

Tearing Modes in Tokamak Plasmas

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1 Fluid Theory

1.1 Fundamental Quantities

Consider an idealized tokamak plasma consisting of an equal number of electrons, with mass m_e and charge $-e$ (here, e denotes the magnitude of the electron charge), and ions, with mass m_i and charge $+e$. We shall employ the symbol

$$T_s = \frac{1}{3} m_s \langle v_s^2 \rangle \quad (1)$$

to denote a *kinetic temperature* measured in units of energy. Here, v is a particle speed, and the angular brackets denote an ensemble average (Reif 1965). The kinetic temperature of species s is a measure of the mean kinetic energy of particles of that species. (Here, s represents either e for electrons, or i for ions.) In tokamak plasma physics, kinetic temperature is invariably measured in *electron-volts* (1 joule is equivalent to 6.24×10^{18} eV).

Quasi-neutrality demands that

$$n_i \simeq n_e, \quad (2)$$

where n_s is the *particle number density* (that is, the number of particles per cubic meter) of species s (Fitzpatrick 2015).

We can estimate typical particle speeds in terms of the so-called *thermal speed*,

$$v_{ts} = \left(\frac{2T_s}{m_s} \right)^{1/2}. \quad (3)$$

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In a tokamak plasma, the ambient magnetic field, \mathbf{B} , is strong enough to significantly alter charged particle trajectories. In particular, magnetized plasmas are highly anisotropic, responding differently to forces that are parallel and perpendicular to the direction of \mathbf{B} . As is well known, charged particles respond to the Lorentz force by freely streaming in the direction of \mathbf{B} , while executing circular *gyro-orbits* in the plane perpendicular to \mathbf{B} (Fitzpatrick 2008). The typical *gyroradius* of a charged particle gyrating in a magnetic field is given by

$$\rho_s = \frac{v_{ts}}{\Omega_s}, \quad (4)$$

where

$$\Omega_s = \frac{e B}{m_s} \quad (5)$$

is the *gyrofrequency* associated with the gyration.

The electron-ion and ion-ion *collision times* are written

$$\tau_e = \frac{6\sqrt{2}\pi^{3/2} \epsilon_0^2 \sqrt{m_e} T_e^{3/2}}{\ln \Lambda_c e^4 n_e}, \quad (6)$$

and

$$\tau_i = \frac{12\pi^{3/2} \epsilon_0^2 \sqrt{m_i} T_i^{3/2}}{\ln \Lambda_c e^4 n_e}, \quad (7)$$

respectively (Fitzpatrick 2015). Here, $\ln \Lambda_c \simeq 15$ is the *Coulomb logarithm* (Richardson 2019). Note that τ_e is the typical time required for the cumulative effect of electron-ion collisions to deviate the path of an electron through 90° . Likewise, τ_i is the typical time required for the cumulative effect of ion-ion collisions to deviate the path of an ion through 90° .

1.2 Braginskii Equations

The electron and ion fluid equations in a collisional plasma take the form:

$$\frac{dn}{dt} + n \nabla \cdot \mathbf{V}_e = 0, \quad (8)$$

$$m_e n \frac{d\mathbf{V}_e}{dt} + \nabla p_e + \nabla \cdot \boldsymbol{\pi}_e + e n (\mathbf{E} + \mathbf{V}_e \times \mathbf{B}) = \mathbf{F}, \quad (9)$$

$$\frac{3}{2} \frac{dp_e}{dt} + \frac{5}{2} p_e \nabla \cdot \mathbf{V}_e + \boldsymbol{\pi}_e : \nabla \mathbf{V}_e + \nabla \cdot \mathbf{q}_e = w_e, \quad (10)$$

and

$$\frac{dn}{dt} + n \nabla \cdot \mathbf{V}_i = 0, \quad (11)$$

$$m_i n \frac{d\mathbf{V}_i}{dt} + \nabla p_i + \nabla \cdot \boldsymbol{\pi}_i - e n (\mathbf{E} + \mathbf{V}_i \times \mathbf{B}) = -\mathbf{F}, \quad (12)$$

$$\frac{3}{2} \frac{dp_i}{dt} + \frac{5}{2} p_i \nabla \cdot \mathbf{V}_i + \boldsymbol{\pi}_i : \nabla \mathbf{V}_i + \nabla \cdot \mathbf{q}_i = w_i, \quad (13)$$

respectively. Equations (8)–(10) and (11)–(13) are called the *Braginskii equations*, because they were first obtained in a celebrated article by S.I. Braginskii (Braginskii 1965). Here, \mathbf{V}_s is the species- s flow velocity, $p_s = n T_s$ is the species- s scalar pressure, $\boldsymbol{\pi}_s$ is the species- s viscosity tensor, \mathbf{F} is the collisional friction force density, \mathbf{q}_s is the species- s heat flux density, w_s is the species- s collisional heating rate density, and \mathbf{E} is the ambient electric field strength. Moreover, $d/dt \equiv \partial/\partial t + \mathbf{V}_e \cdot \nabla$ in the electron fluid equations, (8)–(10), whereas $d/dt \equiv \partial/\partial t + \mathbf{V}_i \cdot \nabla$ in the ion fluid equations, (11)–(13).

A tokamak plasma is highly magnetized. In other words,

$$\Omega_i \tau_i, \quad \Omega_e \tau_e \gg 1, \quad (14)$$

which implies that the electron and ion gyroradii are much smaller than the corresponding mean-free-paths between 90° collisional scattering events. In this limit, a standard two-Laguerre-polynomial Chapman-Enskog closure scheme (Chapman & Cowling 1953) yields

$$\mathbf{F} = n e \left(\frac{\mathbf{j}_\parallel}{\sigma_\parallel} + \frac{\mathbf{j}_\perp}{\sigma_\perp} \right) - 0.71 n \nabla_\parallel T_e - \frac{3 n}{2 \Omega_e \tau_e} \mathbf{b} \times \nabla_\perp T_e, \quad (15)$$

$$w_i = \frac{3 m_e}{m_i} \frac{n (T_e - T_i)}{\tau_e}, \quad (16)$$

$$w_e = -w_i + \frac{\mathbf{j} \cdot \mathbf{F}}{n e}. \quad (17)$$

Here, $\mathbf{b} = \mathbf{B}/B$ is a unit vector parallel to the magnetic field, and $\mathbf{j} = n e (\mathbf{V}_i - \mathbf{V}_e)$ is the net plasma current density. Moreover, the *parallel electrical conductivity*, σ_\parallel , is given by

$$\sigma_\parallel = 1.96 \frac{n e^2 \tau_e}{m_e}. \quad (18)$$

whereas the *perpendicular electrical conductivity*, σ_\perp , takes the form

$$\sigma_\perp = 0.51 \sigma_\parallel = \frac{n e^2 \tau_e}{m_e}. \quad (19)$$

Note that $\nabla_\parallel(\dots) \equiv [\mathbf{b} \cdot \nabla(\dots)]$ \mathbf{b} denotes a gradient parallel to the magnetic field, whereas $\nabla_\perp \equiv \nabla - \nabla_\parallel$ denotes a gradient perpendicular to the magnetic field. Likewise, $\mathbf{j}_\parallel \equiv (\mathbf{b} \cdot \mathbf{j}) \mathbf{b}$ represents the component of the plasma current flowing parallel to the magnetic field, whereas $\mathbf{j}_\perp \equiv \mathbf{j} - \mathbf{j}_\parallel$ represents the perpendicular component of the plasma current.

In a highly magnetized plasma, the electron and ion heat flux densities are written

$$\mathbf{q}_e = -\kappa_\parallel^e \nabla_\parallel T_e - \kappa_\perp^e \nabla_\perp T_e - \kappa_\times^e \mathbf{b} \times \nabla_\perp T_e - 0.71 \frac{T_e}{e} \mathbf{j}_\parallel - \frac{3 T_e}{2 \Omega_e \tau_e e} \mathbf{b} \times \mathbf{j}_\perp, \quad (20)$$

$$\mathbf{q}_i = -\kappa_\parallel^i \nabla_\parallel T_i - \kappa_\perp^i \nabla_\perp T_i + \kappa_\times^i \mathbf{b} \times \nabla_\perp T_i, \quad (21)$$

respectively. Here, the *parallel thermal conductivities*, which control the diffusion of heat parallel to magnetic field-lines, are given by

$$\kappa_{\parallel}^e = 3.2 \frac{n \tau_e T_e}{m_e}, \quad (22)$$

$$\kappa_{\parallel}^i = 3.9 \frac{n \tau_i T_i}{m_i}, \quad (23)$$

whereas the *perpendicular thermal conductivities*, which control the diffusion of heat perpendicular to magnetic flux-surfaces, take the form

$$\kappa_{\perp}^e = 4.7 \frac{n T_e}{m_e \Omega_e^2 \tau_e}, \quad (24)$$

$$\kappa_{\perp}^i = 2 \frac{n T_i}{m_i \Omega_i^2 \tau_i}. \quad (25)$$

Finally, the *cross thermal conductivities*, which control the flow of heat within magnetic flux-surfaces, are written

$$\kappa_{\times}^e = \frac{5 n T_e}{2 m_e \Omega_e}, \quad (26)$$

$$\kappa_{\times}^i = \frac{5 n T_i}{2 m_i \Omega_i}. \quad (27)$$

In order to describe the viscosity tensor in a magnetized plasma, it is helpful to define the *rate-of-strain tensor*

$$W_{\alpha\beta} = \frac{\partial V_{\alpha}}{\partial r_{\beta}} + \frac{\partial V_{\beta}}{\partial r_{\alpha}} - \frac{2}{3} \nabla \cdot \mathbf{V} \delta_{\alpha\beta}. \quad (28)$$

Obviously, there is a separate rate-of-strain tensor for the electron and ion fluids. It is easily demonstrated that this tensor is zero if the plasma translates, or rotates as a rigid body, or if it undergoes isotropic compression. Thus, the rate-of-strain tensor measures the deformation of plasma volume elements.

In a highly magnetized plasma, the viscosity tensor is best described as the sum of five component tensors,

$$\boldsymbol{\pi} = \sum_{n=0,4} \boldsymbol{\pi}_n, \quad (29)$$

where

$$\boldsymbol{\pi}_0 = -3 \eta_0 \left(\mathbf{b}\mathbf{b} - \frac{1}{3} \mathbf{I} \right) \left(\mathbf{b}\mathbf{b} - \frac{1}{3} \mathbf{I} \right) : \nabla \mathbf{V}, \quad (30)$$

with

$$\boldsymbol{\pi}_1 = -\eta_1 \left[\mathbf{I}_{\perp} \cdot \mathbf{W} \cdot \mathbf{I}_{\perp} + \frac{1}{2} \mathbf{I}_{\perp} (\mathbf{b} \cdot \mathbf{W} \cdot \mathbf{b}) \right], \quad (31)$$

and

$$\boldsymbol{\pi}_2 = -4 \eta_1 (\mathbf{I}_{\perp} \cdot \mathbf{W} \cdot \mathbf{b}\mathbf{b} + \mathbf{b}\mathbf{b} \cdot \mathbf{W} \cdot \mathbf{I}_{\perp}). \quad (32)$$

plus

$$\boldsymbol{\pi}_3 = \frac{\eta_3}{2} (\mathbf{b} \times \mathbf{W} \cdot \mathbf{I}_\perp - \mathbf{I}_\perp \cdot \mathbf{W} \times \mathbf{b}), \quad (33)$$

and

$$\boldsymbol{\pi}_4 = 2\eta_3 (\mathbf{b} \times \mathbf{W} \cdot \mathbf{b}\mathbf{b} - \mathbf{b}\mathbf{b} \cdot \mathbf{W} \times \mathbf{b}). \quad (34)$$

Here, \mathbf{I} is the identity tensor, and $\mathbf{I}_\perp = \mathbf{I} - \mathbf{b}\mathbf{b}$. The previous expressions are valid for both electrons and ions.

The tensor $\boldsymbol{\pi}_0$ describes what is known as *parallel viscosity*. This is a viscosity that controls the variation along magnetic field-lines of the velocity component parallel to field-lines. The parallel viscosity coefficients are given by

$$\eta_0^e = 0.73 n \tau_e T_e, \quad (35)$$

$$\eta_0^i = 0.96 n \tau_i T_i, \quad (36)$$

The tensors $\boldsymbol{\pi}_1$ and $\boldsymbol{\pi}_2$ describe what is known as *perpendicular viscosity*. This is a viscosity that controls the variation perpendicular to magnetic field-lines of the velocity components perpendicular to field-lines. The perpendicular viscosity coefficients are given by

$$\eta_1^e = 0.51 \frac{n T_e}{\Omega_e^2 \tau_e}, \quad (37)$$

$$\eta_1^i = \frac{3 n T_i}{10 \Omega_i^2 \tau_i}. \quad (38)$$

Finally, the tensors $\boldsymbol{\pi}_3$ and $\boldsymbol{\pi}_4$ describe what is known as *gyroviscosity*. This is not really viscosity at all, because the associated viscous stresses are always perpendicular to the velocity, implying that there is no dissipation (i.e., viscous heating) associated with this effect. The gyroviscosity coefficients are given by

$$\eta_3^e = -\frac{n T_e}{2 \Omega_e}, \quad (39)$$

$$\eta_3^i = \frac{n T_i}{2 \Omega_i}. \quad (40)$$

1.3 Normalization of Braginskii Equations

As we have just seen, the Braginskii equations contain terms that describe a very wide range of different physical phenomena. For this reason, they are extremely complicated. Fortunately, however, it is not generally necessary to retain all of the terms in these equations when investigating tearing mode dynamics in tokamak plasmas. In this section, we shall attempt to construct a systematic normalization scheme for the Braginskii equations that will, hopefully, enable us to determine which terms to keep, and which to discard, when investigating tearing mode dynamics.

It is convenient to split the friction force \mathbf{F} into a component \mathbf{F}_U corresponding to resistivity, and a component \mathbf{F}_T corresponding to the thermal force. Thus,

$$\mathbf{F} = \mathbf{F}_U + \mathbf{F}_T, \quad (41)$$

where

$$\mathbf{F}_U = n e \left(\frac{\mathbf{j}_{\parallel}}{\sigma_{\parallel}} + \frac{\mathbf{j}_{\perp}}{\sigma_{\perp}} \right), \quad (42)$$

$$\mathbf{F}_T = -0.71 n \nabla_{\parallel} T_e - \frac{3 n}{2 \Omega_e \tau_e} \mathbf{b} \times \nabla_{\perp} T_e. \quad (43)$$

Likewise, the electron collisional energy gain term w_e is split into a component $-w_i$ corresponding to the energy lost to the ions (in the ion rest frame), a component w_U corresponding to work done by the friction force \mathbf{F}_U , and a component w_T corresponding to work done by the thermal force \mathbf{F}_T . Thus,

$$w_e = -w_i + w_U + w_T, \quad (44)$$

where

$$w_U = \frac{\mathbf{j} \cdot \mathbf{F}_U}{n e}, \quad (45)$$

$$w_T = \frac{\mathbf{j} \cdot \mathbf{F}_T}{n e}. \quad (46)$$

Finally, it is helpful to split the electron heat flux density \mathbf{q}_e into a diffusive component \mathbf{q}_{Te} and a convective component \mathbf{q}_{Ue} . Thus,

$$\mathbf{q}_e = \mathbf{q}_{Te} + \mathbf{q}_{Ue}, \quad (47)$$

where

$$\mathbf{q}_{Te} = -\kappa_{\parallel}^e \nabla_{\parallel} T_e - \kappa_{\perp}^e \nabla_{\perp} T_e - \kappa_{\times}^e \mathbf{b} \times \nabla_{\perp} T_e, \quad (48)$$

$$\mathbf{q}_{Ue} = 0.71 \frac{T_e}{e} \mathbf{j}_{\parallel} - \frac{3 T_e}{2 \Omega_e \tau_e e} \mathbf{b} \times \mathbf{j}_{\perp}. \quad (49)$$

Let us, first of all, consider the electron fluid equations, which can be written:

$$\frac{dn}{dt} + n \nabla \cdot \mathbf{V}_e = 0, \quad (50)$$

$$m_e n \frac{d\mathbf{V}_e}{dt} + \nabla p_e + \nabla \cdot \boldsymbol{\pi}_e + e n (\mathbf{E} + \mathbf{V}_e \times \mathbf{B}) = \mathbf{F}_U + \mathbf{F}_T, \quad (51)$$

$$\frac{3}{2} \frac{dp_e}{dt} + \frac{5}{2} p_e \nabla \cdot \mathbf{V}_e + \boldsymbol{\pi}_e : \nabla \mathbf{V}_e + \nabla \cdot \mathbf{q}_{Te} + \nabla \cdot \mathbf{q}_{Ue} = -w_i + w_U + w_T. \quad (52)$$

Let \bar{n} , \bar{v}_e , $\bar{\tau}_e$, $\bar{l}_e = \bar{v}_e \bar{\tau}_e$, \bar{B} , and $\bar{\rho}_e = \bar{v}_e / (e \bar{B} / m_e)$, be typical values of the particle density, the electron thermal velocity, the electron collision time, the electron mean-free-path between

collisions, the magnetic field-strength, and the electron gyroradius, respectively. Suppose that the typical spatial variation lengthscale of fluid variables is L . Let

$$\delta_e = \frac{\bar{\rho}_e}{L}, \quad (53)$$

$$\zeta_e = \frac{\bar{\rho}_e}{\bar{l}_e}, \quad (54)$$

$$\mu = \sqrt{\frac{m_e}{m_i}}. \quad (55)$$

All three of these parameters are assumed to be small compared to unity. Finally, the typical electron flow velocity is assumed to be of order $\delta_e \bar{v}_e$. This corresponds to the so-called *drift ordering* in which the flow velocity is comparable to the curvature and grad-B particle drift velocities (Fitzpatrick 2015). The drift ordering is appropriate to tearing modes in tokamak plasmas, which are comparatively slowly growing instabilities.

We define the following normalized quantities:

$$\begin{aligned} \hat{n} &= \frac{n}{\bar{n}}, & \hat{v}_e &= \frac{v_e}{\bar{v}_e}, & \hat{\mathbf{r}} &= \frac{\mathbf{r}}{L}, \\ \hat{\nabla} &= L \nabla, & \hat{t} &= \frac{\delta_e \bar{v}_e t}{L}, & \hat{\mathbf{V}}_e &= \frac{\mathbf{V}_e}{\delta_e \bar{v}_e}, \\ \hat{\mathbf{B}} &= \frac{\mathbf{B}}{\bar{B}}, & \hat{\mathbf{E}} &= \frac{\mathbf{E}}{\delta_e \bar{v}_e \bar{B}}, & \hat{\mathbf{j}} &= \frac{\mathbf{j}}{n e \delta_e \bar{v}_e}, \\ \hat{p}_e &= \frac{p_e}{m_e \bar{n} \bar{v}_e^2}, & \hat{\pi}_e &= \frac{\pi_e}{\delta_e^2 \zeta_e^{-1} m_e \bar{n} \bar{v}_e^2}, & \hat{\mathbf{q}}_{Te} &= \frac{\mathbf{q}_{Te}}{\delta_e \zeta_e^{-1} m_e \bar{n} \bar{v}_e^3}, \\ \hat{\mathbf{q}}_{Ue} &= \frac{\mathbf{q}_{Ue}}{\delta_e m_e \bar{n} \bar{v}_e^3}, & \hat{\mathbf{F}}_U &= \frac{\mathbf{F}_U}{\zeta_e m_e \bar{n} \bar{v}_e^2 / L}, & \hat{\mathbf{F}}_T &= \frac{\mathbf{F}_T}{m_e \bar{n} \bar{v}_e^2 / L}, \\ \hat{w}_i &= \frac{w_i}{\delta_e^{-1} \zeta_e \mu^2 m_e \bar{n} \bar{v}_e^3 / L}, & \hat{w}_U &= \frac{w_U}{\delta_e \zeta_e m_e \bar{n} \bar{v}_e^3 / L}, & \hat{w}_T &= \frac{w_T}{\delta_e m_e \bar{n} \bar{v}_e^3 / L}. \end{aligned}$$

The normalization procedure is designed to make all hatted quantities $\mathcal{O}(1)$. The normalization of the electric field is chosen such that the $\mathbf{E} \times \mathbf{B}$ velocity is of similar magnitude to the electron fluid velocity. Note that the parallel viscosity makes an $\mathcal{O}(1)$ contribution to $\hat{\pi}_e$, whereas the gyroviscosity makes an $\mathcal{O}(\zeta_e)$ contribution, and the perpendicular viscosity only makes an $\mathcal{O}(\zeta_e^2)$ contribution. Likewise, the parallel thermal conductivity makes an $\mathcal{O}(1)$ contribution to $\hat{\mathbf{q}}_{Te}$, whereas the cross conductivity makes an $\mathcal{O}(\zeta_e)$ contribution, and the perpendicular conductivity only makes an $\mathcal{O}(\zeta_e^2)$ contribution. Similarly, the parallel components of \mathbf{F}_T and \mathbf{q}_{Ue} are $\mathcal{O}(1)$, whereas the perpendicular components are $\mathcal{O}(\zeta_e)$.

The normalized electron fluid equations take the form:

$$\frac{d\hat{n}}{d\hat{t}} + \hat{n} \hat{\nabla} \cdot \hat{\mathbf{V}}_e = 0, \quad (56)$$

$$\hat{n} \frac{d\hat{\mathbf{V}}_e}{d\hat{t}} + \delta_e^{-2} \hat{\nabla} \hat{p}_e + \zeta_e^{-1} \hat{\nabla} \cdot \hat{\pi}_e + \delta_e^{-2} \hat{n} (\hat{\mathbf{E}} + \hat{\mathbf{V}}_e \times \hat{\mathbf{B}}) = \delta_e^{-2} \zeta_e \hat{\mathbf{F}}_U + \delta_e^{-2} \hat{\mathbf{F}}_T, \quad (57)$$

$$\begin{aligned} \frac{3}{2} \frac{d\hat{p}_e}{d\hat{t}} + \frac{5}{2} \hat{p}_e \hat{\nabla} \cdot \hat{\mathbf{V}}_e + \delta_e^2 \zeta_e^{-1} \hat{\boldsymbol{\pi}}_e : \hat{\nabla} \cdot \hat{\mathbf{V}}_e \\ + \zeta_e^{-1} \hat{\nabla} \cdot \hat{\mathbf{q}}_{Te} + \hat{\nabla} \cdot \hat{\mathbf{q}}_{Ue} = -\delta_e^{-2} \zeta_e \mu^2 \hat{w}_i + \zeta_e \hat{w}_U + \hat{w}_T. \end{aligned} \quad (58)$$

The only large or small (compared to unity) quantities in these equations are the parameters δ_e , ζ_e , and μ . Here, $d/d\hat{t} \equiv \partial/\partial\hat{t} + \hat{\mathbf{V}}_e \cdot \hat{\nabla}$. It is assumed that $T_e \sim T_i$.

Let us now consider the ion fluid equations, which can be written:

$$\frac{dn}{dt} + n \nabla \cdot \mathbf{V}_i = 0, \quad (59)$$

$$m_i n \frac{d\mathbf{V}_i}{dt} + \nabla p_i + \nabla \cdot \boldsymbol{\pi}_i - e n (\mathbf{E} + \mathbf{V}_i \times \mathbf{B}) = -\mathbf{F}_U - \mathbf{F}_T, \quad (60)$$

$$\frac{3}{2} \frac{dp_i}{dt} + \frac{5}{2} p_i \nabla \cdot \mathbf{V}_i + \boldsymbol{\pi}_i : \nabla \mathbf{V}_i + \nabla \cdot \mathbf{q}_i = w_i. \quad (61)$$

It is convenient to adopt a normalization scheme for the ion equations which is similar to, but independent of, that employed to normalize the electron equations. Let \bar{n} , \bar{v}_i , \bar{l}_i , \bar{B} , and $\bar{\rho}_i = \bar{v}_i/(e\bar{B}/m_i)$, be typical values of the particle density, the ion thermal velocity, the ion mean-free-path between collisions, the magnetic field-strength, and the ion gyroradius, respectively. Suppose that the typical spatial variation lengthscale of fluid quantities is L . Let

$$\delta_i = \frac{\bar{\rho}_i}{L}, \quad (62)$$

$$\zeta_i = \frac{\bar{\rho}_i}{\bar{l}_i}, \quad (63)$$

$$\mu = \sqrt{\frac{m_e}{m_i}}. \quad (64)$$

All three of these parameters are assumed to be small compared to unity. As before, we adopt the drift ordering in which the typical ion flow velocity is assumed to be of order $\delta_i \bar{v}_i$.

We define the following normalized quantities:

$$\begin{aligned} \hat{n} &= \frac{n}{\bar{n}}, & \hat{v}_i &= \frac{v_i}{\bar{v}_i}, & \hat{\mathbf{r}} &= \frac{\mathbf{r}}{L}, \\ \hat{\nabla} &= L \nabla, & \hat{t} &= \frac{\delta_i \bar{v}_i t}{L}, & \hat{\mathbf{V}}_i &= \frac{\mathbf{V}_i}{\delta_i \bar{v}_i}, \\ \hat{\mathbf{B}} &= \frac{\mathbf{B}}{\bar{B}}, & \hat{\mathbf{E}} &= \frac{\mathbf{E}}{\delta_i \bar{v}_i \bar{B}}, & \hat{\mathbf{j}} &= \frac{\mathbf{j}}{n e \delta_i \bar{v}_i}, \\ \hat{p}_i &= \frac{p_i}{m_i \bar{n} \bar{v}_i^2}, & \hat{\boldsymbol{\pi}}_i &= \frac{\boldsymbol{\pi}_i}{\delta_i^2 \zeta_i^{-1} m_i \bar{n} \bar{v}_i^2}, & \hat{\mathbf{q}}_i &= \frac{\mathbf{q}_i}{\delta_i \zeta_i^{-1} m_i \bar{n} \bar{v}_i^3}, \\ \hat{\mathbf{F}}_U &= \frac{\mathbf{F}_U}{\zeta_i \mu m_i \bar{n} \bar{v}_i^2 / L}, & \hat{\mathbf{F}}_T &= \frac{\mathbf{F}_T}{m_i \bar{n} \bar{v}_i^2 / L}, & \hat{w}_i &= \frac{w_i}{\delta_i^{-1} \zeta_i \mu m_i \bar{n} \bar{v}_i^3 / L}. \end{aligned}$$

As before, the normalization procedure is designed to make all hatted quantities $\mathcal{O}(1)$. The normalization of the electric field is chosen such that the $\mathbf{E} \times \mathbf{B}$ velocity is of similar magnitude to the ion fluid velocity. Note that the parallel viscosity makes an $\mathcal{O}(1)$ contribution to $\hat{\boldsymbol{\pi}}_i$, whereas the gyroviscosity makes an $\mathcal{O}(\zeta_i)$ contribution, and the perpendicular viscosity only makes an $\mathcal{O}(\zeta_i^2)$ contribution. Likewise, the parallel thermal conductivity makes an $\mathcal{O}(1)$ contribution to $\hat{\mathbf{q}}_i$, whereas the cross conductivity makes an $\mathcal{O}(\zeta_i)$ contribution, and the perpendicular conductivity only makes an $\mathcal{O}(\zeta_i^2)$ contribution. Similarly, the parallel component of \mathbf{F}_T is $\mathcal{O}(1)$, whereas the perpendicular component is $\mathcal{O}(\zeta_i \mu)$.

The normalized ion fluid equations take the form:

$$\frac{d\hat{n}}{d\hat{t}} + \hat{n} \hat{\nabla} \cdot \hat{\mathbf{V}}_i = 0, \quad (65)$$

$$\hat{n} \frac{d\hat{\mathbf{V}}_i}{d\hat{t}} + \delta_i^{-2} \hat{\nabla} \hat{p}_i + \zeta_i^{-1} \hat{\nabla} \cdot \hat{\boldsymbol{\pi}}_i - \delta_i^{-2} \hat{n} (\hat{\mathbf{E}} + \hat{\mathbf{V}}_i \times \hat{\mathbf{B}}) = -\delta_i^{-2} \zeta_i \mu \hat{\mathbf{F}}_U - \delta_i^{-2} \hat{\mathbf{F}}_T, \quad (66)$$

$$\frac{3}{2} \frac{d\hat{p}_i}{d\hat{t}} + \frac{5}{2} \hat{p}_i \hat{\nabla} \cdot \hat{\mathbf{V}}_i + \delta_i^2 \zeta_i^{-1} \hat{\boldsymbol{\pi}}_i : \hat{\nabla} \cdot \hat{\mathbf{V}}_i + \zeta_i^{-1} \hat{\nabla} \cdot \hat{\mathbf{q}}_i = \delta_i^{-2} \zeta_i \mu \hat{w}_i. \quad (67)$$

The only large or small (compared to unity) quantities in these equations are the parameters δ_i , ζ_i , and μ . Here, $d/d\hat{t} \equiv \partial/\partial\hat{t} + \hat{\mathbf{V}}_i \cdot \hat{\nabla}$.

1.4 Lowest-Order Fluid Equations

If we restore dimensions to the Braginskii equations then we can write them in the form

$$\frac{\partial n}{\partial t} + \nabla \cdot (n \mathbf{V}_e) = 0, \quad (68)$$

$$m_e n \frac{\partial \mathbf{V}_e}{\partial t} + m_e n (\mathbf{V}_e \cdot \nabla) \mathbf{V}_e + [\delta_e^{-2}] \nabla p_e + [\zeta_e^{-1}] \nabla \cdot \boldsymbol{\pi}_e + [\delta_e^{-2}] e n (\mathbf{E} + \mathbf{V}_e \times \mathbf{B}) = [\delta_e^{-2} \zeta_e] \mathbf{F}_U + [\delta_e^{-2}] \mathbf{F}_T, \quad (69)$$

$$\frac{3}{2} \frac{\partial p_e}{\partial t} + \frac{3}{2} (\mathbf{V}_e \cdot \nabla) p_e + \frac{5}{2} p_e \nabla \cdot \mathbf{V}_e + [\delta_e^2 \zeta_e^{-1}] \boldsymbol{\pi}_e : \nabla \mathbf{V}_e + [\zeta_e^{-1}] \nabla \cdot \mathbf{q}_{Te} + \nabla \cdot \mathbf{q}_{Ue} = -[\delta_e^{-2} \zeta_e \mu^2] w_i + [\zeta_e] w_U + w_T, \quad (70)$$

and

$$\frac{\partial n}{\partial t} + \nabla \cdot (n \mathbf{V}_i) = 0, \quad (71)$$

$$m_i n \frac{\partial \mathbf{V}_i}{\partial t} + m_i n (\mathbf{V}_i \cdot \nabla) \mathbf{V}_i + [\delta_i^{-2}] \nabla p_i + [\zeta_i^{-1}] \nabla \cdot \boldsymbol{\pi}_i - [\delta_i^{-2}] e n (\mathbf{E} + \mathbf{V}_i \times \mathbf{B}) = -[\delta_i^{-2} \zeta_i \mu] \mathbf{F}_U - [\delta_i^{-2}] \mathbf{F}_T, \quad (72)$$

$$\frac{3}{2} \frac{\partial p_i}{\partial t} + \frac{3}{2} (\mathbf{V}_i \cdot \nabla) p_i + \frac{5}{2} p_i \nabla \cdot \mathbf{V}_i + [\delta_i^2 \zeta_i^{-1}] \boldsymbol{\pi}_i : \nabla \mathbf{V}_i$$

$$+[\zeta_i^{-1}] \nabla \cdot \mathbf{q}_i = [\delta_i^{-2} \zeta_i \mu] w_i. \quad (73)$$

The terms in square brackets are just to remind us that the terms they precede are smaller or larger than the other terms in the equations (by the corresponding terms within the brackets).

If we assume that $\delta_e \sim \zeta_e \sim \mu$ then the dominant terms in the electron energy conservation equation (70) yield

$$\nabla \cdot \mathbf{q}_{T_e} \simeq \nabla \cdot (-\kappa_{\parallel}^e \nabla_{\parallel} T_e) \simeq 0, \quad (74)$$

which implies that

$$\mathbf{B} \cdot \nabla T_e = 0. \quad (75)$$

In other words, the parallel electron heat conductivity in a tokamak plasma is usually sufficiently large that it forces the electron temperature to be constant on magnetic flux-surfaces. Likewise, if we assume that $\delta_i \sim \zeta_i \sim \mu$ then the dominant terms in the ion energy conservation equation (73) yield

$$\nabla \cdot \mathbf{q}_{T_i} \simeq \nabla \cdot (-\kappa_{\parallel}^i \nabla_{\parallel} T_i) \simeq 0, \quad (76)$$

which implies that

$$\mathbf{B} \cdot \nabla T_i = 0. \quad (77)$$

In other words, the parallel ion heat conductivity in a tokamak plasma is usually sufficiently large that it forces the ion temperature to be constant on magnetic flux-surfaces.

The dominant terms in the electron and ion momentum conservation equations, (69) and (72), respectively, yield

$$\nabla p_e + n e (\mathbf{E} + \mathbf{V}_e \times \mathbf{B}) \simeq 0, \quad (78)$$

$$\nabla p_i - n e (\mathbf{E} + \mathbf{V}_i \times \mathbf{B}) \simeq 0. \quad (79)$$

The sum of the preceding two equations gives

$$\mathbf{j} \times \mathbf{B} \simeq -\nabla p, \quad (80)$$

where $p = p_e + p_i$. In other words, a conventional tokamak plasma exists in a state in which electromagnetic forces exactly balance the total scalar pressure force. It follows from the previous equation that

$$\mathbf{B} \cdot \nabla p \simeq 0. \quad (81)$$

In other words, the pressure in a conventional tokamak plasma is constant on magnetic flux-surfaces. However, given that $p = n (T_e + T_i)$, and making use of Eqs. (75) and (77), we deduce that

$$\mathbf{B} \cdot \nabla n \simeq 0. \quad (82)$$

In other words, the particle density in a conventional tokamak plasma is also constant on magnetic flux-surfaces.

Taking the difference of the electron and ion particle conservation equations, (68) and (71), respectively, we obtain

$$\nabla \cdot \mathbf{j} = 0. \quad (83)$$

Equations (80) and (83) can be combined to give

$$(\mathbf{B} \cdot \nabla) \mathbf{j} - (\mathbf{j} \cdot \nabla) \mathbf{B} \simeq \mathbf{0}. \quad (84)$$

Finally, Equations (78) and (79) imply that

$$\mathbf{V}_{\perp e} \simeq \mathbf{V}_E + \mathbf{V}_{*e}, \quad (85)$$

$$\mathbf{V}_{\perp i} \simeq \mathbf{V}_E + \mathbf{V}_{*i}, \quad (86)$$

where

$$\mathbf{V}_e = \frac{\mathbf{E} \times \mathbf{B}}{B^2} \quad (87)$$

is the *E-cross-B drift velocity*, and

$$\mathbf{V}_{*e} = \frac{\nabla p_e \times \mathbf{B}}{e n B^2}, \quad (88)$$

$$\mathbf{V}_{*i} = -\frac{\nabla p_i \times \mathbf{B}}{e n B^2}, \quad (89)$$

are termed the *electron diamagnetic velocity* and the *ion diamagnetic velocity*, respectively.

2 Cylindrical Tearing Mode Theory

2.1 Tokamak Equilibrium

Consider a large aspect-ratio tokamak plasma equilibrium with whose magnetic flux-surfaces map out (almost) concentric circles in the poloidal plane. Let us employ a conventional set of right-handed cylindrical coordinates, r, θ, z . The equilibrium magnetic flux-surfaces lie on surfaces of constant r . The system is assumed to be periodic in the z ('toroidal') direction, with periodicity length $2\pi R_0$, where R_0 is the simulated *major radius* of the plasma. The *safety-factor* profile takes the form

$$q(r) = \frac{r B_z}{R_0 B_\theta(r)}, \quad (90)$$

where B_z is the constant 'toroidal' magnetic field-strength, and $B_\theta(r)$ is the poloidal magnetic field-strength. It is assumed that $q \sim \mathcal{O}(1)$. The equilibrium 'toroidal' current density satisfies

$$\mu_0 j_z(r) = \frac{(r B_\theta)'}{r}, \quad (91)$$

where $'$ denotes d/dr . Finally, the standard large aspect-ratio tokamak orderings,

$$\frac{r}{R_0} \ll 1, \quad \frac{B_\theta}{B_z} \ll 1, \quad (92)$$

are adopted (Fitzpatrick 1993).

2.2 Perturbed Magnetic Field

Consider a tearing mode perturbation that has m periods in the poloidal direction, and n periods in the ‘toroidal’ direction, where $m/n \sim \mathcal{O}(1)$. We can write the perturbed magnetic field in the form

$$\delta \mathbf{B} \simeq \nabla \times (\psi \mathbf{e}_z), \quad (93)$$

where

$$\psi(r, \theta, \phi, t) = \psi(r, t) \exp[i(m\theta - n\phi)]. \quad (94)$$

Here, $\phi = z/R_0$ is a simulated toroidal angle. The perturbed current density becomes

$$\mu_0 \delta \mathbf{j} \simeq -\nabla^2 \psi \mathbf{e}_z. \quad (95)$$

2.3 Cylindrical Tearing Mode Equation

The tearing perturbation is governed by the linearized version of Equation (84), which yields

$$(\delta \mathbf{B} \cdot \nabla) \mathbf{j} + (\mathbf{B} \cdot \nabla) \delta \mathbf{j} - (\delta \mathbf{j} \cdot \nabla) \mathbf{B} - (\mathbf{j} \cdot \nabla) \delta \mathbf{B} \simeq \mathbf{0}. \quad (96)$$

Making use of Equations (90)–(95), the z -component of the previous equation gives the *cylindrical tearing mode equation* (Fitzpatrick 1993),

$$\frac{\partial^2 \psi}{dr^2} + \frac{1}{r} \frac{\partial \psi}{\partial r} - \frac{m^2}{r^2} \psi - \frac{J'_z \psi}{r(1/q - n/m)} \simeq 0, \quad (97)$$

where

$$J_z(r) = \frac{R_0 \mu_0 j_z(r)}{B_z}. \quad (98)$$

2.4 Solution in Presence of Perfectly-Conducting Wall

Suppose that the plasma occupies the region $0 \leq r \leq a$, where a is the plasma *minor radius*. It follows that $J_z(r) = 0$ for $r > a$. Suppose that the plasma is surrounded by a concentric perfectly-conducting wall of radius $r_w > a$. An appropriate physical solution of the cylindrical tearing mode equation takes the form

$$\psi(r, t) = \Psi_s(t) \hat{\psi}_s(r), \quad (99)$$

where the real function $\hat{\psi}_s(r)$ is a solution of

$$\frac{d^2 \hat{\psi}_s}{dr^2} + \frac{1}{r} \frac{d \hat{\psi}_s}{dr} - \frac{m^2}{r^2} \hat{\psi}_s - \frac{J'_z \hat{\psi}_s}{r(1/q - n/m)} \simeq 0 \quad (100)$$

that satisfies

$$\hat{\psi}_s(0) = 0, \quad (101)$$

$$\hat{\psi}_s(r_s) = 1, \quad (102)$$

$$\hat{\psi}_s(r \geq r_w) = 0. \quad (103)$$

Note that Equation (100) is singular at the so-called *resonant* magnetic flux-surface, radius $r = r_s$, at which

$$q(r_s) = \frac{m}{n}. \quad (104)$$

At the resonant surface, $\mathbf{k} \cdot \mathbf{B} = 0$, where $\mathbf{k} = (0, m/r, -n/R_0)$ is the wavevector of the tearing perturbation. The value of $\psi(r, t)$ at the resonant surface—namely, $\Psi_s(t)$ —is known as the *reconnected magnetic flux*. Note that Ψ_s is, in general, a complex quantity. Let $\rho = (r - r_s)/r_s$. The solution of Equation (100) in the vicinity of the resonant surface is

$$\hat{\psi}_s(\rho) = 1 + \Delta_{s+} \rho + \alpha_s \rho \ln |\rho| + \mathcal{O}(\rho^2) \quad (105)$$

for $\rho > 0$, and

$$\hat{\psi}_s(\rho) = 1 + \Delta_{s-} \rho + \alpha_s \rho \ln |\rho| + \mathcal{O}(\rho^2) \quad (106)$$

for $\rho < 0$. Here,

$$\alpha_s = - \left(\frac{r q J'_z}{s} \right)_{r=r_s}, \quad (107)$$

$$s(r) = \frac{r q'}{q}. \quad (108)$$

Moreover, the real parameters Δ_{s+} and Δ_{s-} are fully determined by Equation (100) and the boundary conditions (101)–(103). Note that, in general, ψ is continuous across the resonant surface, whereas $\partial\psi/\partial r$ is discontinuous. The discontinuity in $\partial\psi/\partial r$ implies the presence of a radially thin current sheet at the resonant surface. This current sheet can only be resolved by retaining more terms in the perturbed plasma equation of motion, (96).

The complex quantity

$$\Delta\Psi_s = \left[r \frac{\partial\psi}{\partial r} \right]_{r_{s-}}^{r_{s+}} \quad (109)$$

parameterizes the amplitude and phase of the current sheet flowing at the resonant surface. Matching the solutions in the so-called *inner region* (i.e., the region of the plasma in the immediate vicinity of the resonant surface) and the so-called *outer region* (i.e., everywhere in the plasma other than the inner region) with the help of Equations (99), (105), and (106), we obtain

$$\Delta\Psi_s = E_{ss} \Psi_s, \quad (110)$$

where $E_{ss} = \Delta_{s+} - \Delta_{s-}$ is a real quantity determined by the solution in the outer region.

2.5 Solution in Presence of Resistive Wall

Suppose, now, that the wall at $r = r_w$ possesses a finite resistivity, but is surrounded by a second perfectly-conducting wall located at radius $r_c > r_w$. The solution in the outer region can be written

$$\psi(r, t) = \Psi_s(t) \hat{\psi}_s(r) + \Psi_w(t) \hat{\psi}_w(r), \quad (111)$$

where the real function $\hat{\psi}_s(r)$ is specified in the previous section, and the real function $\hat{\psi}_w(r)$ is a solution of

$$\frac{d^2 \hat{\psi}_w}{dr^2} + \frac{1}{r} \frac{d\hat{\psi}_w}{dr} - \frac{m^2}{r^2} \hat{\psi}_w - \frac{J'_z \hat{\psi}_w}{r(1/q - n/m)} \simeq 0 \quad (112)$$

that satisfies

$$\hat{\psi}_w(r \leq r_s) = 0, \quad (113)$$

$$\hat{\psi}_w(r_w) = 1, \quad (114)$$

$$\hat{\psi}_w(r \geq r_c) = 0. \quad (115)$$

It is easily seen that

$$\hat{\psi}_w(r_w < r < r_c) = \frac{(r/r_c)^{-m} - (r/r_c)^m}{(r_w/r_c)^{-m} - (r_w/r_c)^m}. \quad (116)$$

In general, ψ is continuous across the wall, whereas $\partial\psi/\partial r$ is discontinuous. The discontinuity in $\partial\psi/\partial r$ is caused by the currents induced in the wall. The complex quantity $\Psi_w(t)$ determines the amplitude and phase of the perturbed magnetic flux that penetrates the wall. The complex quantity

$$\Delta\Psi_w = \left[r \frac{\partial\psi}{\partial r} \right]_{r_w-}^{r_w+} \quad (117)$$

parameterizes the amplitude and phase of the current sheet flowing in the wall. Simultaneously matching the outer solution (111) across the resonant surface and the wall yields

$$\Delta\Psi_s = E_{ss} \Psi_s + E_{sw} \Psi_w, \quad (118)$$

$$\Delta\Psi_w = E_{ws} \Psi_s + E_{ww} \Psi_w \quad (119)$$

(Fitzpatrick 1993). Here,

$$E_{ww} = \left[r \frac{d\hat{\psi}_w}{dr} \right]_{r_w-}^{r_w+}, \quad (120)$$

$$E_{sw} = \left[r \frac{d\hat{\psi}_w}{dr} \right]_{r=r_s+}, \quad (121)$$

$$E_{ws} = - \left[r \frac{d\hat{\psi}_s}{dr} \right]_{r=r_w-} \quad (122)$$

are real quantities determined by the solution in the outer region.

Equations (100) and (112) can be combined to give

$$\frac{d}{dr} \left(\hat{\psi}_s r \frac{d\hat{\psi}_w}{dr} - \hat{\psi}_w r \frac{d\hat{\psi}_s}{dr} \right) = 0. \quad (123)$$

If we integrate the previous equation from $r = r_{s+}$ to $r = r_{w-}$, making use of Equations (102), (103), (113), (114), (121), and (122), then we obtain

$$E_{sw} = E_{ws} \quad (124)$$

(Fitzpatrick 1993).

2.6 Resistive Wall Physics

It is clear from Equation (93) that

$$\delta \mathbf{A} \simeq \psi \mathbf{e}_z, \quad (125)$$

where $\delta \mathbf{A}$ is the perturbed magnetic vector potential. Hence, the perturbed electric field can be written

$$\delta \mathbf{E} \simeq -\nabla \delta \Phi - \frac{\partial \psi}{\partial t} \mathbf{e}_z, \quad (126)$$

where $\delta \Phi$ is the perturbed electric scalar potential. Assuming that $|\nabla \delta \Phi| \sim |\partial \psi / \partial t|$, the z -component of the previous equation yields

$$\delta E_z \simeq -\frac{\partial \psi}{\partial t}, \quad (127)$$

where use has been made of the large aspect-ratio orderings (92). Within the wall, we can write

$$\delta E_z \simeq -\frac{d\Psi_w}{dt}. \quad (128)$$

Here, we are making use of the so-called *thin wall approximation*, according to which ψ is assumed to only vary weakly in r across the wall. Ohm's law implies that

$$\delta j_z = \frac{\delta E_z}{\eta_w} = -\frac{1}{\eta_w} \frac{d\Psi_w}{dt} \quad (129)$$

within the wall, where η_w is the wall resistivity. Equations (95) and (117) yield

$$\Delta \Psi_w = -\mu_0 \int_{r_{w-}}^{r_{w+}} r \delta j_z dr. \quad (130)$$

Suppose that the radial thickness of the wall is $\delta_w \ll r_w$. The previous two equations yield

$$\Delta \Psi_w = \tau_w \frac{d\Psi_w}{dt}, \quad (131)$$

where

$$\tau_w = \frac{\mu_0 r_w \delta_w}{\eta_w} \quad (132)$$

is the so-called *time constant* of the wall (Fitzpatrick 1993). The thin wall approximation is valid as long as

$$\frac{r_w}{\delta_w} \gg \tau_w \left| \frac{d \ln \Psi_w}{dt} \right|. \quad (133)$$

2.7 Resonant Layer Physics

By analogy with Equation (131), we can write

$$\Delta \Psi_s = \tau_s \left(\frac{d \Psi_w}{dt} + i \varpi_s \Psi_s \right). \quad (134)$$

Here, τ_s is the *reconnection time*, whereas ϖ_s is the so-called *natural frequency*. The natural frequency is the phase velocity of the tearing mode when the wall is perfectly conducting. The natural frequency is non-zero because the reconnected flux in the resonant layer is convected by the local plasma flow (Fitzpatrick 1993).

2.8 Solution in Presence of External Magnetic Field-Coil

Suppose that the perfectly-conducting wall at $r = r_c$ is replaced by a magnetic field-coil that carries a helical current possessing m periods in the poloidal direction, and n periods in the ‘toroidal’ direction. Let the current density in the coil take the form

$$\delta j_z = -\frac{I_c(t)}{r_c} \delta(r - r_c) e^{i(m\theta - n\phi)}. \quad (135)$$

Here, the complex quantity $I_c(t)$ parameterizes the amplitude and phase of the helical current flowing in the field-coil.

The solution in the outer region can be written

$$\psi(r, t) = \Psi_s(t) \hat{\psi}_s(r) + \Psi_w(t) \hat{\psi}_w(r) + \Psi_c \hat{\psi}_c(r), \quad (136)$$

where the real functions $\hat{\psi}_s(r)$ and $\hat{\psi}_w(r)$ are specified in Sections 2.4 and 2.5, respectively. Moreover, the real function $\hat{\psi}_c(r)$ is a solution of

$$\frac{d^2 \hat{\psi}_c}{dr^2} + \frac{1}{r} \frac{d \hat{\psi}_c}{dr} - \frac{m^2}{r^2} \hat{\psi}_c \simeq 0 \quad (137)$$

that satisfies

$$\hat{\psi}_c(r \leq r_w) = 0, \quad (138)$$

$$\hat{\psi}_c(r_c) = 1, \quad (139)$$

$$\hat{\psi}_c(\infty) = 0. \quad (140)$$

It is easily seen that

$$\hat{\psi}_c(r \leq r_w) = 0, \quad (141)$$

$$\hat{\psi}_c(r_w < r \leq r_c) = \frac{(r/r_w)^m - (r/r_w)^{-m}}{(r_c/r_w)^m - (r_c/r_w)^{-m}}, \quad (142)$$

$$\hat{\psi}_c(r > r_c) = \left(\frac{r}{r_c}\right)^{-m}. \quad (143)$$

In general, ψ is continuous across the field-coil, whereas $\partial\psi/\partial r$ is discontinuous. The discontinuity in $\partial\psi/\partial r$ is caused by the currents flowing in the coil. The complex quantity $\Psi_c(t)$ determines the amplitude and phase of the perturbed magnetic flux at the coil. The complex quantity

$$\Delta\Psi_c = \left[r \frac{\partial\psi}{\partial r} \right]_{r_{c-}}^{r_{c+}} \quad (144)$$

parameterizes the amplitude and phase of the current sheet flowing in the coil. It follows from Equations (94), (95), and (135) that

$$\Delta\Psi_c = \mu_0 I_c. \quad (145)$$

Simultaneously matching the outer solution across the resonant surface, the wall, and the field-coil, we obtain

$$\Delta\Psi_s = E_{ss} \Psi_s + E_{sw} \Psi_w, \quad (146)$$

$$\Delta\Psi_w = E_{ws} \Psi_s + E_{ww} \Psi_w + E_{wc} \Psi_c, \quad (147)$$

$$\Delta\Psi_c = E_{cw} \Psi_w + E_{cc} \Psi_c. \quad (148)$$

Here,

$$E_{cc} = \left[r \frac{d\hat{\psi}_c}{dr} \right]_{r_{c-}}^{r_{c+}} = -\frac{2m}{1 - (r_w/r_c)^{2m}}, \quad (149)$$

$$E_{wc} = \left[r \frac{d\hat{\psi}_c}{dr} \right]_{r_{w+}} = \frac{2m (r_w/r_c)^m}{1 - (r_w/r_c)^{2m}}, \quad (150)$$

$$E_{cw} = - \left[r \frac{d\hat{\psi}_w}{dr} \right]_{r_{c-}} = \frac{2m (r_w/r_c)^m}{1 - (r_w/r_c)^{2m}}, \quad (151)$$

where use has been made of Equations (116), (142), and (143).

2.9 Electromagnetic Torques

The flux-surface integrated poloidal and ‘toroidal’ electromagnetic torque densities acting on the plasma can be written

$$T_\theta(r) = \oint \oint R_0 r^2 \mathbf{j} \times \mathbf{B} \cdot \mathbf{e}_\theta d\theta d\phi, \quad (152)$$

$$T_\phi(r) = \oint \oint R_0^2 r \mathbf{j} \times \mathbf{B} \cdot \mathbf{e}_z d\theta d\phi, \quad (153)$$

respectively. However, according to Equation (80),

$$\mathbf{j} \times \mathbf{B} \simeq -\nabla p. \quad (154)$$

Given that the scalar pressure is a single-valued function of θ and ϕ , it immediately follows that $T_\theta = T_\phi = 0$ throughout the plasma. The only exception to this rule occurs in the immediate vicinity of the resonant surface, where Equation (154) breaks down. It follows that we can write

$$T_\theta(r) = T_{\theta s} \delta(r - r_s), \quad (155)$$

$$T_\phi(r) = T_{\phi s} \delta(r - r_s), \quad (156)$$

where

$$T_{\theta s} = \frac{1}{4} \int_{r_{s-}}^{r_{s+}} \oint \oint R_0 r^2 (\delta j_z \delta B_r^* + \delta j_z^* \delta B_r) dr d\theta d\phi, \quad (157)$$

$$T_{\phi s} = -\frac{1}{4} \int_{r_{s-}}^{r_{s+}} \oint \oint R_0^2 r (\delta j_\theta \delta B_r^* + \delta j_\theta^* \delta B_r) dr d\theta d\phi \quad (158)$$

are the net poloidal and ‘toroidal’ torques, respectively, acting at the resonant surface. Note that the equilibrium torques are zero because $B_r = 0$. Furthermore, the linear (in perturbed quantities) torques average to zero over the flux-surface. Hence, the largest non-zero torques are quadratic in perturbed quantities. According to Equation (83),

$$\nabla \cdot \delta \mathbf{j} = i \left(\frac{m}{r} \delta j_\theta - \frac{n}{R_0} \delta j_z \right) = 0, \quad (159)$$

where $\delta \mathbf{j}$ is the density of the current sheet flowing at the resonant surface, and we have made use of the fact that $\delta j_r \simeq 0$. It follows from the previous three equations that

$$T_{\phi s} = -\frac{n}{m} T_{\theta s}. \quad (160)$$

Finally, Equations (93), (95), (157), and (160) imply that

$$T_{\theta s} = -\frac{2\pi^2 R_0 m}{\mu_0} \text{Im}(\Delta \Psi_s \Psi_s^*), \quad (161)$$

$$T_{\phi s} = \frac{2\pi^2 R_0 n}{\mu_0} \text{Im}(\Delta\Psi_s \Psi_s^*) \quad (162)$$

(Fitzpatrick 1993).

By analogy with the previous analysis, the net poloidal and ‘toroidal’ electromagnetic torques acting on the resistive wall are

$$T_{\theta w} = -\frac{2\pi^2 R_0 m}{\mu_0} \text{Im}(\Delta\Psi_w \Psi_w^*), \quad (163)$$

$$T_{\phi w} = \frac{2\pi^2 R_0 n}{\mu_0} \text{Im}(\Delta\Psi_w \Psi_w^*), \quad (164)$$

respectively. Finally, the net poloidal and ‘toroidal’ electromagnetic torques acting on the magnetic field-coil are

$$T_{\theta c} = -\frac{2\pi^2 R_0 m}{\mu_0} \text{Im}(\Delta\Psi_c \Psi_c^*), \quad (165)$$

$$T_{\phi c} = \frac{2\pi^2 R_0 n}{\mu_0} \text{Im}(\Delta\Psi_c \Psi_c^*), \quad (166)$$

respectively.

It follows from Equations (146)–(148) that

$$\text{Im}(\Delta\Psi_s \Psi_s^*) = E_{sw} \text{Im}(\Psi_w \Psi_s^*), \quad (167)$$

$$\text{Im}(\Delta\Psi_w \Psi_w^*) = E_{ws} \text{Im}(\Psi_s \Psi_w^*) + E_{wc} \text{Im}(\Psi_c \Psi_w^*), \quad (168)$$

$$\text{Im}(\Delta\Psi_c \Psi_c^*) = E_{cw} \text{Im}(\Psi_w \Psi_c^*). \quad (169)$$

Thus,

$$\begin{aligned} \text{Im}(\Delta\Psi_s \Psi_s^*) + \text{Im}(\Delta\Psi_w \Psi_w^*) + \text{Im}(\Delta\Psi_c \Psi_c^*) &= (E_{sw} - E_{ws}) \text{Im}(\Psi_w \Psi_s^*) \\ &\quad + (E_{wc} - E_{cw}) \text{Im}(\Psi_c \Psi_w^*). \end{aligned} \quad (170)$$

However, according to Equations (124), (150), and (151), $E_{sw} = E_{ws}$ and $E_{wc} = E_{cw}$. We deduce that

$$\text{Im}(\Delta\Psi_s \Psi_s^*) + \text{Im}(\Delta\Psi_w \Psi_w^*) + \text{Im}(\Delta\Psi_c \Psi_c^*) = 0. \quad (171)$$

Hence, Equations (161)–(166) yield

$$T_{\theta s} + T_{\theta w} + T_{\theta c} = 0, \quad (172)$$

$$T_{\phi s} + T_{\phi w} + T_{\phi c} = 0. \quad (173)$$

In other words, the plasma/wall/field-coil system exerts zero net poloidal electromagnetic torque and zero net toroidal electromagnetic torque on itself.

2.10 Plasma Angular Equations of Motion

We can write

$$\Omega_\theta(r, t) = \Omega_{\theta 0}(r) + \Delta\Omega_\theta(r, t), \quad (174)$$

$$\Omega_\phi(r, t) = \Omega_{\phi 0}(r) + \Delta\Omega_\phi(r, t), \quad (175)$$

where $\Omega_\theta(r, t)$ and $\Omega_\phi(r, t)$ are the poloidal and ‘toroidal’ plasma angular velocity profiles, respectively. [To be more exact, $\Omega_\theta(r, t)$ and $\Omega_\phi(r, t)$ are the ion fluid angular velocity profiles.] Moreover, $\Omega_{\theta 0}(r)$ and $\Omega_{\phi 0}(r)$ are the corresponding unperturbed profiles, and $\Delta\Omega_\theta(r, t)$ and $\Delta\Omega_\phi(r, t)$ are the respective modifications to the profiles induced by the electromagnetic torques that develop at the resonant surface. The modifications to the angular velocity profiles are governed by the poloidal and toroidal angular equations of motion of the plasma, which take the respective forms

$$4\pi^2 R_0 \left[(1 + 2q^2) \rho r^3 \frac{\partial \Delta\Omega_\theta}{\partial t} - \frac{\partial}{\partial r} \left(\mu r^3 \frac{\partial \Delta\Omega_\theta}{\partial r} \right) + \frac{\rho}{\tau_\theta} r^3 \Delta\Omega_\theta \right] = T_{\theta s} \delta(r - r_s), \quad (176)$$

$$4\pi^2 R_0^3 \left[\rho r \frac{\partial \Delta\Omega_\phi}{\partial t} - \frac{\partial}{\partial r} \left(\mu r \frac{\partial \Delta\Omega_\phi}{\partial r} \right) \right] = T_{\phi s} \delta(r - r_s). \quad (177)$$

Here, $\rho(r)$ is the plasma mass density profile, $\mu(r)$ is the anomalous plasma perpendicular ion viscosity (due to plasma turbulence), and $\tau_\theta(r)$ is the characteristic time at which neoclassical parallel viscosity relaxes the plasma poloidal angular velocity profile.

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