

# Calculation of Tearing-Mode Stability in an Inverse Aspect-Ratio Expanded Tokamak Plasma Equilibrium

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The tearing-mode stability of an inverse aspect-ratio expanded tokamak plasma equilibrium of general shape is investigated using asymptotic matching techniques. Particular emphasis is placed on the conservation of toroidal electromagnetic angular momentum. The TJ code, which is a specific implementation of the results of the investigation, is described.

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## I. INTRODUCTION

The calculation of the tearing-mode stability of a high temperature, axisymmetric, tokamak plasma equilibrium is most efficiently formulated as an asymptotic matching problem.<sup>1</sup> In such a problem, the plasma is divided into two regions. In the “outer region”, which comprises most of the plasma, the tearing perturbation is described by the equations of linearized, marginally-stable, ideal magnetohydrodynamics (which, in the following, are referred to as the “ideal-MHD” equations). (See Sect. III B.) However, these equations become singular on so-called “rational” magnetic flux-surfaces at which the perturbed magnetic field resonates with the equilibrium field. In the so-called “inner region”, which consists of a set of narrow layers centered on the various rational surfaces, non-ideal-MHD effects such as plasma inertia, resistivity, and viscosity become important. The growth-rate and angular rotation frequency of the reconnected magnetic flux at a given rational surface (numbered  $k$ ) are fixed by asymptotically matching the resistive layer solution in the associated segment of the inner region, which is characterized by a dimensionless complex quantity  $\Delta_k$ , to the ideal-MHD solution in the outer region. In a realistic axisymmetric tokamak plasma equilibrium, tearing perturbations with different toroidal mode numbers are independent of one another, whereas perturbations with different poloidal mode numbers are coupled together via toroidicity and the non-circular shaping of magnetic flux-surfaces.<sup>2</sup> Consequently, for a tearing perturbation with a given toroidal mode number, the  $\Delta_k$  values associated with the various rational surfaces in the plasma are interrelated via a matrix equation.<sup>3</sup> [See Eq. (309).]

In general, the determination of the elements of the matrix equation that links the various  $\Delta_k$  values from the ideal-MHD equations in the outer region is an exceptionally challenging computational task.<sup>4-18</sup> One way of greatly reducing the complexity of this task is to employ an inverse aspect-ratio expanded plasma equilibrium.<sup>19</sup> In such an equilibrium, the metric elements of the flux-coordinate system can be expressed analytically in terms of a relatively small number of flux-surface functions, which represents a major simplification.<sup>2</sup> Another significant advantage of an inverse aspect-ratio expanded equilibrium is that the magnetic perturbation in the plasma can be efficiently matched to a vacuum solution expressed as

an expansion in toroidal functions.<sup>6</sup> The alternative approach of using a Green's function solution in the vacuum region is much more computationally intensive.<sup>20,21</sup>

The inverse aspect-ratio expansion approach to determining tearing-mode stability in tokamak plasmas was first presented in Ref. 4 in a calculation that features triplets of poloidal harmonics coupled via toroidicity. The inverse aspect-ratio expansion approach was extended in Ref. 6 in a calculation that features septuplets of poloidal harmonics coupled via toroidicity, flux-surface elongation, and flux-surface triangularity. In this paper, we generalize the inverse aspect-ratio expansion approach to allow for an *arbitrary* number of poloidal harmonics coupled by flux-surfaces of *general* shape. Furthermore, unlike Refs. 4 and 6, we do not assume that the plasma equilibrium is up-down-symmetric.

This paper is organized as follows. In Sect. II, we examine a general tokamak plasma equilibrium. In Sect. III, we derive the so-called “outer-region partial differential equations” (p.d.e.s), which are a set of two coupled second-order p.d.e.s that control the ideal-MHD solution in the outer region. In Sect. IV, we derive the so-called “outer region ordinary differential equations” (o.d.e.s), which are a large set of coupled first-order o.d.e.s that control the ideal-MHD solution in the outer region. We also demonstrate that these o.d.e.s conserve toroidal electromagnetic angular momentum. In Sect. V, we discuss the general behavior of the outer-region o.d.e.s in the vicinity of a rational surface. In Sect. VI, we obtain the general boundary condition satisfied by the outer-region o.d.e.s at the plasma/vacuum interface, on the assumption that region surrounding the plasma does not contain any non-axisymmetric currents. We also demonstrate that these boundary conditions conserve toroidal electromagnetic angular momentum. In Sect. VII, we introduce the aspect-ratio expanded tokamak equilibrium, and determine the specific forms of the outer-region o.d.e.s. In Sect. VIII, we calculate the matrix equation that constitutes the tearing-mode dispersion relation, and demonstrate that this equation must be Hermitian in order to conserve toroidal electromagnetic angular momentum. In Sect. IX, we discuss how the tearing-mode dispersion relation is modified by non-axisymmetric currents flowing in resonant magnetic perturbation (RMP) coils external to the plasma. We also derive expressions for the toroidal electromagnetic torques exerted at the various rational surfaces in the plasma by the RMP coils. In Sect. X, we discuss the TJ code, which is a specific implementation of the theory presented

in Sects. II–IX. Finally, the paper is summarized in Sect. XI.

## II. GENERAL PLASMA EQUILIBRIUM

### A. Normalization

All lengths in this paper are normalized to the major radius of the plasma magnetic axis,  $R_0$ . All magnetic field-strengths are normalized to the toroidal field-strength at the magnetic axis,  $B_0$ . All currents are normalized to  $B_0 R_0/\mu_0$ . All current densities are normalized to  $B_0/(\mu_0 R_0)$ . All plasma pressures are normalized to  $B_0^2/\mu_0$ . All toroidal electromagnetic torques are normalized to  $B_0^2 R_0^3/\mu_0$ .

### B. Axisymmetric Tokamak Plasma Equilibrium

Let  $R, \phi, Z$  be right-handed cylindrical coordinates whose Jacobian is

$$(\nabla R \times \nabla \phi \cdot \nabla Z)^{-1} = R. \quad (1)$$

Note that  $|\nabla \phi| = 1/R$ .

Let  $r, \theta, \phi$  be right-handed flux-coordinates whose Jacobian is <sup>4,22</sup>

$$\mathcal{J}(r, \theta) \equiv (\nabla r \times \nabla \theta \cdot \nabla \phi)^{-1} \equiv R \left( \frac{\partial R}{\partial \theta} \frac{\partial Z}{\partial r} - \frac{\partial R}{\partial r} \frac{\partial Z}{\partial \theta} \right) = r R^2. \quad (2)$$

Note that  $r = r(R, Z)$  and  $\theta = \theta(R, Z)$ . The magnetic axis corresponds to  $r = 0$ . The inboard mid-plane corresponds to  $\theta = 0$ .

Consider an axisymmetric tokamak equilibrium <sup>23</sup> whose magnetic field takes the form <sup>4,6</sup>

$$\mathbf{B}(r, \theta) = f(r) \nabla \phi \times \nabla r + g(r) \nabla \phi = f \nabla(\phi - q \theta) \times \nabla r, \quad (3)$$

where

$$q(r) = \frac{r g}{f} \quad (4)$$

is the safety-factor (i.e., the inverse of the rotational transform). Note that  $\mathbf{B} \cdot \nabla r = 0$ , which implies that  $r$  is a magnetic flux-surface label. We require  $g = 1$  on the magnetic axis in order to ensure that the normalized toroidal magnetic field-strength at the axis is unity.

It is easily demonstrated that

$$B^r = \mathbf{B} \cdot \nabla r = 0, \quad (5)$$

$$B^\theta = \mathbf{B} \cdot \nabla \theta = \frac{f}{r R^2}, \quad (6)$$

$$B^\phi = \mathbf{B} \cdot \nabla \phi = \frac{g}{R^2}, \quad (7)$$

$$B_r = \mathcal{J} \nabla \theta \times \nabla \phi \cdot \mathbf{B} = -r f \nabla r \cdot \nabla \theta, \quad (8)$$

$$B_\theta = \mathcal{J} \nabla \phi \times \nabla r \cdot \mathbf{B} = r f |\nabla r|^2, \quad (9)$$

$$B_\phi = \mathcal{J} \nabla r \times \nabla \theta \cdot \mathbf{B} = g, \quad (10)$$

where use has been made of the results and notation of Sect. A.

The Maxwell equation (neglecting the displacement current, because tearing modes are comparatively low-frequency phenomena)  $\mathbf{J} = \nabla \times \mathbf{B}$  yields

$$\mathcal{J} J^r = \frac{\partial B_\phi}{\partial \theta} = 0, \quad (11)$$

$$\mathcal{J} J^\theta = -\frac{\partial B_\phi}{\partial r} = -g', \quad (12)$$

$$\mathcal{J} J^\phi = \frac{\partial B_\theta}{\partial r} - \frac{\partial B_r}{\partial \theta} = \frac{\partial}{\partial r}(r f |\nabla r|^2) + \frac{\partial}{\partial \theta}(r f \nabla r \cdot \nabla \theta), \quad (13)$$

where  $\mathbf{J}$  is the equilibrium current density,  $' \equiv d/dr$ , and use has been made of Eqs. (8)–(10) and (A11)–(A13).

Equilibrium force balance requires that

$$\nabla P = \mathbf{J} \times \mathbf{B}, \quad (14)$$

where  $P(r)$  is the equilibrium plasma pressure. Here, for the sake of simplicity, we have neglected the small centrifugal modifications to force balance due to plasma rotation.<sup>24,25</sup> It follows that

$$P' = \mathcal{J}(J^\theta B^\phi - J^\phi B^\theta) = -g' \frac{g}{R^2} - \frac{f}{r R^2} \left[ \frac{\partial}{\partial r}(r f |\nabla r|^2) + \frac{\partial}{\partial \theta}(r f \nabla r \cdot \nabla \theta) \right], \quad (15)$$

where use has been made of Eqs. (5)–(7), (11)–(13), and (A4)–(A6). The other two components of Eq. (14) are identically zero.

Equation (15) yields the *Grad-Shafranov equation*,<sup>23</sup>

$$\frac{f}{r} \frac{\partial}{\partial r} (r f |\nabla r|^2) + \frac{f}{r} \frac{\partial}{\partial \theta} (r f \nabla r \cdot \nabla \theta) + g g' + R^2 P' = 0. \quad (16)$$

It follows from Eqs. (4), (13), and (16) that

$$\mathcal{J} J^\phi = -q g' - \frac{r R^2 P'}{f}. \quad (17)$$

It is clear from Eqs. (12) and (17) that  $g' = P' = 0$  in the current-free “vacuum” region surrounding the plasma. We shall also assume that  $g' = P' = 0$  at the plasma/vacuum interface, so as to ensure that the equilibrium plasma current density is zero at the interface.

### III. DERIVATION OF OUTER-REGION P.D.E.S

#### A. Introduction

The outer-region p.d.e.s were first presented in Ref. 4 without an explicit derivation. However, the derivation is sufficiently non-obvious that it is worth outlining in this section.

#### B. Governing Equations

In the outer region, the perturbed plasma equilibrium satisfies the ideal-MHD equations<sup>4,6,15,23</sup>

$$\mathbf{b} = \nabla \times (\boldsymbol{\xi} \times \mathbf{B}), \quad (18)$$

$$\nabla p = \mathbf{j} \times \mathbf{B} + \mathbf{J} \times \mathbf{b}, \quad (19)$$

$$\mathbf{j} = \nabla \times \mathbf{b}, \quad (20)$$

$$p = -\boldsymbol{\xi} \cdot \nabla P, \quad (21)$$

where  $\boldsymbol{\xi}(r, \theta, \phi)$  is the plasma displacement,  $\mathbf{b}(r, \theta, \phi)$  the perturbed magnetic field,  $\mathbf{j}(r, \theta, \phi)$  the perturbed current density, and  $p(r, \theta, \phi)$  the perturbed pressure. Let us assume that all perturbed quantities vary with the toroidal angle,  $\phi$ , as  $\exp(-i n \phi)$ , where the real positive integer  $n$  is the toroidal mode number of the tearing mode. For example,  $p(r, \theta, \phi) = p(r, \theta) \exp(-i n \phi)$ .

### C. Radial Plasma Displacement

Equations (A5) and (A6) yield

$$(\boldsymbol{\xi} \times \mathbf{B})_\theta = \mathcal{J} (\xi^\phi B^r - \xi^r B^\phi) = -\mathcal{J} B^\phi \xi^r, \quad (22)$$

$$(\boldsymbol{\xi} \times \mathbf{B})_\phi = \mathcal{J} (\xi^r B^\theta - \xi^\theta B^r) = \mathcal{J} B^\theta \xi^r, \quad (23)$$

where use has been made of the fact that  $B^r = J^r = 0$ . [See Eqs. (5) and (11).] Combining the previous two equations with Eqs. (18) and (A11), we obtain

$$\mathcal{J} b^r = \frac{\partial}{\partial \theta} (\mathcal{J} B^\theta \xi^r) - \text{i} n \mathcal{J} B^\phi \xi^r. \quad (24)$$

Thus, Eqs. (2), (4), (6), and (7) give

$$r R^2 b^r = \left( \frac{\partial}{\partial \theta} - \text{i} n q \right) y, \quad (25)$$

where

$$y(r, \theta) = f \xi^r. \quad (26)$$

### D. Perturbed Force Balance

According to Eq. (21),

$$p = -P' \nabla r \cdot \boldsymbol{\xi} = -P' \xi^r. \quad (27)$$

So, the perturbed force balance equation, (19), yields

$$-\frac{\partial (P' \xi^r)}{\partial r} = (\mathbf{j} \times \mathbf{B})_r + (\mathbf{J} \times \mathbf{b})_r, \quad (28)$$

$$-\frac{\partial (P' \xi^r)}{\partial \theta} = (\mathbf{j} \times \mathbf{B})_\theta + (\mathbf{J} \times \mathbf{b})_\theta, \quad (29)$$

$$\text{i} n P' \xi^r = (\mathbf{j} \times \mathbf{B})_\phi + (\mathbf{J} \times \mathbf{b})_\phi, \quad (30)$$

giving

$$-\frac{\partial (P' \xi^r)}{\partial r} = r R^2 (j^\theta B^\phi - j^\phi B^\theta) + r R^2 (J^\theta b^\phi - J^\phi b^\theta), \quad (31)$$

$$-\frac{\partial(P' \xi^r)}{\partial \theta} = r R^2 (j^\phi B^r - j^r B^\phi) + r R^2 (J^\phi b^r - J^r b^\phi), \quad (32)$$

$$\text{i} n P' \xi^r = r R^2 (j^r B^\theta - j^\theta B^r) + r R^2 (J^r b^\theta - J^\theta b^r), \quad (33)$$

where use has been made of Eqs. (2) and (A4)–(A6). Thus, according to Eqs. (5)–(7), (11), (12), and (17),

$$-\frac{\partial(P' \xi^r)}{\partial r} = f (q j^\theta - j^\phi) - g' b^\phi + \left( q g' + \frac{r R^2 P'}{f} \right) b^\theta, \quad (34)$$

$$-\frac{\partial(P' \xi^r)}{\partial \theta} = -r g j^r - \left( q g' + \frac{r R^2 P'}{f} \right) b^r, \quad (35)$$

$$\text{i} n P' \xi^r = f j^r + g' b^r. \quad (36)$$

It follows from Eqs. (26), (25), and (36) that

$$r j^r = \text{i} n \alpha_p y - \frac{\alpha_g}{R^2} \left( \frac{\partial}{\partial \theta} - \text{i} n q \right) y, \quad (37)$$

where

$$\alpha_p(r) = \frac{r P'}{f^2}, \quad (38)$$

$$\alpha_g(r) = \frac{g'}{f}. \quad (39)$$

Note that Eq. (35) is trivially satisfied. Hence, of the three components of the perturbed force balance equation, only Eq. (34) remains to be solved.

### E. Perturbed Plasma Current Density

Equation (20) yields

$$r R^2 j^r = \frac{\partial b_\phi}{\partial \theta} + \text{i} n b_\theta, \quad (40)$$

$$r R^2 j^\theta = -\text{i} n b_r - \frac{\partial b_\phi}{\partial r}, \quad (41)$$

$$r R^2 j^\phi = \frac{\partial b_\theta}{\partial r} - \frac{\partial b_r}{\partial \theta}, \quad (42)$$

where use has been made of Eqs. (2) and (A11)–(A13).



## F. Perturbed Magnetic Field

According to Sect. A,

$$\mathbf{b} = b_r \nabla r + b_\theta \nabla \theta + b_\phi \nabla \phi, \quad (43)$$

so

$$b^r = \mathbf{b} \cdot \nabla r = |\nabla r|^2 b_r + (\nabla r \cdot \nabla \theta) b_\theta, \quad (44)$$

$$b^\theta = \mathbf{b} \cdot \nabla \theta = (\nabla r \cdot \nabla \theta) b_r + |\nabla \theta|^2 b_\theta, \quad (45)$$

$$b^\phi = \mathbf{b} \cdot \nabla \phi = \frac{b_\phi}{R^2}. \quad (46)$$

Let us define

$$x(r, \theta) = b_\phi. \quad (47)$$

It follows from Eqs. (37), (40), (46), and (47) that

$$b_\theta = -\frac{\alpha_g}{i n} \left( \frac{\partial}{\partial \theta} - i n q \right) y + \alpha_p R^2 y - \frac{1}{i n} \frac{\partial x}{\partial \theta}, \quad (48)$$

$$b^\phi = \frac{x}{R^2}. \quad (49)$$

Equations (44) and (45) can be rearranged to give

$$b_r = \left( \frac{1}{|\nabla r|^2} \right) b^r - \left( \frac{\nabla r \cdot \nabla \theta}{|\nabla r|^2} \right) b_\theta, \quad (50)$$

$$b^\theta = \left( \frac{\nabla r \cdot \nabla \theta}{|\nabla r|^2} \right) b^r + \left[ |\nabla \theta|^2 - \frac{(\nabla r \cdot \nabla \theta)^2}{|\nabla r|^2} \right] b_\theta. \quad (51)$$

But, from Eq. (2),

$$|\nabla r|^2 |\nabla \theta|^2 - (\nabla r \cdot \nabla \theta)^2 = \frac{1}{r^2 R^2}. \quad (52)$$

Thus, Eq. (51) reduces to

$$b^\theta = \left( \frac{\nabla r \cdot \nabla \theta}{|\nabla r|^2} \right) b^r + \left( \frac{1}{r^2 R^2 |\nabla r|^2} \right) b_\theta. \quad (53)$$

Making use of Eqs. (25) and (48), we obtain

$$r^2 R^2 b^\theta = T \left( \frac{\partial}{\partial \theta} - i n q \right) y + U y - Q \frac{\partial x}{\partial \theta}, \quad (54)$$

where

$$Q(r, \theta) = \frac{1}{i n |\nabla r|^2}, \quad (55)$$

$$U(r, \theta) = \frac{\alpha_p R^2}{|\nabla r|^2}, \quad (56)$$

$$T(r, \theta) = \frac{r \nabla r \cdot \nabla \theta}{|\nabla r|^2} - \frac{\alpha_g}{i n |\nabla r|^2}. \quad (57)$$

Equation (50) gives

$$b_r = A \left( \frac{\partial}{\partial \theta} - i n q \right) y - B y + C \frac{\partial x}{\partial \theta}, \quad (58)$$

where

$$A(r, \theta) = \frac{1}{r R^2 |\nabla r|^2} + \frac{\alpha_g}{i n} \frac{\nabla r \cdot \nabla \theta}{|\nabla r|^2}, \quad (59)$$

$$B(r, \theta) = \alpha_p \frac{R^2 \nabla r \cdot \nabla \theta}{|\nabla r|^2}, \quad (60)$$

$$C(r, \theta) = \frac{1}{i n} \frac{\nabla r \cdot \nabla \theta}{|\nabla r|^2}, \quad (61)$$

and use has been made of Eqs. (25) and (48).

### G. First Outer-Region P.D.E.

According to Eq. (18),

$$\nabla \cdot \mathbf{b} = 0, \quad (62)$$

which implies that

$$r \frac{\partial}{\partial r} \left[ \left( \frac{\partial}{\partial \theta} - i n q \right) y \right] + \frac{\partial(r^2 R^2 b^\theta)}{\partial \theta} - S x = 0, \quad (63)$$

where

$$S(r) = i n r^2, \quad (64)$$

and use has been made of Eqs. (2), (25), (49), and (A10). Thus, employing Eq. (54), we obtain the *first outer-region p.d.e.*,<sup>4</sup>

$$r \frac{\partial}{\partial r} \left[ \left( \frac{\partial}{\partial \theta} - i n q \right) y \right] = \frac{\partial}{\partial \theta} \left( Q \frac{\partial x}{\partial \theta} \right) + S x - \frac{\partial}{\partial \theta} \left[ T \left( \frac{\partial}{\partial \theta} - i n q \right) y + U y \right]. \quad (65)$$

## H. Second Outer-Region P.D.E.

According to Eqs. (41), (42), (47), (48), and (58),

$$r R^2 j^\theta = -i n \left[ A \left( \frac{\partial}{\partial \theta} - i n q \right) y - B y + C \frac{\partial x}{\partial \theta} \right] - \frac{\partial x}{\partial r}, \quad (66)$$

$$\begin{aligned} r R^2 j^\phi &= \frac{\partial}{\partial r} \left[ -\frac{\alpha_g}{i n} \left( \frac{\partial}{\partial \theta} - i n q \right) y + \alpha_p R^2 y \right] - \frac{1}{i n} \frac{\partial^2 x}{\partial r \partial \theta} \\ &\quad - \frac{\partial}{\partial \theta} \left[ A \left( \frac{\partial}{\partial \theta} - i n q \right) y - B y + C \frac{\partial x}{\partial \theta} \right]. \end{aligned} \quad (67)$$

So,

$$\begin{aligned} r R^2 (q j^\theta - j^\phi) &= \left( \frac{\partial}{\partial \theta} - i n q \right) \left[ A \left( \frac{\partial}{\partial \theta} - i n q \right) y - B y + C \frac{\partial x}{\partial \theta} \right] \\ &\quad + \frac{1}{i n} \left( \frac{\partial}{\partial \theta} - i n q \right) \frac{\partial x}{\partial r} \\ &\quad - \frac{\partial}{\partial r} \left[ -\frac{\alpha_g}{i n} \left( \frac{\partial}{\partial \theta} - i n q \right) y + \alpha_p R^2 y \right]. \end{aligned} \quad (68)$$

Thus, Eq. (34) gives

$$\begin{aligned} -\frac{r R^2}{f} \frac{\partial}{\partial r} \left( \frac{f}{r} \alpha_p y \right) &= \left( \frac{\partial}{\partial \theta} - i n q \right) \left[ A \left( \frac{\partial}{\partial \theta} - i n q \right) y - B y + C \frac{\partial x}{\partial \theta} \right] \\ &\quad + \frac{1}{i n} \left( \frac{\partial}{\partial \theta} - i n q \right) \frac{\partial x}{\partial r} \\ &\quad - \frac{\partial}{\partial r} \left[ -\frac{\alpha_g}{i n} \left( \frac{\partial}{\partial \theta} - i n q \right) y + \alpha_p R^2 y \right] - r \alpha_g x \\ &\quad + \frac{1}{r} (q \alpha_g + R^2 \alpha_p) \left[ T \left( \frac{\partial}{\partial \theta} - i n q \right) y + U y - Q \frac{\partial x}{\partial \theta} \right], \end{aligned} \quad (69)$$

where use has been made of Eqs. (26), (38), (39), (49), (54). The previous equation reduces to

$$\begin{aligned} -i n \alpha_p \alpha_f R^2 y &= i n \left( \frac{\partial}{\partial \theta} - i n q \right) \left[ r A \left( \frac{\partial}{\partial \theta} - i n q \right) y - r B y + r C \frac{\partial x}{\partial \theta} \right] \\ &\quad + \left( \frac{\partial}{\partial \theta} - i n q \right) r \frac{\partial x}{\partial r} + r \alpha'_g \left( \frac{\partial}{\partial \theta} - i n q \right) y \\ &\quad + \alpha_g r \frac{\partial}{\partial r} \left[ \left( \frac{\partial}{\partial \theta} - i n q \right) y \right] - i n r \frac{\partial R^2}{\partial r} \alpha_p y - \alpha_g S x \end{aligned}$$

$$+ \mathrm{i} n (q \alpha_g + R^2 \alpha_p) \left[ T \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) y + U y - Q \frac{\partial x}{\partial \theta} \right], \quad (70)$$

where

$$\alpha_f(r) = \frac{r^2}{f} \frac{d}{dr} \left( \frac{f}{r} \right), \quad (71)$$

and use has been made of Eq. (64). Employing Eq. (65), we obtain

$$\begin{aligned} -\mathrm{i} n \alpha_p \alpha_f R^2 y &= \mathrm{i} n \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) \left[ r A \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) y - r B y + r C \frac{\partial x}{\partial \theta} \right] \\ &+ \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) r \frac{\partial x}{\partial r} + r \alpha'_g \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) y \\ &+ \alpha_g \frac{\partial}{\partial \theta} \left( Q \frac{\partial x}{\partial \theta} \right) + \alpha_g S x - \alpha_g \frac{\partial}{\partial \theta} \left[ T \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) y + U y \right] \\ &- \mathrm{i} n r \frac{\partial R^2}{\partial r} \alpha_p y - \alpha_g S x \\ &+ \mathrm{i} n (q \alpha_g + R^2 \alpha_p) \left[ T \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) y + U y - Q \frac{\partial x}{\partial \theta} \right], \end{aligned} \quad (72)$$

which yields

$$\begin{aligned} -\mathrm{i} n \alpha_p \alpha_f R^2 y &= \mathrm{i} n \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) \left[ r A \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) y - r B y + r C \frac{\partial x}{\partial \theta} \right] \\ &+ \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) r \frac{\partial x}{\partial r} + r \alpha'_g \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) y \\ &+ \alpha_g \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) \left[ Q \frac{\partial x}{\partial \theta} - T \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) y - U y \right] \\ &- \mathrm{i} n r \frac{\partial R^2}{\partial r} \alpha_p y + \mathrm{i} n R^2 \alpha_p \left[ T \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) y + U y - Q \frac{\partial x}{\partial \theta} \right], \end{aligned} \quad (73)$$

which reduces to the *second outer-region p.d.e.*,<sup>4</sup>

$$\begin{aligned} \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) r \frac{\partial x}{\partial r} &= - \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) T^* \frac{\partial x}{\partial \theta} + U \frac{\partial x}{\partial \theta} + X y \\ &- \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) V \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) y + W \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) y, \end{aligned} \quad (74)$$

where

$$V(r, \theta) = \frac{1}{|\nabla r|^2} \left( \frac{\mathrm{i} n}{R^2} + \frac{\alpha_g^2}{\mathrm{i} n} \right), \quad (75)$$

$$W(r, \theta) = \frac{2 \alpha_g \alpha_p R^2}{|\nabla r|^2} - r \alpha'_g, \quad (76)$$

$$X(r, \theta) = \mathrm{i} n \alpha_p \left[ \frac{\partial}{\partial \theta} (T^* R^2) + r \frac{\partial R^2}{\partial r} - \alpha_f R^2 - U R^2 \right], \quad (77)$$

and  $*$  denotes a complex conjugate.

#### IV. OUTER-REGION O.D.E.S

##### A. Primitive Outer-Region O.D.E.s

Let

$$x(r, \theta) = n z(r, \theta), \quad (78)$$

and let us express  $y(r, \theta)$  and  $z(r, \theta)$  as Fourier series in the poloidal angle,  $\theta$ :

$$y(r, \theta) = \sum_m y_m(r) \exp(\mathrm{i} m \theta), \quad (79)$$

$$z(r, \theta) = \sum_m z_m(r) \exp(\mathrm{i} m \theta), \quad (80)$$

Here, the (not necessarily positive) integers  $m$  are the poloidal mode numbers of the coupled Fourier harmonics included in the calculation. The outer-region p.d.e.s, (65) and (74), reduce to the *primitive outer-region o.d.e.s*,<sup>4,6,15</sup>

$$r \frac{d}{dr} [(m - n q) y_m] = \sum_{m'} \left( A_m^{m'} z_{m'} + B_m^{m'} y_{m'} \right), \quad (81)$$

$$(m - n q) r \frac{dz_m}{dr} = \sum_{m'} \left( C_m^{m'} z_{m'} + D_m^{m'} y_{m'} \right), \quad (82)$$

where

$$n^{-1} A_m^{m'}(r) = \frac{1}{2\pi \mathrm{i}} \oint e^{-\mathrm{i} m \theta} \left( \frac{\partial}{\partial \theta} Q \frac{\partial}{\partial \theta} + S \right) e^{\mathrm{i} m' \theta} d\theta, \quad (83)$$

$$B_m^{m'}(r) = \frac{1}{2\pi \mathrm{i}} \oint e^{-\mathrm{i} m \theta} \left[ -\frac{\partial}{\partial \theta} T \left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) - \frac{\partial U}{\partial \theta} \right] e^{\mathrm{i} m' \theta} d\theta, \quad (84)$$

$$C_m^{m'}(r) = \frac{1}{2\pi \mathrm{i}} \oint e^{-\mathrm{i} m \theta} \left[ -\left( \frac{\partial}{\partial \theta} - \mathrm{i} n q \right) T^* \frac{\partial}{\partial \theta} + U \frac{\partial}{\partial \theta} \right] e^{\mathrm{i} m' \theta} d\theta, \quad (85)$$

$$\begin{aligned}
{}_n D_m^{m'}(r) = \frac{1}{2\pi i} \oint e^{-i m \theta} \left[ - \left( \frac{\partial}{\partial \theta} - i n q \right) V \left( \frac{\partial}{\partial \theta} - i n q \right) \right. \\
\left. + W \left( \frac{\partial}{\partial \theta} - i n q \right) + X \right] e^{i m' \theta} d\theta.
\end{aligned} \tag{86}$$

Hence, it follows from Eqs. (55)–(57), (64), and (75)–(77) that <sup>15</sup>

$$A_m^{m'} = m m' c_m^{m'} + n^2 r^2 \delta_m^{m'} \tag{87}$$

$$B_m^{m'} = m (m' - n q) \left( -f_m^{m'} + n^{-1} \alpha_g c_m^{m'} \right) - m \alpha_p d_m^{m'}, \tag{88}$$

$$C_m^{m'} = -(m - n q) m' \left( f_m^{m'} + n^{-1} \alpha_g c_m^{m'} \right) + m' \alpha_p d_m^{m'}, \tag{89}$$

$$D_m^{m'} = (m - n q) (m' - n q) \left( b_m^{m'} - n^{-2} \alpha_g^2 c_m^{m'} \right) - (m - n q) n^{-1} r \alpha'_g \delta_m^{m'} \tag{90}$$

$$+ \alpha_p \left[ (m - m') g_m^{m'} + n^{-1} \alpha_g (m + m' - 2 n q) d_m^{m'} + r \frac{da_m^{m'}}{dr} - \alpha_f a_m^{m'} - \alpha_p e_m^{m'} \right],$$

where

$$a_m^{m'}(r) = \oint R^2 \exp[-i (m - m') \theta] \frac{d\theta}{2\pi}, \tag{91}$$

$$b_m^{m'}(r) = \oint |\nabla r|^{-2} R^{-2} \exp[-i (m - m') \theta] \frac{d\theta}{2\pi}, \tag{92}$$

$$c_m^{m'}(r) = \oint |\nabla r|^{-2} \exp[-i (m - m') \theta] \frac{d\theta}{2\pi}, \tag{93}$$

$$d_m^{m'}(r) = \oint |\nabla r|^{-2} R^2 \exp[-i (m - m') \theta] \frac{d\theta}{2\pi}, \tag{94}$$

$$e_m^{m'}(r) = \oint |\nabla r|^{-2} R^4 \exp[-i (m - m') \theta] \frac{d\theta}{2\pi}, \tag{95}$$

$$f_m^{m'}(r) = \oint \frac{i r \nabla r \cdot \nabla \theta}{|\nabla r|^2} \exp[-i (m - m') \theta] \frac{d\theta}{2\pi}, \tag{96}$$

$$g_m^{m'}(r) = \oint \frac{i r \nabla r \cdot \nabla \theta}{|\nabla r|^2} R^2 \exp[-i (m - m') \theta] \frac{d\theta}{2\pi}. \tag{97}$$

Here, we have extended the analysis of Ref. 15 to take into account the fact that the  $A_m^{m'}$ ,  $B_m^{m'}$ ,  $a_m^{m'}$ ,  $b_m^{m'}$ , et cetera, are complex quantities in a realistic non-up-down-symmetric tokamak plasma equilibrium. Note, that  $\delta_m^{m'}$  is a Kronecker delta symbol.

## B. Outer-Region O.D.E.s

Let

$$y_m(r) = \frac{\psi_m(r)}{m - n q}, \quad (98)$$

$$z_m(r) = \frac{Z_m(r) + k_m \psi_m(r)}{m - n q}, \quad (99)$$

where

$$k_m(r) = -\text{Re} \left( \frac{B_m^m}{A_m^m} \right) = - \left[ \frac{m (m - n q) n^{-1} \alpha_g c_m^m - m \alpha_p d_m^m}{m^2 c_m^m + n^2 r^2} \right]. \quad (100)$$

Here, we have made use of the fact that  $f_m^m$  is imaginary. [See Eq. (96).] It follows from Eq. (25) that

$$b^r(r, \theta) = i \sum_m \frac{\psi_m(r)}{r R^2} \exp(i m \theta). \quad (101)$$

Furthermore, Eqs. (81) and (82) transform to give the *outer-region o.d.e.s*,<sup>6,15</sup>

$$r \frac{d\psi_m}{dr} = \sum_{m'} \frac{L_m^{m'} Z_{m'} + M_m^{m'} \psi_{m'}}{m' - n q}, \quad (102)$$

$$(m - n q) r \frac{d}{dr} \left( \frac{Z_m}{m - n q} \right) = \sum_{m'} \frac{N_m^{m'} Z_{m'} + P_m^{m'} \psi_{m'}}{m' - n q}, \quad (103)$$

where

$$L_m^{m'}(r) = A_m^{m'}, \quad (104)$$

$$M_m^{m'}(r) = B_m^{m'} + k_{m'} L_m^{m'}, \quad (105)$$

$$N_m^{m'}(r) = C_m^{m'} - k_m L_m^{m'}, \quad (106)$$

$$P_m^{m'}(r) = D_m^{m'} + k_{m'} C_m^{m'} - k_m M_m^{m'} - k_m n q s \delta_m^{m'} - (m - n q) r \frac{dk_m}{dr} \delta_m^{m'}, \quad (107)$$

with

$$s(r) = \frac{r q'}{q}. \quad (108)$$

Note that

$$M_m^m = N_m^m = -m (m - n q) f_m^m. \quad (109)$$

### C. Symmetry Properties

Equations (91)–(97) imply that  $a_{m'}^m = a_m^{m'*}$ ,  $b_{m'}^m = b_m^{m'*}$ ,  $c_{m'}^m = c_m^{m'*}$ ,  $d_{m'}^m = d_m^{m'*}$ ,  $e_{m'}^m = e_m^{m'*}$ ,  $f_{m'}^m = -f_m^{m'*}$ ,  $g_{m'}^m = -g_m^{m'*}$ , for all  $m, m'$ . Hence, Eqs. (87)–(90), Eqs. (100), and (104)–(107) give

$$L_{m'}^m = L_m^{m'}, \quad (110)$$

$$M_{m'}^m = -N_m^{m'}, \quad (111)$$

$$N_{m'}^m = -M_m^{m'}, \quad (112)$$

$$P_{m'}^m = P_m^{m'}, \quad (113)$$

for all  $m, m'$ .

### D. Toroidal Electromagnetic Torque

The volume integrated toroidal electromagnetic torque acting between the magnetic axis and a magnetic flux-surface whose label is  $r$  is given by

$$\begin{aligned} T_\phi(r) &= \int_0^r \oint \oint R^2 \nabla \phi \cdot (\mathbf{J} + \mathbf{j}) \times (\mathbf{B} \times \mathbf{b}) \mathcal{J} d\tilde{r} d\theta d\phi \\ &= \int_0^r \oint \oint (\mathbf{j} \times \mathbf{b})_\phi \mathcal{J} d\tilde{r} d\theta d\phi \end{aligned} \quad (114)$$

Here, use has been made of Eq. (14), as well as the fact that  $P = P(r)$ . We have also taken into account that  $\mathbf{b}$  and  $\mathbf{j}$  vary with  $\phi$  as  $\exp(-in\phi)$ , whereas  $\mathbf{B}$ ,  $\mathbf{J}$ ,  $\mathcal{J}$ , and  $|\nabla\phi|$  are independent of  $\phi$ . It is clear that the zeroth-order (in perturbed quantities) contribution to  $T_\phi$  is identically zero, whereas the first-order contributions average to zero, leaving only second-order (i.e., nonlinear in perturbed quantities) contributions. Making use of Sect. A, as well as Eqs. (2), (20), (50), (53), and (62), we deduce that

$$\begin{aligned} \mathcal{J} (\mathbf{j} \times \mathbf{b})_\phi &= \frac{\partial}{\partial r} (\mathcal{J} b_\phi b^r) + \frac{\partial}{\partial \theta} (\mathcal{J} b_\phi b^\theta) + \frac{\partial}{\partial \phi} (\mathcal{J} b_\phi b^\phi) \\ &\quad - \frac{1}{2} \frac{\partial}{\partial \phi} [\mathcal{J} (b_r b^r + b_\theta b^\theta + b_\phi b^\phi)]. \end{aligned} \quad (115)$$



Hence, we obtain

$$T_\phi(r) = \oint \oint \mathcal{J} b_\phi b^r d\theta d\phi = r \oint \oint R^2 b_\phi b^r d\theta d\phi, \quad (116)$$

where the integral on the right-hand side is evaluated on the magnetic flux-surface whose label is  $r$ . We can reinterpret the previous expression as specifying the net outward flux of toroidal electromagnetic angular momentum across the magnetic flux-surface whose label is  $r$ . Finally, making use of Eqs. (47), (78), (80), and (99)–(101), the previous expression reduces to<sup>6</sup>

$$T_\phi(r) = i \pi^2 n \sum_m \frac{Z_m^* \psi_m - \psi_m^* Z_m}{m - n q}. \quad (117)$$

It follows from Eqs. (102), (103) and (110)–(113) that

$$r \frac{d}{dr} \left( \sum_m \frac{Z_m^* \psi_m - \psi_m^* Z_m}{m - n q} \right) = 0. \quad (118)$$

Hence, we deduce that<sup>6</sup>

$$\frac{dT_\phi}{dr} = 0 \quad (119)$$

in any region of the plasma that satisfies the outer-region o.d.e.s. Thus, the volume integrated toroidal electromagnetic torque acting between the magnetic axis and a given magnetic flux-surface is constant between rational magnetic flux-surfaces. As will become apparent in Sect. V D, the integrated torque can have discontinuous jumps across rational flux-surfaces. It follows that net electromagnetic torques can only develop in the plasma in the immediate vicinity of rational magnetic flux-surfaces, where the ideal-MHD equations become singular.<sup>26</sup>

## V. BEHAVIOR IN VICINITY OF RATIONAL SURFACE

### A. Introduction

The analysis of this section is a generalization of the analysis of Ref. 15 that takes into account the fact that the  $L_m^{m'}$ ,  $M_m^{m'}$ , et cetera, are complex quantities in a realistic non-up-down-symmetric tokamak plasma equilibrium.

Let there be  $K$  rational magnetic flux-surfaces in the plasma. Suppose that the  $k$ th surface lies at  $r = r_k$ , and possesses the resonant poloidal mode number  $m_k$ , where  $q(r_k) = m_k/n$ .

## B. General Case

Consider the solution of the outer-region o.d.e.s, (102) and (103), in the vicinity of the  $k$ th rational surface. Let  $x = r - r_k$ . The most general small- $|x|$  solution of the o.d.e.s can be shown to take the form<sup>6,15</sup>

$$\begin{aligned} \psi_{m_k}(r_k + x) &= A_{Lk}^{\pm} |x|^{\nu_{Lk}} (1 + \lambda_L x + \cdots) + A_{Sk}^{\pm} \text{sgn}(x) |x|^{\nu_{Sk}} (1 + \cdots) \\ &\quad + A_C x (1 + \cdots), \end{aligned} \quad (120)$$

$$\begin{aligned} Z_{m_k}(r_k + x) &= A_{Lk}^{\pm} |x|^{\nu_{Lk}} (b_L + \gamma_L x + \cdots) + A_{Sk}^{\pm} \text{sgn}(x) |x|^{\nu_{Sk}} (b_S + \cdots) \\ &\quad + B_C x (1 + \cdots), \end{aligned} \quad (121)$$

and

$$\begin{aligned} \psi_{m_k+j}(r_k + x) &= A_{Lk}^{\pm} |x|^{\nu_{Lk}} (a_j + c_j x + \cdots) + A_{Sk}^{\pm} \text{sgn}(x) |x|^{\nu_{Sk}} (\tilde{a}_j + \cdots) \\ &\quad + (\bar{\psi}_{m_k+j} + \bar{\psi}'_{m_k+j} x + \cdots), \end{aligned} \quad (122)$$

$$\begin{aligned} Z_{m_k+j}(r_k + x) &= A_{Lk}^{\pm} |x|^{\nu_{Lk}} (b_j + d_j x + \cdots) + A_{Sk}^{\pm} \text{sgn}(x) |x|^{\nu_{Sk}} (\tilde{b}_j + \cdots) \\ &\quad + (\bar{Z}_{m_k+j} + \bar{Z}'_{m_k+j} x + \cdots), \end{aligned} \quad (123)$$

for  $j \neq 0$ . The superscripts  $+$  and  $-$  correspond to  $x > 0$  and  $x < 0$ , respectively. Here,  $A_{Lk}$  is known as the ‘‘coefficient of the large solution,’’ whereas  $A_{Sk}$  is termed the ‘‘coefficient of the small solution.’’<sup>6,15,27</sup> Moreover,

$$\nu_{Lk} = \frac{1}{2} - \sqrt{-D_{Ik}}, \quad (124)$$

$$\nu_{Sk} = \frac{1}{2} + \sqrt{-D_{Ik}}, \quad (125)$$

$$D_{Ik} = -L_0 P_0 - \frac{1}{4}, \quad (126)$$

$$L_0 = - \left( \frac{L_{m_k}^{m_k}}{m_k s} \right)_{r_k}, \quad (127)$$

$$P_0 = - \left( \frac{P_{m_k}^{m_k}}{m_k s} \right)_{r_k}. \quad (128)$$

Note that, ordinarily,  $\nu_{Lk}$ ,  $\nu_{Sk}$ ,  $D_{Ik}$ ,  $L_0$  and  $P_0$  are all real quantities. Furthermore,

$$b_L = \frac{\nu_{Lk}}{L_0}, \quad (129)$$

$$b_S = \frac{\nu_S k}{L_0}, \quad (130)$$

$$A_C = -\frac{1}{r_k P_0} \sum_{j \neq 0} \frac{1}{j} (N_{m_k}^{m_k+j} \bar{Z}_{m_k+j} + P_{m_k}^{m_k+j} \bar{\psi}_{m_k+j})_{r_k}, \quad (131)$$

$$B_C = -\frac{1}{r_k L_0} \sum_{j \neq 0} \frac{1}{j} (L_{m_k}^{m_k+j} \bar{Z}_{m_k+j} + M_{m_k}^{m_k+j} \bar{\psi}_{m_k+j})_{r_k} + \frac{A_C}{L_0}, \quad (132)$$

$$\begin{aligned} \lambda_L = & \frac{1}{2 r_k} \left[ \frac{P_1 L_0}{\nu_L k} + T_1 + \nu_L k \left( \frac{L_1}{L_0} - 2 \right) + 2 M_1 \right]_{r_k} \\ & - \frac{1}{2 (m_k s)_{r_k}} \frac{1}{r_k \nu_L k} \sum_{j \neq 0} \frac{1}{j} \left[ L_{m_k}^{m_k+j} P_{m_k+j}^{m_k} + P_{m_k}^{m_k+j} L_{m_k+j}^{m_k} + M_{m_k}^{m_k+j} M_{m_k+j}^{m_k} + N_{m_k}^{m_k+j} N_{m_k+j}^{m_k} \right. \\ & \left. + b_L (L_{m_k}^{m_k+j} N_{m_k+j}^{m_k} + M_{m_k}^{m_k+j} L_{m_k+j}^{m_k}) + \frac{1}{b_L} (N_{m_k}^{m_k+j} P_{m_k+j}^{m_k} + P_{m_k}^{m_k+j} M_{m_k+j}^{m_k}) \right]_{r_k}, \\ \gamma_L = & \frac{1}{2 r_k} \left[ (1 + \nu_L k) \left( \frac{P_1}{\nu_L k} + \frac{T_1}{L_0} - \frac{\nu_L k}{L_0} \right) + P_0 \left( \frac{L_1}{L_0} - 1 \right) + 2 b_L M_1 \right]_{r_k} \\ & - \frac{1}{2 (m_k s)_{r_k}} \frac{1}{r_k \nu_L k L_0} \sum_{j \neq 0} \frac{1}{j} \left[ (\nu_L k + 1) (P_{m_k}^{m_k+j} L_{m_k+j}^{m_k} + N_{m_k}^{m_k+j} N_{m_k+j}^{m_k}) \right. \\ & \left. + (\nu_L k - 1) (L_{m_k}^{m_k+j} P_{m_k+j}^{m_k} + M_{m_k}^{m_k+j} M_{m_k+j}^{m_k}) + b_L (\nu_L k - 1) (L_{m_k}^{m_k+j} N_{m_k+j}^{m_k} + M_{m_k}^{m_k+j} L_{m_k+j}^{m_k}) \right. \\ & \left. + \frac{1}{b_L} (\nu_L k + 1) (N_{m_k}^{m_k+j} P_{m_k+j}^{m_k} + P_{m_k}^{m_k+j} M_{m_k+j}^{m_k}) \right]_{r_k}, \end{aligned} \quad (134)$$

$$a_j = -\frac{1}{(m_k s)_{r_k}} \left( \frac{L_{m_k+j}^{m_k}}{L_0} + \frac{M_{m_k+j}^{m_k}}{\nu_L k} \right)_{r_k}, \quad (135)$$

$$b_j = -\frac{1}{(m_k s)_{r_k}} \left( \frac{P_{m_k+j}^{m_k}}{\nu_L k} + \frac{N_{m_k+j}^{m_k}}{L_0} \right)_{r_k}, \quad (136)$$

$$\tilde{a}_j = -\frac{1}{(m_k s)_{r_k}} \left( \frac{L_{m_k+j}^{m_k}}{L_0} + \frac{M_{m_k+j}^{m_k}}{\nu_S k} \right)_{r_k}, \quad (137)$$

$$\tilde{b}_j = -\frac{1}{(m_k s)_{r_k}} \left( \frac{P_{m_k+j}^{m_k}}{\nu_S k} + \frac{N_{m_k+j}^{m_k}}{L_0} \right)_{r_k}, \quad (138)$$

$$\begin{aligned} c_j = & \frac{1}{(1 + \nu_L k) r_k} \left[ -\nu_L k a_j + L_{j+1} b_L + M_{j+1} \right. \\ & \left. - \frac{r_k}{m_k s} (L_{m_k+j}^{m_k} \gamma_L + M_{m_k+j}^{m_k} \lambda_L) + \sum_{j' \neq 0} \frac{1}{j'} (L_{m_k+j}^{m_k+j'} b_{j'} + M_{m_k+j}^{m_k+j'} a_{j'}) \right]_{r_k}, \end{aligned} \quad (139)$$

$$d_j = \frac{1}{(1 + \nu_{Lk}) r_k} \left[ - \left( \nu_{Lk} + \frac{m_k s}{j} \right) b_j + N_{j1} b_L + P_{j1} \right. \\ \left. - \frac{r_k}{m_k s} (N_{m_k+j}^{m_k} \gamma_L + P_{m_k+j}^{m_k} \lambda_L) + \sum_{j' \neq 0} \frac{1}{j'} \left( N_{m_k+j}^{m_k+j'} b_{j'} + P_{m_k+j}^{m_k+j'} a_{j'} \right) \right]_{r_k}, \quad (140)$$

$$\bar{\psi}'_{m_k+j} = \frac{1}{r_k} \left[ - \frac{r_k}{m_k s} (L_{m_k+j}^{m_k} B_C + M_{m_k+j}^{m_k} A_C) \right. \\ \left. + \sum_{j' \neq 0} \frac{1}{j'} \left( L_{m_k+j}^{m_k+j'} \bar{Z}_{m_k+j'} + M_{m_k+j}^{m_k+j'} \bar{\psi}_{m_k+j'} \right) \right]_{r_k}, \quad (141)$$

$$\bar{Z}'_{m_k+j} = \frac{1}{r_k} \left[ - \frac{m_k s}{j} \bar{Z}_{m_k+j} - \frac{r_k}{m_k s} (N_{m_k+j}^{m_k} B_C + P_{m_k+j}^{m_k} A_C) \right. \\ \left. + \sum_{j' \neq 0} \frac{1}{j'} \left( N_{m_k+j}^{m_k+j'} \bar{Z}_{m_k+j'} + P_{m_k+j}^{m_k+j'} \bar{\psi}_{m_k+j'} \right) \right]_{r_k}, \quad (142)$$

and

$$L_1 = \lim_{x \rightarrow 0} \left( \frac{L_{m_k}^{m_k}}{m_k - nq} - \frac{r_k L_0}{x} \right), \quad (143)$$

$$P_1 = \lim_{x \rightarrow 0} \left( \frac{P_{m_k}^{m_k}}{m_k - nq} - \frac{r_k P_0}{x} \right), \quad (144)$$

$$T_1 = \lim_{x \rightarrow 0} \left( \frac{-nqs}{m_k - nq} - \frac{r_k}{x} \right), \quad (145)$$

$$M_1 = \lim_{x \rightarrow 0} \left( \frac{M_{m_k}^{m_k}}{m_k - nq} \right), \quad (146)$$

$$L_{j1} = \lim_{x \rightarrow 0} \left( \frac{L_{m_k+j}^{m_k}}{m_k - nq} + \frac{r_k}{m_k s} \frac{L_{m_k+j}^{m_k}}{x} \right), \quad (147)$$

$$M_{j1} = \lim_{x \rightarrow 0} \left( \frac{M_{m_k+j}^{m_k}}{m_k - nq} + \frac{r_k}{m_k s} \frac{M_{m_k+j}^{m_k}}{x} \right), \quad (148)$$

$$N_{j1} = \lim_{x \rightarrow 0} \left( \frac{N_{m_k+j}^{m_k}}{m_k - nq} + \frac{r_k}{m_k s} \frac{N_{m_k+j}^{m_k}}{x} \right), \quad (149)$$

$$P_{j1} = \lim_{x \rightarrow 0} \left( \frac{P_{m_k+j}^{m_k}}{m_k - nq} + \frac{r_k}{m_k s} \frac{P_{m_k+j}^{m_k}}{x} \right), \quad (150)$$

where  $j \neq 0$ .

The coefficients of the large and the small solutions at the  $k$ th rational surface are eval-

uated as follows:

$$\begin{aligned}\bar{\psi}_{m_k+j} &= \psi_{m_k+j}(r_k + \delta) - (a_j + \delta c_j) A_{Lk} |\delta|^{\nu_{Lk}} - \tilde{a}_j \operatorname{sgn}(\delta) |\delta|^{\nu_{Sk}} A_{Sk} \\ &\quad - \bar{\psi}'_{m_k+j} \delta + \mathcal{O}(\delta^2),\end{aligned}\tag{151}$$

$$\begin{aligned}\bar{Z}_{m_k+j} &= Z_{m_k+j}(r_k + \delta) - (b_j + \delta d_j) A_{Lk} |\delta|^{\nu_{Lk}} - \tilde{b}_j \operatorname{sgn}(\delta) |\delta|^{\nu_{Sk}} A_{Sk} \\ &\quad - \bar{Z}'_{m_k+j} \delta + \mathcal{O}(\delta^2),\end{aligned}\tag{152}$$

$$\begin{aligned}A_{Sk} &= \frac{Z_{m_k}(r_k + \delta) - b_L \psi_{m_k}(r_k + \delta) - \delta (B_C - b_L A_C) - \delta (\gamma_L - b_L \lambda_L) A_{Lk} |\delta|^{\nu_{Lk}}}{(b_S - b_L) \operatorname{sgn}(\delta) |\delta|^{\nu_{Sk}}} \\ &\quad + \mathcal{O}(\delta),\end{aligned}\tag{153}$$

$$A_{Lk} = \frac{\psi_{m_k}(r_k + \delta) - A_{Sk} \operatorname{sgn}(\delta) |\delta|^{\nu_{Sk}} - A_C \delta}{(1 + \delta \lambda_L) |\delta|^{\nu_{Lk}}} + \mathcal{O}(\delta^2)\tag{154}$$

for  $j \neq 0$ . The previous set of equations can be solved via iteration.

The analysis in this section is based on the assumption that  $D_{Ik} < 0$ . If  $D_{Ik} > 0$  then the indices  $\nu_{Lk}$  and  $\nu_{Sk}$  become complex, indicating that the plasma in the vicinity of the  $k$ th rational surface is unstable to localized ideal interchange modes.<sup>28</sup>

### C. Special Case

In the limit  $\nu_{Lk} \rightarrow 0$ , some of the previous expressions become singular, and a special treatment is required. Such a special treatment is always needed for rational surfaces characterized by  $q = 1$ . The most general small- $|x|$  solution of the outer-region o.d.e.s takes the form

$$\begin{aligned}\psi_{m_k}(r_k + x) &= A_{Lk}^{\pm} [1 + \nu_{Lk} \ln |x| + \hat{\lambda}_L x (\ln |x| - 1) + \mu_L x (\ln^2 |x| - 2 \ln |x| - 2) + \xi_L x + \dots] \\ &\quad + A_{Sk}^{\pm} x (1 + \dots) + \hat{A}_C x (1 + \dots) + A_D x (\ln |x| - 1 + \dots),\end{aligned}\tag{155}$$

$$\begin{aligned}Z_{m_k}(r_k + x) &= A_{Lk}^{\pm} (b_L + \hat{\gamma}_L x \ln |x| + \delta_L x \ln^2 |x| + \dots) + A_{Sk}^{\pm} x (b_S + \dots) \\ &\quad + B_D x (\ln |x| + \dots),\end{aligned}\tag{156}$$

and

$$\psi_{m_k+j}(r_k + x) = A_{Lk}^{\pm} (\hat{a}_j \ln |x| + \dots) + A_{Sk}^{\pm} x (\tilde{a}_j + \dots) + \bar{\psi}_{m_k+j} (1 + \dots),\tag{157}$$

$$Z_{m_k+j}(r_k+x) = A_{Lk}^{\pm}(\hat{b}_j \ln|x| + \cdots) + A_{Sk}^{\pm}x(\tilde{b}_j + \cdots) + \bar{Z}_{m_k+j}(1 + \cdots), \quad (158)$$

for  $j \neq 0$ . Here,

$$\hat{A}_C = \frac{1}{r_k} \sum_{j \neq 0} \frac{1}{j} (L_{m_k}^{m_k+j} \bar{Z}_{m_k+j} + M_{m_k}^{m_k+j} \bar{\psi}_{m_k+j})_{r_k}, \quad (159)$$

$$\begin{aligned} A_D &= \frac{L_0}{r_k} \sum_{j \neq 0} \frac{1}{j} (N_{m_k}^{m_k+j} \bar{Z}_{m_k+j} + P_{m_k}^{m_k+j} \bar{\psi}_{m_k+j})_{r_k} \\ &\quad - \frac{\nu_{Lk}}{r_k} \sum_{j \neq 0} \frac{1}{j} (L_{m_k}^{m_k+j} \bar{Z}_{m_k+j} + M_{m_k}^{m_k+j} \bar{\psi}_{m_k+j})_{r_k}, \end{aligned} \quad (160)$$

$$B_D = \frac{A_D}{L_0}, \quad (161)$$

$$\begin{aligned} \hat{\lambda}_L &= \frac{P_1 L_0 (1 + \nu_{Lk})}{r_k} + \frac{\nu_{Lk} T_1}{r_k} - \frac{1}{(m_k s)_{r_k}} \frac{1}{r_k} \sum_{j \neq 0} \frac{1}{j} (L_{m_k}^{m_k+j} P_{m_k}^{m_k+j} + M_{m_k}^{m_k+j} M_{m_k}^{m_k+j})_{r_k} \\ &\quad - \frac{1}{(m_k s)_{r_k}} \frac{\nu_{Lk}}{L_0 r_k} (L_{m_k}^{m_k+j} N_{m_k}^{m_k+j} + M_{m_k}^{m_k+j} L_{m_k}^{m_k+j})_{r_k}, \end{aligned} \quad (162)$$

$$\mu_L = -\frac{1}{2(m_k s)_{r_k}} \frac{L_0}{r_k} \sum_{j \neq 0} \frac{1}{j} (N_{m_k}^{m_k+j} P_{m_k}^{m_k+j} + P_{m_k}^{m_k+j} M_{m_k}^{m_k+j})_{r_k}, \quad (163)$$

$$\xi_L = M_1 + \frac{\nu_{Lk}}{r_k} \left( \frac{L_1}{L_0} - 1 \right), \quad (164)$$

$$\hat{\gamma}_L = \frac{P_1 (1 + \nu_{Lk})}{r_k} + \frac{\nu_{Lk} T_1}{L_0 r_k}, \quad (165)$$

$$\delta_L = \frac{\mu_L}{L_0}, \quad (166)$$

$$\hat{a}_j = -\frac{1}{(m_k s)_{r_k}} \left( \frac{\nu_{Lk} L_{m_k}^{m_k+j}}{L_0} + M_{m_k}^{m_k+j} \right)_{r_k}, \quad (167)$$

$$\hat{b}_j = -\frac{1}{(m_k s)_{r_k}} \left( P_{m_k}^{m_k+j} + \frac{\nu_{Lk} N_{m_k}^{m_k+j}}{L_0} \right)_{r_k}. \quad (168)$$

Moreover,  $\tilde{a}_j$  and  $\tilde{b}_j$  are again specified by Eqs. (137)–(138).

The coefficients of the large and the small solutions at the  $k$ th rational surface are evaluated as follows:

$$\bar{\psi}_{m_k+j} = \psi_{m_k+j}(r_k + \delta) - \hat{a}_j A_{Lk} \ln|\delta| + \mathcal{O}(\delta), \quad (169)$$

$$\bar{Z}_{m_k+j} = Z_{m_k+j}(r_k + \delta) - \hat{b}_j A_{Lk} \ln|\delta| + \mathcal{O}(\delta), \quad (170)$$

$$A_{Sk} = \frac{Z_{m_k}(r_k + \delta) - b_L A_{Lk} - \delta \ln |\delta| [B_D + (\hat{\gamma}_L + \delta_L \ln |\delta|) A_{Lk}]}{b_S \delta} + \mathcal{O}(\delta), \quad (171)$$

$$A_{Lk} = \frac{\psi_{m_k}(r_k + \delta) - \delta [A_{Sk} + A_C + A_D (\ln |\delta| - 1)]}{1 + \nu_{Lk} \ln |\delta| + \delta [\hat{\lambda}_L (\ln |\delta| - 1) + \mu_L (\ln^2 |\delta| - 2 \ln |\delta| - 2) + \xi_L]} + \mathcal{O}(\delta^2) \quad (172)$$

for  $j \neq 0$ . As before, the previous equations can be solved via iteration.

#### D. Asymptotic Matching Across Rational Surfaces

Consider the resonant layer solution in the vicinity of the  $k$ th rational surface, whose resonant poloidal mode number is  $m_k$ . This solution can be separated into independent tearing and twisting parity components.<sup>27</sup> The tearing parity component is such that  $\psi_{m_k}(r_k - x) = \psi_{m_k}(r_k + x)$  throughout the layer, whereas the twisting parity component is such that  $\psi_{m_k}(r_k - x) = -\psi_{m_k}(r_k + x)$ . It turns out, however, that the twisting parity response of a resonant layer to the solution in the outer region is generally negligible compared to the tearing parity response.<sup>4,15,29</sup> Hence, in this paper, we shall neglect the twisting parity responses of the various resonant layers in the plasma all together.

The neglect of the twisting parity responses of the various resonant layers in the plasma implies that the coefficients of the large solution to the left and to the right of each rational surface in the plasma are equal to one another.<sup>6</sup> In other words,

$$A_{Lk}^- = A_{Lk}^+ = A_{Lk} \quad (173)$$

for all  $k$ . Note, however, that the coefficients of the small solution to the left and to the right of a given rational surface are not, in general, equal to one another.

Consider a solution that is completely continuous across the  $k$ th rational surface, so that  $A_{Sk}^- = A_{Sk}^+$ . According to the preceding analysis, the continuity condition for the resonant harmonic can be written as

$$\psi_{m_k}(r_k + |\delta|) = \psi_{m_k}(r_k - |\delta|) + 2|\delta| [A_{Lk} |\delta|^{\nu_{Lk}} \lambda_L + A_C] + 2A_{Sk}^- |\delta|^{\nu_{Sk}} + \mathcal{O}(\delta^2), \quad (174)$$

$$\begin{aligned} Z_{m_k}(r_k + |\delta|) &= Z_{m_k}(r_k - |\delta|) + 2|\delta| [A_{Lk} |\delta|^{\nu_{Lk}} \gamma_L + B_C] + 2A_{Sk}^- b_S |\delta|^{\nu_{Sk}} \\ &+ \mathcal{O}(\delta^2), \end{aligned} \quad (175)$$

$$\begin{aligned}\psi_{m_k+j}(r_k + |\delta|) &= \psi_{m_k+j}(r_k - |\delta|) + 2|\delta| [A_{Lk} |\delta|^{\nu_{Lk}} c_j + \bar{\psi}'_{m_k+j}] + 2A_{S_k}^- a_j |\delta|^{\nu_{Sk}} \\ &\quad + \mathcal{O}(\delta^2),\end{aligned}\tag{176}$$

$$\begin{aligned}Z_{m_k+j}(r_k + |\delta|) &= Z_{m_k+j}(r_k - |\delta|) + 2|\delta| [A_{Lk} |\delta|^{\nu_{Lk}} d_j + \bar{Z}'_{m_k+j}] + 2A_{S_k}^- b_j |\delta|^{\nu_{Sk}} \\ &\quad + \mathcal{O}(\delta^2)\end{aligned}\tag{177}$$

in the general case, and

$$\begin{aligned}\psi_{m_k}(r_k + |\delta|) &= \psi_{m_k}(r_k - |\delta|) \\ &\quad + 2|\delta| \{A_{Lk} [\hat{\lambda}_L (\ln |\delta| - 1) + \hat{\mu}_L (\ln^2 |\delta| - 2 \ln |\delta| - 2) + \xi_L] \\ &\quad + A_C + A_D (\ln |\delta| - 1) + A_{S_k}^- \} + \mathcal{O}(\delta^2),\end{aligned}\tag{178}$$

$$\begin{aligned}Z_{m_k}(r_k + |\delta|) &= Z_{m_k}(r_k - |\delta|) + 2|\delta| [A_{Lk} \ln |\delta| (\hat{\gamma}_L + \delta_L \ln |\delta|) + B_D \ln |\delta| + A_{S_k}^- b_S] \\ &\quad + \mathcal{O}(\delta^2),\end{aligned}\tag{179}$$

$$\psi_{m_k+j}(r_k + |\delta|) = \psi_{m_k+j}(r_k - |\delta|) + \mathcal{O}(\delta),\tag{180}$$

$$Z_{m_k+j}(r_k + |\delta|) = Z_{m_k+j}(r_k - |\delta|) + \mathcal{O}(\delta)\tag{181}$$

in the special case. In both cases,  $j \neq 0$ .

Consider a solution that is launched from the  $k$ th rational surface, so that  $A_{Lk} = A_{S_k}^- = 0$ . It follows from the preceding analysis that

$$\psi_{m_k}(r_k + |\delta|) = A_{S_k}^+ |\delta|^{\nu_{Sk}} + \mathcal{O}(\delta^2),\tag{182}$$

$$Z_{m_k}(r_k + |\delta|) = A_{S_k}^+ b_S |\delta|^{\nu_{Sk}} + \mathcal{O}(\delta^2),\tag{183}$$

$$\psi_{m_k+j}(r_k + |\delta|) = A_{S_k}^+ \tilde{a}_j |\delta|^{\nu_{Sk}} + \mathcal{O}(\delta^2),\tag{184}$$

$$Z_{m_k+j}(r_k + |\delta|) = A_{S_k}^+ \tilde{b}_j |\delta|^{\nu_{Sk}} + \mathcal{O}(\delta^2)\tag{185}$$

for  $j \neq 0$ .

It is helpful to define the quantities<sup>6</sup>

$$\Psi_k = r_k^{\nu_{Lk}} \left( \frac{\nu_{Sk} - \nu_{Lk}}{L_{m_k}^{m_k}} \right)_{r_k}^{1/2} A_{Lk},\tag{186}$$

$$\Delta\Psi_k = r_k^{\nu_{Sk}} \left( \frac{\nu_{Sk} - \nu_{Lk}}{L_{m_k}^{m_k}} \right)_{r_k}^{1/2} (A_{S_k}^+ - A_{S_k}^-)\tag{187}$$



at each rational surface in the plasma. Here, the complex parameter  $\Psi_k$  is a measure of the reconnected helical magnetic flux at the  $k$ th rational surface, whereas the complex parameter  $\Delta\Psi_k$  is a measure of the strength of a localized current sheet that flows parallel to the equilibrium magnetic field at the surface. It is evident from Eqs. (117), (119)–(121), (124), (125), (127), (129), (130), and (173)–(187) that<sup>6,15</sup>

$$T_\phi(r) = \int_0^r \sum_{k=1,K} \delta T_k \delta(\tilde{r} - r_k) d\tilde{r}, \quad (188)$$

where

$$\delta T_k = 2\pi^2 n \operatorname{Im}(\Psi_k^* \Delta\Psi_k). \quad (189)$$

Here,  $\delta T_k$  is the net toroidal electromagnetic torque exerted on the plasma in the immediate vicinity of the  $k$ th rational surface.

## VI. VACUUM SOLUTION

### A. Plasma/Vacuum Interface

Let the plasma/vacuum interface correspond to  $r = \epsilon$ , where  $\epsilon$  is the inverse aspect-ratio of the plasma. In other words, let  $\epsilon = a/R_0$ , where  $a$  is the effective minor radius of the plasma. The region external to the plasma,  $r > \epsilon$ , is assumed to be free of non-axisymmetric currents.

### B. Perturbed Vacuum Magnetic Field

In the vacuum region  $r > \epsilon$ , the curl-free perturbed magnetic field can be written in the form<sup>6</sup>

$$\mathbf{b} = \mathbf{i} \nabla [V(r, \theta) \exp(-\mathbf{i} n \phi)]. \quad (190)$$

The physical constraint  $\nabla \cdot \mathbf{b} = 0$  implies that

$$\nabla^2 [V(r, \theta) \exp(-\mathbf{i} n \phi)] = 0. \quad (191)$$

### C. Toroidal Coordinates

It is necessary to obtain a solution of the previous equation that extends to infinity. This goal can be achieved using *orthogonal toroidal coordinates*,  $\mu$ ,  $\eta$ ,  $\phi$ , where<sup>30</sup>

$$R = \frac{\sinh \mu}{\cosh \mu - \cos \eta}, \quad (192)$$

$$Z = \frac{\sin \eta}{\cosh \mu - \cos \eta}. \quad (193)$$

Here,  $\mu(R, Z) \rightarrow 0$  corresponds to either  $R \rightarrow 0$  or  $(R^2 + Z^2)^{1/2} \rightarrow \infty$  (i.e., an approach to the toroidal symmetry axis or to infinity), whereas  $\mu(R, Z) \rightarrow \infty$  corresponds to  $(R, Z) \rightarrow (1, 0)$  (i.e., an approach to the magnetic axis). Furthermore,  $\eta(R, Z)$  is an angular variable in the poloidal plane.

The most general solution of Eq. (191), in toroidal coordinates, that satisfies the physical constraint that the scalar magnetic potential,  $V$ , is well-behaved a long way from the plasma, can be written<sup>31</sup>

$$V = a_0 \frac{\sqrt{\pi} \Gamma(1/2 - n)}{\sqrt{2}} (z - \cos \eta)^{1/2} P_{-1/2}^n(z) \quad (194)$$

$$+ \sum_{m \neq 0} a_m \cos(|m| \pi) \frac{\sqrt{\pi} \Gamma(|m| + 1/2 - n) \epsilon^{|m|}}{2^{|m|-1/2} |m|!} (z - \cos \eta)^{1/2} P_{m-1/2}^n(z) \exp(-i m \eta),$$

where  $z = \cosh \mu$ , the  $P_{m-1/2}^n(z)$  are *toroidal functions*,<sup>32</sup>  $\Gamma(z)$  is a gamma function,<sup>33</sup> and the  $a_m$  are arbitrary complex coefficients. Here, the normalization of the  $a_m$  is the same as that adopted in Ref. 6.

### D. Plasma/Vacuum Interface

In the vicinity of the plasma/vacuum interface, we can write

$$V(r, \theta) = \sum_m V_m(r) \exp(i m \theta), \quad (195)$$

where

$$V_m(\epsilon) = \oint_{r=\epsilon} V \exp(-i m \theta) \frac{d\theta}{2\pi} = \sum_{m'} \mathcal{P}_m^{m'} a_{m'}, \quad (196)$$

and, according to Eq. (194),

$$\begin{aligned} \mathcal{P}_m^{m'} &= \cos(|m'| \pi) \frac{\sqrt{\pi} \Gamma(|m'| + 1/2 - n) \epsilon^{|m'|}}{2^{|m'|-1/2} |m'|!} \\ &\times \oint_{r=\epsilon} (z - \cos \eta)^{1/2} P_{m'-1/2}^n(z) \exp[-i(m\theta + m'\eta)] \frac{d\theta}{2\pi}, \end{aligned} \quad (197)$$

for general  $m'$ , and

$$\mathcal{P}_m^0 = \frac{\sqrt{\pi} \Gamma(1/2 - n)}{\sqrt{2}} \oint_{\hat{r}=1} (z - \cos \eta)^{1/2} P_{-1/2}^n(z) \exp(-i m \theta) \frac{d\theta}{2\pi}, \quad (198)$$

for the special case  $m' = 0$ .

Let

$$\mathcal{J} \mathbf{b} \cdot \nabla r = i \psi(r, \theta) \exp(-i n \phi). \quad (199)$$

In the vicinity of the plasma/vacuum interface, we can write

$$\psi(r, \theta) = \sum_m \psi_m(r) \exp(i m \theta), \quad (200)$$

where

$$\psi_m(\epsilon) = \oint_{r=\epsilon} \mathcal{J} \nabla V \cdot \nabla r \exp(-i m \theta) \frac{d\theta}{2\pi} = \sum_{m'} \mathcal{R}_m^{m'} a_{m'}, \quad (201)$$

and, according to Eq. (194),

$$\begin{aligned} \mathcal{R}_m^{m'} &= \cos(|m'| \pi) \frac{\sqrt{\pi} \Gamma(|m'| + 1/2 - n) \epsilon^{|m'|}}{2^{|m'|-1/2} |m'|!} \\ &\times \oint_{r=\epsilon} \left\{ \left[ \frac{1}{2} (z - \cos \eta)^{-1/2} P_{m'-1/2}^n(z) + (z - \cos \eta)^{1/2} \frac{dP_{m'-1/2}^n}{dz} \right] \mathcal{J} \nabla r \cdot \nabla z \right. \\ &+ \left. \left[ \frac{1}{2} (z - \cos \eta)^{-1/2} \sin \eta - i m' (z - \cos \eta)^{1/2} \right] P_{m'-1/2}^n(z) \mathcal{J} \nabla r \cdot \nabla \eta \right\} \\ &\times \exp[-i(m\theta + m'\eta)] \frac{d\theta}{2\pi}, \end{aligned} \quad (202)$$

for general  $m'$ , and

$$\begin{aligned} \mathcal{R}_m^0 &= \frac{\sqrt{\pi} \Gamma(1/2 - n)}{\sqrt{2}} \\ &\times \oint_{r=\epsilon} \left\{ \left[ \frac{1}{2} (z - \cos \eta)^{-1/2} P_{-1/2}^n(z) + (z - \cos \eta)^{1/2} \frac{dP_{-1/2}^n}{dz} \right] \mathcal{J} \nabla r \cdot \nabla z \right. \\ &+ \left. \frac{1}{2} (z - \cos \eta)^{-1/2} \sin \eta P_{-1/2}^n(z) \nabla r \cdot \nabla \eta \right\} \exp(-i m \theta) \frac{d\theta}{2\pi}, \end{aligned} \quad (203)$$

for the special case  $m' = 0$ .

### E. Homogeneous Boundary Condition at Plasma/Vacuum Interface

According to Eqs. (49), (78), (80), (99)–(101), (190), and (195),

$$V_m(r) = \frac{Z_m(r)}{m - n q(r)}, \quad (204)$$

and the  $\psi_m(r)$  defined in Eq. (98) can be identified with the  $\psi_m(r)$  defined in Eqs. (199) and (200). Thus, Eqs. (196) and (201) yield the following homogenous boundary condition at the plasma/vacuum interface,

$$\frac{Z_m(\epsilon)}{m - n q(\epsilon)} = \sum_{m'} H_{mm'} \psi_{m'}(\epsilon), \quad (205)$$

where

$$\sum_{m''} H_{mm''} \mathcal{R}_{m''}^{m'} = \mathcal{P}_m^{m'}. \quad (206)$$

### F. Toroidal Electromagnetic Angular Momentum Flux

By analogy with Eq. (116), the outward flux of toroidal electromagnetic angular momentum across the plasma/vacuum interface, which is equal to the flux of toroidal electromagnetic angular momentum across a surface of constant  $\mu$  (in the direction of decreasing  $\mu$ ) in the vacuum region, is given by

$$\begin{aligned} T_\phi(\epsilon) &= - \oint \oint (\nabla \mu \times \nabla \eta \cdot \nabla \phi)^{-1} b_\phi b^\mu d\eta d\phi \\ &= - \frac{i\pi n}{2} \oint \frac{z^2 - 1}{z - \cos \eta} \left( \frac{\partial V}{\partial z} V^* - \frac{\partial V^*}{\partial z} V \right) d\eta. \end{aligned} \quad (207)$$

Making use of Eq. (194), we deduce that

$$T_\phi(\epsilon) = 0. \quad (208)$$

In other words, the flux of toroidal electromagnetic angular momentum across the vacuum/plasma interface is zero, as must be the case because an isolated tokamak plasma cannot exert a net toroidal electromagnetic torque on itself.<sup>6</sup>

According to Eq. (117), the outward flux of toroidal electromagnetic angular momentum across the plasma/vacuum interface can also be written

$$T_\phi(\epsilon) = i \pi^2 n \sum_m \left[ \frac{Z_m^* \psi_m - \psi_m^* Z_m}{m - n q} \right]_{r=\epsilon}. \quad (209)$$

It follows from Eq. (205) that Eq. (208) can only be satisfied, in general, if the vacuum response matrix,  $H_{mm'}$ , is Hermitian.

### G. Vacuum Response Matrix

It is clearly important to prove that the vacuum response matrix,  $H_{mm'}$ , is Hermitian. Otherwise, toroidal electromagnetic angular momentum is not conserved.

Let us assume that all perturbed quantities vary with the toroidal angle,  $\phi$ , as  $\exp(-i n \phi)$ . The vacuum region outside the plasma corresponds to the section,  $C$  (say), of the  $R, Z$  plane that lies between the curve  $r = \epsilon$  and the curve  $z = 1$ . Let us define the function  $\mathcal{E}_m(z, \mu)$  such that

$$\mathcal{E}_m = \exp(-i m \theta) \quad \text{at } r = \epsilon, \quad (210)$$

$$\nabla^2 \mathcal{E}_m = \frac{n^2}{R^2} \mathcal{E}_m \quad \text{throughout } C, \quad (211)$$

$$\mathcal{E}_m = 0 \quad \text{at } z = 1. \quad (212)$$

In this section,  $\nabla^2$  denotes a two-dimensional Laplacian in the  $R, Z$  plane, and all vector analysis is two-dimensional, and takes place in the  $R$ - $Z$  plane. Recall that

$$\nabla^2 V = \frac{n^2}{R^2} V \quad \text{throughout } C, \quad (213)$$

$$V = 0 \quad \text{at } z = 1. \quad (214)$$

It follows from Eq. (201) and (210) that

$$\psi_m(\epsilon) = \oint_{r=\epsilon} \mathcal{J} \mathcal{E}_m \nabla V \cdot \nabla r \frac{d\theta}{2\pi}. \quad (215)$$

The previous equation can also be written

$$\psi_m(\epsilon) = -\frac{1}{2\pi} \oint_S \mathcal{E}_m \nabla V \cdot d\mathbf{S} \quad (216)$$

where  $S$  is the bounding surface of the vacuum domain,  $C$ , and use has been made of Eqs. (212) and (214). Note that  $d\mathbf{S} = -\mathcal{J} \nabla r d\theta$ . Now,

$$\begin{aligned} \oint_S (\mathcal{E}_m \nabla V - V \nabla \mathcal{E}_m) \cdot d\mathbf{S} &= \int_C \nabla \cdot (\mathcal{E}_m \nabla V - V \nabla \mathcal{E}_m) dC \\ &= \int_C (\mathcal{E}_m \nabla^2 V - V \nabla^2 \mathcal{E}_m) dC = 0, \end{aligned} \quad (217)$$

where use has been made of Eqs. (211) and (213). The previous three equations imply that

$$\psi_m(\epsilon) = -\frac{1}{2\pi} \oint_S V \nabla \mathcal{E}_m \cdot d\mathbf{S} = \oint_{r=\epsilon} \mathcal{J} V \nabla \mathcal{E}_m \cdot \nabla r \frac{d\theta}{2\pi}, \quad (218)$$

where use has been made of Eqs. (212) and (214). Thus, in accordance with Eqs. (196), (204), and (205), we can write

$$\psi_m(\epsilon) = \sum_{m'} H_{mm'}^{-1} V_{m'}(\epsilon), \quad (219)$$

where

$$H_{mm'}^{-1} = \oint_{r=\epsilon} \mathcal{J} \nabla \mathcal{E}_m \cdot \nabla r \exp(i m' \theta) \frac{d\theta}{2\pi}. \quad (220)$$

The inverse vacuum response matrix can be written

$$H_{mm'}^{-1} = -\frac{1}{2\pi} \oint_S \mathcal{E}_{m'}^* \nabla \mathcal{E}_m \cdot d\mathbf{S}, \quad (221)$$

where use has been made of Eqs. (210), (212), and (220). It follows that

$$\begin{aligned} H_{mm'}^{-1} - H_{m'm}^{-1*} &= -\frac{1}{2\pi} \oint_S (\mathcal{E}_{m'}^* \nabla \mathcal{E}_m - \mathcal{E}_m \nabla \mathcal{E}_{m'}^*) \cdot d\mathbf{S} \\ &\quad - \frac{1}{2\pi} \int_C \nabla \cdot (\mathcal{E}_{m'}^* \nabla \mathcal{E}_m - \mathcal{E}_m \nabla \mathcal{E}_{m'}^*) dC \\ &\quad - \frac{1}{2\pi} \int_C (\mathcal{E}_{m'}^* \nabla^2 \mathcal{E}_m - \mathcal{E}_m \nabla^2 \mathcal{E}_{m'}^*) dC = 0, \end{aligned} \quad (222)$$

where use has been made of Eq. (211). Thus, we conclude that  $H_{mm'}^{-1}$ , as defined in Eq. (220), is Hermitian. It follows that the vacuum response matrix,  $H_{mm'}$ , is also Hermitian.

## VII. INVERSE ASPECT-RATIO EXPANDED TOKAMAK EQUILIBRIUM

### A. Equilibrium Magnetic Flux-Surfaces

Let us assume that the inverse aspect-ratio of the plasma,  $\epsilon$ , is such that  $0 < \epsilon \ll 1$ . Let  $r = \epsilon \hat{r}$ ,  $\nabla = \epsilon^{-1} \hat{\nabla}$ , and  $' \rightarrow \epsilon^{-1} '$ . Suppose that the loci of the equilibrium magnetic

flux-surfaces can be written in the parametric form:<sup>2,6,34,35</sup>

$$R(\hat{r}, \omega) = 1 - \epsilon \hat{r} \cos \omega + \epsilon^2 \sum_{j>0} H_j(\hat{r}) \cos[(j-1)\omega] + \epsilon^2 \sum_{j>1} V_j(\hat{r}) \sin[(j-1)\omega] + \epsilon^3 L(\hat{r}) \cos \omega, \quad (223)$$

$$Z(\hat{r}, \omega) = \epsilon \hat{r} \sin \omega + \epsilon^2 \sum_{j>1} H_j(\hat{r}) \sin[(j-1)\omega] - \epsilon^2 \sum_{j>1} V_j(\hat{r}) \cos[(j-1)\omega] - \epsilon^3 L(\hat{r}) \sin \omega, \quad (224)$$

where  $j$  is a positive integer. Here,  $H_1(\hat{r})$  controls the relative horizontal locations of the flux-surface centroids,  $H_2(\hat{r})$  and  $V_2(\hat{r})$  control the magnitudes and vertical tilts of the flux-surface ellipticities,  $H_3(\hat{r})$  and  $V_3(\hat{r})$  control the magnitudes and vertical tilts of the flux-surface triangularities, et cetera, whereas  $L(\hat{r})$  is a flux-surface re-labelling parameter. Moreover,  $\omega(R, Z)$  is a poloidal angle that is distinct from  $\theta$ . Note that  $V_1$  does not appear in Eq. (224) because such a factor merely gives rise to a rigid vertical shift of the plasma that can be eliminated by a suitable choice of the origin of the flux-coordinate system.<sup>35</sup>

Let

$$J(\hat{r}, \omega) = \frac{1}{\epsilon^2} \left( \frac{\partial R}{\partial \omega} \frac{\partial Z}{\partial \hat{r}} - \frac{\partial R}{\partial \hat{r}} \frac{\partial Z}{\partial \omega} \right) \quad (225)$$

be the Jacobian of the  $\hat{r}, \omega$  coordinate system. We can transform to the  $\hat{r}, \theta$  coordinate system by writing

$$\theta(\hat{r}, \omega) = 2\pi \int_0^\omega \frac{J(\hat{r}, \tilde{\omega})}{R(\hat{r}, \tilde{\omega})} d\tilde{\omega} \Big/ \oint \frac{J(\hat{r}, \omega)}{R(\hat{r}, \omega)} d\omega, \quad (226)$$

$$\hat{r} = \frac{1}{2\pi} \oint \frac{J(\hat{r}, \omega)}{R(\hat{r}, \omega)} d\omega. \quad (227)$$

This transformation ensures that

$$\frac{\partial \theta}{\partial \omega} = \frac{J}{\hat{r} R}, \quad (228)$$

and, hence, that

$$\mathcal{J} \equiv \frac{R}{\epsilon} \left( \frac{\partial R}{\partial \theta} \frac{\partial Z}{\partial \hat{r}} - \frac{\partial R}{\partial \hat{r}} \frac{\partial Z}{\partial \theta} \right) = \epsilon R J \frac{\partial \omega}{\partial \theta} = r R^2, \quad (229)$$

in accordance with Eq. (2).

## B. Metric Elements

We can determine the metric elements of the flux-coordinate system by combining Eqs. (223)–(227). Evaluating the elements up to  $\mathcal{O}(\epsilon)$ , but retaining  $\mathcal{O}(\epsilon^2)$  contributions to terms that are independent of  $\omega$ , we obtain,<sup>6,34,35</sup>

$$L(\hat{r}) = \frac{\hat{r}^3}{8} - \frac{\hat{r} H_1}{2} - \frac{1}{2} \sum_{j>1} (j-1) \frac{H_j^2}{\hat{r}} - \frac{1}{2} \sum_{j>1} (j-1) \frac{V_j^2}{\hat{r}}, \quad (230)$$

$$\begin{aligned} \theta = \omega + \epsilon \hat{r} \sin \omega - \epsilon \sum_{j>0} \frac{1}{j} \left[ H_j' - (j-1) \frac{H_j}{\hat{r}} \right] \sin(j \omega) \\ + \epsilon \sum_{j>1} \frac{1}{j} \left[ V_j' - (j-1) \frac{V_j}{\hat{r}} \right] \cos(j \omega), \end{aligned} \quad (231)$$

$$\begin{aligned} |\hat{\nabla} \hat{r}|^2 = 1 + 2 \epsilon \sum_{j>0} H_j' \cos(j \theta) + 2 \epsilon \sum_{j>1} V_j' \sin(j \theta) \\ + \epsilon^2 \left( \frac{3 \hat{r}^2}{4} - H_1 + \frac{1}{2} \sum_{j>0} \left[ H_j'^2 + (j^2 - 1) \frac{H_j^2}{\hat{r}^2} \right] \right. \\ \left. + \frac{1}{2} \sum_{j>1} \left[ V_j'^2 + (j^2 - 1) \frac{V_j^2}{\hat{r}^2} \right] \right), \end{aligned} \quad (232)$$

$$\begin{aligned} \hat{\nabla} \hat{r} \cdot \hat{\nabla} \theta = \epsilon \sin \theta - \epsilon \sum_{j>0} \frac{1}{j} \left[ H_j'' + \frac{H_j'}{\hat{r}} + (j^2 - 1) \frac{H_j}{\hat{r}^2} \right] \sin(j \theta) \\ + \epsilon \sum_{j>1} \frac{1}{j} \left[ V_j'' + \frac{V_j'}{\hat{r}} + (j^2 - 1) \frac{V_j}{\hat{r}^2} \right] \cos(j \theta), \end{aligned} \quad (233)$$

$$R^2 = 1 - 2 \epsilon \hat{r} \cos \theta - \epsilon^2 \left( \frac{\hat{r}^2}{2} - \hat{r} H_1' - 2 H_1 \right). \quad (234)$$

Here,  $' \equiv d/d\hat{r}$ . Moreover, we have made use of the fact that  $V_j \propto H_j$ , for  $j > 1$ , because  $V_j$  and  $H_j$  satisfy the identical differential equations, (240) and (241).

## C. Expansion of Grad-Shafranov Equation

Let us write

$$f(\hat{r}) = \epsilon \frac{\hat{r} g}{q}, \quad (235)$$



$$g(\hat{r}) = 1 + \epsilon^2 g_2(\hat{r}) + \epsilon^4 g_4(\hat{r}), \quad (236)$$

$$P'(\hat{r}) = \epsilon^2 p'_2(\hat{r}), \quad (237)$$

where  $q$ ,  $g_2$ ,  $g_4$ , and  $p_2$  are all  $\mathcal{O}(1)$ . Here, the safety-factor,  $q(\hat{r})$ , and the second-order plasma pressure gradient,  $p'_2(\hat{r})$ , are the two free flux-surface functions that characterize the plasma equilibrium.<sup>23</sup>

Expanding the Grad-Shafranov equation, (16), order by order in the small parameter  $\epsilon$ , making use of Eqs. (232)–(237), we obtain<sup>2,4,34,35</sup>

$$g'_2 = -p'_2 - \frac{\hat{r}}{q^2} (2 - s), \quad (238)$$

$$H''_1 = -(3 - 2s) \frac{H'_1}{\hat{r}} - 1 + \frac{2p'_2 q^2}{\hat{r}}, \quad (239)$$

$$H''_j = -(3 - 2s) \frac{H'_j}{\hat{r}} + (j^2 - 1) \frac{H_j}{\hat{r}^2} \quad \text{for } j > 1, \quad (240)$$

$$V''_j = -(3 - 2s) \frac{V'_j}{\hat{r}} + (j^2 - 1) \frac{V_j}{\hat{r}^2} \quad \text{for } j > 1, \quad (241)$$

$$\begin{aligned} g'_4 = & -\frac{\hat{r}}{q^2} \left( \frac{3\hat{r}^2}{2} - 2\hat{r} H'_1 \right. \\ & + \sum_{j>0} \left[ H_j'^2 + 2(j^2 - 1) \frac{H'_j H_j}{\hat{r}} - (j^2 - 1) \frac{H_j^2}{\hat{r}^2} \right] \\ & + \sum_{j>1} \left[ V_j'^2 + 2(j^2 - 1) \frac{V'_j V_j}{\hat{r}} - (j^2 - 1) \frac{V_j^2}{\hat{r}^2} \right] \Big) \\ & + \frac{\hat{r}}{q^2} (2 - s) \left( -g_2 - \frac{3\hat{r}^2}{4} + \frac{\hat{r}^2}{q^2} + H_1 + \frac{1}{2} \sum_{j>0} \left[ 3H_j'^2 - (j^2 - 1) \frac{H_j^2}{\hat{r}^2} \right] \right. \\ & \left. + \frac{1}{2} \sum_{j>1} \left[ 3V_j'^2 - (j^2 - 1) \frac{V_j^2}{\hat{r}^2} \right] \right) \\ & + p'_2 \left( g_2 + \frac{\hat{r}^2}{2} + \frac{\hat{r}^2}{q^2} - 2H_1 - 3\hat{r} H'_1 \right). \end{aligned} \quad (242)$$

Note that the relative horizontal shift of magnetic flux-surfaces,  $H_1$ , otherwise known as the *Shafranov shift*,<sup>36</sup> is driven by toroidicity [the second term on the right-hand side of Eq. (239)], and plasma pressure gradients (the third term). All of the other shaping terms

(i.e., the  $H_j$ , for  $j > 1$ , and the  $V_j$ ) are driven by axisymmetric currents flowing in external magnetic field-coils.<sup>35</sup>

Finally, it follows from Eqs. (38), (39), (71), and (235)–(237) that

$$\alpha_p(\hat{r}) = \frac{p'_2 q^2}{\hat{r}} (1 - 2 \epsilon^2 g_2), \quad (243)$$

$$\alpha_g(\hat{r}) = \frac{q}{\hat{r}} (g'_2 - \epsilon^2 g_2 g'_2 + \epsilon^2 g'_4), \quad (244)$$

$$\alpha_f(\hat{r}) = -s + \epsilon^2 \hat{r} g'_2. \quad (245)$$

#### D. Self-Inductance and $\beta$ values

The conventionally defined normalized self-inductance, toroidal beta, poloidal beta, and normalized beta values of the plasma equilibrium can be written<sup>23</sup>

$$l_i = \frac{2 \int_0^1 \hat{r} f^2 \langle |\nabla r|^2 \rangle d\hat{r}}{(f^2 \langle |\nabla r|^2 \rangle^2)_{\hat{r}=1}}, \quad (246)$$

$$\beta_t = \frac{2 \epsilon^2 \int_0^1 \hat{r} \langle R^2 \rangle p_2 d\hat{r}}{\int_0^1 \hat{r} (1 + 2 \epsilon^2 g_2) d\hat{r}}, \quad (247)$$

$$\beta_p = \frac{2 \epsilon^2 \int_0^1 \hat{r} \langle R^2 \rangle p_2 d\hat{r}}{\int_0^1 \hat{r} f^2 \langle |\nabla r|^2 \rangle d\hat{r}}, \quad (248)$$

$$\beta_N = \frac{20 \beta_t}{\epsilon (f \langle |\nabla r|^2 \rangle)_{\hat{r}=1}}, \quad (249)$$

respectively. Here,  $\langle \dots \rangle \equiv \oint (\dots) d\theta / 2\pi$ .

#### E. Coupling Coefficients

Let

$$S_1(\hat{r}) = \frac{1}{2} \sum_{j>0} \left[ 3 (H_j'^2 + V_j'^2) - (j^2 - 1) \frac{H_j^2 + V_j^2}{\hat{r}^2} \right], \quad (250)$$

$$\begin{aligned} S_2(\hat{r}) = & \sum_{j>1} 2 (j^2 - 1) \left( H_j'^2 + V_j'^2 - \frac{11}{3} \frac{H_j' H_j + V_j' V_j}{\hat{r}} + j^2 \frac{H_j^2 + V_j^2}{\hat{r}^2} \right) \\ & - \sum_{j>0} (1 - s) \left( \frac{H_j' H_j + V_j' V_j}{\hat{r}} + \frac{1}{3} \frac{H_j^2 + V_j^2}{\hat{r}^2} \right). \end{aligned} \quad (251)$$

The analysis of Sects. IV A, IV B, VII B, and VII C can be combined to give the following expressions for the coupling coefficients appearing in the outer-region o.d.e.s, (102) and (103):<sup>6</sup>

$$L_m^m(\hat{r}) = m^2 + \epsilon^2 m^2 \left( -\frac{3\hat{r}^2}{4} + H_1 + S_1 \right) + \epsilon^2 n^2 \hat{r}^2, \quad (252)$$

$$M_m^m(\hat{r}) = 0, \quad (253)$$

$$N_m^m(\hat{r}) = 0, \quad (254)$$

$$\begin{aligned} P_m^m(\hat{r}) = & (m - nq)^2 + \frac{m - nq}{m} q \hat{r} \frac{d}{d\hat{r}} \left( \frac{2-s}{q} \right) \\ & + \epsilon^2 (m - nq)^2 \left\{ \frac{7\hat{r}^2}{4} - H_1 - 3\hat{r} H_1' + S_1 \right. \\ & + \frac{1}{m^2} \left[ \frac{n}{m} \hat{r} \frac{d}{d\hat{r}} \left( \hat{r}^2 \frac{2-s}{q} \right) - \hat{r}^2 \frac{(2-s)^2}{q^2} - \hat{r} \frac{d}{d\hat{r}} (\hat{r} p_2') \right] \Big\} \\ & - \epsilon^2 \frac{m - nq}{m} \left\{ 2\hat{r} p_2' (2-s) + q \hat{r} \frac{d}{d\hat{r}} \left[ \hat{r}^2 \frac{2-s}{q^3} + \frac{s}{q} \left( \frac{3\hat{r}^2}{4} - H_1 - S_1 \right) \right. \right. \\ & \left. \left. - \frac{2}{q} \left( \frac{3\hat{r}^2}{2} - H_1 - \hat{r} H_1' - \frac{2}{3} S_1 \right) \right] - S_2 \right\} + \epsilon^2 2\hat{r} p_2' (1 - q^2), \end{aligned} \quad (255)$$

$$L_m^{m\pm 1}(\hat{r}) = -\epsilon m (m \pm 1) H_1', \quad (256)$$

$$L_m^{m\pm j}(\hat{r}) = -\epsilon m (m \pm j) (H_j' \pm i V_j') \quad \text{for } j > 1, \quad (257)$$

$$M_m^{m\pm 1}(\hat{r}) = \mp \epsilon m (m - nq) p_2' q^2 \pm \epsilon m (m \pm 1 - nq) [\hat{r} + (1-s) H_1'], \quad (258)$$

$$\begin{aligned} M_m^{m\pm j}(\hat{r}) = & \pm \epsilon \frac{m}{j} (m \pm j - nq) \left[ (1-s) (H_j' \pm i V_j') - (j^2 - 1) \frac{H_j \pm i V_j}{\hat{r}} \right] \\ & \text{for } j > 1, \end{aligned} \quad (259)$$

$$N_m^{m\pm 1}(\hat{r}) = \mp \epsilon (m \pm 1) (m \pm 1 - nq) p_2' q^2 \pm \epsilon (m \pm 1) (m - nq) [\hat{r} + (1-s) H_1'], \quad (260)$$

$$\begin{aligned} N_m^{m\pm j}(\hat{r}) = & \pm \epsilon \frac{(m \pm j)}{j} (m - nq) \left[ (1-s) (H_j' \pm i V_j') - (j^2 - 1) \frac{H_j \pm i V_j}{\hat{r}} \right] \\ & \text{for } j > 1, \end{aligned} \quad (261)$$

$$P_m^{m\pm 1}(\hat{r}) = -\epsilon (1+s) p_2' q^2 + \epsilon (m - nq) (m \pm 1 - nq) (\hat{r} - H_1'), \quad (262)$$

$$P_m^{m\pm j}(\hat{r}) = -\epsilon (m - nq) (m \pm j - nq) (H_j' \pm i V_j') \quad \text{for } j > 1. \quad (263)$$

When  $m = 0$ , some of the coupling coefficient take on special values:

$$P_0^0(\hat{r}) = n^2 q^2 - \frac{q^2}{\hat{r}} \frac{d}{d\hat{r}} \left( \hat{r}^2 \frac{2-s}{q^2} \right) - q^2 \hat{r} \frac{d}{d\hat{r}} \left( \frac{p_2'}{\hat{r}} \right), \quad (264)$$

$$M_{\pm 1}^0(\hat{r}) = \lim_{m \rightarrow 0} M_{m \pm 1}^m \mp \epsilon (2-s) H_1', \quad (265)$$

$$M_{\pm j}^0(\hat{r}) = \lim_{m \rightarrow 0} M_{m \pm j}^m \mp \epsilon (2-s) j (H_j' \mp i V_j') \quad \text{for } j > 1, \quad (266)$$

$$N_0^{\pm 1}(\hat{r}) = \lim_{m \rightarrow 0} N_m^{m \pm 1} \pm \epsilon (2-s) H_1', \quad (267)$$

$$N_0^{\pm j}(\hat{r}) = \lim_{m \rightarrow 0} N_m^{m \pm j} \pm \epsilon (2-s) j (H_j' \pm i V_j') \quad \text{for } j > 1, \quad (268)$$

$$P_{\pm 1}^0(\hat{r}) = \lim_{m \rightarrow 0} P_{m \pm 1}^m - \epsilon (2-s) \{ \pm n q^3 p_2' + (1 \mp n q) [\hat{r} + (1-s) H_1'] \} \quad (269)$$

$$P_{\pm j}^0(\hat{r}) = \lim_{m \rightarrow 0} P_{m \pm j}^m - \epsilon (2-s) \frac{(j \mp n q)}{j} \left[ (1-s) (H_j' \mp i V_j') - (j^2 - 1) \left( \frac{H_j \mp i V_j}{\hat{r}} \right) \right] \\ \text{for } j > 1, \quad (270)$$

$$P_0^{\pm 1}(\hat{r}) = \lim_{m \rightarrow 0} P_{m \pm 1}^m - \epsilon (2-s) \{ \pm n q^3 p_2' + (1 \mp n q) [\hat{r} + (1-s) H_1'] \}, \quad (271)$$

$$P_0^{\pm j}(\hat{r}) = \lim_{m \rightarrow 0} P_m^{m \pm j} - \epsilon (2-s) \frac{(j \mp n q)}{j} \left[ (1-s) (H_j' \pm i V_j') - (j^2 - 1) \left( \frac{H_j \pm i V_j}{\hat{r}} \right) \right] \\ \text{for } j > 1. \quad (272)$$

Here, the coupling coefficients are evaluated to  $\mathcal{O}(\epsilon)$ , while retaining  $\mathcal{O}(\epsilon^2)$  contributions to diagonal terms.<sup>4,6</sup> Note that the coupling coefficients exactly satisfy the symmetry requirements (110)–(113).

## F. Behavior Close to Magnetic Axis

In the limit  $\hat{r} \ll 1$ , a well-behaved solution of the outer-region o.d.e.s, (102) and (103), with a dominant poloidal mode number  $m > 0$  is such that<sup>6</sup>

$$Z_m(\hat{r}) \simeq \frac{m - n q}{m} \psi_m(\hat{r}), \quad (273)$$

$$\psi_{m+1}(\hat{r}) \simeq -\epsilon \frac{\hat{r} [(m - n q) - 2 p_2'' q^2]}{2 (m - n q)} \psi_m(\hat{r}), \quad (274)$$

$$\psi_{m+j}(\hat{r}) \simeq \epsilon \frac{2 \hat{r}^2 q'' (H_j' - i V_j')}{(m - n q) (m + 1) q} \psi_m(\hat{r}) \quad \text{for } j > 1 \quad (275)$$

to lowest order, with all of the other  $Z_m$  and  $\psi_m$  approximately zero. A well-behaved solution with a dominant poloidal mode number  $m < 0$  is such that

$$Z_m(\hat{r}) \simeq \frac{m - n q}{|m|} \psi_m(\hat{r}), \quad (276)$$

$$\psi_{m-1}(\hat{r}) \simeq -\epsilon \frac{\hat{r} [(m - n q) + 2 p_2'' q^2]}{2 (m - n q)} \psi_m(\hat{r}), \quad (277)$$

$$\psi_{m-j}(\hat{r}) \simeq -\epsilon \frac{2 \hat{r}^2 q'' (H_j' + i V_j')}{(m - n q) (|m| + 1) q} \psi_m(\hat{r}) \quad \text{for } j > 1 \quad (278)$$

to lowest order, with all of the other  $Z_m$  and  $\psi_m$  approximately zero. For the special case in which the dominant poloidal mode number is zero, the well-behaved solution is

$$Z_0(\hat{r}) \simeq \text{constant} \quad (279)$$

to lowest order, with all of the other  $Z_m$  and  $\psi_m$  approximately zero.

Note that the solutions (273)–(278) only exhibit “outward” coupling of different poloidal harmonics (i.e., coupling in the direction away from the  $m = 0$  harmonic). However, the solutions whose central poloidal mode numbers are  $m = \pm 1$  are special cases, and also exhibit inward coupling. Thus, in addition, to the couplings described in Eqs. (273)–(275), an  $m = 1$  solution drives the harmonics

$$\psi_{1-j}(\hat{r}) \simeq 2 \epsilon (H_j' - i V_j') \psi_1(\hat{r}) \quad \text{for } j > 1. \quad (280)$$

Likewise, in addition to the couplings described in Eqs. (276)–(278), an  $m = -1$  solution drives the harmonics

$$\psi_{-1+j}(\hat{r}) \simeq 2 \epsilon (H_j' + i V_j') \psi_{-1}(\hat{r}) \quad \text{for } j > 1. \quad (281)$$

## G. Plasma/Vacuum Interface

We require the equilibrium plasma current to be zero at the plasma/vacuum interface,  $\hat{r} = 1$ , which implies that  $g'(1) = P'(1) = 0$ . (See Sect. II B.) It follows from Eqs. (236)–(238) and (242) that we need<sup>6</sup>

$$p_2'(1) = 0, \quad (282)$$

$$\begin{aligned}
s(1) = 2 + \epsilon^2 & \left( \frac{3\hat{r}^2}{2} - 2\hat{r}H'_1 \right. \\
& + \sum_{j>0} \left[ H_j'^2 + 2(j^2 - 1) \frac{H'_j H_j}{\hat{r}} - (j^2 - 1) \frac{H_j^2}{\hat{r}^2} \right] \\
& \left. + \sum_{j>1} \left[ V_j'^2 + 2(j^2 - 1) \frac{V'_j V_j}{\hat{r}} - (j^2 - 1) \frac{V_j^2}{\hat{r}^2} \right] \right)_{\hat{r}=1} + \mathcal{O}(\epsilon^4). \quad (283)
\end{aligned}$$

## VIII. CALCULATION OF TEARING-MODE DISPERSION RELATION

### A. Introduction

Let the  $m_j$ , for  $j = 0, J$ , be the poloidal mode numbers included in the calculation. Here, it is assumed that  $m_{j+1} = m_j + 1$  for  $j = 0, J - 1$ . Let there be  $K$  rational surfaces in the plasma, and let the  $k$ th surface lie at radius  $\hat{r}_k$ , for  $k = 1, K$ . Here, it is assumed that  $\hat{r}_{k+1} > \hat{r}_k$  for  $k = 1, K - 1$ .

### B. Well-Behaved Solutions Launched from Magnetic Axis

Let us launch  $J+1$  linearly independent, well-behaved solutions of the outer-region o.d.e.s, (102) and (103), from the magnetic axis, as described in Sect. VII F. Let us then numerically integrate these solutions to the plasma/vacuum interface. The poloidal harmonics of the solutions are denoted  $\psi_{m_{j'}, m_j}^a(\hat{r})$  and  $Z_{m_{j'}, m_j}^a(\hat{r})$ , for  $j, j' = 0, J$ . Here,  $m_{j'}$  is the poloidal mode number of the harmonic, whereas  $m_j$  is the dominant poloidal mode number of the solution close to the magnetic axis. The asymptotic matching conditions imposed at the rational surfaces are

$$A_{Lk}^- = A_{Lk}^+, \quad (284)$$

$$\Delta\Psi_k = 0, \quad (285)$$

for  $k = 1, K$ . [Equations (174)–(181) specify how these matching conditions are implemented at a given rational surface.] Let  $\Pi_{kj}^a$ , for  $k = 1, K$  and  $j = 0, J$ , be the value of  $\Psi_k$  at the  $k$ th

rational surface associated with a solution launched from the magnetic axis with dominant poloidal mode number  $m_j$ .

A scheme similar to A.H. Glasser’s “fixups”<sup>12</sup> is employed to periodically re-orthogonalize the set of solutions. These re-orthogonalizations are implemented at user-defined locations between the magnetic axis and the plasma/vacuum interface. At each re-orthogonalization location, the matrix of solutions is forced to become upper triangular, via a process similar to Gaussian elimination, such that only one solution has a non-zero amount of the highest poloidal harmonic, two solutions have non-zero amounts of the next highest harmonic, and so on. The solutions are then renormalized to their largest component. The re-orthogonalizations are necessary to prevent the solutions from becoming colinear as a result of rounding errors, given the significantly different rates at which poloidal harmonics with different poloidal mode numbers grow with increasing  $\hat{r}$  close to the magnetic axis. (In fact, a harmonic with mode number  $m$  grows as  $\hat{r}^{|m|}$ . Hence, an  $m = 10$  harmonic grows far faster than an  $m = 1$  harmonic. Unchecked, each solution would quickly become dominated by its component with the largest mode number.)

### C. Small Solutions Launched from Rational Surfaces

Let us launch a “small” solution of the outer-region o.d.e.s from each rational surface in the plasma, as described in Sects. VB and VC, and numerically integrate it to the plasma/vacuum interface. The poloidal harmonics of the solutions are denoted  $\psi_{m_j k}^s(\hat{r})$  and  $Z_{m_j k}^s(\hat{r})$ , for  $j = 0, J$  and  $k = 1, K$ . Here,  $m_j$  is the poloidal mode number of the harmonic, whereas  $k$  is the index of the rational surface from which the solution is launched. The launch conditions are

$$A_{Lk}^- = A_{Lk}^+ = A_{Sk}^- = 0, \quad (286)$$

$$\Delta\Psi_k = 1. \quad (287)$$

[These launch conditions can be implemented at a given rational surface using Eqs. (182)–(185).] The asymptotic matching conditions imposed at the other rational surfaces are

$$A_{Lk'}^- = A_{Lk'}^+, \quad (288)$$

$$\Delta\Psi_{k'} = 0, \quad (289)$$

for  $k' = k + 1, K$ . [Equations (174)–(181) again specify how these matching conditions are implemented at a given rational surface.] Let  $\Pi_{k'k}^s$ , for  $k' = 1, K$  and  $k = 1, K$ , be the value of  $\Psi_{k'}$  at the  $k'$ th rational surface associated with a small solution launched from the  $k$ th rational surface. Note that  $\Pi_{k'k}^s = 0$  for  $k' \leq k$ .

#### D. Toroidal Tearing-Mode Dispersion Relation

The most general expression for the solution of the outer-region o.d.e.s at the plasma/vacuum interface is

$$\psi_{m_j}(1) = \sum_{j'=0,J} \psi_{m_j m_{j'}}^a(1) \alpha_{j'} + \sum_{k=1,K} \psi_{m_j k}^s(1) \Delta\Psi_k, \quad (290)$$

$$Z_{m_j}(1) = \sum_{j'=0,J} Z_{m_j m_{j'}}^a(1) \alpha_{j'} + \sum_{k=1,K} Z_{m_j k}^s(1) \Delta\Psi_k, \quad (291)$$

for  $j = 0, J$ , where the  $\alpha_j$  are complex coefficients. However, the solution must satisfy the boundary condition (205). It follows that

$$\sum_{j'=0,J} X_{jj'} \alpha_{j'} = \sum_{k=1,K} Y_{jk} \Delta\Psi_k \quad (292)$$

for  $j = 0, J$ , where

$$X_{jj'} = \frac{Z_{m_j m_{j'}}^a(1)}{m_j - n q(1)} - \sum_{j''=0,J} H_{m_j m_{j''}} \psi_{m_{j''} m_{j'}}^a(1), \quad (293)$$

$$Y_{jk} = \sum_{j'=0,J} H_{m_j m_{j'}} \psi_{m_{j'} k}^s(1) - \frac{Z_{m_j k}^s(1)}{m_j - n q(1)} \quad (294)$$

for  $j, j' = 0, J$  and  $k = 1, K$ . Thus, we can write

$$\alpha_j = \sum_{k=1,K} \Omega_{jk} \Delta\Psi_k \quad (295)$$

for  $j = 0, J$ , where

$$\sum_{j'=0,J} X_{jj'} \Omega_{j'k} = Y_{jk} \quad (296)$$



for  $j = 0, J$  and  $k = 1, K$ . Our general solution is now free of arbitrary coefficients. Finally, making use of the definitions of the  $\Pi_{kj}^a$  and the  $\Pi_{kk'}^s$  given in Sects. VIII B and VIII C, we obtain the *homogenous toroidal tearing-mode dispersion relation*,<sup>3-6</sup>

$$\Psi_k = \sum_{k'=1, K} F_{kk'} \Delta\Psi_{k'} \quad (297)$$

for  $k, k' = 1, K$ , where

$$F_{kk'} = \sum_{j=0, J} \Pi_{kj}^a \Omega_{jk'} + \Pi_{kk'}^s. \quad (298)$$

Equation (297) specifies the reconnected helical magnetic flux,  $\Psi_k$ , driven at each rational surface in the plasma as a consequence of the current sheets,  $\Delta\Psi_k$ , flowing at the surfaces. It is clear that  $F_{kk'}$  is a dimensionless inductance matrix.<sup>37</sup>

We can construct the “fully-reconnected” tearing eigenfunction<sup>6</sup> associated with the  $k$ th rational surface, which is defined to have the following properties,

$$\Psi_{k'} = F_{k'k}, \quad (299)$$

$$\Delta\Psi_{k'} = \delta_{k'k} \quad (300)$$

for  $k' = 1, K$ , as follows:

$$\psi_{m_j k}^f(\hat{r}) = \psi_{m_j k}^s(\hat{r}) + \sum_{j'=0, J} \psi_{m_j m_{j'}}^a(\hat{r}) \Omega_{j'k}, \quad (301)$$

$$Z_{m_j k}^f(\hat{r}) = Z_{m_j k}^s(\hat{r}) + \sum_{j'=0, J} Z_{m_j m_{j'}}^a(\hat{r}) \Omega_{j'k} \quad (302)$$

for  $j = 0, J$ . Here,  $\delta_{kk'}$  is a unit matrix. Note that the fully-reconnected solution associated with the  $k$ th rational surface only has a current sheet at that surface. (The current sheets at the other surfaces are all zero.)

The homogeneous toroidal tearing-mode dispersion relation can be written in the alternative form<sup>3,6</sup>

$$\Delta\Psi_k = \sum_{k'=1, K} E_{kk'} \Psi_{k'} \quad (303)$$

for  $k = 1, K$ , where  $E_{kk'}$  is the inverse of  $F_{kk'}$ . The previous equation specifies the current sheets driven at each rational surface in the plasma as a consequence of the reconnected fluxes at the surfaces.

We can construct the “unreconnected” tearing eigenfunction<sup>6</sup> associated with the  $k$ th rational surface, which is defined to have the following properties,

$$\Psi_{k'} = \delta_{k'k}, \quad (304)$$

$$\Delta \Psi_{k'} = E_{k'k} \quad (305)$$

for  $k' = 1, K$ , as follows:

$$\psi_{m_j k}^u(\hat{r}) = \sum_{k'=1, K} \psi_{m_j k'}^f(\hat{r}) E_{k'k}, \quad (306)$$

$$Z_{m_j k}^u(\hat{r}) = \sum_{k'=1, K} Z_{m_j k'}^f(\hat{r}) E_{k'k}, \quad (307)$$

for  $j = 0, J$ . Note that the unreconnected solution associated with the  $k$ th rational surface only has reconnected flux at that surface. (The reconnected fluxes at the other surfaces are all zero.)

Let

$$\Delta_k = \frac{\Delta \Psi_k}{\Psi_k} \quad (308)$$

be the complex quantity that characterizes the tearing response of the resonant layer at the  $k$ th rational surface to the ideal-MHD solution in the outer region.<sup>1</sup> In general,  $\Delta_k$  is a function of the growth-rate and phase-velocity of the reconnected helical magnetic flux at the surface.<sup>6,38,39</sup> The previous two equations can be combined to give the ultimate form of the tearing-mode dispersion relation,

$$\sum_{k'=1, k} (\Delta_k \delta_{kk'} - E_{kk'}) \Psi_{k'} = 0 \quad (309)$$

for  $k = 1, K$ . It is clear that  $E_{kk}$  is the tearing stability index<sup>1</sup> at the  $k$ th rational surface when magnetic reconnection takes place at this surface, but is suppressed at the other surfaces (as is likely to be the case in the presence of sheared plasma rotation<sup>6</sup>).

## E. Toroidal Electromagnetic Torques

According to Eqs. (189) and (303), the net toroidal electromagnetic torque exerted on an isolated plasma in the immediate vicinity of the  $k$ th rational surface is

$$\delta T_k = 2\pi^2 n \sum_{k'=1,K} \text{Im}(\Psi_k^* E_{kk'} \Psi_{k'}). \quad (310)$$

The total electromagnetic torque exerted on the plasma is

$$T_\phi(1) = \sum_{k=1,K} \delta T_k = 2\pi^2 n \sum_{k,k'=1,K} \text{Im}(\Psi_k^* E_{kk'} \Psi_{k'}). \quad (311)$$

However, we have already established that this total torque is zero, irrespective of the values of the  $\Psi_k$ . [See Eq. (208)]. Thus, it follows that

$$E_{kk'} = E_{k'k}^*. \quad (312)$$

In other words, as a consequence of the conservation of toroidal electromagnetic angular momentum, the matrix  $E_{kk'}$  must be Hermitian,<sup>6</sup> which implies that  $F_{kk'}$  is also Hermitian (as ought to be the case if  $F_{kk'}$  can be interpreted as a dimensionless inductance matrix).

## IX. RESONANT MAGNETIC PERTURBATION COILS

### A. Introduction

Suppose that the plasma is subject to a static, non-axisymmetric, resonant magnetic perturbation (RMP), with  $n$  periods in the toroidal direction, that is generated by currents flowing in magnetic field-coils external to the plasma. Let us, rather simplistically, model these RMP coils as a set of  $L$  toroidal strands of negligible cross-section in the  $R, Z$  plane. Suppose that the  $l$ th strand is located at  $R = R_l$ ,  $Z = Z_l$ , and carries a net current  $I_l \exp(-in\phi)$ . Here, the complex quantity  $I_l$  specifies the amplitude and phase of the non-axisymmetric current flowing in the strand.

## B. Externally Generated Perturbed Magnetic Field

Reusing the analysis of Sect. A of Ref. 40, the non-axisymmetric magnetic field generated by the currents flowing in the external magnetic field-coils can be written  $\mathbf{b}^x(R, \phi, Z) = \mathbf{b}^x(R, Z) \exp(-i n \phi)$ , where

$$\mathbf{b}^x(R, Z) = \nabla(R A_\phi) \times \nabla \phi, \quad (313)$$

$$A_\phi(R, Z) = \sum_{l=1, L} I_l \mathcal{G}(R, Z; R_l, Z_l), \quad (314)$$

$$G(R, Z; R', Z') = \frac{(-1)^{n+1} \sqrt{\pi} R R'}{4 \Gamma(n + 1/2)} \left[ \frac{\cosh \eta}{R^2 + R'^2 + (Z - Z')^2} \right]^{1/2} \times \left[ (n - 1/2) P_{-1/2}^{n-1}(\cosh \eta) + \frac{P_{-1/2}^{n+1}(\cosh \eta)}{n + 1/2} \right], \quad (315)$$

$$\tanh \eta = \frac{2 R R'}{R^2 + R'^2 + (Z - Z')^2}. \quad (316)$$

Here, the  $P_{-1/2}^n(z)$  are toroidal functions.<sup>32</sup>

## C. Inhomogeneous Boundary Condition at Plasma/Vacuum Interface

According to Eqs. (2), (46), (78), (80), and (99)–(101), the magnetic perturbation at the plasma/vacuum interface generated by the currents flowing in the RMP coils is characterized by

$$\psi_m^x(\epsilon) = -i \oint_{r=\epsilon} \mathcal{J} \mathbf{b}^x \cdot \nabla r \exp(-i m \theta) \frac{d\theta}{2\pi}, \quad (317)$$

$$\frac{Z_m^x(\epsilon)}{m - n q(\epsilon)} = n^{-1} \oint_{r=\epsilon} R^2 \mathbf{b}^x \cdot \nabla \phi \exp(-i m \theta) \frac{d\theta}{2\pi}. \quad (318)$$

It follows from Eqs. (2) and (313) that

$$\psi_m^x(\epsilon) = m \oint_{r=\epsilon} R A_\phi \exp(-i m \theta) \frac{d\theta}{2\pi}, \quad (319)$$

$$\frac{Z_m^x(\epsilon)}{m - n q(\epsilon)} = 0, \quad (320)$$

where we have integrated by parts.

In the presence of the perturbed magnetic field generated by the RMP coils, the homogeneous boundary condition at the plasma/vacuum interface, (205), is modified to give the following inhomogeneous boundary condition:

$$\frac{Z_m(\epsilon)}{m - n q(\epsilon)} = \sum_{m'} H_{mm'} [\psi_{m'}(\epsilon) - \psi_{m'}^x(\epsilon)]. \quad (321)$$

#### D. Inhomogeneous Toroidal Tearing-Mode Dispersion Relation

The previous boundary condition can be combined with the analysis of Sect. VIID to produce the following inhomogeneous toroidal tearing-mode dispersion relation:<sup>15,40</sup>

$$\Delta\Psi_k = \sum_{k'=1,K} E_{kk'} \Psi_{k'} + \chi_k, \quad (322)$$

for  $k = 1, K$ , where

$$\chi_k = \sum_{k'=1,K} E_{kk'} \Lambda_{k'}, \quad (323)$$

$$\Lambda_k = \sum_{j=0,J} \Pi_{kj}^a \Upsilon_j, \quad (324)$$

$$\sum_{j'=0,J} X_{jj'} \Upsilon_{j'} = \Xi_j, \quad (325)$$

$$\Xi_j = \sum_{j'=0,J} H_{m_j m_{j'}} \psi_{m_{j'}}^x(\epsilon), \quad (326)$$

for  $k = 1, K$  and  $j = 0, J$ .

#### E. Toroidal Electromagnetic Torques

Making use of Eqs. (189), (308), and (322), the toroidal electromagnetic torque exerted by the RMP coils at the  $k$ th rational surface in the plasma is

$$\delta T_k = 2\pi^2 n \operatorname{Im}(\Delta_k) |\Psi_k|^2, \quad (327)$$

where

$$\sum_{k'=1,K} (\Delta_k \delta_{kk'} - E_{kk'}) \Psi_{k'} = \chi_k \quad (328)$$

for  $k = 1, K$ . In situations in which driven magnetic reconnection at the various rational surface in the plasma is strongly shielded by plasma rotation,<sup>15,26</sup> so that  $|\Delta_k| \gg |E_{kk'}|$ , for all  $k, k'$ , Eq. (327) simplifies to give

$$\delta T_k \simeq 2\pi^2 n \frac{\text{Im}(\Delta_k)}{|\Delta_k|^2} |\chi_k|^2. \quad (329)$$

## X. TJ CODE

### A. Introduction

The first computer code that was developed in order to calculate the tearing-mode stability of an aspect-ratio expanded tokamak plasma equilibrium was the T3 code (1998). The T3 code solves a set of coupled first-order o.d.e.s associated with the resonant poloidal harmonics at the various rational surfaces in the plasma, together with their upper and lower sidebands driven by toroidal coupling.<sup>4</sup> The T3 code was quickly followed by the T7 code (1993), which extends the calculation to describe the coupling of poloidal harmonics associated with the elliptic and triangular shaping of up-down-symmetric equilibrium magnetic flux-surfaces, necessitating seven coupled poloidal harmonics for each rational surface in the plasma.<sup>6</sup> Unfortunately, both the T3 and T7 codes were formulated incorrectly, causing them to only conserve toroidal electromagnetic angular momentum at unrealistically low values of the inverse aspect-ratio. The recently developed TJ code (2024), which is an implementation of the analysis of Sects. II–IX of this paper, calculates the tearing stability of an aspect-ratio expanded tokamak equilibrium with magnetic flux-surfaces of arbitrary shape. Moreover, the code has been formulated in such a fashion that it conserves toroidal electromagnetic angular momentum at realistic values of the inverse aspect-ratio. As will become clear in the following discussion, conservation of angular momentum is a vitally important property of a toroidal tearing-mode code.

## B. Example Plasma Equilibrium

Let us investigate the stability of an example tokamak equilibrium to  $n = 1$  tearing modes.

The example equilibrium is characterized by  $\epsilon = 0.2$ ,  $H_2(1) = 1.0$ ,  $V_2(1) = 0.2$ ,  $H_3(1) = 0.5$ ,  $V_3(1) = -0.375$ , and  $H_j(1) = V_j(1) = 0$  for all  $j > 3$ . (See Sect. VII A.) The equilibrium is calculated, according to the method set out in Ref. 35, using the following model pressure and lowest-order (i.e., cylindrical) safety-factor profiles:

$$p_2(\hat{r}) = 0.1 (1 - \hat{r})^3, \quad (330)$$

$$q_0(\hat{r}) = \frac{3.15}{1 - (1 - \hat{r}^2)^{3.5}}. \quad (331)$$

Figure 1 shows the  $p_2(\hat{r})$  profile, as well as the final safety-factor profile,  $q(\hat{r})$ . These two functions are used to calculate all of the aspect-ratio expanded quantities described in Sect. VII.

The  $\hat{r}$ - $\theta$  flux-coordinate system associated with the equilibrium is shown in Fig. 2. It can be seen that the plasma equilibrium is not up-down-symmetric, and also has a fairly realistic shape.

The locations of the four  $n = 1$  rational surfaces in the plasma, as well as the locations of the four toroidal strands that make up the RMP coil system, are shown in Fig. 2.

Finally, the normalized plasma inductance and  $\beta$  values for the example equilibrium are  $l_i = 1.55$ ,  $\beta_t = 1.97 \times 10^{-3}$ ,  $\beta_p = 0.415$ , and  $\beta_N = 0.713$ .

## C. Vacuum Response Matrix

As described in Sect. VI, the conservation of toroidal electromagnetic angular momentum requires the vacuum response matrix,  $H_{m_j m_{j'}} \equiv H_{jj'}$ , defined in Eq. (206), to be Hermitian. Here, the  $m_j$ , for  $j = 0, J$  are the poloidal harmonics included in the calculation. In the present case,  $J = 40$ , and the  $m_j$  range from  $-15$  to  $+25$ . (Hence, in accordance with the T3/T7 nomenclature, this particular instance of the TJ code could be referred to as the T40 code.) It should be noted that this number of included poloidal harmonics is found to be more than sufficient to obtain converged results for the example equilibrium under investigation.

Consider

$$A_{jj'} = \sum_{j''=0,J} \mathcal{P}_{j''j}^* \mathcal{R}_{j''j'}, \quad (332)$$

where  $\mathcal{P}_{jj'} \equiv \mathcal{P}_{m_j}^{m_{j'}}$  and  $\mathcal{R}_{jj'} \equiv \mathcal{R}_{m_j}^{m_{j'}}$  are defined in Sect. VID. It is clear from Eq. (206), as well as some standard matrix analysis, that if  $H_{jj'}$  is Hermitian then  $A_{jj'}$  must also be Hermitian. Figure 3 shows the elements of the  $A_{jj'}$  matrix, as well as its anti-Hermitian component,

$$\tilde{A}_{jj'} = \frac{1}{2} (A_{jj'} - A_{j'j}^*), \quad (333)$$

calculated for the example equilibrium. It can be seen that the elements of  $\tilde{A}_{jj'}$  are all considerably smaller than those of  $A_{jj'}$ , indicating that  $A_{jj'}$  is Hermitian to a very good approximation. Let

$$\hat{A}_{jj'} = \frac{1}{2} (A_{jj'} + A_{j'j}^*) \quad (334)$$

be the Hermitian component of  $A_{jj'}$ . We can ensure that  $H_{jj'}$  is exactly Hermitian by solving

$$\sum_{j''=0,J} \mathcal{P}_{j''j}^* \hat{\mathcal{R}}_{j''j'} = \hat{A}_{jj'}, \quad (335)$$

$$\sum_{j''=0,J} \hat{\mathcal{R}}_{j''j}^* H_{j''j'} = \mathcal{P}_{j'j}^* \quad (336)$$

to obtain first  $\hat{\mathcal{R}}_{jj'}$  and then  $H_{jj'}$ . Here, use has been made of Eq. (206). The elements of the resulting, exactly Hermitian, vacuum response matrix,  $H_{jj'}$ , are shown in Fig. 4.

#### D. Solution of Outer-Region O.D.E.s

As described in Sect. VII F, the tearing-mode eigenfunctions are constructed by launching a set of  $J + 1$  linearly independent, well-behaved solutions of the outer-region o.d.e.s from the magnetic axis, and then integrating them to the plasma boundary. At each rational surface in the plasma, the solutions satisfy jump conditions that ensure that the coefficients of the large and the small solutions are continuous across the surface. Now, each one of these solutions must conserve the toroidal electromagnetic angular momentum flux,  $T_\phi(r)$ , that is defined in Eq. (117). This follows because  $T_\phi(r)$  is exactly conserved by the outer-region o.d.e.s, (102) and (103), provided that the coupling coefficients appearing in these



equations satisfy the symmetry constraints (110)–(113) (which they do—see Sect. VII E). Moreover, this conservation property holds irrespective of how many poloidal harmonics are included in the calculation. The jump conditions ensure continuity of  $T_\phi(\hat{r})$  across the rational surfaces. However, the launch conditions at the magnetic axis imply that  $T_\phi(0) = 0$ . (See Sect. VII F.) Thus, we conclude that every independent solution of the outer-region o.d.e.s, launched from the magnetic axis, and integrated to the plasma boundary, should be characterized by  $T_\phi(\hat{r}) = 0$  throughout the plasma. Obviously, this is a very stringent and powerful test that the integration of the outer-region o.d.e.s is accurate, and also that the jump conditions imposed at the rational surfaces have been correctly formulated.

Figure 5 shows a well-behaved solution of the outer-region o.d.e.s, launched from the magnetic axis, and integrated to the plasma boundary. This particular solution is dominated by the  $m = 1$  harmonic close to the axis. It can be seen that  $T_\phi(\hat{r})$  is constant between rational surfaces. This demonstrates that the Cash-Karp embedded RK4/RK5 adaptive-step integration scheme<sup>41</sup> used to solve the outer-region o.d.e.s does so in an accurate manner. It can also be seen that there are small jumps in  $T_\phi(\hat{r})$  across the rational surfaces. This occurs because the jump conditions specified in Sect. V are based on an expansion in  $\delta$  (the closest distance that the outer-region solution approaches the rational surface) and are, therefore, only approximate. However, the spurious jumps in  $T_\phi(\hat{r})$  across the rational surfaces are relatively insignificant (a jump of unity would be significant). Moreover, these jumps can be made arbitrarily small by decreasing  $\delta$  (in the present case  $\delta = 10^{-9}$ ) because the accuracy of the expansion becomes greater as  $\delta$  decreases. Of course, decreasing  $\delta$  causes the adaptive integration routine to spend more time in the vicinity of the rational surfaces (recall that the outer-region o.d.e.s are singular at the rational surfaces), so a compromise has to be made. Under normal circumstances, the choice  $10^{-8} \leq \delta \leq 10^{-9}$  ensures accurate conservation of angular momentum without unduly slowing down the calculation. (Note that the major results of the code exhibit no dependence on  $\delta$  when it is this small.)

The construction of the tearing-mode eigenfunctions also requires a set of “small” solutions of the outer-region o.d.e.s, launched from each rational surface in the plasma, and integrated to the plasma boundary. (See Sect. VIII C.) The launch conditions ensure that the flux of toroidal angular momentum from the rational surface is zero. At each subsequent rational

surface in the plasma that the solutions are integrated over, the solutions satisfy jump conditions that ensure that the coefficients of the large and the small solutions are continuous across the surface. Thus, by analogy with the previous discussion, each small solution launched from a rational surface should be characterized by  $T_\phi(\hat{r}) = 0$  throughout the plasma. Again, this is a very stringent test of both the integration algorithm and the jump conditions.

Figure 6 shows a small solution launched from the  $q = 2$  surface. It can be seen that  $T_\phi(\hat{r})$  is very small throughout the plasma, indicating that integration algorithm and jump conditions are working properly.

### E. Tearing Eigenfunctions

As described in Sect. VIID, an “unreconnected” tearing eigenfunction is constructed from a linear combination of the well-behaved solutions of the outer-region o.d.e.s launched from the magnetic axis, and small solutions launched from the rational surfaces. The mix of the various solutions that make up the combination is influenced by the vacuum response matrix. There is an independent unreconnected tearing eigenfunction for each rational surface in the plasma.

Figures 8 and 9 show the unreconnected tearing eigenfunctions associated with the  $q = 1$  and the  $q = 2$  rational surfaces. Both of these solutions should be associated with zero toroidal electromagnetic angular momentum flux throughout the plasma. It can be seen that this is the case, to a very good approximation. Figure 9 shows the toroidal electromagnetic angular momentum flux,  $T_\phi(\hat{r})$ , associated with a general complex linear combination of the unreconnected eigenfunctions pictured in Figs. 8 and 9. This figure exhibits three key features:

1.  $T_\phi(\hat{r})$  is constant between rational surfaces: this must be the case because the outer-region o.d.e.s exactly conserve  $T_\phi$ .
2.  $T_\phi(\hat{r})$  is zero inside the innermost rational surface: this must be the case otherwise a net electromagnetic torque would be exerted at the magnetic axis, which is unphysical.

3.  $T_\phi(\hat{r})$  is zero outside the outermost rational surface: this must be the case otherwise there would be a flux of toroidal electromagnetic angular momentum across the plasma boundary, implying that the plasma exerts a net toroidal electromagnetic torque on itself, which is unphysical.

The fact that  $T_\phi(\hat{r})$  is non-zero and constant between the  $q = 1$  and  $q = 2$  surfaces implies that these surfaces (or, to be more exact, the non-ideal plasmas in the inner regions centered on these surfaces) exert equal and opposite toroidal electromagnetic torques on one another. Note that the toroidal angular momentum flux calculated from every possible pair of tearing eigenfunctions must satisfy the previous three criteria. This constitutes an important self-consistency check on the calculation. Incidentally, the T3 and T7 codes fail this test badly, except at very small values of the inverse aspect-ratio (i.e.,  $\epsilon \lesssim 0.01$ ).

### F. Toroidal Tearing-Mode Stability Matrix

As described in Sect. VIID, the general homogeneous toroidal tearing-mode dispersion relation can be written

$$\sum_{k'=1,4} (\Delta_k \delta_{kk'} - E_{kk'}) \Psi_{k'} = 0 \quad (337)$$

for  $k = 1, 4$ . Here,  $k$  indexes the four  $n = 1$  rational surfaces in the plasma: namely, the  $m = 1/n = 1$ ,  $m = 2/n = 1$ ,  $m = 3/n = 1$ , and  $m = 4/n = 1$  surfaces. Moreover,  $\Delta_k$  is the complex inner-region layer response index at the  $k$ th rational surface,<sup>6</sup> whereas  $\Psi_k$  is the reconnected helical magnetic flux at the surface. Finally,  $E_{kk'}$  is the toroidal tearing-mode stability matrix.<sup>3,6</sup> As discussed in Sect. VIIE, the  $E_{kk'}$  matrix must be Hermitian, otherwise an isolated tokamak plasma would be able to exert a net toroidal electromagnetic torque on itself, which is unphysical.

Table I shows the toroidal tearing mode matrix calculated for the example equilibrium. It can be seen that the matrix is Hermitian to a very high degree of accuracy. This constitutes yet another important internal check on the accuracy of the calculation.

Now, the  $\Delta_k$  indices are functions of the angular phase-velocity,  $\omega$ , of the tearing mode.<sup>6,26</sup> Tokamak plasmas generally contain sufficient levels of sheared plasma rotation to ensure

that if  $\omega$  is chosen in such a manner as to make  $\Delta_k \sim \mathcal{O}(1)$  at the  $k$ th rational surface then  $|\Delta|_{k' \neq k} \gg 1$  at the other rational surfaces.<sup>6,37</sup> Under these circumstances the dispersion relation (337) yields

$$\frac{\Psi_{k'}}{\Psi_k} \simeq \frac{E_{k'k}}{\Delta_{k'}} \ll 1 \quad (338)$$

for  $k' \neq k$ , and

$$\Delta_k \simeq E_{kk}. \quad (339)$$

In other words, we obtain a tearing mode that only reconnects significant amounts of magnetic flux at the  $k$ th rational surface, and satisfies the quasi-cylindrical dispersion relation (339).<sup>1</sup> This dispersion relation ensures that  $\omega$  is determined by the plasma flow at the  $k$ th rational surface.<sup>6</sup> It follows that the real quantity  $E_{kk}$  can be interpreted as the effective “tearing stability index” for a mode that only reconnects magnetic flux at the  $k$ th rational surface. To be more exact,  $E_{kk}$  is a measure of the amount of free energy available in the outer region, due to current gradients and pressure gradients,<sup>42</sup> to drive magnetic reconnection at the  $k$ th rational surface.

In accordance with the previous discussion, the fact that  $E_{11} > 0$ ,  $E_{22} > 0$ ,  $E_{33} < 0$ , and  $E_{44} < 0$  in Tab. I suggests that the plasma is subject to four essentially uncoupled  $n = 1$  tearing modes. There is an intrinsically unstable (i.e., possessing positive free-energy from the outer region)  $m = 1/n = 1$  mode that only reconnects magnetic flux at the  $q = 1$  surface,<sup>1</sup> an intrinsically unstable  $m = 2/n = 1$  mode that only reconnects magnetic flux at the  $q = 2$  surface, as well as intrinsically stable  $m = 3/n = 1$  and  $m = 4/n = 1$  modes. It is interesting to note that the inevitable presence of sheared plasma rotation in tokamak plasmas allows the  $n = 1$  tearing stability of a general equilibrium to be described by a small number of real stability indices: namely, the diagonal elements of the  $E_{kk'}$  matrix.<sup>6</sup> In fact, there are only as many indices as there are  $n = 1$  rational surfaces in the plasma. Of course, this constitutes a tremendous simplification over the general case.

## G. Response to RMP

As described in Sect. IX E, if the plasma is subject to an  $n = 1$  RMP generated by non-axisymmetric currents flowing in external magnetic field-coils then, in the presence of sheared plasma rotation, the reconnected magnetic flux driven by the RMP at the  $k$ th  $n = 1$  rational surface is given by

$$\Psi_k \simeq \frac{\chi_k}{\Delta_k}, \quad (340)$$

whereas the toroidal electromagnetic locking torque exerted by the RMP at the surface is written

$$\delta T_k \simeq 2\pi^2 n \frac{\text{Im}(\Delta_k)}{|\Delta_k|^2} |\chi_k|^2. \quad (341)$$

Now, in general,  $\chi_k$  is proportional to the current,  $I_{\text{rmp}}$ , circulating around the RMP coils. Thus, we can write

$$\chi_k = I_{\text{rmp}} \hat{\chi}_k, \quad (342)$$

where  $\hat{\chi}_k$  is calculated on the assumption that unit current circulates around the RMP coils.

Table II shows the  $|\hat{\chi}_k|$  parameters calculated for the example plasma equilibrium and  $n = 1$  RMP coil set pictured in Figs. 1 and 2. It is interesting to note that, despite the complexity of the RMP (which requires a great number of poloidal harmonics to fully describe it), and despite the complexity of the plasma response to the RMP (which is a linear combination of 45 independent solutions of the outer region o.d.e.s, each possessing 41 poloidal harmonics), the ability of the  $n = 1$  RMP to either drive magnetic reconnection or exert electromagnetic locking torques at the four  $n = 1$  rational surfaces in the plasma is encapsulated by just four complex numbers,  $\hat{\chi}_k$ . Again, this constitutes a tremendous simplification.

## XI. SUMMARY

In Sects. II–IX, the tearing-mode stability of an inverse aspect-ratio expanded tokamak plasma equilibrium with magnetic flux-surfaces of general shape is investigated using asymptotic matching techniques. The crucial role played by the conservation of toroidal electromagnetic angular momentum is emphasized throughout the investigation. Note that the

inverse aspect-ratio expansion is only introduced in Sect. VII. So, all of the analysis prior to this section is completely general.

The TJ code, which is a specific implementation of the analysis of Sects. II–IX, is described in Sect. X. This code, which is freely available at <https://github.com/rfitzp/TJ>, represents a significant improvement on the previous T3<sup>4</sup> and T7<sup>6</sup> inverse aspect-ratio expanded toroidal tearing-mode codes, because it is constructed in such a manner as to strictly conserve toroidal electromagnetic angular momentum. In fact, as described in Sect. X, the requirement of angular momentum conservation leads to a large number of stringent self-consistency checks that the TJ code must pass in order for its results to be credible. Fortunately, the TJ code passes all of these checks for the example calculation presented in this paper. Unlike the T3 and T7 codes, the TJ code can deal with equilibrium magnetic flux-surfaces of arbitrary shape, and, in particular, is not restricted to up-down-symmetric plasma equilibria. Furthermore, unlike the much more general PEST-3,<sup>7</sup> RDCON,<sup>18</sup> and STRIDE<sup>17</sup> toroidal tearing-mode codes, the TJ code is comparatively lightweight (there are only about 7000 lines of code), and can easily be run on a laptop computer. Thus, the TJ code is ideal for optimization studies.

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## DATA AVAILABILITY STATEMENT

The digital data used in the figures in this paper can be obtained from the author upon reasonable request.

## Appendix A: Nonorthogonal Curvilinear Coordinates

Consider the nonorthogonal curvilinear coordinate system,  $r, \theta, \phi$ , introduced in Sect. II A, and let  $\mathcal{J} = (\nabla r \times \nabla \theta \cdot \nabla \phi)^{-1}$ .

Let

$$\mathbf{A} = A^r \mathcal{J} \nabla \theta \times \nabla \phi + A^\theta \mathcal{J} \nabla \phi \times \nabla r + A^\phi \mathcal{J} \nabla r \times \nabla \theta, \quad (\text{A1})$$

$$\mathbf{A} = A_r \nabla r + A_\theta \nabla \theta + A_\phi \nabla \phi, \quad (\text{A2})$$

where  $\mathbf{A}$  is a general vector. It is easily demonstrated that

$$\mathbf{A} \cdot \mathbf{B} = A_r B^r + A_\theta B^\theta + A_\phi B^\phi = A^r B_r + A^\theta B_\theta + A^\phi B_\phi, \quad (\text{A3})$$

$$(\mathbf{A} \times \mathbf{B})_r = \mathcal{J} (A^\theta B^\phi - A^\phi B^\theta), \quad (\text{A4})$$

$$(\mathbf{A} \times \mathbf{B})_\theta = \mathcal{J} (A^\phi B^r - A^r B^\phi), \quad (\text{A5})$$

$$(\mathbf{A} \times \mathbf{B})_\phi = \mathcal{J} (A^r B^\theta - A^\theta B^r), \quad (\text{A6})$$

$$\mathcal{J} (\mathbf{A} \times \mathbf{B})^r = A_\theta B_\phi - A_\phi B_\theta, \quad (\text{A7})$$

$$\mathcal{J} (\mathbf{A} \times \mathbf{B})^\theta = A_\phi B_r - A_r B_\phi, \quad (\text{A8})$$

$$\mathcal{J} (\mathbf{A} \times \mathbf{B})^\phi = A_r B_\theta - A_\theta B_r, \quad (\text{A9})$$

where  $\mathbf{B}$  is another general vector. Furthermore,

$$\mathcal{J} \nabla \cdot \mathbf{C} = \frac{\partial (\mathcal{J} C^r)}{\partial r} + \frac{\partial (\mathcal{J} C^\theta)}{\partial \theta} + \frac{\partial (\mathcal{J} C^\phi)}{\partial \phi}, \quad (\text{A10})$$

$$\mathcal{J} (\nabla \times \mathbf{C})^r = \frac{\partial C_\phi}{\partial \theta} - \frac{\partial C_\theta}{\partial \phi}, \quad (\text{A11})$$

$$\mathcal{J} (\nabla \times \mathbf{C})^\theta = \frac{\partial C_r}{\partial \phi} - \frac{\partial C_\phi}{\partial r}, \quad (\text{A12})$$

$$\mathcal{J} (\nabla \times \mathbf{C})^\phi = \frac{\partial C_\theta}{\partial r} - \frac{\partial C_r}{\partial \theta}, \quad (\text{A13})$$

where  $\mathbf{C}(\mathbf{r})$  is a general vector field.

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$\text{Re}(E_{kk'}):$			
$+1.334 \times 10^1$	$-2.282 \times 10^0$	$+8.248 \times 10^{-1}$	$-3.997 \times 10^{-1}$
$-2.282 \times 10^0$	$+3.731 \times 10^0$	$-2.195 \times 10^0$	$+2.821 \times 10^0$
$+8.247 \times 10^{-1}$	$-2.195 \times 10^0$	$-4.319 \times 10^0$	$-2.370 \times 10^0$
$-3.996 \times 10^{-1}$	$+2.821 \times 10^0$	$-2.370 \times 10^0$	$-1.286 \times 10^0$
$\text{Im}(E_{kk'}):$			
$-1.442 \times 10^{-6}$	$+4.470 \times 10^{-2}$	$+3.801 \times 10^{-2}$	$-9.714 \times 10^{-2}$
$-4.470 \times 10^{-2}$	$+4.900 \times 10^{-8}$	$+9.925 \times 10^{-2}$	$+2.826 \times 10^{-1}$
$-3.801 \times 10^{-2}$	$-9.925 \times 10^{-2}$	$-1.607 \times 10^{-8}$	$+2.811 \times 10^{-1}$
$+9.713 \times 10^{-2}$	$-2.826 \times 10^{-1}$	$-2.811 \times 10^{-1}$	$-1.146 \times 10^{-8}$

TABLE I.  $n = 1$  toroidal tearing-mode stability matrix for the example tokamak equilibrium specified in Figs. 1 and 2.

$ \hat{\chi}_k :$			
$9.008 \times 10^{-3}$	$1.294 \times 10^{-2}$	$1.262 \times 10^{-2}$	$1.176 \times 10^{-2}$

TABLE II. RMP drive parameters at the  $n = 1$  rational surfaces for the example tokamak equilibrium and  $n = 1$  RMP coil set specified in Figs. 1 and 2.

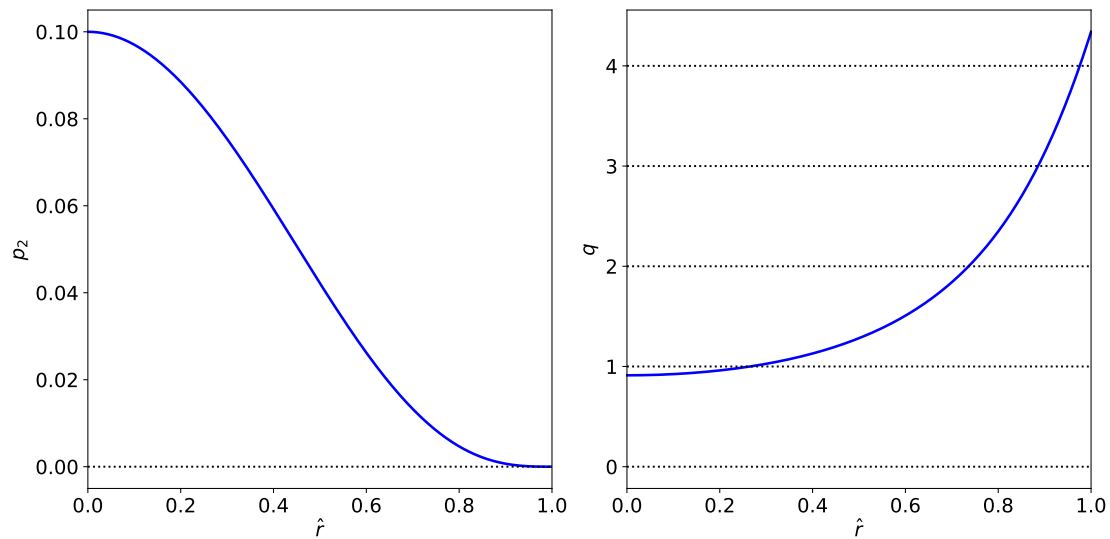


FIG. 1. Normalized pressure and safety-factor profiles for the example tokamak equilibrium.

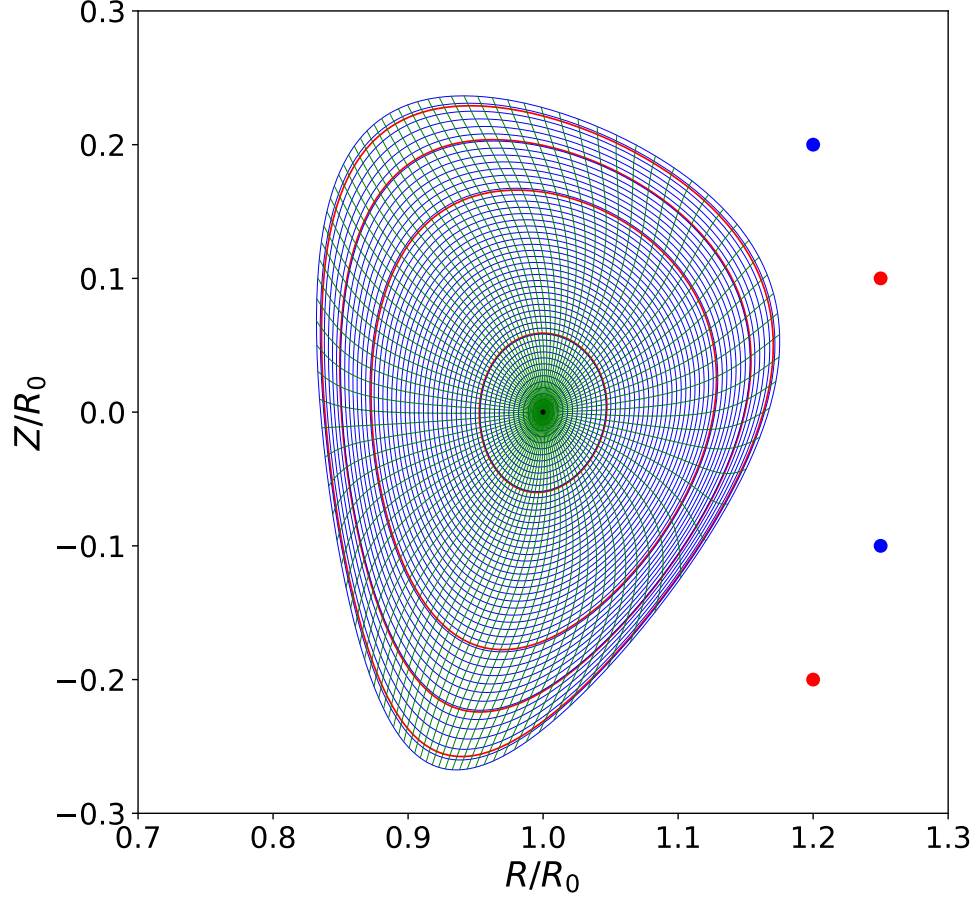


FIG. 2. Flux-coordinate system calculated for the example tokamak equilibrium. Surfaces of constant  $\hat{r}$  are shown as blue curves, whereas surfaces of constant  $\theta$  are shown as green curves. The red curves show the positions of the four  $n = 1$  rational magnetic flux-surfaces in the plasma. The black dot shows the location of the magnetic axis. The red and blue dots show the positions of the four toroidal strands that make up the RMP coil system. Blue indicates that the toroidal current flowing in the strand is positive, whereas red indicates that it is negative.

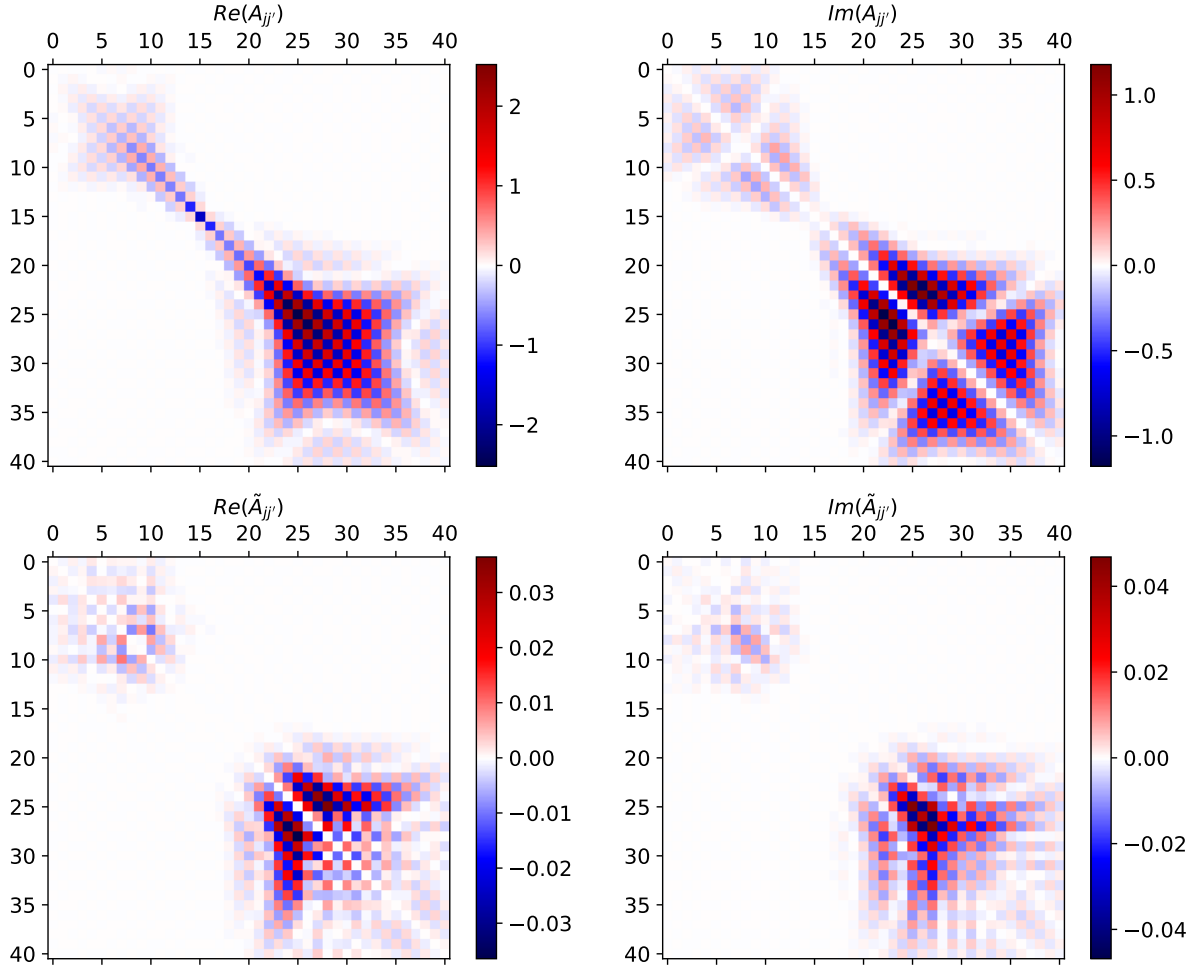


FIG. 3. Elements of the  $n = 1$  vacuum matrix  $A_{jj'}$ , as well as its anti-Hermitian component,  $\tilde{A}_{jj'}$ , calculated for the example tokamak equilibrium specified in the previous two figures.

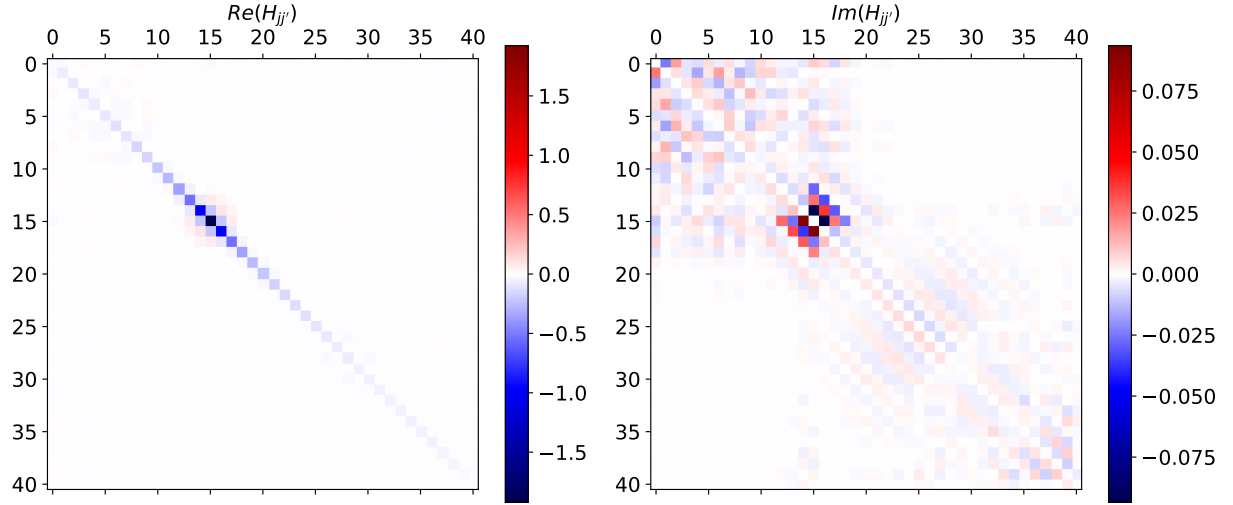


FIG. 4. Elements of the  $n = 1$  vacuum response matrix,  $H_{jj'}$ , calculated for the example tokamak equilibrium specified in Figs. 1 and 2.

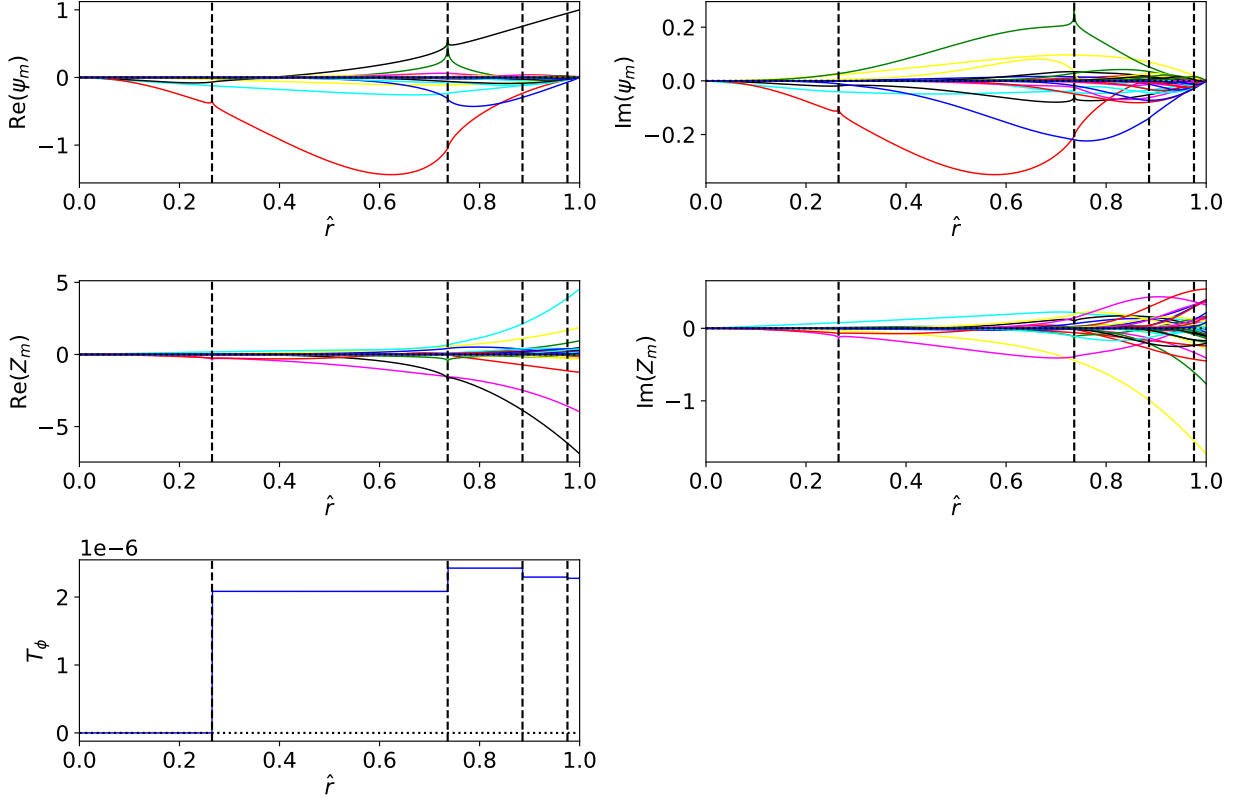


FIG. 5. Poloidal harmonics of a solution of the  $n = 1$  outer-region o.d.e.s, launched from the magnetic axis in such a manner that it is dominated by the  $m = 1$  harmonic close to the axis. Black curves correspond to  $m = 1$ , red to  $m = 0$  or  $m = 2$ , green to  $m = -1$  or  $m = 3$ , blue to  $m = -2$  or  $m = 4$ , yellow to  $m = -3$  or  $m = 5$ , cyan to  $m = -4$  or  $m = 6$ , magenta to  $m = -5$  or  $m = 7$ , black to  $m = -6$  or  $m = 8$ , et cetera. The vertical dashed lines show the locations of the  $n = 1$  rational surfaces. Here,  $T_\phi(\hat{r})$  is the toroidal electromagnetic angular momentum flux associated with the solution.



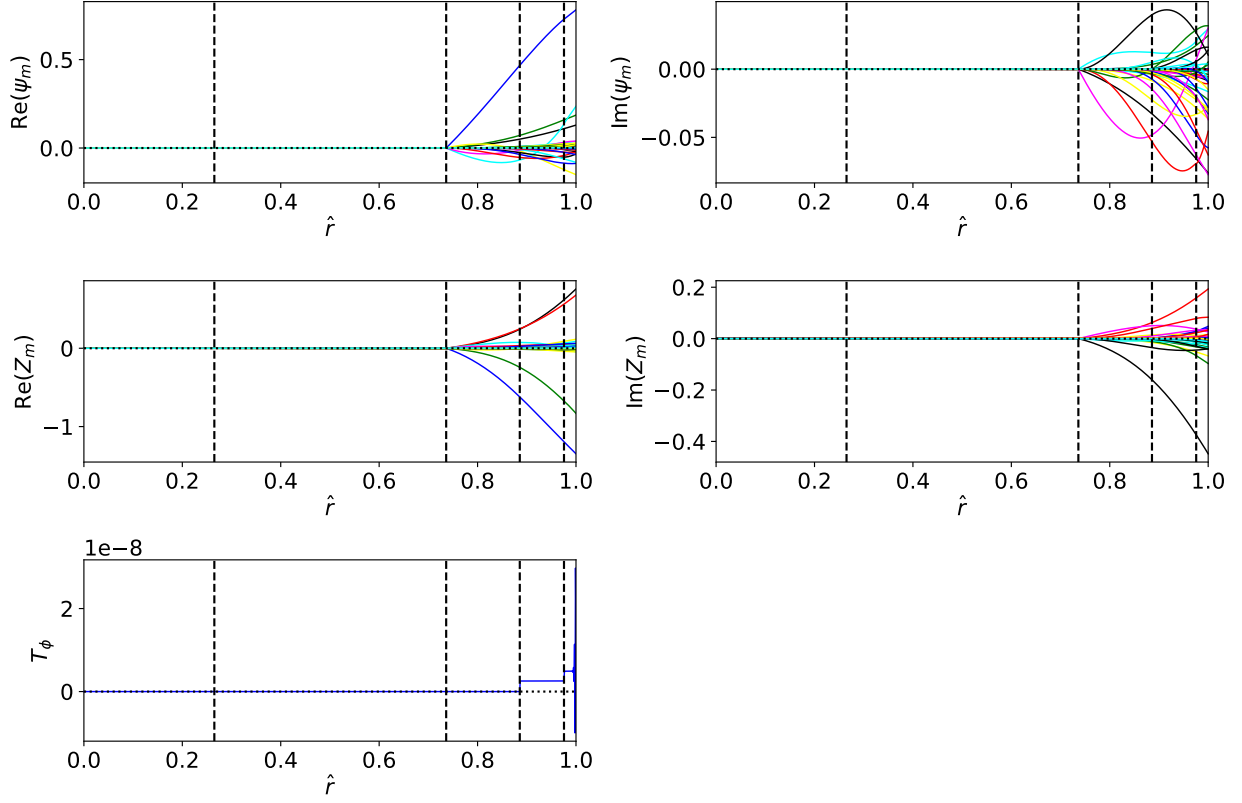


FIG. 6. Poloidal harmonics of a “small” solution of the  $n = 1$  outer-region o.d.e.s, launched from the  $q = 2$  surface. Black curves correspond to  $m = 2$ , red to  $m = 1$  or  $m = 3$ , green to  $m = 0$  or  $m = 4$ , blue to  $m = -1$  or  $m = 5$ , yellow to  $m = -2$  or  $m = 6$ , cyan to  $m = -3$  or  $m = 7$ , magenta to  $m = -4$  or  $m = 8$ , black to  $m = -5$  or  $m = 9$ , et cetera. The vertical dashed lines show the locations of the  $n = 1$  rational surfaces. Here,  $T_\phi(\hat{r})$  is the toroidal electromagnetic angular momentum flux associated with the solution.

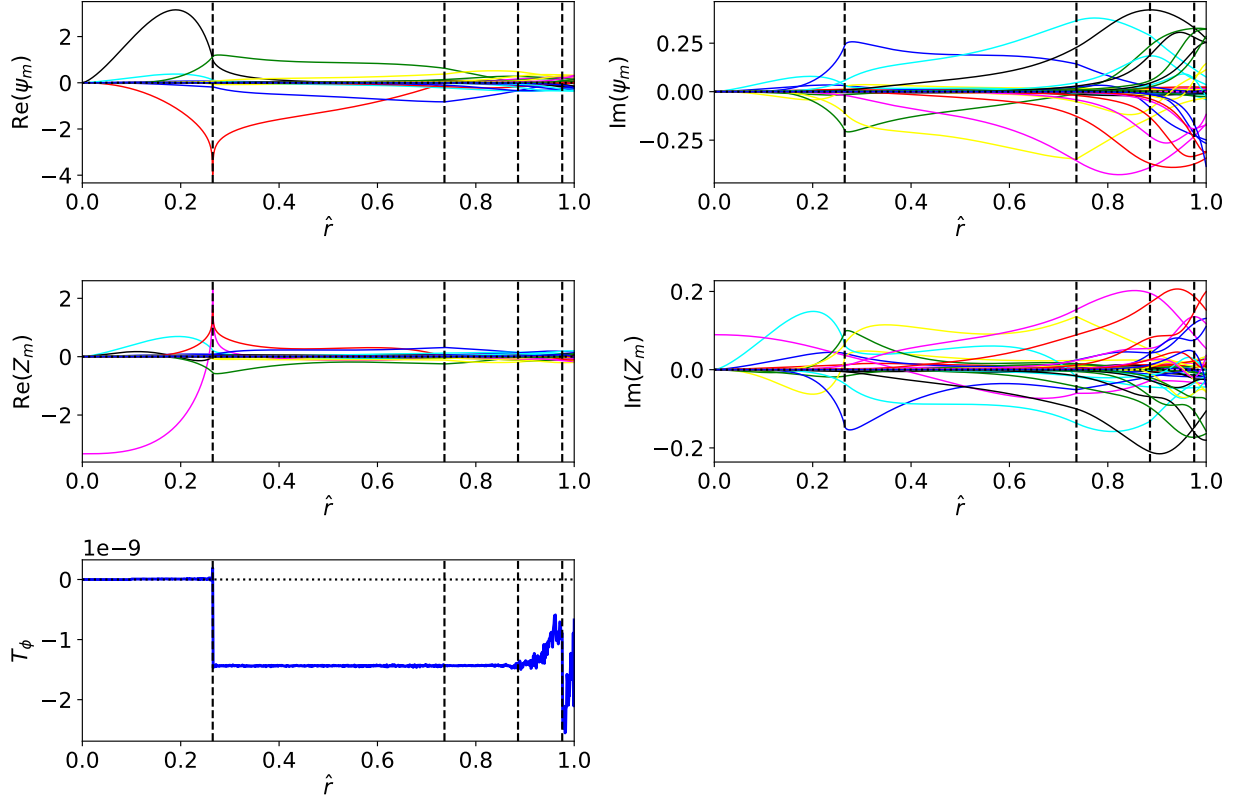


FIG. 7. Poloidal harmonics of the “unreconnected”  $n = 1$  tearing eigenfunction associated with the  $q = 1$  surface. Black curves correspond to  $m = 1$ , red to  $m = 0$  or  $m = 2$ , green to  $m = -1$  or  $m = 3$ , blue to  $m = -2$  or  $m = 4$ , yellow to  $m = -3$  or  $m = 5$ , cyan to  $m = -4$  or  $m = 6$ , magenta to  $m = -5$  or  $m = 7$ , black to  $m = -6$  or  $m = 8$ , et cetera. The vertical dashed lines show the locations of the  $n = 1$  rational surfaces. Here,  $T_\phi(\hat{r})$  is the toroidal electromagnetic angular momentum flux associated with the eigenfunction.

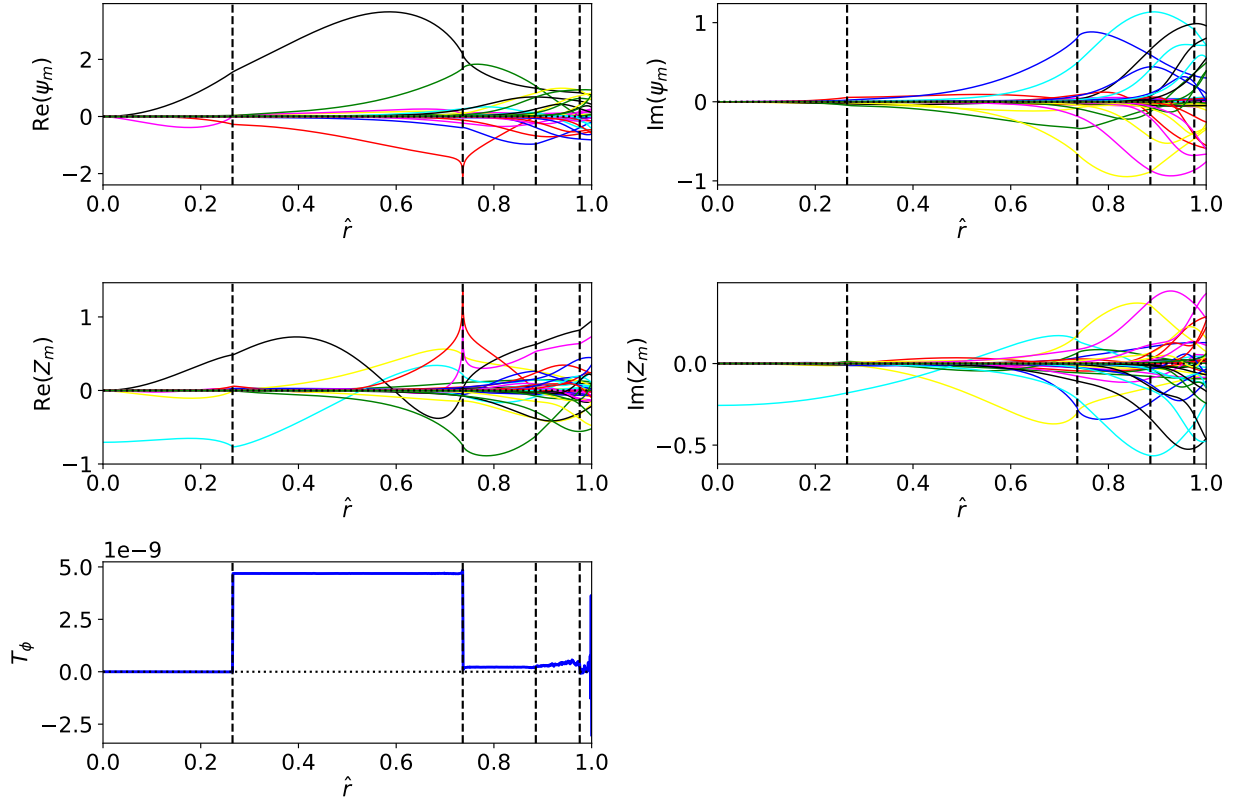


FIG. 8. Poloidal harmonics of the “unreconnected”  $n = 1$  tearing eigenfunction associated with the  $q = 2$  surface. Black curves correspond to  $m = 2$ , red to  $m = 1$  or  $m = 3$ , green to  $m = 0$  or  $m = 4$ , blue to  $m = -1$  or  $m = 5$ , yellow to  $m = -2$  or  $m = 6$ , cyan to  $m = -3$  or  $m = 7$ , magenta to  $m = -4$  or  $m = 8$ , black to  $m = -5$  or  $m = 9$ , et cetera. The vertical dashed lines show the locations of the  $n = 1$  rational surfaces. Here,  $T_\phi(\hat{r})$  is the toroidal electromagnetic angular momentum flux associated with the eigenfunction.

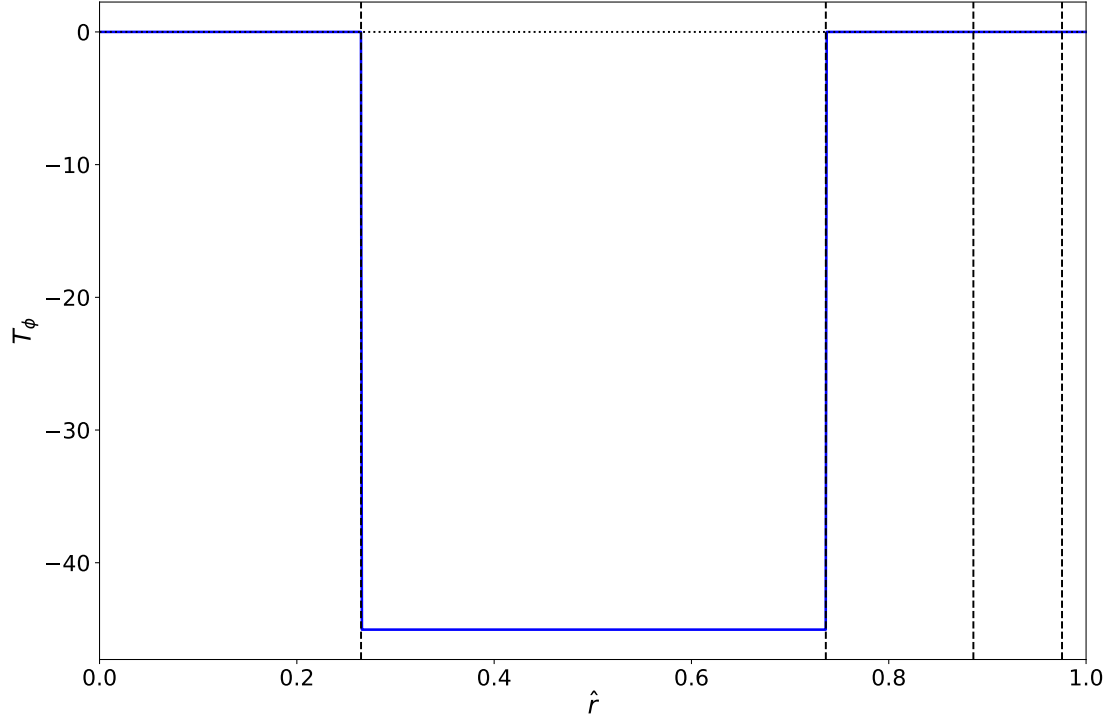


FIG. 9. Toroidal electromagnetic angular momentum flux associated with the tearing eigenfunction pictured in Fig. 7 added to  $i$  times the eigenfunction pictured in Fig. 8. The vertical dashed lines show the locations of the  $n = 1$  rational surfaces.