# DRS project: kinematics push up mechanism



# **Initial setup**

```
> restart: with (LinearAlgebra): with (MBSymba_r6): with (plots): with (Optimization):
```

# **Utility functions**

```
> getCoM:=proc(matrix_point)
    local i,n,xSum,ySum:
    xSum:=0: ySum:=0:
    n:=ColumnDimension(matrix_point):
    for i from 1 to n do
        xSum:=xSum+matrix_point[1,i]:
        ySum:=ySum+matrix_point[2,i]:
    end do:
    xSum/n,ySum/n:
end proc:
```

# Data and shapes

## Shapes

```
> SMS:=[400,250]: # small plot size
> main wing matrix point := <
       \overline{<}0.29\overline{0}00000,
                          0.02281140,
                                             0.,
                                                        1.>|
       <0.27550000,
                          0.01988240,
                                              0.,
                                                        1.>|
       <0.26100000,
                          0.01696500,
                                                        1.>1
       <0.23200000,
                          0.01209300,
                                                        1.>|
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                                                        1.>
                                                        1.>|
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                                                        1.>|
```

```
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                                                       1.>
> flap wing matrix point := <
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                                                       1.>|
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```

```
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      <0.09196752,
                       -0.00295620,
                                           0.,
                                                     1.>
  >:
> box_points_old := [[-0.020, 0.055], [0, 0.065], [0.100, 0.065],
  [0.\overline{100}, 0.\overline{065}], [0.080, 0.065], [0.080, 0], [0.050, 0], [0.050,
  0.035], [0, 0.035], [-0.020, 0.045]]:
> pylon points := [[0.260,0],[0.260,0.050],[0.280,0.050],[0.280,0]]
Data
> pre_fixed data := [
      # FIA regulation
      HEIGHT
                  = 0.220000,
      WIDTH
                   = 0.350000,
      min dist
                   = 0.010000,
      max dist
                   = 0.050000,
       # fixed points
                   = 0.280000,
      хA
                   = 0.000000,
      yА
      xD
                   = 0.335000,
                   = 0.154000,
      уD
                   = 0.280000,
      хR
                   = 0.022300,
      уR
      # fixed lengths
      L1
                  = 0.016000,
      L2
                   = 0.050000,
      L3
                   = 0.100000,
      L wing
                   = 0.120000,
      W wing
                   = 1010.000,
      d wing
                   = 0.0060,
                                       # main wing offset
                                       # allowed by the FIA regulation
      d tip
                   = 0.0100,
      # fixed angles
      gamma
                   = 5*Pi/180,
                                       # main wing inclination
       # manouvre times
      T opening = 0.010,
```

```
T still = 0.0300,
      T closing = 0.0100,
      # masses
     m__pist = 0.0800,
m_link = 0.0375,
m_wing = 2.0000,
                                     # L2*rho
      # physics constants
      rho steel = 0.75,
                                    # linear density of a steel bar
  with radious 1cm
                  = 9.81,
      # external forces (values from paper)
      F drag closed = 145.51319,
      F drag open = 051.32626,
      F down closed = 819.11694,
      F down open = 745.62411
  1:
> data := pre fixed data union evalf(subs(pre fixed data,[
          Iz_pist = 0,
          Iz link = m link*(L2^2)/12,
          Iz wing = m = m \cdot (L \cdot wing)/3
      1)):
```

### **Kinematics**

## Reference frames and points

```
Ground Points
> PA := make POINT(ground, xA, yA, 0):
> PD := make POINT(ground,xD,yD,0):
Reference frames
> RF0 := translate(xA,yA,0):
> RF0a := RF0.translate(0,s(t)+L1,0):
> RF1 := RF0.translate(0,s(t)+L1,0).rotate('Z',psi1(t)):
> RF2 := RF1.translate(0,L2,0):
> RF3 := translate(xD,yD,0).rotate('Z', psi3(t)):
> RF flap wing := RF3.translate(-L wing+d tip,0,0):
> RF main wing := translate(d wing, 0, 0).rotate('Z',gamma):
Support points
\gt PP := make POINT(RF0,0,s(t),0):
> PB := origin(RF1):
> PC := origin(RF2):
PC 3 := make POINT(RF3,-L3,0,0):
The following points are used to calculate the distance
- PT: point on the tip of the flap wing
- PR: point of the main wing used as reference for the open/close distance
> PT := origin(RF_flap_wing):
> PR := make POINT(RF main wing,xR,yR,0):
Wings points (w.r.t. their reference frame)
```

```
> flap wing points := [seq(convert((RF flap wing.
   flap wing matrix point) [1..2,i], list), i=1.. ColumnDimension
   (flap wing matrix point))]:
> main wing points := [seq(convert((RF main wing.
   main wing matrix point) [1..2,i], list), i=1..ColumnDimension
   (main wing matrix point))]:
CoM
Body 1
> G1 := make POINT(RF0a,0,-L1*4/5,0):
> G2 := make POINT(RF1,0,L2/2,0):
Body 3
> xG3,yG3 := evalf(getCoM(flap wing matrix point)):
G3 := make POINT(RF flap wing,xG3,yG3,0):
Constraints
> vCC := join_points(PC, PC_3):
   Phi := [comp_X(vCC,ground), comp Y(vCC,ground)]: <%>;
                    \sin(\psi l(t)) L2 - \cos(\psi 3(t)) L3 - xA + xD
                                                                           (2.2.1)
               -\cos(\psi l(t)) L2 - \sin(\psi 3(t)) L3 - L1 - s(t) - yA + yD
Position analysis
Direct kinematic
> qI := [s(t)]:
   qD := [psi1(t), psi3(t)]:
   qvars := qI union qD;
                         qvars := [s(t), \psi l(t), \psi 3(t)]
                                                                          (2.3.1.1)
> kin sols := solve(Phi,qD,explicit=true):
   nops(kin sols);
                                                                          (2.3.1.2)
> num kin sols := subs(data,kin sols):
> "solution 1" = evalf(subs(s(t)=0,num kin sols[1]));
   "solution 2" = evalf(subs(s(t)=0,num_kin_sols[2]));
            "solution 1" = \left[ \psi I(t) = -0.1824644031, \psi 3(t) = 1.093620968 \right]
            "solution 2" = \left[ \psi I(t) = -0.5760483505, \psi 3(t) = 1.289458931 \right]
                                                                          (2.3.1.3)
Our case is modeled by the third one
> kin sol := kin sols[1]:
Jacobian matrices
With s(t) as independent variable
> JPhiD:=jacobianF(Phi,qD):
   JPhiI:=jacobianF(Phi,qI):
Singular configurations
> SCs:=evalf(solve(subs(data,Phi union [Determinant(JPhiD)=0]),
   qvars,explicit=true)): <%>;
```

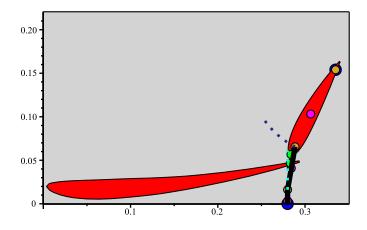
(2.331)

```
[[s(t) = 0.1380000000 - 0.02291287847 \text{ I}, \psi I(t) = 1.570796327 + 0.4435682544 \text{ I}, \psi 3(t)] (2.3.3.1)
    = 0.4435682544 I],
    [s(t) = 0.1380000000 + 0.02291287847 \text{ I}, \psi I(t) = 1.570796327 - 0.4435682544 \text{ I},
    \psi 3(t) = -0.4435682544 \text{ I}],
    [s(t) = 0.2775528574, \psi l(t) = -2.766169046, \psi l(t) = -1.195372719]],
    [s(t) = -0.001552857370, \psi I(t) = -0.3754236080, \psi I(t) = 1.195372719]]
Inverse Kinematics
Elongation "s(t)" of the piston to produce the opened and closed DRS configurations
> s limit:=rhs(SCs[3][1])-0.001;
                            s \ limit := 0.2765528574
                                                                              (2.3.4.1)
> notime := map(x->x=op(0,x),qvars);
                    notime := [s(t) = s, \psi l(t) = \psi l, \psi 3(t) = \psi 3]
                                                                              (2.3.4.2)
_Initial point (10 mm distance from fixed wing)
> s min := rhs(NLPSolve(subs(kin sol,notime,data,comp Y(PT,ground)-
   comp Y(PR,ground)-min dist)^2,s=0..s limit)[2][1]);
                         s \ min := 0.000198939129915359
                                                                              (2.3.4.3)
Final point (50 mm distance from fixed wing)
> s max := rhs(NLPSolve(subs(kin sol,notime,data,comp Y(PT,ground)-
   comp Y(PR, ground) -max dist)^2, s=0..s limit)[2][1]);
                          s \ max := 0.0460748980054946
                                                                              (2.3.4.4)
Tests to check distances
> "actual minimum distance" = evalf(subs(kin sol,s(t)=s min,data,
   comp Y(PT,ground)-comp Y(PR,ground))), # should be 10 mm
   "actual maximum distance" = evalf(subs(kin_sol,s(t)=s_max,data,
   comp Y(PT, ground) - comp Y(PR, ground))); # should be 50 mm
 "actual minimum distance" = 0.01000144013, "actual maximum distance" = 0.05000098592 (2.3.4.5)
> s range := s min..s max;
              s \ range := 0.000198939129915359...0.0460748980054946
                                                                              (2.3.4.6)
> s stroke := s max-s min;
                         s \ stroke := 0.0458759588755792
                                                                              (2.3.4.7)
Working space
> point B := subs(kin sol,data,s(t)=s,[comp_X(PB,ground),comp_Y(PB,
   qround)1):
   space B := [seq(point B,s=s range,0.001)]:
> point C := subs(kin sol,data,s(t)=s,[comp X(PC,ground),comp Y(PC,
   qround)1):
   space C := [seq(point C,s=s range,0.001)]:
Wing angle range (psi3(t))
> psi3 closed := evalf(subs(kin sol,data,s(t)=s min,psi3(t)))
   :"absolute wing open angle"=%,"deg"=%*180/Pi;
   psi3 open := evalf(subs(kin sol,data,s(t)=s max,psi3(t)))
   :"absolute wing closed angle"=%,"deg"=%*1807Pi;
            "absolute wing open angle" = 1.087075800, "deg" = 62.28485533
```

```
"absolute wing closed angle" = 0.5487704485, "deg" = 31.44223061
                                                                        (2.3.6.1)
Direct kinematic with independent psi3(t)
> psi3 kin sols := solve(subs(data,Phi),[op(convert(qvars,set)
  minus {psi3(t)})],explicit=true):
  nops(psi3 kin sols);
                                                                        (2.3.7.1)
> psi3 kin sol := psi3 kin sols[1];
psi3 \ kin \ sol := |\psi I(t)| = \arcsin(2.\cos(\psi 3(t)) - 1.100000000), s(t) =
                                                                        (2.3.7.2)
    -0.005000000000 \sqrt{-21.-400.\cos(\psi 3(t))^2+440.\cos(\psi 3(t))}
    -0.1000000000 \sin(\psi 3(t)) + 0.1380000000
Check the solution
> "closed configuration"=evalf(subs(psi3(t)=psi3 closed,data,
  psi3 kin sol));
  "open configuration"=evalf(subs(psi3(t)=psi3 open,data,
  psi3 kin sol));
        "closed configuration" = [\psi I(t) = -0.1706753036, s(t) = 0.0001994128]
         "open configuration" = [\psi I(t) = 0.6514412053, s(t) = 0.04607560011]
                                                                        (2.3.7.3)
Drawing...
> draw mech := proc(sol,data,dof)
       global PA, PB, PC, PD, G1, G2, G3:
       local pA,pB,pC,pD,pP,pT,pR,g1,g2,g3,r:
       r := 0.004:
       pA:=[comp X(PA,ground),comp Y(PA,ground)]:
       pB:=[comp_X(PB,ground),comp_Y(PB,ground)]:
       pC:=[comp X(PC,ground),comp Y(PC,ground)]:
       pD:=[comp X(PD,ground),comp Y(PD,ground)]:
       g1:=[comp X(G1,ground),comp Y(G1,ground)]:
       g2 := [comp X(G2, ground), comp Y(G2, ground)]:
       g3:=[comp\ X(G3,ground),comp\ Y(G3,ground)]:
       pT:=[comp X(PT,ground),comp Y(PT,ground)]:
       pR:=[comp X(PR,ground),comp Y(PR,ground)]:
       display([
                plottools:-line(subs(sol,data,dof,pA),subs(sol,data,
  dof,pB),color=black,thickness=4),
                plottools:-line(subs(sol,data,dof,pB),subs(sol,data,
  dof,pC),color=black,thickness=4),
                plottools:-disk(subs(sol,data,dof,pB),r,color=
  "Goldenrod")
                plottools:-disk(subs(sol,data,dof,pC),r,color=
   "Goldenrod")
                plottools:-disk(subs(sol,data,dof,pD),r,color=
  "Goldenrod"),
```

plottools:-disk(subs(sol,data,dof,pT),r,color=green),
plottools:-disk(subs(sol,data,dof,pR),r,color=green),

```
plottools:-disk(subs(sol,data,dof,gl),r,color=
  magenta),
              plottools:-disk(subs(sol,data,dof,g2),r,color=
  magenta),
              plottools:-disk(subs(sol,data,dof,g3),r,color=
  magenta),
              plottools:-polygon(subs(sol,data,dof,
  flap wing points), color=red),
              plottools:-polygon(subs(sol,data,dof,
  main wing points),color=red),
              plottools:-disk(subs(sol,data,dof,pA),r*1.5,color=
  blue),
              plottools:-disk(subs(sol,data,dof,pD),r*1.5,color=
  blue),
              plottools:-rectangle([0, 0],[0.350, 0.220], color =
  "LightGrey")
              plottools:-polygon(pylon points, color = red),
              plottools:-rectangle([0, 0], subs(data,[WIDTH, HEIGHT]
  ),color="LightGrey"),
              plottools:-curve(space B,color=cyan,linestyle=dot,
  thickness=2)
              plottools:-curve(space C,color=navy,linestyle=dot,
  thickness=2)
          ],
          scaling=constrained
      ):
  end proc:
> animate(draw mech,[kin sol,data,s(t)=S],S=s range);
```



```
Velocity ratio
```

```
> tau := combine(simplify(-MatrixInverse(JPhiD)).JPhiI): <%>;
   "dependent variables"=qD;

\frac{\sin(\psi 3(t))}{L2\cos(-\psi 3(t) + \psi I(t))} - \frac{\cos(\psi I(t))}{L3\cos(-\psi 3(t) + \psi I(t))}

                       "dependent variables" = [\psi l(t), \psi 3(t)]
                                                                               (2.4.1.1)
Ratio between the opening velocity of the wing and the velocity of s(t).
 > plot(
        subs(kin sol,data,s(t)=S,tau[2]), S=s range,
        title="Tau psi3(t) s(t)", labels=[s,typeset(diff(psi 3(t),t)
   /diff(s(t),t))],
        color="DarkOrange",
        size=SMS
   );
                                       Tau psi3(t) s(t)
                                      0.01 0.02 0.03 0.04
Dependent variables velocities
> vel kin sol:=op(solve(diff(Phi,t),diff(qD,t))):
Velocity of points
Velocity of the point where drag force atcs
> vel PP := collect(subs(vel kin sol, velocity(PP)), {diff}):
Velocity of the centre of mass of the different bodies
> vel P1 := collect(subs(vel kin sol, velocity(G1)), {diff}):
> vel P2 := collect(subs(vel kin sol,velocity(G2)), {diff}):
> vel P3 := collect(subs(vel kin sol, velocity(G3)), {diff}):
Angular velocities of points
Angular velocity of the reference frames of the different bodies
> avel P1 := collect(subs(vel kin sol, angular velocity(RF1)), {diff}
> avel P2 := collect(subs(vel kin sol, angular velocity(RF2)), {diff}
> avel P3 := collect(subs(vel kin sol, angular velocity(RF3)), {diff}
```

## **Acceleration analysis**

Dependent variables accelerations

```
> acc kin sol:=op(solve(diff(Phi,t,t),diff(qD,t,t))):
Acceleration of points
Acceleration of the centre of mass of the different bodies
 > acc P1 := collect(subs(acc kin sol, vel kin sol, acceleration(G1)),
   {diff}):
> acc P2 := collect(subs(acc kin sol,vel kin sol,acceleration(G2)),
  {di\overline{f}f}:
> acc P3 := collect(subs(acc kin sol, vel kin sol, acceleration(G3)),
   {diff}):
Angular acceleration of points
Acceleration of the centre of mass of the different bodies
> aacc P1 := collect(subs(acc kin sol, vel kin sol,
  angular acceleration(RF1)), {diff}):
> aacc P2 := collect(subs(acc kin sol, vel kin sol,
   angular acceleration(RF2)), {diff}):
> aacc P3 := collect(subs(acc kin sol, vel kin sol,
angular acceleration(RF3)),\overline{\{diff\}}):
Opening profile
> T tot := subs(data,T opening+T still+T closing);
                                  T_{tot} := 0.\overline{0500}
                                                                               (2.6.1)
> base profile := a0+a1*t+a2*t^2+a3*t^3+a4*t^4+a5*t^5;
                base profile := t^5 a5 + t^4 a4 + t^3 a3 + t^2 a2 + t a1 + a0
                                                                               (2.6.2)
 Opening part
To find the constants, we can plug in what we know about the profile (s min, s max etc).
 > opening known conditions:=[
        # position
        subs(t=0,data,base profile=s min),
        subs(t=T opening, data, base profile=s max),
        # velocity
        subs(t=0,data,diff(base profile,t)=0),
        subs(t=T opening,data,diff(base profile,t)=0),
        # acceleration
        subs(t=0,data,diff(base profile,t,t)=0),
        subs(t=T opening, data, \overline{d}iff(base profile, t, t)=0)
> opening coefficients:=op(solve(opening known conditions,[seq
   (a||i,i=0..5)]);
 opening coefficients := \begin{bmatrix} a0 = 0.0001989391299, a1 = 0., a2 = 0., a3 = 458759.5888, a4 \end{bmatrix}
                                                                               (2.6.3)
    = -6.881393831 \times 10^7, a5 = 2.752557533 \times 10^9
> opening profile:=subs(opening coefficients,base_profile);
opening profile := 2.752557533 \times 10^9 t^5 - 6.881393831 \times 10^7 t^4 + 458759.5888 t^3
                                                                               (2.6.4)
    +0.0001989391299
 Still part
 > still profile:=s max;
                        still\ profile := 0.0460748980054946
                                                                               (2.6.5)
```

```
Closing part
> closing known condition equations:=subs(data,[
                 # position
                subs(t=T__opening+T__still,data,base_profile=s_max),
subs(t=T__tot,data,base_profile=s_min),
                subs(t=T__opening+T__still,data,diff(base_profile,t)=0),
subs(t=T__tot,data,diff(base_profile,t)=0),
                 # acceleration
                subs(t=T__opening+T__still,data,diff(base_profile,t,t)=0),
subs(t=T__tot,data,diff(base_profile,t,t)=0)
     1);
closing known condition equations := [1.024000000 \times 10^{-7} a5 + 2.560000000 \times 10^{-6} a4]
                                                                                                                                                                                    (2.6.6)
         + 0.000064000000 a3 + 0.00160000 a2 + 0.0400 a1 + a0 = 0.0460748980054946, a0
         +0.0500 a1 + 0.00250000 a2 + 0.000125000000 a3 + 6.250000000 \times 10^{-6} a4
         +3.125000000 \times 10^{-7} a5 = 0.000198939129915359, 0.00001280000000 a5
         + 0.000256000000 \ a4 + 0.00480000 \ a3 + 0.0800 \ a2 + a1 = 0, \ a1 + 0.1000 \ a2
         +0.00750000 \ a3 + 0.0005000000000 \ a4 + 0.00003125000000 \ a5 = 0, 0.001280000000 \ a5
         +0.01920000 a4 + 0.2400 a3 + 2 a2 = 0, 2 a2 + 0.3000 a3 + 0.03000000 a4
         + 0.0025000000000 a5 = 0
> closing coefficients:=op(solve(closing known condition equations,
      [seq(a|\bar{1}, i=0..5)]));
closing coefficients := \begin{bmatrix} a0 = 487.4322620, a1 = -55051.15065, a2 = 2.477301779 \times 10^6, a3 \end{bmatrix} (2.6.7)
        = -5.550991024 \times 10^7, a4 = 6.193254448 \times 10^8, a5 = -2.752557533 \times 10^9
> closing profile:=subs(closing coefficients,base profile);
closing profile := -2.752557533 \times 10^9 t^5 + 6.193254448 \times 10^8 t^4 - 5.550991024 \times 10^7 t^3
                                                                                                                                                                                    (2.6.8)
         +2.477301779 \times 10^{6} t^{2} - 55051.15065 t + 487.4322620
Complete profile
> s profile:=piecewise(
                                                                            and t<=T opening,
     opening_profile,
                                                              and t<=T opening+T still,
                t>T opening
     still profile,
                t \ge T opening+T still and t<=T tot,
     closing profile
     );
                                                                      0.0460748980054946
s profile :=
                             -2.752557533 \times 10^{9} t^{5} + 6.193254448 \times 10^{8} t^{4} - 5.550991024 \times 10^{7} t^{3} + 2.477301779 \times 10^{6} t^{2} - 10^{6} t^{2} + 10^{6}
```

```
> s vel profile:=subs(diff(s profile,t));
                                                                                                                                                      1.376278766 \times 10^{10} t^4 - 2.752557532 \times 10^8 t^3 + 1.376278766 \times 10^6 t^2
                                                                          0
-1.376278766 \times 10^{10} t^{4} + 2.477301779 \times 10^{9} t^{3} - 1.665297307 \times 10^{8} t^{2} + 4.954603558 \times 10^{10} t^{10} 
> s acc profile:=subs(diff(s vel profile,t));
                                                                                                                        5.505115064 \times 10^{10} t^3 - 8.257672596 \times 10^8 t^2 + 2.752557532 \times 10^6 t
                                                                             > profiles:=subs(data,[
                                 diff(s(t),t,t)=s_acc_profile,
                                 diff(s(t),t)=s_vel_profile,
                                  s(t)=s profile
> plot(subs(data,s_profile),t=0..T__tot,color=green),
plot(subs(data,s_vel_profile),t=0..T__tot,color=orange),
          plot(subs(data,s_acc_profile),t=0..T_tot,color=purple)
```

### **Known conditions**

Initial conditions

#### **Position**

```
> ics_qI := [s(t)=eval(subs(t=0,data,s_profile))]; # it corresponds to s_min ics_qI := [s(t) = 0.0001989391299]  (2.7.1.1)  ics_qD := evalf(subs(ics_qI,data,kin_sol));   ics_qD := [\psi I(t) = -0.1706738276, \psi 3(t) = 1.087076363]  (2.7.1.2)  > ics_pos := ics_qI \text{ union } ics_qD;  (2.7.1.3)
```

```
ics\ pos := [s(t) = 0.0001989391299, \psi I(t) = -0.1706738276, \psi 3(t) = 1.087076363] (2.7.1.3)
```

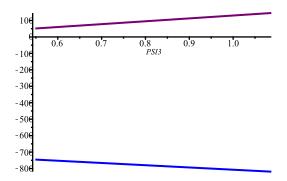
### Velocity

```
[> ics_qI_vel := [diff(s(t),t)=eval(subs(t=0,data,s_vel_profile))]:
[> ics_qD_vel := evalf(subs(ics_qI_vel,data,vel_kin_sol)):
[> ics_vel := ics_qI_vel union ics_qD_vel;
ics_vel := \left[\frac{d}{dt} s(t) = 0., \frac{d}{dt} \psi I(t) = 0., \frac{d}{dt} \psi 3(t) = -0.\right] (2.7.2.1)
```

#### Acceleration

# **Dynamics**

```
> gravity:=make_VECTOR(ground,0,-g,0):
Bodies
> PIST:=make BODY(G1,m_pist,0,0,Iz_pist):
> LINK:=make BODY(G2,m link,0,0,Iz link):
> FLAP WING:=make BODY(G3,m wing,0,0,Iz wing):
Acting forces
Piston force
> piston force:=make VECTOR(RF0,0,F piston(t),0):
                                                            #-
> FP:=make FORCE(piston force, PP, PIST):
Air contact forces (dragforce plus downforce)
> air forces:=make VECTOR(ground,F__drag(t),-F__down(t),0):
> FA:=make FORCE(air forces, G3, FLAP WING):
> air forces law:=[
      F drag(t)=F drag open+(F drag closed-F drag open)*(psi3
   (t)-psi3 open)/(psi3 closed-psi3 open),
      F_down(t)=F_down_open+(F_down_closed-F_down_open)*(psi3
   (t)-psi3 open)/(psi3 closed-psi3 open)
> display([
          plot(subs(air forces law,psi3(t)=PSI3,data,F drag(t)),
  PSI3=psi3 closed..psi3 open),
          plot(subs(air forces law,psi3(t)=PSI3,data,-F down(t)),
  PSI3=psi3 closed..psi3 open)
      color=[purple,blue],
      size=SMS
  );
```



#### **Newton Euler**

### Equation of motion

```
Internal forces
> PJ force := make FORCE(make VECTOR(ground,Np(t),0,0),PP,PIST):
> PJ torque := make TORQUE(make VECTOR(ground,0,0,Tp(t)),PIST):
> RJ1 force := make FORCE (make VECTOR (ground, rj1x(t), rj1y(t), 0), PB,
   PIST, LINK):
> RJ2 force := make FORCE(make VECTOR(ground,rj2x(t),rj2y(t),0),PC,
  LINK, FLAP WING):
> RJ3 force := make FORCE (make VECTOR (ground, rj3x(t), rj3y(t), 0), PD,
   FLAP WING):
> rvars := [Np(t), Tp(t), rj1x(t), rj1y(t), rj2x(t), rj2y(t), rj3x(t),
   rj3y(t)]:
Set of forces
> forces := {PJ force, PJ torque, RJ1 force, RJ2 force, RJ3 force, FP,
   FA}:
Newton-Euler Equations
> newton equations({PIST} union forces):
   euler equations({PIST} union forces,G1):
   NE eqns1 := [comp X(%%, ground), comp Y(%%, ground), comp Z(%,
   ground) 1:
<FA> FORCE is not valid: it must be applied to a BODY
<RJ3 force> FORCE is not valid: it must be applied to a BODY
> newton equations({LINK} union forces):
   euler equations({LINK} union forces,G2):
   NE eqns2 := [comp X(%%,ground), comp Y(%%,ground), comp Z(%,
  ground) ]:
<FA> FORCE is not valid: it must be applied to a BODY
<FP> FORCE is not valid: it must be applied to a BODY
<PJ force> FORCE is not valid: it must be applied to a BODY
\langle RJ\overline{3} \rangle force> FORCE is not valid: it must be applied to a BODY
> newton equations({FLAP WING} union forces):
   euler equations({FLAP WING} union forces,G3):
   NE eqns3 := [\text{comp } X(\sqrt[8]{8}, \text{ground}), \text{ comp } Y(\sqrt[8]{8}, \text{ground}), \text{ comp } Z(\sqrt[8]{8}, \text{ground})]
   ground) ]:
<FP> FORCE is not valid: it must be applied to a BODY
<PJ force> FORCE is not valid: it must be applied to a BODY
> eqns NE := NE eqns1 union NE eqns2 union NE eqns3:
```

```
nops(eqns_NE) + nops(Phi) = nops(rvars) + nops(qvars);
11 = 11 (3.1.1.1)
```

### Inverse dynamic

### Direct dynamic

Variable profile given the force.

In practice this just a check of the inverse dynamic.

#### Set up the system

```
> eqns_NE_static := evalf(subs(air_forces_law,ics_acc,ics_vel, ics_pos,data,eqns_NE)); ics_rvars := op(solve(eqns_NE_static[1..-2],rvars)): <%>; eqns_NE_static := [-1.Np(t) - 1.rjlx(t), 0.784800 - 1.F_{piston}(t) - 1.rjly(t), -0.003200000000 Np(t) + 0.012800000000 rjlx(t) - 1.Tp(t), rjlx(t) - 1.rj2x(t), 0.367875 + rjly(t) - 1.rj2y(t), 0.02463676358 rjlx(t) + 0.02463676358 rj2x(t) - 0.004246160620 rjly(t) - 0.004246160620 rj2y(t), -145.5132885 + rj2x(t) - 1.rj3x(t), 838.7370169 + rj2y(t) - 1.rj3y(t), 0.03767539849 rj2x(t) - 0.01799901303 rj2y(t) + 0.05085213524 rj3x(t) - 0.02850866573 rj3y(t)]
```

(3.1.3.1)

```
Np(t) = -0.1669624750 + 0.1723505852 F_{piston}(t)
                                 Tp(t) = 0.002671399600 - 0.002757609363 F_{piston}(t)
                                   rj1x(t) = 0.1669624750 - 0.1723505852 F_{piston}(t)
                                             rjly(t) = 0.7848000000 - 1.F_{piston}(t)
                                                                                                                                                           (3.1.3.1)
                                   rj2x(t) = 0.1669624750 - 0.1723505852 F_{piston}(t)
                                              rj2y(t) = 1.152675000 - 1.F_{piston}(t)
                                   rj3x(t) = -145.3463260 - 0.1723505852 F_{piston}(t)
                                              rj3y(t) = 839.8896919 - 1.F_{piston}(t)
> ics piston_NE := [F__piston(t)=evalf(subs(t=0,
   piston_force_NE_profile())]:
> ics dae NE := subs(ics piston NE, t=0, convert(ics vel union
     ics pos union ics rvars,D));
ics dae NE := [D(s)(0) = 0, D(\psi I)(0) = 0, D(\psi S)(0) = -0, s(0)
                                                                                                                                                           (3.1.3.2)
        =0.0001989391299, \psi I(0) = -0.1706738276, \psi I(0) = 1.087076363, Np(0)
        = 172.7335602, Tp(0) = -2.763736962, rj1x(0) = -172.7335602, rj1y(0)
        =-1002.406007, rj2x(0) = -172.7335602, rj2y(0) = -1002.038132, rj3x(0)
        =-318.2468487, rj3v(0) = -163.3011151
> eqns NE union Phi union ics dae NE:
> sys NE := subs(
              air forces law,
              F piston(t)=piston force NE profile,
              eqns NE union Phi union ics dae NE
     ):
System solution
Sometimes the dsolve face a singularity and throws an exception; the following approach avoids
interruptions.
> st := time():
     solved:=false:
     do
              try
                        dsol NE := dsolve(sys NE, numeric, implicit=true, stiff=
     true, output=listprocedure, relerr=1e-5):
                        solved:=true:
              catch:
                        print("Exception generated, automatic retrial"):
               end try;
     until solved:
     "computation time"=time() - st;
                                                      "computation time" = 2.094
                                                                                                                                                           (3.1.3.3)
> dsol NE;
    = \operatorname{proc}(t) ... end \operatorname{proc}(Np(t)) = \operatorname{proc}(t) ... end \operatorname{proc}(Tp(t)) = \operatorname{proc}(t) ... end \operatorname{proc}(Tp(t)) = \operatorname{proc}(Tp(t)) ...
```

```
= \mathbf{proc}(t) ... \mathbf{end}\ \mathbf{proc}, \frac{\mathrm{d}}{\mathrm{d}t}\ \psi I(t) = \mathbf{proc}(t) ... \mathbf{end}\ \mathbf{proc}, \psi 3(t) = \mathbf{proc}(t)
end proc, \frac{d}{dt} \psi 3(t) = \operatorname{proc}(t) ... end proc, rjlx(t) = \operatorname{proc}(t) ... end proc, rjly(t) =
     \mathbf{proc}(t)
end proc, rj2x(t) = proc(t) ... end proc, rj2y(t) = proc(t) ... end proc, rj3x(t) = proc(t)
     ...
end proc, rj3y(t) = \mathbf{proc}(t) ... end proc, s(t) = \mathbf{proc}(t) ... end proc, \frac{d}{dt} s(t) = \mathbf{proc}(t)
end proc]
> ## plot ##
   odeplot(dsol_NE,[t,s(t)],t=0..T__tot,color=blue,title="Piston
    position",size=SMS);
    ## plot ##
    odeplot(dsol_NE,[t,diff(s(t),t)],t=0..T__tot,color=blue,title=
    "Piston position", size=SMS);
                                                         Piston position
                                       0.03
                                       0.02^{-1}
                                       0.01
                                                  0.01
                                                         Piston position
## plot ## odeplot(dsol_NE,[t,psi3(t)],t=0..T__tot,color=purple,
title="Flap wing angle",size=SMS,numpoints=100);
## plot ## odeplot(dsol_NE,[t,diff(psi3(t),t)],t=0..T__tot,color=
   pink, title="Flap wing velocity", size=SMS, numpoints=100);
```

```
> ## plot ## odeplot(dsol NE,[t,Np(t)],t=0..T tot,color=brown,
  title="Reaction force on the piston", size=SMS, numpoints=100);
> ## plot ## odeplot(dsol NE,[t,rj3x(t)],t=0..T tot,color=khaki,
  title="Reaction force along x of the revolute joint in point C",
  size=SMS,numpoints=100);
  ## plot ## odeplot(dsol NE,[t,rj3y(t)],t=0..T tot,color=gold,
  title="Reaction force along y of the revolute joint in point C",
  size=SMS,numpoints=100);
```

## Lagrange

### Equation of motion

```
Constraints defintion
> lvars := [seq(lambda||i(t),i=1..nops(Phi))]:
> constraints := make CONSTRAINT(Phi,lvars);
constraints := table ([expr = [sin(\psi l(t)) L2 - cos(\psi 3(t)) L3 - xA + xD, -cos(\psi l(t)) L2 (3.2.1.1)
    -\sin(\psi 3(t))L3-L1-s(t)-vA+vD, obj=CONSTRAINT, vars=[\lambda 1(t), \lambda 2(t)]
Lagrange equations
> eqns lagr := lagrange equations({PIST,LINK,FLAP WING,FP,FA,
   constraints}, quars union lvars, t):
Inverse dynamic
As before, piston force profile given trajectory
> sol vars lagr:=op(solve(eqns lagr[1..3],lvars union [F piston(t)
   1)) = \frac{1}{1}
> piston force lagr:=simplify(combine(rhs(sol vars lagr[3]))):
> piston force lagr profile:=subs(air forces law,acc kin sol,
   vel kin sol, kin sol, profiles, data, piston force lagr):
> plot(piston force lagr profile, t=0..T tot, size=SMS, color=blue);
                         120000
                         100000
                          80000
```

## Direct dynamic

```
As before, check the result of the inverse dynamic
```

60000 40000 20000

```
Set up the system
```

```
> lvars := [seq(lambda||i(t),i=1..nops(Phi))]:
> constraints := make CONSTRAINT(Phi,lvars):
> AA,BB:=GenerateMatrix(eqns lagr[1..nops(qvars)] union diff(Phi,t,
  t), diff(qvars,t,t) union lvars):
> AAN:=evalf(simplify(subs(data,ics pos,AA))):
> BBN:=evalf(subs(air forces law,ics vel,ics pos,data,BB)):
> lin sol:=LinearSolve(AAN,BBN):
```

```
> ics piston lagr:=[F piston(t)=solve(lin sol[1],F piston(t))];
  # the following ways give the same results
       solve(lin_sol[2],F__piston(t)),
solve(lin_sol[3],F__piston(t)):
                   ics\_piston\_lagr := [F_{piston}(t) = 1003.196915]
                                                                            (3.2.3.1)
> ics lvars:=[seq(subs(ics piston lagr,lvars[i]=convert(lin sol,
  list(i) [i]), i=-2..-1):
> ics dae lagr:=subs(ics piston lagr,t=0,convert(ics vel union
  ics pos union ics lvars,D));
ics dae lagr := [D(s)(0) = 0, D(\psi I)(0) = 0, D(\psi S)(0) = -0, s(0)
                                                                            (3.2.3.2)
   =0.0001989391299, \psi I(0) = -0.1706738276, \psi I(0) = 1.087076363, \lambda I(0)
   =-172.7346128, \lambda 2(0) = -1002.044240
> sys lagr:=subs(
       air forces law,
       F piston(t)=piston force lagr profile,
       data,
       eqns lagr union Phi union ics dae lagr
  ):
System solution
Sometimes the dsolve face a singularity and throws an exception; the following approach avoids
interruptions.
> st := time():
  solved:=false:
            dsol lagr:=dsolve(sys lagr,numeric,implicit=true,stiff=
  true, relerr=\overline{1}e-5):
            solved:=true:
           print("Exception generated, automatic retrial"):
       end try;
  until solved:
  "computation time"=time() - st;
                           "computation time" = 1.531
                                                                            (3.2.3.3)
> ## plot ##
  odeplot(dsol lagr,[t,s(t)],t=0..T tot,color=blue,title="Piston
  position", size=SMS, numpoints=100);
  ## plot ## odeplot(dsol lagr,[t,diff(s(t),t)],t=0..T tot,color=
  cyan, title="Piston velocity", size=SMS, numpoints=100);
                                      Piston position
                          0.04^{\circ}
                          0.03
                          0.02
                          0.01
  odeplot(dsol lagr,[t,psi3(t)],t=0..T tot,color=purple, title=
```

```
"Flap wing angle", size=SMS, numpoints=100);
## plot ## odeplot(dsol_lagr,[t,diff(psi3(t),t)],t=0..T__tot,
color=pink, title="Flap wing velcoity", size=SMS, numpoints=100);
Flap wing angle

1.0

0.9

0.9

0.9

0.7

0.6
```

#### Virtual work

Principle of Virtual Work: VW = 0. Helpful to find input/output relationship between forces.

#### Static case

## Dynamic case

```
Principle of d'Alembert
> PVW dynamic:=
      # linear forces
      dot prod(piston force,vel PP)
      +dot prod(air forces, vel P3)
      +dot_prod(make_VECTOR(ground,0,-m__pist*g,0),vel_P1)
      +dot_prod(make_VECTOR(ground,0,-m_link*g,0),vel_P2)
      +dot prod(make VECTOR(ground, 0, -m wing*g, 0), vel P3)
      # angluar momentum
      # there are not external moments to consider
      # linear inertia forces
      -dot_prod(m__pist*acc_P1,vel_P1)
      -dot prod(m link*acc P2,vel P2)
      -dot prod(m wing*acc P3,vel P3)
      # angular inertia forces
      -dot_prod(Iz__pist*aacc_P1,avel_P1)
      -dot prod(Iz link*aacc P2,avel P2)
      -dot prod(Iz wing*aacc P3,avel P3)
```

```
> piston force pvw dynamic := rhs(op(solve(PVW dynamic, {F piston
  (t)}))):
> piston force pvw dynamic profile:=subs(air forces law,
  acc kin sol, vel kin sol, kin sol, profiles, data,
  piston force pvw dynamic):
> ## plot ##
  plot(piston force pvw dynamic profile, t=0..T tot, size=SMS, color=
  orange);
                         120000
                         100000
                          80000
                          60000
                          40000
                          20000
                                       0.02
                                            0.03
> display([
           plot(piston force NE profile, t=0..T tot),
           plot(piston force lagr profile, t=0..T tot),
           plot(piston force pvw dynamic profile, t=0..T tot)
       ],
       color=[green,blue,orange],
       title="Overlapping"
  ),
  plot(piston force NE profile, t=0..T tot, color=green, title=
  "Newton-Euler"),
  plot(piston force lagr profile,t=0..T tot,color=blue,title=
  "Lagrange"),
  plot(piston force pvw dynamic profile, t=0..T tot, color=orange,
  title="PVW dynamic");
                                                          PVW dynamic
                  Overlapping
                               Newton-Euler
                                              Lagrange
               120000
                             120000
                                          120000
                                                       120000
               100000
                             100000
                                          100000
                                                       100000
                8000
                             80000
                                           8000
                                                        80000
                6000
                             6000
                                           6000
                                                        6000
                4000
                             40000
                                           40000
                                                        40000
                2000
                             20000
                                           20000
                                                        20000
```

**Conclusion**: the piston force is the same for all the three methods adopted.