

INFERENCE OF HEATING PROPERTIES FROM “HOT” NON-FLARING PLASMAS IN ACTIVE REGION CORES II. NANOFLARE TRAINS

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ABSTRACT

Faint, high-temperature emission in active region cores has long been predicted as a signature of nanoflare heating. However, the detection of such emission has proved difficult due to a combination of the efficiency of thermal conduction, non-equilibrium ionization, and inadequate instrument sensitivity. In this second paper in our series on “hot” non-flaring plasma in active regions, we investigate the influence of repeating nanoflares of varying frequency on the resulting emission measure distribution. We have used an efficient two-fluid hydrodynamic model to carry out a parameter exploration in preferentially heated species, heating event frequency, and the power-law index determining the distribution of event energies. We compute the emission measure distribution for each point in our multi-dimensional heating parameter space in an effort to understand how each of these variables impacts the observed emission. Additionally, we calculate several observables and compare their efficacy in capturing the character of both the hot and cool parts of the emission measure distribution.

1. INTRODUCTION

Heating of the solar corona by nanoflares, first proposed by Parker (1988), has become one of the most favored and contentious coronal heating models (Cargill 1994; Cargill & Klimchuk 2004; Klimchuk 2006). The term *nanoflare* has now become synonymous with impulsive heating in the energy range $10^{24} - 10^{27}$ erg, with no specific assumption regarding the underlying physical mechanism; though its origin is almost certainly magnetic.

Cargill (1994); Cargill & Klimchuk (2004) have predicted that emission measure distributions resulting from nanoflare models should be wide and have a faint, high-temperature (8-10 MK) component, the so-called “smoking gun” of nanoflare heating. Though many workers (Reale et al. 2009; Schmelz et al. 2009; Miceli et al. 2012; Testa & Reale 2012; Del Zanna & Mason 2014; Petralia et al. 2014; Schmelz et al. 2015) have claimed evidence of this hot, faint component of the emission measure, poor spectral resolution (Testa et al. 2011; Winebarger et al. 2012) and non-equilibrium ionization (Bradshaw & Cargill 2006; Reale & Orlando 2008) have made a positive detection of nanoflare heating difficult. However, Brosius et al. (2014), using observations from the *EUNIS-13* sounding rocket, identified relatively faint emission from Fe XIX in a non-flaring active region (AR), suggesting temperatures of ~ 8.9 MK.

One strategy for constraining potential heating models is analysis of modeled and observed emission measure distributions in active region (AR) cores. Originally pro-

posed by Jordan (1975), it is well-known that the emission measure, $EM(T) = \int n^2 dh$, scales as $EM(T) \sim T^a$ over a temperature range $10^6 \lesssim T \lesssim T_m$, where T_m is the temperature at which $EM(T)$ peaks. Observations have shown that $2 \lesssim a \lesssim 5$, with $T_m \approx 10^{6.5-6.6}$ (Warren et al. 2011, 2012; Winebarger et al. 2011; Tripathi et al. 2011; Schmelz & Pathak 2012; Del Zanna et al. 2015).

A similar scaling has been claimed for hot emission such that $EM \propto T^{-b}$. Typically, this power-law fit to the emission measure is done “hotward” of the peak, usually in the range $T_m \lesssim T \lesssim 10^{7.2}$. However, measured values of these hotward slopes are poorly constrained due to both the magnitude of emission and the lack of available spectroscopic data in this temperature range (Winebarger et al. 2012). Warren et al. (2012), find $7 \lesssim b \lesssim 10$, with uncertainties of $\pm 2.5 - 3$, for 15 AR cores though Del Zanna & Mason (2014), using observations from the Solar Maximum Mission, claim larger values for b .

An important parameter for any proposed coronal heating mechanism is the frequency of energy release. Nanoflare heating is often classified as either *high-frequency* or *low-frequency* heating. In the case of high-frequency heating, t_N , the time between successive events, is such that $t_N \ll \tau_{cool}$, where τ_{cool} is the loop cooling time, and in the case of low-frequency heating $t_N \gg \tau_{cool}$ (Cargill et al. 2015). Steady heating is just high-frequency heating in the limit $t_N \rightarrow 0$.

The frequency of energy release in the solar corona is an important piece of evidence for determining the yet unknown coronal heating mechanism(s). However, measurement of the heating frequency, through both di-

rect and indirect means, has proved challenging. With regard to direct evidence of reconnection-driven (DC) heating, only recently have observations provided sufficient resolution to resolve magnetic field braiding (Cirtain et al. 2013), a possible precursor to bursty energy release. Additionally, while the resulting AR core emission measure distribution holds many clues as to how the coronal plasma is heated and cools, reconstructing $EM(T)$ from spectroscopic and narrow-band observations is non-trivial, with different inversion methods often giving significantly different results (Landi et al. 2012; Aschwanden et al. 2015). Efforts to measure the heating frequency through intensity fluctuations in AR cores have proved similarly difficult (Ugarte-Urra & Warren 2014).

Hydrodynamic loop models, combined with sophisticated forward modeling, provide an accurate method for assessing a wide variety of heating scenarios and calculating observables. Such models of nanoflare-heated loops have found emission measure slopes consistent with those derived from observations. While Bradshaw et al. (2012) found that the full range of a could not be accounted for with low-frequency nanoflares, Reep et al. (2013) showed that using a tapered nanoflare train allowed for $0.9 \lesssim a \lesssim 4.5$. Cargill (2014), using a 0D loop model, investigated a large range of heating frequencies, $250 < t_N < 5000$ s, and found that only when t_N was between a few hundred and 2000 seconds and proportional to the nanoflare energy could the full range of observed emission measure slopes be found.

In our first paper, Barnes et al. (2016) (Paper I, hereafter), we studied the effect of pulse duration, flux limiting, and NEI on hot emission from single nanoflares. We found that emission signatures of the heating are likely to be found in the temperature range $4 \lesssim T \lesssim 10$ MK. We now turn our attention to repeated impulsive events on a single strand.

In this second paper in our series on hot emission in AR cores, we use an efficient two-fluid hydrodynamic model to explore the effect of repeated impulsive heating events of varying frequency on the resulting $EM(T)$. In particular, we look at how the hot emission is affected by heating preferentially the electrons or the ions, with events drawn from a power-law distribution versus uniform heating rates. Additionally, we investigate the effect of scaling the inter-event waiting time to the event energy and as well as how NEI may affect the presence of hot emission. We use an emission measure ratio, similar to that of Brosius et al. (2014), to assess the relative importance of hot emission over the entire range of power-law indices and heating frequencies. Section 2 discusses the numerical model we have used to conduct this study and the parameter space we have investigated. Section 3 shows the resulting emission measure distributions and diagnostics for the entire parameter space. In Section 4, we discuss the impacts of two-fluid effects, pre-nanoflare density, and NEI on these calculated observables and how they may be interpreted in the context of nanoflare heating. Finally, Section 5 provides some concluding comments on our findings.

2. METHODOLOGY

2.1. Numerical Model

1D hydrodynamic models are excellent tools for computing field-aligned quantities in coronal loops. However, because of the small cell sizes needed to resolve the transition region and consequently small timesteps demanded by thermal conduction, the use of such models in large parameter space explorations is made impractical by long computational runtimes (Bradshaw & Cargill 2013). We use the popular 0D enthalpy-based thermal evolution of loops (EBTEL) model (Klimchuk et al. 2008; Cargill et al. 2012a,b, 2015) in order to efficiently simulate the evolution of a coronal loop over a large parameter space. This model, which has been successfully benchmarked against the 1D hydrodynamic HYDRAD code of Bradshaw & Cargill (2013), computes, with very low computational overhead, time-dependent, spatially-averaged loop quantities.

In order to treat the evolution of the electron and ion populations separately, we use a modified version of the usual EBTEL equations. This amounts to computing spatial averages of the two-fluid hydrodynamic equations over both the transition region and corona. A full description and derivation of these equations can be found in the appendix of Paper I. The relevant two-fluid pressure and density equations are,

$$\frac{d}{dt}\bar{p}_e = \frac{\gamma - 1}{L} [\psi_{TR} - (\mathcal{R}_{TR} + \mathcal{R}_C)] + \quad (1)$$

$$k_B \bar{n} \nu_{ei} (\bar{T}_i - \bar{T}_e) + (\gamma - 1) \bar{Q}_e, \quad (2)$$

$$\frac{d}{dt}\bar{p}_i = -\frac{\gamma - 1}{L} \psi_{TR} + k_B \bar{n} \nu_{ei} (\bar{T}_e - \bar{T}_i) + \quad (3)$$

$$(\gamma - 1) \bar{Q}_i, \quad (4)$$

$$\frac{d}{dt}\bar{n} = \frac{c_2(\gamma - 1)}{c_3 \gamma L k_B \bar{T}_e} (\psi_{TR} - F_{ce,0} - \mathcal{R}_{TR}), \quad (5)$$

where $c_2 = \bar{T}_e/T_{e,a} \approx 0.9$, $c_3 = T_{e,0}/T_{e,a} \approx 0.6$, ν_{ei} is the electron-ion binary Coulomb collision frequency and ψ_{TR} is a term included to maintain charge and current and neutrality. These equations are closed by the equations of state $p_e = k_B n T_e$ and $p_i = k_B n T_i$. In the cases where we treat the plasma as a single-fluid, we use the original EBTEL model as described in Klimchuk et al. (2008); Cargill et al. (2012a).

The loop is heated by a prescribed heating function, applied to either the electrons (\bar{Q}_e) or the ions (\bar{Q}_i). Both species cool through a combination of thermal conduction ($F_{ce,0}$, $F_{ci,0}$) and an enthalpy flux to the lower atmosphere, with the electrons also undergoing radiative cooling (\mathcal{R}_C). In the case of conductive cooling, a flux limiter, $F = (1/2) f n k_B T V_e$, is imposed to mitigate runaway cooling in a low-density, high-temperature plasma. In all cases we use a saturation limit of $f = 1$. See Paper I for a discussion of how f is likely to effect the presence of hot emission in a nanoflare-heated plasma.

2.2. Energy Budget

We define our heating function in terms of a series of discrete heating events plus a static background heating to ensure that the loop does not drop to unphysically low temperatures and densities between events. For a triangular heating pulse of duration τ injected into a loop of half-length L and cross-sectional area A , the total event energy is $\varepsilon = LAH\tau/2$, where H is the heating rate. Each model run will consist of N heating events, each

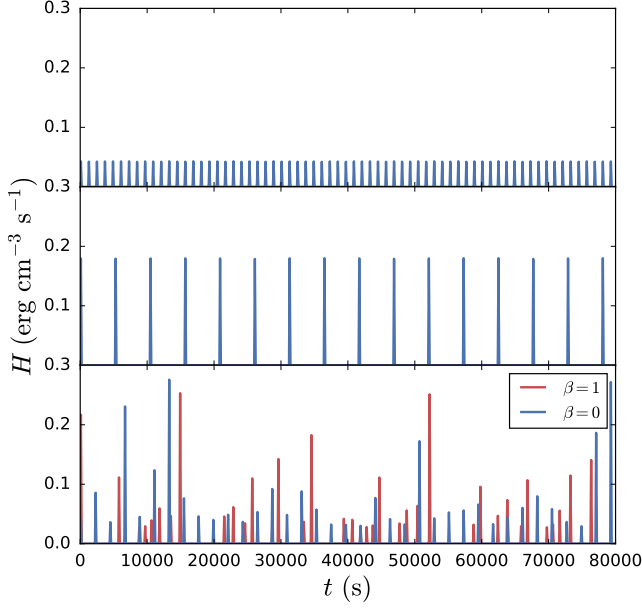


FIG. 1.— **Top:** Uniform heating amplitudes for $t_N = 1000$ s; **Middle:** Uniform heating amplitudes for $t_N = 5000$ s; **Bottom:** Heating amplitudes drawn from a power-law distribution with index $\alpha = -1.5$. The events shown in red have wait times that depend on the previous event energy while the events shown in blue have uniform wait times. The mean wait time in both cases is $t_N = 2000$ s.

with peak amplitude H_i , and a steady background heating of $H_{bg} = 3.5 \times 10^{-5} \text{ erg cm}^{-3} \text{ s}^{-1}$.

Recent observations have suggested that loops in AR cores are maintained at an equilibrium temperature of $T_{peak} \approx 4$ MK (Warren et al. 2011, 2012). Using our modified two-fluid EBTEL model, we have estimated the time-averaged volumetric heating rate needed to keep a loop of half-length $L = 40$ Mm at $\bar{T} \approx 4$ MK as $H_{eq} \sim 3.6 \times 10^{-3}$. In the single-fluid EBTEL model, this value is slightly lower because losses due to electron-ion collisions are ignored. Thus, to maintain an emission measure peaked about T_{peak} , for triangular pulses, the individual event heating rates are constrained by

$$H_{eq} = \frac{1}{t_{total}} \sum_{i=1}^N \int_{t_i}^{t_i+\tau} dt Q(t) = \frac{\tau}{2t_{total}} \sum_{i=1}^N H_i, \quad (6)$$

where t_{total} is the total simulation time. Note that if $H_i = H_0$ for all i , the heating rate for each event is $H_i = H_0 = 2t_{total}H_{eq}/N\tau$. Thus, for $L = 40$ Mm, $A = 10^{14} \text{ cm}^2$, the average energy per event for a loop heated by $N = 20$ nanoflares in $t_{total} = 8 \times 10^4$ s is $\varepsilon = LA t_{total} H_{eq}/N \approx 5.8 \times 10^{24} \text{ erg}$, consistent with the energy budget of the Parker nanoflare model.

We define the heating frequency in terms of the waiting time, t_N , between successive heating events. Following Cargill (2014), the range of waiting times is $250 \leq t_N \leq 5000$ s in increments of 250 s, for a total of 20 different possible heating frequencies. Additionally, t_N can be written as $t_N = (t_{total} - N\tau)/N$, where we fix $t_{total} = 8 \times 10^4$ s and $\tau = 200$ s. Note that because t_{total} and τ are fixed, as t_N increases, N decreases. Correspondingly, $\varepsilon_i = LA\tau H_i/2$, the energy injected per event, increases according to Equation 6 such that the

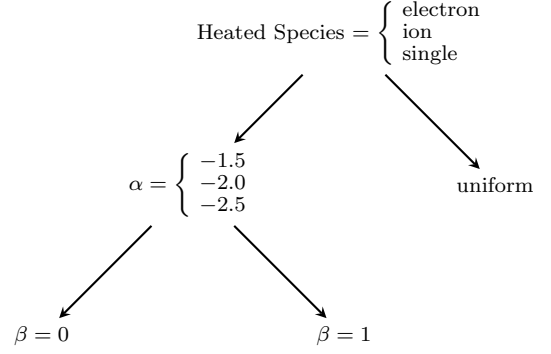


FIG. 2.— Total Parameter space covered. “single” indicates a single-fluid model. α is the power-law index and β indicates the scaling in the relationship $Q \propto T_N^\beta$, where $\beta = 0$ corresponds to the case where t_N and the event energy are independent. Note that $(3 \alpha \text{ values}) \times (2 \beta \text{ values}) + \text{uniform heating} = 7$ different types of heating functions.

total energy injected per run is constant.

According to the nanoflare heating model of Parker (1988), turbulent loop footpoint motions twist and stress the field, leading to a buildup and subsequent release of energy. Following Cargill (2014), we let $\varepsilon_i \propto t_{N,i}^\beta$, where $\varepsilon_i, t_{N,i}$ are the total energy of event i and waiting time following event i , respectively, and $\beta = 1$ such that the event energy scales linearly with the waiting time. The reasoning for such an expression is as follows. Bursty, nanoflare heating is thought to arise from the stressing and subsequent relaxation of the coronal field. If a sufficient amount of energy is released into the loop, the field will need enough time to “unravel” and “wind up” again before the next event such that the subsequent waiting time is large. Conversely, if only a small amount of energy is released, the field will require a shorter unwinding time, resulting in a shorter interval between the subsequent events. Thus, this scaling provides a way to incorporate a more physically motivated heating function into a hydrodynamic model which cannot self-consistently determine the heat input based on the evolving magnetic field. Figure 1 shows the various heating functions used for several example t_N values.

2.3. Heating Statistics

We compute the peak heating rate per event in two different ways: 1) the heating rate is uniform such that $H_i = H_0$ for all i and 2) H_i is chosen from a power-law distribution with index α where $\alpha = -1.5, -2.0$, or -2.5 . For the second case, it should be noted that, when $t_N \approx 5000$ s, $N \sim 16$ events, meaning the events from a single run do not accurately represent the distribution of index α . Thus, a sufficiently large number of runs, N_R , are computed for each t_N to ensure that the total number of events is $N_{tot} = N \times N_R \sim 10^4$ such that the distribution is well-represented. Figure 2 shows the parameter space we will explore. For each set of parameters and waiting time t_N , we compute the resulting emission measure distribution for N events in a period t_{total} . This procedure is repeated N_R times until $N \times N_R \sim 10^4$ is satisfied. Thus, when $t_N = 5000$ s and $N \sim 16$, $N_R = 625$, meaning the model is run 625 times with a heating frequency of $t_N = 5000$ s in order to properly fill out the event energy distribution.

2.4. Non-equilibrium Ionization

When considering the role of nanoflares in the production of hot plasma in AR cores, it is important to take non-equilibrium ionization (NEI) into account (Bradshaw & Cargill 2006; Reale & Orlando 2008). In a steady heating scenario, the ionization state is an adequate measure of the electron plasma temperature. Because the heating timescale is long (effectively infinite), the ionization state has plenty of time to come into equilibrium with the electron temperature.

In a nanoflare train, when the heating frequency is high, the loop is not allowed to drain or cool sufficiently between events, meaning the ionization state is kept at or near equilibrium. However, as the heating frequency decreases, the loop is allowed to cool and drain more and more during the inter-event period. If the heating occurs on a short enough timescale, the ionization state will not be able to reach equilibrium with the electron plasma before the loop undergoes rapid cooling by thermal conduction. Furthermore, if the frequency is sufficiently low so as to allow the loop to drain during the inter-event period, the ionization equilibrium timescale will increase. Thus, in the context of intermediate- to low-frequency nanoflares, NEI should be considered.

As in Paper I, we use the numerical code¹ outlined in Bradshaw (2009) to assess the impact of NEI on our results. Given a temperature ($T(t)$) and density ($n(t)$) profile from EBTEL, we compute the non-equilibrium ionization states for Fe IX through XXVII and the corresponding effective electron temperature, T_{eff} , that would be inferred by assuming ionization equilibrium. Using T_{eff} , we are then able to compute a corresponding NEI emission measure distribution, $EM(T_{eff})$.

3. RESULTS

We now show the results of our loop simulations for each point in our multi-dimensional parameter space: species heated (single-fluid, electron or ion), power-law index (α), heating frequency (t_N), and waiting-time/event energy relationship (β). In each 0D hydrodynamic simulation, a loop of half-length $L = 40$ Mm is heated by N triangular events of duration $\tau = 200$ s and peak heating rate H_i for a duration of $t_{total} = 8 \times 10^4$ s. The average interval between subsequent events is t_N (in the uniform and $\beta = 0$ cases, $t_{N,i} = t_N$ exactly for all i). We focus primarily on the emission measure distribution, $EM(T)$, and observables typically calculated from $EM(T)$. In all cases, the coronal emission measure is calculated according to the method outlined in section 3 of Paper I. The corresponding NEI results, $EM(T_{eff})$, are calculated similarly, but using T_{eff} (see Subsection 2.4) instead of T . All results were processed using the IPython system for interactive scientific computing in Python (Pérez & Granger 2007) as well as the NumPy and SciPy numerical and scientific Python libraries (van der Walt et al. 2011). All results were visualized using the matplotlib graphics library (Hunter 2007).

3.1. Emission Measure Distributions

In our first set of results, we compare $EM(T)$ for three different types of heating functions, across six different heating frequencies. Figure 3, Figure 4, and Figure 5 show the emission measure distributions in the single-fluid case, electron heating case, and ion heating case, respectively. Each panel in each figure corresponds to a different waiting time (t_N) and includes three different types of heating functions: uniform heating events (red), events chosen from a power-law distribution of index $\alpha = -2.5$ ($\beta = 0$ case, blue), and events chosen from a power-law distribution of index $\alpha = -2.5$ where the time between successive events depends on the heating rate of the preceding event ($\beta = 1$ case, green). Note that in all three figures, we show the results for only a single power-law index, $\alpha = 2.5$. Furthermore, the dashed lines denote the corresponding NEI cases, $EM(T_{eff})$.

Recall from Subsection 2.3 that for those heating functions which choose peak heating rates from a power-law distribution, for each t_N , we run the model N_R times. Thus, for each point in our parameter space, we produce N_R $EM(T)$ curves. In order to present our results compactly, the solid lines in Figure 3, Figure 4, and Figure 5 each show the mean $EM(T)$ over all N_R curves. The shading represents 1σ from the mean. In this way, we account for the variations that may occur because of a lack/excess of strong heating events due to limited sampling from the distribution.

We look first at $EM(T)$ for the single-fluid case, Figure 3. Looking at all six panels, we note that as t_N increases, $EM(T)$ widens, extending to both cooler (< 4 MK) and hotter (> 4 MK) temperatures. $EM(T)$ extends toward cooler temperatures because as t_N increases and there is more time between successive heating events, the loop is allowed more time to cool both by radiation and enthalpy-driven cooling. $EM(T)$ extends towards hotter temperatures for similar, but more subtle reasons. As $t_N \rightarrow 0$, we approach the steady heating case in which conductive and radiative cooling exactly balance the heating. As t_N increases and becomes comparable to and greater than a cooling time, the loop becomes increasingly tenuous at the time of the subsequent heating event, allowing the loop to reach much hotter temperatures since radiative cooling is very inefficient at low densities and the heat flux saturates. In this way, $EM(T)$ can “see” this greater range of temperatures, both hot and cool, provided it is allowed to undergo a typical heating and cooling cycle. The more curtailed this cycle is by continued reheatings, the more narrow $EM(T)$ will be.

Looking at the different curves in each panel of Figure 3, it is important to note that, although $EM(T)$ for all three types of heating functions widen with increasing wait time, their dependence on t_N is quite different. The uniform (red) and $\beta = 0$ (blue) $EM(T)$ curves evolve similarly as they extend to cooler temperatures with increasing t_N while the $\beta = 1$ curves (green) extend to cooler temperatures much more rapidly. For example, at $t_N = 1500$ s, both the uniform and $\beta = 0$ cases show little to no emission below 2 MK while the $\beta = 1$ cases extends to temperatures well below 1 MK (Cargill 2014). Contrastingly, on the hot side, the $\beta = 0$ and $\beta = 1$ curves evolve nearly identically with increasing t_N while the uniform heating case shows a cutoff at much lower temperatures, particularly for $t_N \leq 2500$ s.

The $EM(T)$ curves for the different types of heating

¹ This code has been made freely available by the author and can be downloaded at: <https://github.com/rice-solar-physics/IonPopSolver>.

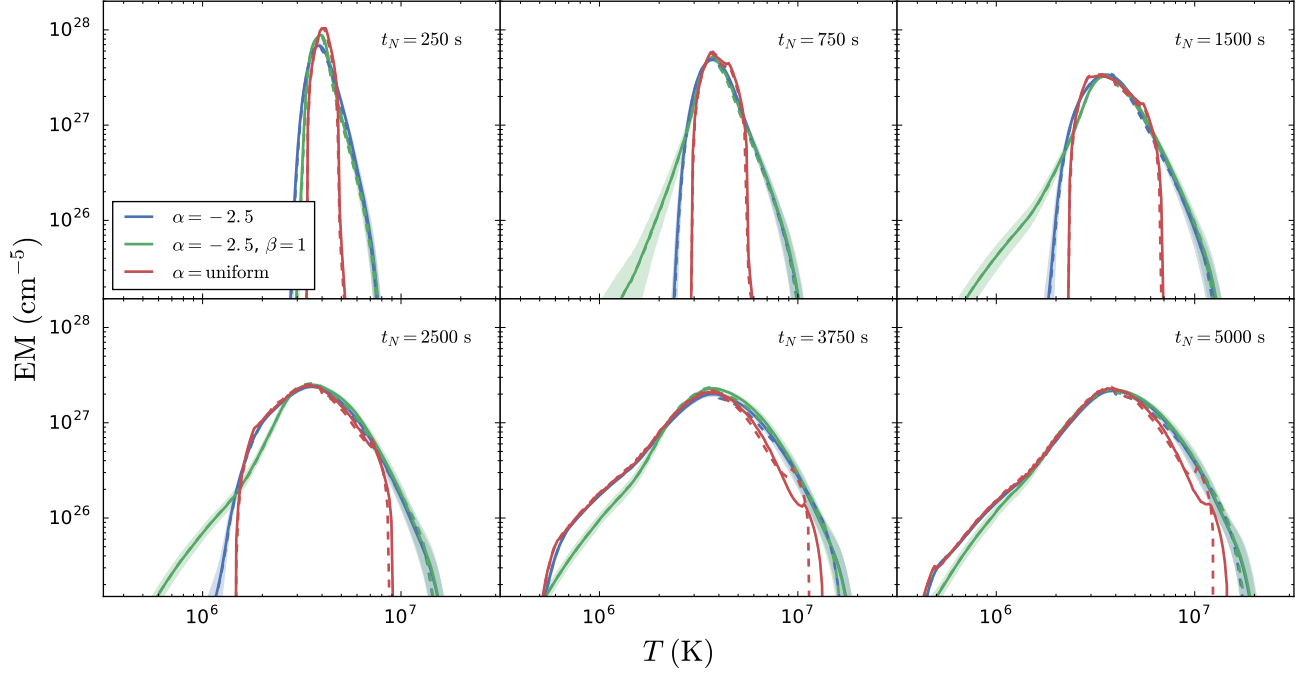


FIG. 3.— Emission measure distributions for waiting-times $t_N = 250, 750, 1500, 2500, 3750, 5000$ s in the single-fluid case. The three types of heating functions shown are uniform heating rates (red), heating rates chosen from a power-law distribution of $\alpha = -2.5$ (blue), and heating rates chosen from a power-law distribution of $\alpha = -2.5$ where the time between successive events is proportional to the heating rate of the preceding event (green). The solid lines in the two power-law cases show the mean $EM(T)$ over N_R runs and the shading indicates 1σ from the mean. The dashed lines denote the corresponding $EM(T_{eff})$ distribution. The standard deviation is not included in the NEI results.

functions shown in Figure 4, in which only the electrons are heated, evolve similarly to those shown in Figure 3. This is particularly true on the cool side where the density is sufficiently high, allowing the electrons and the ions to equilibrate such that there is no discernible difference compared to the single-fluid case. On the hot side, for $t_N \leq 750$ s, the electron and single-fluid cases are quite similar. However, for $t_N \geq 1500$ s, in the electron heating case, $EM(T)$ steepens just above 4 MK and then flattens out near 10 MK. This change in shape is most obvious in the uniform heating case where a distinct “hot shoulder” forms just above 10 MK. In the power-law cases, this feature is less pronounced though $EM(T)$ extends to slightly higher temperatures.

In Figure 5 in which only the ions are heated, the cool side of the $EM(T)$ is very similar to both the single-fluid and electron heating cases because the electron and ion populations are in equilibrium during this portion of the loop’s evolution. On the hot side, for intermediate to low heating frequencies (i.e. $t_N \geq 1500$ s), the $EM(T)$ in the uniform heating case is truncated below 10 MK and in the power-law cases extends to just above 10 MK for the lowest heating frequency ($t_N = 5000$ s). This cutoff at lower temperatures is due to the fact that electrons cannot “see” the ions until they have cooled well below their peak temperature. This is discussed in Paper I though in the single-pulse cases, the cutoff occurred at lower temperatures. Additionally, in both the uniform and power-law cases, the peak of $EM(T)$ is wider for these low frequencies compared to those cases shown in the lower right panels of Figure 3 and Figure 4.

The dashed lines in the panels of Figure 3, Figure 4, and Figure 5 show the corresponding $EM(T_{eff})$ for each

heating function type. Only the mean $EM(T_{eff})$ over N_R runs is shown for these results. In all three figures, for the intermediate to high frequencies (i.e. $t_N \leq 1500$ s), there is no discernible difference between $EM(T)$ and $EM(T_{eff})$. Furthermore, both of the power-law cases show little deviation from ionization equilibrium in the emission measure for even the lowest heating frequencies in the single-fluid, electron heating, and ion heating cases. For $t_N \geq 2500$ s in the uniform heating case, in both Figure 3 and Figure 4, $EM(T_{eff})$ is truncated at slightly lower temperatures as compared to $EM(T)$. This hot emission is relocated to cooler temperatures, resulting in a “bump” in the emission measure distribution near 10 MK. None of the panels of Figure 5 show any significant difference between $EM(T)$ and $EM(T_{eff})$. This is because the electrons are essentially heated on a timescale dictated by the Coulomb collision frequency which is slow enough to ensure ionization equilibrium during the entire heating phase.

3.2. Pre-nanoflare Density

In the single-fluid and electron heating cases, while $EM(T)$ in the uniform and power-law heating cases generally agree for low-frequency heating ($t_N = 5000$ s), for intermediate frequencies ($t_N \approx 750 - 2500$ s), the power-law cases show an enhanced high-temperature component compared to the uniform case as seen in Figure 3 and Figure 4.

Figure 6 shows sample heating, temperature, and density profiles for an intermediate heating frequency ($t_N = 2500$ s), in the case where only the electrons are heated, for the three different types of heating functions. In the uniform heating rate case (red), each event has a max

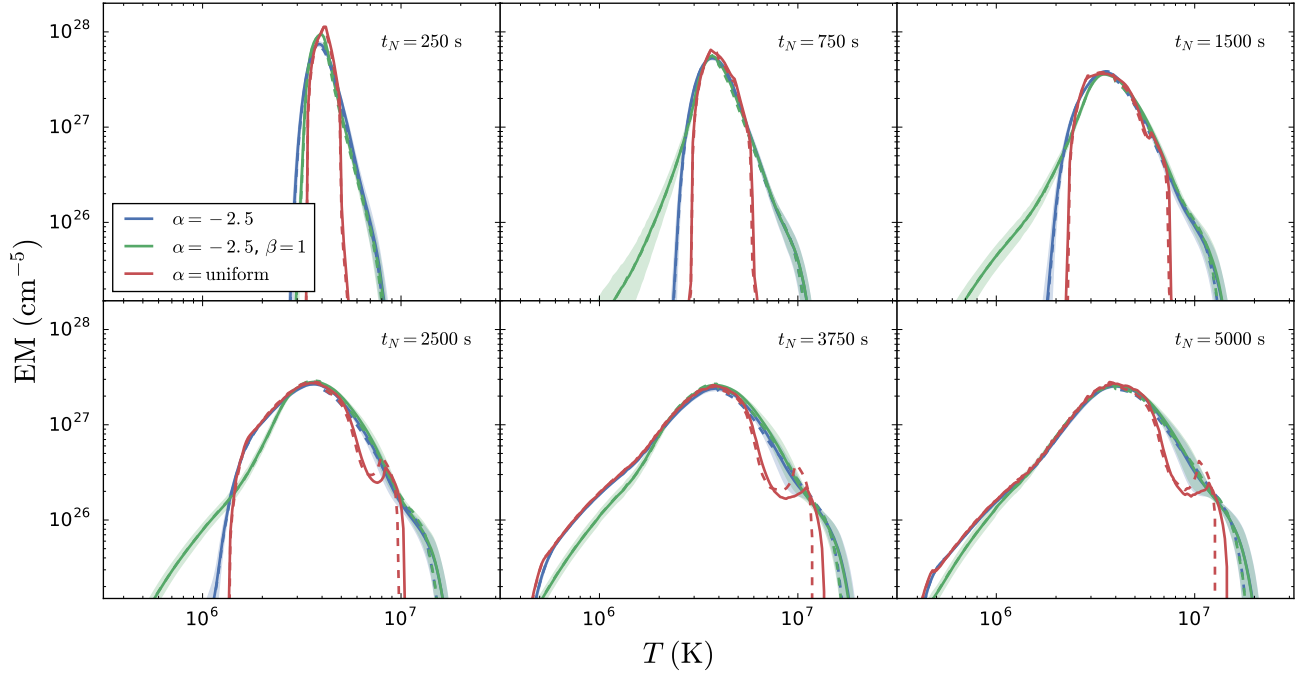


FIG. 4.— Same as Figure 3, but for the case where only the electrons are heated.

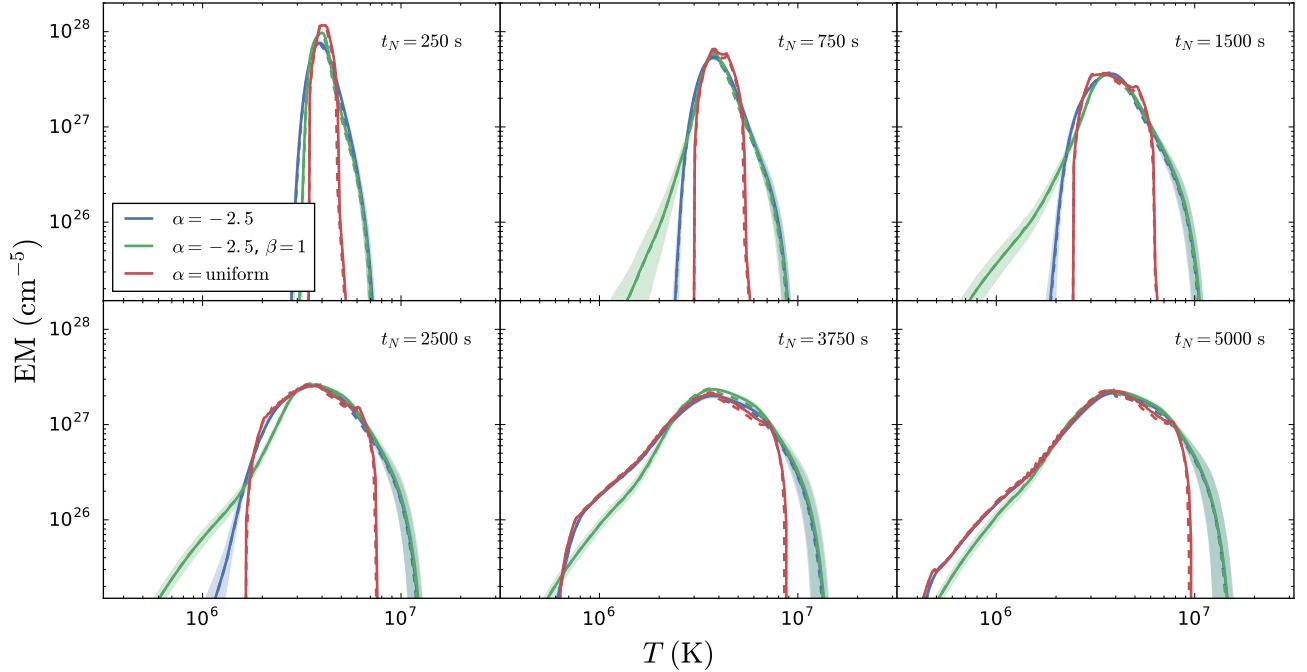


FIG. 5.— Same as Figure 3, but for the case where only the ions are heated.

heating rate of H_0 such that the loop undergoes $N \approx 30$ identical heating and cooling cycles, each time reaching a maximum temperature and density of $T_{max,0}$ and $n_{max,0}$, respectively. Recall from Equation 6 that the total energy injected into the loop is constrained such that $H_0 = (1/N) \sum_{i=1}^N H_i$. In the case where the heating rates are distributed according to a power-law, there will be many events where $H_i < H_0$ and a few events where $H_i \gg H_0$.

These few high energy events allow for $T \gg T_{max,0}$ in

the case where the events are chosen from a power-law distribution (blue and green curves) as seen in the middle panel of Figure 6. Because these events are injected into a plasma that is already sufficiently dense due to the relatively short draining and cooling times, the emission measure is able to “see” these hot temperatures, resulting in a > 10 MK component of $EM(T)$ (see lower left panel of Figure 3 and Figure 4). Contrastingly, in the uniform case, $T_{max,0} < 10$ MK such that $EM(T)$ has a steep cutoff right at 10 MK. Additionally, we note that the

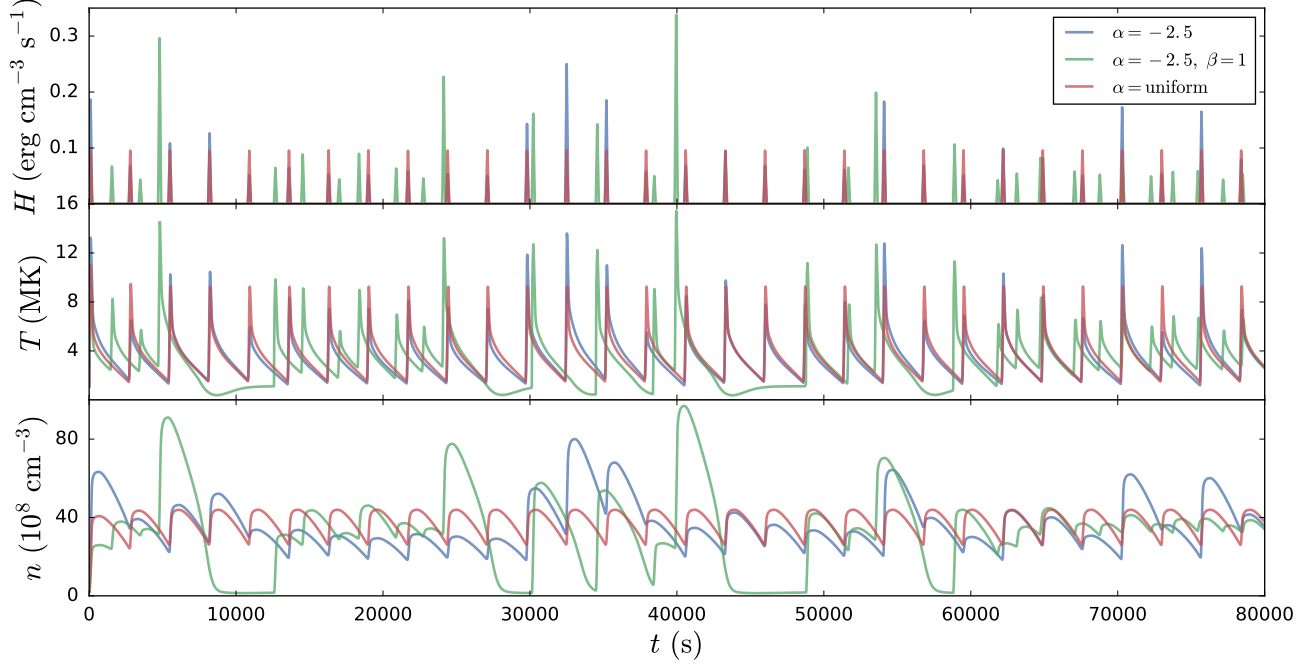


FIG. 6.— Example heating (top), temperature (middle), and density (bottom) profiles for the case in which only the electrons are heated with an intermediate heating frequency of $t_N = 2500$ s. The three curves shown in each panel correspond to uniform heating rates (red), heating rates chosen from a power-law distribution of $\alpha = -2.5$ (blue), and heating rates chosen from a power-law distribution of $\alpha = -2.5$ where the time between successive events is proportional to the heating rate of the preceding event (green).

only effect of the longer wait times in the $\beta = 1$ case as compared to the $\beta = 0$ case is an extended cool emission measure at intermediate frequencies (e.g. $t_N = 2500$ s); the hot part of EM(T) for both power-law cases is nearly identical. In this way, the hot and cool sides of the emission measure distribution are largely isolated from one another as they are determined by separate phases of the loop evolution.

Another important discrepancy between the uniform and power-law cases is the impact of NEI on the hot part of EM(T). Recall from [Subsection 2.2](#) that the uniform heating rate $H_0 = 2t_{\text{total}}H_{\text{eq}}/N\tau = 2H_{\text{eq}}(t_N/\tau + 1)$. From the top panel of [Figure 6](#) we see that in the power-law case, the heating rate can be as high as $H_i \sim 0.3 \text{ erg cm}^{-3} \text{ s}^{-1}$. In terms of a uniform heating rate, this corresponds to a waiting time of $t_N \approx 8100$ s. So even for the lowest heating frequency in the uniform case, the loop is still much lower. Furthermore, for $t_N = 5000$ s, the lowest heating frequency considered here, the loop is allowed to drain to its equilibrium value (as determined by the background heating) between each event such that events with a heating rate $H_0 \approx 0.2 \text{ erg cm}^{-3} \text{ s}^{-1}$ are injected into a low-density loop, meaning that the ionization state will not be able to keep pace with the subsequently rapid rise in temperature, resulting in EM(T_{eff}) having a lower temperature cutoff. On the other hand, when the heating events are selected from a power-law distribution, events with $H_i > 0.2 \text{ erg cm}^{-3} \text{ s}^{-1}$ can be injected into a much higher density loop (because lower values of t_N prevent longer draining times). This allows the ionization state to be relatively representative of the electron temperature such that EM(T) \approx EM(T_{eff}).

3.3. Hot Plasma Diagnostics

3.3.1. Emission Measure Slope

We now examine several observables often used to characterize the emission measure distribution. The most common observable is the emission measure slope a such that EM $\propto T^a$ for $10^{5.5} \leq T \leq 10^{6.6}$ K. Both observational and modeling studies have found that $2 < a < 5$ (see Table 3 of [Bradshaw et al. 2012](#)) and in particular, [Cargill \(2014\)](#) found that a heating function of the form $t_N \propto \varepsilon$ was needed in order to account for this range of slopes. Additionally, a similar scaling of EM $\propto T^{-b}$ for $10^{6.6} \leq T \leq 10^{7.0}$ has been claimed though measurements of b have been subject to large uncertainties ([Warren et al. 2012](#)).

[Figure 7](#) shows an example of how both T^a and T^{-b} can be fit to the cool and hot sides of EM(T), respectively. We select a single sample run from our parameter space in which only the electrons are heated by the events chosen from a power-law distribution of $\alpha = -2.5$ and spaced uniformly by an interval of $t_N = 5000$ s. We calculate the resulting EM(T) and fit $\log \text{EM}$ to $a \log T$ on $\log T_{c,\min} < \log T < \log T_{c,\max}$ and $-b \log T$ on $\log T_{h,\min} < \log T < \log T_{h,\max}$ using the Levenburg-Marquardt algorithm for least-squares curve fitting as implemented in the SciPy scientific Python package ([van der Walt et al. 2011](#)). We fix the lower limit on each interval such that $T_{c,\min} = 10^{5.7}$ K and $T_{h,\min} = 10^{6.7}$ K and vary the upper limits over $10^{6.1} < T_{c,\max} < 10^{6.5}$ and $10^{6.8} < T_{h,\max} < 10^{7.2}$. The left panel of [Figure 7](#) shows a (blue) and b (red) as a function upper limit of the fit interval, $T_{c,\max}$ (bottom axis) and $T_{h,\max}$ (top axis), respectively. The shading denotes the uncertainty of the fit. The right panel of [Figure 7](#) shows the resulting fit lines superimposed on the emission measure distribution.

From the left panel of [Figure 7](#), we see that, while

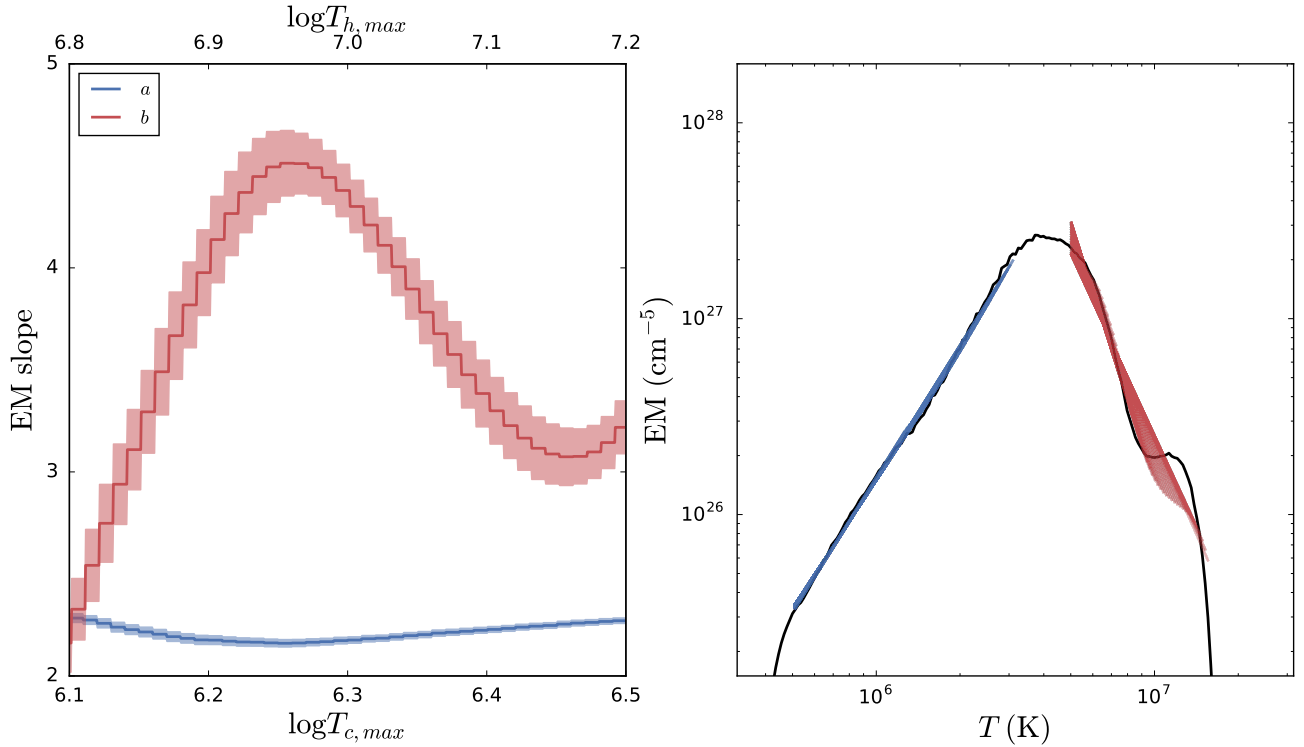


FIG. 7.— Fits to a sample emission measure distribution constructed from a loop plasma in which only the electrons were heated by events chosen from a power-law distribution with $\alpha = -2.5$ and equally spaced by an interval of $t_N = 5000$ s. **Left:** $EM(T)$ slope as a function of upper bound on fit interval for both the hot (red) and cool (blue) side of $EM(T)$. The shading denotes the uncertainty of the fit. The bottom axis corresponds to the varying upper limit on the fit to the cool side while the top axis corresponds to the varying upper limit on the fit to the hot side. **Right:** $EM(T)$ with the overlaid hot (red) and cool (blue) fit lines whose slopes correspond to those shown on the left. The cool power-law fits describe $EM(T)$ for $T < 4$ MK quite well while a similar fit on the hot side fails to accurately describe the shape of the emission measure distribution for $T > 4$ MK.

a is relatively insensitive to the fit interval, b varies between approximately 2 and 4.5 depending on the choice of bounds of the fit interval. Furthermore, the uncertainty in the fitting procedure for b is relatively large, with the average uncertainty over the entire range of $T_{h,max}$ being $\bar{\sigma}_b \approx 0.17$. Contrastingly, we find that $a \approx 2.3$ with little variation over all values of $T_{c,max}$ considered here and that $\bar{\sigma}_a \approx 0.018$, nearly an order of magnitude smaller than $\bar{\sigma}_b$. The overlaid fit lines in the right panel of Figure 7 similarly show that while $\log EM$ is roughly linear over $5.7 < \log T < 6.5$, this is not the case for the interval $6.7 < \log T < 7.2$. In particular, a function of the form T^{-b} cannot describe the hot shoulder in the emission measure distribution near $10^{7.1}$ K.

3.3.2. Emission Measure Ratio

Brosius et al. (2014), using observations of an active region from the *EUNIS-13* sounding rocket, found that the intensity ratio of Fe XIX (formed at $T \approx 10^{6.95}$ K) to Fe XII (formed at $T \approx 10^{6.2}$ K) is ~ 0.59 inside the AR core as compared to ~ 0.076 outside, providing possible evidence for impulsive heating. As a proxy for this intensity ratio and an alternative to the hot emission measure slope b , we propose using an emission measure ratio, $EM(T_{hot})/EM(T_{cool})$. Unlike an emission measure slope, a simple emission measure ratio gives information about the emission at only a single “hot” temperature relative to a single “cool” temperature. We choose $T_{hot} = 10^{6.95}$ K and $T_{cool} = 10^{6.3} \approx 2 \times 10^6$ K, the latter slightly higher (closer to $T_{peak} \approx 4$ MK) than the formation tempera-

ture of Fe XII such that the emission measure ratio is less sensitive to variations in the cool emission and thus a more accurate measure of the amount of hot plasma.

The emission measure ratio provides a way to compactly compare every point in our multidimensional parameter space while acknowledging that we are reducing 8×10^4 s of loop evolution to a single value. The left panel of Figure 8 shows the case in which only the electrons are heated, where each individual histogram (denoted by linestyle and color) corresponds to a different type of heating function. This means, for example, that the solid blue histogram includes emission measure ratios for all values of t_N , but for only those cases where heating events are chosen from a power-law distribution of $\alpha = -1.5$ and $t_{N,i} = t_N$ for all i (i.e. $\beta = 0$). We see that the emission measure ratio is largely insensitive to α and is peaked sharply at approximately 0.25; the distribution peaks at slightly higher values for the $\beta = 1$ case though the overall shape of the distribution is the same. Here we have not included the uniform heating case due to small number statistics (i.e. < 20 emission measure ratios). The right panel of Figure 8 shows these same emission measure ratios, but now separated by t_N . For example, the solid red histogram includes emission measure ratios for every type of heating function (i.e. uniform, all α and all β), but for only those runs where $t_N = 3000$ s. Note that we choose to only show results for five values of t_N for aesthetic purposes. We find that for $t_N \leq 3000$ s, the emission measure ratios are largely clustered below 0.5, with $t_N = 2000, 3000, 4000$ s peak-

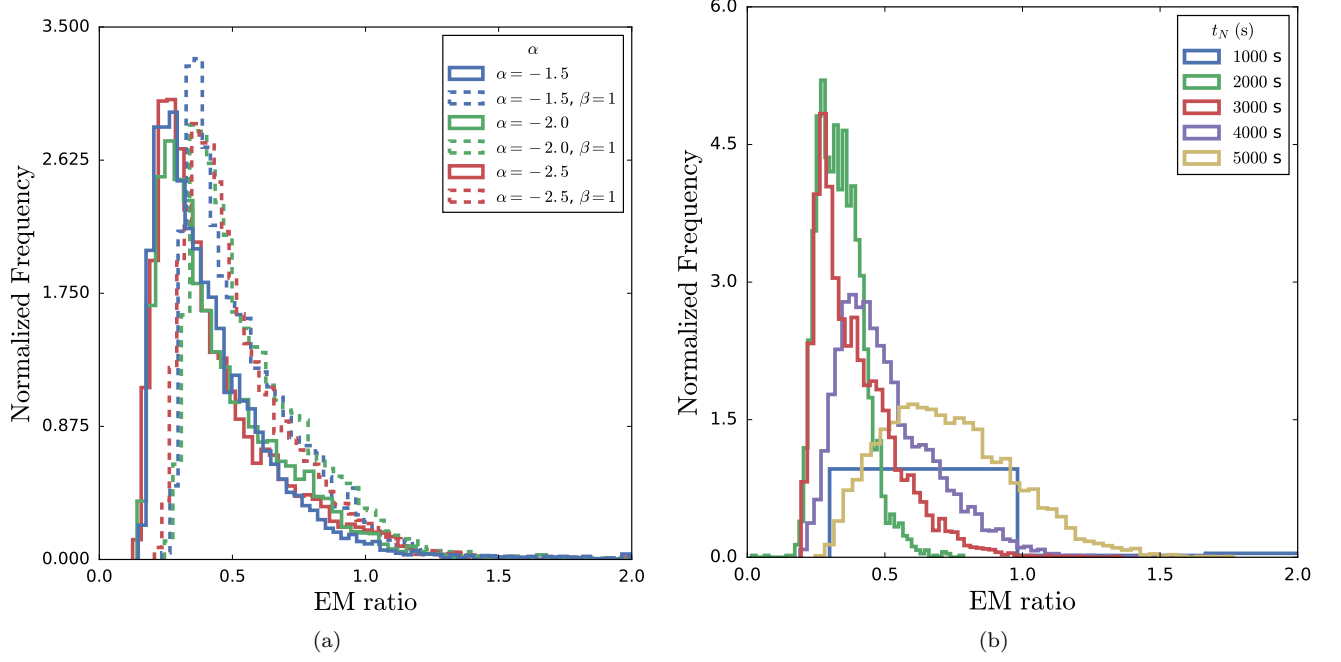


FIG. 8.— Histograms of emission measure ratios for all heating function types and heating frequencies for the case in which only the electrons are heated. In both panels each histogram is normalized such that for each distribution $P(x)$, $\int_{-\infty}^{\infty} dx P(x) = 1$ and the bin widths are calculated using the well-known Freedman-Diaconis formula (Freedman & Diaconis 1981). **Left:** Emission measure ratios separated by heating function type. **Right:** Emission measure ratios separated by waiting time, t_N . For aesthetic purposes, only five values of t_N are shown.

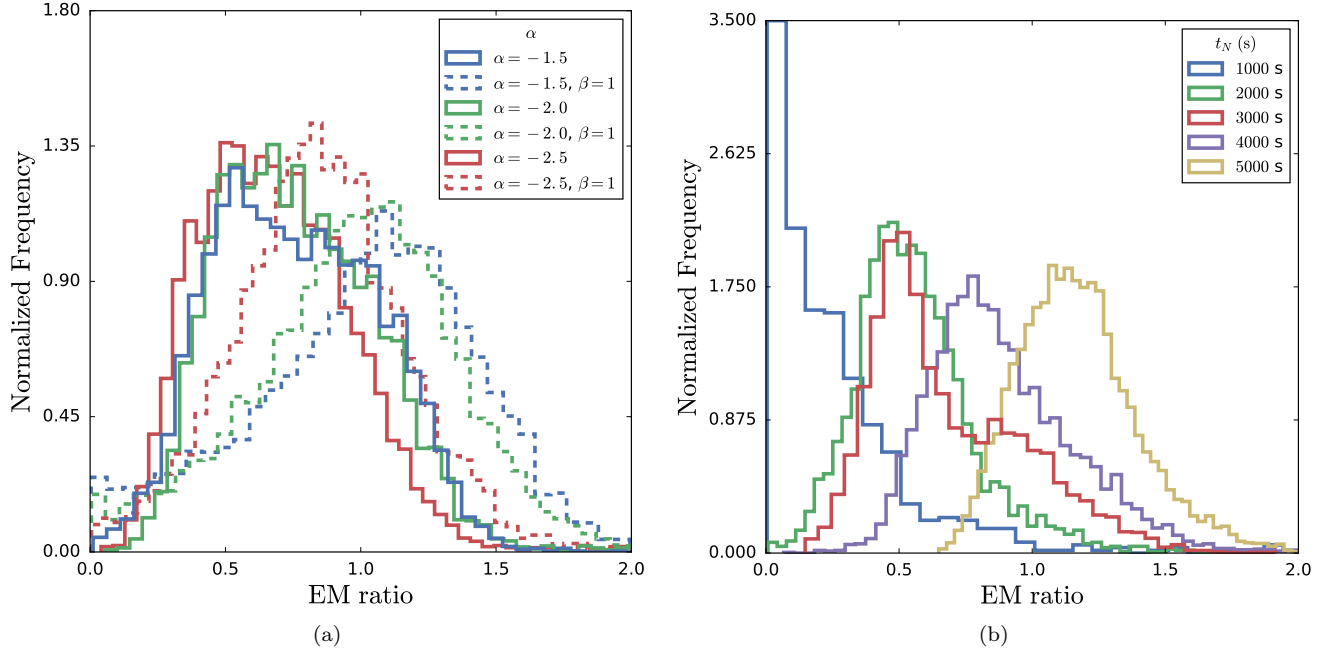


FIG. 9.— Same as Figure 8, but for the case where only the ions are heated.

ing between $\sim 0.3 - 0.45$. For $t_N > 4000$ s, the emission measure ratio seems to be more sensitive to the heating frequency.

Similarly, we compute the same emission measure ratio for the case in which only the ions are heated. The left panel of Figure 9 shows histograms for each type of heating function. Similar to the electron heating results, we find that the $\beta = 0$ distributions peak at lower values compared to the $\beta = 1$ distributions and that in the $\beta = 0$ case, the distribution of emission measure ratios is relatively insensitive to α . However, unlike the electron heating case, the distributions in all cases are much wider and peak at higher values, ~ 0.5 for $\beta = 0$ and > 1 for $\beta = 1$. Furthermore, in the $\beta = 1$ case, the $\alpha = -2.5$ distribution peaks at lower values compared $\alpha = -1.5, -2.0$. The right panel of Figure 9 shows the same emission measure ratios now grouped by waiting time where again we only show five values of t_N . With the exception of the $t_N = 2000$ s and $t_N = 3000$ s group, the distributions for each value of t_N are much more spread out (as compared Figure 8). In particular, $t_N = 5000$ s peaks above 1.0 and extends past 1.5 while $t_N = 1000$ peaks near 0 and drops off very steeply before 0.5. In general, the emission measure ratio appears to be more sensitive to t_N compared to the electron heating

case.

4. DISCUSSION

1. **> 10 MK present in nanoflare train runs relative to single pulse results from paper I**
2. **consistency of results with Cargill (2014) on the cool side; unsuitability of the hot emission measure slope**
3. **importance of density preconditioning in departures from IEQ**
4. **emission measure ratio results in light of Brosius et al, 2014**
5. **can we say something about possible heating frequencies? likelihood of electron heating over ion heating?**

5. CONCLUSIONS

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