here,  $\Omega_\theta(r, t)$  and  $\Omega_\varphi(r, t)$  are the ion poloidal and toroidal angular velocity profiles, respectively. When  $\langle r \nabla \cdot \boldsymbol{\pi}_i \cdot \mathbf{e}_\theta \rangle$  is evaluated with the ion parallel viscosity tensor, and the zeroth-order ion flow, it gives rise to a term that acts to relax the ion poloidal angular velocity profile toward a so-called *neoclassical profile* determined by ion density and temperature gradients (Stix 1973; Hirshman & Sigmar 1981). In principle, the contribution of the ion perpendicular viscosity tensor to  $\langle r \nabla \cdot \boldsymbol{\pi}_i \cdot \mathbf{e}_\theta \rangle$  is  $\mathcal{O}(\zeta_i^2)$  smaller than the contribution of the ion parallel viscosity tensor. (See Section 1.3.) In practice, the magnitude of the ion perpendicular viscosity tensor is greatly enhanced above the value predicted by the Braginskii equations by the action of small-scale plasma turbulence (Wesson 2011). Hence, it

is reasonable to include the contribution of the enhanced perpendicular viscosity tensor to  $\langle r \nabla \cdot \boldsymbol{\pi}_i \cdot \mathbf{e}_\theta \rangle$ . Our model form for  $\langle r \nabla \cdot \boldsymbol{\pi}_i \cdot \mathbf{e}_\theta \rangle$  is written

$$\langle r \nabla \cdot \boldsymbol{\pi}_i \cdot \mathbf{e}_\theta \rangle = 4\pi^2 R_0 \left[ \frac{\rho}{\tau_\theta} r^3 (\Omega_\theta - \Omega_{\theta \text{nc}}) - \frac{\partial}{\partial r} \left( \mu r^3 \frac{\partial \Omega_\theta}{\partial r} \right) \right]. \quad (178)$$

Here,  $\rho(r)$  is the equilibrium plasma mass density profile,  $\tau_\theta(r)$  is the *poloidal flow-damping time* (which is generally of order  $\tau_i$ ),  $\Omega_{\theta \text{nc}}(r)$  is the neoclassical poloidal angular velocity profile, and  $\mu(r)$  is a phenomenological perpendicular viscosity due to plasma turbulence.

When evaluated with the zeroth-order ion flow, Equation (176) reduces to

$$4\pi^2 R_0 \left[ \rho r^3 \frac{\partial \Omega_\theta}{\partial t} + \frac{\rho}{\tau_\theta} r^3 (\Omega_\theta - \Omega_{\theta \text{nc}}) - \frac{\partial}{\partial r} \left( \mu r^3 \frac{\partial \Omega_\theta}{\partial r} \right) \right] = T_{\theta s} \delta(r - r_s) + S_\theta, \quad (179)$$

where use has been made of Equation (178). Here, we have added a source term,  $S_\theta(r)$ , to the equation. Let  $\Omega_{\theta 0}(r)$  be the unperturbed (by the tearing mode) ion poloidal angular velocity profile. It follows that

$$S_\theta = 4\pi^2 R_0 \left[ \frac{\rho}{\tau_\theta} r^3 (\Omega_{\theta 0} - \Omega_{\theta \text{nc}}) - \frac{d}{dr} \left( \mu r^3 \frac{d\Omega_{\theta 0}}{dr} \right) \right]. \quad (180)$$

Hence, writing

$$\Omega_\theta(r, t) = \Omega_{\theta 0}(r) + \Delta\Omega_\theta(r, t), \quad (181)$$

where  $\Delta\Omega_\theta(r, t)$  is the modification to the ion poloidal angular velocity profile induced by the poloidal electromagnetic torque that develops at the resonant surface, Equation (179) yields

$$4\pi^2 R_0 \left[ \rho r^3 \frac{\partial \Delta\Omega_\theta}{\partial t} + \frac{\rho}{\tau_\theta} r^3 \Delta\Omega_\theta - \frac{\partial}{\partial r} \left( \mu r^3 \frac{\partial \Delta\Omega_\theta}{\partial r} \right) \right] = T_{\theta s} \delta(r - r_s). \quad (182)$$

There is one further refinement that we can make to the previous equation. It turns out that neoclassical poloidal flow damping gives rise to an enhancement of poloidal ion inertia by a factor of  $1 + 2q^2$  (Hirshman 1978). Hence, our final version of the perturbed plasma poloidal angular equation of motion becomes

$$4\pi^2 R_0 \left[ (1 + 2q^2) \rho r^3 \frac{\partial \Delta\Omega_\theta}{\partial t} + \frac{\rho}{\tau_\theta} r^3 \Delta\Omega_\theta - \frac{\partial}{\partial r} \left( \mu r^3 \frac{\partial \Delta\Omega_\theta}{\partial r} \right) \right] = T_{\theta s} \delta(r - r_s). \quad (183)$$

Taking the scalar product of  $R_0 \mathbf{e}_z$  with the plasma equation of motion, (175), and integrating around magnetic flux-surfaces, similar arguments to those just employed for the ion poloidal flow allow us to write the zeroth-order ion toroidal angular velocity profile in the form

$$\Omega_\varphi(r, t) = \Omega_{\varphi 0}(r) + \Delta\Omega_\varphi(r, t), \quad (184)$$

where  $\Omega_{\varphi 0}(r)$  is the unperturbed (by the tearing mode) ion toroidal angular velocity profile, and  $\Delta\Omega_\varphi(r, t)$  is the modification to this profile induced by the toroidal electromagnetic

torque that develops at the resonant surface. The perturbed ion toroidal angular equation of motion is written

$$4\pi^2 R_0^3 \left[ \rho r \frac{\partial \Delta \Omega_\varphi}{\partial t} - \frac{\partial}{\partial r} \left( \mu r \frac{\partial \Delta \Omega_\varphi}{\partial r} \right) \right] = T_{\varphi s} \delta(r - r_s). \quad (185)$$

Note that the ion parallel viscosity tensor does not give rise to damping of the toroidal flow profile. Furthermore, there is no neoclassical enhancement of the plasma toroidal ion inertia.

Equations (183) and (185) are subject to the boundary conditions

$$\frac{\partial \Delta \Omega_\theta(0, t)}{\partial r} = \frac{\partial \Delta \Omega_\varphi(0, t)}{\partial r} = 0, \quad (186)$$

$$\Delta \Omega_\theta(a, t) = \Delta \Omega_\varphi(a, t) = 0. \quad (187)$$

The boundary conditions (186) merely ensure that the ion angular velocities remain finite at the magnetic axis. On the other hand, the boundary conditions (187) are a consequence of the action of charge exchange with neutrals emitted isotropically from the wall in the edge regions of the plasma (Braun, et al., 1983; Fitzpatrick 1993; Monier-Garbet, et al., 1997). Charge exchange with neutrals gives rise to dominant damping torques acting at the edge of the plasma that relaxes the edge ion angular velocities toward particular values. Moreover, the electromagnetic torques that develop at the resonant surface are not large enough, compared with the charge-exchange torques, to modify the edge ion angular velocities (Fitzpatrick 1993).

## 2.12 Solution of Plasma Angular Equations of Motion

In general, the perturbed angular velocity profiles,  $\Delta \Omega_\theta(r, t)$  and  $\Delta \Omega_\varphi(r, t)$ , are localized in the vicinity of the resonant surface (Fitzpatrick 1993). Hence, it is reasonable to write the perturbed angular equations of motion, (183) and (185), in the simplified forms

$$4\pi^2 R_0 \left[ (1 + 2q_s^2) \rho_s r^3 \frac{\partial \Delta \Omega_\theta}{\partial t} + \frac{\rho_s}{\tau_{\theta s}} r^3 \Delta \Omega_\theta - \mu_s \frac{\partial}{\partial r} \left( r^3 \frac{\partial \Delta \Omega_\theta}{\partial r} \right) \right] = T_{\theta s} \delta(r - r_s), \quad (188)$$

$$4\pi^2 R_0^3 \left[ \rho_s r \frac{\partial \Delta \Omega_\varphi}{\partial t} - \mu_s \frac{\partial}{\partial r} \left( r \frac{\partial \Delta \Omega_\varphi}{\partial r} \right) \right] = T_{\varphi s} \delta(r - r_s), \quad (189)$$

where  $q_s = q(r_s)$ ,  $\rho_s = \rho(r_s)$ ,  $\tau_{\theta s} = \tau_\theta(r_s)$ , and  $\mu_s = \mu(r_s)$ .

Let us write

$$\Delta \Omega_\theta(r, t) = -\frac{1}{m} \sum_{p=1, \infty} \alpha_p(t) \frac{y_p(r/a)}{y_p(r_s/a)}, \quad (190)$$

$$\Delta \Omega_\varphi(r, t) = \frac{1}{n} \sum_{p=1, \infty} \beta_p(t) \frac{z_p(r/a)}{z_p(r_s/a)}, \quad (191)$$

where

$$y_p(r) = \frac{J_1(j_{1p} r/a)}{r/a}, \quad (192)$$

$$z_p(r) = J_0(j_{0p} r/a). \quad (193)$$

Here,  $J_m(z)$  is a Bessel function, and  $j_{m,p}$  denotes its  $p$ th zero. Note that Equations (190)–(193) automatically satisfy the boundary conditions (186) and (187).

It is easily demonstrated that

$$\frac{d}{dr} \left( r^3 \frac{dy_p}{dr} \right) = -\frac{j_{1p}^2 r^3 y_p}{a^2}, \quad (194)$$

$$\frac{d}{dr} \left( r \frac{dz_p}{dr} \right) = -\frac{j_{0p}^2 r z_p}{a^2}, \quad (195)$$

and

$$\int_0^a r^3 y_p(r) y_q(r) dr = \frac{a^4}{2} [J_2(j_{1p})]^2 \delta_{p,q}, \quad (196)$$

$$\int_0^a r z_p(r) z_q(r) dr = \frac{a^2}{2} [J_1(j_{0p})]^2 \delta_{p,q}. \quad (197)$$

Equations (188) and (189) yield

$$(1 + 2 q_k^2) \frac{d\alpha_p}{dt} + \left( \frac{1}{\tau_{\theta s}} + \frac{j_{1,p}^2}{\tau_{Ms}} \right) \alpha_p = \frac{m^2 [y_p(r_s/a)]^2}{\tau_A^2 \epsilon^2 [J_2(j_{1,p})]^2} \text{Im}(\Delta \hat{\Psi}_s \hat{\Psi}_s^*), \quad (198)$$

$$\frac{d\beta_p}{dt} + \frac{j_{0,p}^2}{\tau_{Ms}} \beta_p = \frac{n^2 [z_p(r_s/a)]^2}{\tau_A^2 [J_1(j_{0,p})]^2} \text{Im}(\Delta \hat{\Psi}_s \hat{\Psi}_s^*). \quad (199)$$

Here,  $\tau_{Ms} = \rho_s a^2 / \mu_s$  is the *momentum confinement time*,  $\tau_A = (\mu_0 \rho_s a^2 / B_z^2)^{1/2}$  is the *Alfvén time*,  $\epsilon = a/R_0 \ll 1$  is the *inverse aspect-ratio* of the plasma,  $\Delta \Psi_s = R_0 B_z \Delta \hat{\Psi}_s$ , and  $\Psi_s = R_0 B_z \hat{\Psi}_s$ . Moreover, use has been made of Equations (162), (163), and (190)–(197).

## 2.13 No-Slip Constraint

The reconnected magnetic flux at the resonant surface is assumed to be convected by the local plasma flow. (See Section 2.8.) Hence, changes in the plasma flow at the resonant surface induced by the electromagnetic torques that develop in the vicinity of this surface will modify the convection velocity. Consequently, the natural frequency of the reconnected flux can be written

$$\varpi_s(t) = \varpi_{s0} + (\mathbf{k} \cdot \Delta \mathbf{V}_i)_{r=r_s} = \varpi_{s0} + m \Delta \Omega_\theta(r_s, t) - n \Delta \Omega_\varphi(r_s, t), \quad (200)$$

where  $\varpi_{s0}$  is the unperturbed natural frequency. The previous expression is known as the *no-slip constraint* (Fitzpatrick 1993), and has been verified experimentally (Vahala, et al., 1980). It follows from Equations (190) and (191) that

$$\varpi_s(t) = \varpi_{s0} - \sum_{p=1, \infty} [\alpha_p(t) + \beta_p(t)]. \quad (201)$$



## 2.14 Final Equations

Equations (124), (131), (134), (145)–(151), (198), (199), and (201) can be combined to give the following complete set of equations that determine the time evolution of the reconnected magnetic flux at the resonant surface:

$$\tau_s \left( \frac{d\hat{\Psi}_s}{dt} + i \varpi_s \hat{\Psi}_s \right) = E_{ss} \hat{\Psi}_s + E_{sw} \hat{\Psi}_w, \quad (202)$$

$$\tau_w \frac{d\hat{\Psi}_w}{dt} = E_{sw} \hat{\Psi}_s + \tilde{E}_{ww} \hat{\Psi}_w + \hat{I}_c, \quad (203)$$

$$\varpi_s(t) = \varpi_{s0} - \sum_{p=1, \infty} [\alpha_p(t) + \beta_p(t)], \quad (204)$$

$$(1 + 2q_k^2) \frac{d\alpha_p}{dt} + \left( \frac{1}{\tau_{\theta s}} + \frac{j_{1,p}^2}{\tau_{Ms}} \right) \alpha_p = \frac{m^2 [y_p(r_s/a)]^2}{\tau_A^2 \epsilon^2 [J_2(j_{1,p})]^2} E_{sw} \text{Im}(\hat{\Psi}_w \hat{\Psi}_s^*), \quad (205)$$

$$\frac{d\beta_p}{dt} + \frac{j_{0,p}^2}{\tau_{Ms}} \beta_p = \frac{n^2 [z_p(r_s/a)]^2}{\tau_A^2 [J_1(j_{0,p})]^2} E_{sw} \text{Im}(\hat{\Psi}_w \hat{\Psi}_s^*). \quad (206)$$

Here,

$$\hat{I}_c = \frac{\mu_0 I_c}{R_0 B_z} \left( \frac{r_w}{r_c} \right)^m, \quad (207)$$

$$\tilde{E}_{ww} = E_{ww} + \frac{2m (r_w/r_c)^{2m}}{1 - (r_w/r_c)^{2m}}. \quad (208)$$

## 3 Reduced Drift-Magnetohydrodynamical Model

### 3.1 Introduction

Equations (202)–(208) contain two quantities—namely, the reconnection time,  $\tau_s$ , and the unperturbed natural frequency,  $\varpi_{s0}$ —that can only be determined by solving for the plasma response in the radially thin resonant layer surrounding the resonant surface. Unfortunately, determining the resonant plasma response is not a straightforward task. The problem is that the small characteristic lengthscale in the resonant region (i.e., the resonant layer width) causes the ordering parameters  $\delta_e$  and  $\delta_i$  (see Section 1.4) to take values that are of order unity. Consequently, most of the simplifications described in Section 1.5 are not applicable in the resonant layer. In particular, many of the terms in the Braginskii equations (see Section 1.3) that are negligible in the outer region (e.g., plasma resistivity) have to be taken into account in the resonant layer.

A tearing mode is a modified shear-Alfvén wave (Hazeltine & Meiss 1985), and has very little connection with the compressible-Alfvén wave. For instance, the resonance condition,  $\mathbf{k} \cdot \mathbf{B} = 0$ , which determines the position of the resonant surface, is identical to the resonance

condition for a shear-Alfvén wave, but differs substantially from that of a compressible-Alfvén wave (Fitzpatrick 2015). Hence, one very effective way of simplifying the resonant layer equations is to remove the physics of a compressible-Alfvén wave from them, in the process converting a drift-magnetohydrodynamical (MHD) model into a so-called *reduced drift-MHD model* (Strauss 1976; Hazeltine, et al. 1985; Furuya, et al. 2003). The aim of this section is to describe the reduction process (which essentially boils down to arguing that the divergence of the plasma flow is small), and to derive the reduced drift-MHD equations that will subsequently be used to model the resonant response of the plasma.

### 3.2 Drift-MHD Equations

It is helpful to define the following parameters:

$$n_0 = n(r_s), \quad (209)$$

$$p_0 = p(r_s), \quad (210)$$

$$\eta_e = \left. \frac{d \ln T_e}{d \ln n} \right|_{r=r_s}, \quad (211)$$

$$\eta_i = \left. \frac{d \ln T_i}{d \ln n} \right|_{r=r_s}, \quad (212)$$

$$\tau = \left( \frac{T_e}{T_i} \right)_{r=r_s} \left( \frac{1 + \eta_e}{1 + \eta_i} \right), \quad (213)$$

where  $n(r)$ ,  $p(r)$ ,  $T_e(r)$ , and  $T_i(r)$  refer to density, pressure, and temperature profiles that are unperturbed by the tearing mode.

Let us assume, for the sake of simplicity, that the perturbed electron and ion temperature profiles in the vicinity of the resonant layer are functions of the perturbed electron number density profile. In other words,  $T_e = T_e(n)$  and  $T_i = T_i(n)$ . It follows that the perturbed total pressure profile is also a function of the perturbed electron number density profile: that is,  $p = p(n)$ . Let us define

$$\mathbf{V}_* = \frac{\mathbf{b} \times \nabla p}{e n_0 B_z}. \quad (214)$$

To lowest order, the electron and ion diamagnetic velocities take the respective forms

$$\mathbf{V}_{*e} = - \left( \frac{\tau}{1 + \tau} \right) \mathbf{V}_*, \quad (215)$$

$$\mathbf{V}_{*i} = \left( \frac{1}{1 + \tau} \right) \mathbf{V}_*. \quad (216)$$

(See Section 1.5.) The so-called *MHD velocity* is defined

$$\mathbf{V} = \mathbf{V}_E + V_{\parallel i} \mathbf{b}, \quad (217)$$

where  $\mathbf{V}_E$  is the  $\mathbf{E} \times \mathbf{B}$  velocity, and  $V_{\parallel i}$  is the parallel component of the ion fluid velocity. The lowest order electron and ion fluid velocities take the respective forms:

$$\mathbf{V}_e = \mathbf{V} + \mathbf{V}_{*i} - \frac{\mathbf{j}}{n_0 e}, \quad (218)$$

$$\mathbf{V}_i = \mathbf{V} + \mathbf{V}_{*i}. \quad (219)$$

(See Section 1.5.)

Following Hazeltine & Meiss 1992, if we neglect electron inertia and electron viscosity in the electron equation of motion, (9), then we obtain the *generalized Ohm's law*:

$$\mathbf{E} + \mathbf{V} \times \mathbf{B} + \frac{1}{e n_0} \left[ \nabla p + \frac{1}{1 + \tau} \left( \frac{0.71 \eta_e \tau}{1 + \eta_e} - 1 \right) (\mathbf{b} \cdot \nabla p) \mathbf{b} - \mathbf{j} \times \mathbf{b} \right] \simeq \eta_{\parallel} \mathbf{j}_{\parallel} + \eta_{\perp} \mathbf{j}_{\perp}. \quad (220)$$

Here,  $\eta_{\parallel} = 1/\sigma_{\parallel}$  and  $\eta_{\perp} = 1/\sigma_{\perp}$  are the parallel and perpendicular plasma resistivities, respectively. (See Section 1.3.) We have neglected the cross term in Equation (15) because it is a factor  $(\Omega_e \tau_e)^{-1}$  smaller than  $\nabla p$ .

Next, we can add the electron and ion equations of motion, (9) and (12), again neglecting electron inertia and electron viscosity, to give the *plasma equation of motion*:

$$n_0 m_i \left[ \frac{\partial \mathbf{V}}{\partial t} + (\mathbf{V} \cdot \nabla) \mathbf{V} + \frac{1}{1 + \tau} (\mathbf{V}_* \cdot \nabla) \mathbf{V}_E \right] + \nabla p + \nabla \cdot \boldsymbol{\pi}_i - \mathbf{j} \times \mathbf{B} \simeq 0. \quad (221)$$

Here,  $\nabla \cdot \boldsymbol{\pi}_i$  includes the contribution from the anomalous perpendicular viscosity tensor. The contribution from the gyroviscosity tensor, which is the same size as the ion inertial terms, has already been incorporated into the equation (Hazeltine & Meiss 1992). We are neglecting the contribution of the parallel viscosity tensor because we expect it to be much smaller than its nominal magnitude in a large aspect-ratio tokamak plasma.

Finally, we can combine the electron and ion energy evolution equations, (10) and (13), to obtain a *plasma energy evolution equation*:

$$\frac{\partial p}{\partial t} + \mathbf{V} \cdot \nabla p + \Gamma p \nabla \cdot \mathbf{V} + \frac{2}{3} \nabla \cdot \mathbf{q} \simeq 0, \quad (222)$$

where  $\Gamma = 5/3$ . Here, we have neglected a number of terms (e.g., the ohmic heating terms) because they are, at least, factors  $(\Omega_e \tau_e)^{-1}$  or  $(\Omega_i \tau_i)^{-1}$  smaller than  $\nabla \cdot \mathbf{q}$ . We have also neglected the viscous heating term because we expect the dominant contribution, which comes from the parallel viscosity, to be much smaller than its nominal magnitude in a large aspect-ratio tokamak plasma.

Equations (220)–(222) are known collectively as the *drift-MHD equations*, and contain both shear-Alfvén and compressible-Alfvén wave dynamics. The system of equations is completed by Maxwell's equations:

$$\nabla \cdot \mathbf{B} = 0, \quad (223)$$

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}, \quad (224)$$

$$\mu_0 \mathbf{j} = \nabla \times \mathbf{B}. \quad (225)$$

### 3.3 Normalization Scheme

Let  $L$  be a typical variation lengthscale in the resonant layer. The *Alfvén velocity*, which is the typical phase velocity of compressible Alfvén waves, is defined

$$V_A = \frac{B_z}{\sqrt{\mu_0 n_0 m_i}}. \quad (226)$$

It is helpful to define the *collisionless ion skin-depth*:

$$d_i = \left( \frac{m_i}{n_0 e^2 \mu_0} \right)^{1/2}. \quad (227)$$

It is convenient to adopt the following normalization scheme that renders all quantities in the drift-MHD equations dimensionless:  $\hat{\nabla} = L \nabla$ ,  $\hat{d}_i = d_i/L$ ,  $\hat{t} = t/(L/V_A)$ ,  $\hat{\mathbf{B}} = \mathbf{B}/B_z$ ,  $\hat{\mathbf{E}} = \mathbf{E}/(B_z V_A)$ ,  $\hat{\mathbf{j}} = \mathbf{j}/(B_z/\mu_0 L)$ ,  $\hat{\eta}_{\parallel, \perp} = \eta_{\parallel, \perp}/(\mu_0 V_A L)$ ,  $\hat{\mathbf{V}} = \mathbf{V}/V_A$ ,  $\hat{\mathbf{V}}_{*,i} = \mathbf{V}_{*,i}/V_A$ ,  $\hat{V}_{\parallel i} = V_{\parallel i}/V_A$ ,  $\hat{p} = p/(B_z^2/\mu_0)$ ,  $\hat{p}_0 = p_0/(B_z^2/\mu_0)$ ,  $\hat{\boldsymbol{\pi}}_i = \boldsymbol{\pi}_i/(B_z^2/\mu_0)$ ,  $\hat{\mathbf{q}} = \mathbf{q}/(B_z^2 V_A/\mu_0)$ . Equations (220)–(225) yield

$$\hat{\mathbf{E}} + \hat{\mathbf{V}} \times \hat{\mathbf{B}} + \hat{d}_i \left[ \hat{\nabla} \hat{p} + \frac{1}{1+\tau} \left( \frac{0.71 \eta_e \tau}{1+\eta_e} - 1 \right) (\mathbf{b} \cdot \hat{\nabla} \hat{p}) \mathbf{b} + \hat{\nabla} \cdot \hat{\boldsymbol{\pi}}_e - \hat{\mathbf{j}} \times \hat{\mathbf{b}} \right] \simeq \hat{\eta}_{\parallel} \hat{\mathbf{j}}_{\parallel} + \hat{\eta}_{\perp} \hat{\mathbf{j}}_{\perp}, \quad (228)$$

$$\frac{\partial \hat{\mathbf{V}}}{\partial \hat{t}} + (\hat{\mathbf{V}} \cdot \hat{\nabla}) \hat{\mathbf{V}} + \frac{1}{1+\tau} (\hat{\mathbf{V}}_* \cdot \hat{\nabla}) \hat{\mathbf{V}}_E + \hat{\nabla} \hat{p} + \hat{\nabla} \cdot \hat{\boldsymbol{\pi}}_i - \hat{\mathbf{j}} \times \hat{\mathbf{B}} \simeq 0, \quad (229)$$

$$\frac{\partial \hat{p}}{\partial \hat{t}} + \hat{\mathbf{V}} \cdot \hat{\nabla} \hat{p} + \Gamma \hat{p} \hat{\nabla} \cdot \hat{\mathbf{V}} + \frac{2}{3} \hat{\nabla} \cdot \hat{\mathbf{q}} \simeq 0, \quad (230)$$

and

$$\hat{\nabla} \cdot \hat{\mathbf{B}} = 0, \quad (231)$$

$$\hat{\nabla} \times \hat{\mathbf{E}} = -\frac{\partial \hat{\mathbf{B}}}{\partial \hat{t}}, \quad (232)$$

$$\hat{\mathbf{j}} = \hat{\nabla} \times \hat{\mathbf{B}}. \quad (233)$$

Finally,

$$\hat{\mathbf{V}}_E = \hat{\mathbf{E}} \times \mathbf{b}, \quad (234)$$

$$\hat{\mathbf{V}} = \hat{\mathbf{V}}_E + \hat{V}_{\parallel i} \mathbf{b}, \quad (235)$$

$$\hat{\mathbf{V}}_* = \hat{d}_i \mathbf{b} \times \hat{\nabla} \hat{p}, \quad (236)$$

$$\hat{\mathbf{V}}_i = \hat{\mathbf{V}} + \frac{\hat{\mathbf{V}}_{*,i}}{1+\tau}. \quad (237)$$

### 3.4 Reduction Process

All variables in the resonant layer are assumed to be functions of  $\hat{x} = (r - r_s)/L$  and  $\zeta = m\theta - n\varphi$ . Let  $\mathbf{n} = (0, \epsilon_s/q_s, 1)$ . It follows that  $\mathbf{n} \cdot \nabla A$  for any  $A(\hat{x}, \zeta)$ . Let us write

$$\hat{\mathbf{B}} \simeq (1 + \delta b) \mathbf{n} + \hat{\nabla} \psi \times \mathbf{n}, \quad (238)$$

which automatically satisfies Equation (231). Here,  $\delta b(\hat{x}, \zeta)$  and  $\psi(\hat{x}, \zeta)$  are assumed to be small compared to unity, which merely indicates that the perturbed magnetic field due to the tearing mode is small compared to the equilibrium magnetic field. We can write

$$\hat{\mathbf{E}} \simeq \left( \hat{E}_{\parallel} - \frac{\partial \psi}{\partial \hat{t}} \right) \mathbf{n} + \hat{\nabla} \left( \frac{\partial \chi}{\partial \hat{t}} \right) \times \mathbf{n} + \hat{\nabla} \phi, \quad (239)$$

which automatically satisfies Equation (232) provided that

$$\hat{\nabla}^2 \chi = \delta b. \quad (240)$$

Here,  $\hat{E}_{\parallel} = E_{\parallel}/(B_z V_A)$  represents the constant inductive electric field that drives the equilibrium plasma current in the vicinity of the resonant surface. Now,  $\partial/\partial \hat{t}$  and  $\phi(\hat{x}, \zeta)$  are assumed to be first order in small quantities, whereas  $\hat{E}_{\parallel}$  is assumed to be second order. It follows that

$$\hat{\mathbf{V}}_E \simeq \hat{\nabla} \phi \times \mathbf{n}, \quad (241)$$

$$\hat{\mathbf{V}} \simeq \hat{V}_{\parallel i} \mathbf{n} + \hat{\nabla} \phi \times \mathbf{n} + \hat{\nabla} \Xi, \quad (242)$$

where  $\hat{V}_{\parallel i}(\hat{x}, \zeta)$  is assumed to be first order in small quantities, whereas  $\Xi(\hat{x}, \zeta)$  is assumed to be second order. We can write

$$\hat{p} \simeq \frac{\beta}{\Gamma} + \delta p, \quad (243)$$

where

$$\beta = \Gamma \hat{p}_0 = \frac{\Gamma p_0 \mu_0}{B_z^2}. \quad (244)$$

Here,  $\delta p(\hat{x}, \zeta)$  is assumed to be first order in small quantities. It follows that

$$\hat{\mathbf{V}}_* \simeq \hat{d}_i \mathbf{n} \times \hat{\nabla} \delta p, \quad (245)$$

$$\hat{\mathbf{V}}_i \simeq \hat{V}_{\parallel i} \mathbf{n} + \hat{\nabla} \left( \phi - \frac{\hat{d}_i \delta p}{1 + \tau} \right) \times \mathbf{n}. \quad (246)$$

The normalized drift-MHD equations, (228)–(230), yield

$$\begin{aligned} & \hat{d}_i \hat{\nabla} (\delta p + \delta b) \\ & + \left( \hat{E}_{\parallel} - \frac{\partial \psi}{\partial \hat{t}} - [\psi, \phi] + \frac{\hat{d}_i [\psi, \delta p]}{1 + \tau} \left( 1 - \frac{0.71 \eta_e \tau}{1 + \eta_e} \right) + \hat{d}_i [\psi, \delta b] + \hat{\eta}_{\parallel} \hat{\nabla}^2 \psi \right) \mathbf{n} \end{aligned}$$

$$+\hat{\nabla}\left(\frac{\partial\chi}{\partial\hat{t}}+\Xi-\hat{\eta}_\perp\delta b\right)\times\mathbf{n}-b_z\hat{\nabla}\phi+\hat{V}_{\parallel i}\hat{\nabla}\psi+\hat{d}_i\delta b\hat{\nabla}\delta b+\hat{d}_i\hat{\nabla}^2\psi\hat{\nabla}\psi\simeq 0, \quad (247)$$

$$\begin{aligned} & \hat{\nabla}(\delta p+\delta b)+\left(\frac{\partial\hat{V}_{\parallel i}}{\partial\hat{t}}+[\hat{V}_{\parallel i},\phi]+[\psi,\delta b]\right)\mathbf{n} \\ & +\hat{\nabla}\left(\frac{\partial\phi}{\partial\hat{t}}-\frac{\hat{d}_i[\phi,\delta p]}{2(1+\tau)}\right)\times\mathbf{n}+\frac{1}{2}\hat{\nabla}\left(\hat{V}_\perp^2+\frac{\hat{\mathbf{V}}_*\cdot\hat{\mathbf{V}}_E}{1+\tau}+\delta b^2\right) \\ & -\hat{\nabla}^2\phi\hat{\nabla}\phi+\frac{\hat{d}_i}{2(1+\tau)}\left(\hat{\nabla}^2\phi\hat{\nabla}\delta p+\hat{\nabla}^2\delta p\hat{\nabla}\phi\right)+\hat{\nabla}^2\psi\hat{\nabla}\psi+\hat{\nabla}\cdot\hat{\boldsymbol{\pi}}_i\simeq 0, \end{aligned} \quad (248)$$

$$\frac{\partial\delta p}{\partial\hat{t}}+[\delta p,\phi]+\beta\hat{\nabla}^2\Xi+\frac{2}{3}\hat{\nabla}\cdot\hat{\mathbf{q}}\simeq 0, \quad (249)$$

where use has been made of Equation (233), and

$$[A,B]\equiv\hat{\nabla}A\times\hat{\nabla}B\cdot\mathbf{n}. \quad (250)$$

Here,  $\hat{d}_i$  and  $\beta$  are assumed to be zeroth order in small quantities,  $\hat{\eta}_\parallel$  and  $\hat{\eta}_\perp$  are assumed to be first order, while  $\hat{\nabla}\cdot\hat{\boldsymbol{\pi}}_i$  and  $\hat{\nabla}\cdot\hat{\mathbf{q}}$  are assumed to be second order.

To first order in small quantities, both Equations (247) and (248) yield

$$\delta b\simeq-\delta p, \quad (251)$$

which is an expression of lowest-order force balance. The scalar product of Equation (247) with  $\mathbf{n}$  gives

$$\frac{\partial\psi}{\partial\hat{t}}\simeq[\phi,\psi]+\hat{d}_i\left(\frac{\tau}{1+\tau}\right)\left(1+\frac{0.71\eta_e}{1+\eta_e}\right)[\delta p,\psi]+\hat{\eta}_\parallel J+\hat{E}_\parallel, \quad (252)$$

where

$$J=\hat{\nabla}^2\psi. \quad (253)$$

The scalar product of Equation (248) with  $\mathbf{n}$  yields

$$\frac{\partial\hat{V}_{\parallel i}}{\partial\hat{t}}\simeq[\phi,\hat{V}_{\parallel i}]-[\delta p,\psi]-\mathbf{n}\cdot\hat{\nabla}\cdot\hat{\boldsymbol{\pi}}_i. \quad (254)$$

The scalar product of the curl of Equation (247) with  $\mathbf{n}$  gives

$$\frac{\partial\delta p}{\partial\hat{t}}\simeq[\phi,\delta p]+\hat{\nabla}^2\Xi-[\hat{V}_{\parallel i},\psi]-\hat{d}_i[J,\psi]+\hat{\eta}_\perp\hat{\nabla}^2\delta p. \quad (255)$$

Eliminating  $\hat{\nabla}^2\Xi$  between Equation (249) and the previous equation, we obtain

$$\frac{\partial\delta p}{\partial\hat{t}}\simeq[\phi,\delta p]-c_\beta^2[\hat{V}_{\parallel i},\psi]-c_\beta^2\hat{d}_i[J,\psi]-\frac{2}{3}(1-c_\beta^2)\hat{\nabla}\cdot\hat{\mathbf{q}}+c_\beta^2\hat{\eta}_\perp\hat{\nabla}^2\delta p, \quad (256)$$

where

$$c_\beta = \sqrt{\frac{\beta}{1+\beta}}. \quad (257)$$

Finally, the scalar product of the curl of Equation (248) with  $\mathbf{n}$  gives

$$\begin{aligned} \frac{\partial U}{\partial \hat{t}} &\simeq [\phi, U] + \frac{\hat{d}_i}{2(1+\tau)} \left( \hat{\nabla}^2 [\phi, \delta p] + [\hat{\nabla}^2 \phi, \delta p] + [\hat{\nabla}^2 \delta p, \phi] \right) + [J, \psi] \\ &\quad + \mathbf{n} \cdot \hat{\nabla} \times \hat{\nabla} \cdot \hat{\boldsymbol{\pi}}_i, \end{aligned} \quad (258)$$

where

$$U = \hat{\nabla}^2 \phi. \quad (259)$$

We can write

$$\begin{aligned} \hat{\nabla} \cdot \hat{\mathbf{q}} &\simeq - \left( \frac{\eta_e}{1+\eta_e} \frac{\tau}{1+\tau} \hat{\chi}_{\parallel e} + \frac{\eta_i}{1+\eta_i} \frac{1}{1+\tau} \hat{\chi}_{\parallel i} \right) [[\delta p, \psi], \psi] \\ &\quad - \left( \frac{\eta_e}{1+\eta_e} \frac{\tau}{1+\tau} \hat{\chi}_{\perp e} + \frac{\eta_i}{1+\eta_i} \frac{1}{1+\tau} \hat{\chi}_{\perp i} \right) \nabla_{\perp}^2 \delta p, \end{aligned} \quad (260)$$

where  $\chi_{\parallel e,i} = \kappa_{\parallel e,i}/n_0$ ,  $\chi_{\perp e,i} = \kappa_{\perp e,i}/n_0$ ,  $\hat{\chi}_{\parallel e,i} = \chi_{\parallel e,i}/(L V_A)$ ,  $\hat{\chi}_{\perp e,i} = \chi_{\perp e,i}/(L V_A)$ , and use has been made of Equations (20), (21), (211)–(213), and (238). We can also write

$$\hat{\nabla} \cdot \hat{\boldsymbol{\pi}}_i \simeq -\hat{\chi}_\phi \hat{\nabla}^2 \hat{\mathbf{V}}_i, \quad (261)$$

where  $\chi_\phi = \mu_{\perp i}/(n_0 m_i)$ ,  $\hat{\chi}_\phi = \chi_\phi/(L V_A)$ , and  $\mu_{\perp}$  is the anomalous ion perpendicular viscosity. It is easily seen that

$$\mathbf{n} \cdot \hat{\nabla} \cdot \hat{\boldsymbol{\pi}}_i \simeq -\hat{\chi}_\phi \hat{\nabla}^2 \hat{V}_{\parallel i}, \quad (262)$$

$$\mathbf{n} \cdot \hat{\nabla} \times \hat{\nabla} \cdot \hat{\boldsymbol{\pi}}_i \simeq \hat{\chi}_{\perp} \hat{\nabla}^4 \left( \phi - \frac{\hat{d}_i \delta p}{1+\tau} \right). \quad (263)$$

Let us define  $V = \hat{V}_{\parallel i}$  and  $N = c_\beta \delta p$ . Equations (252)–(254), (256), (258)–(260), (262), and (263) yield the following closed set of equations:

$$\frac{\partial \psi}{\partial \hat{t}} \simeq [\phi, \psi] + \hat{d}_\beta \left( \frac{\tau}{1+\tau} \right) \left( 1 + \frac{0.71 \eta_e}{1+\eta_e} \right) [N, \psi] + \hat{\eta}_{\parallel} J + \hat{E}_{\parallel}, \quad (264)$$

$$\begin{aligned} \frac{\partial U}{\partial \hat{t}} &\simeq [\phi, U] + \frac{\hat{d}_\beta}{2(1+\tau)} \left( \hat{\nabla}^2 [\phi, N] + [\hat{\nabla}^2 \phi, N] + [\hat{\nabla}^2 N, \phi] \right) + [J, \psi] \\ &\quad + \hat{\chi}_{\perp} \hat{\nabla}^4 \left( \phi - \frac{\hat{d}_\beta N}{1+\tau} \right), \end{aligned} \quad (265)$$

$$\frac{\partial N}{\partial \hat{t}} \simeq [\phi, N] - c_\beta [V, \psi] - \hat{d}_\beta [J, \psi] + \hat{D}_{\parallel} [[N, \psi], \psi] + \hat{D}_{\perp} \hat{\nabla}^2 N, \quad (266)$$

$$\frac{\partial V}{\partial t} \simeq [\phi, V] - c_\beta [N, \psi] + \hat{\chi}_\phi \hat{\nabla}^2 V, \quad (267)$$

$$J = \hat{\nabla}^2 \psi, \quad (268)$$

$$U = \hat{\nabla}^2 \phi. \quad (269)$$

Here,

$$d_\beta = c_\beta d_i, \quad (270)$$

and  $\hat{d}_\beta = d_\beta/L$ . Moreover,

$$\hat{D}_\parallel = \frac{2}{3} (1 - c_\beta^2) \left( \frac{\eta_e}{1 + \eta_e} \frac{\tau}{1 + \tau} \hat{\chi}_{\parallel e} + \frac{\eta_i}{1 + \eta_i} \frac{1}{1 + \tau} \hat{\chi}_{\parallel i} \right), \quad (271)$$

$$\hat{D}_\perp = c_\beta^2 \hat{\eta}_\perp + \frac{2}{3} (1 - c_\beta^2) \left( \frac{\eta_e}{1 + \eta_e} \frac{\tau}{1 + \tau} \hat{\chi}_{\perp e} + \frac{\eta_i}{1 + \eta_i} \frac{1}{1 + \tau} \hat{\chi}_{\perp i} \right). \quad (272)$$

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