

# Stability analysis of nonsmooth systems for control

Riccardo Bertollo

(Eindhoven University of Technology)

UCLouvain – January 21, 2025

# About me



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MSc – Mechatronics Engineering  
(2017 - 2019)



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PhD – Mechatronics Engineering  
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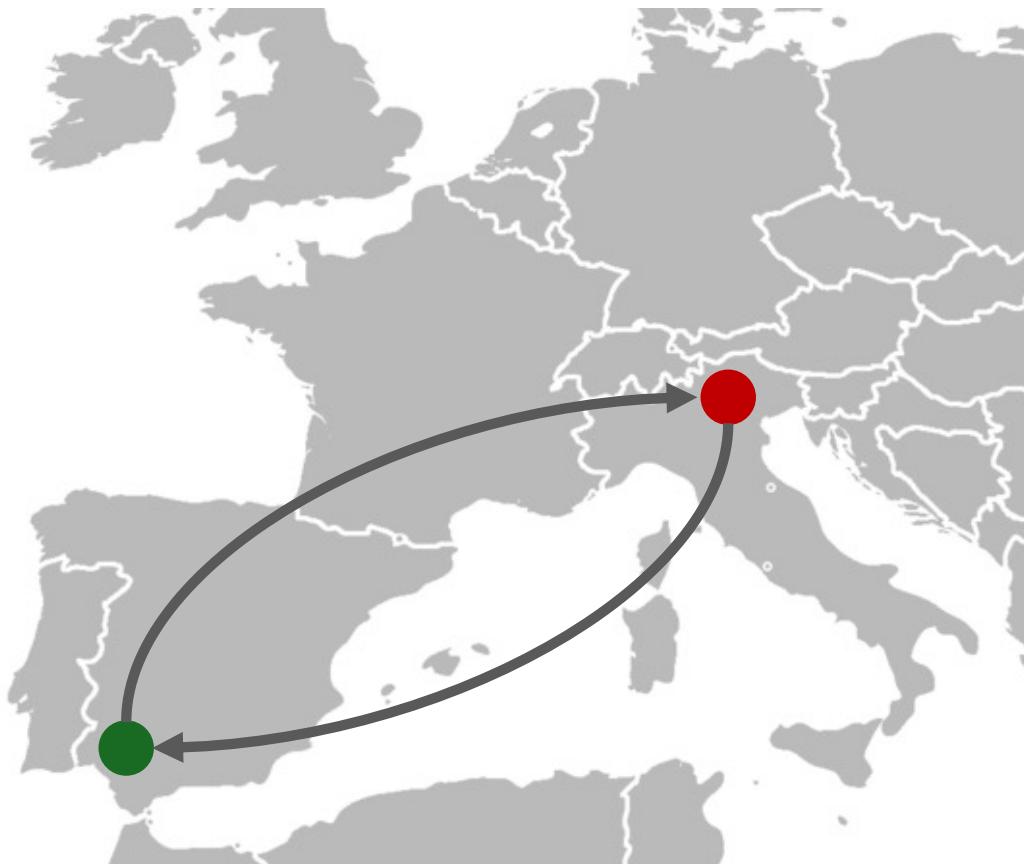
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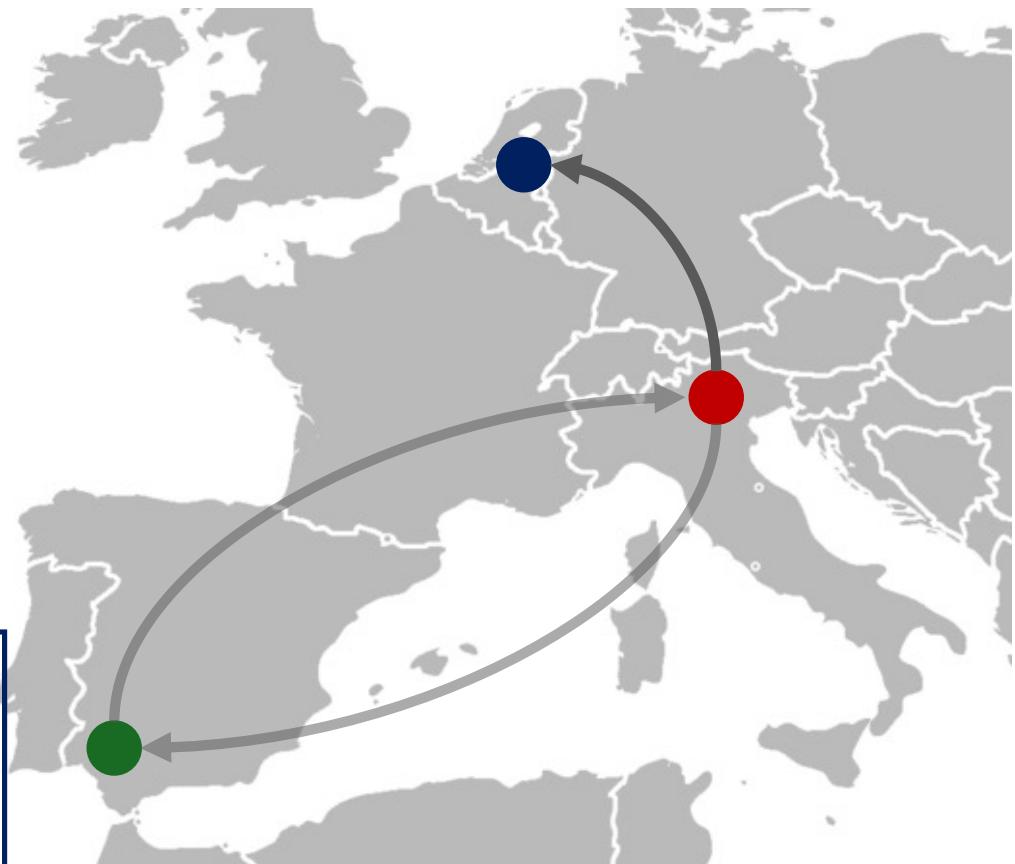
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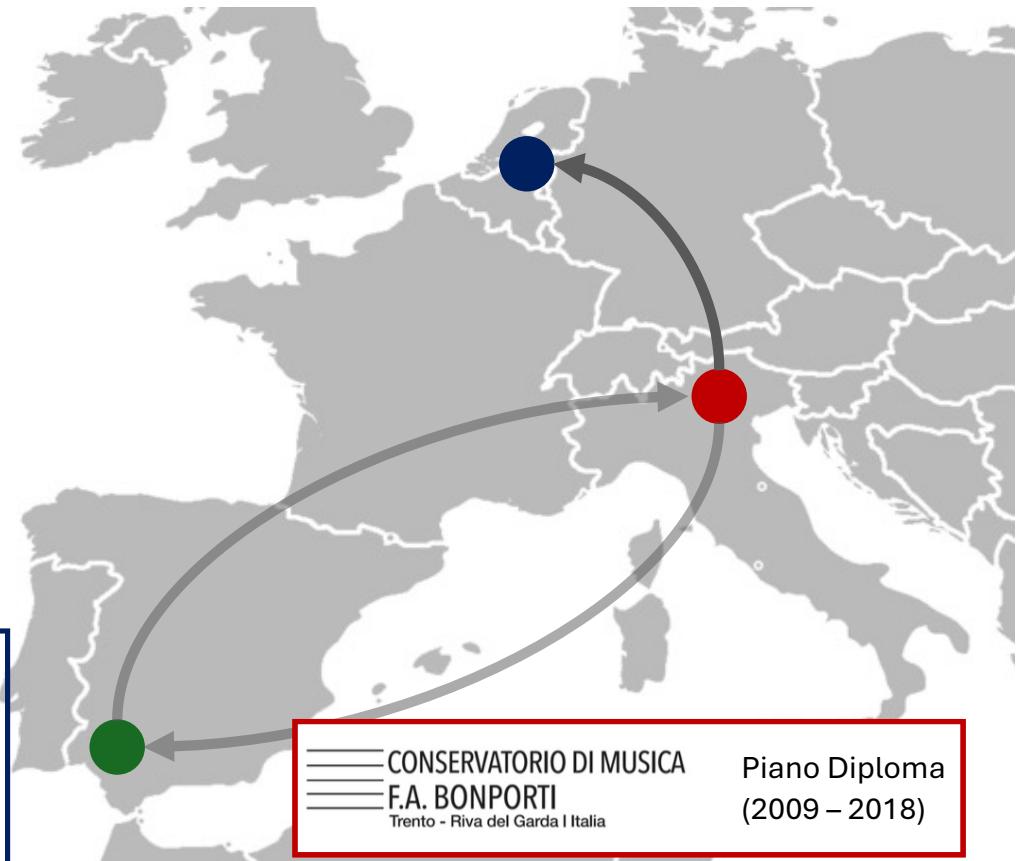
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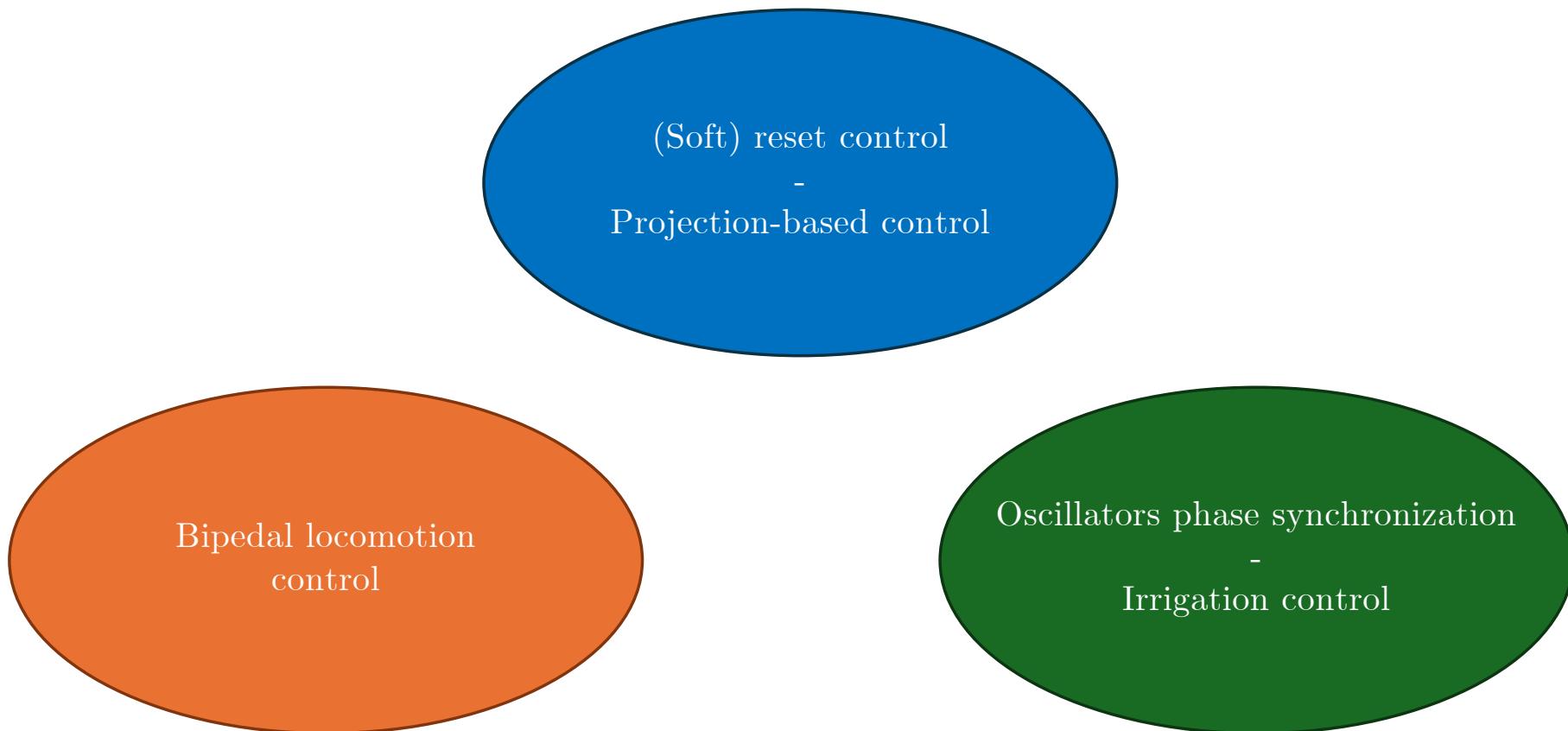
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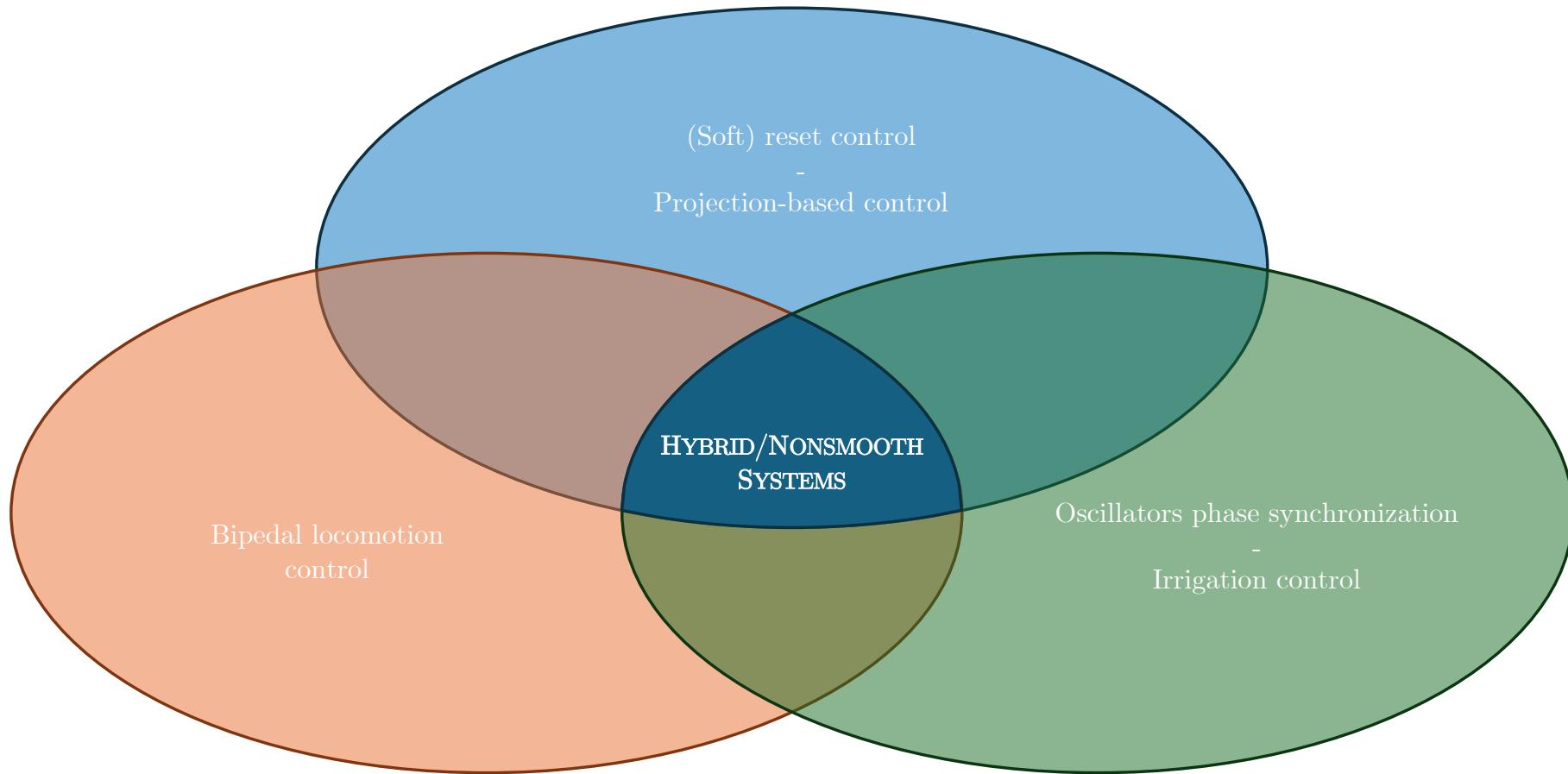
CONSERVATORIO DI MUSICA  
**F.A. BONPORTI**  
Trento - Riva del Garda | Italia

Piano Diploma  
(2009 – 2018)

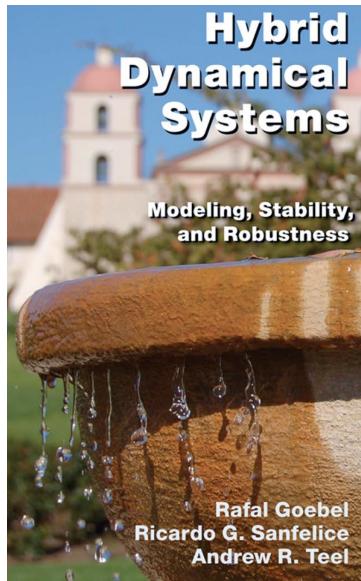
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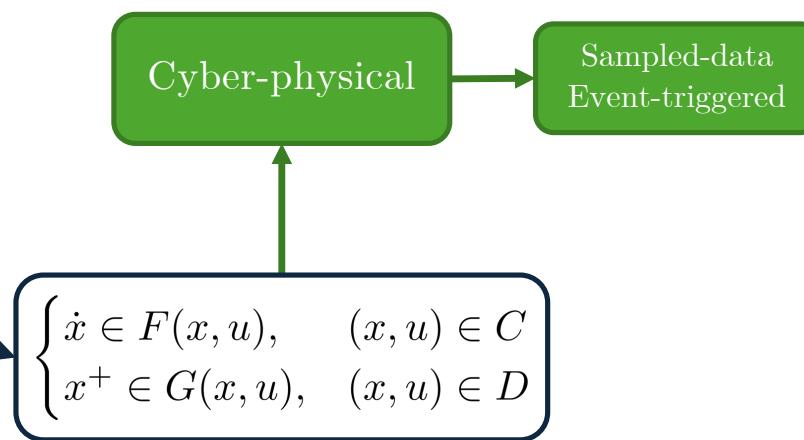
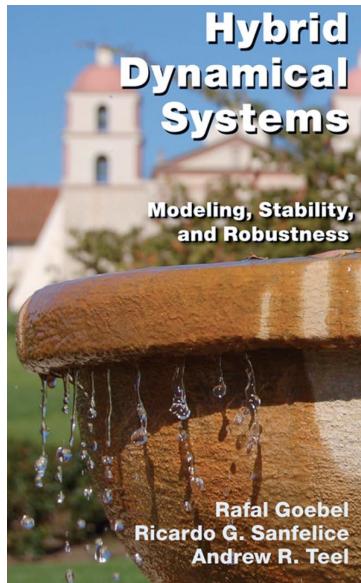


# Hybrid dynamical systems

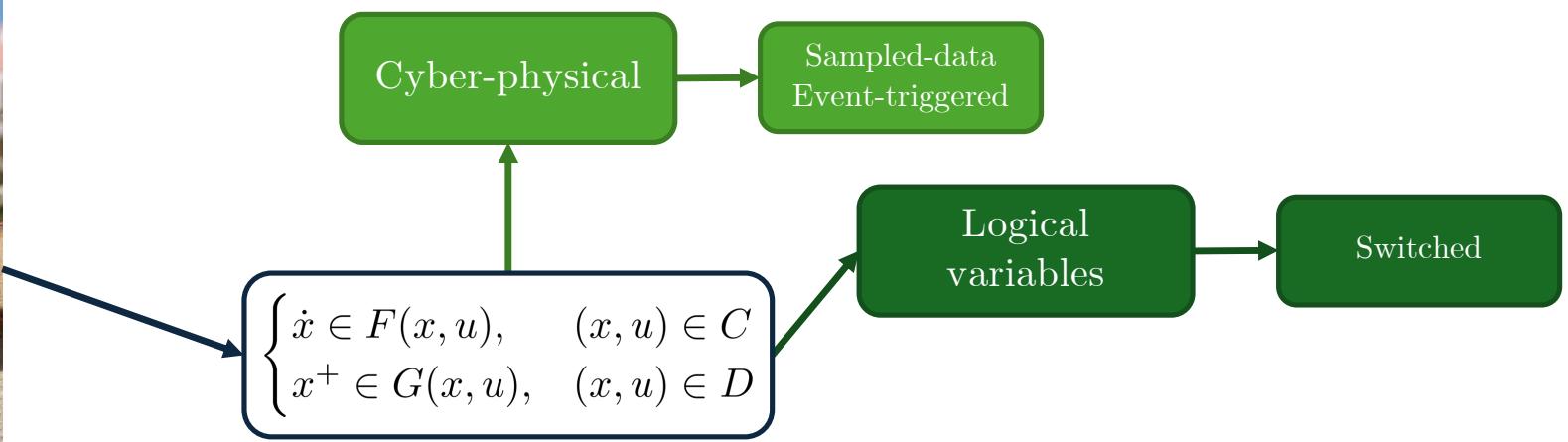
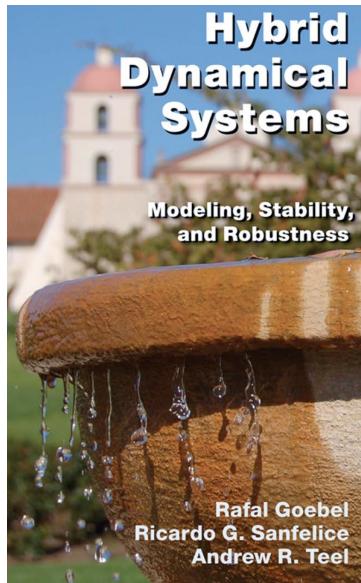


$$\begin{cases} \dot{x} \in F(x, u), & (x, u) \in C \\ x^+ \in G(x, u), & (x, u) \in D \end{cases}$$

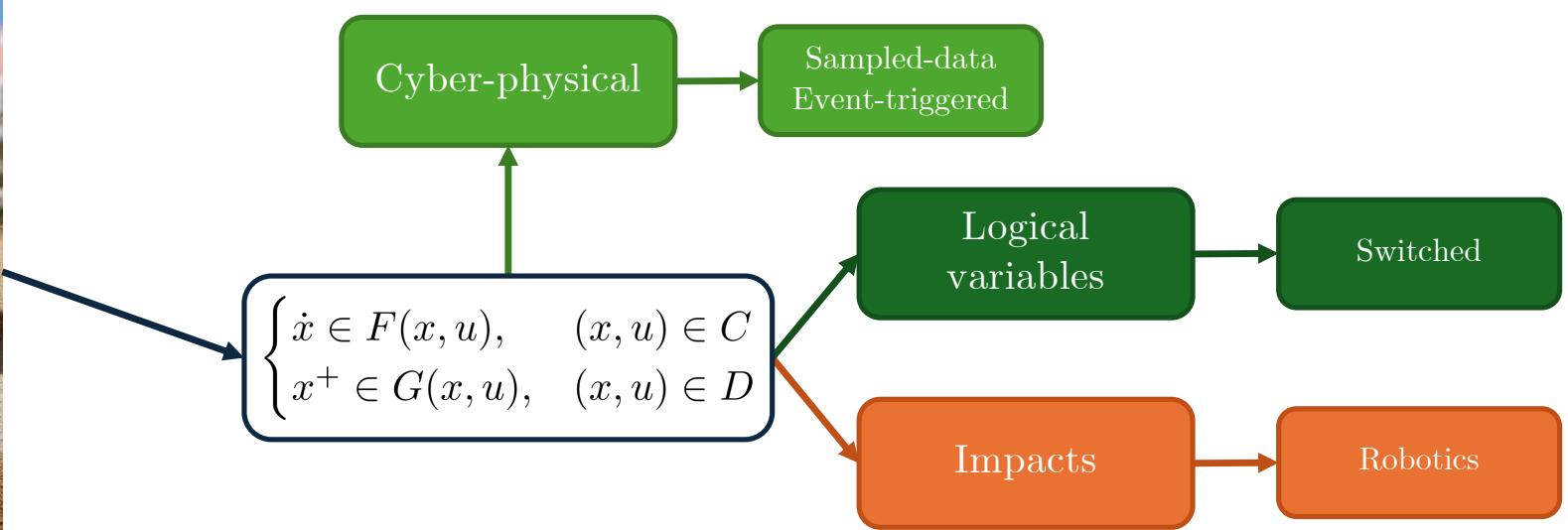
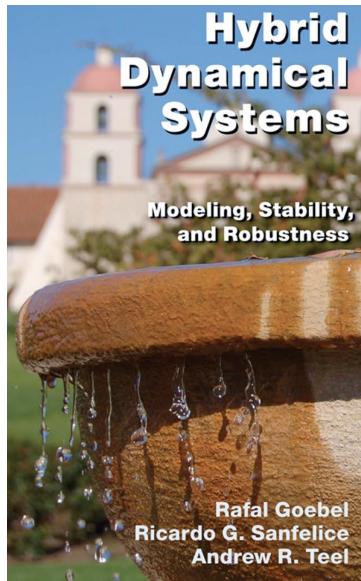
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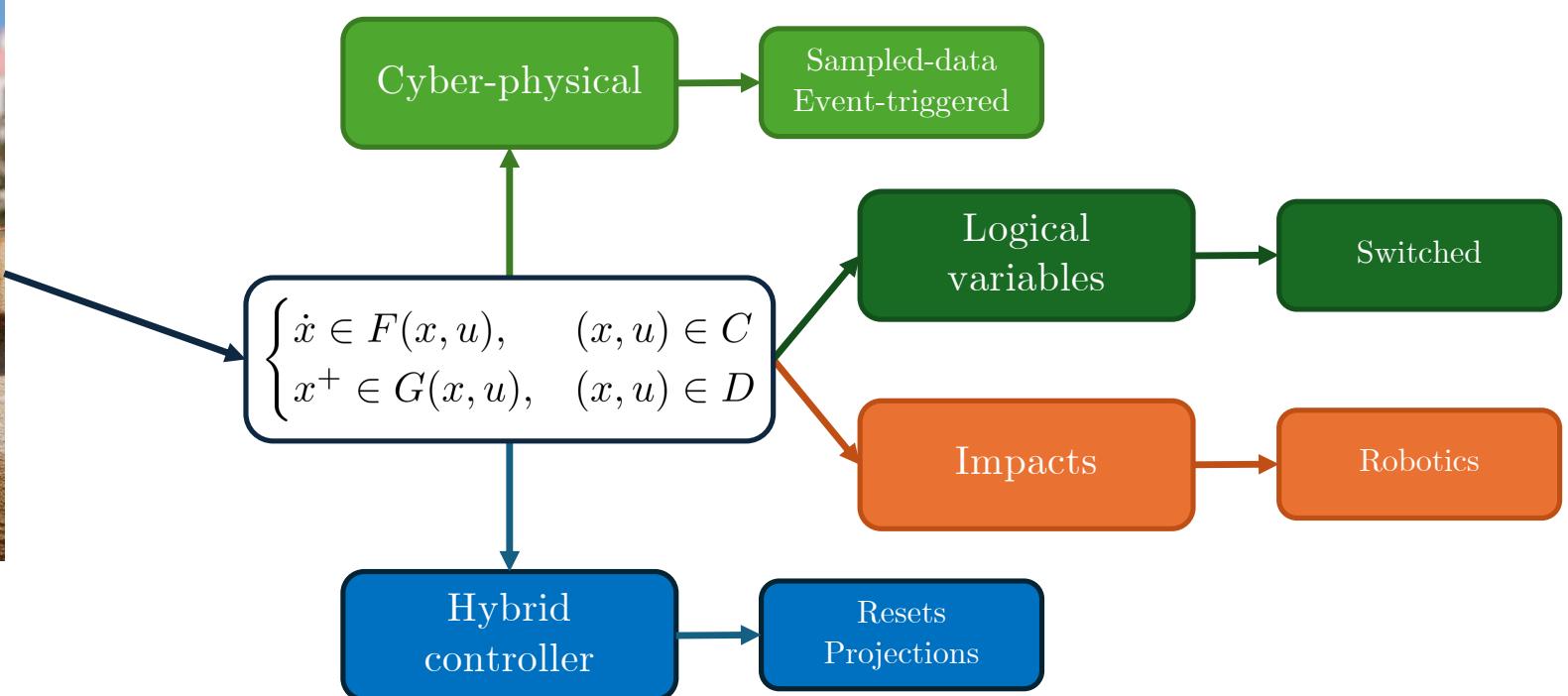
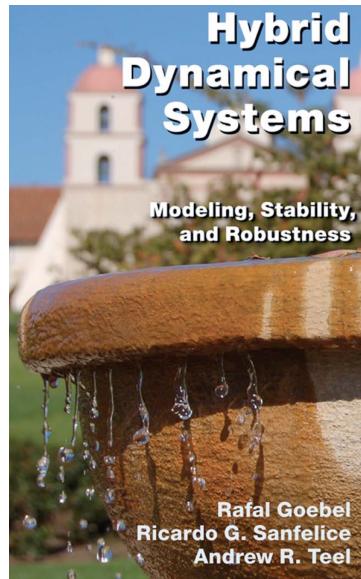
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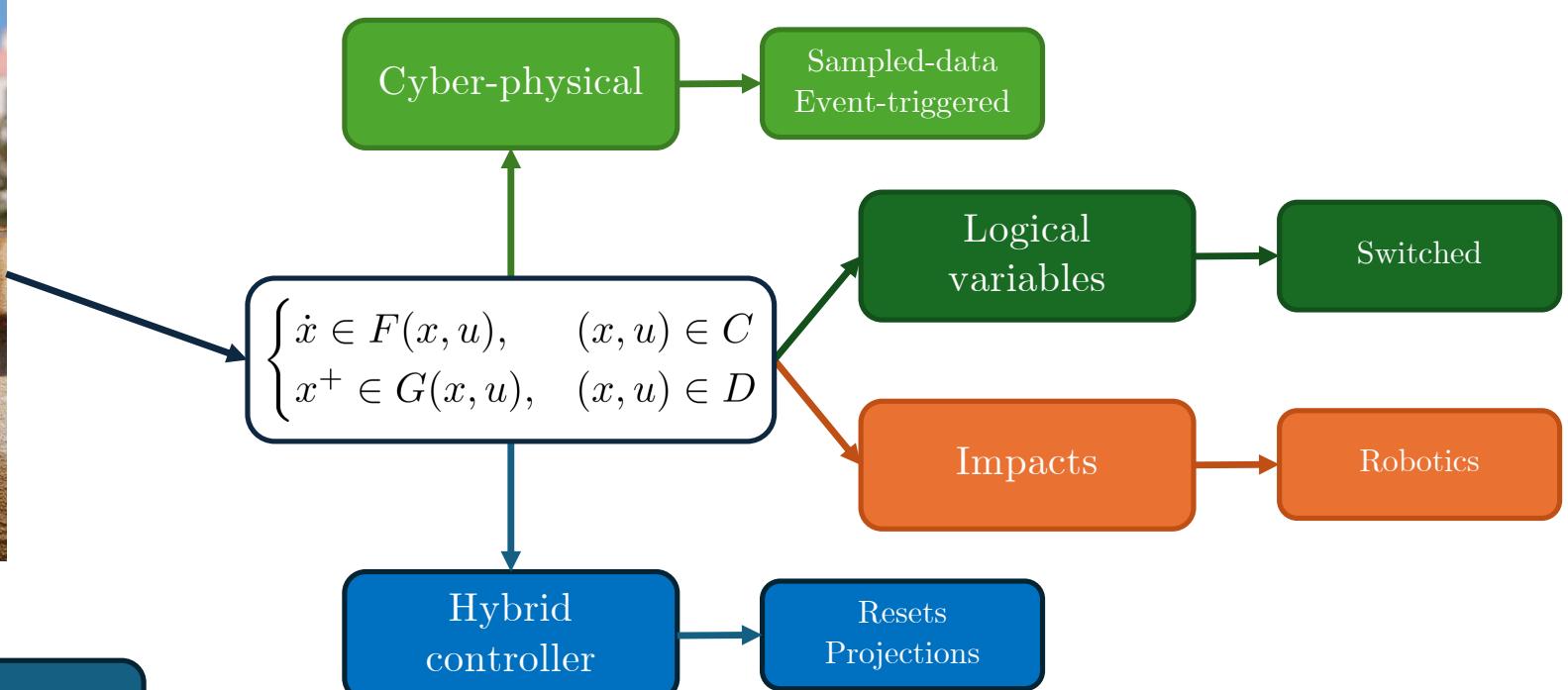
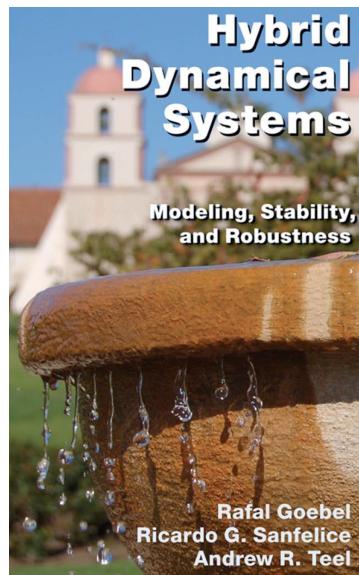
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LYAPUNOV TECHNIQUES

# First Order Reset Elements

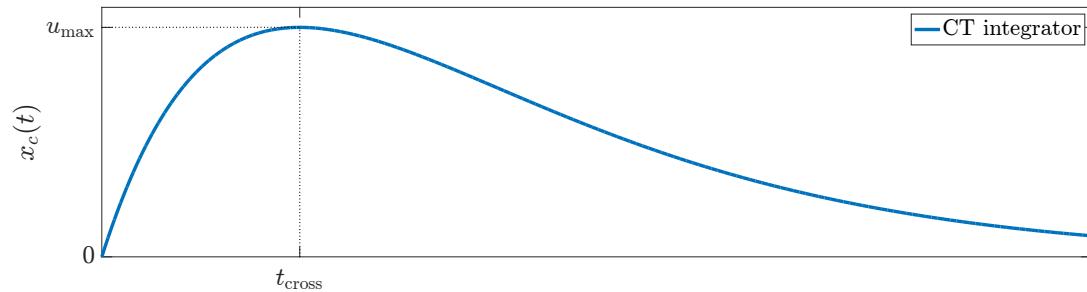
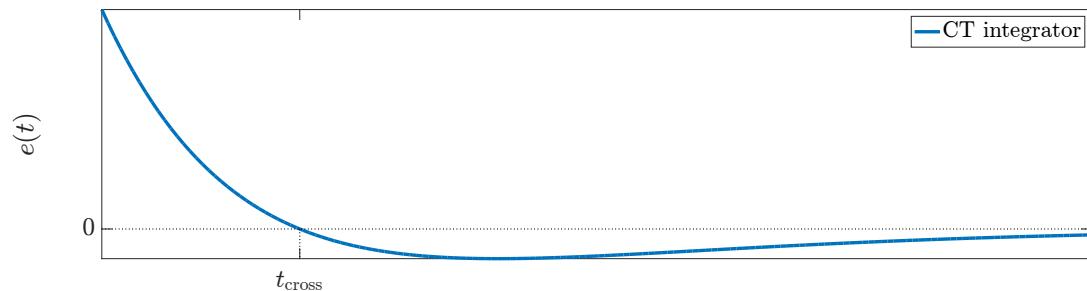
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$$\begin{cases} \dot{x}_c = e, & \text{"normally"} \\ x_c^+ = 0, & \text{"at the right moment"} \end{cases}$$

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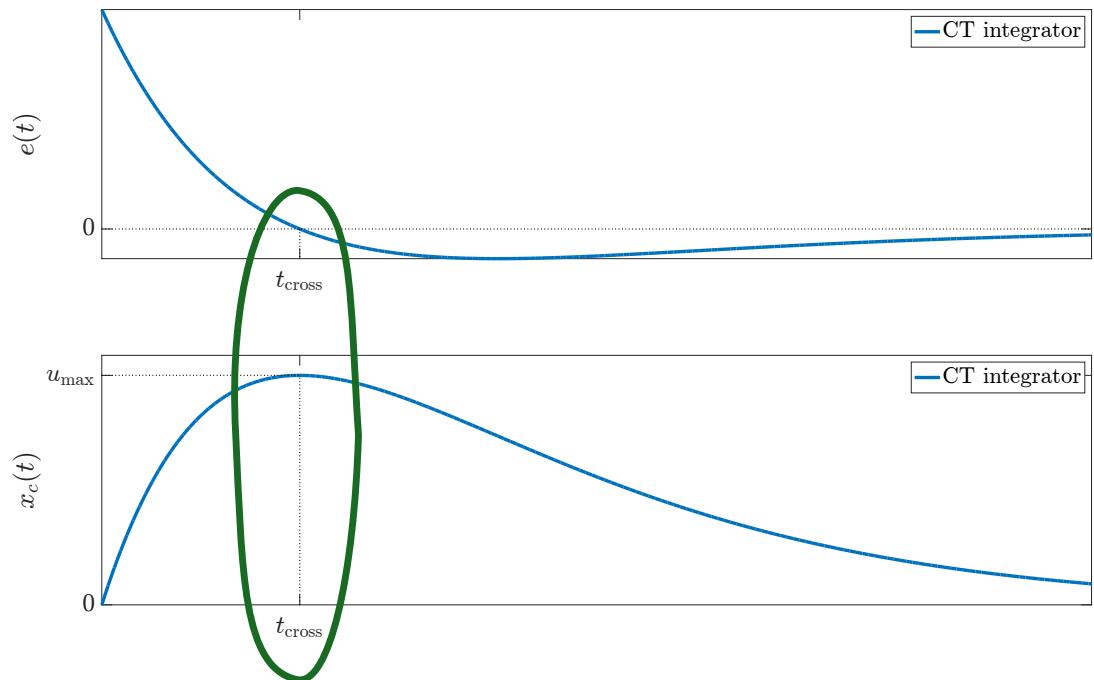
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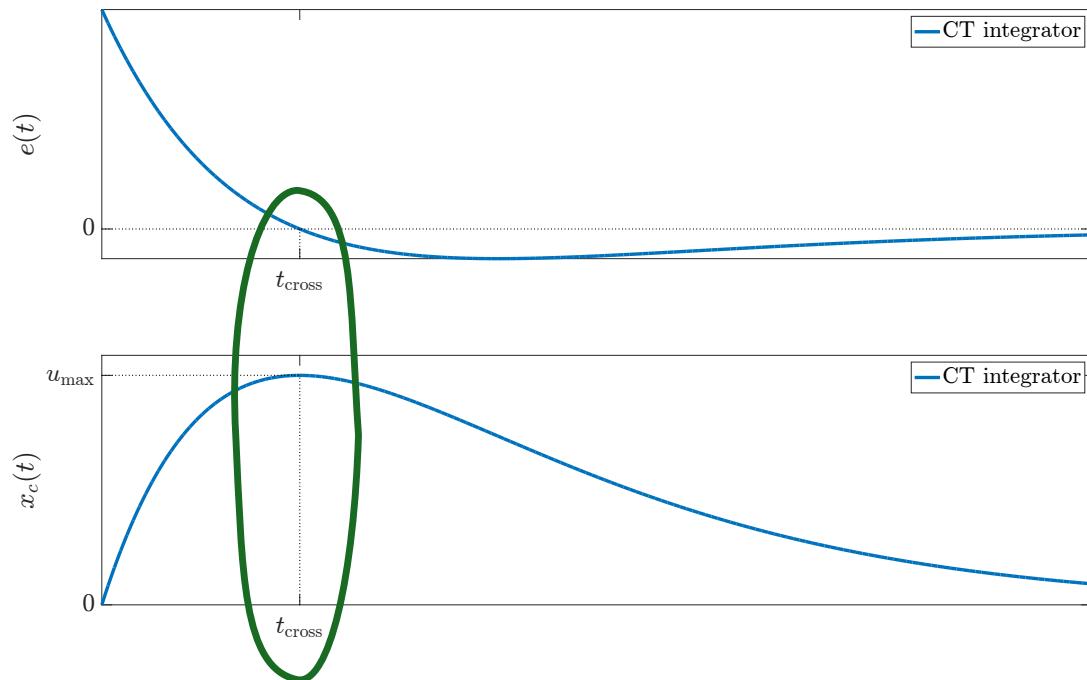
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Clegg integrator dynamics:

$$\begin{cases} \dot{x}_c = e, & x_c e \geq 0 \\ x_c^+ = 0, & x_c e \leq 0 \end{cases}$$



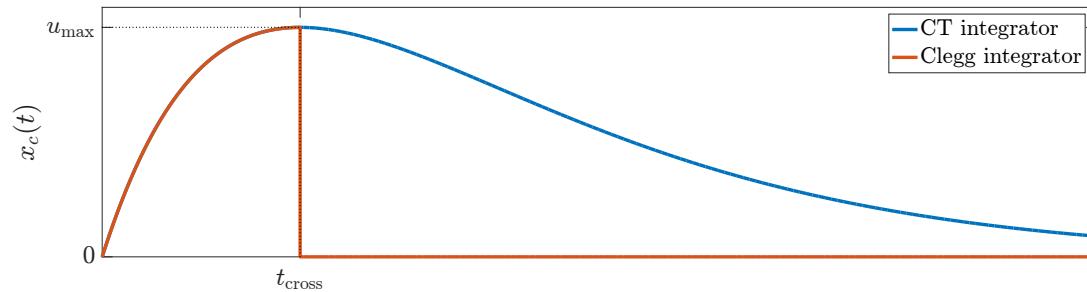
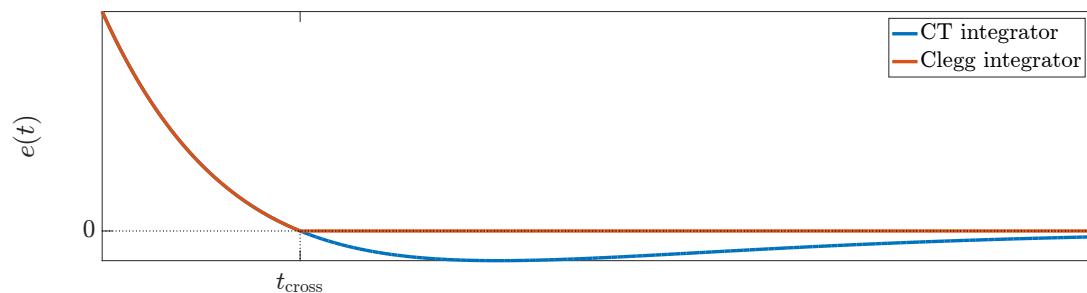
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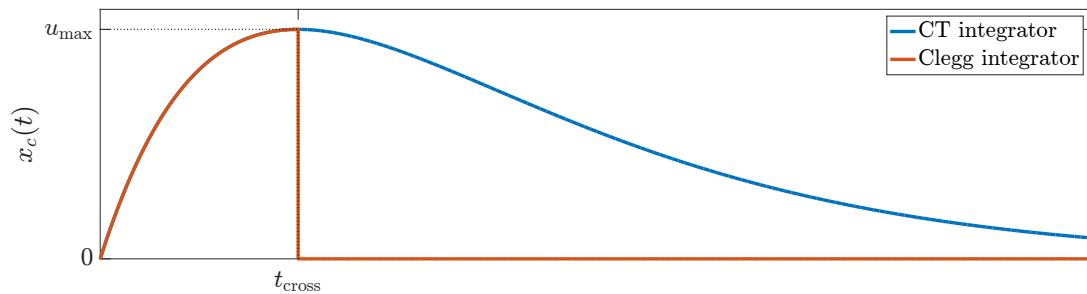
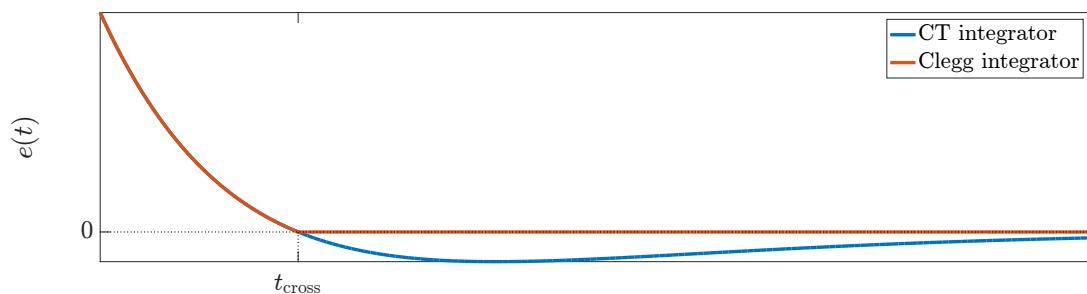
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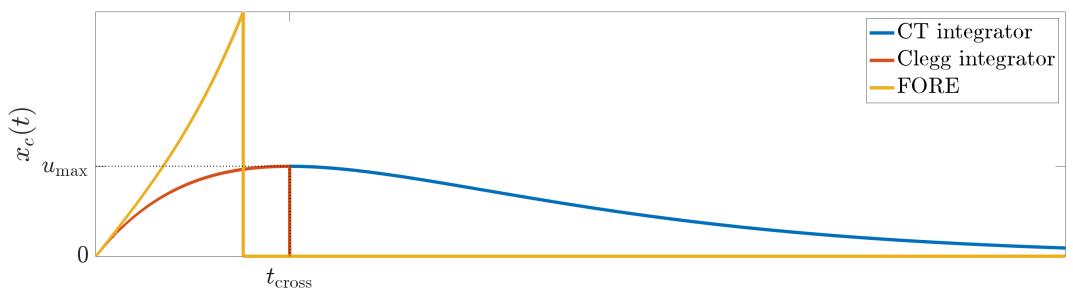
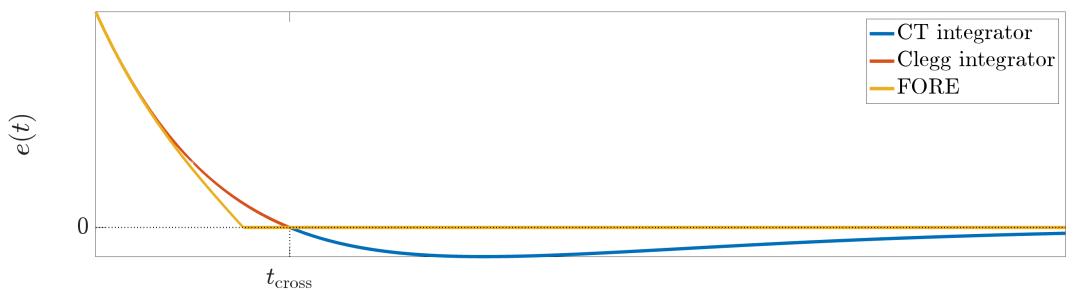
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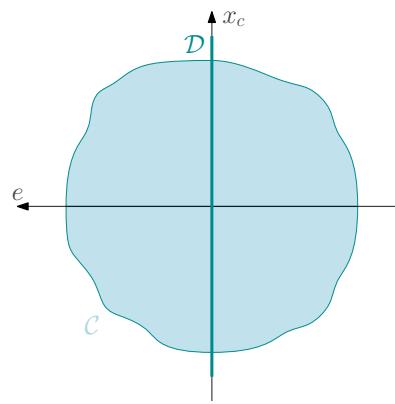
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# FORE: modelling nuances

Initial model [1]

$$\begin{cases} \dot{x}_c = e, & e \neq 0 \\ x_c^+ = 0, & e = 0 \end{cases}$$



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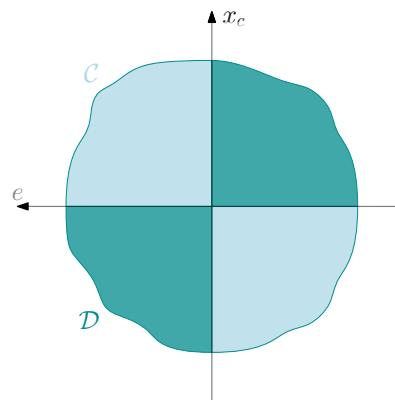
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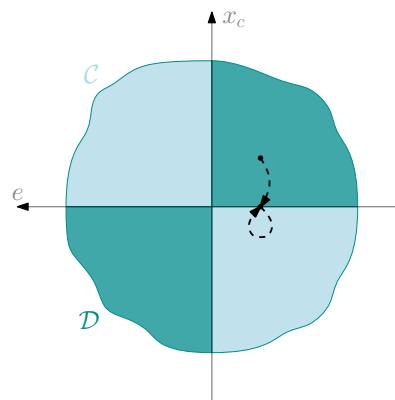
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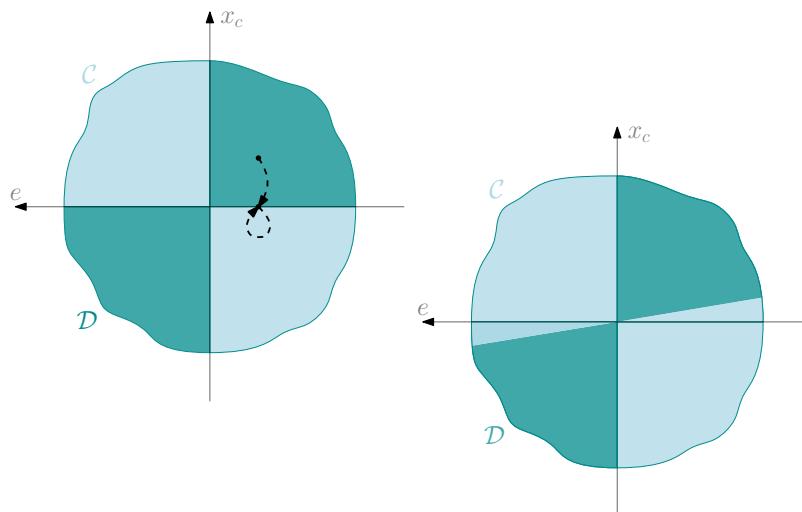
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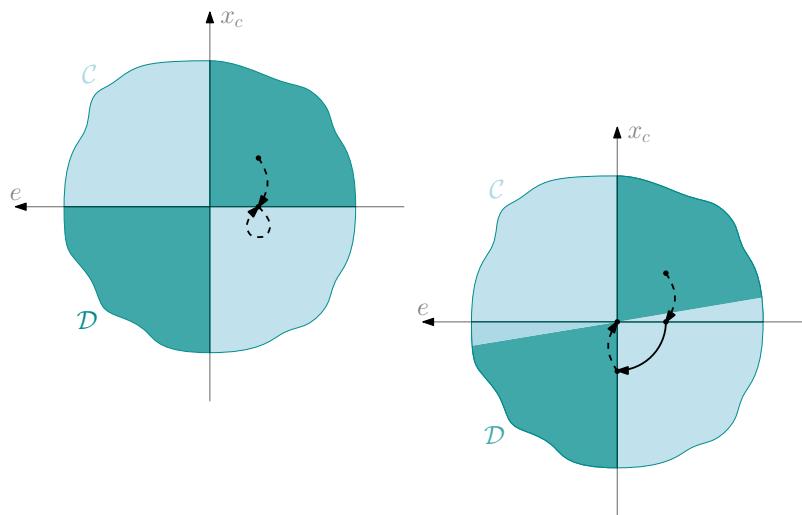
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Start from generic reset-based closed loop...

$$\begin{cases} \dot{x} = Ax, & x^\top Mx \leq 0 \\ x^+ = Rx, & x^\top Mx \geq 0 \end{cases}$$

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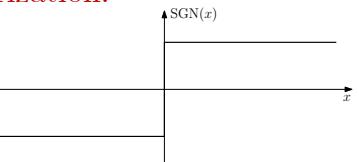
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Krasovskii regularization:

$$\text{SGN}(x) := \begin{cases} \text{sgn}(x), & \text{if } x \neq 0 \\ [-1, 1], & \text{if } x = 0 \end{cases}$$



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$$F(x) = Ax$$

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Regulates how closely the CT  
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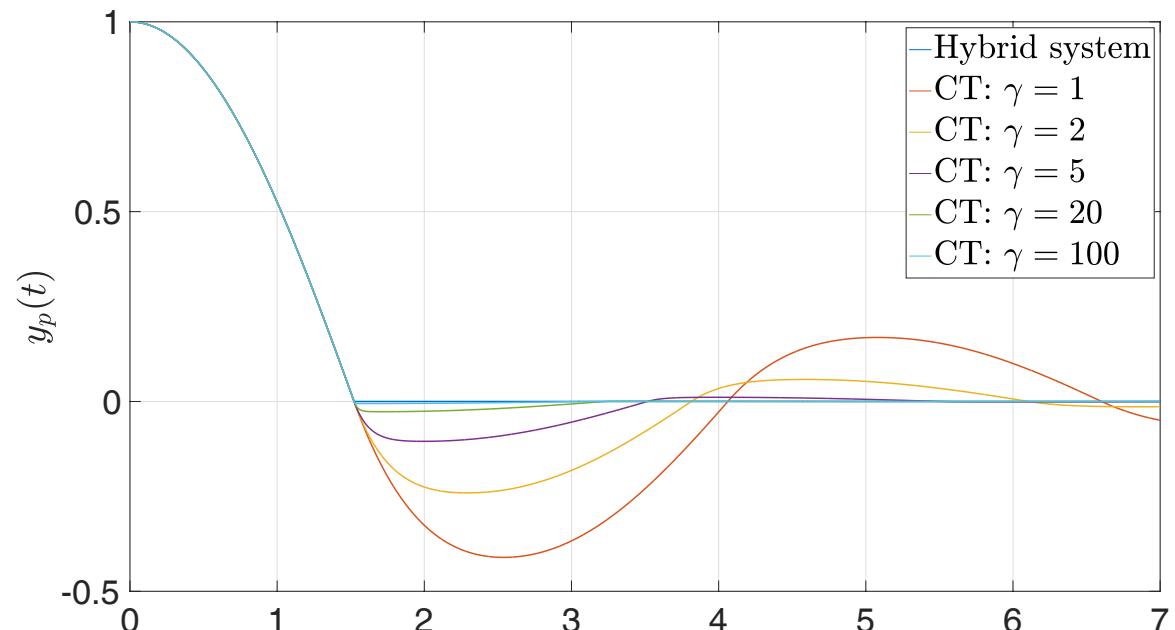
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# Stability with soft-reset control

$$\dot{x} \in F(x) := Ax + \gamma(\text{SGN}(x^\top Mx) + 1)(Rx - x)$$

## Theorem

If  $\exists \varepsilon > 0$  and a Lyapunov function  $V$  such that

1.  $V$  is **Lipschitz continuous**, homogeneous of degree 2, positive definite, strongly convex;
2. defined  $C_\varepsilon := \{x \in \mathbb{R}^b : x^\top Mx \leq \varepsilon x^\top x\}$ , we have

$$\begin{aligned}\langle \nabla V, Ax \rangle &\leq 0, && \text{for almost all } x \in C_\varepsilon, \\ V(Rx) - V(x) &\leq 0, && \text{for all } x \in D;\end{aligned}$$

3.  $x \in D$  implies  $Rx \in C$ ;
4. no continuous solution of the hybrid system keeps  $V$  constant and nonzero;

then the origin is GES for  $\dot{x} \in F(x)$ , for  $\gamma > 0$  large enough.

# Why do we need nonsmoothness?

**FORE + integrator closed loop:**

$$\dot{x} = \begin{bmatrix} \dot{x}_c \\ \dot{e} \end{bmatrix} = \begin{bmatrix} 0.1 & 1 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} x_c \\ e \end{bmatrix} = Ax$$

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**Quadratic Lyapunov function:**

$$V = x^\top Px = x^\top \begin{bmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{bmatrix} x$$

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**Flow condition:**

$$\dot{V}(x) := \langle \nabla V, Ax \rangle = 2x^\top APx = 2x^\top \begin{bmatrix} 0.1p_{11} - p_{12} & p_{11} \\ 0.1p_{12} - p_{22} & p_{12} \end{bmatrix} x$$

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$$V = x^\top Px = x^\top \begin{bmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{bmatrix} x$$

**Flow condition:**

$$\dot{V}(x) := \langle \nabla V, Ax \rangle = 2x^\top APx = 2x^\top \begin{bmatrix} 0.1p_{11} - p_{12} & p_{11} \\ 0.1p_{12} - p_{22} & p_{12} \end{bmatrix} x$$

$$\dot{V}([0, 1]^\top) \leq 0$$

$$\downarrow$$

$$p_{12} \leq 0$$

$$\dot{V}([1, 0]^\top) \leq 0$$

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$$p_{12} - 0.1p_{11} \geq 0$$

# Why do we need nonsmoothness?

**FORE + integrator closed loop:**

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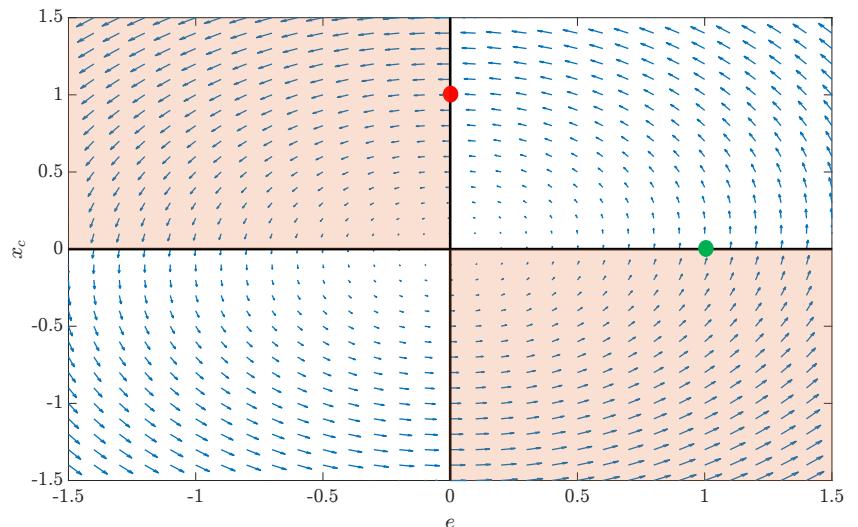
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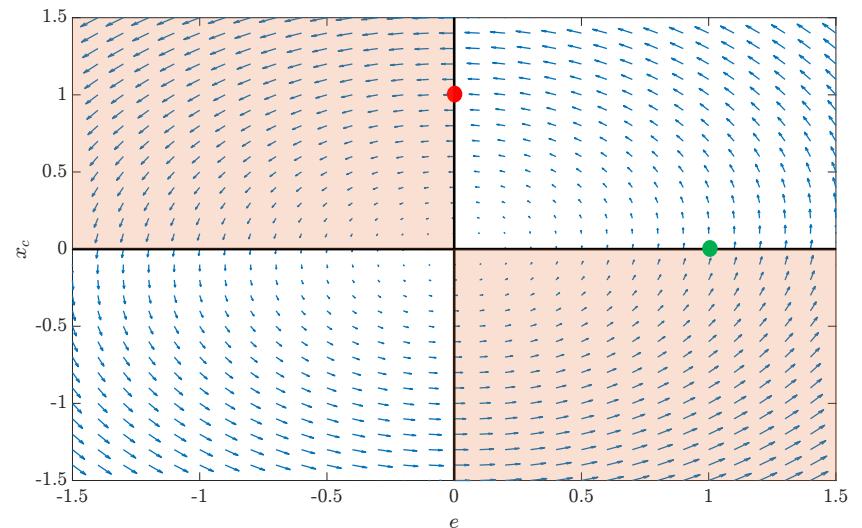
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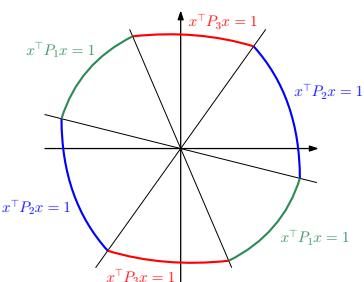
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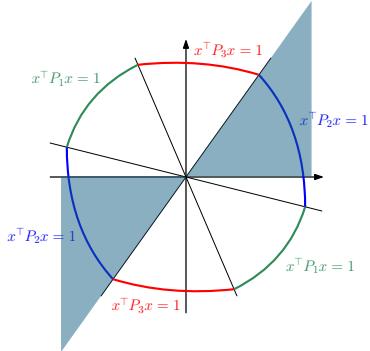


**Piecewise-quadratic  
(max-of-quadratics)  
functions!**



# Numerical sufficient conditions

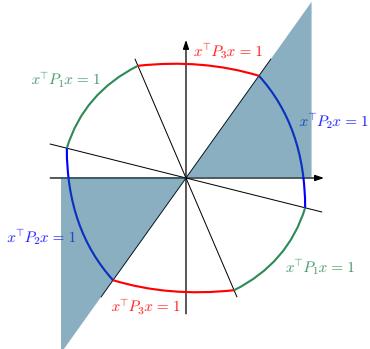
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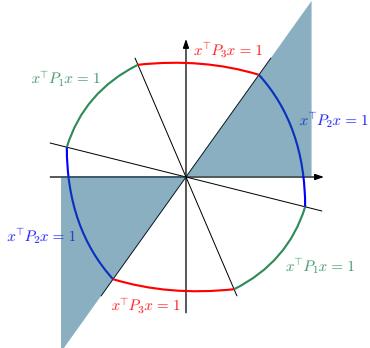


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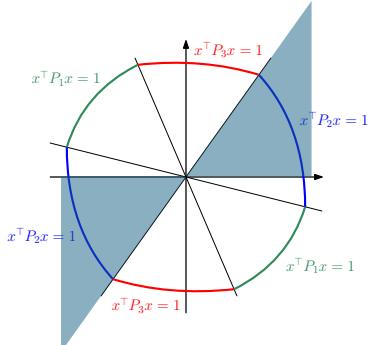
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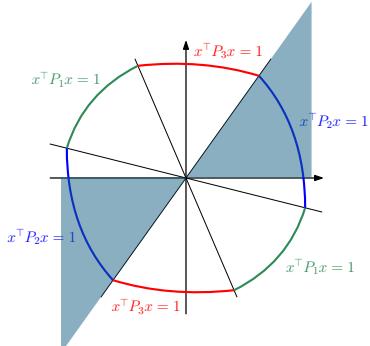
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S-procedure

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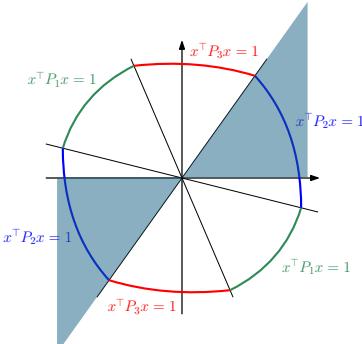
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S-procedure

Applied once: necessary and sufficient

$$x^\top Q x \geq 0 \implies x^\top S x \geq 0 \quad \text{iff} \quad \exists \mu > 0 : S - \mu Q \succeq 0$$

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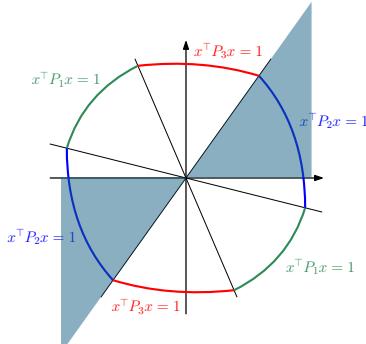
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$$x^\top Q_1 x \geq 0, \dots, x^\top Q_q x \geq 0 \implies x^\top Sx \geq 0$$

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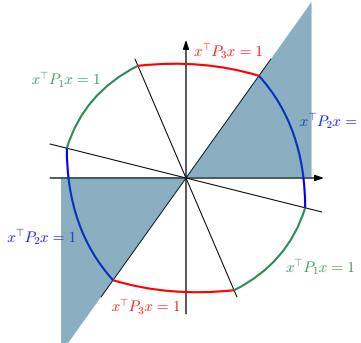
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Many numerical tests, none feasible



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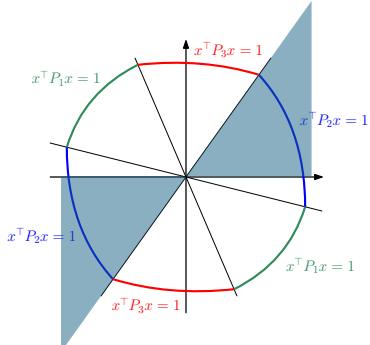
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Sum Of Squares (SOS)  
programming

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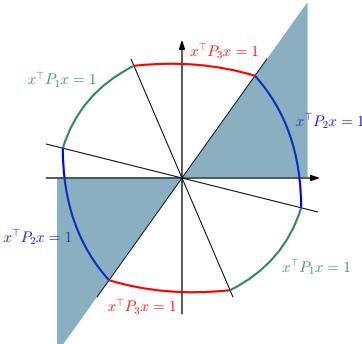
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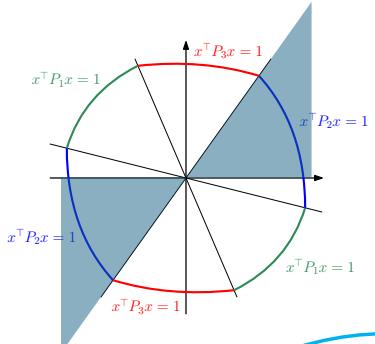
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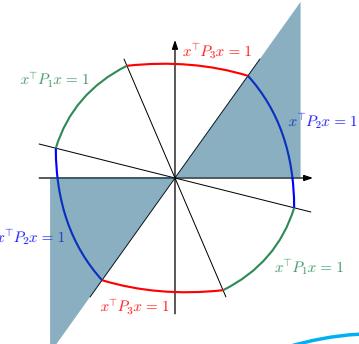
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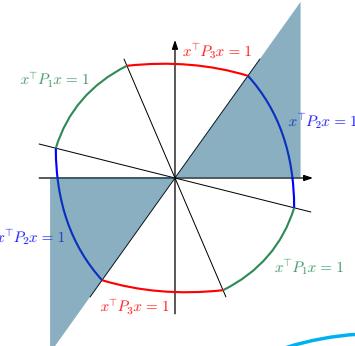
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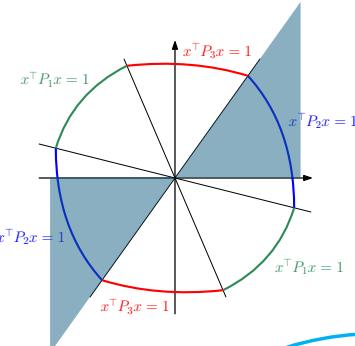
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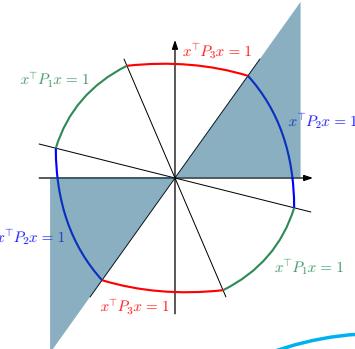
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Check only on  
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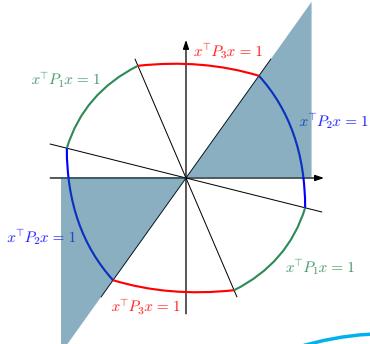
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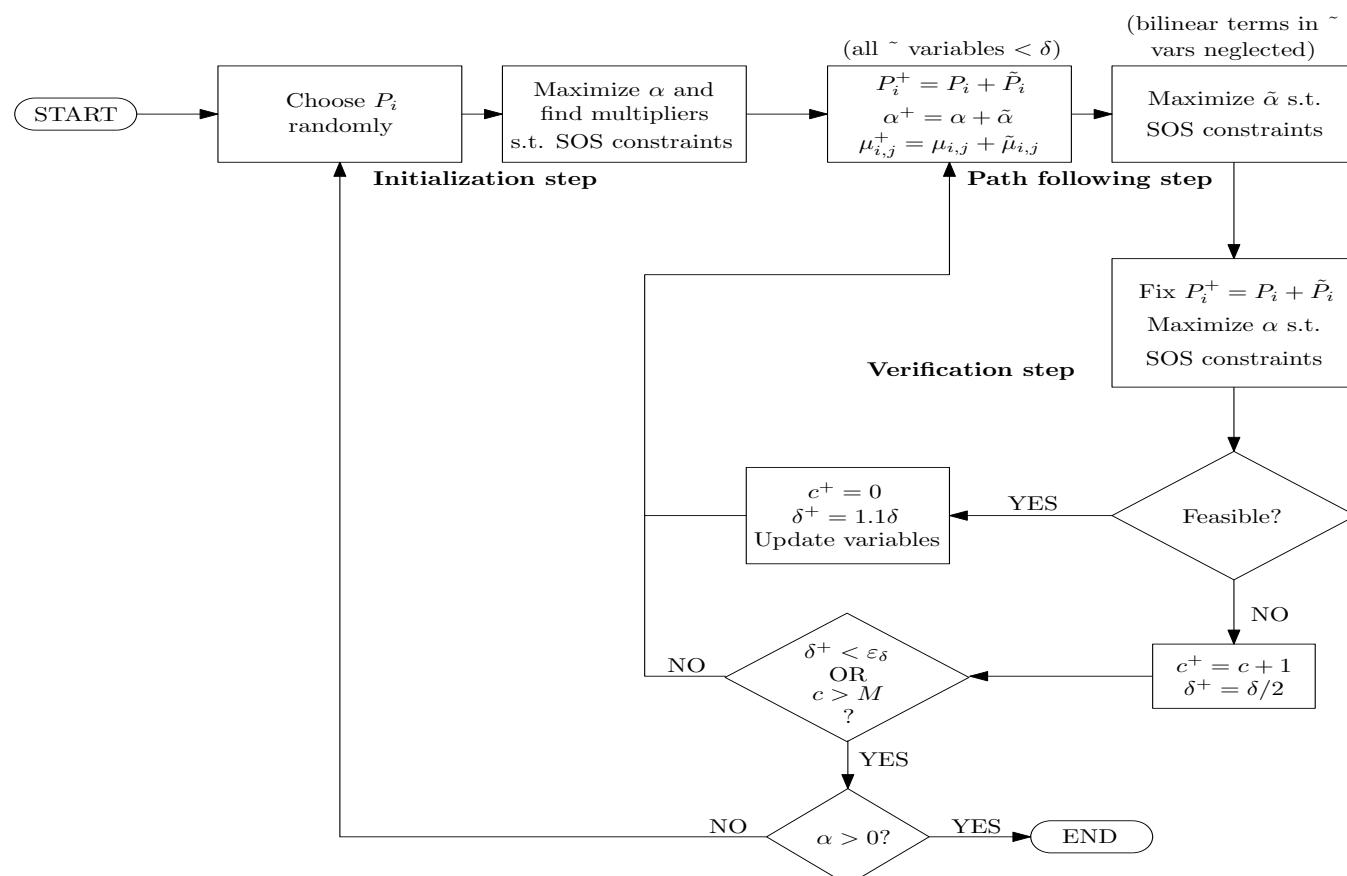
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We cannot optimize over  $P_i$  because  
this term would be bilinear!

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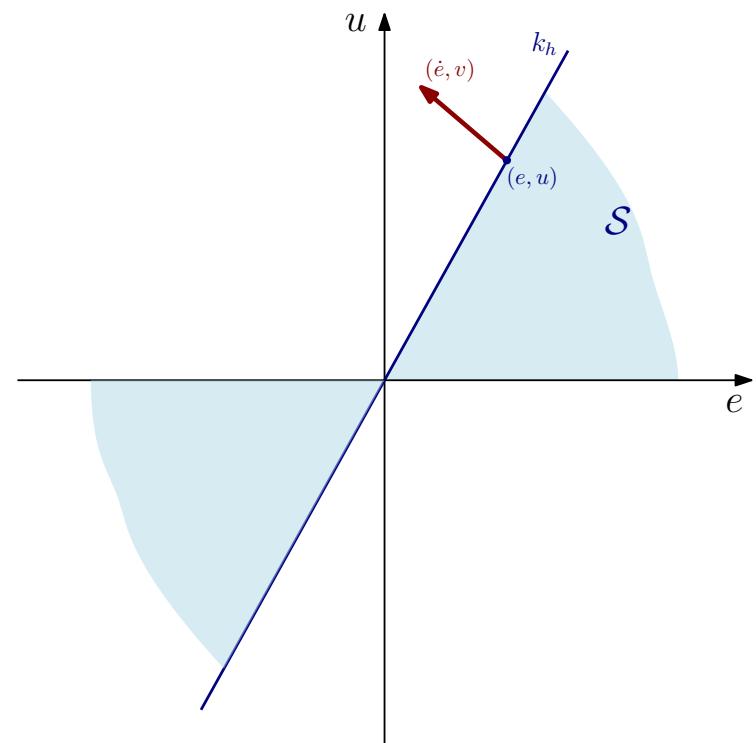
# Recursive algorithm for synthesis



<sup>[1]</sup> A. Hassibi, J. How, S. Boyd, “A path-following method for solving BMI problems in control”. *Proceedings of the American Control Conference*. 1999.

# To (soft-)reset or to project?

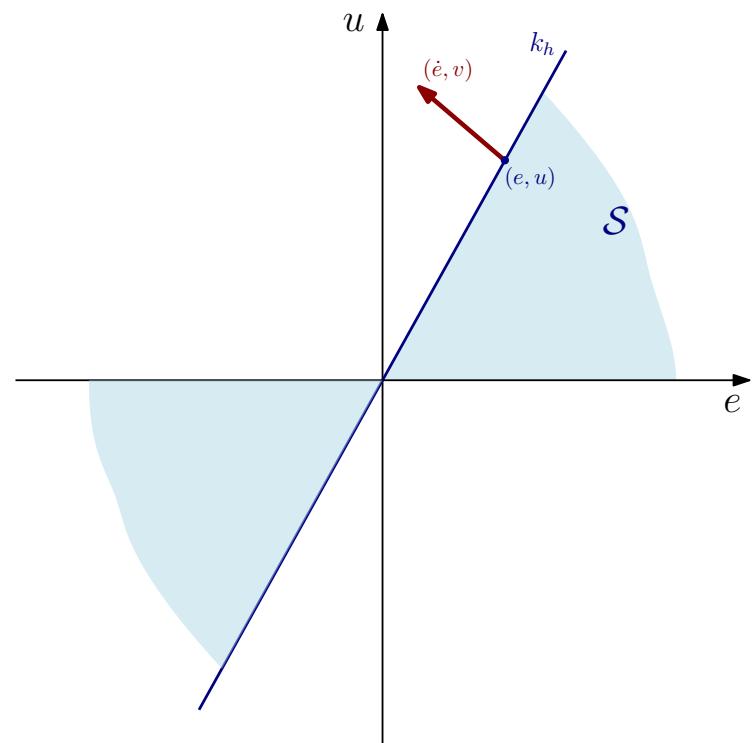
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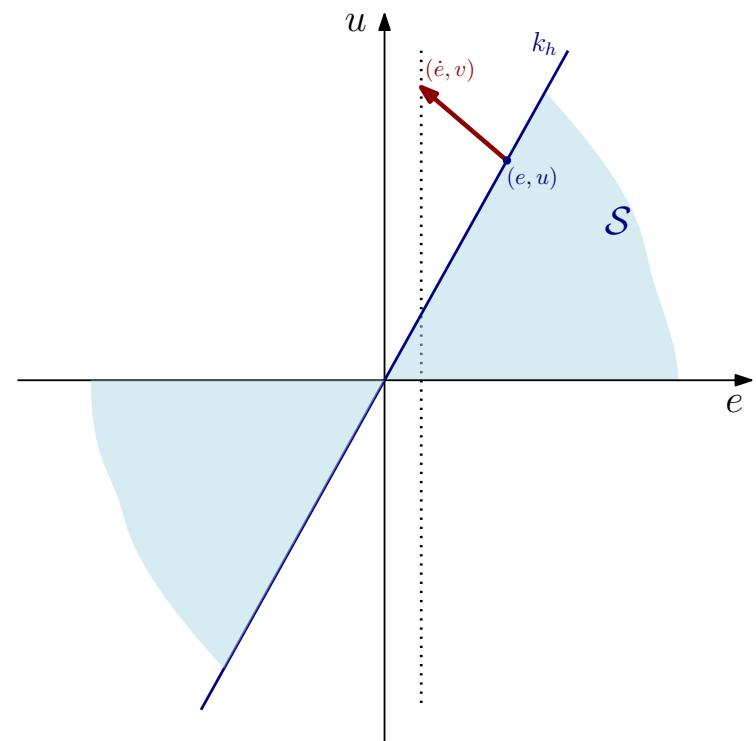
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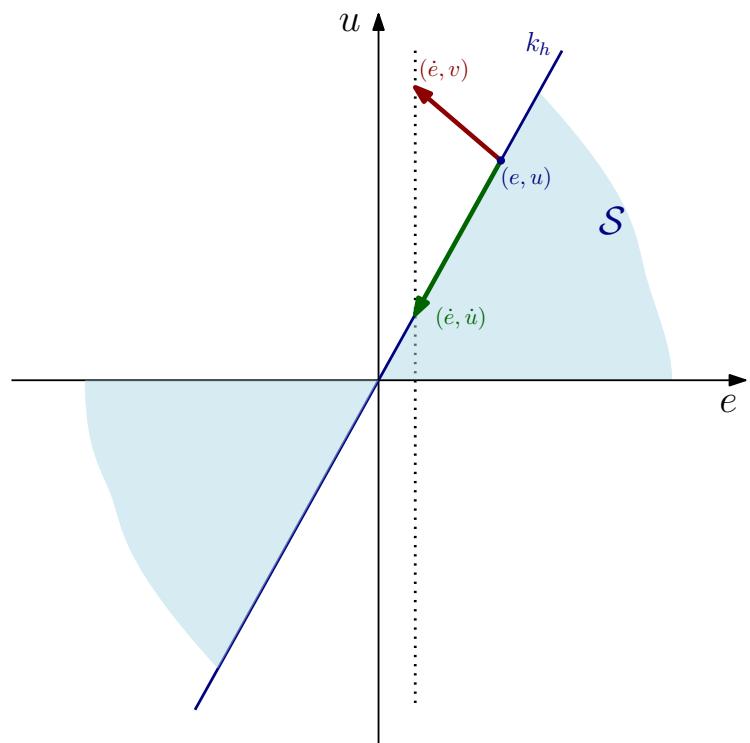
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[1] D.A. Deenen et al., "Projection-based integrators for improved motion control: formalization, well-posedness and stability of Hybrid Integrator-Gain Systems". *Automatica*. 2021.

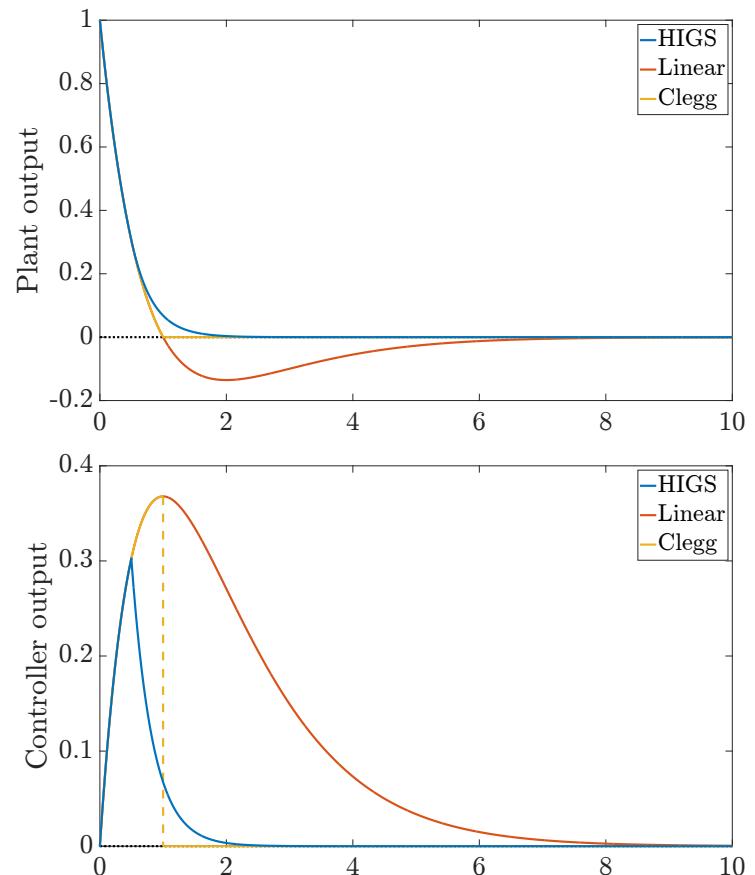
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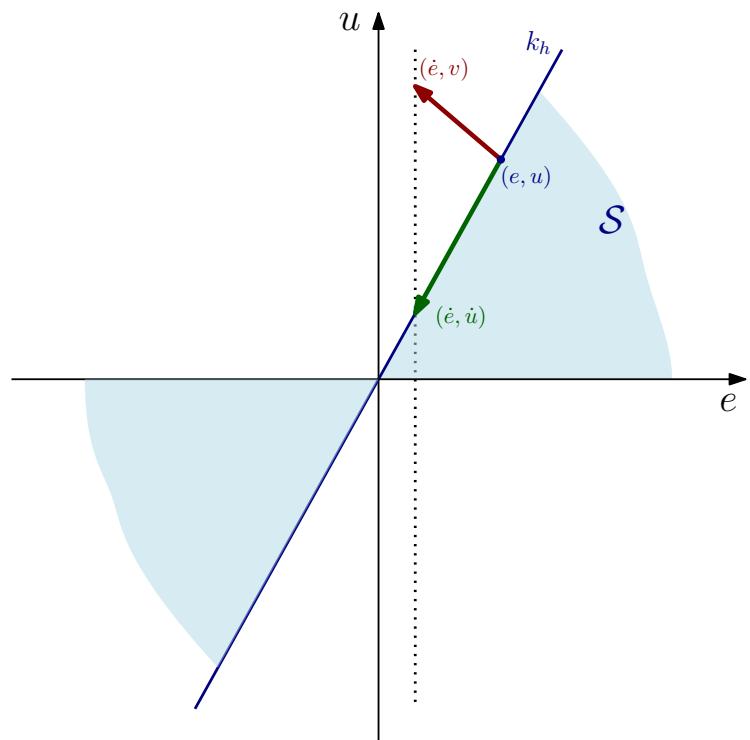
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Can be any “nominal” dynamics

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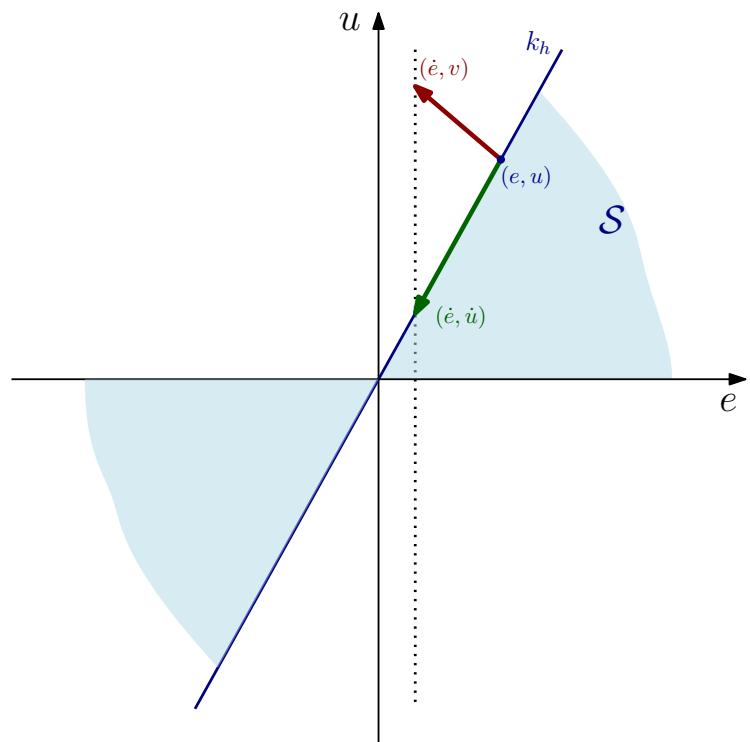
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$$\dot{u} = \begin{cases} \omega_h e, & (\omega_h e, \dot{e}) \in T_{\mathcal{S}}(e, u) \\ k_h \dot{e}, & (\omega_h e, \dot{e}) \notin T_{\mathcal{S}}(e, u) \end{cases}$$

First-Order Projection Elements (FOPE)

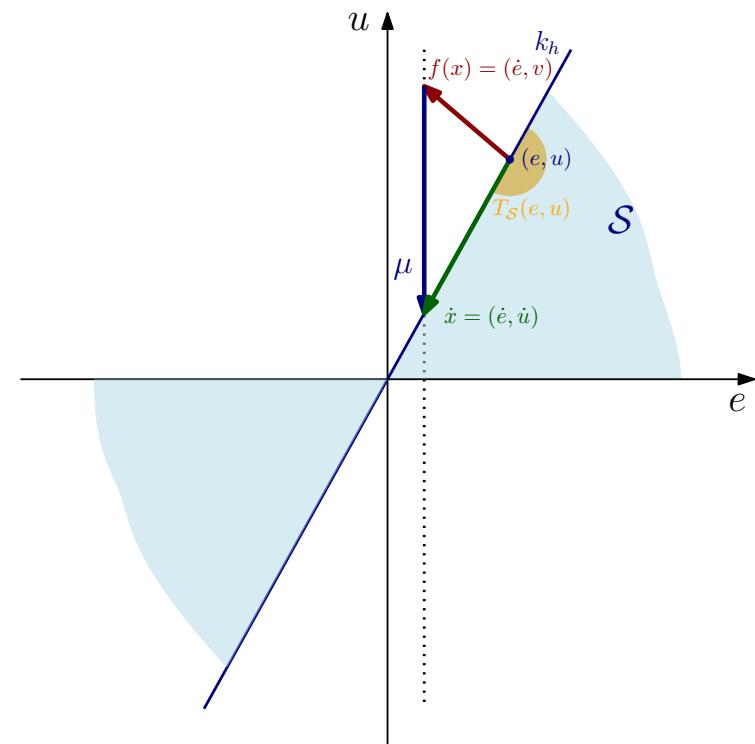
$$\dot{u} = \begin{cases} au + be, & (au + be, \dot{e}) \in T_{\mathcal{S}}(e, u) \\ k_h \dot{e}, & (au + be, \dot{e}) \notin T_{\mathcal{S}}(e, u) \end{cases}$$



[1] D.A. Deenen et al., "Projection-based integrators for improved motion control: formalization, well-posedness and stability of Hybrid Integrator-Gain Systems". *Automatica*. 2021.

# Analysis is not trivial

(1) The set  $\mathcal{S}$  is **not convex**!

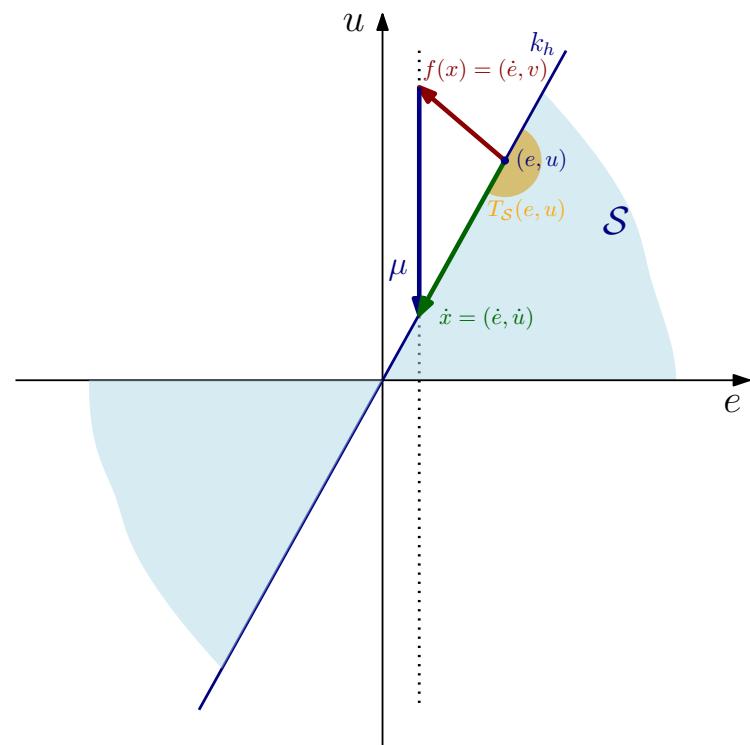


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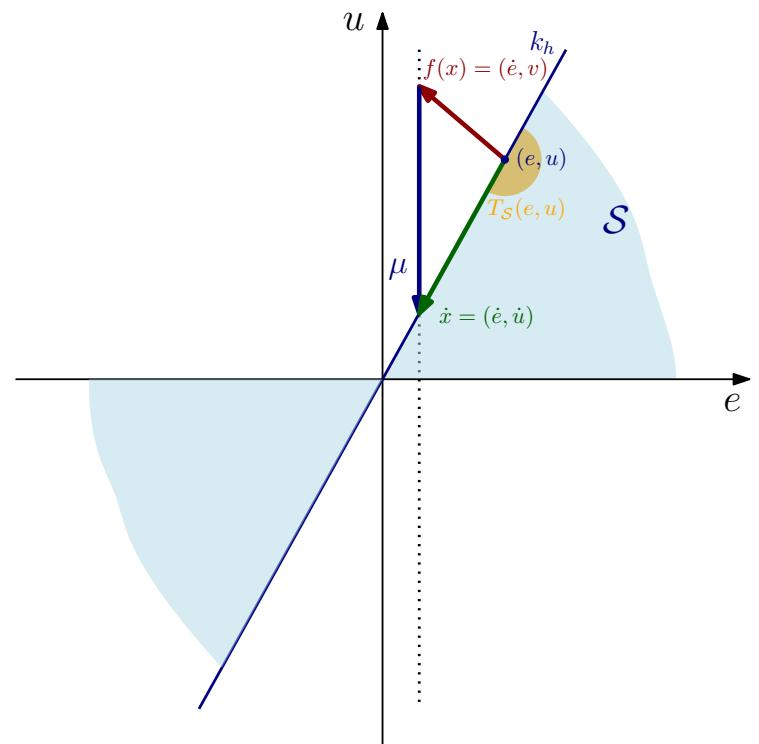
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# A bunch of cool properties

Solutions to HIGS exist and **are complete** [1]

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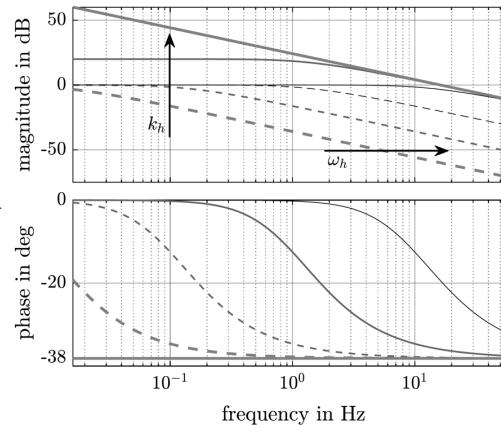
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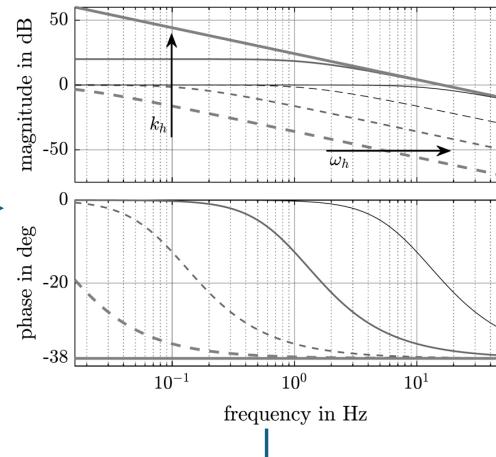
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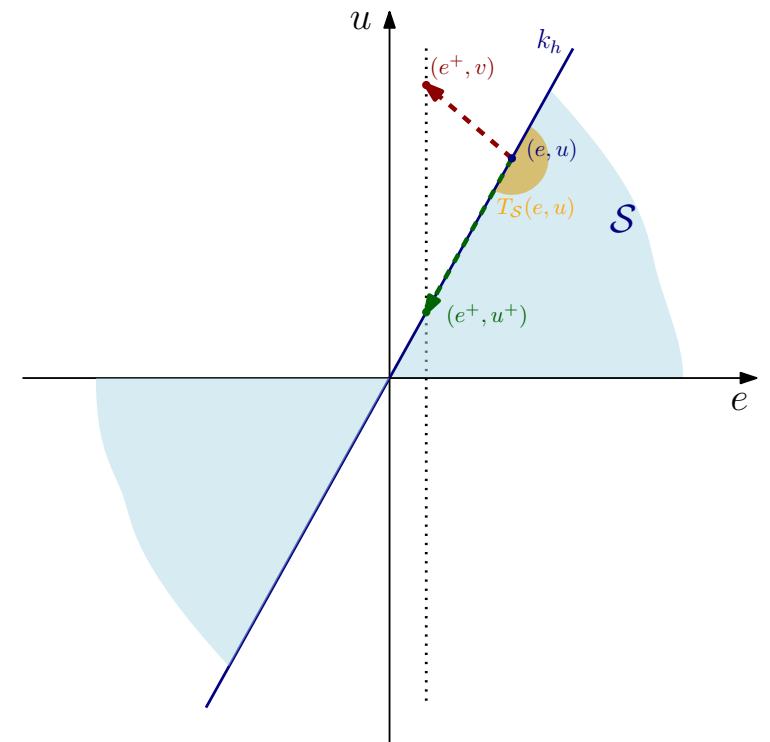
HIGS improves performance  
w.r.t. linear integrators<sup>[2]</sup>  
(phase lag reduced to 38.15°)



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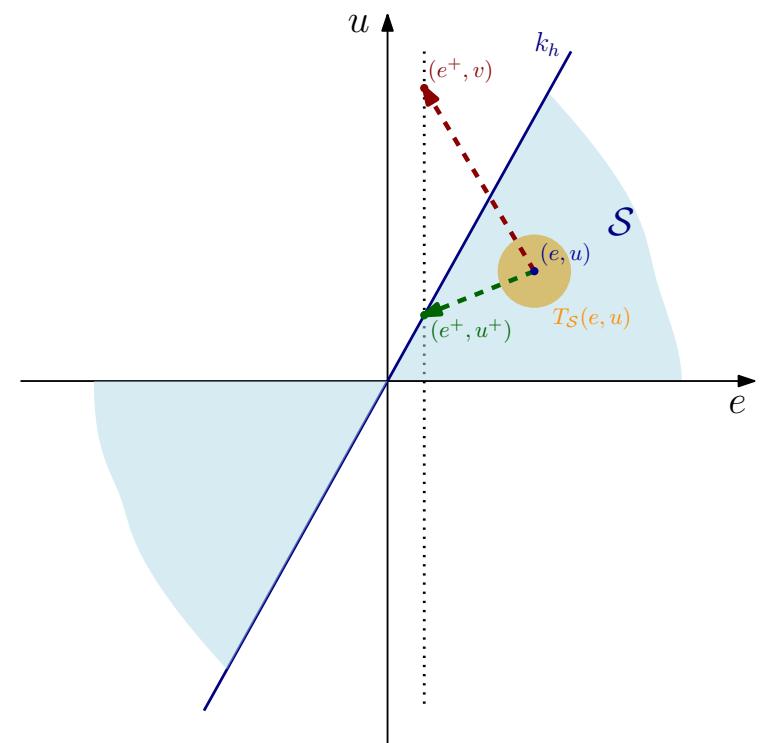
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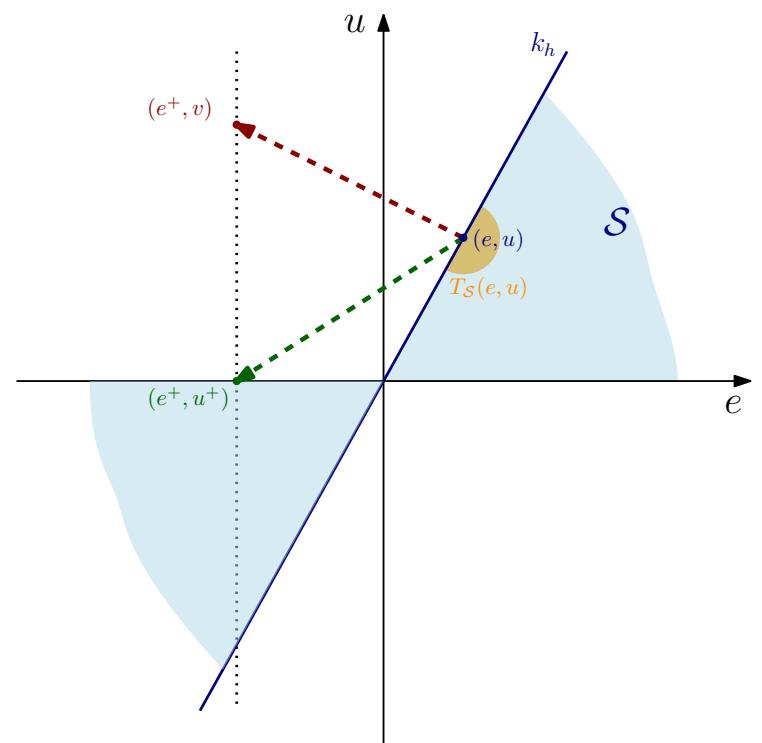
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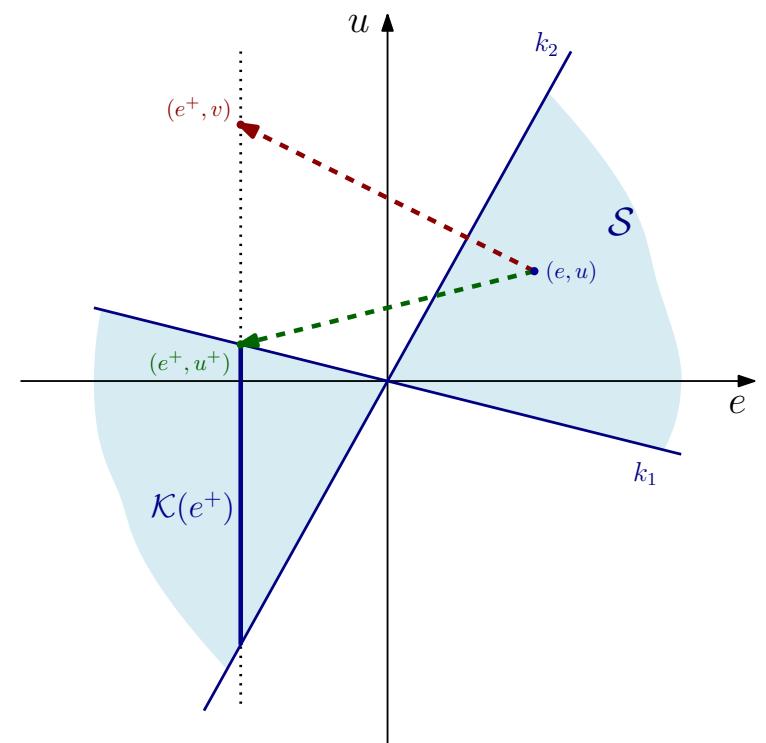
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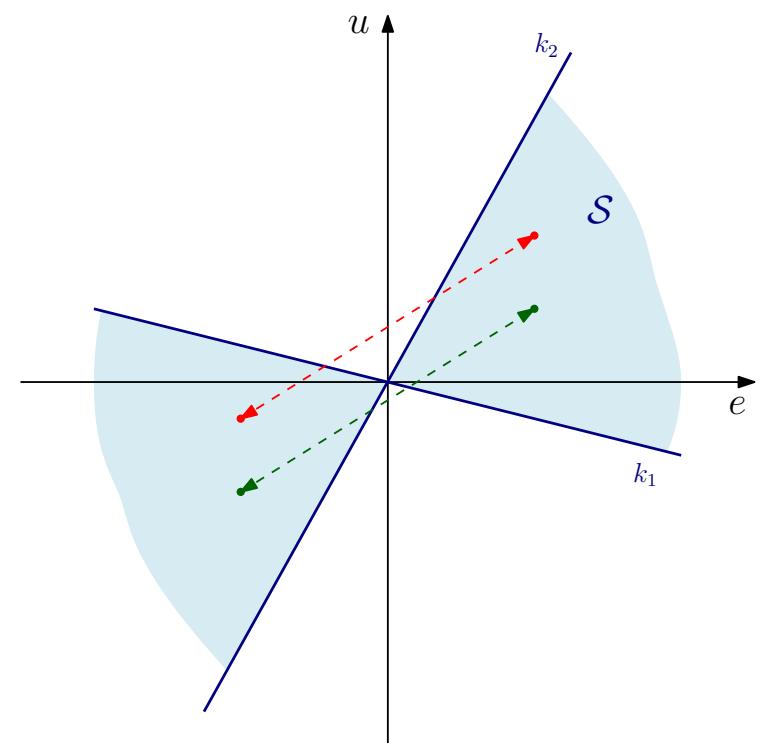
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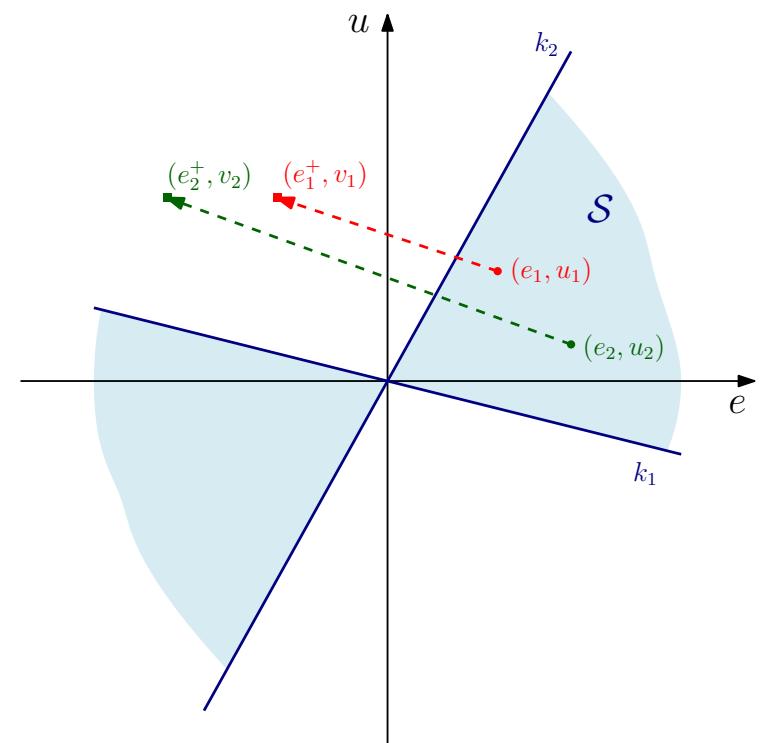
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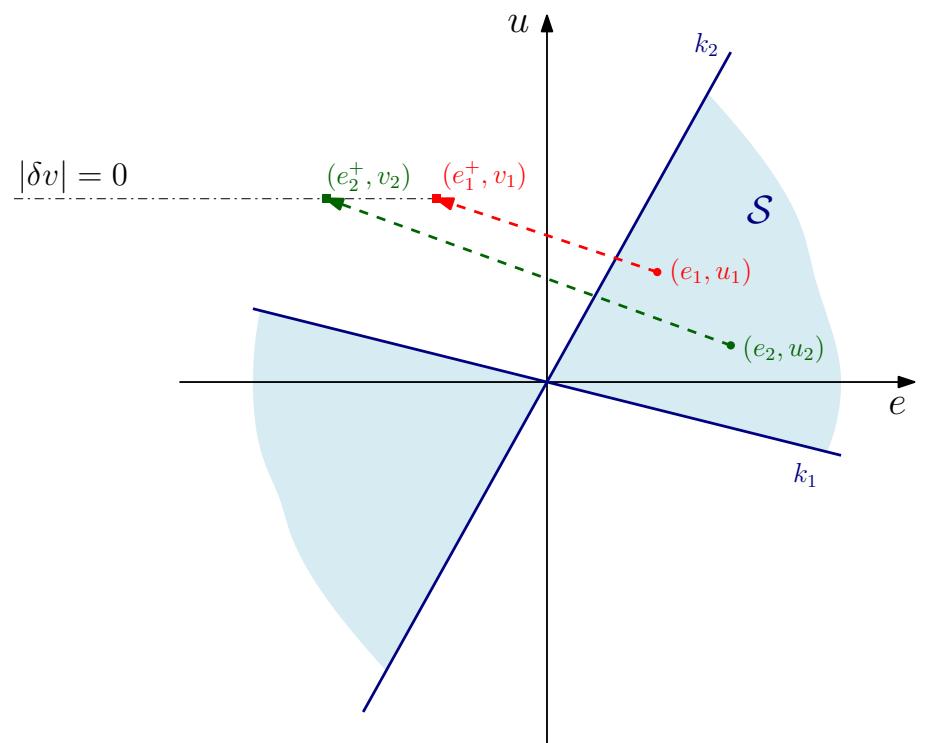
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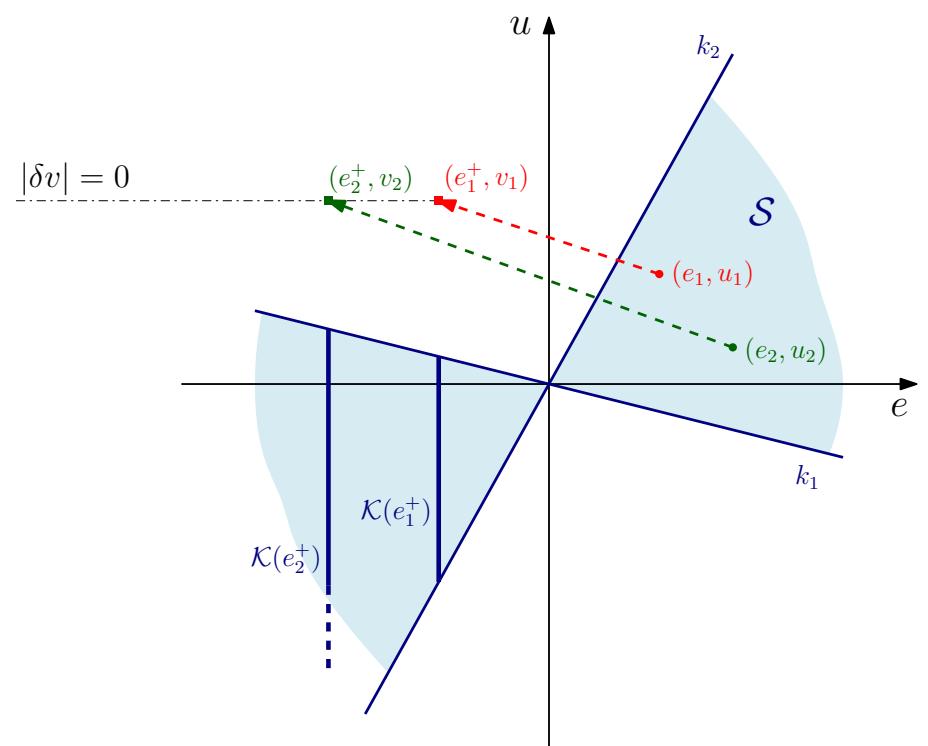
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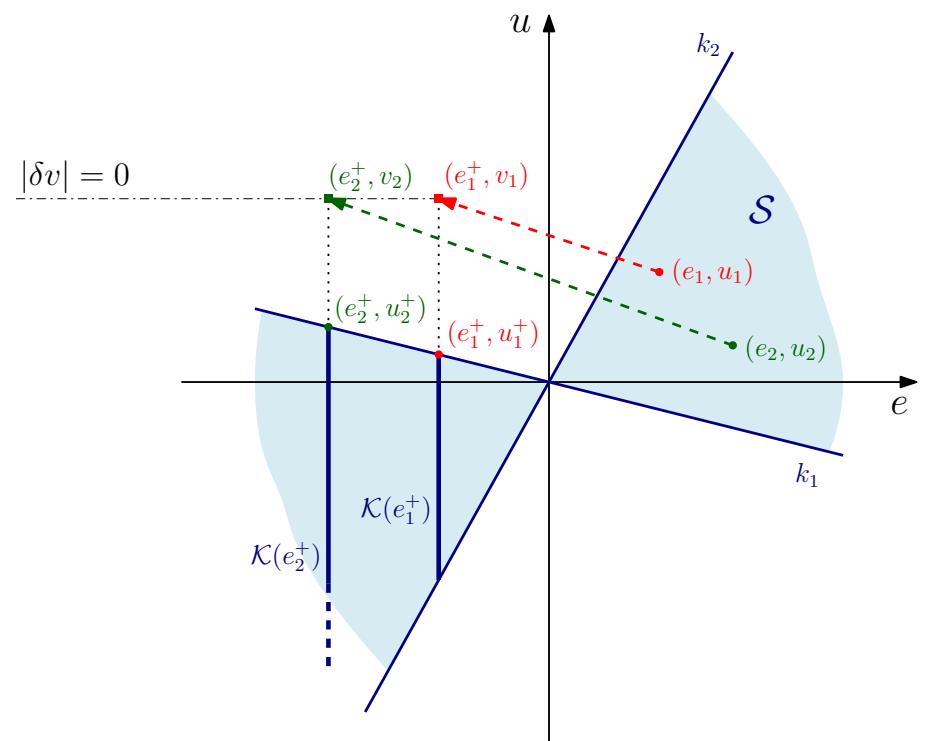
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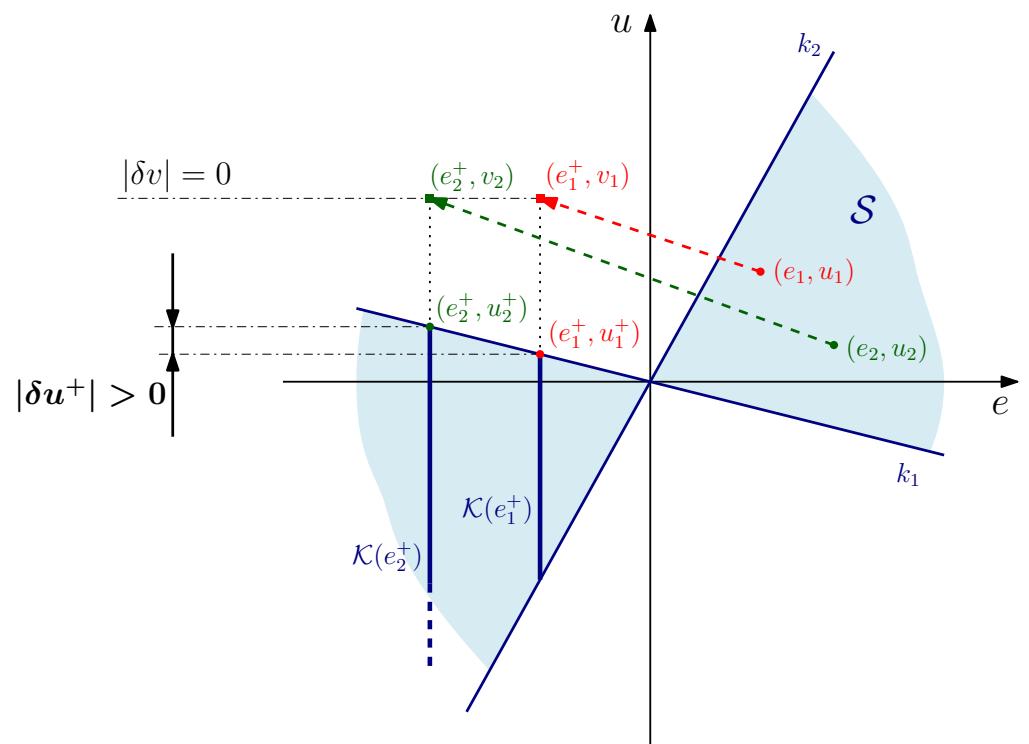
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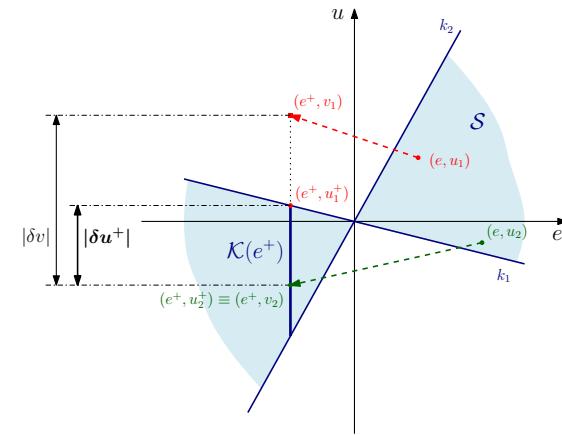
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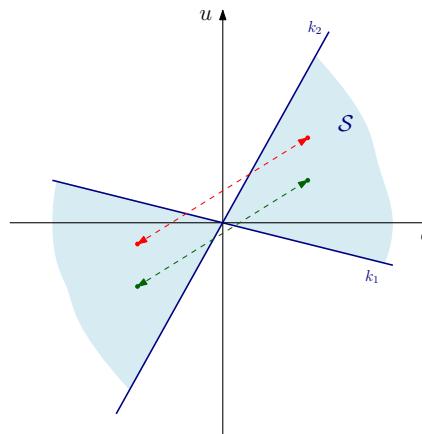
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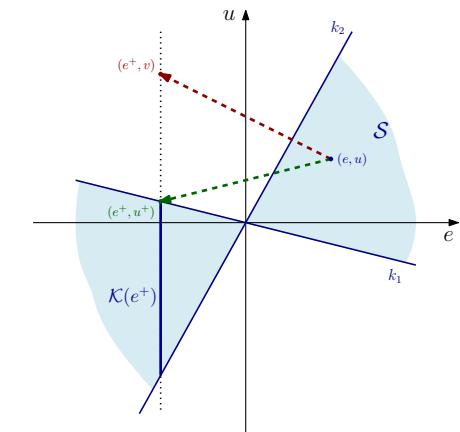
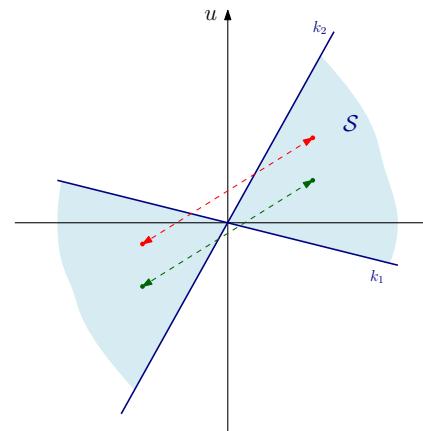
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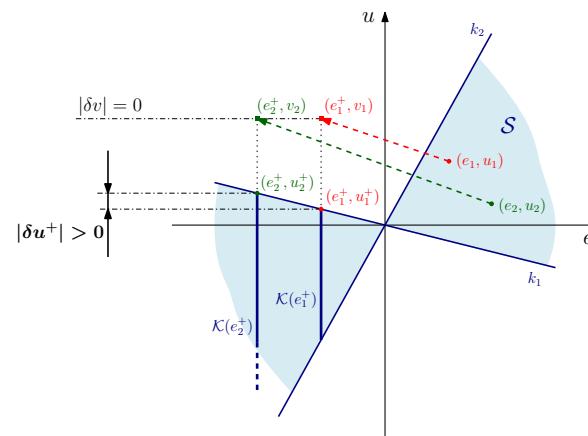
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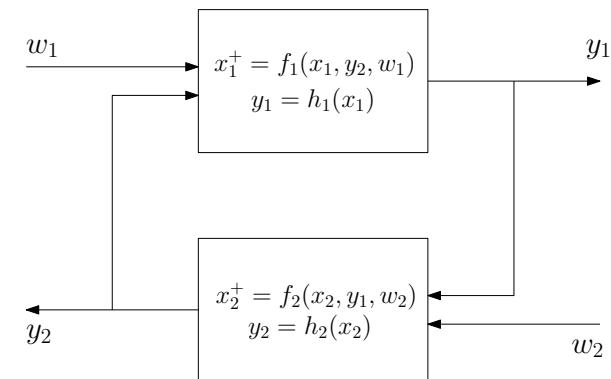
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# More general analysis: ePDS, and connection to regular PDS

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- First result: sufficient conditions for existence and completeness of solutions
- Second result: a norm matrix  $P(x)$  for equivalence can always be defined
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## Application to feedback optimization with state constraints

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- Modelling of partially elastic impacts as a “hybrid singular perturbation” of inelastic impacts, for control purposes?

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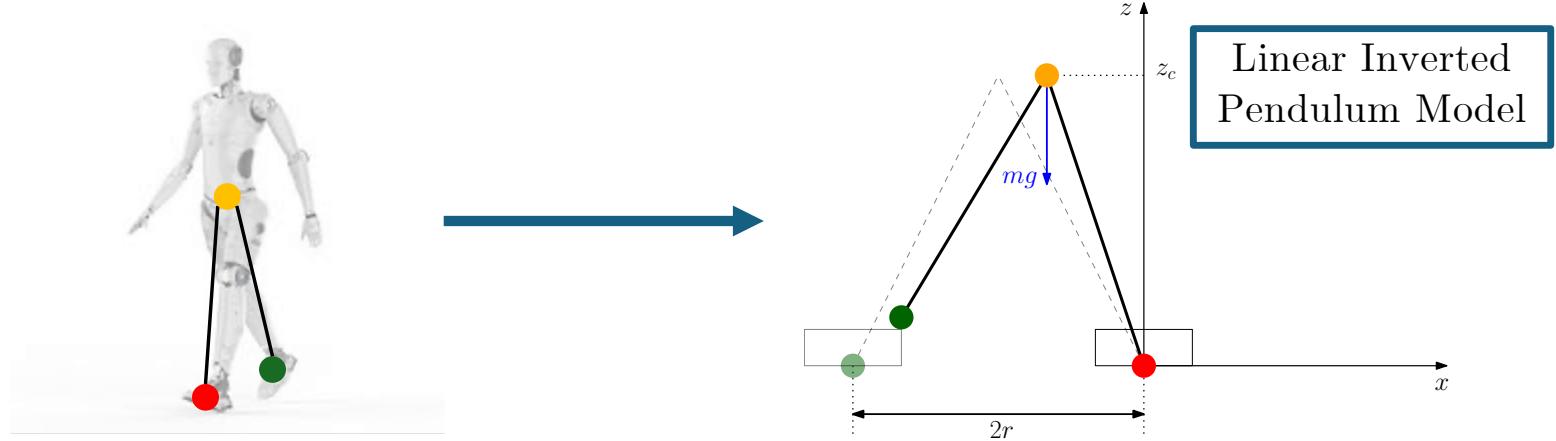
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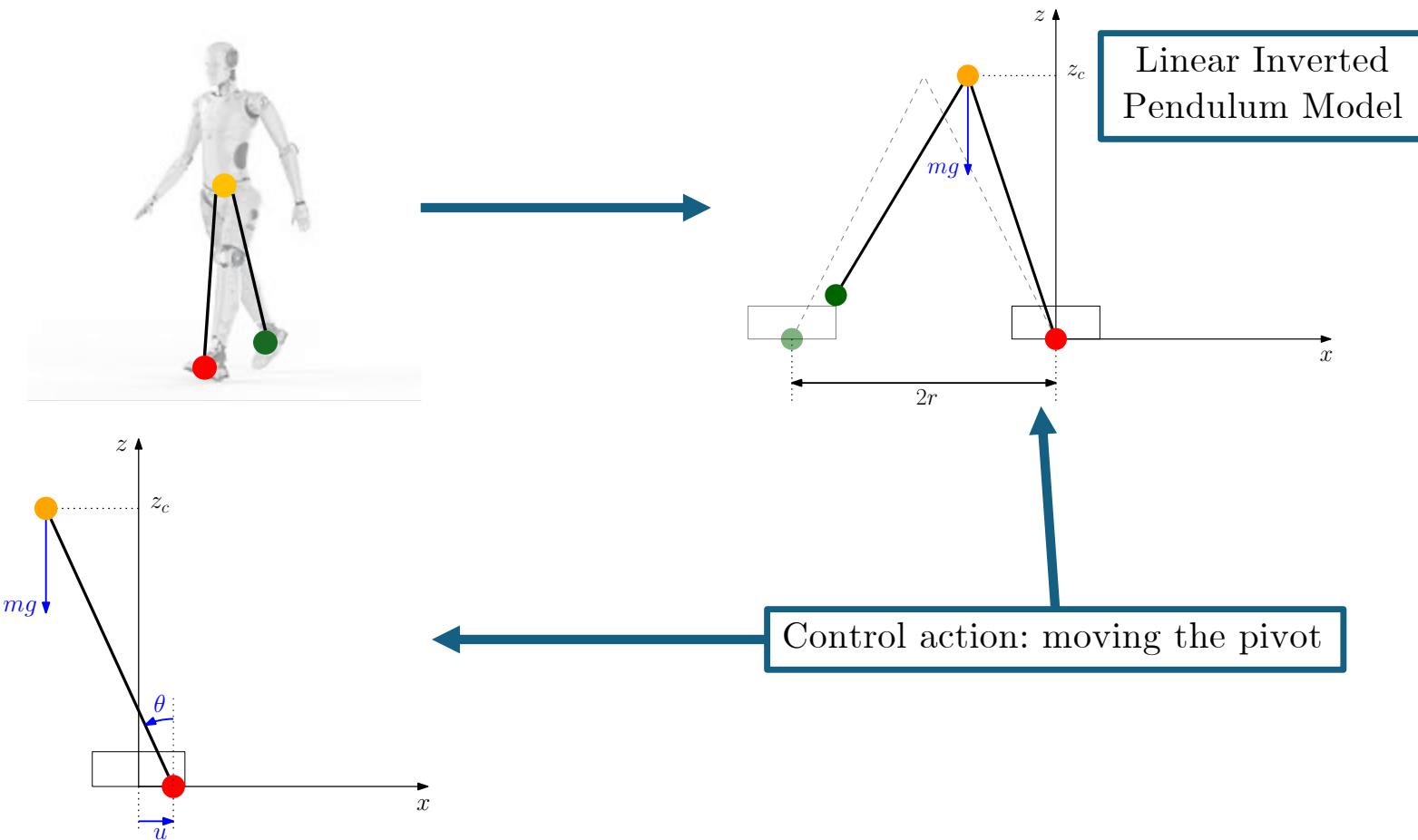
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- Distributed observers with different timescales (sampled-data systems with hybrid systems formalism)

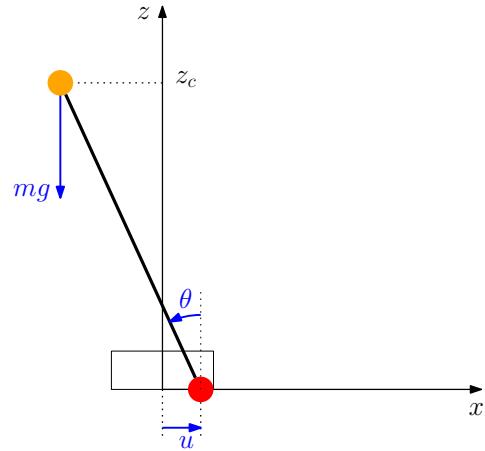
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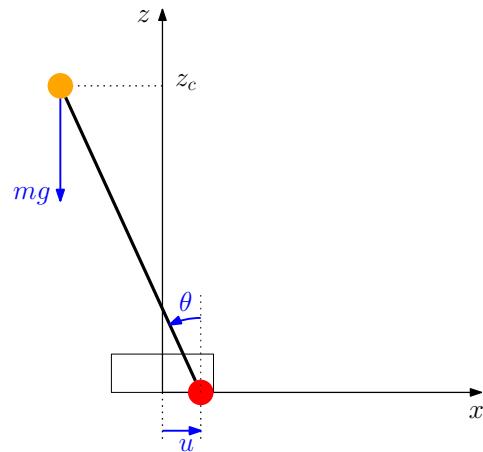
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$$\ddot{\theta} = -\frac{g}{z_c} \sin \theta = -\omega^2 \sin \theta$$

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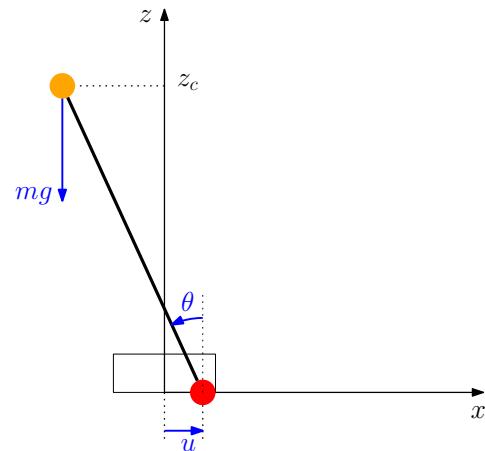
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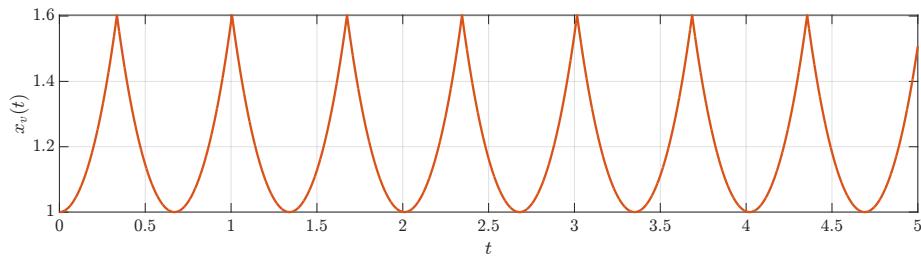
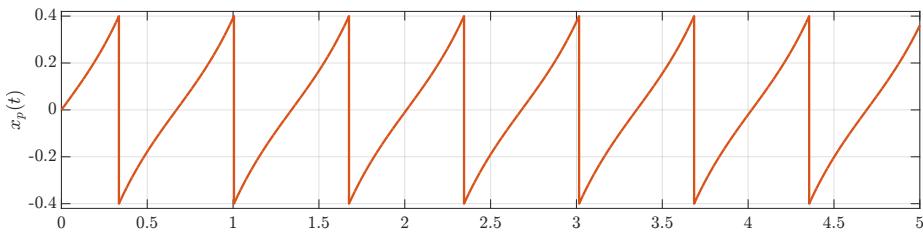
Hybrid dynamical system!

$$x = \begin{bmatrix} x_p \\ x_v \end{bmatrix} \rightarrow \begin{cases} \dot{x} = \begin{bmatrix} 0 & 1 \\ \omega^2 & 0 \end{bmatrix} x + \begin{bmatrix} 0 \\ -\omega^2 \end{bmatrix} u, & x_p \in [-r, r] \\ x^+ = x - \begin{bmatrix} 2r \\ 0 \end{bmatrix}, & x_p = r \end{cases}$$

# Bipedal gait stabilization using reference spreading

The hybrid LIPM has a periodic trajectory (no inputs)

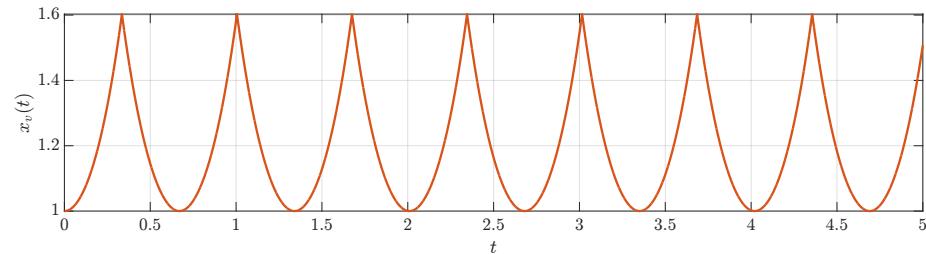
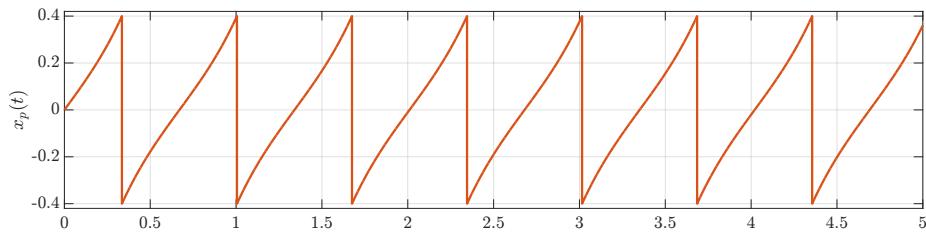
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First idea:

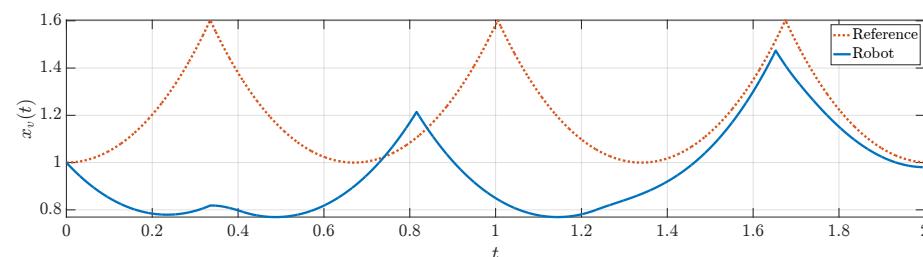
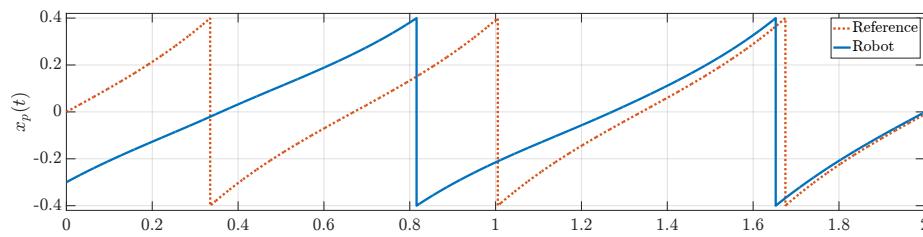
$$e = x - x_{\text{ref}}$$

Issues when robot and reference are **standing on different feet**

# Bipedal gait stabilization using reference spreading

The hybrid LIPM has a periodic trajectory (no inputs)

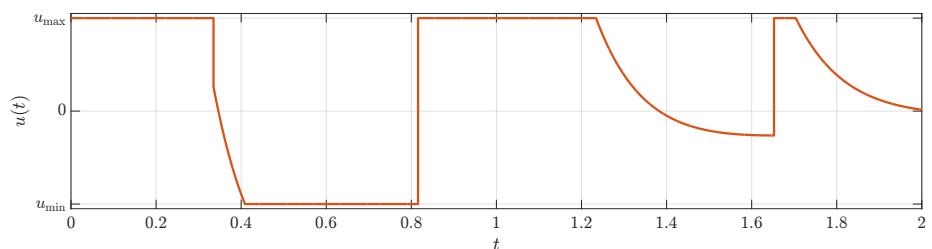
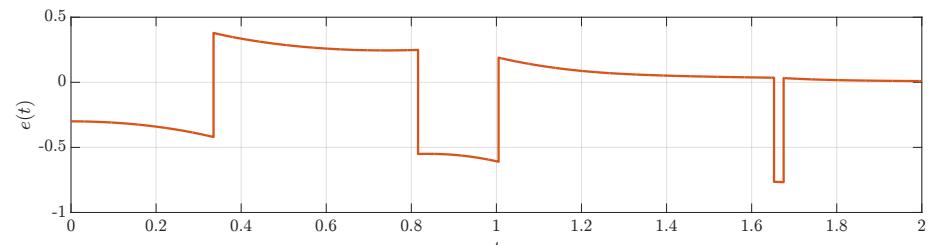
Goal: stabilize the gait on the periodic reference



First idea:

$$e = x - x_{\text{ref}}$$

Issues when robot and reference are **standing on different feet**



# Bipedal gait stabilization using reference spreading

New idea:

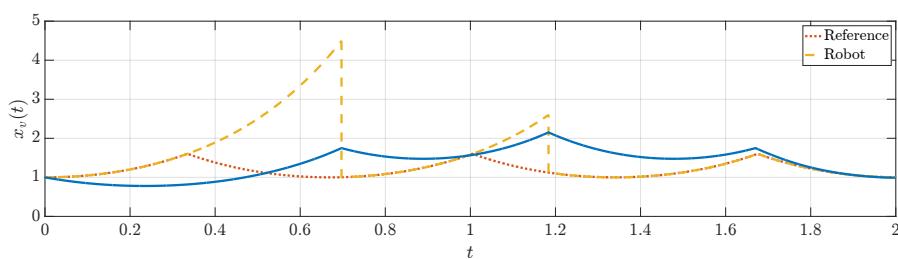
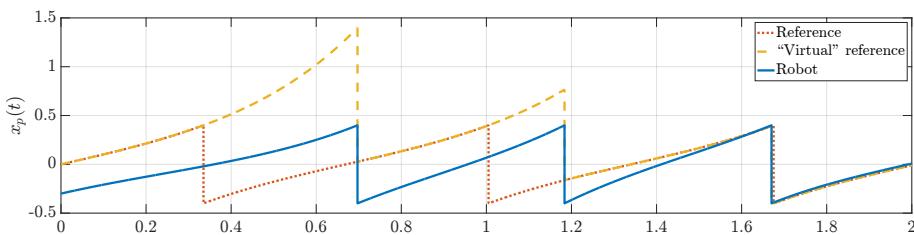
- Introduce a timer state to parametrize the reference
  - Reset the timer when the robot changes foot

$$\begin{cases} \dot{\tau} = 1, & x_p \in [-r, r] \\ \tau^+ = \tau - T, & x_p = r \end{cases}$$

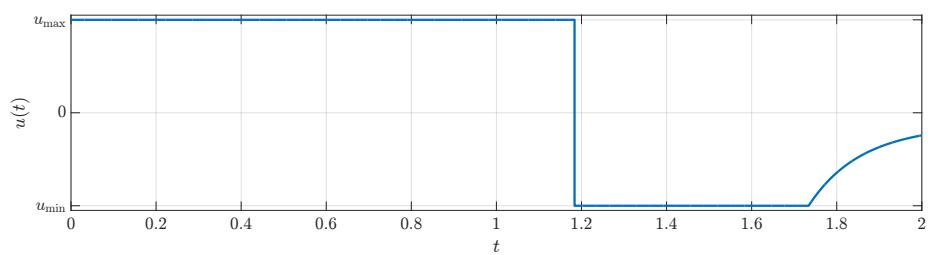
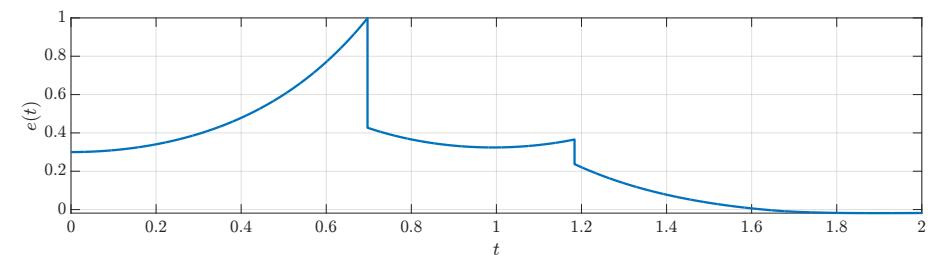
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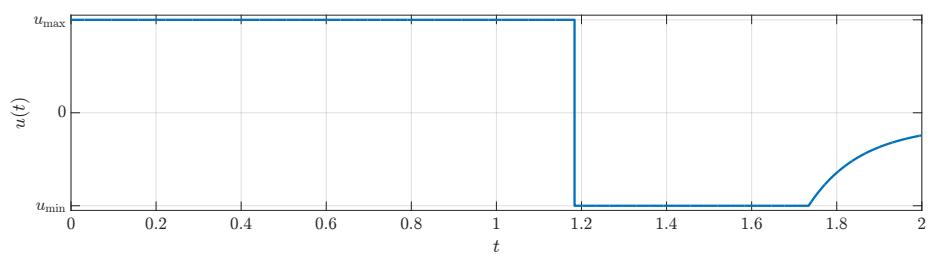
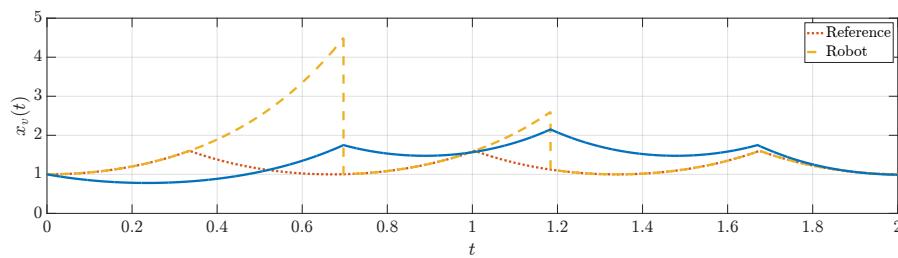
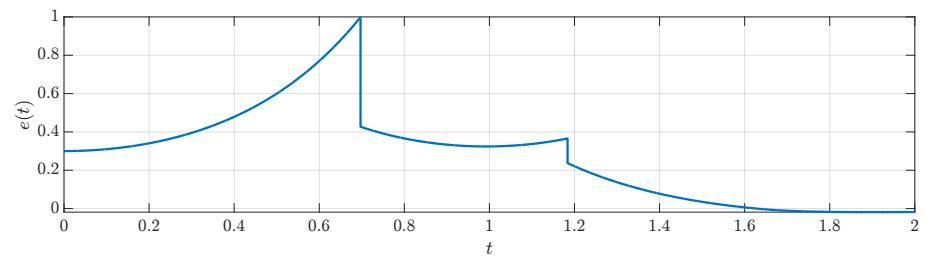
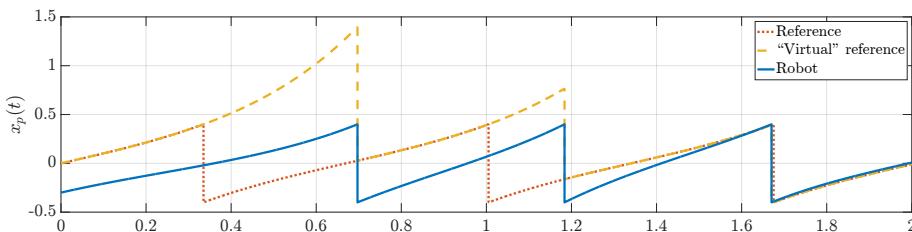


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With such a “regular” error trajectory, the control synthesis problem becomes easier! We defined **LMIs** to synthesize a stabilizing saturated full-state feedback, and we identified necessary and sufficient conditions for feasibility