

Universidade Federal de Alagoas - UFAL  
Centro de Tecnologia - CTEC  
Curso de Engenharia Civil

Mecânica dos Sólidos 3 - ECIV051D (2020.2)

**Exercícios:**  
**Deslocamentos em vigas isostáticas usando a equação diferencial da elástica**  
Encontro Assíncrono  
([Versão atualizada 23/07/2021](#))

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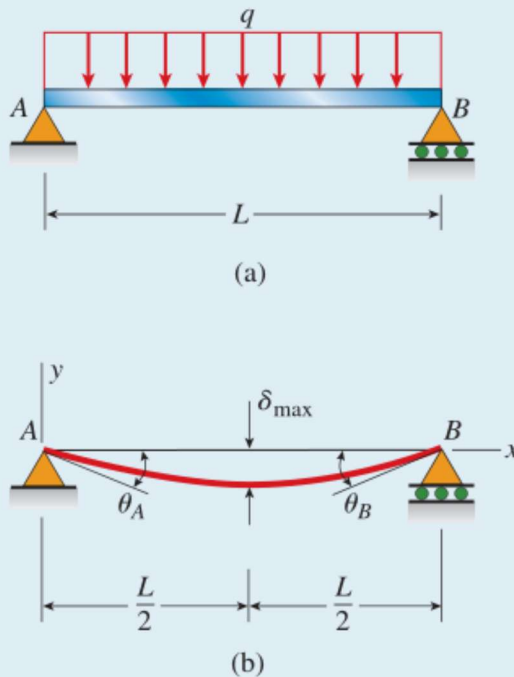
Maceió/AL, 16/07/2021

### Exemplo 9.1

Referência: Gere & Goodno (2013). Mechanics of Materials, 8th Edition. Cengage Learning.

Determine the equation of the deflection curve for a simple beam  $AB$  supporting a uniform load of intensity  $q$  acting throughout the span of the beam (Fig. 9-8a).

Also, determine the maximum deflection  $\delta_{\max}$  at the midpoint of the beam and the angles of rotation  $\theta_A$  and  $\theta_B$  at the supports (Fig. 9-8b). (Note: The beam has length  $L$  and constant flexural rigidity  $EI$ .)



restart :

#### Reações de apoio

$\text{assign}\left(\text{solve}\left(\left\{R_A + R_B - q \cdot L = 0, R_B \cdot L - (q \cdot L) \cdot \frac{L}{2} = 0\right\}, \{R_A, R_B\}\right)\right) :$

$$R_A, R_B = \frac{qL}{2}, \frac{qL}{2}$$

#### Momento fletor

$M := \text{unapply}\left(\text{solve}\left(M - R_A \cdot x + (q \cdot x) \cdot \frac{x}{2} = 0, M\right), x\right) :$

$$M(x) = \frac{1}{2} q L x - \frac{1}{2} q x^2$$

#### Equação da curva de deflexão

$$\text{diff}(v(x), x\$2) = \frac{d^2}{dx^2} v(x)$$

$v := \text{unapply}\left(\text{rhs}\left(\text{dsolve}\left(\left\{\text{diff}(v(x), x\$2) = \frac{M(x)}{EI}, v(0) = 0, v(L) = 0\right\}, v(x)\right)\right), x\right) :$

$$v(x) = \frac{q L x^3}{12 EI} - \frac{q x^4}{24 EI} - \frac{q L^3 x}{24 EI}$$

**Deflexão máxima**

$$\text{solve}\left(D[1](v)(x_{\max}) = 0, x_{\max}\right) = \frac{L}{2}, \left(\frac{1}{2} + \frac{\sqrt{3}}{2}\right)L, \left(\frac{1}{2} - \frac{\sqrt{3}}{2}\right)L$$

$$\text{evalf}(\%) = 0.50000000000 L, 1.366025404 L, -0.3660254040 L$$

$$\delta_{\max} := -v\left(\frac{L}{2}\right) = \frac{5}{384} \frac{q L^4}{EI}$$

**Ângulo de rotação nas extremidades**

$$\theta_A := -D[1](v)(0) = \frac{1}{24} \frac{q L^3}{EI}$$

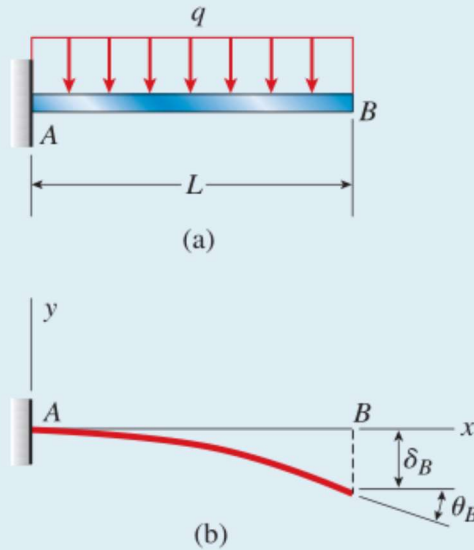
$$\theta_B := D[1](v)(L) = \frac{1}{24} \frac{q L^3}{EI}$$

### Exemplo 9.2

Referência: Gere & Goodno (2013). Mechanics of Materials, 8th Edition. Cengage Learning.

Determine the equation of the deflection curve for a cantilever beam  $AB$  subjected to a uniform load of intensity  $q$  (Fig. 9-10a).

Also, determine the angle of rotation  $\theta_B$  and the deflection  $\delta_B$  at the free end (Fig. 9-10b). (Note: The beam has length  $L$  and constant flexural rigidity  $EI$ .)



restart :

#### Reações de apoio

$assign\left(solve\left(\left\{R_A - q \cdot L = 0, M_A - (q \cdot L) \cdot \frac{L}{2} = 0\right\}, \{R_A, M_A\}\right)\right) :$

$$R_A, M_A = q L, \frac{q L^2}{2}$$

#### Momento fletor

$M := unapply\left(solve\left(M + M_A - R_A \cdot x + (q \cdot x) \cdot \frac{x}{2} = 0, M\right), x\right) :$

$$M(x) = -\frac{1}{2} q L^2 + q L x - \frac{1}{2} q x^2$$

#### Equação da curva de deflexão

$v := unapply\left(rhs\left(dsolve\left(\left\{diff(v(x), x^2) = \frac{M(x)}{EI}, v(0) = 0, D[1](v)(0) = 0\right\}, v(x)\right)\right), x) :$

$$v(x) = -\frac{q (L-x)^4}{24 EI} - \frac{q L^3 x}{6 EI} + \frac{q L^4}{24 EI}$$

**Ângulo de rotação e deflexão na extremidade livre**

$$\theta_B := -D[1](v)(L) = \frac{1}{6} \frac{q L^3}{EI}$$

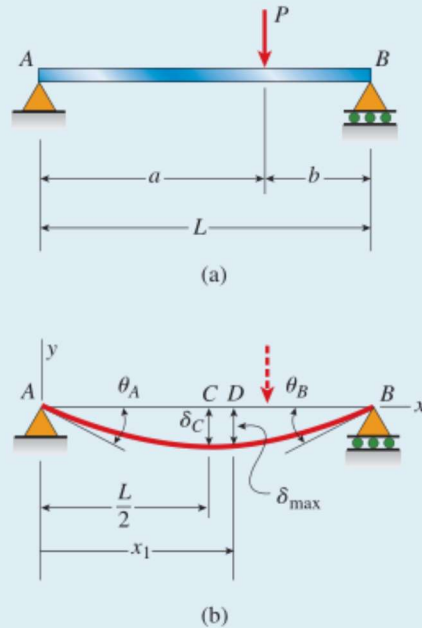
$$\delta_B := -v(L) = \frac{1}{8} \frac{q L^4}{EI}$$

### Exemplo 9.3

Referência: Gere & Goodno (2013). Mechanics of Materials, 8th Edition. Cengage Learning.

A simple beam  $AB$  supports a concentrated load  $P$  acting at distances  $a$  and  $b$  from the left-hand and right-hand supports, respectively (Fig. 9-12a).

Determine the equations of the deflection curve, the angles of rotation  $\theta_A$  and  $\theta_B$  at the supports, the maximum deflection  $\delta_{\max}$ , and the deflection  $\delta_C$  at the midpoint  $C$  of the beam (Fig. 9-12b). (Note: The beam has length  $L$  and constant flexural rigidity  $EI$ .)



restart :

$L := a + b :$

#### Reações de apoio

$\text{assign}(\text{solve}(\{R_A + R_B - P = 0, -P \cdot a + R_B \cdot L = 0\}, \{R_A, R_B\})) :$

$$R_A, R_B = \frac{Pb}{a+b}, \frac{Pa}{a+b}$$

#### Momento fletor

$M_{AP} := \text{unapply}(\text{solve}(M - R_A \cdot x = 0, M), x) :$

$M_{PB} := \text{unapply}(\text{solve}(-M + R_B \cdot (L - x) = 0, M), x) :$

$$M_{AP}(x), M_{PB}(x) = \frac{Pbx}{a+b}, \frac{Pa(a+b-x)}{a+b}$$

#### Equação da curva de deflexão

$bc := v_{AP}(0) = 0, v_{PB}(L) = 0, v_{AP}(a) = v_{PB}(a), D[1](v_{AP})(a) = D[1](v_{PB})(a) :$

$\text{res} := \text{dsolve}\left(\left\{\text{diff}(v_{AP}(x), x\$2) = \frac{M_{AP}(x)}{EI}, \text{diff}(v_{PB}(x), x\$2) = \frac{M_{PB}(x)}{EI}, bc\right\}, \{v_{AP}(x), v_{PB}(x)\}\right) :$

$v_{AP} := \text{unapply}(\text{simplify}(\text{rhs}(\text{res}[1])), x) :$

$v_{PB} := \text{unapply}(\text{simplify}(\text{rhs}(\text{res}[2])), x) :$

$$v_{AP}(x) = -\frac{P b x (a^2 + 2 a b - x^2)}{6 (a + b) EI}$$

$$v_{PB}(x) = \frac{(a^2 - 2 a x - 2 x b + x^2) (a + b - x) P a}{6 (a + b) EI}$$

$$\text{simplify}\left(v_{AP}(x) - \left(-\frac{P \cdot b \cdot x}{6 \cdot L \cdot EI} \cdot (L^2 - b^2 - x^2)\right)\right) = 0$$

$$\text{simplify}\left(v_{PB}(x) - \left(-\frac{P \cdot b \cdot x}{6 \cdot L \cdot EI} \cdot (L^2 - b^2 - x^2) - \frac{P \cdot (x - a)^3}{6 \cdot EI}\right)\right) = 0$$

### Ângulos de rotação nos suportes

$$\theta_A := -D[1](v_{AP})(0) = \frac{1}{6} \frac{P b (a^2 + 2 a b)}{(a + b) EI}$$

$$\theta_B := \text{simplify}(D[1](v_{PB})(L)) = \frac{1}{6} \frac{b (2 a + b) P a}{(a + b) EI}$$

$$\text{simplify}\left(\theta_A - \left(\frac{P \cdot a \cdot b \cdot (L + b)}{6 \cdot L \cdot EI}\right)\right) = 0$$

$$\text{simplify}\left(\theta_B - \left(\frac{P \cdot a \cdot b \cdot (L + a)}{6 \cdot L \cdot EI}\right)\right) = 0$$

### Deflexão máxima

Considerando  $a \geq b$

$$\text{solve}(D[1](v_{AP})(x_{\max}) = 0, x_{\max}) = \frac{\sqrt{3 a^2 + 6 a b}}{3}, -\frac{\sqrt{3 a^2 + 6 a b}}{3}$$

$$x_{\max} := \%[1] = \frac{1}{3} \sqrt{3 a^2 + 6 a b}$$

$$\delta_{\max} := \text{simplify}(-v_{AP}(x_{\max})) = \frac{1}{27} \frac{P b \sqrt{3} \sqrt{a (a + 2 b)} a (a + 2 b)}{(a + b) EI}$$

$$\text{simplify}\left(\delta_{\max} - \left(\frac{P \cdot b \cdot (L^2 - b^2)^{\frac{3}{2}}}{9 \cdot \sqrt{3} \cdot L \cdot EI}\right)\right) = 0$$

### Deflexão do ponto médio da viga

Considerando  $a \geq b$

$$\delta_C := \text{simplify}\left(-v_{AP}\left(\frac{L}{2}\right)\right) = \frac{1}{48} \frac{(3 a^2 + 6 a b - b^2) P b}{EI}$$

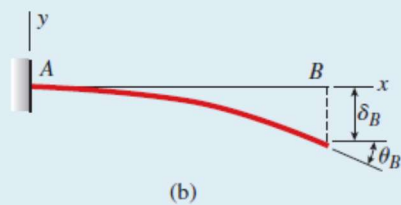
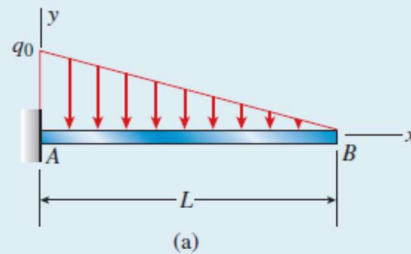
$$\text{simplify}\left(\delta_C - \left(\frac{P \cdot b \cdot (3 \cdot L^2 - 4 \cdot b^2)}{48 \cdot EI}\right)\right) = 0$$

### Exemplo 9.4

Referência: Gere & Goodno (2013). Mechanics of Materials, 8th Edition. Cengage Learning.

Determine the equation of the deflection curve for a cantilever beam  $AB$  supporting a triangularly distributed load of maximum intensity  $q_0$  (Fig. 9-14a).

Also, determine the deflection  $\delta_B$  and angle of rotation  $\theta_B$  at the free end (Fig. 9-14b). Use the fourth-order differential equation of the deflection curve (the load equation). (Note: The beam has length  $L$  and constant flexural rigidity  $EI$ .)



restart :

$$q := \text{unapply}\left(q_0 - q_0 \cdot \frac{x}{L}, x\right) :$$

**Reações de apoio**

$$\text{assign}\left(\text{solve}\left(\left\{R_A - \frac{q_0 \cdot L}{2} = 0, M_A - \left(\frac{q_0 \cdot L}{2}\right) \cdot \frac{L}{3} = 0\right\}, \{R_A, M_A\}\right)\right) :$$

$$R_A, M_A = \frac{q_0 L}{2}, \frac{q_0 L^2}{6}$$

**Momento fletor**

$$M := \text{unapply}\left(\text{solve}\left(M + M_A - R_A \cdot x + (q(x) \cdot x) \cdot \frac{x}{2} + \left((q_0 - q(x)) \cdot \frac{x}{2}\right) \cdot \frac{2 \cdot x}{3} = 0, M\right), x\right) :$$

$$M(x) = -\frac{q_0 (L^3 - 3 L^2 x + 3 x^2 L - x^3)}{6 L}$$

**Equação da curva de deflexão**

$$v := \text{unapply}\left(\text{rhs}\left(\text{dsolve}\left(\left\{\text{diff}(v(x), x\$2) = \frac{M(x)}{EI}, v(0) = 0, D[1](v)(0) = 0\right\}, v(x)\right)\right), x) :$$

$$v(x) = -\frac{q_0 (L - x)^5}{120 L EI} - \frac{q_0 L^3 x}{24 EI} + \frac{q_0 L^4}{120 EI}$$



$$\text{Simplify}\left(v(x) - \left(-\frac{q_0 \cdot x^2}{120 \cdot L \cdot EI} \cdot (10 \cdot L^3 - 10 \cdot L^2 \cdot x + 5 \cdot L \cdot x^2 - x^3)\right)\right) = 0$$

**Deflexão e ângulo de rotação na extremidade livre**

$$\delta_B := -v(L) = \frac{1}{30} \frac{q_0 L^4}{EI}$$

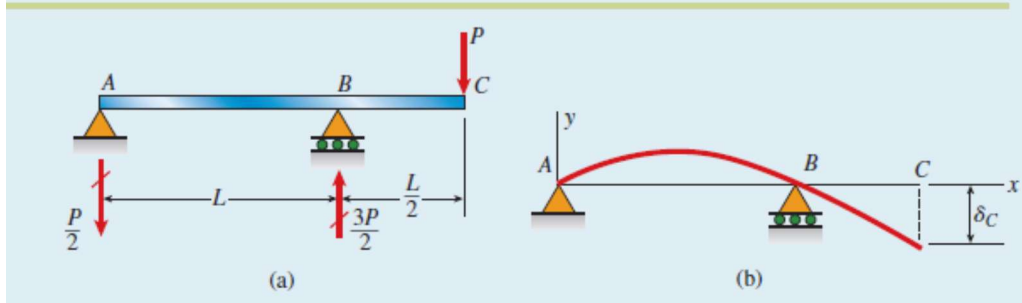
$$\theta_B := -D[1](v)(L) = \frac{1}{24} \frac{q_0 L^3}{EI}$$

### Exemplo 9.5

Referência: Gere & Goodno (2013). Mechanics of Materials, 8th Edition. Cengage Learning.

A simple beam  $AB$  with an overhang  $BC$  supports a concentrated load  $P$  at the end of the overhang (Fig. 9-15a). The main span of the beam has length  $L$  and the overhang has length  $L/2$ .

Determine the equations of the deflection curve and the deflection  $\delta_C$  at the end of the overhang (Fig. 9-15b). ~~Use the third-order differential equation of the deflection curve (the shear force equation).~~ (Note: The beam has constant flexural rigidity  $EI$ .)



restart :

### Reações de apoio

$assign\left(solve\left(\left\{R_A + R_B - P = 0, R_B \cdot L - P \cdot \frac{3 \cdot L}{2} = 0\right\}, \{R_A, R_B\}\right)\right) :$

$$R_A, R_B = -\frac{P}{2}, \frac{3P}{2}$$

### Momento fletor

$M_{AB} := unapply(solve(M - R_A \cdot x = 0, M), x) :$

$M_{BC} := unapply\left(solve\left(-M - P \cdot \left(\frac{3 \cdot L}{2} - x\right) = 0, M\right), x\right) :$

$$M_{AB}(x) = -\frac{Px}{2}$$

$$M_{BC}(x) = -\frac{P(3L - 2x)}{2}$$

$$simplify(M_{AB}(L) - M_{BC}(L)) = 0$$

### Equação da curva de deflexão

$bc := v_{AB}(0) = 0, v_{AB}(L) = 0, v_{BC}(L) = 0, D[1](v_{AB})(L) = D[1](v_{BC})(L) :$

$res := dsolve\left(\left\{diff(v_{AB}(x), x) = \frac{M_{AB}(x)}{EI}, diff(v_{BC}(x), x) = \frac{M_{BC}(x)}{EI}, bc\right\}, \{v_{AB}(x), v_{BC}(x)\}\right)$

$$res := \left\{v_{AB}(x) = -\frac{Px^3}{12EI} + \frac{PL^2x}{12EI}, v_{BC}(x) = \frac{-3L^3P + 10L^2Px - 9PLx^2 + 2Px^3}{12EI}\right\} \quad (1)$$

$v_{AB} := unapply(simplify(rhs(res[1])), x) :$

$v_{BC} := unapply(simplify(rhs(res[2])), x) :$

$$v_{AB}(x) = \frac{P x (L^2 - x^2)}{12 EI}$$

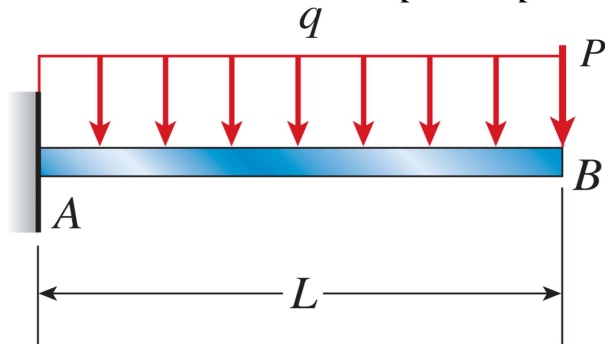
$$v_{BC}(x) = - \frac{(3 L - x) P (L - 2 x) (L - x)}{12 EI}$$

$$\text{simplify} \left( v_{BC}(x) - \left( - \frac{P}{12 \cdot EI} \cdot (3 \cdot L^3 - 10 \cdot L^2 \cdot x + 9 \cdot L \cdot x^2 - 2 \cdot x^3) \right) \right) = 0$$

**Deflexão na extremidade em balanço**

$$\delta_C := -v_{BC} \left( \frac{3 \cdot L}{2} \right) = \frac{1}{8} \frac{P L^3}{EI}$$

### Problema adicional #1: recalques de apoio



restart :

#### Reações de apoio

$$\text{assign}\left(\text{solve}\left(\left\{R_A - q \cdot L - P = 0, M_A - (q \cdot L) \cdot \frac{L}{2} - P \cdot L = 0\right\}, \{R_A, M_A\}\right)\right) :$$

$$R_A, M_A = qL + P, \frac{1}{2} qL^2 + PL$$

#### Momento fletor

$$M := \text{unapply}\left(\text{solve}\left(M + M_A - R_A \cdot x + (q \cdot x) \cdot \frac{x}{2} = 0, M\right), x\right) :$$

$$M(x) = -\frac{1}{2} qL^2 - PL + Lqx + Px - \frac{1}{2} qx^2$$

#### Equação da curva de deflexão e rotação

$$bc := v(0) = v_0, D[1](v)(0) = \theta_0 :$$

$$v := \text{unapply}\left(\text{expand}\left(\text{rhs}\left(\text{dsolve}\left(\left\{\text{diff}(v(x), x\$2) = \frac{M(x)}{EI}, bc\right\}, v(x)\right)\right), x\right) :$$

$$\theta := \text{unapply}(\text{expand}(\text{diff}(v(x), x)), x) :$$

$$v(x) = -\frac{qx^4}{24EI} + \frac{Lx^3q}{6EI} + \frac{x^3P}{6EI} - \frac{L^2x^2q}{4EI} - \frac{Lx^2P}{2EI} + \theta_0x + v_0$$

$$\theta(x) = -\frac{qx^3}{6EI} + \frac{Lx^2q}{2EI} + \frac{x^2P}{2EI} - \frac{L^2xq}{2EI} - \frac{LxP}{EI} + \theta_0$$

#### Avaliação de rotação e deflexão em $x = L$

$$\text{expand}(\theta(L)) = -\frac{qL^3}{6EI} - \frac{L^2P}{2EI} + \theta_0$$

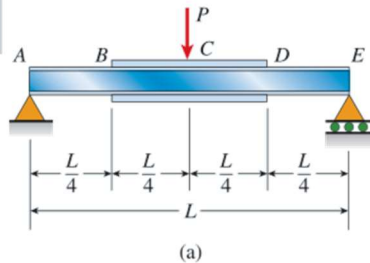
$$\text{expand}(v(L)) = -\frac{qL^4}{8EI} - \frac{L^3P}{3EI} + \theta_0L + v_0$$

## Problema adicional #2: Exemplo 9-13 (viga não prismática)

Referência: Gere & Goodno (2013). Mechanics of Materials, 8th Edition. Cengage Learning.

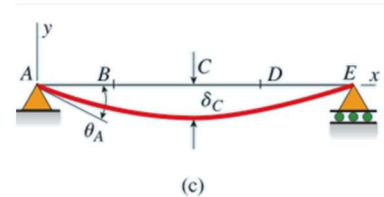
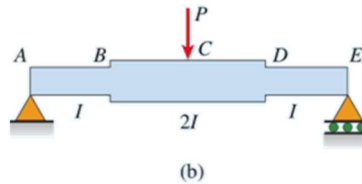
### ● Example 9-13

Example 9-13: Simple beam with two different moments of inertia



A beam  $ABCDE$  on simple supports is constructed from a wide-flange beam by welding cover plates over the middle half of the beam (Fig. 9-28a). The effect of the cover plates is to double the moment of inertia (Fig. 9-28b). A concentrated load  $P$  acts at the midpoint  $C$  of the beam.

Determine the equations of the deflection curve, the angle of rotation  $\theta_A$  at the left-hand support, and the deflection  $\delta_C$  at the midpoint (Fig. 9-28c).



restart :

**Reações de apoio**

$$\text{assign}\left(\text{solve}\left(\left\{R_A + R_E - P = 0, -P \cdot \frac{L}{2} + R_E \cdot L = 0\right\}, \{R_A, R_E\}\right)\right) :$$

$$R_A, R_E = \frac{P}{2}, \frac{P}{2}$$

**Momento fletor**

$$M_{AC} := \text{solve}(M - R_A \cdot x = 0, M) = \frac{1}{2} P x$$

**Equação da curva de deflexão**

$$\text{eqn} := \text{diff}(v_{AB}(x), x\$2) = \frac{M_{AC}}{EI}, \text{diff}(v_{BC}(x), x\$2) = \frac{M_{AC}}{2 \cdot EI} :$$

$$\text{bc} := v_{AB}(0) = 0, D[1](v_{BC})\left(\frac{L}{2}\right) = 0, v_{AB}\left(\frac{L}{4}\right) = v_{BC}\left(\frac{L}{4}\right), D[1](v_{AB})\left(\frac{L}{4}\right) = D[1](v_{BC})\left(\frac{L}{4}\right) :$$

$$\text{res} := \text{dsolve}(\{\text{eqn}, \text{bc}\}, \{v_{AB}(x), v_{BC}(x)\}) :$$

$$v_{AB} := \text{unapply}(\text{simplify}(\text{rhs}(\text{res}[1])), x) :$$

$$v_{BC} := \text{unapply}(\text{simplify}(\text{rhs}(\text{res}[2])), x) :$$

$$v_{AB}(x) = -\frac{Px(15L^2 - 32x^2)}{384EI}$$

$$v_{BC}(x) = -\frac{P(L^3 + 24L^2x - 32x^3)}{768EI}$$

**Ângulo de rotação em A e deflexão em C**

$$\theta_A := -D[1](v_{AB})(0) = \frac{5}{128} \frac{PL^2}{EI}$$

$$\delta_C := -v_{BC}\left(\frac{L}{2}\right) = \frac{3}{256} \frac{PL^3}{EI}$$