Universidade Federal de Alagoas - UFAL Centro de Tecnologia - CTEC Curso de Engenharia Civil

Mecânica dos Sólidos 3 - ECIV051D (2020.2)

Exercícios: Deslocamentos em vigas hiperestáticas usando a equação diferencial da elástica Encontro Assíncrono

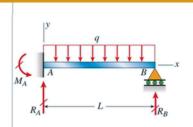
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Exemplo 10-1

Referência: Gere & Goodno (2013). Mechanics of Materials, 8th Edition. Cengage Learning.

• • Example 10-1



A propped cantilever beam AB of length L supports a uniform load of intensity q (Fig. 10-6). Analyze this beam by solving the second-order differential equation of the deflection curve (the bending-moment equation). Determine the reactions, shear forces, bending moments, slopes, and deflections of the beam.

restart:

Reações de apoio (em função de R_B)

$$assign\Big(solve\Big(\Big\{R_A+R_B-q\cdot L=0,M_A-(q\cdot L)\cdot \frac{L}{2}+R_B\cdot L=0\Big\},\,\big\{R_A,M_A\big\}\Big)\Big):R_A,M_A=q\;L-R_B,\,\frac{1}{2}\;q\;L^2-R_B\;L$$

Esforço cortante

$$V := unapply(solve(-V + R_A - q \cdot x = 0, V)) :$$

$$V(x) = q L - q x - R_B$$

Momento fletor

$$\begin{split} M &:= \mathit{unapply}\Big(\mathit{solve}\Big(M + M_A - R_A \cdot x + (q \cdot x) \cdot \frac{x}{2} = 0, M\Big), x\Big) : \\ M(x) &= -\frac{1}{2} \ q \ L^2 + R_B \ L + L \ q \ x - R_B x - \frac{1}{2} \ q \ x^2 \end{split}$$

Equação da curva de deflexão

$$\begin{array}{l} bc := v(0) = 0, \, \mathrm{D}[1](v)(0) = 0, \, v(L) = 0: \\ assign\bigg(dsolve\bigg(\bigg\{diff(v(x), x\$2) = \frac{M(x)}{EI}, \, bc\bigg\}, \, \big\{v(x), \, R_{B}\big\}\bigg)\bigg): \\ v := unapply(v(x), x): \end{array}$$

Respostas: reações, esforço cortante, momento fletor, deflexão e inclinação

$$R_{A}, R_{B}, M_{A} = \frac{5 q L}{8}, \frac{3 q L}{8}, \frac{q L^{2}}{8}$$

$$V(x), M(x) = \frac{5}{8} q L - q x, -\frac{1}{8} q L^{2} + \frac{5}{8} L q x - \frac{1}{2} q x^{2}$$

$$v(x), D[1](v)(x) = \frac{-\frac{3}{2} L^{2} q x^{2} + \frac{5}{2} L q x^{3} - q x^{4}}{24 EI}, \frac{-3 L^{2} q x + \frac{15}{2} L q x^{2} - 4 q x^{3}}{24 EI}$$

Exemplo 10-2

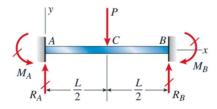
Referência: Gere & Goodno (2013). Mechanics of Materials, 8th Edition. Cengage Learning.

• • Example 10-2

The fixed-end beam ACB shown in Fig. 10-9 supports a concentrated load P at the midpoint. Analyze this beam by solving the fourth-order differential equation of the deflection curve (the load equation). Determine the reactions, shear forces, bending moments, slopes, and deflections of the beam.

Fig. 10-9

Example 10-2: Fixed-end beam with a concentrated load at the midpoint



restart:

Reações de apoio (em função de R_R e M_R)

$$assign\Big(solve\Big(\left\{R_A+R_B-P=0,M_A-M_B-P\cdot\frac{L}{2}\right. + R_B\cdot L=0\Big\}, \\ \left\{R_A,M_A=-R_B+P, \\ \frac{1}{2}\right. PL-R_BL+M_B$$

Esforço cortante

$$\begin{split} V_{AC} &:= solve(-V + R_A = 0, V) : \\ V_{CB} &:= solve(V + R_B = 0, V) : \\ V_{AC} &V_{CB} = -R_B + P, -R_B \end{split}$$

Momento fletor

$$\begin{split} &M_{AC} := unapply \big(solve \big(M + M_A - R_A \cdot x = 0, M \big), x \big) : \\ &M_{CB} := unapply \big(solve \big(-M - M_B + R_B \cdot (L - x) = 0, M \big), x \big) : \\ &M_{AC}(x), M_{CB}(x) = x P - x R_B - \frac{1}{2} PL + R_B L - M_B, R_B L - x R_B - M_B \big) \end{split}$$

Equação da curva de deflexão

$$\begin{split} &edo_{AC} := diff\left(v_{AC}(x), x\$2\right) = \frac{M_{AC}(x)}{EI}: \\ &edo_{CB} := diff\left(v_{CB}(x), x\$2\right) = \frac{M_{CB}(x)}{EI}: \\ &bc_v := v_{AC}(0) = 0, \ v_{AC}\left(\frac{L}{2}\right) = v_{CB}\left(\frac{L}{2}\right), \ v_{CB}(L) = 0: \\ &bc_\theta := D[1](v_{AC})(0) = 0, \ D[1](v_{AC})\left(\frac{L}{2}\right) = D[1](v_{CB})\left(\frac{L}{2}\right), D[1](v_{CB})(L) = 0: \\ &assign(dsolve(\{edo_{AC}, edo_{CB}, bc_v, bc_\theta\}, \{v_{AC}(x), v_{CB}(x), R_B, M_B\})): \\ &v_{AC} := unapply(v_{AC}(x), x): v_{CB} := unapply(v_{CB}(x), x): \end{split}$$

Respostas: reações, esforço cortante, momento fletor, deflexão e inclinação

$$\begin{split} R_{A}, R_{B}, M_{A}, M_{B} &= \frac{P}{2}, \frac{P}{2}, \frac{PL}{8}, \frac{PL}{8} \\ V_{AC}, V_{CB} &= \frac{P}{2}, -\frac{P}{2} \\ M_{AC}(x), M_{CB}(x) &= \frac{1}{2} x P - \frac{1}{8} PL, \frac{3}{8} PL - \frac{1}{2} x P \\ v_{AC}(x), v_{CB}(x) &= \frac{-\frac{3}{4} LPx^{2} + Px^{3}}{12 EI}, \frac{\frac{1}{8} L^{3}P - \frac{3}{4} L^{2}Px + \frac{9}{8} LPx^{2} - \frac{1}{2} Px^{3}}{6 EI} \\ D[1](v_{AC})(x), D[1](v_{CB})(x) &= \frac{-\frac{3}{2} LPx + 3Px^{2}}{12 EI}, \frac{-\frac{3}{4} L^{2}P + \frac{9}{4} LPx - \frac{3}{2} Px^{2}}{6 EI} \\ simplify \Big(v_{AC}(x) - \Big(-\frac{P \cdot x^{2}}{48 \cdot EI} \cdot (3 \cdot L - 4 \cdot x) \Big) \Big) &= 0 \\ simplify \Big(D[1](v_{AC})(x) - \Big(-\frac{P \cdot x}{8 \cdot EI} \cdot (L - 2 \cdot x) \Big) \Big) &= 0 \end{split}$$

Exemplo 11.4

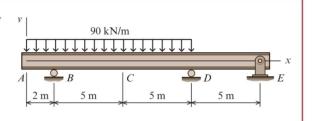
Referência: Philpot (2017). Mechanics of Materials: An integrated Learning System, 4th Edition. Wiley.

EXAMPLE 11.4

For the statically indeterminate beam shown, use discontinuity functions to determine

- (a) the force reactions at B, D, and E.
- (b) the deflection of the beam at A.
- (c) the deflection of the beam at C.

Assume a constant value of $EI = 120,000 \text{ kN} \cdot \text{m}^2$ for the beam.



restart:

Dados no SI

$$L_{AB}, L_{BC}, L_{CD}, L_{DE} := 2, 5, 5, 5 :$$

 $q, EI := 90 \cdot 10^{3}, 120000 \cdot 10^{3} :$
 $L := L_{AB} + L_{BC} + L_{CD} + L_{DE} = 17$

Reações de apoio (em função de R_E)

$$\begin{split} sfv &:= R_B + R_{\rm D} + R_E - q \cdot \left(L_{AB} + L_{BC} + L_{CD}\right) = 0 : \\ smE &:= -R_B \cdot \left(L_{BC} + L_{CD} + L_{DE}\right) - R_{\rm D} \cdot L_{DE} + q \cdot \left(L_{AB} + L_{BC} + L_{CD}\right) \cdot \left(L_{DE} + \frac{L_{AB} + L_{BC} + L_{CD}}{2}\right) = 0 : \end{split}$$

 $assign(solve(\{sfv, smE\}, \{R_B, R_D\}))$:

$$R_B, R_D = 648000 + \frac{R_E}{2}, 432000 - \frac{3 R_E}{2}$$

Momento fletor

$$\begin{split} &M_{AB} \coloneqq \textit{unapply} \Big(\textit{solve} \Big(M + q \cdot \frac{x^2}{2} = 0, M \Big), x \Big) : \\ &M_{BD} \coloneqq \textit{unapply} \Big(\textit{solve} \Big(M + q \cdot \frac{x^2}{2} - R_B \cdot \big(x - L_{AB} \big) = 0, M \Big), x \Big) : \\ &M_{DE} \coloneqq \textit{unapply} \big(\textit{solve} \big(-M + R_E \cdot \big(L_{AB} + L_{BC} + L_{CD} + L_{DE} - x \big) = 0, M \big), x \big) : \\ &M \coloneqq \textit{unapply} \big(\textit{piecewise} \big(x \geq 0 \text{ and } x \leq L_{AB}, M_{AB}(x), x > L_{AB} \text{ and } x \leq L - L_{DE}, M_{BD}(x), x > L - L_{DE} \\ &\text{and } x \leq L, M_{DE}(x), 0 \big), x \big) : \end{split}$$

$$M(x) = \begin{cases} -45000 x^{2} & 0 \le x \le 2 \\ -45000 x^{2} + 648000 x - 1296000 + \frac{1}{2} R_{E} x - R_{E} & 2 < x \le 12 \\ -R_{E} (-17 + x) & 12 < x \le 17 \\ 0 & otherwise \end{cases}$$

Equação da curva de deflexão

$$\begin{split} bc &:= v \big(L_{AB} \big) = 0, \, v \big(L - L_{DE} \big) = 0, \, v(L) = 0: \\ assign \bigg(dsolve \bigg(\left\{ diff \left(v(x), x\$2 \right) = \frac{M(x)}{EI}, \, bc \right\}, \, \left\{ v(x), \, R_E \right\} \bigg) \bigg): \\ v &:= unapply(v(x), x): \\ v(x) &= \end{split}$$

$$-\frac{47 x}{3000} + \frac{191}{6000} + \begin{cases} 0 & x \le 0 \\ -\frac{x^4}{32000} & x \le 2 \end{cases}$$

$$-\frac{47 x}{3000} + \frac{191}{6000} + \begin{cases} \frac{193}{240000} x^3 - \frac{193}{40000} x^2 - \frac{1}{32000} x^4 + \frac{193}{20000} x - \frac{193}{30000} & x \le 12 \\ -\frac{391}{40000} x^2 + \frac{23}{120000} x^3 + \frac{3541}{20000} x - \frac{26761}{30000} & x \le 17 \\ \frac{87 x}{8000} + \frac{397}{8000} & 17 < x \end{cases}$$

Respostas: Forças de reação, Deflexões em A e C

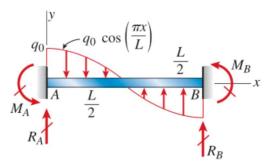
$$R_B, R_D, R_E = 579000, 639000, -138000$$

$$\delta_{\!A}, \delta_{\!C} := -v(0.), -v\big(evalf\big(L_{AB} + L_{BC}\big)\big) = -0.03183333333, 0.05234375000$$

Problema 10.3-9

Referência: Gere & Goodno (2013). Mechanics of Materials, 8th Edition. Cengage Learning.

- 10.3-8 A fixed-end beam of length L is loaded by a distributed load in the form of a cosine curve with maximum intensity q_0 at A.
- (a) Use the fourth-order differential equation of the deflection curve to solve for reactions at *A* and *B* and also the equation of the deflection curve.
- (b) Repeat part (a) using the distributed load $q_0 \sin(\pi x/L)$.



PROB. 10.3-8

restart:

Equação diferencial de 4a ordem

$$bc := v(0) = 0, v(L) = 0, D[1](v)(0) = 0, D[1](v)(L) = 0:$$

 $edo := diff(v(x), x\$4) = -\frac{q(x)}{EI}:$

A) usando a carga cossenoidal

$$\begin{aligned} q &:= x \rightarrow q_0 \cdot \cos\left(\frac{\pi \cdot x}{L}\right) : \\ v &:= unapply(rhs(dsolve(\{edo, bc\}, v(x))), x) : \end{aligned}$$

$$v(x) = -\frac{6L^2q_0x^2}{EI\pi^4} - \frac{q_0L^4\cos\left(\frac{\pi x}{L}\right)}{EI\pi^4} + \frac{4Lq_0x^3}{EI\pi^4} + \frac{q_0L^4}{EI\pi^4}$$

$$V := unapply(EI \cdot diff(v(x), x\$3), x) :$$

 $R_A, R_R := V(0), -V(L) :$

$$R_A, R_B = \frac{24 L q_0}{\pi^4}, -\frac{24 L q_0}{\pi^4}$$

$$\begin{split} M &:= unapply(EI \cdot diff(v(x), x\$2), x): \\ assign(solve(\left\{M(0) + M_A = 0, -M(L) + M_B\right\}, \left\{M_A, M_B\right\})): \end{split}$$

$$M_{A}, M_{B} = -\frac{L^{2} q_{0} (\pi^{2} - 12)}{\pi^{4}}, -\frac{L^{2} q_{0} (\pi^{2} - 12)}{\pi^{4}}$$

B) usando a carga senoidal

unassign('v', 'V', 'M', ' R_A ', ' R_B ', ' M_A ', ' M_B '):

$$q := x {
ightarrow} q_0 {
ightarrow} \sin\!\left(rac{\pi {
ightarrow} x}{L}
ight)$$
 :

 $v := unapply(rhs(dsolve(\{edo, bc\}, v(x))), x) :$

$$v(x) = -\frac{L^2 q_0 x^2}{EI \pi^3} - \frac{q_0 L^4 \sin\left(\frac{\pi x}{L}\right)}{EI \pi^4} + \frac{q_0 L^3 x}{EI \pi^3}$$

 $V := unapply(EI \cdot diff(v(x), x\$3), x) :$

 $R_A, R_B := V(0), -V(L)$:

$$R_A$$
, $R_B = \frac{q_0 L}{\pi}$, $\frac{q_0 L}{\pi}$

 $M := unapply(EI \cdot diff(v(x), x\$2), x):$

 $assign(solve(\{M(0) + M_A = 0, -M(L) + M_B\}, \{M_A, M_B\})):$

$$M_A, M_B = \frac{2L^2q_0}{\pi^3}, -\frac{2L^2q_0}{\pi^3}$$