

# Separatrix

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## I. SAFETY-FACTOR

Let  $\hat{r} = r/a$ . Suppose that the last closed magnetic flux surface is at  $\hat{r} = 1$ . Suppose that the safety-factor profile takes the form

$$q(\hat{r}) = q_0 + (q_{95} - q_0) \frac{\ln(1 - \hat{r}^2)}{\ln(1 - \hat{r}_{95}^2)}. \quad (1)$$

## II. POLOIDAL MAGNETIC FLUX

Now,

$$\frac{d\Psi_p}{dr} = B_0 R_0 f = B_0 a \frac{\hat{r}}{q}, \quad (2)$$

assuming that  $g(\hat{r}) = 1$ . Let  $\psi_p = \Psi_p/(B_0 a^2)$ . It follows that

$$\frac{d\psi_p}{d\hat{r}} = \frac{\hat{r}}{q} = \frac{\hat{r}}{q_0 - \alpha \ln(1 - \hat{r}^2)}, \quad (3)$$

where

$$\alpha = -\frac{q_{95} - q_0}{\ln(1 - \hat{r}_{95}^2)}. \quad (4)$$

So,

$$\begin{aligned} \psi_p(\hat{r}) &= \int_0^{\hat{r}} \frac{d\hat{\psi}_p}{d\hat{r}} d\hat{r} = \frac{1}{2} \int_0^{\hat{r}^2} \frac{dx}{q_0 - \alpha \ln(1 - x)} = \frac{1}{2} \int_{1-\hat{r}^2}^1 \frac{dy}{q_0 - \alpha \ln y} \\ &= \frac{e^{q_0/\alpha}}{2\alpha} \int_{q_0/\alpha}^{q_0/\alpha - \ln(1 - \hat{r}^2)} \frac{e^{-z} dz}{z} = \frac{e^{q_0/\alpha}}{2\alpha} \left[ \int_{q_0/\alpha}^{\infty} \frac{e^{-z} dz}{z} - \int_{q_0/\alpha - \ln(1 - \hat{r}^2)}^{\infty} \frac{e^{-z} dz}{z} \right] \\ &= \frac{e^{q_0/\alpha}}{2\alpha} \left[ \int_1^{\infty} \frac{e^{-(q_0/\alpha)t} dt}{t} - \int_1^{\infty} \frac{e^{-[q_0/\alpha - \ln(1 - \hat{r}^2)]t} dt}{t} \right], \end{aligned} \quad (5)$$

giving

$$\psi_p(\hat{r}) = \frac{e^{q_0/\alpha}}{2\alpha} \{ E_1(q_0/\alpha) - E_1[q_0/\alpha - \ln(1 - \hat{r}^2)] \}. \quad (6)$$

Thus,

$$\psi_p(1) = \frac{e^{q_0/\alpha}}{2\alpha} E_1(q_0/\alpha). \quad (7)$$

Let  $\hat{\psi}_p(\hat{r}) = \psi_p(\hat{r})/\psi_p(1)$ . It follows that

$$\hat{\psi}_p(\hat{r}) = 1 - \frac{E_1[q_0/\alpha - \ln(1 - \hat{r}^2)]}{E_1(q_0/\alpha)}. \quad (8)$$

By definition,  $\hat{\psi}_p(\hat{r}_{95}) = 0.95$ , so

$$0.95 = 1 - \frac{E_1[q_0/\alpha - \ln(1 - \hat{r}_{95}^2)]}{E_1(q_0/\alpha)} = 1 - \frac{E_1(q_{95}/\alpha)}{E_1(q_0/\alpha)}, \quad (9)$$

giving

$$0.05 = \frac{E_1(q_{95}/\alpha)}{E_1(q_0/\alpha)}. \quad (10)$$

Assuming that  $q_0$  and  $q_{95}$  are specified, the previous equation can be solved to give  $\alpha$ , which then determines  $\hat{r}_{95}$ .

### III. RATIONAL SURFACES

Suppose that  $n$  is the toroidal mode number. The  $m, n$  rational surface lies at  $\hat{r} = \hat{r}_m$ , where  $q(\hat{r}_m) = q_m$  and  $q_m = m/n$ . Thus,

$$\hat{r}_m = \left[ 1 - \exp \left( \frac{q_0 - q_m}{\alpha} \right) \right]^{1/2}. \quad (11)$$

Hence, if  $\hat{\psi}_m = \hat{\psi}_p(\hat{r}_m)$  then

$$\hat{\psi}_m = 1 - \frac{E_1(q_m/\alpha)}{E_1(q_0/\alpha)}. \quad (12)$$

The spacing (in  $\hat{r}$ ) between successive rational surfaces is

$$\delta_m = \frac{d\hat{r}_m}{dm} = \frac{1 - \hat{r}_m^2}{2\hat{r}_m n \alpha}. \quad (13)$$

In the continuum limit, assuming that  $\hat{r}_m \simeq 1$ , we get

$$\hat{\delta}_{\text{rational}}(\hat{r}) \simeq \frac{1 - \hat{r}}{n \alpha} = \frac{x}{n \alpha}, \quad (14)$$

where  $x = 1 - \hat{r}$ .

## IV. MAGNETIC SHEAR

The magnetic shear is

$$s(\hat{r}) = \frac{\hat{r}}{q} \frac{dq}{d\hat{r}} = \frac{2\alpha \hat{r}^2}{(1 - \hat{r}^2)q} \simeq \frac{1}{f(x)}, \quad (15)$$

where

$$f(x) = -x \ln(2x). \quad (16)$$

## V. PROFILES

Let

$$n_e(\hat{\psi}_p) = 20 n_{e95} (1 - \hat{\psi}_p) + n_{e100}, \quad (17)$$

$$T_e(\hat{\psi}_p) = 20 T_{e95} (1 - \hat{\psi}_p) + T_{e100}, \quad (18)$$

$$T_i(\hat{\psi}_p) = 20 T_{i95} (1 - \hat{\psi}_p) + T_{i100}. \quad (19)$$

Thus,

$$\begin{aligned} \omega_{*e}(\hat{\psi}_p) &= \frac{T_e}{e} \left( \frac{d \ln n_e}{d \Psi_p} + \frac{d \ln T_e}{d \Psi_p} \right) = \frac{T_e}{e B_0 a^2 \psi_p(1)} \left( \frac{d \ln n_e}{d \hat{\psi}_p} + \frac{d \ln T_e}{d \hat{\psi}_p} \right) \\ &\simeq -\frac{20 T_{e100}}{e B_0 a^2 \psi_p(1)} \left( \frac{n_{e95}}{n_{e100}} + \frac{T_{e95}}{T_{e100}} \right), \end{aligned} \quad (20)$$

$$\begin{aligned} \omega_{*i}(\hat{\psi}_p) &= -\frac{T_i}{e} \left( \frac{d \ln n_e}{d \Psi_p} + \frac{d \ln T_i}{d \Psi_p} \right) = -\frac{T_i}{e B_0 a^2 \psi_p(1)} \left( \frac{d \ln n_e}{d \hat{\psi}_p} + \frac{d \ln T_i}{d \hat{\psi}_p} \right) \\ &\simeq -\frac{20 T_{i100}}{e B_0 a^2 \psi_p(1)} \left( \frac{n_{e95}}{n_{e100}} + \frac{T_{i95}}{T_{i100}} \right). \end{aligned} \quad (21)$$

## VI. LAYER QUANTITIES

Now,

$$\tau_{ee}(\hat{\psi}_p) = \frac{6\sqrt{2} \pi^{3/2} \epsilon_0^2 m_e^{1/2} T_e^{3/2}}{\ln \Lambda e^4 n_e} \simeq \frac{6\sqrt{2} \pi^{3/2} \epsilon_0^2 m_e^{1/2} T_{e100}^{3/2}}{\ln \Lambda e^4 n_{e100}}, \quad (22)$$

$$\sigma_{\parallel} = 1.96 \frac{n_e e^2 \tau_{ee}}{m_e}, \quad (23)$$

$$\tau_R = \mu_0 a^2 \sigma_{\parallel} \hat{r}^2 \simeq \mu_0 a^2 \sigma_{\parallel}, \quad (24)$$

$$\tau_H = \frac{R_0}{B_0} \frac{\sqrt{\mu_0 m_i n_e}}{n s} \simeq \tau_A f(x), \quad (25)$$

$$\tau_A = \frac{R_0}{B_0} \frac{\sqrt{\mu_0 m_i n_{e100}}}{n}, \quad (26)$$

$$\tau_{\perp} = \frac{a^2 \hat{r}^2}{D_{\perp}} \simeq \frac{a^2}{D_{\perp}}, \quad (27)$$

$$\tau_{\varphi} = \frac{a^2 \hat{r}^2}{\chi_{\varphi}} \simeq \frac{a^2}{\chi_{\varphi}}, \quad (28)$$

$$\tau = -\frac{\omega_{*e}}{\omega_{*i}}, \quad (29)$$

$$d_{\beta} = \frac{\sqrt{(5/3) m_i (T_e + T_i)}}{e B_0} \simeq \frac{\sqrt{(5/3) m_i (T_{e100} + T_{i100})}}{e B_0}, \quad (30)$$

$$S = \frac{\tau_R}{\tau_H} = \frac{\mathcal{S}}{f(x)}, \quad (31)$$

$$\mathcal{S} = \frac{\tau_R}{\tau_A}, \quad (32)$$

$$P_{\varphi} = \frac{\tau_R}{\tau_{\varphi}}, \quad (33)$$

$$P_{\perp} = \frac{\tau_R}{\tau_{\perp}}, \quad (34)$$

$$D = S^{1/3} \left( \frac{\tau}{1 + \tau} \right)^{1/2} \frac{d_{\beta}}{a \hat{r}} \simeq \mathcal{D} [f(x)]^{-1/3}, \quad (35)$$

$$\mathcal{D} = \mathcal{S}^{1/3} \left( \frac{\tau}{1 + \tau} \right)^{1/2} \frac{d_{\beta}}{a}, \quad (36)$$

$$Q_E = -S^{1/3} n \omega_E \tau_H \simeq \mathcal{Q}_E [f(x)]^{2/3}, \quad (37)$$

$$\mathcal{Q}_E = -\mathcal{S}^{1/3} n \omega_E \tau_A, \quad (38)$$

$$\mathcal{Q}_{e,i} = -S^{1/3} n \omega_{*e,i} \tau_H \simeq \mathcal{Q}_{*e,i} [f(x)]^{2/3}, \quad (39)$$

$$\mathcal{Q}_{e,i} = -\mathcal{S}^{1/3} n \omega_{*e,i} \tau_A, \quad (40)$$

$$Q = S^{1/3} \omega \tau_H = \mathcal{Q} [f(x)]^{2/3}, \quad (41)$$

$$\mathcal{Q} = \mathcal{S}^{1/3} \omega \tau_A. \quad (42)$$

## VII. LAYER EQUATION

The layer equation is written

$$\frac{d}{dp} \left[ A(p) \frac{dY_e}{dp} \right] - \frac{B(p)}{C(p)} p^2 Y_e = 0, \quad (43)$$

where

$$A = \frac{p^2}{-i(Q - Q_E - Q_e) + p^2}, \quad (44)$$

$$B = -i(Q - Q_E)(Q - Q_E - Q_i) - i(Q - Q_E - Q_i)(P_\varphi + P_\perp)p^2 + P_\varphi P_\perp p^4, \quad (45)$$

$$C = -i(Q - Q_E - Q_e) + [P_\perp - i(Q - Q_E - Q_i)D^2]p^2 + (1 + 1/\tau)P_\varphi D^2 p^4. \quad (46)$$

Let

$$p = f^{-1/9} \hat{p}. \quad (47)$$

It follows that

$$\frac{d}{d\hat{p}} \left[ \mathcal{A} \frac{dY_e}{d\hat{p}} \right] - \frac{\mathcal{B}}{\mathcal{C}} \hat{p}^2 Y_e = 0, \quad (48)$$

where

$$\mathcal{A} = \frac{\hat{p}^2}{-i(\mathcal{Q} - \mathcal{Q}_E - \mathcal{Q}_e)f^{8/9} + \hat{p}^2}, \quad (49)$$

$$\mathcal{B} = -i(\mathcal{Q} - \mathcal{Q}_E)(\mathcal{Q} - \mathcal{Q}_E - \mathcal{Q}_i)f^{16/9} - i(\mathcal{Q} - \mathcal{Q}_E - \mathcal{Q}_i)(P_\varphi + P_\perp)\hat{p}^2 f^{8/9} + P_\varphi P_\perp \hat{p}^4, \quad (50)$$

$$\mathcal{C} = -i(\mathcal{Q} - \mathcal{Q}_E - \mathcal{Q}_e)f^{12/9} + [P_\perp - i(\mathcal{Q} - \mathcal{Q}_E - \mathcal{Q}_i)D^2]\hat{p}^2 f^{8/9} + (1 + 1/\tau)P_\varphi D^2 \hat{p}^4. \quad (51)$$

Thus, Eq. (48) reduces to

$$\frac{d^2 Y_e}{d\hat{p}^2} - \frac{P_\perp}{(1 + 1/\tau)D^2} \hat{p}^2 Y_e \simeq 0. \quad (52)$$

The characteristic layer width in  $\hat{p}$  space is

$$\hat{p}_* = \left[ \frac{D^2 (1 + 1/\tau)}{P_\perp} \right]^{1/4}. \quad (53)$$

Thus, the characteristic layer width in  $\hat{r}$  space is

$$\hat{\delta}_{\text{layer}} = \frac{S^{-1/3}}{f^{-1/9} \hat{p}_*} = \mathcal{S}^{-1/3} \left[ \frac{P_\perp}{\mathcal{D}^2 (1 + 1/\tau)} \right]^{1/4} f^{-2/9} = \Delta_{\text{layer}} f^{-2/9}, \quad (54)$$

where

$$\Delta_{\text{layer}} = \left( \frac{\tau_A^{1/6} \tau_\perp^{1/4}}{\tau_R^{5/6}} \right) \hat{d}_\beta^{1/2}, \quad (55)$$

$$\hat{d}_\beta = \frac{\sqrt{(5/3) m_i (T_{e100} + T_{i100})}}{e B_0 a}. \quad (56)$$

## VIII. OVERLAP CRITERION

The resistive layer width exceeds the spacing between rational surfaces when

$$\hat{\delta}_{\text{layer}} > \hat{\delta}_{\text{rational}}, \quad (57)$$

or

$$x > x_c \quad (58)$$

where

$$x_c^{11/4} [-\ln(2 x_c)]^{2/9} = n \alpha \Delta_{\text{layer}}. \quad (59)$$