

AE 6210: Advanced Dynamics Homework 2

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1 Problem Statement

The inertial frame is \mathbf{I} (gray). A helicopter is flying in a maneuver, and its body is modeled as a rigid body with frame \mathbf{A} (blue) attached to it. Frame \mathbf{A} has an angular acceleration ${}^I\boldsymbol{\alpha}^{\mathbf{A}}$ relative to frame \mathbf{I} . There is a point C on the rigid body that is fixed in the \mathbf{A} frame with a velocity ${}^I\mathbf{v}^C$ and acceleration ${}^I\mathbf{a}^C$ viewed in the inertial frame.

At a displacement \mathbf{r}^{CO} from point C is the rotor hub which is modeled as point O , where point O is also fixed in the \mathbf{A} frame. Point O is also the origin of frame \mathbf{H} (red), and frame \mathbf{H} is rotating at a constant angular speed ω^H relative to a \mathbf{A} about the $\hat{\mathbf{h}}_3 = \hat{\mathbf{a}}_3$ axis. The rotor blade mounting point, modeled as point P , is fixed in the \mathbf{H} frame at a displacement \mathbf{r}^{OP} along the $\hat{\mathbf{h}}_2$ axis.

The rotor blade is modeled as a rigid body with an attached frame \mathbf{B} (green). The blade flaps about the $\hat{\mathbf{b}}_1 = \hat{\mathbf{h}}_1$ axis where the flap angle varies as $\beta = \beta_0 + \beta_1 \sin \omega_b t$. The tip of the rotor blade is modeled as point T , and it is at a displacement \mathbf{r}^{PT} from the blade root along the $\hat{\mathbf{b}}_2$ axis.

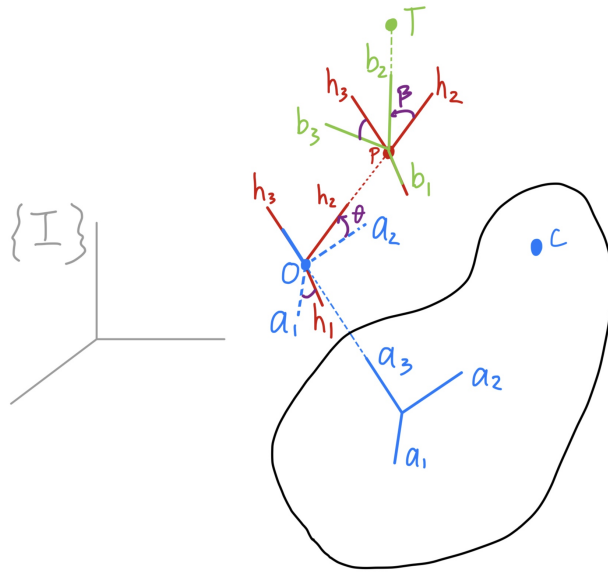


Figure 1: Diagram of the problem. A point that is the same color as a frame means that that point is fixed in that frame.

2 Rotor Blade Angular Velocity ${}^I\boldsymbol{\omega}^B$

The angular velocity of the rotor blade relative to the inertial frame ${}^I\boldsymbol{\omega}^B$ is the angular velocity of frame B relative to frame I . ${}^I\boldsymbol{\omega}^B$ can be expressed as the known values.

$${}^I\boldsymbol{\omega}^B = {}^I\boldsymbol{\omega}^A + {}^A\boldsymbol{\omega}^H + {}^H\boldsymbol{\omega}^B$$

$$\text{where } \begin{cases} {}^A\boldsymbol{\omega}^H = \omega^H \hat{\mathbf{a}}_3 \\ {}^H\boldsymbol{\omega}^B = \dot{\beta} \hat{\mathbf{b}}_1 = \omega_b \beta_1 \cos \omega_b t \hat{\mathbf{b}}_1 = \omega_b \beta_1 \cos \omega_b t \hat{\mathbf{h}}_1 \end{cases}$$

3 Rotor Blade Angular Acceleration ${}^I\boldsymbol{\alpha}^B$

The angular acceleration of the rotor blade relative to the inertial frame ${}^I\boldsymbol{\alpha}^B$ can be computed by taking the inertial frame derivative of ${}^I\boldsymbol{\omega}^B$ and using the transport theorem.

$$\begin{aligned} {}^I\boldsymbol{\alpha}^B &= \frac{{}^I d}{dt} [{}^I\boldsymbol{\omega}^B] \\ &= \frac{{}^I d}{dt} [{}^I\boldsymbol{\omega}^A + {}^A\boldsymbol{\omega}^H + {}^H\boldsymbol{\omega}^B] \\ &= {}^I\boldsymbol{\alpha}^A + \left(\frac{{}^A d}{dt} [{}^A\boldsymbol{\omega}^H] + {}^I\boldsymbol{\omega}^A \times {}^A\boldsymbol{\omega}^H \right) + \left(\frac{{}^H d}{dt} [{}^H\boldsymbol{\omega}^B] + {}^I\boldsymbol{\omega}^H \times {}^H\boldsymbol{\omega}^B \right) \end{aligned}$$

Noting that $\frac{{}^A d}{dt} [{}^A\boldsymbol{\omega}^H] = \mathbf{0}$, the equation simplifies.

$${}^I\boldsymbol{\alpha}^B = {}^I\boldsymbol{\alpha}^A + {}^I\boldsymbol{\omega}^A \times {}^A\boldsymbol{\omega}^H + \frac{{}^H d}{dt} [{}^H\boldsymbol{\omega}^B] + {}^I\boldsymbol{\omega}^H \times {}^H\boldsymbol{\omega}^B$$

$$\text{where } \begin{cases} \frac{{}^H d}{dt} [{}^H\boldsymbol{\omega}^B] = -\omega_b^2 \beta_1 \sin \omega_b t \hat{\mathbf{h}}_1 \\ {}^I\boldsymbol{\omega}^H = {}^I\boldsymbol{\omega}^A + {}^A\boldsymbol{\omega}^H \end{cases}$$

4 Rotor Blade Tip Velocity ${}^I\mathbf{v}^T$

Begin by computing the position of the rotor blade tip relative to the inertial frame's origin \mathbf{r}^{Tip} . Differentiating \mathbf{r}^{Tip} in the inertial frame gives the velocity of the rotor blade tip in the inertial frame.

$$\begin{aligned} \mathbf{r}^{Tip} &= \mathbf{r}^C + \mathbf{r}^{CO} + \mathbf{r}^{OP} + \mathbf{r}^{PT} \\ {}^I\mathbf{v}^T &= \frac{{}^I d}{dt} [\mathbf{r}^{Tip}] \\ &= \frac{{}^I d}{dt} [\mathbf{r}^C + \mathbf{r}^{CO} + \mathbf{r}^{OP} + \mathbf{r}^{PT}] \\ &= {}^I\mathbf{v}^C + \left(\frac{{}^A d}{dt} [\mathbf{r}^{CO}] + {}^I\boldsymbol{\omega}^A \times \mathbf{r}^{CO} \right) + \left(\frac{{}^H d}{dt} [\mathbf{r}^{OP}] + {}^I\boldsymbol{\omega}^H \times \mathbf{r}^{OP} \right) + \left(\frac{{}^B d}{dt} [\mathbf{r}^{PT}] + {}^I\boldsymbol{\omega}^B \times \mathbf{r}^{PT} \right) \end{aligned}$$

The final equation simplifies in terms of the known values.

$${}^I\mathbf{v}^T = {}^I\mathbf{v}^C + {}^I\boldsymbol{\omega}^A \times \mathbf{r}^{CO} + {}^I\boldsymbol{\omega}^H \times \mathbf{r}^{OP} + {}^I\boldsymbol{\omega}^B \times \mathbf{r}^{PT}$$

5 Rotor Blade Tip Acceleration ${}^I\mathbf{a}^T$

Differentiating ${}^I\mathbf{v}^T$ in the inertial frame gives the acceleration of the rotor blade tip in the inertial frame. For a more organized computation, ${}^I\mathbf{v}^T$ is differentiated in four segments.

First Term

$$\frac{{}^I d}{dt}[{}^I\mathbf{v}^C] = {}^I\mathbf{a}^C$$

Second Term

$$\begin{aligned}\frac{{}^I d}{dt}[{}^I\boldsymbol{\omega}^A \times \mathbf{r}^{CO}] &= \frac{{}^I d}{dt}[{}^I\boldsymbol{\omega}^A] \times \mathbf{r}^{CO} + {}^I\boldsymbol{\omega}^A \times \frac{{}^I d}{dt}[\mathbf{r}^{CO}] \\ &= {}^I\boldsymbol{\alpha}^A \times \mathbf{r}^{CO} + {}^I\boldsymbol{\omega}^A \times \left(\cancel{\frac{{}^A d}{dt}[\mathbf{r}^{CO}]}^{\mathbf{0}} + {}^I\boldsymbol{\omega}^A \times \mathbf{r}^{CO} \right)\end{aligned}$$

Third Term

$$\begin{aligned}\frac{{}^I d}{dt}[{}^I\boldsymbol{\omega}^H \times \mathbf{r}^{OP}] &= \frac{{}^I d}{dt}[{}^I\boldsymbol{\omega}^H] \times \mathbf{r}^{OP} + {}^I\boldsymbol{\omega}^H \times \frac{{}^I d}{dt}[\mathbf{r}^{OP}] \\ &= \frac{{}^I d}{dt}[({}^I\boldsymbol{\omega}^A + {}^A\boldsymbol{\omega}^H) \times \mathbf{r}^{OP}] + {}^I\boldsymbol{\omega}^H \times \frac{{}^I d}{dt}[\mathbf{r}^{OP}] \\ &= \frac{{}^I d}{dt}[{}^I\boldsymbol{\omega}^A] \times \mathbf{r}^{OP} + \frac{{}^I d}{dt}[{}^A\boldsymbol{\omega}^H] \times \mathbf{r}^{OP} + {}^I\boldsymbol{\omega}^H \times \left(\cancel{\frac{{}^H d}{dt}[\mathbf{r}^{OP}]}^{\mathbf{0}} + {}^I\boldsymbol{\omega}^H \times \mathbf{r}^{OP} \right) \\ &= {}^I\boldsymbol{\alpha}^A \times \mathbf{r}^{OP} + \left(\cancel{\frac{{}^A d}{dt}[{}^A\boldsymbol{\omega}^H]}^{\mathbf{0}} + {}^I\boldsymbol{\omega}^A \times {}^A\boldsymbol{\omega}^H \right) \times \mathbf{r}^{OP} + {}^I\boldsymbol{\omega}^H \times ({}^I\boldsymbol{\omega}^H \times \mathbf{r}^{OP})\end{aligned}$$

Fourth Term

$$\begin{aligned}\frac{{}^I d}{dt}[{}^I\boldsymbol{\omega}^B \times \mathbf{r}^{PT}] &= \frac{{}^I d}{dt}[{}^I\boldsymbol{\omega}^B] \times \mathbf{r}^{PT} + {}^I\boldsymbol{\omega}^B \times \frac{{}^I d}{dt}[\mathbf{r}^{PT}] \\ &= {}^I\boldsymbol{\alpha}^B \times \mathbf{r}^{PT} + {}^I\boldsymbol{\omega}^B \times ({}^I\boldsymbol{\omega}^B \times \mathbf{r}^{PT})\end{aligned}$$

Sum all of the terms for the final expression.

$$\begin{aligned}{}^I\mathbf{a}^T &= {}^I\mathbf{a}^C + {}^I\boldsymbol{\alpha}^A \times \mathbf{r}^{CO} + {}^I\boldsymbol{\omega}^A \times ({}^I\boldsymbol{\omega}^A \times \mathbf{r}^{CO}) \\ &\quad + {}^I\boldsymbol{\alpha}^A \times \mathbf{r}^{OP} + ({}^I\boldsymbol{\omega}^A \times {}^A\boldsymbol{\omega}^H) \times \mathbf{r}^{OP} + {}^I\boldsymbol{\omega}^H \times ({}^I\boldsymbol{\omega}^H \times \mathbf{r}^{OP}) \\ &\quad + {}^I\boldsymbol{\alpha}^B \times \mathbf{r}^{PT} + {}^I\boldsymbol{\omega}^B \times ({}^I\boldsymbol{\omega}^B \times \mathbf{r}^{PT})\end{aligned}$$

6 Numerical Example

Some numerical values were given for example implementation in MATLAB.

$$\begin{aligned}
 t &= 25 \text{ s} \\
 {}^I\boldsymbol{\omega}^A &= 1.0 \hat{\mathbf{a}}_1 + 2.0 \hat{\mathbf{a}}_2 + 3.0 \hat{\mathbf{a}}_3 \text{ (rad/s)} \\
 {}^I\boldsymbol{\alpha}^A &= 0.1 \hat{\mathbf{a}}_1 + 0.2 \hat{\mathbf{a}}_2 + 0.3 \hat{\mathbf{a}}_3 \text{ (rad/s}^2\text{)} \\
 {}^I\mathbf{v}^C &= 4.0 \hat{\mathbf{a}}_1 + 5.0 \hat{\mathbf{a}}_2 + 6.0 \hat{\mathbf{a}}_3 \text{ (m/s)} \\
 {}^I\mathbf{a}^C &= 0.4 \hat{\mathbf{a}}_1 + 0.5 \hat{\mathbf{a}}_2 + 0.6 \hat{\mathbf{a}}_3 \text{ (m/s}^2\text{)} \\
 x_0 &= 1.5 \text{ m} \\
 y_0 &= -2.5 \text{ m} \\
 \omega^H &= -10 \text{ rad/s} \\
 r_h &= 0.5 \text{ m} \\
 \beta_0 &= -0.1 \text{ rad} \\
 \beta_1 &= 0.1 \text{ rad} \\
 \omega_b &= 20 \text{ rad/s} \\
 L &= 10 \text{ m}
 \end{aligned}$$

Compute the rotation matrices where $[{}^B C^A]$ sends a vector resolved in the \mathbf{B} basis to the same vector resolved in the \mathbf{A} basis i.e. $\mathbf{v}_A = [{}^B C^A] \mathbf{v}_B$ where $\mathbf{v}_A = u_a \hat{\mathbf{a}}_1 + v_a \hat{\mathbf{a}}_2 + w_a \hat{\mathbf{a}}_3$ and $\mathbf{v}_B = u_b \hat{\mathbf{b}}_1 + v_b \hat{\mathbf{b}}_2 + w_b \hat{\mathbf{b}}_3$

$$[{}^H C^A] = \begin{bmatrix} \hat{\mathbf{a}}_1 \cdot \hat{\mathbf{h}}_1 & \hat{\mathbf{a}}_1 \cdot \hat{\mathbf{h}}_2 & \hat{\mathbf{a}}_1 \cdot \hat{\mathbf{h}}_3 \\ \hat{\mathbf{a}}_2 \cdot \hat{\mathbf{h}}_1 & \hat{\mathbf{a}}_2 \cdot \hat{\mathbf{h}}_2 & \hat{\mathbf{a}}_2 \cdot \hat{\mathbf{h}}_3 \\ \hat{\mathbf{a}}_3 \cdot \hat{\mathbf{h}}_1 & \hat{\mathbf{a}}_3 \cdot \hat{\mathbf{h}}_2 & \hat{\mathbf{a}}_3 \cdot \hat{\mathbf{h}}_3 \end{bmatrix} = \begin{bmatrix} \cos \omega_b t & -\sin \omega_b t & 0 \\ \sin \omega_b t & \cos \omega_b t & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$[{}^B C^H] = \begin{bmatrix} \hat{\mathbf{h}}_1 \cdot \hat{\mathbf{b}}_1 & \hat{\mathbf{h}}_1 \cdot \hat{\mathbf{b}}_2 & \hat{\mathbf{h}}_1 \cdot \hat{\mathbf{b}}_3 \\ \hat{\mathbf{h}}_2 \cdot \hat{\mathbf{b}}_1 & \hat{\mathbf{h}}_2 \cdot \hat{\mathbf{b}}_2 & \hat{\mathbf{h}}_2 \cdot \hat{\mathbf{b}}_3 \\ \hat{\mathbf{h}}_3 \cdot \hat{\mathbf{b}}_1 & \hat{\mathbf{h}}_3 \cdot \hat{\mathbf{b}}_2 & \hat{\mathbf{h}}_3 \cdot \hat{\mathbf{b}}_3 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 \\ 0 & \cos \beta & -\sin \beta \\ 0 & \sin \beta & \cos \beta \end{bmatrix}$$

$$[{}^B C^A] = [{}^H C^A] [{}^B C^H]$$

Now, every term can be resolved in the \mathbf{A} basis.

$${}^H\boldsymbol{\omega}_A^B = [{}^BC^A] \begin{bmatrix} \omega_b \beta_1 \cos \omega_b t \\ 0 \\ 0 \end{bmatrix}_B$$

$$\left(\frac{{}^H d}{{}^H dt} [{}^H\boldsymbol{\omega}^B] \right)_A = [{}^HC^A] \begin{bmatrix} -\omega_b^2 \beta_1 \sin \omega_b t \\ 0 \\ 0 \end{bmatrix}_H$$

$$\mathbf{r}_A^{OP} = [{}^HC^A] \begin{bmatrix} 0 \\ r_h \\ 0 \end{bmatrix}_H$$

$$\mathbf{r}_A^{PT} = [{}^BC^A] \begin{bmatrix} 0 \\ L \\ 0 \end{bmatrix}_B$$

Substituting the example values into the derived equations, the following values are obtained.

$${}^I\boldsymbol{\omega}_A^B = [0.5740, \quad 0.2844, \quad -7.0000]_A \text{ rad/s}$$

$${}^I\boldsymbol{\omega}_B^B = [{}^BC^A]^\top {}^I\boldsymbol{\omega}_A^B = [0.4143, \quad 0.5405, \quad -6.996]_B \text{ rad/s}$$

$${}^I\boldsymbol{\alpha}_A^B = [-27.4001, \quad 31.3414, \quad -0.5636]_A \text{ rad/s}^2$$

$${}^I\mathbf{v}_A^T = [16.1153, \quad 83.4428, \quad 8.1899]_A \text{ m/s}$$

$${}^I\mathbf{a}_A^T = [431.8179, \quad -168.8583, \quad 291.5781]_A \text{ m/s}^2$$

These values match perfectly with the expected values. The MATLAB code is given in a separate file.