

HOMER Help Manual

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1. Welcome to HOMER

Welcome to HOMER



What is HOMER?

HOMER (Hybrid Optimization of Multiple Electric Renewables), the micropower optimization model, simplifies the task of evaluating designs of both off-grid and grid-connected power systems for a variety of applications. When you design a power system, you must make many decisions about the configuration of the system: What components does it make sense to include in the system design? How many and what size of each component should you use? The large number of technology options and the variation in technology costs and availability of energy resources make these decisions difficult. HOMER's optimization and sensitivity analysis algorithms make it easier to evaluate the many possible system configurations.

How do I use HOMER?

To use HOMER, you provide the model with inputs, which describe technology options, component costs, and resource availability. HOMER uses these inputs to simulate different system configurations, or combinations of components, and generates results that you can view as a list of feasible configurations sorted by net present cost. HOMER also displays simulation results in a wide variety of tables and graphs that help you compare configurations and evaluate them on their economic and technical merits. You can export the tables and graphs for use in reports and presentations.

When you want to explore the effect that changes in factors such as resource availability and economic conditions might have on the cost-effectiveness of different system configurations, you can use the model to perform sensitivity analyses. To perform a sensitivity analysis, you provide HOMER with sensitivity values that describe a range of resource availability and component costs. HOMER simulates each system configuration over the range of values. You can use the results of a sensitivity analysis to identify the factors that have the greatest impact on the design and operation of a power system. You can also use HOMER sensitivity analysis results to answer general questions about technology options to inform planning and policy decisions.

How does HOMER work?

Simulation

HOMER simulates the operation of a system by making energy balance calculations in each time step of the year. For each time step, HOMER compares the electric and thermal demand in that time step to the energy that the system can supply in that time step, and calculates the flows of energy to and from each component of the system. For systems that include batteries or fuel-powered generators, HOMER also decides in each time step how to operate the generators and whether to charge or discharge the batteries.

HOMER performs these energy balance calculations for each system configuration that you want to consider. It then determines whether a configuration is feasible, i.e., whether it can meet the electric demand under the conditions that you specify, and estimates the cost of installing and operating the system over the lifetime of the project. The system cost calculations account for costs such as capital, replacement, operation and maintenance, fuel, and interest.

Optimization

After simulating all of the possible system configurations, HOMER displays a list of configurations, sorted by net present cost (sometimes called lifecycle cost), that you can use to compare system design options.

Sensitivity Analysis

When you define sensitivity variables as inputs, HOMER repeats the optimization process for each sensitivity variable that you specify. For example, if you define wind speed as a sensitivity variable, HOMER will simulate system configurations for the range of wind speeds that you specify.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

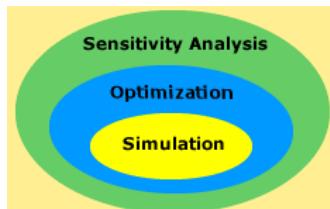
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1.1 Solving Problems with HOMER



Solving Problems with HOMER



HOMER simplifies the task of designing distributed generation (DG) systems - both on and off-grid. HOMER's optimization and sensitivity analysis algorithms allow

you to evaluate the economic and technical feasibility of a large number of technology options and to account for variations in technology costs and energy resource availability.

Working effectively with HOMER requires understanding of its three core capabilities - *simulation*, *optimization*, and *sensitivity analysis* - and how they interact.

Simulation, Optimization, Sensitivity Analysis

Simulation: At its core, HOMER is a simulation model. It will attempt to simulate a viable system for all possible combinations of the equipment that you wish to consider. Depending on how you set up your problem, HOMER may simulate hundreds or even thousands of systems.

Optimization: The optimization step follows all simulations. The simulated systems are sorted and filtered according to criteria that you define, so that you can see the best possible fits. Although HOMER fundamentally is an economic optimization model, you may also choose to minimize fuel usage.

Sensitivity analysis: This is an optional step that allows you to model the impact of variables that are beyond your control, such as wind speed, fuel costs, etc, and see how the optimal system changes with these variations.

HOMER models both conventional and renewable energy technologies:

Power sources in HOMER:

- solar photovoltaic (PV)
- wind turbine
- generator: diesel
- electric utility grid
- run-of-river hydro power
- biomass power
- generator: gasoline, biogas, alternative and custom fuels, cofired
- microturbine
- fuel cell

Storage in HOMER:

- flywheels
- customizable batteries
- flow batteries
- hydrogen

Loads in HOMER:

- get started quickly with the HOMER Quick Load Builder
- daily profiles with seasonal variation
- deferrable (water pumping, refrigeration)
- thermal (space heating, crop drying)
- efficiency measures

See also:

[Simulation Results](#)

[Optimization Results](#)

[Sensitivity Results](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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1.2 The HOMER Knowledgebase



Knowledgebase

The Knowledgebase is a searchabale database of questions from HOMER users concerning system modeling, training, downloads and licensing. Questions are addressed by HOMER support experts.

The Knowledgebase can be accessed online at <http://support.homerenergy.com/index.php?/Knowledgebase>List>

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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1.3 HOMER Professional Quick Start Guide

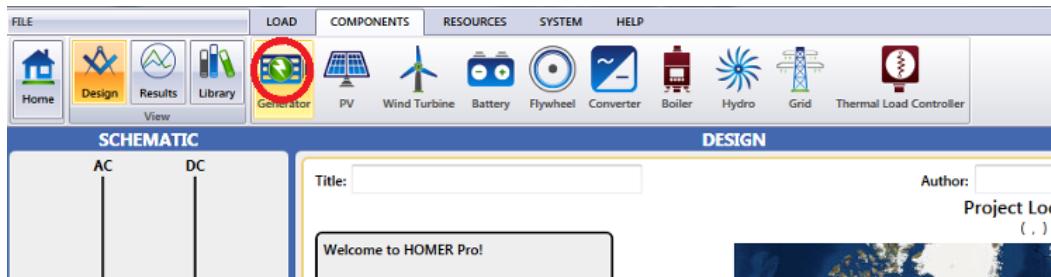
Quick Start Tutorial

HOMER® Professional can help you design the best micropower system to suit your needs. With HOMER Professional, you can:

- Evaluate off-grid or grid-connected system designs
- Choose the best system based on cost, technical requirements, or environmental considerations.
- Simulate many design configurations under market price uncertainty and evaluate risk
- Choose the best addition or retrofit for an existing system

This worked example is intended to get you started in HOMER Professional quickly by walking through one way to run an analysis. It is not intended to replace the study of how power systems operate or to cover all areas of HOMER. It should provide you with basic familiarity of the interface.

Step 1. Open HOMER Professional. A new project will display. Enter title, author, or notes if desired. Notice the Component, Load, and Resources tabs at the top of the screen. These allow you to navigate through the model. The load tab will be displayed at start-up.



Step 2. Switch to the Components tab. Select “Generator” from the component menu. Select “100 kW Genset” from the drop-down menu and click “Add Generator”. The generator specification menu will display and an icon will appear on the AC bus in the schematic on the left. In the costs table, enter the following values:

Size (kW) 1; Capital (\$) 1500; Replace (\$) 1200; and O&M (\$/hr) 0.05

This tells HOMER that the generator initially costs \$1,500 per kilowatt, costs \$1,200 per kilowatt to replace at the end of life, and costs \$0.05 per hour to operate and maintain (excluding fuel).

Step 3. In the Search Space table, change “Size (kW)” from 100 to 15. Change “Fuel Price (\$/L)” to 0.4.

The screenshot shows the HOMER Professional interface with the '100kW Genset' component selected. The 'Properties' panel shows the component name and abbreviation. The 'Costs' table is highlighted with red circles around the values: Size (kW) 1, Capital (\$) 1500, Replace (\$) 1200, and O&M (\$/hr) 0.05. The 'Search Space' panel shows the 'Size (kW)' field set to 15. The 'Fuel Resource' panel shows 'Diesel' selected. The 'Fuel' section shows 'Fuel Price (\$/L)' set to 0.4, which is also circled in red.

Step 4. Now choose “Wind Turbine” from the components menu. From the drop-down menu on the landing page, choose “Generic 10 kW”. Click “Add Wind Turbine”. In the costs table, enter:

Size (kW) 1; Capital (\$) 30000; Replace (\$) 25000; O&M (\$/yr) 500

Step 5. Similarly, add a battery from the components menu and choose “Generic 1 kWh Lead Acid”. Set the costs table values to: Size (kW) 1; Capital (\$) 300; Replace (\$) 300; O&M (\$/yr) 20. Change the number of batteries under “Search Space” to 8.

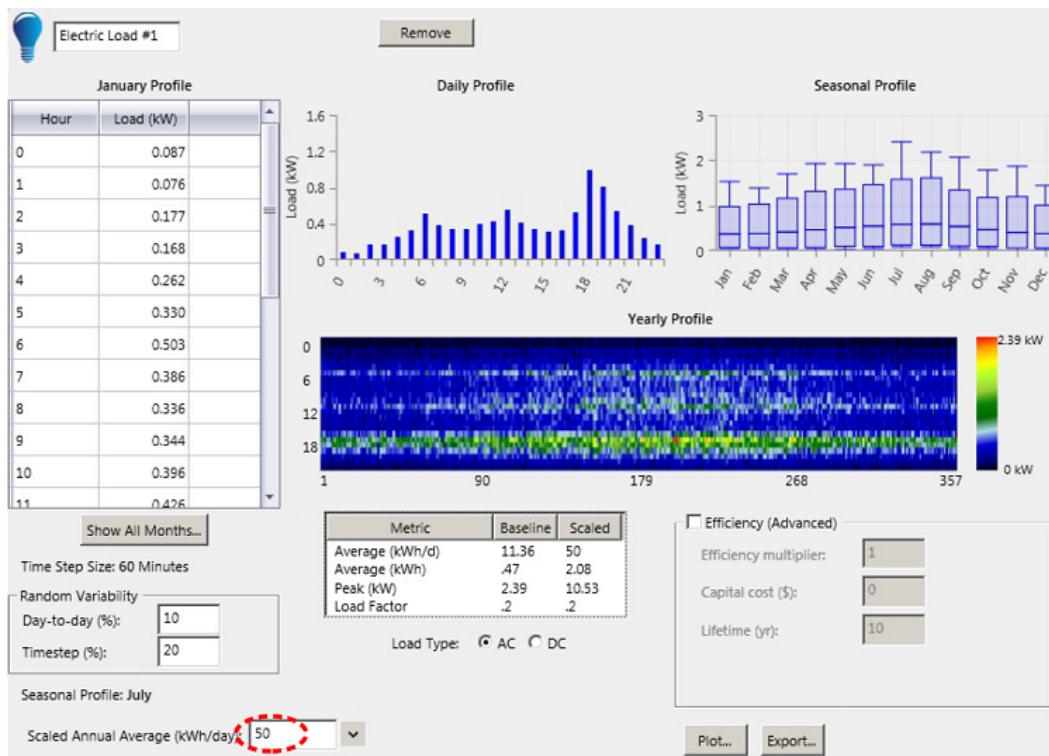
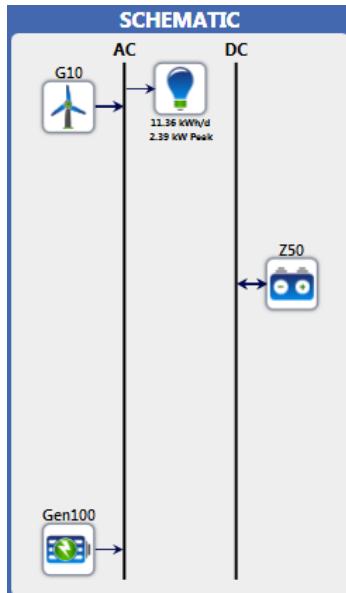
Step 6. Pick the Load tab at the top of the window and choose “Electric #1”. Use option 1: Create a synthetic load from a profile. Leave “Residential” selected and set the “Peak Month” to July. Click “Ok”.

Choose one of the following options:

1. Create a synthetic load from a profile.

Peak Month: January July NoneResidential

2. Import a load from a time series file.

Step 7. A load specification menu should display similar to the image below. Change the "Scaled Annual Average (kWh/day)" to 50.**Step 8.** The schematic on the left side of the window should now look like this:**Step 9.** Now you will specify the details of the wind resource. Select the "Resources" tab at the top and pick "Wind". You can enter monthly wind data manually or load it from a file. For the purpose of this example, manually enter 1 for all months below "Average Wind Speed (m/s)". Then change the "Scaled Annual Average (m/s)" to 4.

| Monthly Wind Data | | |
|-------------------|-----------------|--|
| Month | Average Wind Sp | |
| January | 1.000 | |
| February | 1.000 | |
| March | 1.000 | |
| April | 1.000 | |
| May | 1.000 | |
| June | 1.000 | |
| July | 1.000 | |
| August | 1.000 | |
| September | 1.000 | |
| October | 1.000 | |
| November | 1.000 | |
| December | 1.000 | |

Annual Average: 1.00

Scaled Annual Average (m/s):

Step 10. Set "Anemometer Height (m)" to 25 to indicate that the specified wind speed (in this case 4 m/s avg.) is as measured at 25 m above ground level.

Step 11. Click "Calculate".

Step 12. An error will be generated. That is because you need a converter to allow power to flow between the AC bus and the DC bus for the system to function.

Step 13. Select the Components tab and add a converter. Set the capital cost to \$1000 and the replacement cost to \$1000. Set the operations and maintenance cost to 100 \$/yr. In the search space table, add the values 0, 6, and 12 for Size (kW).

| Size (kW) |
|-----------|
| 0 |
| 6 |
| 12 |

Step 14. Now calculate again. The results will display. The upper table shows the best design for each case. In this optimization there is only one case. A system with a 6 kW converter is the lowest net present cost design. The lower table displays all configurations that were simulated for this single case – a system with a 6 kW converter and one with a 12 kW converter. The system with a 0 kW converter is not displayed since it is not feasible.

| Architecture | | | | | | | Cost | | | | | | | |
|--------------|------|---------|-----------|-----|--------|---------|----------------|----------|----------|----------------|-----------|--------|--------------|-------|
| ! | Wind | Battery | Generator | G10 | Gen100 | 1kWh LI | Converter (kW) | Dispatch | Init Cap | Operating Cost | NPC | COE | Ren Frac (%) | Footp |
| ! | Wind | Battery | Generator | G10 | Gen100 | 1kWh LI | Converter (kW) | Dispatch | Init Cap | Operating Cost | NPC | COE | Ren Frac (%) | Footp |
| <hr/> | | | | | | | | | | | | | | |
| ! | Wind | Battery | Generator | 1 | 15 | 8 | 6 | LF | \$60,900 | \$14,105 | \$241,213 | \$1.03 | 0 | 2,000 |
| <hr/> | | | | | | | | | | | | | | |
| ! | Wind | Battery | Generator | 1 | 15 | 8 | 6 | LF | \$60,900 | \$14,105 | \$241,213 | \$1.03 | 0 | 2,000 |
| ! | Wind | Battery | Generator | 1 | 15 | 8 | 12 | LF | \$66,900 | \$14,770 | \$255,705 | \$1.10 | 0 | 2,000 |

Step 15. Now that you have generated some simple results, you can go back and add additional system configurations (called "Search Space") and input variable values (i.e. fuel price; this is called "Sensitivity Analysis") to your optimization.

Return to the design menu:

Step 16. Select the battery icon in the schematic. Add more values to the quantity search space: 8, 16, 24.

| Search Space |
|--------------|
| Batteries |
| 8 |
| 16 |
| 24 |

Step 17. Do the same for the wind turbine search space: 0, 1, 2.

Step 18. For the generator, enter 10, 15, and 20 kW in the search space.

| Size (kW) | Capital (\$) | Replace (\$) | O&M (\$/hr) |
|-----------|--------------|--------------|-------------|
| 1 | 1500 | 1200 | 0.05 |

Step 19. These three variables (number of batteries, number of wind turbines, and size of generator) are configurations in the Search Space. We can also add sensitivity variables to see the effect of different environmental or economic variations. In the generator menu, click the down arrow next the "Fuel Price" and in the table that appears, enter 0.6, 0.8, 1.2, 1.8 and 2.6 \$/L.

Step 20. Similarly, we can check the impact of a larger or smaller load on our costs and optimal system configuration. In the load menu, click the down arrow next to "Scaled Annual Average (kWh/day)" and enter 30, 50, and 80 kWh/d.

Step 20. At the top of the window, choose the "Resources" tab and select "Wind". Click the down arrow next to "Scaled Annual Average (m/s)" and enter 2, 4, and 6.

Step 21. Press calculate again. HOMER will run a few thousand simulations, and the results tables will display. In the upper table, each row corresponds to one sensitivity case. For each case, the configuration for the lowest net present cost system is listed. Click on the column headings to sort by the different parameters. If you select a sensitivity case, the lower table will show all system configurations that were simulated for that case. Infeasible system configurations are not included.

In the image below, the sensitivity cases in the top table are sorted by number of batteries. The case with 0.80 \$/L fuel cost, 30 kWh/day average load, and 6 m/s average wind speed is selected. The winning system configuration for this case is listed in the top table: One G10 (general 10 kW) wind turbine, a 10 kW generator, 24 batteries (1 kWh lead acid), and a 6 kW converter.

In the lower table, all the simulation results for this case with different system configurations are shown, sorted by net present cost. The top row is the same winning system configuration that is listed in the upper table. The second row reports simulation results from a system with 16 batteries instead of 24. The initial capital cost decreases from \$58,200 to \$55,800, but the operating cost increases from \$4,841 to \$5,117, resulting in a higher net present cost.

Step 22. Above and to the right of the table in the results window is the option to switch to a graphic results display. Set the Fuel Cost to display on the x-axis and Wind Speed to display on the y-axis. Set the Avg. Load to 30 (kWh/day). The colors describe the optimal system configuration: in this optimization, the wind turbine is beneficial with higher average wind speeds and higher fuel cost (green shading). At lower wind speeds and fuel costs, the system configuration without the wind turbine (blue) yields a lower net present cost.

Double click on a system to view detailed simulation results. You can change the economic variables that determine net present cost, the optimal system selection criteria (lowest cost, weight, or fuel use), and other optimization settings in the Project menu:

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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1.4 Add-on Modules

Modules



Several add-on modules are available that add advanced functionality to HOMER Pro. New modules will become available as they are developed. The table below lists the currently available modules.

| Module | Features |
|-------------------------|--|
| Biomass | Biomass resource , bio-gas fuel, bio-gas and co-fired generator. |
| Hydro | Hydro component and hydro resource . |
| Combined Heat and Power | Thermal load , boiler , thermal load controller , and generator heat recovery ratio. |
| Advanced Load | Additional electric load and deferrable load . |

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2. Navigating HOMER



Navigating HOMER

HOMER has three project views: [Design](#), [Results](#), and [Library](#). When you first open HOMER, or when you load a new or existing project, the [Home](#) page is displayed.

The [Design](#) view is the next step. You can use the [Load](#), [Components](#), and [Resources](#) tabs to build your system while in the Design view. You can also use the [System](#) tab to change project parameters, check inputs, and change sensitivity and optimization variables.

Finally, when you click calculate, you will be taken to the [Results](#) view (also accessible from the Results button). Here you can review and plot the sensitivity cases, investigate optimal systems, and review the details of individual simulations.

The [Library](#) button accesses your library, where you can save definitions for components, resources, loads, grid connections, and simulation configurations.

Home

When you open a file or start a new project, HOMER displays the Home page. On the Home page, you can display and edit metadata describing your project including project author, title and description. You can also assign a location for your project with the map. If you plan to add PV to your system, picking a location while on the Home page can streamline the process of adding PV and a solar resource.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.1 Loads Tab



Loads Tab

The Loads tab contains primary (electrical), thermal, and deferrable loads. This help topic explains several aspects of the process of specifying a load:

- [Adding a Load to the Model](#) - Instructions on how to add a load
- [Load Profile Menu](#) - Change load specifications after the load is added to the model
- [Primary Load](#), [Thermal Load](#), [Deferrable Load](#), [Hydrogen Load](#) - More details on each load type

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.1.1 Adding a Load to the Model



Adding a Load to the Model

You can add electric or thermal load data using exactly the same process, described here. Measured load data is seldom available, so users often synthesize load data by specifying typical daily load profiles and then adding in some randomness. This process produces one year of hourly load data.

Electric Load Set Up

HOMER provides four methods to specify an electric load profile.

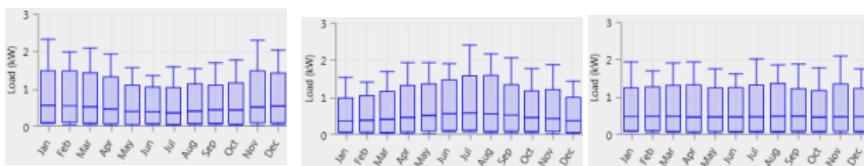
- **Create a synthetic load from a profile.**

This is a quick way to generate a load that can be relatively realistic. If you would like the load to have a cyclic annual variation, you can choose "January" or "July" as the peak month. Choosing "None" will yield an annual profile that is uniform except for random variation.

1. Create a synthetic load from a profile.

| | | | | | |
|-------------|-------------------------------|----------------------------|---------------------------------------|-------------|-----------------------------------|
| Peak Month: | <input type="radio"/> January | <input type="radio"/> July | <input checked="" type="radio"/> None | Residential | <input type="button" value="Ok"/> |
|-------------|-------------------------------|----------------------------|---------------------------------------|-------------|-----------------------------------|

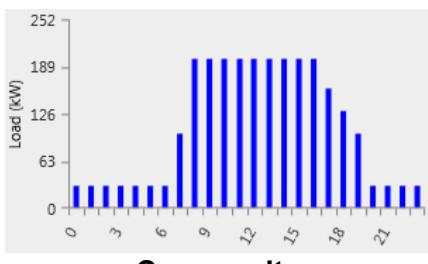
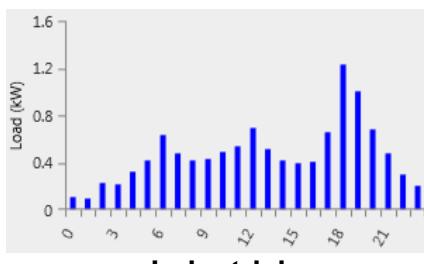
Peak Month: January Peak Month: July Peak Month: None

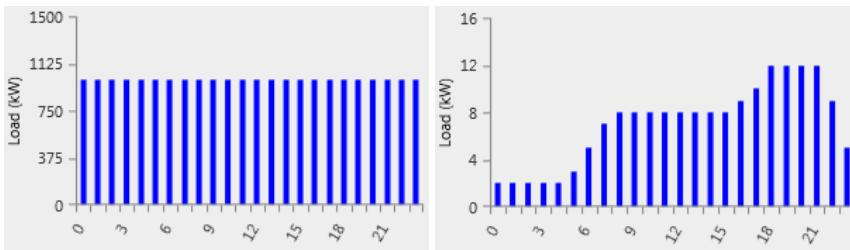


The drop-down menu contains a few pre-set load profiles: Residential, Commercial, Industrial, Community, and Blank. Blank is an empty template.

Residential

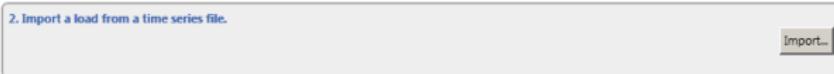
Commercial





These load templates all have different default overall magnitudes: 11.35, 2620, 24000, and 170 kWh/day respectively. You can easily scale the average load of any of them to fit your application by changing the value for "Scaled Annual Average (kWh/day)".

- Import a load from a time series file.



To import a file, you must prepare a text file that contains the electric load in each time step for a complete year.

Tip: You can import data with any time step down to one minute. HOMER detects the time step when you import the data file. For example, if the data file contains 8760 lines, HOMER will assume that it contains hourly data. If the data file contains 52,560 lines, HOMER will assume that it contains 10-minute data.

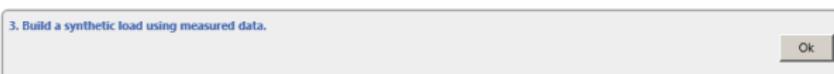
The data file must contain a single value on each line, where each line corresponds to one time step. Each value in the file represents the average load (in kW) for that time step. The first time step starts at midnight on January 1st. A sample input file appears below.

| File | Edit | View | Insert | Format | Help |
|-----------------------------|------|------|--------|--------|------|
| Sample.dmd - WordPad | | | | | |
| File | Edit | View | Insert | Format | Help |
| 0.80 | | | | | |
| 0.71 | | | | | |
| 0.63 | | | | | |
| 0.68 | | | | | |
| 0.71 | | | | | |
| 3.61 | | | | | |
| 2.70 | | | | | |
| 2.66 | | | | | |
| 2.16 | | | | | |
| 1.04 | | | | | |
| 0.90 | | | | | |
| 2.68 | | | | | |
| 2.71 | | | | | |
| 1.40 | | | | | |
| 1.33 | | | | | |
| 1.51 | | | | | |
| 2.95 | | | | | |

When you import data from a text file, HOMER makes a copy of the data set and integrates it with the HOMER (.hmr) file. Once the data is part of the HOMER file, HOMER no longer refers to the original text file. If you modify data in the original file, you must import the modified file in order for the modification to be included in the HOMER file. After you import a data file, HOMER calculates the average 24-hour load profile *for the whole year* displays it in the table and graph. HOMER also displays the name of the imported data file in the title of the load profile graph.

If you click Enter daily load profile(s) after importing data from a file, HOMER discards the data from the imported file and synthesizes new data based on the twelve monthly average load profiles it calculated from the imported data. You can edit synthesized data by selecting the month and changing values in the load profile table. To edit values from an imported file, you must edit the file directly and then import the modified file, as described above.

- Build a synthetic load using measured data.



You can import load data for specific devices as a CSV file with 24 hours of data, either in hourly or minute-resolution. Refer to the chart below for appropriate formatting. The first row and first two columns are ignored, reserved for user row titles if desired. The second row (column 3 and onward, highlighted below in yellow) should contain descriptive names for each device. Row 3 through row 1442 (or row 3 through 26 for hourly data, below in orange) contains the load profile for each device in watts.

Note that HOMER will accept a mix of 1440-row and 24-row data columns in a single document. HOMER will infer the time step based on the number of rows of data for each column individually.

| | A | B | C | D | E | F | G | H |
|---|-----------------------|-----------|------|------|------|------|------|------|
| 1 | Time (min) | | 0 | 1 | 2 | 3 | 4 | |
| 2 | Coffee Pot | Coffee | 1 | 857 | 1 | 1.1 | 1 | 1.. |
| 3 | Microwave | Micro | 1 | 0.8 | 1.1 | 1 | 0.9 | 1.. |
| 4 | 24" TV | TV 24 | 54.2 | 55.8 | 53.2 | 54.9 | 55.1 | 53.. |
| 5 | 15" Laptop 2 | Laptop 15 | 15.2 | 16.1 | 15.8 | 35.8 | 31.5 | 15.. |
| 6 | Refrigerator | Refr | 0.2 | 0.3 | 0.1 | 0.2 | 65.6 | 66.. |
| 7 | Fan | Fan | 14.3 | 15.8 | 14.9 | 15.1 | 15.7 | 14.. |
| 8 | Single LED Light 9 W | | 10.1 | 9.5 | 9.1 | 9.2 | 10.1 | 8.. |
| 9 | Single CFL Light 14 W | | 14.1 | 12.5 | 14.5 | 12.0 | 12.5 | 14.. |

Select the "Open Equipment Database" button in the upper right corner of the Load Designer menu, choose "Open...", and select your csv file. The load designer will import each column in the file as a separate device. You can drag and drop rows from the Equipment Database popup into the Load Designer. Once you are done, close the Equipment Database popup. You can now edit the quantities of each item, if desired. You can also set the "Jitter", which offsets the load profiles randomly so that load peaks in the duplicate devices (if set to quantity greater than one) will not always line up exactly.

• Choose a load from the library.

Choose this option to retrieve load profiles from the [HOMER Library](#).

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.1.2 Load Profile Menu



Load Profile Menu

Once you have created a load using one of the methods offered by the [Load Set Up](#), you will be taken to the Load Profile Menu. You can return to this page by clicking on the corresponding load icon in the system schematic or through the Load tab at the top of the HOMER window. The options for electric and thermal loads are similar.

The load profile menu displays the load profile graphically and presents summary statistics for the data. You can modify some details of the load in this menu.

Hourly Data

You can modify the daily profile, hour-by-hour in the table on the left side of the menu.

| January Profile | |
|-----------------|-----------|
| Hour | Load (kW) |
| 0 | 0.109 |
| 1 | 0.095 |
| 2 | 0.221 |
| 3 | 0.210 |
| 4 | 0.327 |
| 5 | 0.413 |
| 6 | 0.629 |
| 7 | 0.482 |
| 8 | 0.420 |
| 9 | 0.430 |
| 10 | 0.495 |
| 11 | 0.533 |

Show All Months...

Time Step Size: 60 Minutes

By clicking on "Show All Months..." you can set a different daily profile for weekends and weekdays and for each month of the year.

| Yearly Load Data | | | | | |
|--|---------|----------|-------|-------|------|
| <input type="checkbox"/> Copy Changes To Right | | | | | |
| Weekdays | | Weekends | | | |
| Hour | January | February | March | April | May |
| 0 | 0.109 | 0.109 | 0.109 | 0.109 | 0.10 |
| 1 | 0.095 | 0.095 | 0.095 | 0.095 | 0.09 |
| 2 | 0.221 | 0.221 | 0.221 | 0.221 | 0.22 |
| 3 | 0.210 | 0.210 | 0.210 | 0.210 | 0.21 |
| 4 | 0.327 | 0.327 | 0.327 | 0.327 | 0.32 |
| 5 | 0.413 | 0.413 | 0.413 | 0.413 | 0.41 |
| 6 | 0.629 | 0.629 | 0.629 | 0.629 | 0.62 |

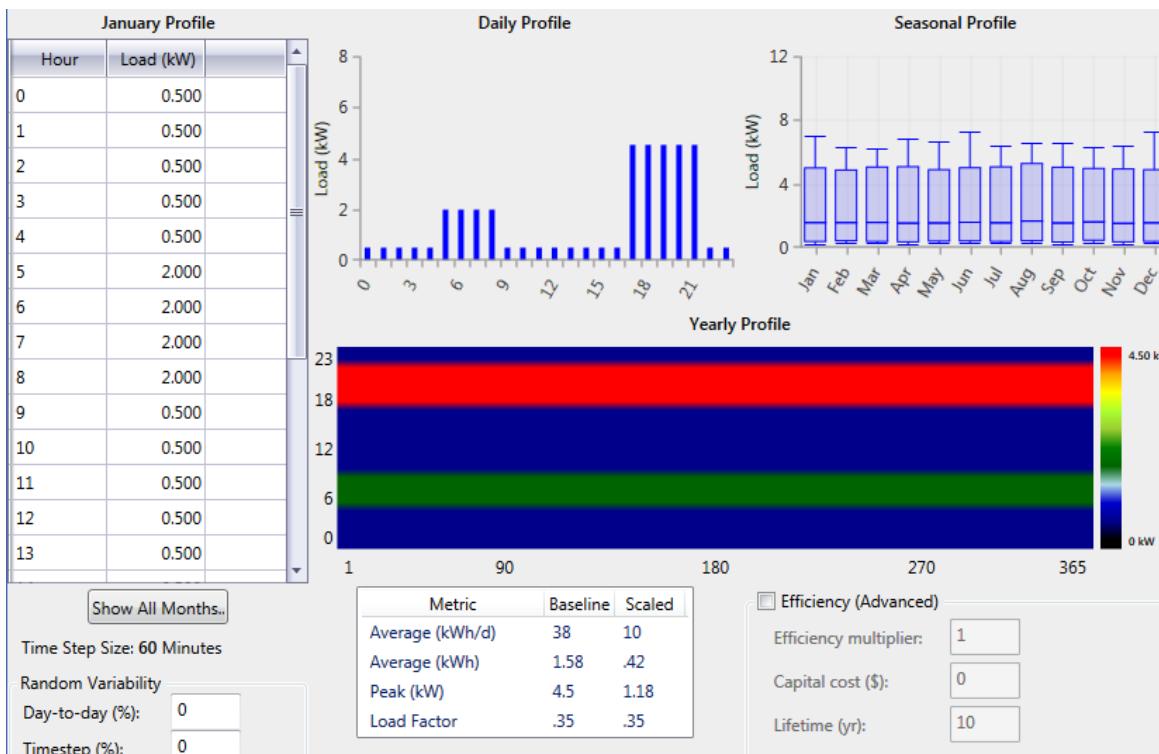
Ok **Cancel**

If you select "Copy Changes to Right", any value you enter will be copied across all remaining months. For example, if you enter "10" for January, hour 0, then all months, hour 0, will be set to 10. If you then enter "9" for hour 0 in February, January will stay set to 10 and February through December will be set to 9. You can edit values for weekends or for weekdays by selecting the tab at the top of the table. Changes made to the profile for weekends do not affect the profile for weekdays, and vice versa.

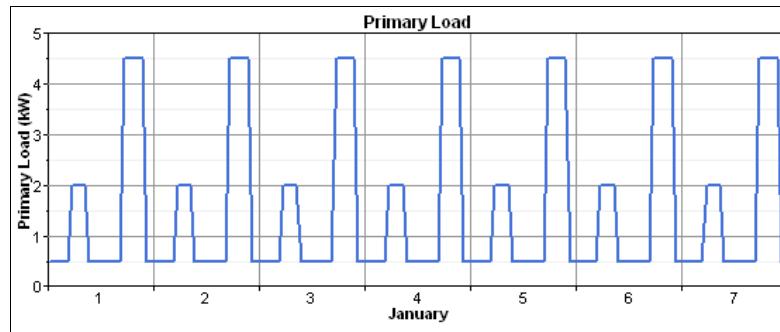
Random variability

Random variability is defined with two values, "Day-to-day" and "Timestep". If you have imported time-series load data, these values will be listed for reference and will not be editable. If you are generating synthetic load with HOMER, you can change these values.

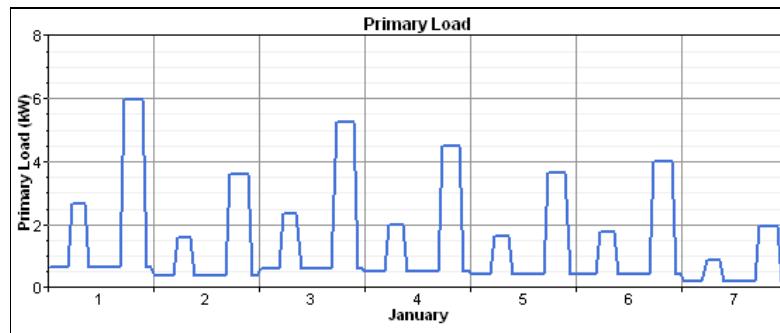
The random variability inputs allow you to add randomness to the load data to make it more realistic. To see the effect that each type of variability has on the load data, let's consider the following average load profile:



First let's look at the load data without any added variability. A plot of the first week of the year shows that the load profile repeats precisely day after day:

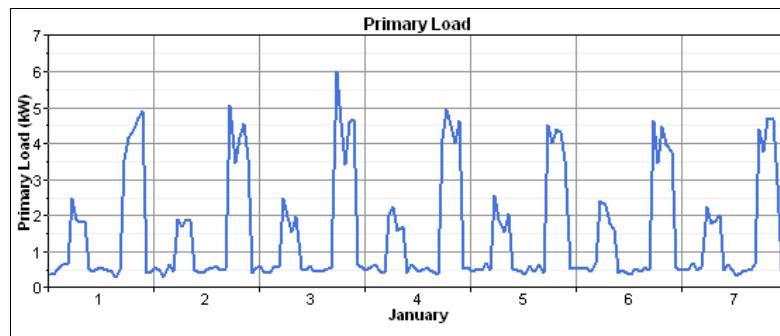


In reality though, the size and shape of the load profile will vary from day to day. So adding variability can make the load data more realistic. First, let's add 20% day-to-day variability. That causes HOMER to perturb each day's load profile by a random amount, so that the load retains the same shape for each day, but is scaled upwards or downwards. Now a plot of the first week of the year looks like this:



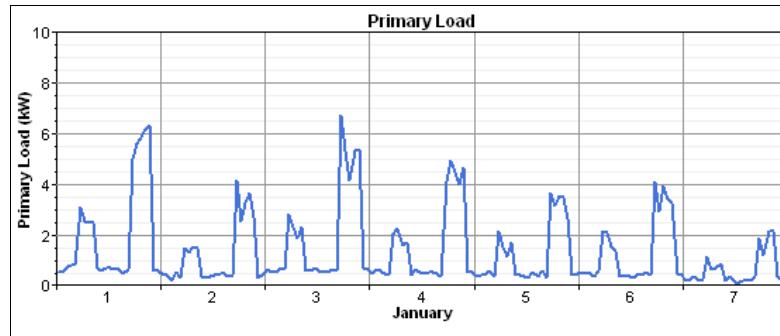
So day-to-day variability causes the *size* of the load profile to vary randomly from day to day, although the *shape* stays the same.

To see the effect of time-step-to-time-step variability, let's reset the day-to-day variability to zero and add 15% time-step-to-time-step variability. Now a plot of the first week of the year looks like this:



So the time-step-to-time-step variability disturbs the *shape* of the load profile without affecting its *size*.

By combining day-to-day and time-step-to-time-step variability, we can create realistic-looking load data. With 20% day-to-day variability and 15% time-step-to-time-step variability, a plot of the first week of the year looks like this:



The mechanism for adding day-to-day and time-step-to-time-step variability is simple. First HOMER assembles the year-long array of load data from the daily profiles you specify. Then it steps through that time series, and in each time step it multiplies the value in that time step by a perturbation factor α :

$$\alpha = 1 + \delta_d + \delta_{ts}$$

where:

δ_d = daily perturbation value

δ_{ts} = time step perturbation value

HOMER randomly draws the daily perturbation value once per day from a normal distribution with a mean of zero and a standard deviation equal to the "daily variability" input value. It randomly draws the time step perturbation value every time step from a normal distribution with a mean of zero and a standard deviation equal to the "time-step-to-time-step variability" input value.

Scaled data for simulation

| | | |
|----------------------------------|-----|----------------------------------|
| Scaled Annual Average (kWh/day): | 300 | <input type="button" value="▼"/> |
|----------------------------------|-----|----------------------------------|

HOMER uses scaled data for calculations. To create scaled data, HOMER multiplies each of the baseline data values by a common factor that results in an annual average value equal to the value that you specify in Scaled annual average. To determine the value of this factor, HOMER divides the scaled annual average by the baseline annual average. The scaled data retains the shape and statistical characteristics of the baseline data, but may differ in magnitude. The default value for the scaled annual average is the baseline annual average. When the two values are equal, the scaled data and baseline are identical. Note that the average load is reported in kWh/day but the peak load is reported in kW.

Two reasons to use a scaled annual average that is different from the baseline annual average are for unit conversion (eg. to convert from W to kW) or to perform a [sensitivity analysis](#) on the size of the thermal load. Click the sensitivities button (to the right of the text box) to enter multiple values for a sensitivity analysis.

The Export button allows you to export the scaled data to a text file.

Other options

| Variable | Description |
|---------------------------------------|--|
| Load Type | Select whether the load is alternating current (AC) or direct current (DC) |
| Efficiency (Advanced) | Check this box to calculate cost-effectiveness of efficiency measures. The inputs below are enabled when the box is checked. |
| Efficiency multiplier | The percentage by which the load is reduced when efficiency measures are in effect. |
| Capital cost (\$) | The cost of implementing efficiency measures, in \$. |
| Lifetime (yr) | The lifetime of efficiency measures, in years. |

See also

[Generating synthetic load data](#)

[Why do I have to scale load and resource data?](#)

[Does HOMER model solar thermal?](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.1.2.1 Efficiency



Efficiency (Advanced)

Use this window to analyze the cost-effectiveness of efficiency measures that reduce the electrical demand. For example, you might want to consider using fluorescent lights which are more efficient but also more expensive than incandescent lights. Using the Efficiency Inputs window, you could specify the cost of switching to fluorescent lights and the effect this would have on the size of the primary load. HOMER would then simulate each system both with and without the efficiency measures to see if their savings offset their cost.

The three variables used to define efficiency measures are as follows:

| Variable | Description |
|-----------------------|--|
| Efficiency multiplier | The factor by which this primary load would be multiplied if the efficiency package was implemented. (Enter 0.80 for a 20% reduction in load.) |
| Capital cost | The amount of money required to implement the efficiency package. |
| Lifetime | The number of years over which the capital cost is annualized. |

Example: Switching to fluorescent lights would reduce the demand of a particular system by 25%, but would cost an additional \$8000. The fluorescent lights are expected to last 6 years before they need to be replaced. In this case, the efficiency multiplier would be 0.75, the capital cost would be \$8000, and the lifetime

would be 6 years.

The Efficiency Inputs window is accessed by clicking the Efficiency Inputs button on the [Primary Load Inputs](#) window.

See also

[Primary Load Inputs window](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.1.3 Electric Load



Electric Load Inputs

Primary load is electrical load that the system must meet immediately in order to avoid [unmet load](#). In each time step, HOMER dispatches the power-producing components of the system to serve the *total primary load*.

The load characteristics required for HOMER to successfully model a system are sometimes not available, so HOMER can build (simulates) a load a few different ways (see [Adding a Load to the Model](#)). Once HOMER has created the load, you can edit it down to a 1-hr time step.

Note: To the right of the Annual Average input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also

[Generating synthetic load data](#)

[Finding data to run HOMER](#)

[Why do I have to scale load and resource data?](#)

For more information

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2.1.4 Thermal Load



Thermal Load Inputs

This feature requires the
[Combined Heat and Power Module](#).
Click for more information.

Thermal load is demand for heat energy. The heat may be needed for space heating, hot water heating, or some industrial process. The thermal load can be served by the boiler, by a generator from which waste heat can be recovered, or by surplus electricity. If you want a generator to serve the thermal load with waste heat, you must specify a non-zero value for that generator's [heat recovery ratio](#). If you want surplus electricity to serve the thermal load, you must indicate so on the [System Control Inputs](#) window.

Excess electricity can serve thermal load

This option is in the [System Control](#) tab of the [Project](#) screen.

Check this box if the system can convert [excess electricity](#) into heat to serve the thermal load. You should include the cost associated with such *resistive heating*

either in the cost of the component you expect to produce the excess electricity (a wind turbine, for example) or in the [system fixed capital cost](#).

See also

[Generating synthetic load data](#)

[Why do I have to scale load and resource data?](#)

[Does HOMER model solar thermal?](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.1.5 Deferrable Load

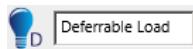


Deferrable Load

This feature requires the
[Advanced Load Module](#).
[Click for more information.](#)

Deferrable load is electrical load that must be met within some time period, but the exact timing is not important. Loads are normally classified as deferrable because they have some storage associated with them. Water pumping is a common example - there is some flexibility as to when the pump actually operates, provided the water tank does not run dry. Other examples include ice making and battery charging.

The descriptive name is used as a label to identify the deferrable load in the schematic.



Monthly Average Values

The baseline data is the set of 12 values representing the average deferrable load, in kWh/day, for each month of the year. The average deferrable load is the rate at which energy leaves the deferrable load storage tank. So it is the amount of power required to keep the level in the storage tank constant.

Enter the average deferrable load for each month of the year in the table on the left. HOMER assumes that the deferrable load is constant throughout each month. HOMER calculates the resulting annual average deferrable load and displays it below the table. The monthly average values are displayed in the deferrable load graph as you enter them.

Scaled data for simulation

Scaled Annual Average (kWh/d):

HOMER scales the baseline deferrable load data for use in its calculations. To scale the baseline data, HOMER multiplies each of the 12 baseline values by a common factor that results in an annual average value equal to the value that you specify in Scaled annual average. To determine the value of this factor, HOMER divides the scaled annual average by the baseline annual average. The scaled data retains the seasonal shape of the baseline data, but may differ in magnitude. The default value for the scaled annual average is the baseline annual average. When the two values are equal, the scaled data and baseline are identical. HOMER interprets a scaled annual average of zero to mean that there is no deferrable load.

You can use the scaled annual average to perform a [sensitivity analysis](#) on the size of the deferrable load.

Other inputs

| Variable | Description |
|--------------------|---|
| Storage capacity | The size of the storage tank, expressed in kWh of energy needed to fill the tank |
| Peak Load | The maximum amount of power, in kW, that can serve the deferrable load. In a water pumping application, it is equal to the rated electrical consumption of the pump. |
| Minimum Load Ratio | The minimum amount of power that can serve the deferrable load, expressed as a percentage of the peak load. In a water pumping application, if the pump is rated at 0.75 kW and requires at least 0.5 kW to operate, the minimum load ratio is 67%. |
| Electrical | Specifies whether the deferrable load must be served by alternating current (AC) or direct current (DC) power |

Bus

The deferrable load is second in priority behind the primary load, but ahead of charging the batteries. Under the [load following](#) strategy, HOMER serves the deferrable load only when the system is producing excess electricity or when the storage tank becomes empty. Under the [cycle charging](#) strategy, HOMER will also serve the deferrable load whenever a generator is operating and able to produce more electricity than is needed to serve the primary load.

Regardless of dispatch strategy, when the level of the storage tank drops to zero, the peak deferrable load is treated as a primary load. The dispatchable power sources (generator, grid or battery bank) will then serve as much as possible of the peak deferrable load.

Example: Each day, 4.5 m³ of water is needed for irrigation, and there is an 18 m³ water tank. At full power, the pump draws 400 W of electrical power and pumps 3 m³ per hour. To model this situation using HOMER:

- The peak deferrable load is 0.4 kW, which is the rated power of the pump.
- It would take the pump 6 hours at full power to fill the tank, so the storage capacity is 6 hours times 0.4 kW, which is 2.4 kWh.
- It would take the pump 1.5 hours at full power to meet the daily requirement of water, so the average deferrable load is 1.5 hours per day times 0.4 kW, which is 0.6 kWh/day.

Note: To the right of each numerical input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also:

[Why do I have to scale load and resource data?](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.1.6 Hydrogen Load



Hydrogen Load P

A hydrogen load represents an external demand for hydrogen. Either the reformer or the electrolyzer will serve this demand. You have the same options for specifying the hydrogen load as you do for the primary electrical load and the thermal load: you can either synthesize hourly data by entering daily load profiles, or you can import time series data. Please refer to the articles on the primary or thermal load for information on doing so.

See also:

[Primary Load Inputs](#)

[Thermal Load Inputs](#)

[Reformer Inputs](#)

[Electrolyzer Inputs](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.2 Components Tab



Components Tab

A component is a piece of equipment that is part of a power system. You can include [generator](#), [PV](#), [wind](#), [battery](#), [converter](#), [hydro](#), and [flywheel](#) components.

Select all the components you want to consider as part of the power system.

If you add a component that requires resource information, you should add the corresponding resource. The [resources help page](#) lists the resources and the corresponding components.

For the wind turbine, generator, and battery components, you can add more than one component to consider. Adding more than one component makes it possible to compare components that have different properties. You can compare wind turbines with different power curves, generators with different fuels and efficiency curves, and batteries with different chemistries.

Tip: Add more than one component only if you want to compare components that have different properties. Use the [search space](#) to compare different quantities or sizes of the same component.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.2.1 Generator



Generator

The Generator inputs window allows you to enter the cost, and size characteristics of a generator. It also provides access to the following tabs:

- [Fuel Resource](#): specify the fuel used by the generator, set the cost, and optionally set a maximum consumption.
- [Fuel Curve](#): set fuel consumption parameters
- [Emissions](#): enter the emission factors for the generator
- [Maintenance](#): set a maintenance costs and down-time for the generator.
- [Schedule](#): set the generator to be forced on, forced off, or optimized (default) according to the HOMER dispatcher.

Generator Size

Use the box labeled Generator Size to input what size generator you would like to consider.

| Search Space | |
|---|-----|
| Size (kW) | 100 |
| <input style="width: 100%; height: 20px;" type="button" value="..."/> | |

In this table, enter the generator sizes you want HOMER to consider as it searches for the optimal system. HOMER will use the information you entered in the cost table to calculate the costs of each generator size, interpolating and extrapolating as necessary. You can see the results in the cost curve graph.

By default, once you have added the generator component, HOMER will only consider systems that include a generator. If you want HOMER to consider systems both with and without a generator, be sure to include zero in the search space.

| Search Space | |
|---|----------|
| Size (kW) | 0 100 |
| <input style="width: 100%; height: 20px;" type="button" value="..."/> | |

System designers commonly specify just a single nonzero generator size, one large enough to comfortably serve the peak load. When given a choice of generator sizes, HOMER will invariably choose the smallest one that meets the [maximum annual capacity shortage](#) constraint, since smaller generators typically cost less to operate than larger generators.

Costs

The Costs box includes the initial [capital cost](#) and [replacement cost](#) of the generator, as well as annual [operation and maintenance](#) (O&M) costs. When specifying the capital and replacement costs, remember to account for all costs associated with the generator, including installation.

| Costs | | | |
|-------------|--------------|--------------|-------------|
| Size (kW) | Capital (\$) | Replace (\$) | O&M (\$/hr) |
| 1 | 500 | 500 | 0.03 |
| | | | |
| Multiplier: | ▼ | ▼ | ▼ |

Note that the [capital cost](#) is the initial purchase price, the [replacement cost](#) is the cost of replacing the generator at the end of its lifetime (relevant only if the [project lifetime](#) exceeds the generator lifetime), and the [O&M](#) cost is the annual cost of operating and maintaining the generator. The costs in each row should correspond to the size entered in the first column.

You can enter additional rows in the costs table to account for changing costs with scale. For more information on this, see the help article [Why a Cost Table and a Sizes To Consider Table?](#)

Cost Curve Example

In the cost table, enter the generator cost curve, meaning the way the cost varies with size. If you have a particular generator in mind, you can enter its size and cost. Take an example where a 40 kW generator costs \$20,000 initially, \$16,000 to replace at the end of its life, and \$0.60 per hour for operation and maintenance.

| Costs | | | |
|-------------|--------------|--------------|-------------|
| Size (kW) | Capital (\$) | Replace (\$) | O&M (\$/hr) |
| 1 | 500 | 400 | 0.015 |
| | | | |
| Multiplier: | ▼ | ▼ | ▼ |

HOMER only uses this table to calculate costs, so it is exactly equivalent to specify these costs as follows:

| Costs | | | |
|-----------|--------------|--------------|-------------|
| Size (kW) | Capital (\$) | Replace (\$) | O&M (\$/hr) |
| 2 | 1000 | 800 | 0.03 |
| | | | |

In other words, for both sets of inputs, the capital cost is \$500/kW, the replacement cost is \$400/kW, and the operating and maintenance cost is \$0.015/kW per hour.

Fuel Resource

| | | |
|-------------------------------|--------------------|--|
| Diesel | Fuel: | Diesel |
| PROPERTIES | Fuel Price (\$/L): | 1 |
| Lower Heating Value (MJ/kg): | 43.2 | <input type="checkbox"/> Limit Consumption |
| Density (kg/m ³): | 820 | Limit Amount (L/year): |
| Carbon Content (%): | 88 | 5000 |
| Sulfur Content (%): | 0.33 | |

This drop-down box contains all the fuels stored in your [component library](#). Choose the appropriate fuel from this list.

Fuel Curve

| Variable | Description |
|---------------------------------------|---|
| Intercept coefficient | the no-load fuel consumption of the generator divided by its rated capacity |
| Slope | marginal fuel consumption of the generator |

See the [Fuel Curve](#) tab documentation for more information on these inputs, and for instructions on how to use the fuel curve calculator.

Emissions

The Emissions tab in the [Generator](#) window gives you access to the following emissions factors input variables:

| Variable | Description |
|---------------------------------|---|
| Carbon Monoxide | The quantity of carbon monoxide emitted per unit of fuel consumed by the generator, in g/L* |

| | |
|---|--|
| Unburned Hydrocarbons | The quantity of unburned hydrocarbons emitted per unit of fuel consumed by the generator, in g/L* |
| Particulate Matter | The quantity of particulate matter emitted per unit of fuel consumed by the generator, in g/L* |
| Proportion of Fuel Sulfur Converted to PM | The fraction of the sulfur in the fuel that is emitted as particulate matter (the rest is emitted as sulfur dioxide), in % |
| Nitrogen Oxides | The quantity of nitrogen oxides emitted per unit of fuel consumed by the generator, in g/L* |

*These units will be in g/m³ for fuels that are measured in m³ and g/kg for fuels measured in kg.

Note: To the right of each numerical input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

Maintenance

HOMER can include the cost and downtime for specific maintenance tasks in the simulation. Check the option "Consider Maintenance Schedule" if you wish to use this option. The following inputs, found under the "Maintenance" tab, can be used to define a maintenance requirement:

| Variable | Description |
|-----------------------|--|
| Procedure | Descriptive name for the maintenance item |
| Interval (op hrs.) | How often the maintenance will have to be performed, in terms of number hours that the generator is operating |
| Down time (real hrs.) | Number of hours for which the generator will be forced off once the number when the end of the maintenance interval is reached |
| Cost (\$) | Cost of the maintenance procedure. This cost will be incurred at the end of each maintenance interval |

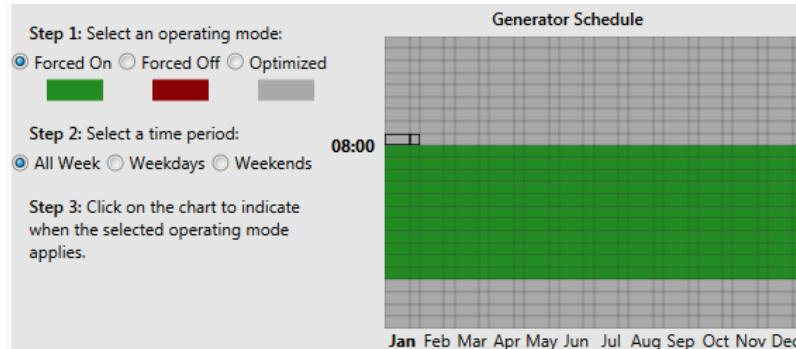
The generator maintenance down time will only be considered in the results if the maintenance occurs within the first year of the simulation. This is because the HOMER engine extrapolates for results beyond one year. This will not affect the dispatch decisions, since the engine amortizes the cost of the maintenance operation over the interval and so will include the anticipated cost in dispatch at every time step.

This behavior could cause an unexpected absence of a capacity shortage resulting from generator down time. For example, consider a system with one generator and a load, and zero capacity shortage allowed. Adding a maintenance item with an interval of 1,000 hours would make this system infeasible, since there would be a capacity shortage during the down time hours. If we set the maintenance interval to 9,000 hours, however, HOMER will report that the case is feasible.

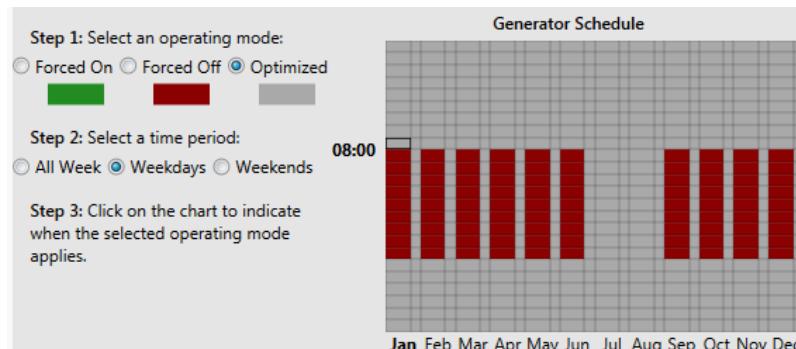
Schedule

By default, HOMER decides each time step whether or not to operate the generator based on the electrical demand and the economics of the generator versus other power sources. You can, however, use the generator schedule inputs to prevent HOMER from using the generator during certain times, or force it to use the generator during other times.

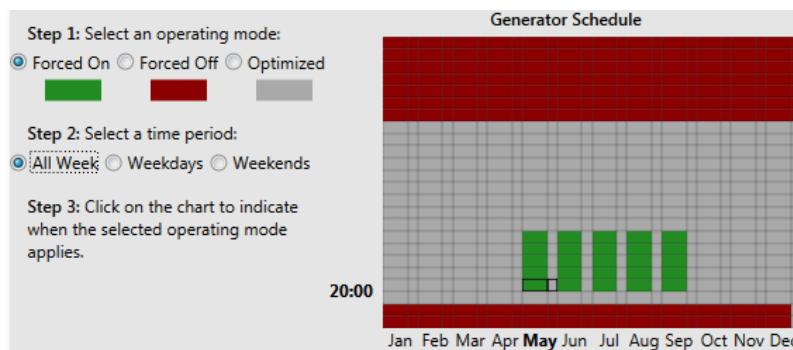
The schedule diagram on the right side of the window shows the times of the day and year during which the generator must operate and must not operate, and when HOMER can decide based on economics. In the example below, the generator must operate between 8am and 8pm every day. At all other times, HOMER can decide whether to run the generator based on economics.



It is also possible to treat weekdays and weekends differently. In the example below, the generator may not operate during school hours, which are 8am to 5pm on weekdays, except for July and August. (Such constraints are sometimes necessary in small village power systems because of generator noise.) At all other times, HOMER can decide whether to run the generator or not.



In the example below, the generator must operate during weekday evenings May through September, and must not operate before 7am or after 10pm throughout the year. At all other times, HOMER can decide whether to run the generator or not.



To modify the generator schedule, choose a drawing mode on the left side of the window and then draw on the schedule diagram on the right side of the window. For example, to force the generator to operate weekdays afternoons in July:

1. Click the button labeled Forced On
2. Click the button labeled Weekdays
3. Move the mouse to the column representing July and row representing 12pm-1pm
4. Click and drag the mouse to the row representing 5pm-6pm

Note that when you move the mouse over the schedule diagram, the cursor changes depending on whether you have selected weekdays, weekends, or all week.

Note: To the right of each numerical input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also:

[How HOMER calculates emissions](#)

For more information

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2.2.1.1 Fuel Curve



Fuel Curve P

The Fuel Curve tab provides assistance in calculating the two fuel curve inputs on the [Generator](#) window.

Generator size

Enter the rated size of the generator for which you have fuel consumption data.

Fuel consumption data

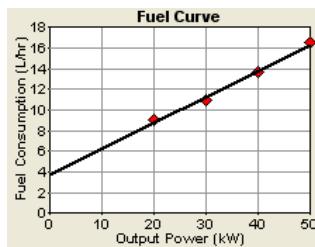
| Fuel Curve Table: | |
|-------------------|--------------------|
| Output (kW) | Consumption (L/hr) |
| 20 | 9 |
| 30 | 11 |
| 40 | 13.7 |
| 50 | 16.5 |

In this table, you enter data points on the generator's fuel curve. You must enter at least two points, but you can enter more than that if you have sufficient data.

Note: The units of the fuel consumption column change according to the units of the fuel this generator uses. If the generator consumes a fuel denominated in liters, the units of the fuel consumption column will be L/hr. But if the fuel is denominated in cubic meters, the units of the fuel consumption will be m³/hr.

HOMER plots the fuel consumption data in the fuel curve. The example shown below corresponds to the data shown in the table above. HOMER fits a line to the data points using the linear least-squares method. The straight line represents the line of best fit, which in this example fits the data very well. A straight line may

not represent certain types of generators, such as fuel cells and variable-speed diesels, quite as well. But for the more common constant-speed internal combustion generators and microturbines, the straight-line fuel curve is a good fit.



The y-intercept of the fuel curve is sometimes called the "no-load fuel consumption". This represents the amount of fuel consumed by the generator when idling (producing no electricity). The slope of the fuel curve is sometimes called the "marginal fuel consumption".

Using the straight line it fits to the fuel consumption data, HOMER calculates the generator's efficiency at various points between zero output and rated output. That calculation takes into account the energy content of the fuel. HOMER plots the results as the efficiency curve.

Calculated fuel curve parameters

Note that HOMER's two fuel curve inputs are not the intercept and slope, but rather the *intercept coefficient* and the slope. The intercept coefficient is equal to the intercept divided by the generator capacity. Defining the fuel curve in this manner allows HOMER to apply it to a family of generators, over a range of sizes. This is necessary when you enter multiple sizes in the "Sizes to consider" table of the [Generator Inputs](#) window, since the fuel curve inputs apply to each specified generator size.

The units of the two fuel curve parameters correspond to the units of the fuel used by the generator. For example, if the fuel is measured in liters, the fuel curve slope and intercept coefficient will be in units of L/hr/kW (liters per hour per kilowatt, or equivalently L/kWh).

When you click OK, HOMER copies the two calculated parameters to the Generator Inputs window.

See also

[Fuel curve intercept coefficient](#)

[Fuel curve slope](#)

[Generator Inputs window](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.2.2 PV (Photovoltaic)



Photovoltaic Panels

The PV inputs window allows you to enter the cost, performance characteristics and orientation of an array of photovoltaic (PV) panels as well as choose the sizes you want HOMER to consider as it searches for the optimal system. This window also provides access to the following tabs:

- [Inverter](#): If the "Electrical Bus" is set to "AC", inverter parameters are specified here.
- [MPPT](#): If the "Electrical Bus" is set to "DC", the parameters of the maximum power point tracker (DC to DC converter) are set here.
- [Advanced Inputs](#), where you can set certain advanced variables
- [Temperature](#): specify whether to consider the effect of ambient temperature on panel efficiency, and if so set the relevant inputs

You can also access the [Solar Resource](#) window by clicking the button at the top of the screen.

Costs

| Size (kW) | Capital (\$) | Replace (\$) | O&M (\$/yr) |
|--------------|-----------------|-----------------|----------------|
| 1 | 3000 | 3000 | 10 |
| | | | |

Multiplier:

The Costs box includes the initial [capital cost](#) and [replacement cost](#) per kilowatt of the PV system, as well as annual [operation and maintenance](#) (O&M) costs per kilowatt. When specifying the capital and replacement costs, remember to account for all costs associated with the PV system, which may include:

- PV panels
- mounting hardware
- tracking system
- control system (maximum power point tracker)
- wiring
- installation

Note that the capital cost is the initial purchase price, the replacement cost is the cost of replacing the PV system at the end of its lifetime (relevant only if the [project lifetime](#) exceeds the PV system lifetime), and the O&M cost is the annual cost of operating and maintaining the PV system.

Cost Curve

In the cost table, enter the PV *cost curve*, meaning the way the cost varies with size. Typically this requires only a single row since analysts often assume that PV costs vary linearly with size. In the sample above, the capital cost of PV panels is specified at \$7,000/kW and the replacement cost is specified at \$6,000/kW. The operating and maintenance cost is specified as zero.

You would enter multiple rows of data in the cost table if the cost of the PV subsystem was not linear with size. For example, if the capital and replacement costs dropped from \$7,000/kW to \$5,000/kW for quantities above 2 kW, you could fill in the cost table as follows:

| Costs | | | |
|-----------|--------------|--------------|-----------------|
| Size (kW) | Capital (\$) | Replace (\$) | O&M (\$/ yr) |
| 1 | 7000 | 7000 | 0 |
| 2 | 14000 | 14000 | 0 |
| 3 | 19000 | 19000 | 0 |

Multiplier:

If HOMER then had to simulate a system with a PV array size of 0.1 kW, it would extrapolate from the 1 kW and 2 kW costs, giving a capital cost of \$700. For a PV array size of 2.5 kW, HOMER would interpolate between the 2 kW costs and the 3 kW costs, giving a capital cost of \$16,500. For a PV array size of 6 kW, HOMER would extrapolate from the 2 kW and 3 kW costs, giving a capital cost of \$34,000.

Note that the [capital cost](#) is the initial purchase price, the [replacement cost](#) is the cost of replacing the PV panels at the end of their lifetime (relevant only if the [project lifetime](#) exceeds the PV array lifetime), and the operating and maintenance cost is the annual cost of operating and maintaining the PV array (often assumed to be zero).

PV Inputs

From the main section of the PV window, you can edit the following inputs:

| Variable | Description |
|---------------------------------|--|
| Electrical Bus | This determines whether the PV array produces AC or DC power. All PV cells produce DC electricity, but some PV arrays have built-in inverters to convert to AC. |
| Lifetime | The number of years before the PV panels must be replaced at the replacement cost specified in the costs table |
| Derating Factor | A scaling factor applied to the PV array power output to account for reduced output in real-world operating conditions compared to operating conditions at which the array was rated |

Note: To the right of each numerical input is a sensitivity button () which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

Inverter

If the PV system is on the AC electrical bus, you can specify a dedicated inverter. You can define the cost table, size (search space), and lifetime in a similar manner to other components. You can also specify the efficiency with a single value, or check "Use efficiency table".

If you don't want to model the inverter, you can set the cost to zero, enter a large size, and set the efficiency to 100%.

MPPT

A Maximum Power Point Tracker (or MPPT) is a DC to DC converter that matches the PV to the DC bus voltage, while varying the voltage of the PV array itself to maximize the power output. The inputs for the MPPT are identical to those for the inverter, described above.

Advanced Inputs

The Advanced Input tab contains options that affect the calculation of the PV power output. The article [How HOMER Calculates the Radiation Incident on the PV](#) contains more information on ground reflectance, panel slope, and panel azimuth.

| Variable | Description |
|------------------------------------|--|
| Ground Reflectance | The fraction of solar radiation incident on the ground that is reflected, in % |
| Tracking System | The type of tracking system used to direct the PV panels towards the sun |
| Panel Slope | The angle at which the panels are mounted relative to the horizontal, in degrees |
| Panel Azimuth | The direction towards which the panels face, in degrees |

Temperature

The Temperature tab contains setting model or ignore temperature effects. See [How HOMER Calculates the PV Array Output](#) for detailed information on temperature effects on power, nominal operating cell temperature, and efficiency at standard test conditions.

| Variable | Description |
|--|---|
| Consider Effect of Temperature | HOMER will consider the effect of PV cell temperature on the power output of the PV array |
| Temperature Coefficient of Power | A number indicating how strongly the power output of the PV array depends on cell temperature, in %/degrees Celsius |
| Nominal Operating Cell Temperature | The cell temperature at 0.8 kW/m ² , 20°C ambient temperature, and 1 m/s wind speed, in degrees Celsius |
| Efficiency at Standard Test Conditions | The maximum power point efficiency under standard test conditions, in % |

See also:

[How HOMER calculates the radiation incident on the PV array](#)

[How HOMER calculates the PV cell temperature](#)

[How HOMER calculates the output of the PV array](#)

[Search Space window](#)

[Standard test conditions](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.2.3 Wind Turbine



Wind Turbine

The Wind Turbine inputs window allows you to choose the type of wind turbine you want to model, specify its costs, and tell HOMER how many to consider as it searches for the optimal system. This window also provides access to the following tabs:

- [Power Curve](#): view and edit the power curve for the selected wind turbine
- [Turbine Losses](#): specify different loss modes
- [Maintenance](#): consider maintenance tasks, costs, and down time

You can access the [Wind Resource](#) window by clicking the button at the top of the screen.

Turbine type



This drop-down menu located at the top of the wind turbine set up page contains all the wind turbine types stored in your [component library](#). Choose an appropriate wind turbine model from this list. When you make a selection with this drop-down box, a summary of the selected wind turbine's properties are

displayed in the space below. Click on "Add Wind Turbine" to add the selected turbine to your model.

Costs

| Costs | | | |
|-------------|---|---|---|
| Quantity | Capital (\$) | Replacement (\$) | O&M (\$/year) |
| 1 | \$10,000.00 | \$10,000.00 | \$500.00 |
| | | | |
| Multiplier: | ( | ( | ( |

In the Costs table, the [capital cost](#) is the initial purchase price for a turbine, the [replacement cost](#) is the cost of replacing the wind turbine at the end of its lifetime (relevant only if the [project lifetime](#) exceeds the wind turbine lifetime), and the operating and maintenance cost is the annual cost of operating and maintaining the turbine (about 2% percent of the capital cost is typical).

When specifying the capital and replacement costs, remember to account for all costs associated with the wind energy system, which may include:

- turbine rotor and tower
- control system
- wiring
- installation

Cost Curve

In the cost table, enter the wind turbine's *cost curve* in as much detail as you would like. In the simplest case, where each wind turbine costs the same regardless of how many you purchase, you only need to enter one row of data in the cost table. You would enter a quantity of one, along with the per-turbine capital, replacement, and operating and maintenance costs. HOMER extrapolates these costs as needed, so if you modeled a system with three wind turbines, the associated capital, replacement, and O&M costs would be three times the values entered in the cost table.

| Costs | | | |
|-------------|---|---|--|
| Quantity | Capital (\$) | Replace (\$) | O&M (\$/yr) |
| 1 | 10000 | 9000 | 100 |
| 2 | 18000 | 16000 | 140 |
| | | | |
| Multiplier: |  |  |  |

You would enter multiple rows of data in the cost table if the cost of wind power was not directly proportional to the number of wind turbines purchased. In the example shown above, the second wind turbine is cheaper than the first (this could be because of a volume discount from the manufacturer or because certain fixed costs can be spread over multiple turbines). If the third turbine were cheaper yet, another row of costs could be added. With just these two rows specified though, HOMER would extrapolate the costs by assuming that the third, fourth, and subsequent turbines cost the same as the second.

Search Space

Enter the quantity of turbines you would like, or enter several quantities for HOMER to consider in the system optimization. Include a zero if you would like HOMER to consider systems without this wind turbine.

Electrical Bus

Select whether the turbine will produce AC or DC power. Power electronics are not modeled explicitly, but you can account for a dedicated converter efficiency by scaling the power curve.

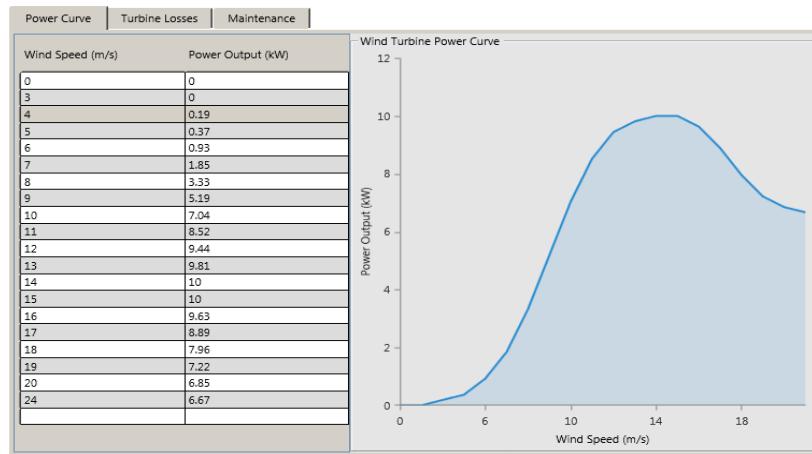
Site Specific Inputs

| Variable | Description |
|---------------------------------------|---|
| Lifetime | The number of years the turbine is expected to last before it requires replacement |
| Hub height | The height above ground of the hub (the center of the rotor), in meters |
| Consider ambient temperature effects? | HOMER will compensate for the change in air density with temperature. If checked, you must define a temperature resource. |

Note: To the right of each numerical input is a sensitivity button () which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

Power Curve

The Power Curve tab in the [Wind Turbine](#) window allows you to view the power curve of the selected wind turbine model in both tabular and graphical form. A wind turbine's power curve shows how much power it will produce depending on the incoming hub-height wind speed at standard atmospheric conditions. Use this graph to verify that the wind turbine you have selected is an appropriate size for your system.



Manufacturer Properties

The Manufacturer Properties box displays some basic information for the wind turbine model you have selected.

| Variable | Description |
|----------------|--|
| Abbreviation | A short label which is used to identify the wind turbine |
| Rated Capacity | The maximum rated power output for the wind turbine, in kW |
| Manufacturer | The company that manufacturers the wind turbine model |
| Website | The manufacturer's website |

See also

[Component library](#)

[Search Space window](#)

[Wind resource inputs window](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.2.4 Battery



Battery

The Battery window allows you to choose a type of battery, look at the technical details and specify battery costs. You can define new battery models in the [Component Library](#).

You can select your desired battery model using the drop-down menu at the top of the Battery Set Up page. This menu contains all the batteries stored in your library.

Hoppecke 10 OPzS 1000

Click on "Add Battery" to add the selected battery to your model. The battery specification page will then display. You can navigate between the Battery Set Up page and one or more battery specification pages with the tabs at the top of the pane.



Note: HOMER can only simulate one battery component at a time. You can add more than one battery component to the model, but each one must include a zero

in the search space. HOMER will simulate each of the battery types, one component at a time.

Costs

| Costs | | | |
|-------------|--------------|--------------|-------------|
| Quantity | Capital (\$) | Replace (\$) | O&M (\$/yr) |
| 1 | 1800 | 1600 | 10 |
| | | | |
| Multiplier: | ▼ | ▼ | ▼ |

The Costs box includes the initial [capital cost](#) and [replacement cost](#) per battery, as well as annual [operation and maintenance](#) (O&M) costs per battery. When specifying the capital and replacement costs, remember to account for all costs associated with the battery, including installation.

Note that the capital cost is the initial purchase price, the replacement cost is the cost of replacing the battery at the end of its lifetime (relevant only if the [project lifetime](#) exceeds the battery lifetime), and the O&M cost is the annual cost of operating and maintaining the battery.

Note: Below each numerical input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

Cost Curve

In this table, enter the battery's *cost curve* in as much detail as you would like. In the simplest case, where each battery costs the same regardless of how many you purchase, you only need to enter one row of data in the cost table. You would enter a quantity of one, along with the per-battery capital, replacement, and operating and maintenance costs. In the example shown above, each battery costs \$1,800 initially, \$1,600 to replace, and \$10 annually for operating and maintenance. HOMER extrapolates these costs as needed, so if you modeled a system with three batteries, the associated capital, replacement, and O&M costs would be three times the values entered in the cost table.

You would enter multiple rows of data in the cost table if the battery bank's costs were not directly proportional to the number of batteries purchased. In the example shown below, the fixed cost of the battery bank is \$2,000 initially plus \$30/yr for operating and maintenance. (This could be the cost of a room or a building in which to house the batteries.) Each battery then costs \$700 plus \$5/yr for operating and maintenance.

Note: HOMER will not assess this \$2,000 capital cost to a system that contains zero batteries. It applies only to systems containing battery banks. To add a fixed capital or O&M cost, see [Economics Inputs](#).

| Costs | | | |
|-------------|--------------|--------------|-------------|
| Quantity | Capital (\$) | Replace (\$) | O&M (\$/yr) |
| 0 | 2000 | 0 | 30 |
| 1 | 2700 | 700 | 35 |
| | | | |
| Multiplier: | ▼ | ▼ | ▼ |

Note that the [capital cost](#) is the initial purchase price, the [replacement cost](#) is the cost of replacing the batteries at the end of their lifetime (relevant only if the [project lifetime](#) exceeds the [battery lifetime](#), which is a calculated output), and the O&M cost is the annual cost of operating and maintaining the battery bank.

HOMER will use the number of batteries/strings you entered in the cost table to calculate the corresponding costs, interpolating and extrapolating as necessary. You can see the results in the cost curve graph.

Search Space with Strings

| Search Space | |
|--------------|--|
| Strings | |
| 0 | |
| 1 | |
| 2 | |
| 3 | |
| | |

Two or more batteries connected in series form a string, and strings are connected in parallel to form a battery bank. Batteries per string determines whether the sizes to consider table shows numbers of batteries or numbers of strings. In results tables and graphs, HOMER always displays the number of batteries, regardless of how you specify the number of batteries in the sizes to consider table. When the number of batteries per string is

- one, the sizes to consider table shows numbers of batteries;
- two or more, the sizes to consider table shows numbers of strings.

HOMER shows the DC bus voltage in parentheses next to the number of batteries per string. (The bus voltage is the battery's nominal voltage multiplied by the number of batteries per string.) You can use that to decide how many batteries to use per string.

Note: If you want to determine the optimal storage capacity and you are not concerned with the system voltage, you can set the number of batteries per string to one and ignore the bus voltage. This approach might be appropriate for a preliminary sizing analysis.

Battery Inputs

| Variable | Description |
|------------------------------|--|
| Batteries per String | A string is a set of batteries connected in series. The number of batteries per string multiplied by the nominal voltage is the bus voltage. |
| Initial State of Charge | The state of charge of the battery bank at the beginning of the HOMER simulation, in % |
| Minimum State of Charge | A lower limit on the state of charge of the battery bank, in % |
| Enforce Minimum Battery Life | Enable the Minimum Battery Life constraint |
| Minimum Battery Life | A lower limit on the lifetime of the battery bank (systems that do not meet this constraint are discarded as infeasible) |

Note: To the right of each numerical input is a sensitivity button () which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

Minimum Battery Life

The minimum battery life is a lower limit on the [lifetime of the battery bank](#). This constraint is not normally necessary, but you can use it if necessary to prevent HOMER from recommending a relatively small battery bank that lasts an unacceptably short time. For example, HOMER may determine that the optimal system contains a small battery bank that lasts only 1.5 years before needing replacement. If that 1.5 year replacement cycle is unacceptably short, you could implement a minimum 4 year battery lifetime, which would cause HOMER to discard that optimal system and choose another, probably with a larger battery bank. It would be a more expensive system (otherwise it would have been optimal without the battery life constraint) but it would conform to the constraint.

Manufacturer Properties

The Manufacturer Properties box displays some basic information for the battery type you have selected.

| Variable | Description |
|---------------------|--|
| Manufacturer | The company that manufactures the battery model |
| Website | Web address where more information on the battery model can be found |
| Nominal Voltage | The rated voltage (it is called nominal because the actual voltage varies according to the battery's operating conditions and state of charge) |
| Nominal Capacity | The amount of energy that can be drawn out of the battery at the rated discharge current, starting from a fully charged state, in kWh |
| Lifetime Throughput | The total amount of energy that can be cycled through the battery before it needs replacement, in kWh |
| Abbreviation | The abbreviation used in HOMER |

Note: HOMER does not model the battery charge controller as a separate component. You must include its cost and efficiency in the values you specify for the battery or in other components in the system.

See also

[How can I specify the DC bus voltage?](#)

[Component Library - Battery](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.2.5 Flywheel



Flywheel

A flywheel provides operating reserve on the AC bus, helping to absorb sudden increases in renewable power output or to make up for sudden decreases in renewable power output. rapid surges of power from renewable power from the wind turbine (or photovoltaic array) or alternatively supplying power to make up for

short term lulls.

A flywheel can also maintain power quality and system stability through active and reactive power control, although HOMER does not explicitly model those effects. These effects can be important in medium and high renewable penetration systems serving isolated networks or on soft grids (such as near the end of distribution lines).

Flywheels typically connect to the AC bus via an AC/AC inverter system that converts the variable-frequency AC power from the flywheel rotor to constant-frequency, grid-quality AC power on the AC bus.

Use the Flywheel Inputs window to choose the type of flywheel you want to model, specify its costs, and tell HOMER how many to consider as it searches for the optimal system configuration.

Flywheel type

This drop-down box contains all the flywheel types stored in your component library. Choose an appropriate flywheel model from this list. When you make a selection with this drop-down box, a summary of the selected flywheel's properties appears in the space below. To add a new flywheel or edit the properties, use the [component library](#).

Costs

In the cost table, enter the flywheel's *cost curve* in as much detail as you would like. In the simplest case, where each flywheel costs the same regardless of how many you purchase, you only need to enter one row of data in the cost table. You would enter a quantity of one, along with the per-flywheel capital, replacement, and operating and maintenance costs. HOMER extrapolates these costs as needed, so if you modeled a system with three flywheels, the associated capital, replacement, and O&M costs would be three times the values you entered in the cost table.

You would enter multiple rows of data in the cost table if the cost of flywheels was not directly proportional to the number of flywheels purchased. For example, the second flywheel may cost less than the first due to a volume discount or because certain fixed costs can be spread over multiple flywheels. If the third flywheel were cheaper yet, you could add a third row of costs.

Note that the [capital cost](#) is the initial purchase price, the [replacement cost](#) is the cost of replacing the flywheel at the end of its lifetime (relevant only if the [project lifetime](#) exceeds the flywheel lifetime), and the operating and maintenance cost is the annual cost of operating and maintaining the flywheel.

Search Space

In this table, enter the number of flywheels you want HOMER to consider as it searches for the optimal system configuration. Be sure to include a zero if you want to consider systems without flywheels. HOMER will use the information you entered in the cost table to calculate the corresponding costs, interpolating and extrapolating as necessary. You can see the results in the cost curve graph.

Note: You can also access the values in this table using the [Search Space](#) window.

Properties

| Variable | Description |
|----------|--|
| Lifetime | The number of years you expect the flywheel to last before it requires replacement |

Note: To the right of each numerical input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also

[Operating reserve](#)

[Component library](#)

[Search Space window](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.2.6 Converter



Converter

Any system that contains both AC and DC elements requires a converter. The Converter inputs window allows you to define the costs of the converter as well as specify inverter and rectifier parameters. It also gives you access to the converter [Search Space](#) where you can set one or more sizes to test.

Costs

| Size (kW) | Capital (\$) | Replace (\$) | O&M (\$/yr) |
|-----------|--------------|--------------|-------------|
| 1 | 750.00 | 750.00 | 0 |
| | | | |

Multiplier:

The Costs box includes the initial capital cost and [replacement cost](#) of the converter, as well as annual [operation and maintenance](#) (O&M) costs. When specifying the capital and replacement costs, remember to account for all costs associated with the converter, including installation.

Note that the [capital cost](#) is the initial purchase price, the replacement cost is the cost of replacing the converter at the end of its lifetime (relevant only if the [project lifetime](#) exceeds the converter lifetime), and the O&M cost is the annual cost of operating and maintaining the converter.

Cost Curve

In the cost table, you can enter the converter *cost curve*, meaning the way the cost varies with size. Typically this requires only a single row since analysts often assume that costs vary linearly with size. In the sample above, the capital cost and the replacement cost of the converter is specified at \$750/kW. The operating and maintenance cost is specified as zero.

You would enter multiple rows of data in the cost table if the cost of the converter subsystem was not linear with size. For example, if the capital and replacement costs dropped from \$750/kW to \$550/kW for quantities above 2 kW, you could fill in the cost table as follows:

| Size (kW) | Capital (\$) | Replace (\$) | O&M (\$/yr) |
|-----------|--------------|--------------|-------------|
| 1 | 750.00 | 750.00 | 0 |
| 2 | 1300 | 1300 | 0 |
| | | | |

Multiplier:

If you specify sizes other than those listed in the cost table, HOMER will interpolate or extrapolate based on the nearest two data points.

Inverter inputs

An inverter converts DC electricity to AC electricity. The Inverter Inputs box contains the following inputs:

| Variable | Description |
|-----------------------------|--|
| Lifetime | The expected lifetime of the inverter, in years |
| Efficiency | The efficiency with which the inverter converts DC electricity to AC electricity, in % |
| Parallel with AC generator? | Check this box if the inverter can operate at the same time as one or more AC generators. Inverters that are not able to operate this way are sometimes called switched inverters. |

Rectifier inputs

A rectifier converts AC electricity to DC electricity. The Rectifier Inputs box contains the following inputs:

| Variable | Description |
|-------------------|---|
| Relative capacity | The rated capacity of the rectifier relative to that of the inverter, in % |
| Efficiency | The efficiency with which the rectifier converts AC electricity to DC electricity, in % |

Note: To the right of each numerical input is a sensitivity button ()which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

Note: HOMER assumes the inverter and rectifier efficiencies are constant. In fact, most solid-state converters are less efficient at very low load because of

standing losses.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.2.7 Boiler



Boiler

This feature requires the
[Combined Heat and Power Module](#).
[Click for more information](#).

HOMER considers the serving of thermal load to be less important than the serving of electric load. When dispatching generators to serve the electric load, HOMER considers the value of any usable waste heat that can be recovered from each generator, but it will not dispatch a generator simply to serve the thermal load. It assumes the boiler can serve any thermal load that the generators do not. In other words, HOMER treats the boiler as a backup source of heat that can serve any amount of thermal load whenever necessary. HOMER automatically adds a boiler to the system when you add a thermal load. There is no cost associated with the boiler.

Fuel Resource

This drop-down box contains all the fuels stored in your [component library](#). Choose the appropriate fuel from this list. When a fuel is selected from the drop-down menu, detailed properties of the selected fuel are displayed.

| | | | | | | | | | |
|---|--|------------------------------|------|-------------------------------|-----|---------------------|----|---------------------|------|
| <input style="width: 100%; height: 25px;" type="button" value="Diesel"/> | <p>Fuel: Diesel</p> <p>Fuel Price (\$/L): <input type="text" value="1"/></p> <p><input type="checkbox"/> Limit Consumption</p> <p>Limit Amount (L/year): <input type="text" value="5000"/></p> | | | | | | | | |
| PROPERTIES <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 30%;">Lower Heating Value (MJ/kg):</td> <td style="width: 70%;">43.2</td> </tr> <tr> <td>Density (kg/m³):</td> <td>820</td> </tr> <tr> <td>Carbon Content (%):</td> <td>88</td> </tr> <tr> <td>Sulfur Content (%):</td> <td>0.33</td> </tr> </table> | | Lower Heating Value (MJ/kg): | 43.2 | Density (kg/m ³): | 820 | Carbon Content (%): | 88 | Sulfur Content (%): | 0.33 |
| Lower Heating Value (MJ/kg): | 43.2 | | | | | | | | |
| Density (kg/m ³): | 820 | | | | | | | | |
| Carbon Content (%): | 88 | | | | | | | | |
| Sulfur Content (%): | 0.33 | | | | | | | | |

You can create a new fuel type and remove or redefine an existing fuel in the library.

Fuel Price

Enter the price for the chosen fuel, and add sensitivity values for this cost. Will depend on the fuel, either in \$/L or \$/m³.

Efficiency

Enter the fraction of the fuel's energy that gets converted to heat in the boiler.

Emissions factors

In this box, you can modify the following variables:

| Variable | Description |
|---|--|
| Carbon Monoxide Emissions Factor | The quantity of carbon monoxide (in grams) emitted per unit of fuel consumed by the boiler |
| Unburned Hydrocarbons Emissions Factor | The quantity of unburned hydrocarbons (in grams) emitted per unit of fuel consumed by the boiler |
| Particulate Matter Emissions Factor | The quantity of particulate matter (in grams) emitted per unit of fuel consumed by the boiler |
| Proportion of fuel sulfur emitted as PM | The fraction of the sulfur in the fuel that is emitted as particulate matter (the rest is emitted as sulfur dioxide) |
| Nitrogen Oxides Emissions Factor | The quantity of nitrogen oxides (in grams) emitted per unit of fuel consumed by the boiler |

See also:

[How HOMER calculates emissions](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.2.8 Hydro



Hydro

This feature requires the
[Hydro Module](#).
[Click for more information](#).

HOMER can only consider a single size of hydro system. For this reason, the Hydro Inputs window does not contain tables of costs or sizes to consider. Instead, you simply specify the cost and properties of the size of hydro system that you want to consider.

Economics

These inputs specify the costs of the hydro system. Remember to include all costs associated with the hydro system, including the civil works.

| Variable | Description |
|------------------|---|
| Capital Cost | The initial capital cost of the hydro system |
| Replacement Cost | The replacement cost of the hydro system |
| O&M Cost | The annual cost of operating and maintaining the hydro system |
| Lifetime | The number of years that the hydro system is expected to last |

Turbine

These inputs specify the properties of the hydro turbine.

| Variable | Description |
|------------------------------------|--|
| Available Head | The vertical drop between the intake and the turbine |
| Design Flow Rate | The flow rate for which this hydro turbine was designed. It is often the flow rate at which the turbine operates at maximum efficiency. |
| Minimum Flow Ratio | The minimum flow rate of the hydro turbine, as a percentage of its design flow rate. Below this rate, the turbine will produce no power. |
| Maximum Flow Ratio | The maximum flow rate of the hydro turbine, as a percentage of its design flow rate. The turbine will generate power at the specified efficiency up to this flow. Additional flow above this level will not increase turbine power output. |
| Efficiency | The efficiency with which the hydro system converts the energy in the water to electricity |
| Generator Type | The type of current (AC or DC) produced by the hydro turbine |

Intake pipe

This input allows you to specify the frictional losses that occur in the intake pipe which reduce the energy of the water before it goes through the hydro turbine.

| Variable | Description |
|--------------------------------|--|
| Pipe Head Loss | Pipe friction losses expressed as a percentage of the available head |

Tip: For assistance in calculating the pipe head loss, click the Pipe Head Loss Calculator button.

Systems to consider

The choice you make in this section will affect which systems HOMER considers as it searches for the least-cost system.

| Variable | Description |
|--|---|
| Simulate systems both with and without the hydro turbine | Choose this option to simulate systems both with and without the hydro turbine. HOMER will rank the systems according to cost so you can see whether or not the hydro system is cost-effective. |
| Include the hydro turbine in all simulated systems | Choose this option if you want all systems to include the hydro turbine. |

Note: To the right of each numerical input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also:

[Calculating hydro power output](#)

[Pipe Head Loss Calculator](#) window

The hydro section of [Recommended Reading](#)

[Why do I have to scale load and resource data?](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.2.8.1 Pipe Head Loss Calculator



Pipe Head Loss Calculator

This window helps you calculate the head loss in the intake pipe of the hydro power system. Enter the flow rate along with the length, diameter, and material of the pipe, and HOMER will calculate the resulting head loss using the standard fluid mechanics equations on which the Moody diagram is based.

This window provides assistance in estimating the value of the [pipe head loss](#).

| | |
|--------------------|--|
| Available Head | The vertical drop between the intake and the turbine (specified on the Hydro input window) |
| Design Flow Rate | The flow rate for which you wish to calculate the head loss. Although in reality the head loss changes with flow rate, HOMER assumes the head loss is constant. |
| Pipe Length | The length of the pipe between the intake and the turbine |
| Pipe Diameter | The diameter of a circular pipe. If the pipe is not circular, you must calculate and specify the hydraulic diameter. An explanation of hydraulic diameter is available in most standard fluid mechanics textbooks. |
| Pipe Material | This affects the pipe loss because each material has a particular roughness |
| Absolute Head Loss | The result of the Darcy-Weisbach equation of fluid mechanics. More information on the Darcy-Weisbach equation is available in most standard fluid mechanics textbooks. |
| Relative Head Loss | The absolute head loss divided by the available head. This value gets copied into the Hydro input window when you click OK. |

When you click OK, HOMER will copy the calculated value into the pipe head loss input box on the [Hydro Inputs](#) window.

If you enter a flow rate so high as to be impossible through the pipe as specified, HOMER will display a warning message.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

2.2.9 Hydrokinetic



Hydrokinetic

The hydrokinetic component can represent several different types of low-head hydro power generation including run-of-the-river, tidal, and wave energy electric generation. The component is described as a turbine, but the hydrokinetic component can also represent other technologies such as a wave energy converter. With a hydrokinetic component, you must also specify the [hydrokinetic resource](#).

The Hydrokinetic inputs window allows you to choose the type of hydrokinetic installation you want to model, specify its costs, and tell HOMER how many to consider as it searches for the optimal system. You can also view and modify the power curve of the hydrokinetic turbine in the lower portion of the menu.

Turbine type

Generic Hydrokinetic ▾

This drop-down menu located at the top of the hydrokinetic set up page contains all the hydrokinetic component types stored in your [component library](#). Choose an appropriate model from this list. When you make a selection with this drop-down box, the selected turbine's properties are displayed in the space below.

Costs

| Costs | | | |
|----------|--------------|------------------|---------------|
| Quantity | Capital (\$) | Replacement (\$) | O&M (\$/year) |
| 1 | \$10,000.00 | \$10,000.00 | \$500.00 |
| | | | |

Multiplier:

In the Costs table, the [capital cost](#) is the initial purchase price for a turbine, the [replacement cost](#) is the cost of replacing the turbine at the end of its lifetime (relevant only if the [project lifetime](#) exceeds the turbine lifetime), and the operating and maintenance cost is the annual cost of operating and maintaining the turbine.

Cost Curve

In the cost table, enter the turbine's [cost curve](#) in as much detail as you would like. In the simplest case, where each turbine costs the same regardless of how many you purchase, you only need to enter one row of data in the cost table. You would enter a quantity of one, along with the per-turbine capital, replacement, and operating and maintenance costs. HOMER extrapolates these costs as needed, so if you were to model a system with three turbines, the associated capital, replacement, and O&M costs would be three times the values entered in the cost table.

| Costs | | | |
|----------|--------------|--------------|-------------|
| Quantity | Capital (\$) | Replace (\$) | O&M (\$/yr) |
| 1 | 10000 | 9000 | 100 |
| 2 | 18000 | 16000 | 140 |
| | | | |

Multiplier:

You would enter multiple rows of data in the cost table if the cost of power was not directly proportional to the number of turbines purchased. In the example shown above, the second turbine is cheaper than the first (this could be because of a volume discount from the manufacturer or because certain fixed costs can be spread over multiple turbines). If the third turbine were cheaper yet, another row of costs could be added. With just these two rows specified though, HOMER would extrapolate the costs by assuming that the third, fourth, and subsequent turbines cost the same as the second.

Search Space

Enter the quantity of turbines you would like, or enter several quantities for HOMER to consider in the system optimization. Include a zero if you would like HOMER to consider systems without this hydrokinetic turbine.

Electrical Bus

Select whether the turbine will produce AC or DC power. Power electronics are not modeled explicitly, but you can account for a dedicated converter efficiency by scaling the power curve.

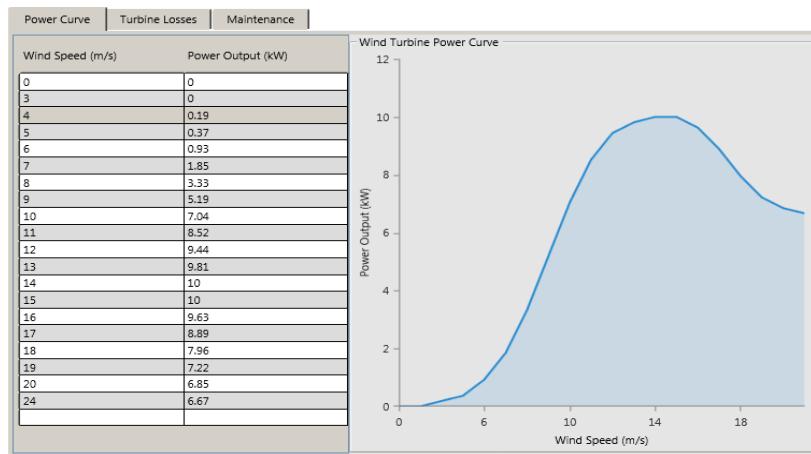
Site Specific Inputs

| Variable | Description |
|---------------------------------------|---|
| Lifetime | The number of years the turbine is expected to last before it requires replacement |
| Hub height | The height above ground of the hub (the center of the rotor), in meters |
| Consider ambient temperature effects? | HOMER will compensate for the change in air density with temperature. If checked, you must define a temperature resource. |

Note: To the right of each numerical input is a sensitivity button ()which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

Power Curve

The Power Curve pane allows you to view the power curve of the selected turbine model in both tabular and graphical form. A turbine's power curve shows how much power it will produce depending on the water speed. Use this graph to verify that the turbine you have selected is an appropriate size for your system.



Manufacturer Properties

The Manufacturer Properties box displays some basic information for the turbine model you have selected.

| Variable | Description |
|----------------|---|
| Abbreviation | A short label which is used to identify the turbine |
| Rated Capacity | The maximum rated power output for the turbine, in kW |
| Manufacturer | The company that manufacturers the turbine model |
| Website | The manufacturer's website |

See also

[Component library](#)

[Search Space window](#)

[Hydrokinetic resource inputs window](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.2.10 Thermal Load Controller



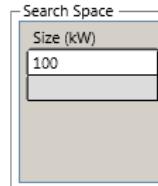
Thermal Load Controller

[This feature requires the Combined Heat and Power Module.](#)
[Click for more information.](#)

The thermal load controller allows excess electrical production to serve loads on the thermal bus. A thermal load controller is not required for systems with a thermal load, but without it excess electrical production is not used.

Size

Use the box labeled Size to input what capacities you would like to consider.



In this table, enter the capacities you want HOMER to consider as it searches for the optimal system. HOMER will use the information you entered in the cost table to calculate the costs of each size, interpolating and extrapolating as necessary. You can see the results in the cost curve graph.

Costs

The Costs box includes the initial [capital cost](#) and [replacement cost](#), as well as annual [operation and maintenance](#) (O&M) costs. The table also includes the size (kW) corresponding to the costs in each row. When specifying the capital and replacement costs, remember to account for all costs associated with the thermal load controller, including installation.

| Costs | | | |
|-----------|--------------|--------------|-------------|
| Size (kW) | Capital (\$) | Replace (\$) | O&M (\$/yr) |
| 1 | 200 | 200 | 0 |
| | | | |

Note that the [capital cost](#) is the initial purchase price, the [replacement cost](#) is the cost of replacing the thermal load controller at the end of its lifetime (relevant only if the [project lifetime](#) exceeds the component lifetime), and the [O&M](#) cost is the annual cost of operating and maintaining the thermal load controller.

You can enter additional rows in the costs table to account for changing costs with scale. For more information on this, see the help article [Why a Cost Table and a Sizes To Consider Table?](#)

Other Inputs

| Variable | Description |
|--|--|
| Lifetime | The service life in years of the thermal load controller |
| Bus Connection | Specify "AC", "DC", or "Both" for the buses from which excess electrical production can be drawn |
| Do not include the thermal load controller in the optimization | This option models the thermal load controller with infinite capacity. Capital, replacement, and O&M costs are still included in the simulation. |

Note: To the right of each numerical input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also:

[Boiler](#)

[Thermal Load](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.2.11 Grid



Grid

You can add the grid like any component and it will be treated as another part of your hybrid system. If you want an off-grid system, do not add a grid component.

Grid Prices

The Grid inputs window allows you to specify the grid several different ways:

- [Simple rates](#) mode allows you to specify a constant power price, sellback price, and sale capacity. All other modes require the Advanced Grid module.
- [Real time rates](#) define prices on an hourly basis by importing a properly formatted text file with time series data (requires Advanced Grid module).
- [Scheduled rates](#) permit different prices at each time of day and month of the year (requires Advanced Grid module).
- [Grid extension](#) mode will compare the cost of a grid extension with the cost of each stand-alone system configuration in the model (requires Advanced Grid module).

Emissions

The Emissions tab allows you to specify emissions factors for several pollutants.

| Variable | Description |
|-----------------------|---|
| Carbon Dioxide | The amount of carbon dioxide released per kWh of grid power consumed by the system, in grams/kWh |
| Carbon Monoxide | The amount of carbon monoxide released per kWh of grid power consumed by the system, in grams/kWh |
| Unburned Hydrocarbons | The amount of unburned hydrocarbons released per kWh of grid power consumed by the system, in grams/kWh |
| Particulate Matter | The amount of particulate matter released per kWh of grid power consumed by the system, in grams/kWh |
| Sulfur Dioxide | The amount of sulfur dioxide released per kWh of grid power consumed by the system, in grams/kWh |
| Nitrogen Oxides | The amount of nitrogen oxides released per kWh of grid power consumed by the system, in grams/kWh |

HOMER uses these emissions factors to calculate:

- the emissions of each pollutant resulting from grid power purchases
- the avoided emissions of each pollutant resulting from grid power sales

The values of these coefficients depend on the generation mix of the electricity in your area. In an area where the majority of the electricity is produced from coal, these values will be relatively high because burning coal results in large emissions of pollutants. Natural gas generation results in somewhat lower emissions, and nuclear and hydro generation result in virtually no emissions of these pollutants.

This help file contains a [table of US grid emissions factors](#). For additional resources, see the article on [Finding data to run HOMER](#).

See also:

[How HOMER calculates emissions](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.2.11.1 Simple rates



Simple Rates

Simple rates mode allows you to set a constant power price and sellback price. You can also set a sale capacity, use net metering, and set emissions factors

associated with grid electricity. Simple rates mode is the only option that does not require the Advanced Grid module.

Rates

Grid rates refer to the prices associated with buying electricity from the grid and selling electricity to the grid. In HOMER, grid rates encompass the following variables:

| Variable | Description |
|------------------------------|---|
| Grid Power Price (\$/kWh) | The cost of buying power from the grid, in \$/kWh. |
| Grid Sellback Price (\$/kWh) | The price that the utility pays you for power you sell to the grid under net metering, in \$/kWh. This variable is only used in simulation if one of the net metering options have been selected. |
| Sale Capacity (kW) | The maximum rate at which power can be sold back to the grid. |

Net metering

| Variable | Description |
|-----------------------------------|--|
| Net Metering | Select this option to base grid energy charges on net usage. See Net metering below for explanation. |
| Net purchases calculated monthly | With this option net usage is calculated monthly |
| Net Purchases Calculated Annually | With this option net usage is calculated annually |

Net metering is a billing scheme by which the utility allows you to sell power to the grid at the retail rate. Effectively, and often literally, your electrical meter runs backwards when you are selling surplus power to the grid. At the end of the billing period (either monthly or annually) you are charged for the net amount purchased (purchases minus sales). If the 'net grid purchases' value is negative, meaning you sold more than you bought over the billing period, the utility pays you according to the sellback price, which is typically equal to the wholesale or 'avoided cost' of power, or zero.

Since the sellback price is often lower than the purchase price, generally net metering results in lower grid costs or greater income. For example, consider a scenario where the price is \$0.20 per kWh, and the sellback price is \$0.10 per kWh. The monthly usage is 1,000 kWh, and the monthly sales is 900 kWh. Without net metering, the cost is \$200 purchased minus \$90 sold, resulting in \$110 cost. With net monthly net metering, we calculate the net usage for the month, which is 100 kWh. Then we calculate the cost which is now only \$20.

If we use annual net metering, we have the rest of the year to return this 100 kWh to the grid. In other words: consider an example where six months out of the year we net 100 kWh of usage per month, and the other six months we net 110 kWh of sales to the grid. If we calculate net purchases monthly, we buy \$120 of power and sell \$66, resulting in \$54 in annual cost. If we calculate net purchases annually, we use 600 kWh over the year, and sell 660 kWh, resulting in net sales of 60 kWh or \$6 in income (and \$0 purchased).

See also:

[How HOMER calculates emissions](#)

For more information

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2.2.11.2 Real time prices



Real Time Prices

This feature requires the
[Advanced Grid Module](#).
Click for more information.

To model real time prices you must create an input file with two data columns, one for the power price [\$/kWh] in each time step and one for the sellback rate [\$/kWh] in each time step. The data file must contain one line of data for each time step of one year: 8,760 lines for hourly data, 35,040 lines for 15-minute data, 52,560 for 10-minute data, and so on. The file cannot contain any header information, so every line of the file should simply contain two numbers separated by commas or tabs. The screenshot below shows an example of a valid input file.

```

TimbuktuGridRates.txt - Notepad
File Edit Format View Help
0.16 0.02
0.12 0.10
0.07 0.05
0.08 0.03
0.07 0.09
0.11 0.05
0.11 0.02
0.14 0.08
0.09 0.04
0.12 0.05
0.16 0.10
0.12 0.01
0.08 0.02
0.12 0.05
0.17 0.04
0.12 0.10
0.11 0.06
0.09 0.01
0.14 0.07
0.14 0.07
0.10 0.07

```

You cannot specify the demand charge on a time step by time step basis, so even if you choose real time prices you will need to specify a demand charge using the rate schedule.

Additional Charges, Capacities, and Constraints

The following options affect when the system is able to buy from or sell to the grid.

| Control | Description |
|--|---|
| Prohibit grid from charging battery above power price | If enabled, this prevents the grid from charging the battery if the grid power price is above the specified value |
| Prohibit any battery charging above power price | If enabled, this prevents any battery charging if the grid power price is above the specified value |
| Prohibit grid from discharging battery below power price | If enabled, this prevents discharging of the battery to the grid if the grid power price is below the specified value |
| Prohibit grid sales from battery below sellback rate | If enabled, this prevents grid sales from the battery if the grid sellback rate is below the specified value |
| Prohibit any grid sales below sellback rate | If enabled, this prevents any grid sales if the grid sellback rate is below the specified value |

These options allow you to set different fees and limits.

| Variable | Description |
|--|--|
| Interconnection Charge | The one-time fee charged by the utility for allowing a power system to be connected to the grid, in \$ (this fee does not apply to grid-only systems) |
| Standby Charge | The annual fee charged by the utility for providing backup grid power for a grid-connected power system, in \$/year (this fee does not apply to grid-only systems) |
| Sale Capacity | The maximum rate at which power can be sold back to the grid, in kW |
| Maximum Net Grid Purchases | The maximum amount of power that can be drawn from the grid, in kW |
| Net Metering | Select this option to base grid energy charges on net usage. See Net metering below for explanation. |
| Net purchases calculated monthly | With this option net usage is calculated monthly |
| Net Purchases Calculated Annually | With this option net usage is calculated annually |

See also:

[How HOMER calculates emissions](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.2.11.3 Scheduled rates



Scheduled Rates

This feature requires the [Advanced Grid Module](#).
[Click for more information.](#)

The scheduled rates option allows you to define grid prices with a regular schedule according to time of day, month of the year, and weekdays or weekends. To define a scheduled price structure, add one or more rates to the rate table, specify the properties for each rate, and define the schedule on the grid rate schedule chart. You can also set additional options. Details for these steps are described in the sections that follow.

Rate Table

Users can define several rates and use the schedule diagram to indicate when each rate applies. Each rate can have different values of power price, sellback rate, and demand rate.

You can change the properties of a rate in the rate table. Click on the button to create a new rate. Click and drag over the rate schedule chart while that row is highlighted to schedule the new rate.

If the power price, sellback rate, and demand rate never change, you only need to define a single rate (equivalent to [Simple rates mode](#)). This is often the case for residential consumers. On the other hand, if the power price, sellback rate, or demand rate changes according to the time of day or the day of the year, you will need to define more than one rate. In the following example, the user has defined three rates, each with different values of power price, sellback rate, and demand rate.

| Step 1: Define and select a rate: | | | | |
|-----------------------------------|-------|----------|--------|--|
| | Price | Sellback | Demand | |
| Rate 1 | 0.040 | 0 | 0 | |
| Rate 2 | 0.06 | 0.03 | 4 | |
| Rate 3 | 0.12 | 0.06 | 8 | |

Rate Properties

Each rate is defined in the rate properties window. Click on the button to access the rate properties menu.

Rate Properties

| | | | | |
|--|-----------|--------|--|-------------------|
| Name: | Base Rate | Color: | | Choose Rate Color |
| Grid power price (\$/kWh): | 0.12 | | | |
| Sellback rate (\$/kWh): | 0.06 | | | |
| Demand rate (\$/kW/mo): | 0 | | | |
| Control parameters | | | | |
| For this rate period: | | | | |
| <input type="checkbox"/> Prohibit grid purchase or sales. <input type="checkbox"/> Prohibit grid from charging battery. <input type="checkbox"/> Prohibit any battery charging. <input type="checkbox"/> Prohibit grid sales from battery. <input type="checkbox"/> Prohibit any battery discharging. <input type="checkbox"/> Prohibit any grid sales. | | | | |

This window allows you to view and edit the properties of a grid rate, including:

| Variable | Description |
|----------|--|
| Name | The name HOMER uses to identify the rate |

| | |
|---------------|---|
| Power Price | The cost of buying power from the grid, in \$/kWh |
| Sellback Rate | The price that the utility pays you for power you sell to the grid, in \$/kWh. Under net metering, the sellback rate applies only to net excess generation. |
| Demand Rate | The monthly fee charged by the utility on the monthly peak demand, in \$/kW/month |

Note: To the right of each numerical input is a sensitivity button () which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

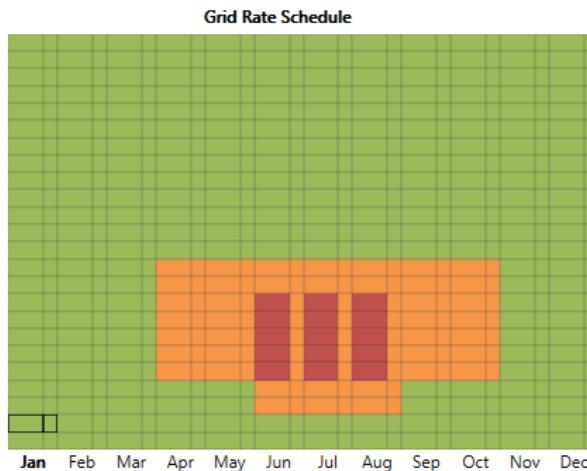
In addition to these basic options, you can set six control options that affect the behavior of the system. These settings affect the system control only during times when the selected rate is scheduled.

| Control | Description |
|--|---|
| Prohibit grid from charging battery above power price | If enabled, this prevents the grid from charging the battery if the grid power price is above the specified value |
| Prohibit any battery charging above power price | If enabled, this prevents any battery charging if the grid power price is above the specified value |
| Prohibit grid from discharging battery below power price | If enabled, this prevents discharging of the battery to the grid if the grid power price is below the specified value |
| Prohibit grid sales from battery below sellback rate | If enabled, this prevents grid sales from the battery if the grid sellback rate is below the specified value |
| Prohibit any grid sales below sellback rate | If enabled, this prevents any grid sales if the grid sellback rate is below the specified value |

Schedule

The table at the bottom of the window shows the times at which each rate applies. You cannot change this information in this window. The only way to indicate when each rate applies is to click on the Rate Schedule chart on the Rates page of the [Grid Inputs](#) window.

If you define multiple rates, you can click and drag on the rate schedule chart to indicate when each rate applies. In the following example the 'Peak' rate applies weekdays from 4pm to 8pm June to August. The 'Shoulder' rate applies all week from 2pm to 8pm in April, May, September, and October, all week from 2pm to 4pm and from 8pm to 10pm June to August, and weekends from 4pm to 8pm June to August. The 'Off-peak' rate applies at all other times.



To draw the schedule shown above, you would select the 'Shoulder' rate, click the All Week button below the rate table, then click on the rate schedule cell for 2pm-3pm in April, then holding the mouse button down, drag to the cell for 7pm-8pm in October and release the mouse button. Then you would click the cell for 8pm-9pm in June and drag to the cell for 9pm-10pm in August. Then you would select the 'Peak', click the Weekdays button below the rate table, click the rate schedule cell for 4pm-5pm in June, and drag to the cell for 7pm-8pm in August.

Additional Charges, Capacities, and Constraints

| Variable | Description |
|--|--|
| Interconnection Charge | The one-time fee charged by the utility for allowing a power system to be connected to the grid, in \$ (this fee does not apply to grid-only systems) |
| Standby Charge | The annual fee charged by the utility for providing backup grid power for a grid-connected power system, in \$/year (this fee does not apply to grid-only systems) |
| Sale Capacity | The maximum rate at which power can be sold back to the grid, in kW |
| Maximum Net Grid Purchases | The maximum amount of power that can be drawn from the grid, in kW |
| Net Metering | Select this option to base grid energy charges on net usage. See Net metering below for explanation. |

| | |
|-----------------------------------|---|
| Net purchases calculated monthly | With this option net usage is calculated monthly |
| Net Purchases Calculated Annually | With this option net usage is calculated annually |

Note: Maximum net grid purchases is a [decision variable](#) because of the effect of demand charges. If the demand rate is zero, you need only specify a single value for the maximum grid demand. If the demand rate is not zero, specify a value equal to or greater than the peak load, plus at least one value smaller than the peak load. HOMER will find the optimal value.

Net metering

Net metering is a billing scheme by which the utility allows you to sell power to the grid at the retail rate. Effectively, and often literally, your electrical meter runs backwards when you are selling surplus power to the grid. At the end of the billing period (either monthly or annually) you are charged for the net amount purchased (purchases minus sales). If the 'net grid purchases' value is negative, meaning you sold more than you bought over the billing period, the utility pays you according to the sellback price, which is typically equal to the wholesale or 'avoided cost' of power, or zero.

Since the sellback price is often lower than the purchase price, generally net metering results in lower grid costs or greater income. For example, consider a scenario where the price is \$0.20 per kWh, and the sellback price is \$0.10 per kWh. The monthly usage is 1,000 kWh, and the monthly sales is 900 kWh. Without net metering, the cost is \$200 purchased minus \$90 sold, resulting in \$110 cost. With net monthly net metering, we calculate the net usage for the month, which is 100 kWh. Then we calculate the cost which is now only \$20.

If we use annual net metering, we have the rest of the year to return this 100 kWh to the grid. In other words: consider an example where six months out of the year we net 100 kWh of usage per month, and the other six months we net 110 kWh of sales to the grid. If we calculate net purchases monthly, we buy \$120 of power and sell \$60, resulting in \$54 in annual cost. If we calculate net purchases annually, we use 600 kWh over the year, and sell 660 kWh, resulting in net sales of 60 kWh or \$6 in income (and \$0 purchased).

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.2.11.4 Grid extension



Grid Extension Inputs

[This feature requires the Advanced Grid Module.](#)
[Click for more information.](#)

Use this option if you want to consider grid extension as an *alternative* to a stand-alone system. HOMER will compare the cost of the grid extension with the cost of each stand-alone system configuration that you model. For each stand-alone system configuration, HOMER will calculate the breakeven grid extension distance, which is the distance from the grid at which the total net present cost of the grid extension is equal to the total net present cost of the stand-alone system.

| Variable | Description |
|------------------|--|
| Capital Cost | The initial capital cost of the grid extension, in \$/km |
| O&M Cost | The annual cost of maintaining the grid extension, in \$/yr/km |
| Grid Power Price | The price of electricity from the grid, in \$kWh |

Note: To the right of each numerical input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also

[Grid Inputs window](#)

[Breakeven grid extension distance](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.2.12 Hydrogen Tank



Hydrogen Tank Inputs

This window gives access to the cost and performance inputs of the hydrogen storage tank.

Costs

| Costs | | | |
|-------------|--------------|------------------|---------------|
| Quantity | Capital (\$) | Replacement (\$) | O&M (\$/year) |
| 1 | \$0.00 | \$0.00 | \$0.00 |
| | | | |
| Multiplier: | (| (| (|

In the hydrogen tank cost table, enter the hydrogen tank cost curve, meaning the way the cost varies with size. If you have a particular hydrogen tank in mind, you can enter its size and cost. In the example above, a 1 kg tank costs \$1400 initially, \$1200 to replace at the end of its life, and \$30/yr for operation and maintenance.

Sizes to consider

| Search Space | |
|--------------|--|
| Size (kg) | |
| 100 | |
| 0 | |

In this table, enter the hydrogen tank sizes you want HOMER to consider as it searches for the optimal system. Be sure to include a zero size if you want to consider systems without a hydrogen tank. HOMER will use the information you entered in the cost table to calculate the costs of each tank size, interpolating and extrapolating as necessary.

Properties

| Variable | Description |
|---|---|
| Lifetime | The number of years the hydrogen storage tank is expected to last before it needs replacement |
| Initial Tank Level | The level of the tank at the start of the simulation. You can specify the initial level as a percentage of the tank size, or as an absolute amount in kg. |
| Require year-end tank level to equal or exceed initial tank level | If you check this box, HOMER will consider infeasible any system whose year-end hydrogen tank level is lower than its initial level |

Note: To the right of each numerical input is a sensitivity button ()which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.2.13 Electrolyzer



Electrolyzer

This window gives access to the cost and performance inputs of the electrolyzer, which generates hydrogen from electricity.

Costs

| Quantity | Capital (\$) | Replacement (\$) | O&M (\$/year) |
|----------|--------------|------------------|---------------|
| 1 | \$0.00 | \$0.00 | \$0.00 |
| | | | |

Multiplier:

In the electrolyzer cost table, enter the electrolyzer cost curve, meaning the way the cost varies with size. If you have a particular electrolyzer in mind, you can enter its size and cost. In the example above, a 0.7 kW electrolyzer costs \$1400 initially, \$1200 to replace at the end of its life, and \$30/yr for operation and maintenance.

Sizes to consider

| |
|-----------|
| Size (kW) |
| 100 |

In this table, enter the electrolyzer sizes you want HOMER to consider as it searches for the optimal system. Be sure to include a zero size if you want to consider systems without an electrolyzer. HOMER will use the information you entered in the cost table to calculate the costs of each electrolyzer size, interpolating and extrapolating as necessary. You can see the results in the cost curve graph.

Properties

| Variable | Description |
|--------------------|---|
| Lifetime | The number of years the electrolyzer is expected to last before it requires replacement |
| Efficiency | The energy content (based on the higher heating value) of the hydrogen produced divided by the amount of electricity consumed |
| Minimum Load Ratio | The minimum power at which the electrolyzer can operate, as a fraction of its rated capacity |
| Type | Specifies whether the electrolyzer consumes alternating current (AC) or direct current (DC) power |

Note: To the right of each numerical input is a sensitivity button ()which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

For more information

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2.2.14 Reformer



Reformer Inputs

A reformer generates hydrogen by reforming a hydrocarbon, typically natural gas. Use this window to define the costs and properties of the reformer.

Note: HOMER cannot model a system where a reformer supplies a fuel cell with hydrogen. The only purpose of the reformer is to serve a [hydrogen load](#).

Costs

| Quantity | Capital (\$) | Replacement (\$) | O&M (\$/year) |
|----------|--------------|------------------|---------------|
| 1 | \$0.00 | \$0.00 | \$0.00 |

Multiplier:

In the cost table, enter the reformer *cost curve*, meaning the way the cost varies with size.

Note that the [capital cost](#) is the initial purchase price, the [replacement cost](#) is the cost of replacing the reformer at the end of its lifetime (relevant only if the [project lifetime](#) exceeds the reformer lifetime), and the operating and maintenance cost is the annual cost of operating and maintaining the reformer.

Sizes to consider

| |
|-----------|
| Size (kW) |
| 100 |

In this table, enter the reformer sizes you want HOMER to consider as it searches for the optimal system. Be sure to include a zero size if you want to consider systems without a reformer. HOMER will use the information you entered in the cost table to calculate the costs of each reformer size, interpolating and extrapolating as necessary. You can see the results in the cost curve graph.

Tip: You can also access the values in this table using the [Search Space](#) window.

Performance parameters

| | |
|--|--|
| <input style="width: 100%;" type="button" value="Diesel"/> | Fuel: Diesel Fuel Price (\$/L): <input type="text" value="1"/> <input type="checkbox"/> Limit Consumption Limit Amount (L/year): <input type="text" value="5000"/> |
| PROPERTIES Lower Heating Value (MJ/kg): 43.2 Density (kg/m3): 820 Carbon Content (%): 88 Sulfur Content (%): 0.33 | |

The fuel drop-down box contains all the fuels stored in your [component library](#). Choose the appropriate fuel from this list. To see the properties of the selected fuel, click the Details button.

You can create a new fuel type by clicking the New button. The new fuel type will be added to your component library. You can also remove a fuel type from the component library by clicking on the Delete button. Note that additions and deletions from the component library are canceled if you close the Reformer Inputs window with the Cancel button.

| Variable | Description |
|----------------------------|--|
| Efficiency | The efficiency with which the reformer converts the fuel to hydrogen, in % |

Economic parameters

| Variable | Description |
|---------------|--|
| Lifetime | The number of years the reformer will last |
| Delivery Cost | The cost of transporting the hydrogen produced by the reformer to the site of use, in \$/kg/km |

Tip: You do not need to input cost data if you do not want to consider delivery cost. HOMER will assume the delivery cost to be zero if there is no delivery cost entered.

Note: To the right of each numerical input is a sensitivity button () which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.3 Resources



Resources

In HOMER, a "resource" is anything coming from outside the system that is used by a [component](#) to generate electric or thermal energy.

| Resource | Components |
|--------------------------------------|---|
| Solar GHI Resource | PV (Flat Panel) |
| Solar DNI Resource | PV (Concentrating) |
| Temperature Resource | PV (Consider temperature effects) |
| Wind Resource | Wind Turbine |
| Hydro Resource | Hydro Component |
| Fuel Resource | Generator |
| Biomass Resource | Generator (Biogas) |

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.3.1 Solar GHI Resource



Solar GHI Resource

The Global Horizontal Irradiation (GHI) Resource is used to calculate flat panel PV array output. GHI is the sum of beam radiation (also called direct normal irradiance or DNI), diffuse irradiance, and ground-reflected radiation. For more details on the equations that determine the incident radiation based on the GHI, see [How HOMER Calculates the Radiation Incident on the PV Array](#).

Note: For concentrating PV, enter a Solar DNI Resource, not GHI. Concentrating PV only captures DNI, the beam radiation component of GHI, and so uses the Solar DNI resource.

The Solar Resource inputs window can be reached from the resources tab by clicking the icon in the resources tab of the navigation ribbon at the top of the HOMER window or by clicking the [Solar Resource](#) button at the top of the [PV](#) inputs pane.

Choose Locale

If you select a location on the map in the home page, the latitude and longitude will appear here. Otherwise, you can enter the latitude and longitude manually. Select the time zone by clicking the "Update" button or by choosing from the drop down menu. HOMER uses the location for several aspects of the PV power calculation, so it is important to specify this even if you are not downloading solar data.

Choose Data Source

The baseline data is a one-year time series representing the average global solar radiation on the horizontal surface, expressed in kWh/m², for each time step of the year. HOMER displays the monthly average radiation and [clearness index](#) of the baseline data in the solar resource table and graph.

There are two ways to create baseline data: you can use HOMER to synthesize hourly data from monthly averages, or you can import time series radiation data from a file. If you are looking for solar data, see [Finding data to run HOMER](#).

Enter Monthly Averages

Solar resource data can be input via the monthly solar radiation table. You can enter the monthly data manually, or you can download it from the HOMER website.

To enter twelve average monthly values into the solar resource table manually, you can input either solar radiation (in kWh/m² per day) or clearness index. You do not have to enter both; HOMER calculates one from the other using the latitude.

To download solar data from the HOMER Energy website, simply click the "Download" button. This will automatically fill in the twelve monthly average values for you based on the latitude and longitude.

Once you have values in the monthly solar radiation table, either by manual entry or download, HOMER builds a set of 8,760 solar radiation values, or one for each hour of the year. HOMER creates the synthesized values using the [Graham algorithm](#), which results in a data sequence that has realistic day-to-day and hour-to-hour variability and autocorrelation. For more information please see the article on [synthetic solar data](#).

Import Solar Data

You can prepare your own text file that contains the solar radiation data in each time step for a complete year.

Tip: You can import data with any time step down to one minute. HOMER detects the time step when you import the data file. For example, if the data file contains 8760 lines, HOMER will assume that it contains hourly data. If the data file contains 52,560 lines, HOMER will assume that it contains 10-minute data.

The data file must contain a single value on each line, where each line corresponds to one time step. Each value in the file represents the average solar radiation (in kW/m^2) for that time step. The first time step starts at midnight on January 1st. A sample input file appears below.

The screenshot shows a Windows-style window titled "Sample.sol - WordPad". The menu bar includes File, Edit, View, Insert, Format, and Help. The main content area displays a list of 8760 values, each starting with a zero and followed by three decimal places. The values range from 0.000 to 0.294. The window has scroll bars on the right and bottom. At the bottom, there is a status bar with the text "For Help, press F1".

| Value |
|-------|
| 0.000 |
| 0.000 |
| 0.000 |
| 0.000 |
| 0.000 |
| 0.000 |
| 0.000 |
| 0.000 |
| 0.038 |
| 0.148 |
| 0.213 |
| 0.294 |
| 0.238 |
| 0.278 |
| 0.202 |
| 0.103 |
| 0.019 |
| 0.000 |
| 0.000 |
| 0.000 |
| 0.000 |

Click **Import...** to open the text file. You can import a text file with any extension.

When you import data from a text file, HOMER makes a copy of the data set and integrates it with the HOMER (.homer) file. Once the data is part of the HOMER file, HOMER no longer refers to the original text file. If you modify data in the original file, you must import the modified file in order for the modification to be included in the HOMER file. After you import a data file, HOMER calculates monthly average radiation and clearness index values and displays them in the table and graph. HOMER also displays the name of the imported data file in the title of the graph.

If you enter new monthly solar radiation values after importing data from a file, HOMER discards the data from the imported file and synthesizes new data based on the twelve new monthly averages. You can edit synthesized data by changing values in the solar resource table. To edit values from an imported file, you must edit the file directly and then import the modified file, as described above.

Scaled data for simulation

Scaled Annual Average ($\text{kWh/m}^2/\text{day}$):

HOMER uses scaled data for calculations. To create scaled data, HOMER multiplies each of the values in the baseline data by a common factor that results in an annual average value equal to the value that you specify in Scaled Annual Average. To determine the value of this factor, HOMER divides the scaled annual average by the baseline annual average solar radiation. The scaled data retains the shape and statistical characteristics of the baseline data, but may differ in magnitude. The default value for the scaled annual average is the baseline annual average solar radiation. When the two values are equal, the scaled data and baseline are identical. HOMER interprets a scaled annual average of zero to mean that there is no solar radiation.

Two reasons to use a scaled annual average that is different from the baseline annual average are for unit conversion or to perform a sensitivity analysis.

An example of using the scaled annual average for unit conversion is to convert data from an imported file that contains solar radiation data expressed in Wh/m^2 rather than kWh/m^2 . If the baseline annual average is 4800 Wh/m^2 , you should enter 4.8 in Scaled Annual Average, so that the scaled data is equivalent to the baseline data, but expressed in kWh/m^2 : $1 \text{ kWh/m}^2 = 1000 \text{ Wh/m}^2$.

Note: To the right of the Scaled Annual Average input is a sensitivity button ()which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also

[Generating synthetic solar data](#)

[Finding data to run HOMER](#)

The solar resource section of [Recommended Reading](#)

[Why do I have to scale load and resource data?](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.3.2 Solar DNI Resource



Solar DNI Resource

The Direct Normal Irradiance (DNI) Resource is used to calculate concentrating PV output. Concentrating PV uses optics to concentrate the solar radiation in a way that only captures the direct beam radiation (also called DNI) and does not capture the diffuse or reflected components of the incident solar radiation.

Note: For a flat panel PV, enter a Solar GHI resource, not DNI. Flat panel PV captures direct, diffuse, and reflected radiation, and so uses the Solar GHI resource to calculate output.

The Solar DNI Resource inputs window can be reached from the resources tab by clicking the icon in the resources tab of the navigation ribbon at the top of the HOMER window or by clicking the [Solar Resource](#) button at the top of the [PV](#) inputs pane.

Choose Locale

You can select a location on the map in the home page.

Importing Solar Data

The Solar DNI resource can only be specified by importing a time-series data file. See the help article [Finding data to run HOMER](#) for a list of sources for solar data.

You can prepare your own text file that contains the solar radiation data in each time step for a complete year.

Tip: You can import data with any time step down to one minute. HOMER detects the time step when you import the data file. For example, if the data file contains 8760 lines, HOMER will assume that it contains hourly data. If the data file contains 52,560 lines, HOMER will assume that it contains 10-minute data.

The data file must contain a single value on each line, where each line corresponds to one time step. Each value in the file represents the average solar radiation (in kW/m²) for that time step. The first time step starts at midnight on January 1st. A sample input file appears below.

Sample.sol - WordPad

| File | Edit | View | Insert | Format | Help |
|-------|------|------|--------|--------|------|
| 0.000 | | | | | |
| 0.000 | | | | | |
| 0.000 | | | | | |
| 0.000 | | | | | |
| 0.000 | | | | | |
| 0.000 | | | | | |
| 0.000 | | | | | |
| 0.038 | | | | | |
| 0.148 | | | | | |
| 0.213 | | | | | |
| 0.294 | | | | | |
| 0.238 | | | | | |
| 0.278 | | | | | |
| 0.202 | | | | | |
| 0.103 | | | | | |
| 0.019 | | | | | |
| 0.000 | | | | | |
| 0.000 | | | | | |
| 0.000 | | | | | |
| 0.000 | | | | | |

Click [Import...](#) to open the text file. You can import a text file with any extension.

When you import data from a text file, HOMER makes a copy of the data set and integrates it with the HOMER (.homer) file. Once the data is part of the HOMER

file, HOMER no longer refers to the original text file. If you modify data in the original file, you must import the modified file in order for the modification to be included in the HOMER file. After you import a data file, HOMER calculates monthly average radiation and clearness index values and displays them in the table and graph. HOMER also displays the name of the imported data file in the title of the graph.

If you enter new monthly solar radiation values after importing data from a file, HOMER discards the data from the imported file and synthesizes new data based on the twelve new monthly averages. You can edit synthesized data by changing values in the solar resource table. To edit values from an imported file, you must edit the file directly and then import the modified file, as described above.

Scaled data for simulation

HOMER uses scaled data for calculations. To create scaled data, HOMER multiplies each of the values in the baseline data by a common factor that results in an annual average value equal to the value that you specify in Scaled Annual Average. To determine the value of this factor, HOMER divides the scaled annual average by the baseline annual average solar radiation. The scaled data retains the shape and statistical characteristics of the baseline data, but may differ in magnitude. The default value for the scaled annual average is the baseline annual average solar radiation. When the two values are equal, the scaled data and baseline are identical. HOMER interprets a scaled annual average of zero to mean that there is no solar radiation.

Two reasons to use a scaled annual average that is different from the baseline annual average are for unit conversion or to perform a sensitivity analysis.

An example of using the scaled annual average for unit conversion is to convert data from an imported file that contains solar radiation data expressed in Wh/m² rather than kWh/m². If the baseline annual average is 4800 Wh/m², you should enter 4.8 in Scaled Annual Average, so that the scaled data is equivalent to the baseline data, but expressed in kWh/m²: 1 kWh/m² = 1000 Wh/m².

Note: To the right of the Scaled Annual Average input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also

[Generating synthetic solar data](#)

[Finding data to run HOMER](#)

The solar resource section of [Recommended Reading](#)

[Why do I have to scale load and resource data?](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.3.3 Temperature Resource



Temperature Resource

The Temperature Resources window can be reached by selecting the Resources tab and clicking the temperature icon.

Use this window to specify the ambient temperature for the year. Enter twelve monthly numbers or import a time series data file. If you import a TMY2 or TMY3 file, HOMER will extract the dry bulb temperature.

If you enter a scaled average different from the average of the baseline data, HOMER will offset the temperature data to correspond to the average value that you enter.

HOMER uses the ambient temperature to calculate the PV cell temperature, as described in the article on how HOMER calculates the PV cell temperature.

The Plot button allows you to view the scaled data in several graphical formats. The Export button allows you to export the scaled data to a text file.

See also:

[How HOMER calculates the PV cell temperature](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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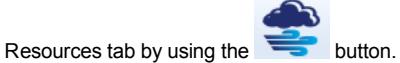
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2.3.4 Wind Resource



Wind Resource

The Wind Resource inputs window can be reached from the [Wind Turbine](#) inputs window by clicking the **Wind Resource** button at the top of the screen or from the



You can use this window to describe the available wind resource. HOMER will use this data to calculate the output of the wind turbine in each time step. This window also provides access to the following tabs:

- [Parameters](#): Variables related to altitude
- [Variation with Height](#): Parameters describing wind shear and the wind velocity's vertical profile
- [Advanced Parameters](#): Parameters controlling variation of the wind over time

If you are looking for wind resource data, see [Finding data to run HOMER](#)

Baseline data

The baseline data is a one-year time series representing the average wind speed, expressed in meters per second, for each time step of the year. HOMER displays the monthly averages calculated from the baseline data in the wind resource table and graph.

You can create baseline data either by using HOMER to synthesize time series data, or by importing time series data from a file.

To synthesize data, you must enter twelve average wind speed values: one for each month of the year. You can also edit the four advanced parameters. Enter each month's average wind speed (m/s) in the table. As you enter values in the table, HOMER synthesizes time series data with the statistical characteristics you have specified. For more information please see the article on [synthetic wind data](#).

Scaled data for simulation

Scaled Annual Average (m/s): [3]

HOMER uses scaled data for calculations. To create scaled data, HOMER multiplies each of the baseline data values by a common factor that results in an annual average value equal to the value that you specify in Scaled annual average. To determine the value of this factor, HOMER divides the scaled annual average by the baseline annual average. The scaled data retains the shape and statistical characteristics of the baseline data, but may differ in magnitude. The default value for the scaled annual average is the baseline annual average. When the two values are equal, the scaled data and baseline are identical. HOMER interprets a scaled annual average of zero to mean that there is no wind resource.

Two reasons to use a scaled annual average that is different from the baseline annual average are for unit conversion or to perform a sensitivity analysis.

An example of using the scaled annual average for unit conversion is to convert data from an imported file that contains wind speed expressed in kilometers per hour. If the baseline annual average is 20 km/hr, you should enter 5.56 in Scaled annual average, so that the scaled data is equivalent to the baseline data, but expressed in m/s rather than km/hr: 1 m/s = 3.6 km/hr; 5.56 m/s = 20 km/hr.

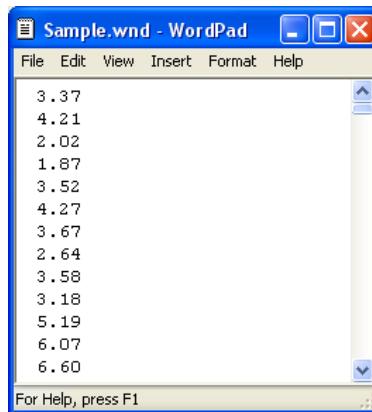
Note: To the right of the Scaled Annual Averages input is a sensitivity button (which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

Importing Wind Speed Data

To import a file, you must prepare a text file that contains the wind speed in each time step for a complete year.

Tip: You can import data with any time step down to one minute. HOMER detects the time step when you import the data file. For example, if the data file contains 8760 lines, HOMER will assume that it contains hourly data. If the data file contains 52,560 lines, HOMER will assume that it contains 10-minute data.

The data file must contain a single value on each line, where each line corresponds to one time step. Each value in the file represents the average wind speed (in m/s) for that time step. The first time step starts at midnight on January 1st. A sample input file appears below.



When you import data from a text file, HOMER makes a copy of the data set and integrates it with the HOMER (.hmr) file. Once the data is part of the HOMER file, HOMER no longer refers to the original text file. If you modify data in the original file, you must import the modified file in order for the modification to be included in the HOMER file. After you import a data file, HOMER calculates twelve monthly average wind speed values and displays them in the table and graph. HOMER also displays the name of the imported data file in the title of the graph. HOMER calculates the four advanced parameters from the imported data and displays them (read-only) in the text boxes.

Pro: If you click Enter monthly averages after importing data from a file, HOMER discards the data from the imported file and synthesizes new data based on the twelve monthly average wind speed values and four advanced parameters it calculated from the imported data. You can edit synthesized data by changing values in the monthly wind speed table. To edit values from an imported file, you must edit the file directly and then import the modified file, as described above.

See also:

[Generating synthetic wind data](#)

[Finding data to run HOMER](#)

The wind resource section of [Recommended Reading](#)

[Why do I have to scale load and resource data?](#)

[How HOMER calculates wind turbine power output](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.3.4.1 Wind Resource Parameters



Wind Resource Parameters

The Parameters tab in the [Wind Resource](#) window gives you access to the following variables:

| Variable | Description |
|-----------------------------------|---|
| Altitude | The altitude in meters above sea level |
| Anemometer Height | The height above ground at which the wind speed data were measured, in meters |

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.3.4.2 Wind Resource Variation with Height

Wind Resource Variation with Height

Use this window to describe the way the wind speed increases with height above ground. HOMER uses this information to calculate the wind speed at the hub height of the wind turbine.

Ground-level obstacles such as vegetation, buildings, and topographic features tend to slow the wind near the surface. Since the effect of these obstacles decreases with height above ground, wind speeds tend to increase with height above ground. This variation of wind speed with height is called *wind shear*. Wind energy engineers typically model wind shear using one of two mathematical models, the logarithmic profile or the power law profile.

Logarithmic profile

The logarithmic profile (or log law) assumes that the wind speed is proportional to the logarithm of the height above ground. The following equation therefore gives the ratio of the wind speed at hub height to the wind speed at anemometer height:

$$\frac{U_{\text{hub}}}{U_{\text{anem}}} = \frac{\ln(z_{\text{hub}} / z_0)}{\ln(z_{\text{anem}} / z_0)}$$

where:

U_{hub} = the wind speed at the hub height of the wind turbine [m/s]

U_{anem} = the wind speed at anemometer height [m/s]

z_{hub} = the hub height of the wind turbine [m]

z_{anem} = the [anemometer height](#) [m]

z_0 = the surface roughness length [m]

$\ln(\cdot)$ = the natural logarithm

The surface roughness length is a parameter that characterizes the roughness of the surrounding terrain. The table below contains representative surface roughness lengths taken from [Manwell, McGowan, and Rogers](#):

| Terrain Description | z_0 |
|-----------------------------|-----------|
| Very smooth, ice or mud | 0.00001 m |
| Calm open sea | 0.0002 m |
| Blown sea | 0.0005 m |
| Snow surface | 0.003 m |
| Lawn grass | 0.008 m |
| Rough pasture | 0.010 m |
| Fallow field | 0.03 m |
| Crops | 0.05 m |
| Few trees | 0.10 m |
| Many trees, few buildings | 0.25 m |
| Forest and woodlands | 0.5 m |
| Suburbs | 1.5 m |
| City center, tall buildings | 3.0 m |

Power law profile

The power law profile assumes that the ratio of wind speeds at different heights is given by the following equation:

$$\frac{U_{\text{hub}}}{U_{\text{anem}}} = \left(\frac{z_{\text{hub}}}{z_{\text{anem}}} \right)^a$$

where:

U_{hub} = the wind speed at the hub height of the wind turbine [m/s]

U_{anem} = the wind speed at anemometer height [m/s]

z_{hub} = the hub height of the wind turbine [m]

z_{anem} = the [anemometer height](#) [m]

a = the power law exponent

The power law exponent is a dimensionless parameter. Foundational research in fluid mechanics showed that its value is equal to 1/7 for turbulent flow over a flat plate. Wind speed researchers have found that in practice the power law exponent depends on terrain roughness, atmospheric stability, and several other factors.

See also:

[Wind resource inputs](#)

[Anemometer height](#)

[Wind turbine hub height](#)[How HOMER calculates wind turbine power output](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.3.4.3 Wind Resource Advanced Parameters



Advanced Parameters

The Advanced Inputs tab in the [Wind Resource](#) window gives you access to the following variables:

| Variable | Description |
|--|---|
| Weibull k | A measure of the long-term distribution of wind speeds |
| Autocorrelation Factor | A measure of the hour-to-hour randomness of the wind speed |
| Diurnal Pattern Strength | A measure of how strongly the wind speed depends on the time of day |
| Hour of Peak Wind Speed | The time of day that tends to be windiest on average |

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.3.5 Hydro Resource



Hydro Resource

[This feature requires the
Hydro Module.
Click for more information.](#)

Use the Hydro Resource Inputs window to describe the stream flow available to the hydro turbine. HOMER uses this data to calculate the output of the hydro turbine in each time step.

Baseline data

The baseline data is a one-year time series representing the average stream flow, expressed in liters per second, for each time step of the year. HOMER displays the monthly averages calculated from the baseline data in the stream flow table and graph.

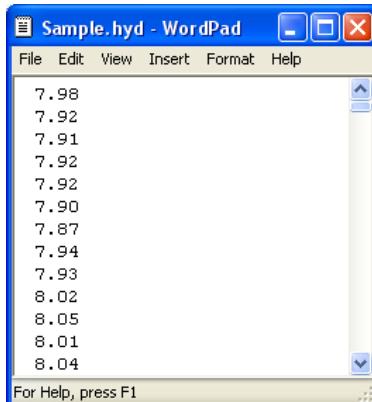
There are two ways to create baseline data: you can use HOMER to synthesize hourly data, or you can import time series data from a file.

To synthesize data, you must enter twelve average stream flow values: one for each month of the year. Enter each month's average stream flow (L/s) in the appropriate row on the stream flow table. As you enter values in the table, HOMER builds a set of 8,760 values, or one stream flow value for each hour of the year. HOMER creates the synthesized values by assuming that the stream flow is constant throughout each month; HOMER simply assigns the monthly average value to each hour in that month.

To import a file, you must prepare a text file that contains the stream flow in each time step for a complete year.

Tip: You can import data with any time step down to one minute. HOMER detects the time step when you import the data file. For example, if the data file contains 8760 lines, HOMER will assume that it contains hourly data. If the data file contains 52,560 lines, HOMER will assume that it contains 10-minute data.

The data file must contain a single value on each line, where each line corresponds to one time step. Each value in the file represents the average stream flow (in L/s) for that time step. The first time step starts at midnight on January 1st. A sample input file appears below.



When you import data from a text file, HOMER makes a copy of the data set and integrates it with the HOMER (.hmr) file. Once the data is part of the HOMER file, HOMER no longer refers to the original text file. If you modify data in the original file, you must import the modified file in order for the modification to be included in the HOMER file. After you import a data file, HOMER calculates twelve monthly average stream flow values and displays them in the table and graph. HOMER also displays the name of the imported data file in the title of the stream flow graph.

If you click Enter monthly averages after importing data from a file, HOMER discards the data from the imported file and synthesizes new data based on the twelve monthly average values it calculated from the imported data. You can edit synthesized data by changing values in the stream flow table. To edit values from an imported file, you must edit the file directly and then import the modified file, as described above.

Scaled data for simulation

Scaled Annual Average (L/s):

HOMER uses scaled data for calculations. To create scaled data, HOMER multiplies each of the baseline data values by a common factor that results in an annual average value equal to the value that you specify in Scaled annual average. To determine the value of this factor, HOMER divides the scaled annual average by the baseline annual average. The scaled data retains the shape and statistical characteristics of the baseline data, but may differ in magnitude. The default value for the scaled annual average is the baseline annual average. When the two values are equal, the scaled data and baseline are identical. HOMER interprets a scaled annual average of zero to mean that there is no stream flow.

Two reasons to use a scaled annual average that is different from the baseline annual average are for unit conversion or to perform a sensitivity analysis.

An example of using the scaled annual average for unit conversion is to convert data from an imported file that contains stream flow data expressed in US gallons per minute. If the baseline annual average is 90 gal/min, you should enter 5.68 in Scaled annual average, so that the scaled data is equivalent to the baseline data, but expressed in L/s rather than U.S. gallons per hour: 1 L/s = 15.85 gal/min; 5.68 L/s = 90 gal/min.

Another reason to scale the baseline data is to do a [sensitivity analysis](#) on the hydro resource. Click the sensitivities button (to the right of the text box) to enter multiple values for a sensitivity analysis.

The Plot button allows you to view the scaled data in several graphical formats. The Export button allows you to export the scaled data to a text file.

See also:

The hydro section of [Recommended Reading](#)

[Why do I have to scale load and resource data?](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.3.6 Fuel Resource



Fuel Resource

When specifying a generator component, you must select a fuel. Several common fuels are already built in to the library.

See also:

[Create a New Fuel](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.3.7 Biomass Resource



Biomass Resource

This feature requires the
[Biomass Module](#).
Click for more information.

HOMER assumes the biomass feedstock is fed into a gasifier to create [biogas](#). One or more generators then consume the biogas to produce electricity (and optionally heat). Use the Biomass Resource Inputs window to describe the availability of biomass feedstock. HOMER uses this data to calculate (in each time step of the year) the amount of biogas that can be supplied by the gasifier to the biogas-fueled generator(s).

Baseline data

The baseline data is a one-year time series representing the average biomass feedstock availability, expressed in kilograms, for each time step of the year. HOMER displays the monthly averages calculated from the baseline data in the biomass resource table and graph.

There are two ways to create baseline data: you can use HOMER to synthesize hourly data from monthly averages, or you can import time series data from a file.

To synthesize data, you must enter twelve average values of biomass availability: one for each month of the year. Enter each month's average biomass availability (in tonnes per day) in the appropriate row of the biomass resource table. As you enter values in the table, HOMER builds a set of 8,760 values, or one value for each hour of the year. HOMER creates the synthesized values by assuming that the biomass availability is constant throughout each month; HOMER simply assigns the monthly average value to each hour in that month.

To import a file, you must prepare a text file that contains the biomass feedstock availability in each time step for a complete year.

Tip: You can import data with any time step down to one minute. HOMER detects the time step when you import the data file. For example, if the data file contains 8760 lines, HOMER will assume that it contains hourly data. If the data file contains 52,560 lines, HOMER will assume that it contains 10-minute data.

The data file must contain a single value on each line, where each line corresponds to one time step. Each value in the file represents the biomass feedstock availability (in kilograms) for that time step. The first time step starts at midnight on January 1st. A sample input file appears below.

```
750
750
750
750
750
750
875
875
875
875
875
875
```

When you import data from a text file, HOMER makes a copy of the data set and integrates it with the HOMER (.hmr) file. Once the data is part of the HOMER file, HOMER no longer refers to the original text file. If you modify data in the original file, you must import the modified file in order for the modification to be included in the HOMER file. After you import a data file, HOMER calculates twelve monthly average biomass availability values and displays them in the table and graph. HOMER also displays the name of the imported data file in the title of the biomass resource graph.

If you click Enter monthly averages after importing data from a file, HOMER discards the data from the imported file and synthesizes new data based on the twelve monthly average values it calculated from the imported data. You can edit synthesized data by changing values in the biomass resource table. To edit values from an imported file, you must edit the file directly and then import the modified file, as described above.

Properties

| Variable | Description |
|------------------------------------|--|
| Average cost | The average cost per tonne of the biomass feedstock. |
| Carbon content | The carbon content of the biomass feedstock as a mass-based percentage. |
| Gasification ratio | The ratio of biogas generated to biomass feedstock consumed in the gasifier. |
| LHV of biogas | The energy content (lower heating value) of the biogas produced by the gasifier. |

Scaled data for simulation

Scaled Annual Average (t/d): 

HOMER uses scaled data for calculations. To create scaled data, HOMER multiplies each of the baseline data values by a common factor that results in an annual average value equal to the value that you specify in Scaled annual average. To determine the value of this factor, HOMER divides the scaled annual average by the baseline annual average. The scaled data retains the shape and statistical characteristics of the baseline data, but may differ in magnitude. The default value for the scaled annual average is the baseline annual average. When the two values are equal, the scaled data and baseline are identical. HOMER interprets a scaled annual average of zero to mean that there is no biomass resource.

Two reasons to use a scaled annual average that is different from the baseline annual average are for unit conversion or to perform a sensitivity analysis.

The Plot button allows you to view the scaled data in several graphical formats. The Export button allows you to export the scaled data to a text file.

Note: To the right of each numerical input is a sensitivity button () which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also:

The biomass section of [Recommended Reading](#)

[Why do I have to scale load and resource data?](#)

For more information

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2.3.8 Hydrokinetic



Hydrokinetic Resource

Use the Hydrokinetic Resource Inputs window to describe the flow available to the hydrokinetic turbine. HOMER uses this data to calculate the output of the hydro turbine in each time step.

Baseline water speed data

The baseline data is a one-year time series representing the water speed, expressed in meters per second, for each time step of the year. HOMER displays the monthly averages calculated from the baseline data in the water speed table and graph.

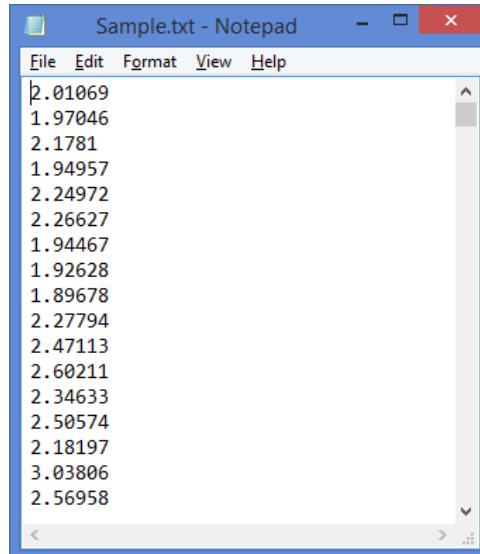
There are two ways to create baseline data: you can enter monthly averages, or you can import time series data from a file.

To enter twelve monthly averages, enter each month's average water speed (m/s) in the appropriate row on the water speed table. As you enter values in the table, HOMER builds a set of 8,760 values, or one water speed value for each hour of the year. HOMER creates the hourly values by assuming that the stream flow is constant throughout each month; HOMER simply assigns the monthly average value to each hour in that month.

To import a file, you must prepare a text file that contains the water speed in each time step for a complete year.

Tip: You can import data with any time step down to one minute. HOMER detects the time step when you import the data file. For example, if the data file contains 8760 lines, HOMER will assume that it contains hourly data. If the data file contains 52,560 lines, HOMER will assume that it contains 10-minute data.

The data file must contain a single value on each line, where each line corresponds to one time step. Each value in the file represents the average water speed (in m/s) for that time step. The first time step starts at midnight on January 1st. A sample input file appears below.



When you import data from a text file, HOMER makes a copy of the data set and integrates it with the HOMER (.homer) file. Once the data is part of the HOMER file, HOMER no longer refers to the original text file. If you modify data in the original file, you must import the modified file in order for the modification to be included in the HOMER file. After you import a data file, HOMER calculates twelve monthly average water speed values and displays them in the table and graph. You can view a plot of the time series data by clicking on the "Plot..." button at the bottom of the window.

Scaled data for simulation

Scaled Annual Average (m/s):

HOMER uses scaled data for calculations. To create scaled data, HOMER multiplies each of the baseline data values by a common factor that results in an annual average value equal to the value that you specify in Scaled annual average. To determine the value of this factor, HOMER divides the scaled annual average by the baseline annual average. The scaled data retains the shape and statistical characteristics of the baseline data, but may differ in magnitude. The default value for the scaled annual average is the baseline annual average. When the two values are equal, the scaled data and baseline are identical. HOMER interprets a scaled annual average of zero to mean that there is no stream flow.

You can use the scaled annual average for unit conversion. For example, you could convert data from an imported file that contains water speed data expressed in miles per hour. If the baseline annual average is 4 mi/hr, you should enter 1.79 in Scaled annual average, so that the scaled data is equivalent to the baseline data, but expressed in m/s rather than miles per hour: $1 \text{ m/s} = 2.24 \text{ mi/hr}$; $1.79 \text{ m/s} = 4 \text{ mi/hr}$.

Another reason to scale the baseline data is to do a [sensitivity analysis](#) on the hydro resource. Click the sensitivities button (to the right of the text box) to enter multiple values for a sensitivity analysis.

The Plot button allows you to view the scaled data in several graphical formats. The Export button allows you to export the scaled data to a text file.

See also:

[The hydro section of Recommended Reading](#)

[Why do I have to scale load and resource data?](#)

For more information

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2.4 System Tab



System Tab



The System tab gives you access all of the menus where you can review your project and model as a whole. It is a good place to review your model and inputs before you calculate results. The system tab contains the following menus:

| Name | Description |
|------------------------------------|--|
| Project Set Up | Options that apply to the entire model: economics , system control , emissions , and constraints |
| Input Report | create an HTML-format report summarizing all the model inputs, and display it in a browser |
| Search Space | View and edit the system parameters HOMER simulates to find the optimal system configuration |
| Sensitivity Inputs | View and modify all the sensitivity variables in the model |

For more information

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2.4.1 Project Set Up



Project set up

In the Project Set Up window you can set options that apply to your entire model. They are grouped onto the following tabs:

- [Economics](#)
- [System Control](#)
- [Emissions](#)
- [Constraints](#)

See also

Definition of [sensitivity variable](#)

For more information

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2.4.1.1 Economics



Economic Inputs

The Economics tab under the [Project Setup](#) tab gives access to the following variables:

| Variable | Description |
|---|---|
| Annual Real Interest Rate | The discount rate used to convert between one-time costs and annualized costs, in % |
| Project Lifetime | The number of years over which the net present cost of the project should be calculated |
| System Fixed Capital Cost | The fixed capital cost that occurs regardless of the size or architecture of the system, in \$ |
| System Fixed O&M Cost | The fixed annual costs that occur regardless of the size or architecture of the system, in \$/yr |
| Capacity Shortage Penalty | A penalty applied to the system for any capacity shortage , in \$/kWh |

Note: To the right of each numerical input is a sensitivity button () which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

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2.4.1.2 System Control



System Control

The System Control tab under the [Project](#) tab allows you to modify how HOMER simulates your systems.

Simulation

The [simulation time step](#) is the time step that HOMER uses to simulate the operation of each system configuration. You can set the simulation time step to anything from several hours down to one minute. The simulation time step does not have to match the time step of any time series load or resource data you may have imported. See the article on the simulation time step for details.

Dispatch Strategy Inputs

A [dispatch strategy](#) is a set of rules that govern the operation of the generator(s) and the battery bank. HOMER can model two dispatch strategies, cycle charging and load following. Which is optimal depends on many factors, including the sizes of the generators and battery bank, the price of fuel, the O&M cost of the generators, the amount of renewable power in the system, and the character of the renewable resources. If you choose to model both, HOMER will simulate each system using both dispatch strategies and you will be able to see which is optimal.

Under the [load following](#) strategy, whenever a generator is needed it produces only enough power to meet the demand. Load following tends to be optimal in systems with a lot of renewable power, when the renewable power output sometimes exceeds the load.

Under the [cycle charging](#) strategy, whenever a generator has to operate, it operates at full capacity with surplus power going to charge the battery bank. Cycle charging tends to be optimal in systems with little or no renewable power.

If you can apply a [setpoint state of charge](#) to the cycle charging strategy, the generator(s) will not stop charging the battery bank until it reaches the specified state of charge. The sensitivity button to the right allows you to do a [sensitivity analysis](#) on this setpoint.

Note that the dispatch strategy is abbreviated "Disp. Strgy" in the sensitivity and optimization results tables.

Generator control

| | |
|---|--|
| Allow systems with multiple generators | This check box controls whether HOMER considers systems that contain more than one generator. It has no effect if you are considering only one generator. |
| Multiple generators can operate simultaneously | This check box only affects the operation of systems that include two or more generators on the same bus. If you check this box, HOMER will allow multiple generators on the same bus to operate at once whenever necessary. Otherwise, multiple generators on the same bus must take turns operating. |
| Allow systems with generator capacity less than peak load | This check box controls whether HOMER will consider systems whose total generator capacity is less than the annual peak primary load |

Other settings

| | |
|--|--|
| Allow systems with two types of wind turbines | This check box controls whether HOMER will simulate system configurations that contain more than one type of wind turbine. If you add two types of wind turbine to the schematic and you simply wish to choose between them, then leave this checkbox unchecked. If you want HOMER to simulate systems that contain both types of turbine, then check this checkbox. |
| Allow excess electricity to serve thermal load | If you check this checkbox, HOMER will assume that excess electricity serves the thermal load through a resistive heater or electric boiler |
| Limit excess | If you check this checkbox, HOMER will prevent the system from producing more than the allowable amount of excess thermal |

Note: To the right of each numerical input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

For more information

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2.4.1.3 Emissions



Emissions

The Emissions tab under the [Project](#) tab allows you to specify a cost penalty associated with a pollutant, or a limit on the emissions of a pollutant.

Emissions Penalties

If you specify a non-zero cost penalty for a particular pollutant, HOMER will add the corresponding cost to the total annual cost of the power system. For example, if you specify a cost penalty for CO₂ emissions of \$10 per tonne and the power system produces 15 tonnes of CO₂ per year, HOMER will penalize the system by adding \$150/yr to its total annual cost. The emissions cost appears in the "other O&M cost" column of the in the [Costs](#) page of the Simulation Results window.

You can specify a penalty for any of the six pollutants that HOMER tracks. To the right of each input is a sensitivity button which allows you to do a [sensitivity analysis](#) on that variable.

In its dispatch logic, HOMER takes emissions penalties into account when comparing the costs of different dispatchable generation sources. For a simple example, consider a system containing two generators whose properties are identical except that one has a higher NOx emissions factor. If the user specifies a non-zero cost penalty for NOx emissions, then whenever HOMER must choose between operating one generator or the other, it will choose the one with the lower NOx emissions factor.

| Variable | Description |
|--|--|
| CO₂ Emissions Penalty | A cost penalty HOMER applies to the system's emissions of carbon dioxide, in \$/ton |
| CO Emissions Penalty | A cost penalty HOMER applies to the system's emissions of carbon monoxide, in \$/ton |
| HC Emissions Penalty | A cost penalty HOMER applies to the system's emissions of unburned hydrocarbons, in \$/ton |
| PM Emissions Penalty | A cost penalty HOMER applies to the system's emissions of particulate matter, in \$/ton |
| SO₂ Emissions Penalty | A cost penalty HOMER applies to the system's emissions of sulfur dioxide, in \$/ton |
| NO_x Emissions Penalty | A cost penalty HOMER applies to the system's emissions of nitrogen oxides, in \$/ton |

Limits on Emissions

If you specify a limit to the emissions of a particular pollutant, HOMER will reject as infeasible any system that emits more than the allowed amount of that pollutant. You can constrain the emissions of any of the six pollutants that HOMER tracks. To the right of each input is a sensitivity button which allows you to do a [sensitivity analysis](#) on that variable. You can use such a sensitivity analysis to determine the cost of limiting emissions to a range of values.

| Variable | Description |
|---------------------------------|---|
| CO ₂ Emissions Limit | A limit on the system's annual emissions of carbon dioxide, in kg/yr |
| CO Emissions Limit | A limit on the system's annual emissions of carbon monoxide, in kg/yr |
| UHC Emissions Limit | A limit on the system's annual emissions of unburned hydrocarbons, in kg/yr |
| PM Emissions Limit | A limit on the system's annual emissions of particulate matter, in kg/yr |
| SO ₂ Emissions Limit | A limit on the system's annual emissions of sulfur dioxide, in kg/yr |
| NO _x Emissions Limit | A limit on the system's annual emissions of nitrogen oxides, in kg/yr |

Note: To the right of each numerical input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also:

[How HOMER calculates emissions](#)

For more information

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2.4.1.4 Constraints



Constraints

The Constraints tab under the [Project Setup](#) tab allows you to modify system constraints which are conditions the [systems](#) must satisfy. HOMER discards systems that do not satisfy the specified constraints, so they do not appear in the optimization results or sensitivity results.

| Variable | Description |
|--|--|
| Maximum Annual Capacity Shortage | The maximum allowable value of the capacity shortage fraction , which is the total capacity shortage divided by the total annual electric load, in % |
| Minimum Renewable Fraction | The minimum allowable value of the annual renewable fraction , in % |

Operating reserve

Note: Under most circumstances you do not need to change the values of these advanced inputs. Their default values are appropriate for most systems.

[Operating reserve](#) is surplus [operating capacity](#) that ensures reliable electricity supply even if the load suddenly increases or renewable power output suddenly decreases. HOMER defines the required amount of operating reserve using four inputs, two related to the variability of the electric load and two related to the variability of the renewable power. These four inputs are described in the article on [required operating reserve](#). The total required operating reserve is the sum of the four values resulting from these four inputs. In its simulation, HOMER operates the power system so as to keep the operating reserve equal to or greater than the required operating reserve. It records any shortfall as a [capacity shortage](#).

| Variable | Description |
|------------------------------------|--|
| As a percent of the current load | HOMER adds this percentage of the primary load in the current time step (AC and DC separately) to the required operating reserve in each time step. A value of 10% means that the system must keep enough spare capacity operating to serve a sudden 10% increase in the load. |
| As a percent of annual peak load | HOMER adds this percentage of the peak primary load (AC and DC separately) to the required operating reserve in each time step. It therefore defines a constant amount of operating reserve. For example, if the peak AC primary load is 40 kW and you want to ensure at least 8 kW of operating reserve on the AC bus at all times (maybe to cover an 8 kW motor starting load), set this input to 20%. |
| As a percent of wind power output | HOMER adds this percentage of the wind turbine power output to the required operating reserve in each time step. A value of 60% means that the system must keep enough spare capacity operating to serve the load even if the wind turbine output suddenly decreases 60%. The more variable you expect the output of the wind turbine to be, the higher you should set this input. |
| As a percent of solar power output | HOMER adds this percentage of the PV array power output to the required operating reserve in each time step. A value of 25% means that the system must keep enough spare capacity operating to serve the load even if the PV array output suddenly decreases 25%. In most cases, the output of the PV array should be less variable than the output of a wind turbine, so this input will usually be set at a lower value than the previous one. |

Note: To the right of each numerical input is a sensitivity button ()which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also

[Operating reserve](#)

[Required operating reserve](#)

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2.4.2 Input Report



Input Summary Report

HOMER will create an HTML-format report summarizing all the relevant inputs, and display it in a browser. From the browser, you can save or print the report, or copy it to the clipboard so that you can paste it into a word processor or spreadsheet program.

Written by: Tom Lambert (support@homerenergy.com)

Last modified: November 10, 2004

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2.4.3 Search Space



Search Space

The Search Space optimization values table gives access to the search space for the whole system. You can view and edit the values for any component in your model. HOMER will simulate all combinations of these values to determine the most efficient system configuration.

See also

Definition of [search space](#)

For more information

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2.4.4 Sensitivity Inputs



Sensitivity Inputs

This window gives convenient access to all the sensitivity variables. You can view and edit the values in tabular format.

See also

Definition of [sensitivity variable](#)

For more information

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2.4.5 Estimate



Estimate

The estimate button provides a quick calculation of the amount of time it will take to complete calculation for the current project. You do not need to estimate before running the calculation, but it can be useful for determining compute time. The number of simulations and estimated compute time will display in the space to the right of the buttons.

For more information

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2.5 Design View



Design View

Click the design button to display the design view, where the schematic is displayed and where you can add and edit loads, components, and resources. When you click the design button, HOMER will display the load, component, or resource you were last working on (or the home screen by default). The load, components and resources tabs continue to display when you are not in the design view (other views are the results view and the library view), and if you select any items from within these tabs, you will automatically be taken back to the design view.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

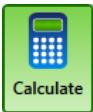
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2.6 Calculate Button





Calculate Button

The calculate button appears on the right end of the toolbar, and is visible from all menus. It changes color depending on the status of the current design:



If the current design contains all the necessary components and resources, the calculate button will appear green. If the design is obviously incomplete (i.e. if a PV is added and no solar resource is defined, or if there are both AC and DC components but no system converter) the calculate button will appear gray.

Note: It is possible for the calculate button to appear green, but still find no feasible solutions after calculating.

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2.7 Results View



Results

In the Results view, HOMER displays two tables. The top table is the [Sensitivity Cases](#) table. It shows a list of the best feasible systems for each sensitivity case entered. You can click a sensitivity case to view all feasible systems for that case in the lower, [Optimization Results](#) table. Double click on a system in the Optimization Cases table (the lower table) to see its details in a [Simulation Results](#) window.

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2.7.1 Simulation Results



Simulation Results

Double click a row in the [Optimization Results](#) table to open the Simulation Results window for that system. At the top of the window will be displayed the system [Net Present Cost](#), the system Architecture which lists the components of the system, and Sensitivities which is the [sensitivity case](#) that was used.

The Simulation Results window always contains the following tabs:

- The [Cost Summary](#) tab displays the total cash flow, categorized either by component or by cost type
- The [Cash Flow](#) tab displays the year-by-year cash flows in a customizable graphical format
- The [Electrical](#) tab displays details about the production and consumption of electricity by the system

- The [Emissions](#) tab displays the annual pollutants emitted by the system

The Simulation Results window may also contain the following tabs, if the equipment is included:

- The [PV](#) tab shows details about the operation of the PV array
- The [Wind Turbine](#) tab shows details about the operation of the wind turbine
- The [Generator](#) tab shows details about the operation of the generator
- The [Battery](#) tab shows details about the use and expected lifetime of the battery
- The [Grid](#) tab shows details about the purchases from and sales to the grid if the system is grid-connected, or information about the [break-even grid extension](#) (P) if you are considering extending the grid
- The [Converter](#) tab shows details about the operation of the inverter and rectifier, including capacity, electrical input and output, hours of operation, and losses
- The [Thermal](#) tab shows details about the production and consumption of thermal energy by the system P
- The [Boiler](#) tab shows details about the operation of the boiler. Systems with thermal loads will always contain boilers. P
- The [Hydro](#) tab shows details about the operation of the hydro turbine P

In addition to the tabs, the Simulation Results window also contains two buttons in the upper right:

- The [Time Series data](#) buttons allow you to analyze those variables that HOMER stores for each time step of the simulation.
- The [Report](#) button allows you to print out a report with basic information about the system to easily share your simulation results with others.

For more information

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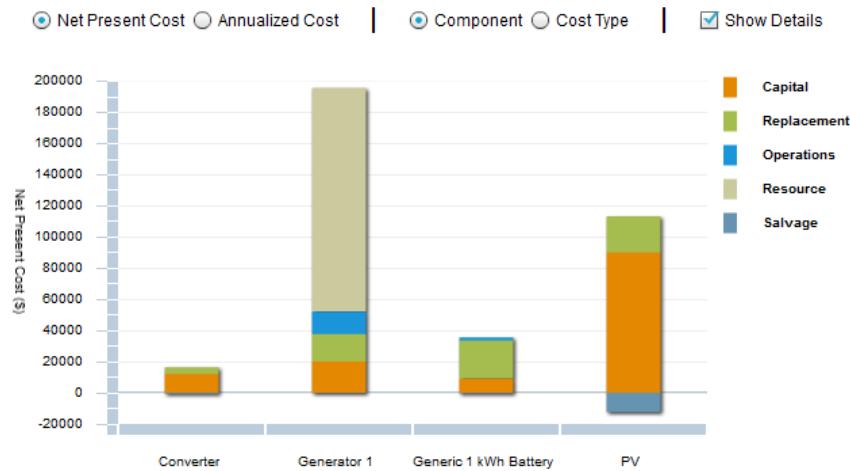
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2.7.1.1 Cost Summary Outputs



Cost Summary

The Cost Summary tab in the [Simulation Results](#) window displays cash flows as either a present value or annualized cost, categorized by component or cost type. It also provides access to the [Compare Economics](#) window (P).



You can choose among several options for displaying the cash flow summary:

- Net Present Cost displays the cost breakdown in terms of [net present costs](#).
- Annualized Cost displays the cost breakdown in terms of [annualized costs](#).
- Component causes HOMER to categorize costs by component.
- Cost Type causes HOMER to categorize costs according to type: capital, O&M, replacement, resource, and salvage value.
- Show details causes HOMER to categorize costs both by component and type in a single graph.

The table below the graph displays the cash flow summary broken down by component and by cost type. The values displayed in the graph appear highlighted in the table.

Pro: The Compare button opens the [Compare Economics](#) window, which allows you to compare two systems and calculate payback or internal rate of return.

Tip: For systems connected to the grid, HOMER puts the costs and revenues associated with buying and selling power from the grid into the grid O&M cost.

Note that the [net present cost](#) appears not on the Cost Summary tab, but rather in the top left corner of the Simulation Results window.

See also

[Simulation Results window](#)

[Cash Flow tab](#)

[Compare Economics window](#)

[Net present cost](#)

[Annualized cost](#)

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2.7.1.1.1 Compare Economics Window



Compare Economics Window

This window allows you to compare the economic merits of the current system and a base case system. The window displays cash flow graphs and a table of economic metrics. To open the window, choose a system to be the current system in [optimization results](#), and then click Compare on the [Cost Summary](#) page of the [Simulation Results](#) window.

You must choose a base case system to compare with the current system to make the economic metrics meaningful. The metrics show you the value of the difference between two options, taking into account the lifecycle costs of both systems. You can compare the current system to any other system in the optimization results. For example:

- Compare a PV-wind-diesel hybrid system with a diesel-only base case system for an off-grid project to find the present worth of fuel saved by installing a hybrid system instead of a diesel-only system, taking into account the cost of installing, operating, and maintaining each system.
- Compare a grid-connected PV system to a grid-only system to find the payback period required for grid sales to recover the cost of installing the PV system.

The table at the top of the window displays a list of systems from the optimization results from which you can choose a base case. You can display the list as a categorized list to display only the top-ranked system in each category, or as an overall list to display all systems.

The system summary table shows the component sizes, capital cost and net present cost of the base case system and current system.

The display options control what appears in the cash flow graph.

Tip: Right-click the cash flow graph to export a table of values to a text file, which you can open in a text editor or spreadsheet program.

When you choose a base case system, the metric table shows economic measures representing the value of the difference between the two systems:

- The present worth is the difference between the [net present costs](#) of the base case system and the current system. The sign of the present worth indicates whether the current system compares favorably as an investment option with the base case system: A positive value indicates that the current system saves money over the project lifetime compared to the base case system.
- The annual worth is the present worth multiplied by the [capital recovery factor](#).
- To see how HOMER calculates return on investment (ROI), choose the following display options: Graph, Difference, Cumulative. Subtract the cumulative nominal cash flow in year zero from the cumulative nominal cash flow in the final year. Divide that number by the lifetime and then again by the cumulative nominal cash flow in year zero. Note that the cumulative nominal cash flow in year zero is equivalent to the base case capital cost minus the current system capital cost.
- Internal rate of return (IRR) is the discount rate at which the base case and current system have the same net present cost. HOMER calculates the IRR by determining the discount rate that makes the present value of the difference of the two cash flow sequences equal to zero.
- Payback is the number of years at which the cumulative cash flow of the difference between the current system and base case system switches from negative to positive. The payback is an indication of how long it would take to recover the difference in investment costs between the current system and the base case system. You can see a visual representation of the payback by choosing the following display options: Graph, Difference, and Cumulative. The simple payback is where the nominal cash flow difference line crosses zero. The discounted payback is where the discounted cash flow difference line crosses zero.

See also

[Why does HOMER require a base case to calculate payback and other economic metrics?](#)

[Is there a way to calculate simple payback by hand?](#)

For more information

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2.7.1.1.2 Calculating Payback, Internal Rate of Return (IRR) and Other Economic Metrics



Calculating payback

HOMER calculates payback by comparing one system with another. In general, payback tells you how many years it will take to recover an investment. You invest a certain amount of money up front, then earn income from that investment, and the payback is the number of years it takes for the cumulative income to equal the value of the initial investment. HOMER can also calculate other economic metrics such as IRR, present worth, and return on investment.

Sometimes, the "income" of a power system can be defined intrinsically, without a reference for comparison. If, for example, a grid-sales system does not need to serve any load, but simply sells power to the grid, then you can define the income of the system as the money it makes by selling power to the grid minus the expense of operating the system. In that case, you could compare the initial cost of the system with its income to calculate the payback.

For distributed power systems, it's usually not that simple, and the income must be defined relative to some alternative. Say you are designing a system to provide electricity to an off-grid house. A pure diesel system might have low capital cost and high operating cost, whereas a PV-diesel-battery system might have high capital cost and low operating cost. Neither system produces any income. In both cases you spend money up front to build the system, then you keep spending money each year to operate the system. The concept of payback has meaning only if you compare one system to the other. You can define the payback of the additional investment required for the PV-diesel-battery system by comparing the difference in capital cost with the difference in operating cost. HOMER does exactly that in the [Compare Economics](#) window.

So, to calculate the payback of one alternative, we must compare to another alternative. Even to calculate the payback of the simple grid-sales system mentioned above involves an implicit comparison with the base case, which is to do nothing. The do-nothing alternative is easy to compare to, since all its costs are zero, but if we have an electric load to serve, the do-nothing alternative is not an acceptable one.

A renewable power system designer will often use a non-renewable power system as the base case, but HOMER lets you choose any base case you want. You could compare a system with two wind turbines to a system that has one wind turbine to calculate the payback of the second wind turbine. Or you could compare a PV-diesel-battery system with a PV-diesel system to calculate the payback of the battery.

See also:

[Compare Economics window](#)

[Is there a way to calculate simple payback by hand?](#)

For more information

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2.7.1.1.3 Grid Costs



Grid Costs

Since the grid is unlike any other component, HOMER calculates the costs associated with the grid in a unique way. This article explains how HOMER calculates each of the grid cost outputs.

Grid capital cost

If the system is connected to the grid and contains some other power producing device (such as a microturbine, a fuel cell, a PV array, or a wind turbine), the grid capital cost is equal to the interconnection charge. Otherwise, the grid capital cost is zero.

Grid replacement cost

The replacement cost of the grid is always zero.

Grid O&M cost

The grid O&M cost is equal to the annual cost of buying electricity from the grid (energy cost plus demand cost) minus any income from the sale of electricity to the grid. For grid-connected systems that contain some other power producing device (such as a microturbine, a fuel cell, a PV array, or a wind turbine), the grid O&M

cost also includes the standby charge.

See also

[Interconnection charge](#)

[Standby charge](#)

[Capital recovery factor](#)

[Project lifetime](#)

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2.7.1.2 Cash Flow Outputs



Cash Flow

The Cash Flow tab in the [Simulation Results](#) window displays the system cash flow in either [graphical](#) or [tabular](#) form. You can choose the display with the radio buttons at the top of the window. Both views are described below.

Bar Chart

Each bar in the graph represents either a total inflow or total outflow of cash for a single year. The first bar, for year zero, shows the [capital cost](#) of the system, which also appears in the [optimization results](#). A negative value represents an outflow, or expenditure for fuel, equipment replacements, or operation and maintenance (O&M). A positive value represents an inflow, which may be income from electricity sales or the salvage value of equipment at the end of the project lifetime.



You can choose to display the cash flows as either nominal or discounted values. A nominal cash flow is the actual income minus cost that HOMER anticipates in a particular year. A discounted cash flow is the nominal cash flow discounted to year zero. HOMER calculates the discounted cash flow by multiplying the nominal cash flow by the [discount factor](#).

You can choose among three options for displaying the cash flow graph:

- Totals displays each cash flow as a solid-colored bar.
- By Component displays each cash flow as a stacked bar, with a different color representing each of the components in the system. Note that penalties and system fixed costs appear in the graph as "other" costs.
- By Cost Type shows each cash flow as a stacked bar, with each color representing one of five cost types: capital, replacement, salvage, O&M, and fuel. Note that the salvage value appears as a positive value at the end of the project lifetime. For grid connected systems that sell electricity to the grid, grid sales are included in the O&M cost type.

More detailed cash flow information can be found in the [Cash Flow Details](#) window, which displays a table of cash flows broken down by year and by component.

Pivot Table

Choose "Pivot Table" from the radio buttons at the top of the cash flow window. The cash flow details table shows a detailed breakdown of all the costs that occur throughout the project lifetime. It appears in the [Cash Flow Details window](#).

An example of the cash flow details table appears below. Each year of the project lifetime appears as a column. The rows list the capital cost, replacement cost, salvage value, O&M cost, fuel cost, and total cost for each component. Nominal costs appear in the top half of the table, and discounted costs appear in the bottom half. The discount factors, which HOMER uses to calculate discounted costs from nominal costs, appear in between.

Tip: Using the controls at the top of the window, you can choose to display a less-detailed breakdown of the costs, or to display only nominal or only discounted costs.

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|-------------------------------|----------------------|-------------------|-------------------|-------------------|-------------------|---------------------|-------------------|-------------------|-------------------|-------------------|---------------------|-------------------|-------------------|-------------------|-------------------|-------------------|----|
| Fuel | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Operating | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Replacement | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Salvage | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Converter Total | (\$750.00) | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | (\$750.00) | |
| Generator | | | | | | | | | | | | | | | | | |
| Capital | (\$900.00) | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Fuel | \$0.00 | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | (\$457.00) | |
| Operating | \$0.00 | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | (\$38.00) | |
| Replacement | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | (\$900.00) | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | (\$900.00) | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Salvage | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Generator Total | (\$900.00) | (\$495.00) | (\$495.00) | (\$495.00) | (\$495.00) | (\$1,395.00) | (\$495.00) | (\$495.00) | (\$495.00) | (\$495.00) | (\$1,395.00) | (\$495.00) | (\$495.00) | (\$495.00) | (\$495.00) | (\$495.00) | |
| PV | | | | | | | | | | | | | | | | | |
| Capital | (\$10,500.00) | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Fuel | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Operating | \$0.00 | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | |
| Replacement | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Salvage | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| PV Total | (\$10,500.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | (\$120.00) | |
| PV Dedicated Converter | | | | | | | | | | | | | | | | | |
| Capital | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Fuel | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Operating | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| Replacement | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |

The example above shows the cash flows for a system comprised of a diesel generator and a wind turbine. The project lifetime is ten years. The diesel generator needs to be replaced at a cost of \$5,500 every two years, and the wind turbine needs to be replaced at a cost of \$12,000 every eight years.

Capital Costs

Capital costs occur only at the beginning of the project, meaning at the end of year zero. No capital costs occur after year zero.

Replacement Costs

Replacements costs occur whenever a component needs a replacement. Note that replacement costs may not necessarily occur at integer year numbers. For example, if a generator requires replacement every 3.25 years, HOMER will assign replacement costs at 3.25 years, 6.5 years, and so on. Use the controls at the top of the window if you want to see the precise timing of these cash flows.

Salvage Value

Salvage value occurs as a positive cash flow at the end of the project lifetime, for any component that has some remaining life at this point. In the example above, the wind turbine requires replacement after eight years, so the second wind turbine is only two years old at the end of the ten-year project lifetime, meaning it has six years remaining in its lifetime. HOMER assumes linear depreciation, so it calculates a salvage value of $6/8 = 75\%$ of the replacement cost of the wind turbine. Since the wind turbine replacement cost is \$12,000, that leads to a salvage value of \$9,000 for the wind turbine at the end of the project lifetime.

Operating and Maintenance Costs

For many components, such as the PV array and the wind turbine, you enter the O&M costs in dollars per year. For other components, such as the generator, you enter the O&M cost in dollars per operating hour, and HOMER multiplies that number by the operating hours per year to calculate the resulting annual O&M cost in dollars per year. Note that the number HOMER reports for the grid O&M cost is actually the annual cost of buying power from the grid minus the annual revenue gained from sales of power to the grid.

Fuel Costs

For components that consume fuel, HOMER calculates the annual fuel cost by multiplying the fuel price by the annual fuel consumption.

Tip: The bottom row of the table, when displaying discounted costs, shows the total discounted cost for each year of the project lifetime. The sum of these numbers, which appears in the bottom right corner of the table, equals the total net present cost of the system.

See also

[Simulation Results window](#)

[Cost Summary tab](#)

[Cash Flow Details window](#)

[Discount factor](#)

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2.7.1.3 Electrical Outputs



Electrical Outputs

The Electrical tab in the [Simulation Results](#) window shows details about the annual production and consumption of electrical energy by the system.

Production

This table lists the total annual energy output of each electrical energy producing component of the power system, plus the [total electrical production](#).

Consumption

This table lists the total amount of electrical energy that went to serve each of the system's electrical loads. Values that appear here when applicable include:

| Variable | Description |
|--|---|
| AC Primary Load Served | The amount of energy that went towards serving the AC primary load(s) |
| DC Primary Load Served P | The amount of energy that went towards serving the DC primary load(s) |
| Deferrable Load Served P | The amount of energy that went towards serving the deferrable load |
| Electrolyzer Load Served P | The amount of electrical energy consumed by the electrolyzer |
| Grid Sales | The total amount of electricity sold to the grid during the year |
| Total Load Served | The total amount of electrical load served during the year |

Note: The total production can exceed the sum of the total consumption and the excess electricity because of losses in the battery and converter.

Excess and Shortage

This table lists the following values:

| Variable | Description |
|-------------------------------------|---|
| Excess Electricity | The total amount of excess electricity that occurred during the year, as well as the excess electricity fraction expressed as a percentage of the total electrical production |
| Unmet Electric Load | The total amount of unmet load that went unserved because of insufficient generation during the year, as well as the unmet load fraction expressed as a percentage of the total electrical demand |
| Capacity Shortage | The total amount of capacity shortage that occurred during the year, as well as the capacity shortage fraction expressed as a percentage of the total electrical demand |

Other Outputs

The final table lists the following variables:

| Variable | Description |
|---|---|
| Renewable Fraction | The fraction of the total electrical production that is produced by renewable sources |
| Maximum Renewable Penetration | The maximum value of the renewable penetration that occurs over the year |

See also

[Simulation Results window](#)

[Constraints window](#)Written by: Tom Lambert (support@homerenergy.com)

Last modified: September 27, 2010

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[\[TOP\]](#)**2.7.1.4 PV Outputs****PV Outputs**The PV tab in the [Simulation Results](#) window contains the following output variables:

| Variable | Description |
|--------------------|--|
| Rated Capacity | The rated capacity of the PV array under standard conditions, in kW |
| Mean Output | The average power amount of the PV array over the year, in kW and kWh/day |
| Capacity Factor | The average power output of the PV array (in kW) divided by its rated power, in % |
| Total Production | The total power output of the PV array over the year, in kWh/yr |
| Minimum Output | The minimum power output of the PV array over the year, in kW |
| Maximum Output | The maximum power output of the PV array over the year, in kW |
| PV Penetration | The average power output of the PV array divided by the average primary load, in % |
| Hours of Operation | The number of hours of the year during which the PV array output was greater than zero |
| Levelized Cost | The levelized cost of energy of the PV array, in \$/kWh |

In the bottom half of the page a [DMap](#) appears showing the power output of the PV array in each time step of the year.Written by: Tom Lambert (support@homerenergy.com)

Last modified: October 27, 2004

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[\[TOP\]](#)**2.7.1.5 Wind Turbine Outputs****Wind Turbine Outputs**The Wind Turbine tab in the [Simulation Results](#) window contains the following output variables:

| Variable | Description |
|----------------------|---|
| Total Rated Capacity | The highest possible power amount from the wind turbine(s), in kW |

| | |
|--------------------|--|
| Mean Output | The average power amount of the wind turbine over the year, in kW |
| Capacity Factor | The average power output of the wind turbine(s) divided by the total wind turbine capacity, in % |
| Total Production | The total power output of the wind turbine(s) over the year, in kWh/yr |
| Minimum Output | The minimum power output of the wind turbine over the year, in kW |
| Maximum Output | The maximum power output of the wind turbine over the year, in kW |
| Wind Penetration | The average power output of the wind turbine(s) divided by the average primary load, in % |
| Hours of Operation | The number of hours of the year during which the wind turbine output was greater than zero |
| Levelized Cost | The leveled cost of energy of the wind turbine(s), in \$/kWh |

In the bottom half of the page a [DMap](#) appears showing the power output of the wind turbine(s) in each time step of the year.

Written by: Tom Lambert (support@homerenergy.com)

Last modified: October 27, 2004

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2.7.1.6 Generator Outputs



Generator Outputs

The Generator tab in the [Simulation Results](#) window contains the following output variables:

| Variable | Description |
|---|---|
| Hours of Operation | The total run time of the generator during the year, in hr/yr |
| Number of Starts | The number of times the generator was started during the year |
| Operational Life | The number of years the generator will last before it requires replacement |
| Capacity Factor | The average power output of the generator divided by its total capacity |
| Fixed Generation Cost | The fixed cost of running the generator, in \$/hr |
| Electrical Production | The total power output of the generator over the year, in kWh/yr |
| Mean Electrical Output | The average electrical power output of the generator over the hours that it runs, in kW |
| Minimum Electrical Output | The lowest electrical power output of the generator over the year, in kW |
| Maximum Electrical Output | The highest electrical power output of the generator over the year, in kW |
| Average Thermal Output | The average thermal power output of the generator over the hours that it runs |
| Minimum Thermal Output | The lowest thermal power output of the generator over the year |
| Maximum Thermal Output | The highest thermal power output of the generator over the year |
| Fuel Consumption | The total amount of fuel consumed by the generator during the year, in L/yr |
| Specific Fuel Consumption | The average quantity of fuel consumed per kWh of energy produced by the generator, in L/kWh |
| Fuel Energy Input | The total amount of energy in the fuel consumed by the generator during the year in kWh/yr |
| Mean Electrical Efficiency | The average electrical efficiency of the generator during the year, in % |

Note : The thermal output variables appear only if the [heat recovery ratio](#) is nonzero.

In the bottom half of the page a [DMap](#) appears showing the power output of the generator in each hour of the year.

Written by: Tom Lambert (support@homerenergy.com)

Last modified: October 27, 2004

For more information

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2.7.1.7 Battery Outputs



Battery Outputs

The Battery tab in the [Simulation Results](#) window contains the following output variables:

| Variable | Description |
|-------------------------------------|---|
| String Size | The number of batteries connected in series in each string |
| Strings in Parallel | The number of battery strings connected in parallel |
| Batteries | The number of batteries in the array is the string size multiplied by the number of strings |
| Bus Voltage | The voltage of the battery array, calculated by multiplying battery voltage by string size, in volts |
| Nominal Capacity | The amount of energy that could be withdrawn from the battery at a particular constant current, starting from a fully charged state, in kWh |
| Usable Nominal Capacity | The battery capacity adjusted to exclude all capacity below the minimum state of charge of the battery, in kWh |
| Autonomy | The capacity of the battery bank divided by the average electrical load, in hours |
| Lifetime Throughput | The total amount of energy that can be cycled through the battery before it needs to be replaced, in kWh |
| Battery Wear Cost | The cost of cycling energy through the battery bank, in \$/kWh |
| Average Energy Cost | The average cost of the energy that goes into the battery, in \$/kWh |
| Energy In | The total amount of energy charged to the battery, in kWh |
| Energy Out | The total amount of energy discharged from the battery, in kWh |
| Storage Depletion | The difference in the battery state of charge at the beginning and end of the year, in kWh/yr |
| Losses | Annual energy losses due to battery inefficiency, in kWh/yr |
| Annual Throughput | The total amount of energy that cycled through the battery bank during the year, in kWh/yr |
| Expected Life | The number of years the battery bank will last before it requires replacement |

In the bottom half of the page a [DMap](#) appears showing the state of charge of the battery bank in each time step of the year.

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2.7.1.8 Grid Outputs



Grid Outputs

The Grid tab in the [Simulation Results](#) window displays details about the buying and selling of electricity from and to the grid, and the resulting costs. The outputs table contains the following variables:

| Variable | Description |
|------------------|---|
| Energy Purchased | The total amount of electricity purchased from the grid, in kWh |
| Energy Sold | The total amount of electricity sold to the grid, in kWh |
| Net Purchased | The net electricity purchased from the grid, in kWh |
| Peak Demand | The peak power demand serviced by the grid, in kW |
| Energy Charge | The total amount paid in energy charges, in \$ |
| Demand Charge | The total amount paid in demand charges, in \$ |

Pro: If you defined more than one rate in the [Grid Inputs](#) window, a combo box will appear allowing you to choose a rate, or select All to see the summation over all rates.

Energy Charge

If net metering does not apply, HOMER calculates the total annual energy charge using the following equation:

$$C_{grid,energy} = \sum_i^{\text{rates}} \sum_j^{12} E_{gridpurchases,i,j} \cdot c_{power,i} - \sum_i^{\text{rates}} \sum_j^{12} E_{gridsales,i,j} \cdot c_{sellback,i}$$

where:

$E_{gridpurchases,i,j}$ = the amount of energy purchased from the grid in month j during the time that rate i applies [kWh]

$c_{power,i}$ = the grid power price for rate i [\$/kWh]

$E_{gridsales,i,j}$ = the amount of energy sold to the grid in month j during the time that rate i applies [kWh]

$c_{sellback,i}$ = the sellback rate for rate i [\$/kWh]

If net metering applies and net generation is calculated monthly, HOMER calculates the total annual energy charge using the following equation:

$$C_{grid,energy} = \sum_i^{\text{rates}} \sum_j^{12} \begin{cases} E_{netgridpurchases,i,j} \cdot c_{power,i} & \text{if } E_{netgridpurchases,i,j} \geq 0 \\ E_{netgridpurchases,i,j} \cdot c_{sellback,i} & \text{if } E_{netgridpurchases,i,j} < 0 \end{cases}$$

where:

$E_{netgridpurchases,i,j}$ = the net grid purchases (grid purchases minus grid sales) in month j during the time that rate i applies [kWh]

$c_{power,i}$ = the grid power price for rate i [\$/kWh]

$c_{sellback,i}$ = the sellback rate for rate i [\$/kWh]

If net metering applies and net generation is calculated annually, HOMER calculates the total annual energy charge using the following equation:

$$C_{grid,energy} = \sum_i^{\text{rates}} \begin{cases} E_{netgridpurchases,i} \cdot c_{power,i} & \text{if } E_{netgridpurchases,i} \geq 0 \\ E_{netgridpurchases,i} \cdot c_{sellback,i} & \text{if } E_{netgridpurchases,i} < 0 \end{cases}$$

where:

$E_{netgridpurchases,i}$ = the annual net grid purchases (grid purchases minus grid sales) during the time that rate i applies [kWh]

$c_{power,i}$ = the grid power price for rate i [\$/kWh]

$c_{sellback,i}$ = the sellback rate for rate i [\$/kWh]

Demand Charge

HOMER calculates the total annual grid demand charge using the following equation:

$$C_{grid,demand} = \sum_i^{\text{rates}} \sum_j^{12} P_{grid,peak,i,j} \cdot c_{demand,i}$$

where:

$P_{grid,peak,i,j}$ = the peak hourly grid demand in month j during the time that rate i applies [kWh]

$c_{demand,i}$ = the grid demand rate for rate i [\$/kW/month]

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2.7.1.9 Converter Outputs



Converter Outputs

The Converter tab in the [Simulation Results](#) window displays the following variables for both the inverter, which converts DC to AC electricity, and the rectifier, which converts AC to DC electricity:

| Variable | Description |
|--------------------------|---|
| Capacity | The maximum possible power output, in AC kW for the inverter and DC kW for the rectifier |
| Mean, Min and Max Output | The inverter values are in terms of AC kW, and the rectifier values are in terms of DC kW |
| Capacity Factor | The mean output divided by the capacity, in % |
| Hours of Operation | The number of hours of non-zero power output |
| Energy In | The total amount of energy into the device, in DC kWh/yr for the inverter and AC kWh/yr for the rectifier |
| Energy Out | The total amount of energy out of the device, in AC kWh for the inverter and DC kWh for the rectifier |
| Losses | The total energy lost in the device, in kWh/yr |

In the bottom half of the page a [DMap](#) appears showing the power output of the inverter and/or rectifier in each time step of the year.

For more information

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2.7.1.10 Emissions Outputs



Emissions Outputs

The Emissions tab in the [Simulation Results](#) window shows the total amount of each pollutant produced annually by the power system in kg/yr. Pollutants originate from the consumption of fuel and biomass in generators, the boiler, and the reformer, as well as from the consumption of grid power.

Sales of power to the grid result in reduced grid emissions, and HOMER credits the power system with these reductions. The system can even achieve negative emissions of one or more pollutants if it sells a lot of low-emissions electricity to the grid.

See also

[How HOMER calculates emissions](#)

Written by: Tom Lambert (support@homereenergy.com)

Last modified: October 27, 2004

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.7.1.11 Thermal Outputs



Thermal Outputs

This feature requires the
[Combined Heat and Power Module.](#)
[Click for more information.](#)

The Thermal tab in the [Simulation Results](#) window shows details about the annual production and consumption of thermal energy by the system.

Annual Thermal Energy Production

This section lists the total annual output of each thermal energy producing component of the power system, as well as the [total thermal production](#).

Annual Thermal Load Served

This section shows the total [total thermal load served](#) over the year, plus any surplus.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.7.1.12 Boiler Outputs



Boiler Outputs

This feature requires the
[Combined Heat and Power Module.](#)
[Click for more information.](#)

The Boiler tab in the [Simulation Results](#) window contains the following output variables:

| Variable | Description |
|---------------------------|--|
| Hours of Operation | The total run time of the boiler during the year, in hr/yr |
| Total Production | The total amount of thermal energy produced by the boiler per year, in kWh/yr |
| Mean Output | The average thermal power output of the boiler over the hours that it runs, in kW |
| Min. Output | The lowest thermal power output of the boiler over the year, in kW |
| Max. Output | The highest thermal power output of the boiler over the year, in kW |
| Fuel Consumption | The total amount of fuel consumed by the boiler during the year, in L/yr |
| Specific Fuel Consumption | The average quantity of fuel consumed per kWh of thermal energy produced by the boiler, in L/kWh |
| Mean Efficiency | The total annual thermal energy production divided by the total annual fuel energy consumption, in % |

In the bottom half of the page a [DMap](#) appears showing the thermal power output of the boiler in each time step of the year.

Written by: Tom Lambert (support@homerenergy.com)

Last modified: January 21, 2010

For more information

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2.7.1.13 Hydro Outputs



Hydro Outputs

[This feature requires the
Hydro Module.](#)
[Click for more information.](#)

The Hydro tab in the [Simulation Results](#) window contains the following output variables:

| Variable | Description |
|--------------------|---|
| Average Output | The average power amount of the hydro turbine over the year, in kW |
| Minimum Output | The minimum power output of the hydro turbine over the year, in kW |
| Maximum Output | The maximum power output of the hydro turbine over the year, in kW |
| Hydro Penetration | The average power output of the hydro turbine divided by the average primary load |
| Capacity Factor | The average power output of the hydro turbine divided by its nominal capacity |
| Hours of Operation | The number of hours of the year during which the hydro turbine output was greater than zero |

In the bottom half of the page a [DMap](#) appears showing the power output of the hydro turbine in each time step of the year.

Written by: Tom Lambert (support@homereenergy.com)

Last modified: October 27, 2004

For more information

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2.7.1.14 Time Series Outputs



Time series outputs

Plot

The time series plot can graph a number of model variables over the duration of the simulation.

Scatterplot [P](#)

The scatterplot graph allows you to plot any variable against any other variable. This kind of graph can often help you to understand how the system operates. For example, plotting diesel power output versus battery state of charge may reveal that the diesel only operates when the battery is at or near its minimum state of charge.

Deltaplot

The deltaplot shows the frequency of changes in any variable over some length of time. Choose the variable from the drop-down box, and choose the length of time using the slider control.

Table

The table displays all of the time series data generated by the simulation for each time step.

Export

The export function writes all time series data from the selected simulation to a csv file. You will be prompted for a location and name for the output file.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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2.7.1.15 Hydrogen Outputs



Hydrogen Outputs

The Hydrogen tab in the [Simulation Results](#) window contains the following output variables:

| Variable | Description |
|------------------------------|---|
| Electrolyzer Production | The total amount of hydrogen produced by the electrolyzer, in kg/yr |
| Reformer Production | The total amount of hydrogen produced by the reformer, in kg/yr |
| Total Hydrogen Production | The total amount of hydrogen produced by the system, in kg/yr |
| Unmet Hydrogen Load | The total hydrogen demand that the system was unable to supply, in kg/yr |
| Electrolyzer Capacity Factor | The average production of the electrolyzer divided by its rated production capacity |
| Reformer Capacity Factor | The average production of the reformer divided by its rated production capacity |

Written by: Tom Lambert (support@homerenergy.com)

Last modified: October 27, 2004

For more information

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2.7.1.16 Hydrogen Tank Outputs



Hydrogen Tank Outputs

The Hydrogen Tank tab in the [Simulation Results](#) window contains the following output variables:

| Variable | Description |
|--|---|
| Hydrogen Production | The total amount of hydrogen produced annually by the system |
| Hydrogen Consumption | The total amount of hydrogen consumed annually by the system |
| Hydrogen Tank Autonomy | The energy capacity of the hydrogen tank divided by the average electrical load |

This page also contains three graphs showing the amount of hydrogen in the tank over the year.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.7.1.17 Electrolyzer Outputs



Electrolyzer Outputs P

The Electrolyzer tab in the [Simulation Results](#) window contains the following output variables:

| Variable | Description |
|----------------------|--|
| Rated Capacity | The maximum electrical input power the electrolyzer can accept |
| Mean Input | The average electrical input power to the electrolyzer over the year |
| Minimum Input | The minimum electrical input power to the electrolyzer over the year |
| Maximum Input | The maximum electrical input power to the electrolyzer over the year |
| Total Input Energy | The total electrical energy that the electrolyzer consumes annually |
| Capacity Factor | The mean input power divided by the rated capacity |
| Hours of Operation | The number of hours per year that the electrolyzer produces hydrogen |
| Mean Output | The average rate of hydrogen production over the year |
| Minimum Output | The minimum rate of hydrogen production over the year |
| Maximum Output | The maximum rate of hydrogen production over the year |
| Total Production | The total amount of hydrogen produced annually by the electrolyzer |
| Specific Consumption | The average quantity of fuel consumed per kWh of thermal energy produced by the electrolyzer |

In the bottom half of the page a [DMap](#) appears showing the electrical power consumption of the electrolyzer in each time step of the year.

Written by: Tom Lambert (support@homerenergy.com)

Last modified: January 22, 2010

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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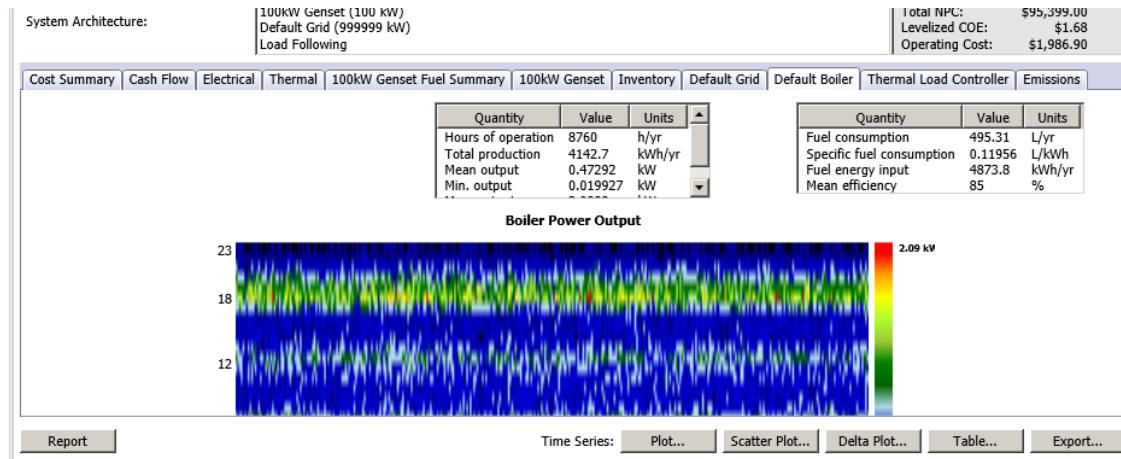
[TOP]

2.7.1.18 Report Summarizing the Simulation Results



Report Summarizing the Simulation Results

To view a report summarizing the results of a simulation, click the Report button in the bottom left corner of the [Simulation Results](#) window:



HOMER will create a report containing all the information shown in the various pages of the Simulation Results window. You can print the report or save it to a file by clicking the Print button at the bottom of the window.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.7.2 Optimization Results



Optimization Results

For each [sensitivity case](#) that it solves, HOMER simulates every system in the [Search Space](#) and ranks all the [feasible](#) systems according to increasing [net present cost](#). The Results tab of HOMER's main window displays that list of systems in the [Sensitivity Results](#) table.

You can view the Optimization Results table by clicking on a row in the Sensitivity Results table. Sensitivity variables appear in the left-most columns of the Sensitivity Results table. HOMER updates the list of systems in the Optimization Results each time you make a selection from the Sensitivity Results table.

The radio buttons above the Optimization Results table let you filter the list of feasible systems according to system type. The two choices, Overall and Categorized, are explained below.

Overall

If you choose to display the overall system rankings, HOMER shows the top-ranked [system configurations](#) according to net present cost. (You can set the maximum size of this list in the [Preferences](#) window.) An example is shown below. If you look closely, you'll see that the numbers under the Architecture section indicate the presence of each type of component under consideration. In this example, the icons indicate the presence of, from left to right: batteries, the diesel generator, wind turbines, PV panels, and the converter. To the right are several columns that indicate a few summary values drawn from the simulation results of the least-cost system, such as the initial capital cost, operating cost, and total net present cost.

Tip: Click any system in the list to see detailed [Simulation Results](#).

| 2.00 | 3.00 | | | 4.0 | 2 | 2 | 100 | LF | \$2.31 | \$122,511 | \$2,262 |
|---|--------|---------|----------------|----------|----------|-----------|---------------------|----------------------|--------|-----------|---------|
| 2.00 | 4.00 | | | | | | | | | \$117,713 | \$2,121 |
| Export... Optimization Cases: Left Double Click on simulation to examine details. | | | | | | | | | | | |
| <input type="radio"/> Categorized <input checked="" type="radio"/> Overall | | | | | | | | | | | |
| Architecture | | | | | | | | Cost | | | |
| PV | Gen100 | 1kWh LI | Converter (kW) | Dispatch | COE (\$) | NPC (\$) | Operating Cost (\$) | Initial Capital (\$) | | | |
| 3.0 | 2 | 1 | 100 | LF | \$2.25 | \$119,129 | \$2,451 | \$87,800 | | | |
| 2.0 | 2 | 1 | 100 | LF | \$2.25 | \$119,148 | \$2,687 | \$84,800 | | | |
| | 2 | 1 | 100 | LF | \$2.27 | \$120,008 | \$3,224 | \$78,800 | | | |
| 4.0 | 2 | 1 | 100 | LF | \$2.28 | \$120,535 | \$2,326 | \$90,800 | | | |
| 5.0 | 2 | 1 | 100 | LF | \$2.32 | \$122,884 | \$2,275 | \$93,800 | | | |
| 3.0 | 2 | 2 | 100 | LF | \$2.33 | \$123,351 | \$2,562 | \$90,600 | | | |
| 2.0 | 2 | 2 | 100 | LF | \$2.33 | \$123,387 | \$2,800 | \$87,600 | | | |

Categorized

The overall rankings are typically dominated by two or three [system types](#). In the above example, the top systems are all either wind/generator/battery or PV/wind/generator/battery systems. For a broader comparison, select Categorized from the drop-down menu above Filter by Architecture. The categorized rankings show the least-cost system of each type. In the example shown below, the top-ranked system corresponds to the top-ranked system in the overall rankings shown above. But the second system listed corresponds to the sixth-place system in the overall rankings, because the second-place system in the overall rankings was of the same type as the first-place system.

The fifth system in the categorized rankings is interesting for comparison because it represents the least-cost pure diesel system. This system would both appear so far down the overall rankings that it would be hard to see. But the categorized rankings makes it easy to compare this system with the other alternatives.

Tip: Click any system in the list to see detailed [Simulation Results](#).

| 2.00 | 3.00 | | | 4.0 | 2 | 2 | 100 | LF | \$2.31 | \$122,511 | \$2,262 |
|---|--------|---------|----------------|----------|----------|-----------|---------------------|----------------------|--------|-----------|---------|
| 2.00 | 4.00 | | | | | | | | | \$117,713 | \$2,121 |
| Export... Optimization Cases: Left Double Click on simulation to examine details. | | | | | | | | | | | |
| <input checked="" type="radio"/> Categorized <input type="radio"/> Overall | | | | | | | | | | | |
| Architecture | | | | | | | | Cost | | | |
| PV | Gen100 | 1kWh LI | Converter (kW) | Dispatch | COE (\$) | NPC (\$) | Operating Cost (\$) | Initial Capital (\$) | | | |
| 3.0 | 2 | 1 | 100 | LF | \$2.25 | \$119,129 | \$2,451 | \$87,800 | | | |
| | 2 | 1 | 100 | LF | \$2.27 | \$120,008 | \$3,224 | \$78,800 | | | |
| 2.0 | 2 | | 100 | LF | \$2.45 | \$129,898 | \$3,746 | \$82,000 | | | |

See also

[Sensitivity results](#)

For more information

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2.7.3 Sensitivity Results



Sensitivity Results

A [sensitivity analysis](#) can result in a huge amount of output data. Every simulation that HOMER performs results in several dozen summary outputs (like the annual fuel consumption and the total capital cost) plus about a dozen arrays of time series data (e.g. the output of the wind turbine). HOMER typically performs hundreds

or thousands of these simulations per [sensitivity case](#), and a sensitivity analysis can easily involve hundreds of sensitivity cases. We designed HOMER's graphic and tabular output capabilities to let you efficiently analyze all that data.

Tabular

The tabular sensitivity results consist of a list showing the least-cost [system](#) for each sensitivity case. In the example shown below, the first two columns display the values of the two sensitivity variables: the diesel fuel price and the wind speed. The next five columns contain values indicating in the least-cost system the presence and size of the five components under consideration. From left to right, they are batteries, the diesel generator, wind turbines, PV panels, and the converter. Following are several columns with summary values drawn from the simulation results of the least-cost system including initial capital, operating cost, and total net present cost.

| RESULTS | | | | | | | | | | | | | | | | | |
|-------------|-----------|--|--|--|--|--|--|-----|-------|--------|---------|----------------|----------|----------|-----------|---------------------|-----------|
| | | Sensitivity Cases: Left Click on sensitivity case to see optimization cases. | | | | | | | | | | | | | | | |
| Sensitivity | | Architecture | | | | | | | | | | Cost | | | | | |
| Interest | Fuel Cost | ! | | | | | | PV | 15/50 | Gen100 | 1kWh LA | Converter (kW) | Dispatch | COE (\$) | NPC (\$) | Operating Cost (\$) | Initial |
| 10.00 | 0.60 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.13 | \$207,643 | \$4,919 | \$163,000 |
| 10.00 | 0.80 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.19 | \$211,635 | \$5,358 | \$163,000 |
| 10.00 | 1.20 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.31 | \$219,620 | \$6,238 | \$163,000 |
| 10.00 | 1.00 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.25 | \$215,628 | \$5,798 | \$163,000 |
| 12.00 | 0.60 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.51 | \$200,928 | \$4,836 | \$163,000 |
| 12.00 | 0.80 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.57 | \$204,378 | \$5,276 | \$163,000 |
| 12.00 | 1.20 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.69 | \$211,277 | \$6,156 | \$163,000 |
| 10.00 | 1.00 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.33 | \$207,807 | \$5,746 | \$163,000 |

You can click on any row in the table to jump to the [optimization results](#) for that sensitivity case. That lets you see the sub-optimal systems (the ones that were not least cost) and view the [simulation results](#) for any of the ranked systems.

| Sensitivity | | Architecture | | | | | | | | | | Cost | | | | | |
|-------------|-----------|--------------|--|--|--|--|--|-----|-------|--------|---------|----------------|----------|----------|-----------|---------------------|-------------|
| Interest | Fuel Cost | ! | | | | | | PV | 15/50 | Gen100 | 1kWh LA | Converter (kW) | Dispatch | COE (\$) | NPC (\$) | Operating Cost (\$) | Initial Cap |
| 10.00 | 0.60 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.13 | \$207,643 | \$4,919 | \$163,000 |
| 10.00 | 0.80 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.19 | \$211,635 | \$5,358 | \$163,000 |
| 10.00 | 1.20 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.71 | \$210,670 | \$6,720 | \$163,000 |

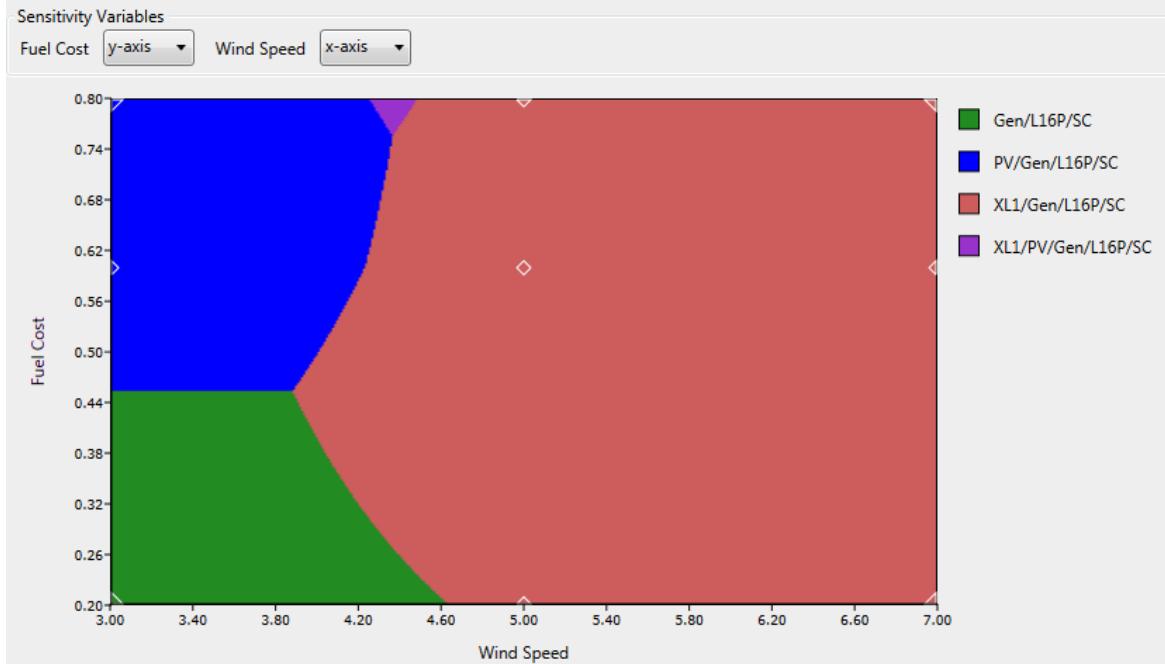
| Sensitivity | | Architecture | | | | | | | | | | Cost | | | | System | | |
|-------------|-----------|--------------|--|--|--|--|--|-----|-------|--------|---------|----------------|----------|----------|-----------|---------------------|----------------------|---------------|
| Interest | Fuel Cost | ! | | | | | | PV | 15/50 | Gen100 | 1kWh LA | Converter (kW) | Dispatch | COE (\$) | NPC (\$) | Operating Cost (\$) | Initial Capital (\$) | Ren. Frac (%) |
| 10.00 | 0.60 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.19 | \$211,635 | \$5,358 | \$163,000 | 17.5 |
| 10.00 | 0.80 | | | | | | | 1.0 | 2 | 100 | 4 | 100 | LF | \$3.24 | \$214,488 | \$6,003 | \$160,000 | 0 |
| 10.00 | 1.20 | | | | | | | 1.0 | 2 | 100 | 3 | 100 | LF | \$3.34 | \$221,364 | \$7,091 | \$157,000 | 0 |
| 10.00 | 1.00 | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.43 | \$227,277 | \$9,285 | \$143,000 | 0 |

When the analysis involves more than one [sensitivity variable](#), a graph often conveys the results in a more meaningful way than a table can. You can create three types of graphs: optimal system type charts, surface plots, and line graphs. These graphs are drawn right on the Sensitivity Results tab, but you can also create them in their own resizable windows by clicking the button labeled New Window. A right-click on any graph allows you to change its properties, copy it to the clipboard, or save it as an image file.

Sensitivity Graph

The optimal system type (OST) graph gives the highest-level view of the sensitivity results. It shows the least-cost type of system (diesel-battery is one type of system, wind-diesel-battery is another) versus two sensitivity variables. The example below shows the same information we just saw in the tabular display above. The graphic format makes it easier to see under which conditions the different types of systems are optimal. Diamonds indicate points where HOMER actually solved for the least-cost system. All other points are colored using interpolation.

Tabular Graphic



Written by: Tom Lambert (support@homerenergy.com)

Last modified: May 6, 2004

For more information

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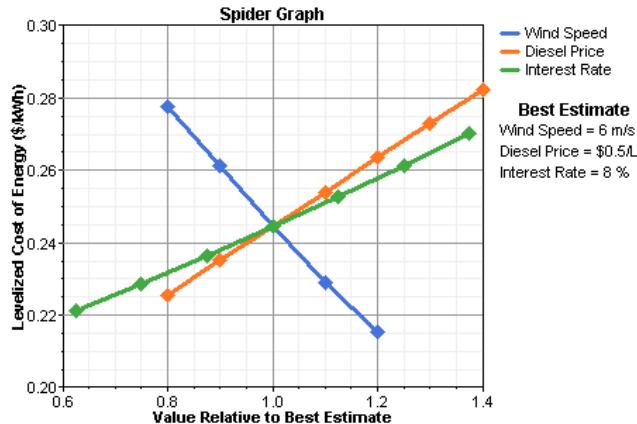
2.7.3.1 Why would I do a sensitivity analysis?



Why Would I Do a Sensitivity Analysis?

There are good reasons why you might want to enter multiple values for a particular input variable. First, you might be uncertain as to what the exact value of some variable should be. By specifying a range of values, you can determine how important that variable is, and how the answers change depending on its value. In other words, you can determine the *sensitivity* of the outputs to changes in that variable.

For example, imagine that a modeler doing a preliminary analysis of a wind-diesel system was uncertain about three variables: the annual average wind speed, the average fuel price over the life of the project, and the interest rate. To determine the sensitivity of the system's cost of energy to those three variables, she did a sensitivity analysis using HOMER. Her best estimate for the wind speed was 6 m/s, for the fuel price was \$0.50/L, and for the interest rate was 8%. But she entered multiple values for each variable, covering the range of uncertainty of each. HOMER produced the spider graph shown below, showing that the cost of energy is most sensitive to the wind speed (the wind speed line is the steepest). As a result, the modeler chose to invest more time and money to obtain a more accurate estimate of the wind speed.



Another reason for performing a sensitivity analysis is to make a single analysis applicable to more than one installation. For example, imagine you are designing small renewable power systems for six telecom sites. If the sites are similar in most respects but there is some variation in wind speed from one site to another, you could specify several wind speeds spanning the appropriate range. Then a single analysis would be sufficient to design all six hybrid systems. The results of such an analysis might look like the example shown below, where HOMER has suggested a PV/battery system for the site with the lowest wind speed, and wind/PV/battery systems for the sites with higher wind speeds.

| RESULTS | | | | | | | | | | | | | | | | | | |
|-------------|-----------|--|---|---|---|---|---|---|-----|-------|--------|---------|----------------|----------|----------|-----------|---------------------|-----------|
| | | Sensitivity Cases: Left Click on sensitivity case to see optimization cases. | | | | | | | | | | | | | | | | |
| Sensitivity | | Architecture | | | | | | | | | | | Cost | | | | | |
| Interest | Fuel Cost | ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦ | PV | 15/50 | Gen100 | 1kWh LA | Converter (kW) | Dispatch | COE (\$) | NPC (\$) | Operating Cost (\$) | Initial |
| 10.00 | 0.60 | | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.13 | \$207,643 | \$4,919 | \$163,000 |
| 10.00 | 0.80 | | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.19 | \$211,635 | \$5,358 | \$163,000 |
| 10.00 | 1.20 | | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.31 | \$219,620 | \$6,238 | \$163,000 |
| 10.00 | 1.00 | | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.25 | \$215,628 | \$5,798 | \$163,000 |
| 12.00 | 0.60 | | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.51 | \$200,928 | \$4,836 | \$163,000 |
| 12.00 | 0.80 | | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.57 | \$204,378 | \$5,276 | \$163,000 |
| 12.00 | 1.20 | | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.69 | \$211,277 | \$6,156 | \$163,000 |
| 12.00 | 1.00 | | | | | | | | 1.0 | 2 | 100 | 5 | 100 | LF | \$3.60 | \$207,027 | \$5,746 | \$163,000 |

See also

[Definition of sensitivity analysis](#)

Written by: Tom Lambert (support@homerenergy.com)
Last modified: June 18, 2004

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2.7.3.2 Adding Sensitivity Values



Adding Sensitivity Values

The Sensitivity Values drop-down appears when you click on a sensitivity button. Use it to enter multiple values for a particular input variable in order to perform a [sensitivity analysis](#) on that variable. The values you enter in this table do not have to be evenly spaced, nor do they have to be in ascending or descending order. You can enter them in any order you want. You can link this variable to another by making a selection from the drop-down box labeled Linked to. For more information, see [Linked Sensitivities](#).

In the following example, the user has entered several values for the [interest rate](#). The interest rate is therefore a [sensitivity variable](#) in this example.

| | | |
|----------------------------------|----|--------------------------------------|
| Annual Real Interest Rate (%): | 6 | <input type="button" value="▲ [4]"/> |
| Project Lifetime (years): | 25 | <input type="button" value="▼"/> |
| System Fixed Capital Cost (\$): | 0 | <input type="button" value="6"/> |
| System Fixed O&M Cost (\$/year): | 0 | <input type="button" value="8"/> |
| | | <input type="button" value="10"/> |
| | | <input type="button" value="12"/> |

See also

[Definition: Sensitivity variable](#)

[Definition: Sensitivity analysis](#)

[Linked sensitivities](#)

[Sensitivity Inputs window](#)

[Sensitivity results](#)

[Why would I do a sensitivity analysis?](#)

For more information

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2.8 Library View



Library

In the Library view, you can add, remove, or modify saved definitions for components, resources, and the grid. You can save simulation parameter sets, and load saved ones. You can also change the defaults for components, resources, and grid.

A Library tree will display on the left side of the screen listing [Components](#), [Resources](#), [Grid](#), and [Simulation Parameters](#). Different types of library entries are listed under each category. Entries in **bold** are in your user library. The non-bold entries are part of the HOMER built-in library and can't be modified. To change any of the built-in components, first select it and click the button to make a copy of the entry in your user library. You can then edit the copy, which will appear in the list in bold.

You can change the default settings by selecting a library entry type (i.e. battery, wind turbine, fuels). We will use Battery, under the Components category, as an example. Click on the word Battery. In the space to the right of the tree, a drop-down menu will appear. You can use this menu to change the default Battery. You change the default for any of the entry types in the Library this way.

To view or edit any of the entries under the battery entry type, click on the triangle to the left of the word battery to expand the list, and then click on any of the entries.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.8.1 Components



Components Library

The components library contains saved component definitions, and allows you to specify new ones. You can create new battery models, and change advanced parameters.

See also

[Create a New Fuel](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.8.1.1 Battery



Battery

The battery library listing is under the components category. Here you can view or specify the properties of the library batteries. You can create a new battery from scratch or by copying an existing one.

Use this menu to give the battery a unique name and to set its properties. HOMER will add the new battery to your [component library](#). You will then see the new battery in the list of available battery types on the Battery menu.

Parameters

| Variable | Description |
|---|--|
| Description | A unique name used to identify this type of battery |
| Manufacturer | An optional field used to specify the manufacturer of the battery |
| Notes | An optional field used to specify manufacturer contact information, prices, or anything noteworthy |
| Nominal Voltage | The rated voltage. It is called nominal because the actual voltage varies according to the battery's operating conditions and state of charge. |
| Round Trip Efficiency | The round trip DC-to-storage-to-DC efficiency of the battery bank |
| Minimum State of Charge | The relative state of charge below which the battery bank is never drawn |
| Maximum Charge Rate | The battery's maximum allowable charge rate, measured in amps per amp-hour of unfilled capacity |
| Maximum Charge Current | The absolute maximum charge current, in amps |
| Maximum Discharge Current | The absolute maximum discharge current, in amps |
| Float Life | The maximum lifetime of the battery, regardless of usage, in years |

Battery Storage Model

You can specify the battery storage model under the "Storage" tab of the battery library menu. First, choose whether to use a simple or kinetic storage model for the battery.

Storage model: simple kinetic battery model

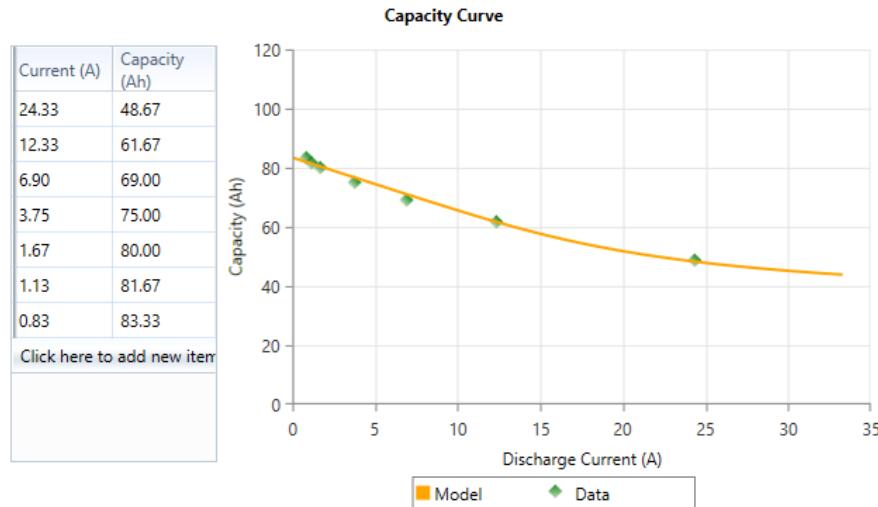
Nominal capacity is the total capacity of the battery's storage, and assumes that the percentage loss on charge and on discharge are the same. For example, if you choose a round trip efficiency of 81%, HOMER divides this up into 90% efficiency for charging, and 90% efficiency for discharging. So if the capacity of the battery is 100 kWh, you can put in 111.1 kWh ($100/0.9$) and you can take out 90 kWh ($100*0.9$).

Simple

If you set the storage model to simple, you need enter only the nominal capacity in amp-hours. HOMER will use this as the actual capacity of the battery.

Kinetic

The kinetic battery model represents the battery as a two-tank energy storage device. The *available tank* can be immediately charged or discharged, while the *bound tank* can only be charged or discharged at a limited rate.



You can define a kinetic battery model by entering points into the capacity table pictured above. HOMER calculates the parameters of a two-tank system that best fit the data given in the capacity curve. For detailed information about these parameters and how they are used, please see the article on the [kinetic battery model](#).

| Variable | Description |
|------------------|--|
| Maximum Capacity | The combined size of the available and bound tanks |
| Capacity Ratio | The ratio of the size of the available tank to the combined size of both tanks |
| Rate Constant | A measure of how quickly energy can move between the available and bound tanks |

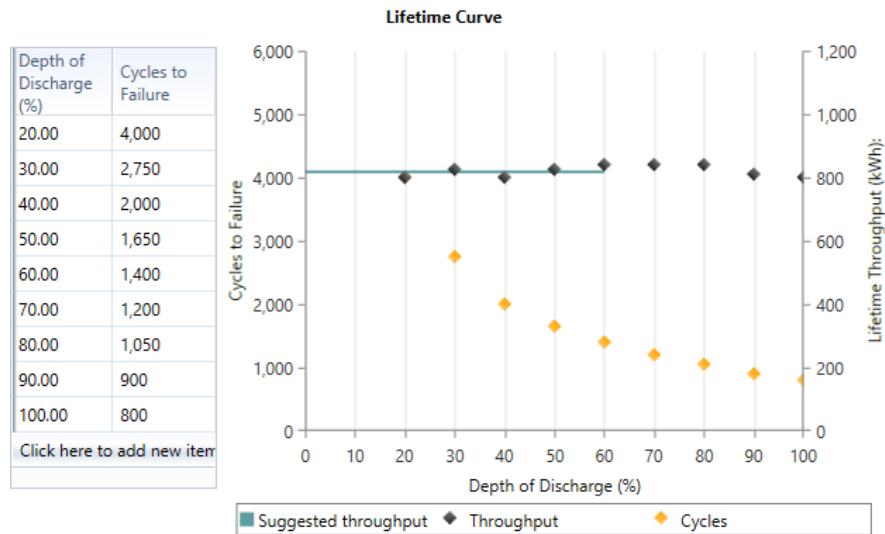
Lifetime

You can choose whether the battery will need replacement after a fixed length of time, or after a fixed quantity of energy cycles through it, or whichever of those two happens first. If you choose to limit the battery life to a certain number of years, you will need to enter that number of years as the [float life](#).

If you choose to limit the battery life to a certain quantity of energy throughput, you will need to enter that quantity as the [lifetime throughput](#). You will also have the option of entering the battery lifetime curve to help calculate this lifetime throughput value.

In a lifetime test, the tester subjects the battery to repeated regular charge and discharge cycles. Each cycle, the battery is discharged down to a certain depth of discharge, then fully charged again. The lifetime test determines how many such cycles the battery can withstand before it needs replacement. Manufacturers perform a series of these tests at different depths of discharge to create the battery's lifetime curve.

A lifetime curve shows the number of cycles to failure versus the depth of the cycles. An example appears below. Such curves result from the lifetime tests that battery manufacturers typically perform to characterize the longevity of their products.



You specify the battery lifetime curve in HOMER as a table of cycles to failure versus depth of discharge. HOMER plots that series of points as yellow diamonds. As in the example that appears above, that plot typically shows a sharp decrease in the number of cycles to failure with increasing depth of discharge. But HOMER also plots the lifetime throughput, which it calculates for each point in the lifetime curve using the following equation:

$$Q_{\text{lifetime},i} = f_i d_i \left(\frac{q_{\max} V_{\text{nom}}}{1000 W/kW} \right)$$

where:

- $Q_{\text{lifetime},i}$ = the lifetime throughput [kWh]
- f_i = the number of cycles to failure
- d_i = the depth of discharge [%]
- q_{\max} = the maximum capacity of the battery [Ah]
- V_{nom} = the nominal voltage of the battery [V]

HOMER plots these values as black diamonds on the lifetime curve (using the right-hand y-axis). Their values typically show only a weak dependence on the depth of discharge. HOMER's simulation logic makes the simplifying assumption that the lifetime throughput does not depend on the depth of discharge. The horizontal black line in the lifetime curve shows the specified value of lifetime throughput. The line is drawn only across the allowable range of depth of discharge.

See also

[Battery Inputs window](#)

[Component library](#)

[Kinetic battery model](#)

For more information

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2.8.1.1.1 Vanadium Battery



Vanadium Battery

The Vanadium battery model is intended to simulate certain kinds of vanadium redox flow batteries that allow users to size energy and power independently. This option requires several parameters, listed and described here.

General

| Variable | Description |
|----------|-------------|
| | |

| | |
|---------------------------------------|--|
| Round Trip Efficiency | The round trip DC-to-storage-to-DC efficiency of the battery bank |
| Cell Stack Lifetime | The lifetime of the cell stack. The cell stack replacement cost occurs at the end of the cell stack lifetime. |
| Electrolyte Lifetime | The lifetime of the electrolyte. The electrolyte replacement cost occurs at the end of the electrolyte lifetime. |

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2.8.1.1.2 Zinc Battery



Zinc Battery

The Zinc battery model is appropriate for some batteries that allow replacement of the cell stack and electrolyte separately. This option requires several parameters, listed in the table below.

General

| Variable | Description |
|---------------------------------------|--|
| Nominal Voltage | The rated DC voltage. HOMER multiplies the nominal voltage by the nominal capacity in Ah to calculate the nominal capacity in kWh. |
| Nominal Capacity | The amount of energy that the battery stores at full charge |
| Round Trip Efficiency | The round trip DC-to-storage-to-DC efficiency of the battery bank |
| Lifetime | The number of years the battery will last before it requires a complete replacement |
| Cell Stack Lifetime | The number of years the cell stack will last before it needs replacement |
| Max Charge Current | The maximum rate at which the system can put energy into the battery |
| Max Discharge Current | The maximum rate at which the system can take energy out of the battery |

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2.8.1.2 Generator



Generator

The Generator tab in the [Generator](#) window gives you access to the following variables:

| Variable | Description |
|----------|--|
| AC | The type of generator output current (alternating current or direct current) |
| Capacity | |

| | |
|--|--|
| | Nominal capacity (kW) of the generator. If the generator size is different in the search space, the fuel curve will be scaled. |
| Lifetime (Operating Hours) | The number of hours the generator can operate before needing replacement |
| Minimum Load Ratio | The minimum allowable load on the generator expressed as a percentage of its capacity |
| Heat Recovery Ratio | The percentage of waste heat that can be used to serve the thermal load. If you are not modeling a thermal load or you do not intend to recover waste heat from the generator, set this to zero. |
| Cofire with Biogas | If selected, this allows access to inputs relating to the cofiring of a generator with a mixture of fossil fuel (usually diesel fuel, natural gas, or propane) and biogas |
| Substitution Ratio | The ratio with which the biogas replaces fossil fuel in the cofired generator, in % |
| Minimum Fossil Fraction | The minimum allowable fossil fraction, in %, for a cofired generator |
| Derating Factor | The relative capacity of the generator at the minimum fossil fraction, in % |
| Minimum Run Time | Once the dispatch starts the generator, it will remain on for this duration or longer |

Note: To the right of each numerical input is a sensitivity button (▼) which allows you to do a [sensitivity analysis](#) on that variable. For more information, please see [Why would I want to do a sensitivity analysis?](#)

For more information

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2.8.1.3 PV

Manufacturer Properties

The Manufacturer Properties box displays some basic information for the type of PV panel you have selected.

| Variable | Description |
|--------------|---|
| Manufacturer | The company that manufactures the PV panel |
| Website | The manufacturer's website |
| Type | The type of PV technology |
| Abbreviation | A short label used to identify the PV array |
| Notes | Hints for modeling the PV system |

[\[TOP\]](#)

2.8.1.4 Wind Turbine



Wind Turbine

This menu lets you view or specify the properties of the library wind turbines. You can create a new wind turbine from scratch or by copying an existing one. Change the properties as required and give the new wind turbine a unique name to distinguish it from others. HOMER will add this new wind turbine to your [component library](#) when you click OK. The new wind turbine will then be included in the list of available wind turbine types on the [Wind Turbine Inputs](#) window.

General

| Variable | Description |
|-------------|--|
| Description | A unique name used to identify this type of wind turbine |

| | |
|--------------|--|
| Abbreviation | A short label which is used in column headings to identify this wind turbine |
| Manufacturer | An optional field used to specify the manufacturer of the wind turbine |
| Website | An optional field to hold the website of the manufacturer |
| Notes | An optional field used to specify manufacturer contact information, prices, or anything noteworthy |
| Current Type | The type of electricity produced by the wind turbine, either direct current (DC) or alternating current (AC) |

Power curve

The power curve is the most important property of the wind turbine. It describes the amount of power the turbine produces versus the wind speed at hub height.

Enter as many points on the power curve as you have available. HOMER uses linear interpolation to calculate the output of the wind turbine at intervening points.

Written by: Tom Lambert (support@homerenergy.com)

Last modified: October 29, 2004

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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2.8.1.5 Flywheel



Create New Flywheel

This window lets you view or specify the properties of library flywheels. You can create a new flywheel from scratch or by copying an existing one. Change the properties as required and give the new wind turbine a unique name to distinguish it from others. HOMER will add this new flywheel to your component library when you click OK. The new flywheel will then appear in the list of available flywheel types on the Flywheel Inputs window.

Properties

| Variable | Description |
|---------------------------|--|
| Description | A unique name used to identify this type of flywheel |
| Manufacturer | An optional field used to specify the manufacturer of the flywheel |
| Website | An optional field to hold the website of the manufacturer |
| Notes | An optional field used to specify manufacturer contact information, prices, or anything noteworthy |
| Charge/Discharge Capacity | The maximum amount of power the flywheel can absorb or provide. (HOMER assumes that the flywheel's capacity to absorb power is equal to its capacity to provide power.) This is the amount of operating capacity that the flywheel provides to the system. |
| Parasitic load | The amount of electricity necessary to operate the flywheel. HOMER models this as a constant electrical load, and considers a system feasible only if it can meet this load at all times during the simulation. |

See also

[Flywheel Inputs window](#)

[Component library](#)

[Operating reserve](#)

For more information

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2.8.2 Resources



Resources Library

The resources library contains saved resource definitions, and allows you to specify new resources. In this initial HOMER Pro release, only Fuels are implemented in the resource library. You can specify new fuels here, and access them from the Fuels dropdown menu in the Generator component. Solar, Wind, Temperature, Hydro and Biomass library resources are forthcoming.

See also

[Create a New Fuel](#)

For more information

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2.8.2.1 Create a New Fuel



Create a New Fuel

HOMER Pro users can create new fuels with specific properties. The properties are initially copied from the fuel that was selected when you clicked the New button. Change the properties as required and give the new fuel a unique name to distinguish it from others. HOMER will add this new fuel to your [component library](#) when you click OK. The new fuel will then be included in the list of available fuel types on the [Generator Inputs](#) and [Boiler Inputs](#) windows.

| Variable | Description |
|--------------------------------|--|
| Description | A unique name for the fuel |
| Lower Heating Value | The energy released per kg of fuel consumed |
| Density | Density in kg/m ³ (the density of water is 1000 kg/m ³) |
| Carbon Content | The mass-based carbon content of the fuel, in % |
| Sulfur Content | The mass-based sulfur content of the fuel, in % |
| Units | The preferred units for amount and price of the fuel |

For more information

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2.8.3 Grid



Grid Library

The grid library contains saved definitions of custom grid configurations. Here you can view existing grid definitions, modify advanced grid parameters, and save new grid definitions that you can quickly add to any model.

See also

[Grid component](#)

For more information

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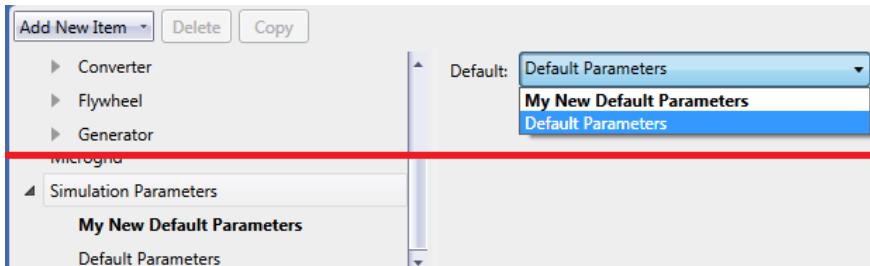
2.8.4 Simulation Parameters



Simulation Parameters Library

The simulation parameters library contains preset saved configurations for simulations. Here you can view existing simulation parameter sets, modify existing ones, and save new definitions that you can quickly set on any model.

You can use this library to create your own default settings. First copy an existing simulation parameters entry or create a new one from scratch. Adjust the settings as desired. Then, as described for Batteries in the main [library help page](#), click on "Simulation Parameters" and change the entry in the drop down menu to the right of the library tree.



The parameters here correspond to those in the [Project Set Up](#).

See also

[Project Set Up](#)

For more information

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3. HOMER's Calculations

3.1 How HOMER Calculates the PV Array Output



How HOMER Calculates the PV Array Power Output

HOMER uses the following equation to calculate the output of the PV array:

$$P_{PV} = Y_{PV} f_{PV} \left(\frac{\bar{G}_T}{\bar{G}_{T,STC}} \right) \left[1 + \alpha_p (T_c - T_{c,STC}) \right]$$

where:

- Y_{PV} is the rated capacity of the PV array, meaning its power output under [standard test conditions](#) [kW]
- f_{PV} is the [PV derating factor](#) [%]
- \bar{G}_T is the [solar radiation incident on the PV array](#) in the current time step [kW/m²]
- $\bar{G}_{T,STC}$ is the incident radiation at [standard test conditions](#) [1 kW/m²]
- α_P is the [temperature coefficient of power](#) [%/°C]
- T_c is the [PV cell temperature](#) in the current time step [°C]
- $T_{c,STC}$ is the PV cell temperature under [standard test conditions](#) [25 °C]

If on the PV Inputs window you choose not to model the effect of temperature on the PV array, HOMER assumes that the temperature coefficient of power is zero, so that the above equation simplifies to:

$$P_{PV} = Y_{PV} f_{PV} \left(\frac{\bar{G}_T}{\bar{G}_{T,STC}} \right)$$

See also

- [PV Inputs window](#)
- [PV derating factor](#)
- [PV temperature coefficient of power](#)
- [Calculating the radiation incident on the PV array](#)
- [Calculating the PV cell temperature](#)
- [Standard test conditions](#)
- [Can HOMER model a maximum power point tracker?](#)

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3.2 Beacon Power Smart Energy 25 Flywheel



Beacon Power Smart Energy 25 Flywheel

The Smart Energy 25 is a 25 kWh, 100 kW carbon fiber flywheel. It is an AC device, but HOMER will connect it to the DC bus because it cannot model AC electrical storage. To model this flywheel in HOMER, you should add a converter, but make it free, 100% efficient, and larger than the aggregate capacity of the largest number of flywheels that you are considering. If your system also includes PV, we recommend modeling the PV as an AC device with the inverter costs and losses included with the PV module.

In a hybrid power application, energy storage provides a buffer so that diesel generators can be turned off and remain off during short lulls in the wind or passing clouds. To maximize this benefit HOMER may use the full range of the energy storage device's state of charge before turning on another generator and recharging the device close to 100% state of charge.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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3.3 How HOMER Calculates Emissions



How HOMER Calculates Emissions

HOMER calculates the emissions of the following six pollutants:

| Pollutant | Description |
|------------------------------------|---|
| Carbon Dioxide (CO ₂) | Nontoxic greenhouse gas. |
| Carbon Monoxide (CO) | Poisonous gas produced by incomplete burning of carbon in fuels. Prevents delivery of oxygen to the body's organs and tissues, causing headaches, dizziness, and impairment of visual perception, manual dexterity, and learning ability. |
| Unburned Hydrocarbons (UHC) | Products of incomplete combustion of hydrocarbon fuel, including formaldehyde and alkenes. Lead to atmospheric reactions causing photochemical smog. |
| Particulate Matter (PM) | A mixture of smoke, soot, and liquid droplets that can cause respiratory problems and form atmospheric haze. |
| Sulfur Dioxide (SO ₂) | A corrosive gas released by the burning of fuels containing sulfur (like coal, oil and diesel fuel). Cause respiratory problems, acid rain, and atmospheric haze. |
| Nitrogen Oxides (NO _x) | Various nitrogen compounds like nitrogen dioxide (NO ₂) and nitric oxide (NO) formed when any fuel is burned at high temperature. These compounds lead to respiratory problems, smog, and acid rain. |

Emissions of these pollutants result from:

- the production of electricity by the generator(s)
- the production of thermal energy by the boiler
- the consumption of grid electricity

HOMER models the emissions of the generators and the boiler in a similar way, since both consume fuel of known properties. It models the grid slightly differently. This article will first cover how HOMER calculates the emissions of the generators and boiler, then how it calculates the emissions from the grid.

Generators, Boiler, and Reformer

Before simulating the power system, HOMER determines the emissions factor (kg of pollutant emitted per unit of fuel consumed) for each pollutant. After the simulation, it calculates the annual emissions of that pollutant by multiplying the emissions factor by the total annual fuel consumption.

You directly specify the emissions factors for four of the six pollutants: carbon monoxide, unburned hydrocarbons, particulate matter, and nitrogen oxides. Using these values and the carbon and sulfur content of the fuel, HOMER does some calculations to find the emissions factors for the two remaining pollutants: carbon dioxide and sulfur dioxide. In doing so, HOMER uses three principal assumptions:

1. Any carbon in the fuel that does not get emitted as carbon monoxide or unburned hydrocarbons gets emitted as carbon dioxide.
2. The carbon fraction of the unburned hydrocarbon emissions is the same as that of the fuel.
3. Any sulfur in the *burned* fuel that does not get emitted as particulate matter gets emitted as sulfur dioxide.

Grid

In simulating a grid-connected system, HOMER calculates the net grid purchases, equal to the total grid purchases minus the total grid sales. To calculate the emissions of each pollutant associated with these net grid purchases, HOMER multiplies the net grid purchases (in kWh) by the emission factor (in g/kWh) for each pollutant. If the system sells more power to the grid than it buys from the grid over the year, the net grid purchases will be negative and so will the grid-related emissions of each pollutant.

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3.4 How HOMER Calculates the Hydro Power Output



How HOMER Calculates the Hydro Power Output

In each time step, HOMER calculates the electrical power output of the hydro turbine using the following equation:

$$P_{\text{hyd}} = \frac{\eta_{\text{hyd}} \cdot \rho_{\text{water}} \cdot g \cdot h_{\text{net}} \cdot \dot{Q}_{\text{turbine}}}{1000 \text{ W/kW}}$$

where:

P_{hyd} = power output of the hydro turbine [kW]

η_{hyd} = [hydro turbine efficiency](#) [%]

ρ_{water} = density of water [1000 kg/m³]

g = acceleration due to gravity [9.81 m/s²]

h_{net} = [effective head](#) [m]

\dot{Q}_{turbine} = [hydro turbine flow rate](#) [m³/s]

See also

[Nominal hydro power](#)

For more information

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3.5 How HOMER Calculates Clearness Index



How HOMER Calculates Clearness Index

On the Solar Resource window, for each month of the year you can enter either the average radiation or the average clearness index. When you enter one, HOMER calculates the other. This article describes the relationship between the two variables, and how HOMER calculates one from the other.

The [clearness index](#) is a dimensionless number between 0 and 1 indicating the fraction of the solar radiation striking the top of the atmosphere that makes it through the atmosphere to strike the Earth's surface. The following equation defines the monthly average clearness index:

$$K_T = \frac{H_{\text{ave}}}{H_{0,\text{ave}}}$$

where:

H_{ave} is the monthly average radiation on the horizontal surface of the earth [kWh/m²/day]

$H_{0,\text{ave}}$ is the *extraterrestrial horizontal radiation*, meaning the radiation on a horizontal surface at the top of the earth's atmosphere [kWh/m²/day]

For a given latitude, we can calculate $H_{0,\text{ave}}$ for any month of the year. So if we know either H_{ave} or K_T , we can calculate the other using the above equation. HOMER does exactly that every time you enter a value into the monthly data table on the Solar Resource Inputs window. If you enter an average radiation value, HOMER will calculate the corresponding clearness index.

The rest of this article describes how HOMER calculates $H_{0,\text{ave}}$, the monthly average extraterrestrial radiation.

As described in more detail in the article on calculating the radiation incident on the PV array, HOMER uses the following equation to calculate the intensity of solar

radiation at the top of the Earth's atmosphere:

$$G_{on} = G_{sc} \left(1 + 0.033 \cdot \cos \frac{360n}{365} \right)$$

where:

G_{sc} is the solar constant [1.367 kW/m²]

n is the day of the year [a number between 1 and 365]

The equation above gives the extraterrestrial radiation on a surface normal to the sun's rays. To calculate the extraterrestrial radiation on the *horizontal* surface, HOMER uses the following equation:

$$G_o = G_{on} \cos \theta_z$$

where:

θ_z is the zenith angle [°]

HOMER calculates the zenith angle using the following equation:

$$\cos \theta_z = \cos \phi \cos \delta \cos \omega + \sin \phi \sin \delta$$

where:

f is the latitude [°]

d is the solar declination [°]

w is the hour angle [°]

HOMER calculates the solar declination according to the following equation:

$$\delta = 23.45^\circ \sin \left(360^\circ \frac{284+n}{365} \right)$$

where:

n is the day of the year [a number between 1 and 365]

We can find the total daily extraterrestrial radiation per square meter by integrating the equation for G_o from sunrise to sunset. This integration gives the following equation:

$$H_o = \frac{24}{\pi} G_{on} \left[\cos \phi \cos \delta \sin \omega_s + \frac{\pi \omega_s}{180^\circ} \sin \phi \sin \delta \right]$$

where:

H_o is the average extraterrestrial horizontal radiation for the day [kWh/m²/day]

ω_s is the sunset hour angle [°]

HOMER calculates the sunset hour angle using the following equation:

$$\cos \omega_s = -\tan \phi \tan \delta$$

HOMER calculates H_o for each day of the month, and finds the average for the month as follows:

$$H_{o,ave} = \frac{\sum_{n=1}^N H_o}{N}$$

where:

$H_{o,ave}$ is the average extraterrestrial horizontal radiation for the month [kWh/m²/day]

N is the number of days in the month

If you enter the monthly average global solar radiation, HOMER divides it by $H_{o,ave}$ to find the monthly average clearness index.

See also

[Clearness index](#)

[PV Inputs window](#)

[Calculating the radiation incident on the PV array](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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3.6 How HOMER Calculates the Maximum Battery Charge Power



How HOMER Calculates the Maximum Battery Charge Power

In each time step, HOMER calculates the maximum amount of power that the battery bank can absorb. It uses this "maximum charge power" when making decisions such as whether the battery can absorb all available surplus renewable power, or how much surplus power a cycle charging generator should produce. The maximum charge power varies from one time step to the next according to its state of charge and its recent charge and discharge history.

HOMER imposes three separate limitations on the battery bank's maximum charge power. The first limitation comes from the kinetic battery model. As described in the article on the [kinetic battery model](#), the maximum amount of power that can be absorbed by the two-tank system is given by the following equation:

$$P_{batt,cmax,kbm} = \frac{kQ_1 e^{-k\Delta t} + Qkc(1 - e^{-k\Delta t})}{1 - e^{-k\Delta t} + c(k\Delta t - 1 + e^{-k\Delta t})}$$

where

Q_1 is the available energy [kWh] in the battery at the beginning of the time step,

Q is the total amount of energy energy [kWh] in the battery at the beginning of the time step,

c is the battery capacity ratio [unitless],

k is the battery rate constant [h^{-1}], and

Δt is the length of the time step [h].

The second limitation relates to the [maximum charge rate](#) of the battery, which is the A/Ah value visible on the [battery details window](#). The battery charge power corresponding to this maximum charge rate is given by the following equation:

$$P_{batt,cmax,mcr} = \frac{(1 - e^{-\alpha \Delta t})(Q_{\max} - Q)}{\Delta t}$$

where

a_c is the battery's maximum charge rate [A/Ah], and

Q_{\max} is the total capacity of the battery bank [kWh].

The third limitation relates to the battery's maximum charge current, which also appears on the battery details window. The maximum battery bank charge power corresponding to this maximum charge current is given by the following equation:

$$P_{batt,cmax,mcc} = \frac{N_{batt} I_{\max} V_{nom}}{1000}$$

where

N_{batt} is the number of batteries in the battery bank,

I_{\max} is the battery's maximum charge current [A], and

V_{nom} is the battery's nominal voltage [V].

HOMER sets the maximum battery charge power equal to the least of these three values, assuming each applies after charging losses, hence:

$$P_{batt,cmax} = \frac{\text{MIN}(P_{batt,cmax,kbm}, P_{batt,cmax,mcr}, P_{batt,cmax,mcc})}{\eta_{batt,c}}$$

where $\eta_{batt,c}$ is the [battery charge efficiency](#).

See also

[Kinetic battery model](#)

[Calculating maximum battery discharge power](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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3.7 How HOMER Calculates the Maximum Battery Discharge Power



How HOMER Calculates the Maximum Battery Discharge Power

In each time step, HOMER calculates the maximum amount of power that the battery bank can discharge. It uses this "maximum discharge power" when making decisions such as whether the battery can serve the load on its own. The maximum discharge power varies from one time step to the next according to its state of charge and its recent charge and discharge history, as determined by the kinetic battery model.

As described in the article on the [kinetic battery model](#), the maximum amount of power that the battery bank can discharge over a specific length of time is given by the following equation:

$$P_{batt,dmax,kbm} = \frac{-kcQ_{max} + kQ_1 e^{-k\Delta t} + Qkc(1 - e^{-k\Delta t})}{1 - e^{-k\Delta t} + c(k\Delta t - 1 + e^{-k\Delta t})}$$

where

Q_1 is the available energy [kWh] in the battery at the beginning of the time step,

Q is the total amount of energy energy [kWh] in the battery at the beginning of the time step,

Q_{max} is the total capacity [kWh] of the battery bank,

c is the battery capacity ratio [unitless],

k is the battery rate constant [h^{-1}], and

Δt is the length of the time step [h].

HOMER assumes that the discharging losses occur after the energy leaves the two-tank system, hence the battery bank's maximum discharge power is given by the following equation:

$$P_{batt,dmax} = \eta_{batt,d} P_{batt,dmax,kbm}$$

where $\eta_{batt,d}$ is the [battery discharge efficiency](#).

See also

[Kinetic battery model](#)

[Calculating maximum battery charge power](#)

For more information

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3.8 How HOMER Calculates the Radiation Incident on the PV Array



How HOMER Calculates the Radiation Incident on the PV Array

In the solar resource input window you specify, for each time step, the *global horizontal radiation*. That is the total amount of solar radiation striking the horizontal surface on the earth. But the power output of the PV array depends on the amount of radiation striking the surface of the PV array, which in general is not horizontal. So in each time step, HOMER must calculate the global solar radiation incident on the surface of the PV array. This article describes that process, which

is based on the methods in the first two chapters of [Duffie and Beckman \(1991\)](#)

We can describe the orientation of the PV array using two parameters, a slope and an azimuth. The slope is the angle formed between the surface of the panel and the horizontal, so a slope of zero indicates a horizontal orientation, whereas a 90° slope indicates a vertical orientation. The azimuth is the direction towards which the surface faces. HOMER uses the convention whereby zero azimuth corresponds to due south, and positive values refer to west-facing orientations. So an azimuth of -45° corresponds to a southeast-facing orientation, and an azimuth of 90° corresponds to a west-facing orientation.

The other factors relevant to the geometry of the situation are the latitude, the time of year, and the time of day. The time of year affects the solar declination, which is the latitude at which the sun's rays are perpendicular to the earth's surface at solar noon. HOMER uses the following equation to calculate the solar declination:

$$\delta = 23.45^\circ \sin\left(360^\circ \frac{284+n}{365}\right)$$

where:

n is the day of the year [a number 1 through 365]

The time of day affects the location of the sun in the sky, which we can describe by an hour angle. HOMER uses the convention whereby the hour angle is zero at solar noon (the time of day at which the sun is at its highest point in the sky), negative before solar noon, and positive after solar noon. HOMER uses the following equation to calculate the hour angle:

$$\omega = (t_s - 12\text{hr}) \cdot 15^\circ/\text{hr}$$

where:

t_s is the solar time [hr]

The value of t_s is 12hr at solar noon, and 13.5hr ninety minutes later. The above equation follows from the fact that the sun moves across the sky at 15 degrees per hour.

HOMER assumes that all time-dependent data, such as solar radiation data and electric load data, are specified not in solar time, but in *civil time*, also called local standard time. HOMER calculates solar time from civil time using the following equation:

$$t_s = t_c + \frac{\lambda}{15^\circ/\text{hr}} - Z_c + E$$

where:

t_c is the civil time in hours corresponding to the midpoint of the time step [hr]

λ is the longitude [°]

Z_c is the time zone in hours east of GMT [hr]

E is the equation of time [hr]

Note that west longitudes are negative, and time zones west of GMT are negative as well.

The equation of time accounts for the effects of obliquity (the tilt of the earth's axis of rotation relative to the plane of the ecliptic) and the eccentricity of the earth's orbit. HOMER calculates the equation of time as follows:

$$E = 3.82 \left(\begin{array}{l} 0.000075 + 0.001868 \cdot \cos B - 0.032077 \cdot \sin B \\ -0.014615 \cdot \cos 2B - 0.04089 \cdot \sin 2B \end{array} \right)$$

where B is given by:

$$B = 360^\circ \frac{(n-1)}{365}$$

where n is the day of the year, starting with 1 for January 1st.

Now, for a surface with any orientation, we can define the angle of incidence, meaning the angle between the sun's beam radiation and the normal to the surface, using the following equation:

$$\begin{aligned} \cos\theta &= \sin\delta \sin\phi \cos\beta \\ &\quad - \sin\delta \cos\phi \sin\beta \cos\gamma \\ &\quad + \cos\delta \cos\phi \cos\beta \cos\omega \\ &\quad + \cos\delta \sin\phi \sin\beta \cos\gamma \cos\omega \\ &\quad + \cos\delta \sin\beta \sin\gamma \sin\omega \end{aligned}$$

where:

θ is the angle of incidence [°]

β is the slope of the surface [°]

γ is the azimuth of the surface [°]

Φ is the latitude [°]

δ is the solar declination [°]

ω is the hour angle [°]

An incidence angle of particular importance, which we will need shortly, is the *zenith angle*, meaning the angle between a vertical line and the line to the sun. The zenith angle is zero when the sun is directly overhead, and 90° when the sun is at the horizon. Because a horizontal surface has a slope of zero, we can find a equation for the zenith angle by setting $B = 0^\circ$ in the above equation, which yields:

$$\cos \theta_z = \cos \phi \cos \delta \cos \omega + \sin \phi \sin \delta$$

where:

θ_z is the zenith angle [°]

Now we turn to the issue of the amount of solar radiation arriving at the top of the atmosphere over a particular point on the earth's surface. HOMER assumes the output of the sun is constant in time. But the amount of sunlight striking the top of the earth's atmosphere varies over the year because the distance between the sun and the earth varies over the year due to the eccentricity of earth's orbit. To calculate the *extraterrestrial normal radiation*, defined as the amount of solar radiation striking a surface normal (perpendicular) to the sun's rays at the top of the earth's atmosphere, HOMER uses the following equation:

$$G_{on} = G_{sc} \left(1 + 0.033 \cdot \cos \frac{360n}{365} \right)$$

where:

G_{on} is the extraterrestrial normal radiation [kW/m²]

G_{sc} is the solar constant [1.367 kW/m²]

n is the day of the year [a number between 1 and 365]

To calculate the *extraterrestrial horizontal radiation*, defined as the amount of solar radiation striking a horizontal surface at the top of the atmosphere, HOMER uses the following equation:

$$G_o = G_{on} \cos \theta_z$$

where:

G_o is the extraterrestrial horizontal radiation [kW/m²]

G_{on} is the extraterrestrial normal radiation [kW/m²]

θ_z is the zenith angle [°]

Since HOMER simulates on a time step by time step basis, we integrate the above equation over one time step to find the average extraterrestrial horizontal radiation over the time step:

$$\bar{G}_o = \frac{12}{\pi} G_{on} \left[\cos \phi \cos \delta (\sin \omega_2 - \sin \omega_1) + \frac{\pi(\omega_2 - \omega_1)}{180^\circ} \sin \phi \sin \delta \right]$$

where:

\bar{G}_o is the extraterrestrial horizontal radiation averaged over the time step [kW/m²]

G_{on} is the extraterrestrial normal radiation [kW/m²]

w_1 is the hour angle at the beginning of the time step [°]

w_2 is the hour angle at the end of the time step [°]

The above equation gives the average amount of solar radiation striking a horizontal surface at the top of the atmosphere in any time step. The solar resource data give the average amount of solar radiation striking a horizontal surface at the bottom of the atmosphere (the surface of the earth) in every time step. The ratio of the surface radiation to the extraterrestrial radiation is called the [clearness index](#). The following equation defines the clearness index:

$$k_T = \frac{\bar{G}}{\bar{G}_o}$$

where:

\bar{G} is the global horizontal radiation on the earth's surface averaged over the time step [kW/m²]

\bar{G}_o is the extraterrestrial horizontal radiation averaged over the time step [kW/m²]

Now let us look more closely at the solar radiation on the earth's surface. Some of that radiation is *beam radiation*, defined as solar radiation that travels from the sun to the earth's surface without any scattering by the atmosphere. Beam radiation (sometimes called direct radiation) casts a shadow. The rest of the radiation is *diffuse radiation*, defined as solar radiation whose direction has been changed by the earth's atmosphere. Diffuse radiation comes from all parts of the sky and does not cast a shadow. The sum of beam and diffuse radiation is called global solar radiation, a relation expressed by the following equation:

$$\bar{G} = \bar{G}_b + \bar{G}_d$$

where:

\bar{G}_b is the beam radiation [kW/m²]

\bar{G}_d is the diffuse radiation [kW/m²]

The distinction between beam and diffuse radiation is important when calculating the amount of radiation incident on an inclined surface. The orientation of the surface has a stronger effect on the beam radiation, which comes from only one part of the sky, than it does on the diffuse radiation, which comes from all parts of the sky.

However, in most cases we measure only the global horizontal radiation, not its beam and diffuse components. For that reason, HOMER expects you to enter global horizontal radiation in HOMER's Solar Resource Inputs window. That means that in every time step, HOMER must resolve the global horizontal radiation into its beam and diffuse components to find the radiation incident on the PV array. For this purpose HOMER uses correlation of [Erbs et al. \(1982\)](#), which gives the *diffuse fraction* as a function of the clearness index as follows:

$$\frac{\bar{G}_d}{\bar{G}} = \begin{cases} 1.0 - 0.09 \cdot k_T & \text{for } k_T \leq 0.22 \\ 0.9511 - 0.1604 \cdot k_T + 4.388 \cdot k_T^2 - 16.638 \cdot k_T^3 + 12.336 \cdot k_T^4 & \text{for } 0.22 < k_T \leq 0.80 \\ 0.165 & \text{for } k_T > 0.80 \end{cases}$$

For each time step, HOMER uses the average global horizontal radiation to calculate the clearness index, then the diffuse radiation. It then calculates the beam radiation by subtracting the diffuse radiation from the global horizontal radiation.

We are now almost ready to calculate the global radiation striking the tilted surface of the PV array. For this purpose HOMER uses the HDKR model, which assumes that there are three components to the diffuse solar radiation: an isotropic component which comes all parts of the sky equally, a circumsolar component which emanates from the direction of the sun, and a horizon brightening component which emanates from the horizon. Before applying that model we must first define three more factors.

The following equation defines R_b , the ratio of beam radiation on the tilted surface to beam radiation on the horizontal surface:

$$R_b = \frac{\cos \theta}{\cos \theta_z}$$

The anisotropy index, with symbol A_i , is a measure of the atmospheric transmittance of beam radiation. This factor is used to estimate the amount of circumsolar diffuse radiation, also called forward scattered radiation. The anisotropy index is given by the following equation:

$$A_i = \frac{\bar{G}_b}{\bar{G}_o}$$

The final factor we need to define is a factor used to account for 'horizon brightening', or the fact that more diffuse radiation comes from the horizon than from the rest of the sky. This term is related to the cloudiness and is given by the following equation:

$$f = \sqrt{\frac{\bar{G}_b}{\bar{G}}}$$

The HDKR model calculates the global radiation incident on the PV array according to the following equation:

$$\bar{G}_T = (\bar{G}_b + \bar{G}_d A_i) R_b + \bar{G}_d (1 - A_i) \left(\frac{1 + \cos \beta}{2} \right) \left[1 + f \sin^3 \left(\frac{\beta}{2} \right) \right] + \bar{G} \rho_g \left(\frac{1 - \cos \beta}{2} \right)$$

where:

b is the slope of the surface [°]

ρ_g is the ground reflectance, which is also called the albedo [%]

HOMER uses this quantity to calculate the cell temperature and the power output of the PV array.

See also

[Solar Resource Inputs window](#)

[Clearness index](#)

[How HOMER calculates the PV cell temperature](#)

[How HOMER calculates the PV array power output](#)

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3.9 How HOMER Calculates Wind Turbine Power Output



How HOMER Calculates Wind Turbine Power Output

HOMER calculates the power output of the wind turbine in each time step. This entails a three-step process to first calculate the wind speed at the hub height of the wind turbine, then to calculate how much power the wind turbine would produce at that wind speed at standard air density, then to adjust that power output value for the actual air density.

Calculating Hub Height Wind Speed

In each time step, HOMER calculates the wind speed at the hub height of the wind turbine using the inputs you specify in the Wind Resource Inputs window and the Wind Shear Inputs window.

If you choose to apply the logarithmic law, HOMER calculates the hub height wind speed using the following equation:

$$U_{hub} = U_{anem} \cdot \frac{\ln(z_{hub}/z_0)}{\ln(z_{anem}/z_0)}$$

where:

U_{hub} = the wind speed at the hub height of the wind turbine [m/s]

U_{anem} = the wind speed at anemometer height [m/s]

z_{hub} = the hub height of the wind turbine [m]

z_{anem} = the [anemometer height](#) [m]

z_0 = the surface roughness length [m]

$\ln(\dots)$ = the natural logarithm

If you choose to apply the power law, HOMER calculates the hub height wind speed using the following equation:

$$U_{hub} = U_{anem} \cdot \left(\frac{z_{hub}}{z_{anem}} \right)^a$$

where:

U_{hub} = the wind speed at the hub height of the wind turbine [m/s]

U_{anem} = the wind speed at anemometer height [m/s]

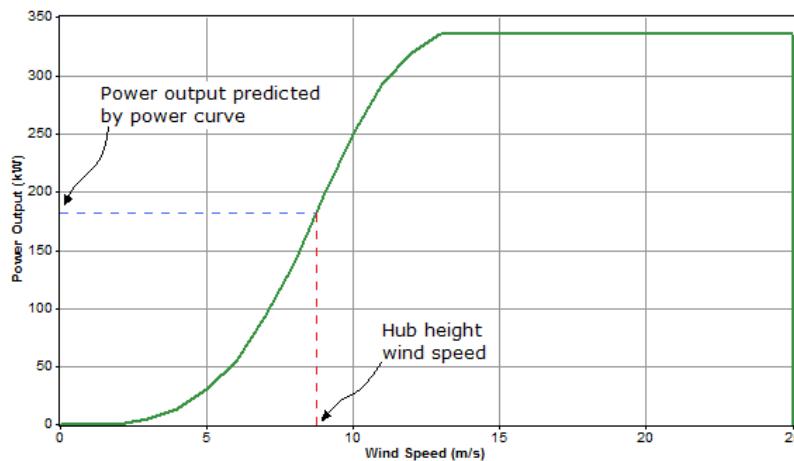
z_{hub} = the hub height of the wind turbine [m]

z_{anem} = the [anemometer height](#) [m]

a = the power law exponent

Calculating Turbine Power Output At Standard Air Density

Once HOMER has determined the hub height wind speed, it refers to the wind turbine's power curve to calculate the power output one would expect from that wind turbine at that wind speed under standard conditions of temperature and pressure. In the diagram below, the red dotted line indicates the hub height wind speed, and the blue dotted line indicates the wind turbine power output that the power curve predicts for that wind speed.



Applying Density Correction

Power curves typically specify wind turbine performance under conditions of standard temperature and pressure (STP). To adjust to actual conditions, HOMER multiplies the power value predicted by the power curve by the air density ratio, according to following equation:

$$P_{WTG} = \left(\frac{\rho}{\rho_0} \right) \cdot P_{WTG,STP}$$

where:

P_{WTG} = the wind turbine power output [kW]

$P_{WTG,STP}$ = the wind turbine power output at standard temperature and pressure [kW]

ρ = the actual air density [kg/m³]

ρ_0 = the air density at standard temperature and pressure (1.225 kg/m³)

See also

[Wind Resource Inputs window](#)

[Wind Shear Inputs window](#)

[Altitude](#)

For more information

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3.10 Operation of a Cofired Generator



Operation of a Cofired Generator

A co-fired generator operates on a mixture of fossil fuel and [biogas](#). In each time step, HOMER calculates the required output of the generator and the corresponding mass flow rates of fossil fuel and biogas. This calculation is based on several key assumptions:

Assumptions:

1. The biogas [substitution ratio](#) (z_{gas}) is a constant, independent of engine output power or fuel mixture.
2. The system will at all times attempt to maximize the use of biogas and minimize the use of fossil fuel.
3. The [fossil fraction](#) cannot go below a certain minimum.
4. Even if the derating factor associated with operating in dual-fuel mode is less than 100%, the generator can produce up to 100% of its rated power provided the fossil fraction is high enough.

The fuel curve of a cofired generator defines the fuel consumption of the generator in pure fossil mode. So the fossil fuel consumption in pure fossil mode is given by the following equation: (please see table of nomenclature below for a definition of all symbols)

$$\dot{m}_0 = \rho_{fossil} (F_0 \cdot Y_{gen} + F_1 \cdot P_{gen}) \quad (1)$$

And from assumption 1,

$$\begin{aligned} \dot{m}_0 &= \dot{m}_{fossil} + \frac{\dot{m}_{gas}}{z_{gas}} \\ \therefore \quad \dot{m}_{gas} &= z_{gas} (\dot{m}_0 - \dot{m}_{fossil}) \end{aligned} \quad (2)$$

Where z_{gas} is the biogas [substitution ratio](#). Now from the definition of the [fossil fraction](#),

$$x_{fossil} \equiv \frac{\dot{m}_{fossil}}{\dot{m}_0} \quad (3)$$

Using equations 2 and 3,

$$\begin{aligned} \dot{m}_{gas} &= z_{gas} (\dot{m}_0 - x_{fossil} \dot{m}_0) \\ \therefore \quad \dot{m}_{gas} &= z_{gas} \dot{m}_0 (1 - x_{fossil}) \end{aligned} \quad (4)$$

But for a given value of P_{bio} , the value of x_{fossil} is unknown so the above equation is not enough on its own to solve for the biogas flow rate. From assumption 2, we want to maximize \dot{m}_{gas} , which means we want to minimize x_{fossil} . But from assumption 3,

$$x_{fossil}^* \leq x_{fossil} \leq 1$$

where x_{fossil}^* is the [minimum fossil fraction](#) required for ignition. So the target value for \dot{m}_{gas} corresponds to . Using equation 4,

$$\dot{m}_{gas}^t = Z_{gas} \dot{m}_0 (1 - x_{fossil}^*) \quad (5)$$

But there are two independent upper limits on the actual value of \dot{m}_{gas} . At the minimum fossil fraction, the output of the generator is limited to Y_{gen}^* , defined as follows:

$$Y_{gen}^* = \tau \cdot Y_{gen}$$

where t , the [derating factor](#), is less than or equal to 1. This limitation can be implemented by imposing an upper limit on \dot{m}_{gas} corresponding to and . Using equations 1 and 4, this maximum value can be defined as:

$$\dot{m}_{gas}^* = Z_{gas} P_{fossil} (F_0 \cdot Y_{gen} + F_1 \cdot Y_{gen}^*) \cdot (1 - x_{fossil}^*) \quad (6)$$

This upper limit can be thought of as a physical limitation -- the maximum rate at which biogas can be ingested in the engine. The available biomass resource, a_{gas} , constitutes the other upper limit on \dot{m}_{gas} . So the actual value of \dot{m}_{gas} is the minimum of \dot{m}_{gas}^t , \dot{m}_{gas}^* , and a_{gas} :

$$\dot{m}_{gas} = \text{MIN}(\dot{m}_{gas}^t, \dot{m}_{gas}^*, a_{gas}) \quad (7)$$

Knowing the value of \dot{m}_{gas} , we can determine x_{fossil} . Solving equation 4 for x_{fossil} ,

$$x_{fossil} = 1 - \frac{\dot{m}_{gas}}{Z_{gas} \dot{m}_0} \quad (8)$$

And from equation 3,

$$\dot{m}_{fossil} = x_{fossil} \cdot \dot{m}_0 \quad (9)$$

So at any time step, given particular values of P_{bio} and a_{gas} , the biogas flow rate and the fossil fuel flow rate can be calculated from equations 7 and 9, respectively.

Table of Nomenclature

| Symbol | Units | Description |
|--------------------|---------|--|
| r_{fossil} | kg/L | density of fossil fuel |
| t | % | generator derating factor |
| a_{gas} | kg/hr | available biogas flow rate |
| \dot{m}_0 | kg/hr | fossil fuel flow rate (in pure fossil mode) |
| \dot{m}_{fossil} | kg/hr | fossil fuel flow rate (in dual-fuel mode) |
| \dot{m}_{gas} | kg/hr | biogas flow rate (in dual-fuel mode) |
| \dot{m}_{gas}^* | kg/hr | maximum value of biogas flow rate |
| \dot{m}_{gas}^t | kg/hr | target value of biogas flow rate |
| x_{fossil} | % | fossil fraction |
| x_{fossil}^* | % | minimum fossil fraction |
| Z_{gas} | none | biogas substitution ratio |
| F_0 | L/hr/kW | generator fuel curve intercept coefficient |
| F_1 | L/hr/kW | generator fuel curve slope |
| P_{gen} | kW | power output of the generator |
| Y_{gen}^* | kW | maximum output of generator at minimum fossil fraction |
| Y_{gen} | kW | rated capacity of the generator |

For more information

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3.11 How HOMER Creates the Generator Efficiency Curve



How HOMER Creates the Generator Efficiency Curve

On the Generator Inputs window, when you enter the fuel curve inputs HOMER draws the corresponding efficiency curve. This article explains how HOMER creates that graph from the fuel curve inputs.

Fuel units

You may have noticed that the units of the fuel curve inputs sometimes change when you select a different fuel from the drop-down box. That's because in HOMER, fuels can be denominated in units of kg, L, or m³. When you create a new fuel, you choose which units you want to use for that fuel. For example, you may choose to denote liquid fuels (e.g. diesel, gasoline, ethanol) in L, and gaseous fuels (e.g. natural gas, hydrogen) in m³. Once you have created a fuel, all the inputs that relate to that fuel will use the specified units. For example, if diesel fuel is denominated in L, then the price of diesel fuel will be in \$/L and the fuel curve inputs for a diesel generator will be in L/hr/kW. Similarly, if natural gas is denominated in m³ then its price will be in \$/m³ and the fuel curve inputs for a natural gas engine will be in m³/hr/kW. This article uses the term "units" to mean the units specified for the particular fuel, whether kg, L, or m³. For example, "units/hr" means L/hr for a fuel denominated in L, and kg/hr for a fuel denominated in kg.

Fuel curve

The fuel curve describes the amount of fuel the generator consumes to produce electricity. HOMER assumes that the fuel curve is a straight line. The following equation gives the generator's fuel consumption in units/hr as a function of its electrical output:

$$F = F_0 \cdot Y_{gen} + F_1 \cdot P_{gen}$$

where F_0 is the fuel curve intercept coefficient in units/hr/kW, F_1 is the fuel curve slope in units/hr/kW, Y_{gen} is the rated capacity of the generator in kW, and P_{gen} is the electrical output of the generator in kW.

Efficiency curve

In HOMER, we define the generator's electrical efficiency as the electrical energy coming out divided by the chemical energy of the fuel going in. The following equation gives this relationship:

$$\eta_{gen} = \frac{3.6 \cdot P_{gen}}{\dot{m}_{fuel} \cdot LHV_{fuel}}$$

where P_{gen} is the electrical output in kW, \dot{m}_{fuel} is the mass flow rate of the fuel in kg/hr and LHV_{fuel} is the lower heating value (a measure of energy content) of the fuel in MJ/kg. The factor of 3.6 arises because 1 kWh = 3.6 MJ.

The mass flow rate of the fuel is related to F , the generator's fuel consumption, but the exact relationship depends on the units of the fuel. If the fuel units are kg, then \dot{m}_{fuel} and F are equal, so the equation for \dot{m}_{fuel} is as follows:

$$\dot{m}_{fuel} = F = F_0 \cdot Y_{gen} + F_1 \cdot P_{gen}$$

If the fuel units are L, the relationship between \dot{m}_{fuel} and F involves the density. The equation for \dot{m}_{fuel} is as follows:

$$\dot{m}_{fuel} = \rho_{fuel} \left(\frac{F}{1000} \right) = \frac{\rho_{fuel} (F_0 \cdot Y_{gen} + F_1 \cdot P_{gen})}{1000}$$

where ρ_{fuel} is the fuel density in kg/m³. If the fuel units are m³ the factor of 1000 is unnecessary, and the equation for \dot{m}_{fuel} is as follows:

$$\dot{m}_{fuel} = \rho_{fuel} F = \rho_{fuel} (F_0 \cdot Y_{gen} + F_1 \cdot P_{gen})$$

Let us further develop the efficiency equation for the case where the fuel units are L. In this case, the efficiency equation becomes:

$$\eta_{gen} = \frac{3600 \cdot P_{gen}}{\rho_{fuel} (F_0 \cdot Y_{gen} + F_1 \cdot P_{gen}) \cdot LHV_{fuel}}$$

If we divide numerator and denominator by Y_{gen} , the capacity of the generator, and define a new symbol p_{gen} for the relative output of the generator ($p_{gen} = P_{gen}/Y_{gen}$) then the efficiency equation becomes:

$$\eta_{gen} = \frac{3600 \cdot p_{gen}}{\rho_{fuel}(F_0 + F_1 \cdot p_{gen}) \cdot LHV_{fuel}}$$

That equation gives the efficiency of the generator as a function of its relative output. It is this relation that HOMER plots in the efficiency curve on the Generator Inputs window when the fuel units are L.

If the fuel units are m3, the efficiency equation becomes:

$$\eta_{gen} = \frac{3.6 \cdot p_{gen}}{\rho_{fuel}(F_0 + F_1 \cdot p_{gen}) \cdot LHV_{fuel}}$$

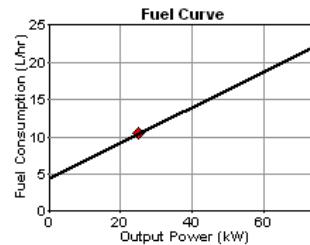
Finally, if the fuel units are kg, the efficiency equation becomes:

$$\eta_{gen} = \frac{3.6 \cdot p_{gen}}{(F_0 + F_1 \cdot p_{gen}) \cdot LHV_{fuel}}$$

Example

For an example, let's analyze a 75 kW generator that burns diesel. Assume diesel has a density of 820 kg/m³ and a lower heating value of 43.2 MJ/kg. If the generator consumes 22.5 L/hr at full load and 10.5 L/hr at 25 kW, what does its efficiency curve look like?

First we need to calculate the fuel curve slope and intercept coefficient. We assume (as we must in HOMER) that the fuel curve is a straight line passing through the two given points, as shown in the graph below.



Note that if we were given more than two points on this curve, we could calculate the line of best fit, using a linear regression technique for example. But since we are given only two points, we can directly calculate the slope and intercept of the line that passes through those points.

We can find the slope and intercept of that line as follows:

$$\text{slope} = \frac{22.5 \text{ L/hr} - 10.5 \text{ L/hr}}{75 \text{ kW} - 25 \text{ kW}} = 0.24 \text{ L/hr/kW}$$

$$\text{intercept} = 10.5 \text{ L/hr} - (25 \text{ kW})(0.24 \text{ L/hr/kW}) = 4.5 \text{ L/hr}$$

Note that HOMER's first fuel curve input is not the intercept itself, but rather the intercept coefficient, defined as the intercept divided by the rated capacity of the generator. (This is so that HOMER can apply the fuel curve inputs to each generator size that you specify in the Sizes to consider table.) So the two fuel curve inputs are:

$$F_0 = \frac{\text{intercept}}{\text{rated output}} = \frac{4.5 \text{ L/hr}}{75 \text{ kW}} = 0.06 \text{ L/hr/kW}$$

$$F_1 = \text{slope} = 0.24 \text{ L/hr/kW}$$

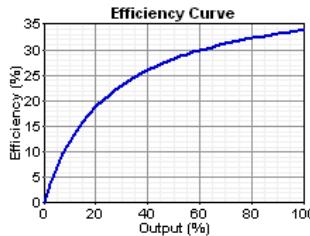
Since this is a liquid fuel denominated in L, the appropriate efficiency equation is:

$$\eta_{gen} = \frac{3600 \cdot p_{gen}}{\rho_{fuel}(F_0 + F_1 \cdot p_{gen}) \cdot LHV_{fuel}}$$

So we can substitute our values of density, lower heating value, and fuel curve as follows:

$$\eta_{gen} = \frac{3600 \cdot p_{gen}}{820(0.06 + 0.24 \cdot p_{gen}) \cdot 43.2}$$

Therefore the efficiency is 33.9% at full load ($p_{gen} = 1$), 28.2% at 50% load, 18.8% at 20% load, and 7.0% at 5% load. The efficiency curve is shown below:



For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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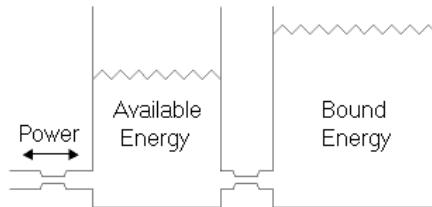
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3.12 Kinetic Battery Model



Kinetic Battery Model

HOMER uses the Kinetic Battery Model ([Manwell and McGowan, 1993](#)) to determine the amount of energy that can be absorbed by or withdrawn from the battery bank each time step. The kinetic battery model, so named because it is based on the concepts of electrochemical kinetics, models a battery as a two tank system. The first tank contains "available energy", or energy that is readily available for conversion to DC electricity. The second tank contains "bound energy", or energy that is chemically bound and therefore not immediately available for withdrawal. The following diagram illustrates the concept:



Three parameters are used to describe this two tank system. The maximum (or theoretical) battery capacity (Q_{max}) is the total amount of energy the two tanks can contain. The capacity ratio (c) is the ratio of the size of the available energy tank to the combined size of both tanks. The rate constant (k) relates to the conductance between the two tanks, and is therefore a measure of how quickly the battery can convert bound energy to available energy or vice-versa. HOMER determines these three parameters from the battery's capacity curve, which you specify in the [Create New Battery](#) window.

The total amount of energy stored in the battery at any time is the sum of the available and bound energy, hence:

$$Q = Q_1 + Q_2$$

where Q_1 is the available energy and Q_2 is the bound energy.

Using differential equations, one can show that the maximum amount of power that the battery can discharge over a specific length of time Dt is given by the following equation:

$$P_{batt,dmax,kbm} = \frac{-kcQ_{max} + kQ_1 e^{-k\Delta t} + Q_2 c(1 - e^{-k\Delta t})}{1 - e^{-k\Delta t} + c(k\Delta t - 1 + e^{-k\Delta t})}$$

Similarly, the maximum amount of power that the battery can absorb over a specific length of time is given by the following equation:

$$P_{batt,cmax,kbm} = \frac{kQ_1 e^{-k\Delta t} + Q_2 c(1 - e^{-k\Delta t})}{1 - e^{-k\Delta t} + c(k\Delta t - 1 + e^{-k\Delta t})}$$

The preceding two equations give the allowable range for the power into or out of the battery bank in any one time step. (HOMER imposes two additional limitations on the charge power. For more information please see the article on [calculating the maximum charge power](#). Once HOMER calculates the actual charge or discharge power, it calculates the resulting amount of available and bound energy at the end of the time step using the following two equations:

$$Q_{1,end} = Q_1 e^{-k\Delta t} + \frac{(Q_k c - P)(1 - e^{-k\Delta t})}{k} + \frac{P c (k\Delta t - 1 + e^{-k\Delta t})}{k}$$

$$Q_{2,end} = Q_2 e^{-k\Delta t} + Q(1 - c)(1 - e^{-k\Delta t}) + \frac{P(1 - c)(k\Delta t - 1 + e^{-k\Delta t})}{k}$$

where

- Q_1 is the available energy [kWh] at the beginning of the time step,
- Q_2 is the bound energy [kWh] at the beginning of the time step,
- $Q_{1,end}$ is the available energy [kWh] at the end of the time step,
- $Q_{2,end}$ is the bound energy [kWh] at the end of the time step,
- P is the power [kW] into (positive) or out of (negative) the battery bank, and
- Dt is the length of the time step [h].

See also

[Calculating maximum battery charge power](#)

[Calculating maximum battery discharge power](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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3.13 Generating Synthetic Load Data



Adding a Load to the Model

You can add electric or thermal load data using exactly the same process, described here. Measured load data is seldom available, so users often synthesize load data by specifying typical daily load profiles and then adding in some randomness. This process produces one year of hourly load data.

Electric Load Set Up

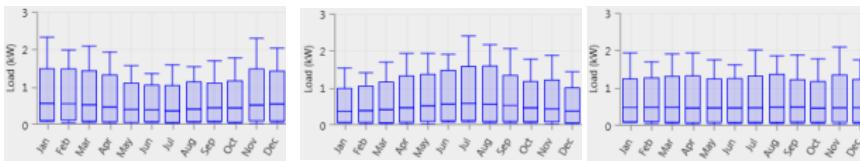
HOMER provides four methods to specify an electric load profile.

- **Create a synthetic load from a profile.**

This is a quick way to generate a load that can be relatively realistic. If you would like the load to have a cyclic annual variation, you can choose "January" or "July" as the peak month. Choosing "None" will yield an annual profile that is uniform except for random variation.



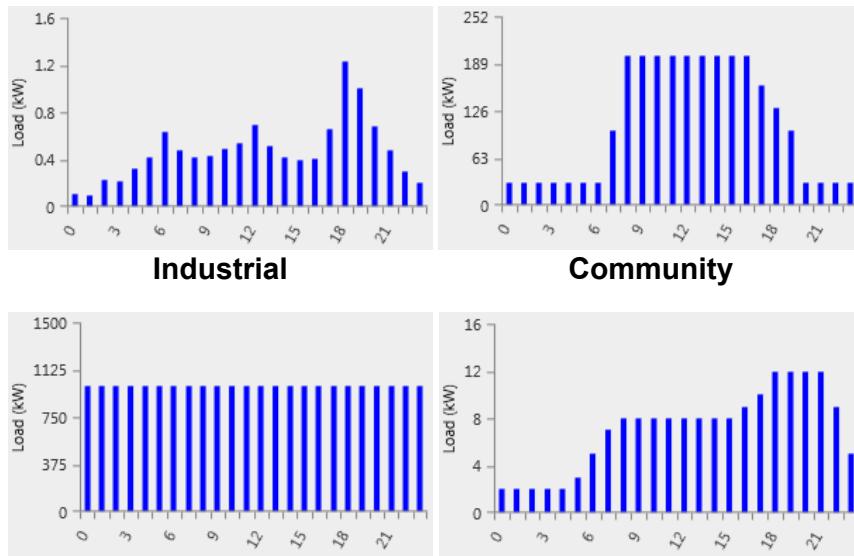
Peak Month: January Peak Month: July Peak Month: None



The drop-down menu contains a few pre-set load profiles: Residential, Commercial, Industrial, Community, and Blank. Blank is an empty template.

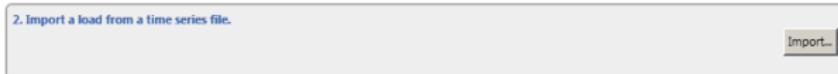
Residential

Commercial



These load templates all have different default overall magnitudes: 11.35, 2620, 24000, and 170 kWh/day respectively. You can easily scale the average load of any of them to fit your application by changing the value for "Scaled Annual Average (kWh/day)".

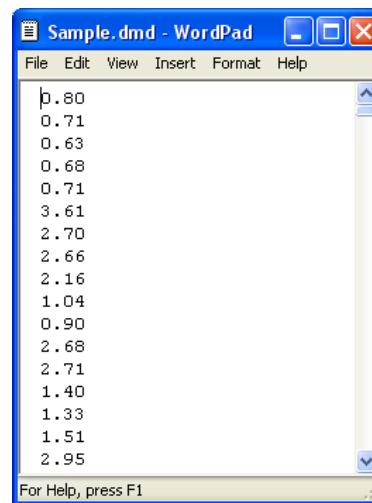
- Import a load from a time series file.



To import a file, you must prepare a text file that contains the electric load in each time step for a complete year.

Tip: You can import data with any time step down to one minute. HOMER detects the time step when you import the data file. For example, if the data file contains 8760 lines, HOMER will assume that it contains hourly data. If the data file contains 52,560 lines, HOMER will assume that it contains 10-minute data.

The data file must contain a single value on each line, where each line corresponds to one time step. Each value in the file represents the average load (in kW) for that time step. The first time step starts at midnight on January 1st. A sample input file appears below.



When you import data from a text file, HOMER makes a copy of the data set and integrates it with the HOMER (.hmr) file. Once the data is part of the HOMER file, HOMER no longer refers to the original text file. If you modify data in the original file, you must import the modified file in order for the modification to be included in the HOMER file. After you import a data file, HOMER calculates the average 24-hour load profile for the whole year displays it in the table and graph. HOMER also displays the name of the imported data file in the title of the load profile graph.

If you click Enter daily load profile(s) after importing data from a file, HOMER discards the data from the imported file and synthesizes new data based on the twelve monthly average load profiles it calculated from the imported data. You can edit synthesized data by selecting the month and changing values in the load profile table. To edit values from an imported file, you must edit the file directly and then import the modified file, as described above.

- Build a synthetic load using measured data.



You can import load data for specific devices as a CSV file with 24 hours of data, either in hourly or minute-resolution. Refer to the chart below for appropriate formatting. The first row and first two columns are ignored, reserved for user row titles if desired. The second row (column 3 and onward,

highlighted below in yellow) should contain descriptive names for each device. Row 3 through row 1442 (or row 3 through 26 for hourly data, below in orange) contains the load profile for each device in watts.

Note that HOMER will accept a mix of 1440-row and 24-row data columns in a single document. HOMER will infer the time step based on the number of rows of data for each column individually.

| | A | B | C | D | E | F | G | H |
|---|-----------------------|-----------|------|------|------|------|------|------|
| 1 | Time (min) | | 0 | 1 | 2 | 3 | 4 | |
| 2 | Coffee Pot | Coffee | 1 | 857 | 1 | 1.1 | 1 | 1.. |
| 3 | Microwave | Micro | 1 | 0.8 | 1.1 | 1 | 0.9 | 1.. |
| 4 | 24" TV | TV 24 | 54.2 | 55.8 | 53.2 | 54.9 | 55.1 | 53.. |
| 5 | 15" Laptop 2 | Laptop 15 | 15.2 | 16.1 | 15.8 | 35.8 | 31.5 | 15.. |
| 6 | Refrigerator | Refr | 0.2 | 0.3 | 0.1 | 0.2 | 65.6 | 66.. |
| 7 | Fan | Fan | 14.3 | 15.8 | 14.9 | 15.1 | 15.7 | 14.. |
| 8 | Single LED Light 9 W | | 10.1 | 9.5 | 9.1 | 9.2 | 10.1 | 8.. |
| 9 | Single CFL Light 14 W | | 11.5 | 12.5 | 11.5 | 12.0 | 12.5 | 11.. |

Select the "Open Equipment Database" button in the upper right corner of the Load Designer menu, choose "Open...", and select your csv file. The load designer will import each column in the file as a separate device. You can drag and drop rows from the Equipment Database popup into the Load Designer. Once you are done, close the Equipment Database popup. You can now edit the quantities of each item, if desired. You can also set the "Jitter", which offsets the load profiles randomly so that load peaks in the duplicate devices (if set to quantity greater than one) will not always line up exactly.

• Choose a load from the library.

Choose this option to retrieve load profiles from the [HOMER Library](#).

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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3.14 Generating Synthetic Solar Data



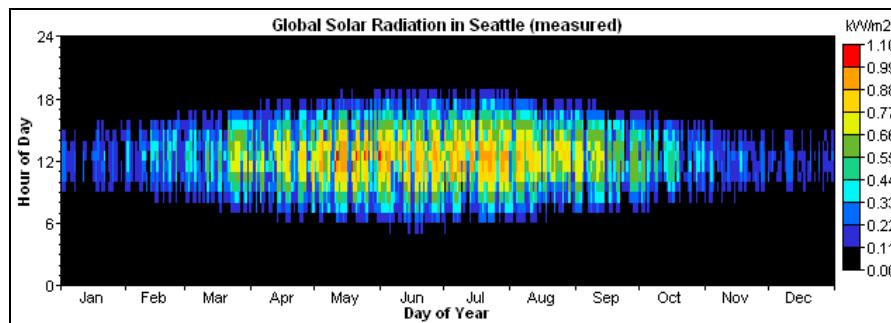
Generating Synthetic Solar Data

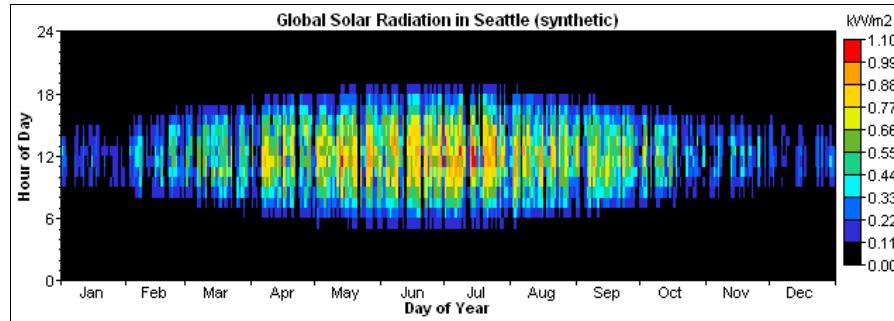
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-SCREENSHOTS

When you do not have access to measured solar radiation data, you can use HOMER's capability to generate synthetic hourly solar data from monthly average data. HOMER synthesizes hourly solar radiation data using an algorithm based on the work of [V.A. Graham](#). We have found this algorithm to produce realistic hourly data, and it is easy to use because it requires only the latitude and the twelve monthly average values.

The realistic nature of synthetic data created by this algorithm is demonstrated in the two [DMaps](#) below. The first shows the measured TMY2 solar data for Seattle, WA. The second shows the synthetic data created by specifying Seattle's latitude and monthly average radiation values. The synthetic data display realistic day-to-day and hour-to-hour patterns. If one hour is cloudy, there is a relatively high likelihood that the next hour will also be cloudy. Similarly, one cloudy day is likely to be followed by another cloudy day.





The algorithm creates synthetic solar data with certain statistical properties that reflect global averages. So data generated for a particular location will not perfectly replicate the characteristics of the real solar resource. But our tests show that synthetic solar data produce virtually the same simulation results as real data. Differences in key performance output variables like annual PV array production, fuel consumption, generator run time, and [battery throughput](#) are typically less than 5%. Differences in key economic output variables like [total net present cost](#) and [levelized cost of energy](#) are typically less than 2%.

To generate synthetic solar data, go to the Solar Resource window. For each month enter either the average [clearness index](#) or the average daily radiation. If you enter the clearness index, HOMER will calculate the average daily radiation, and vice versa, using the latitude. For details, see the [article on how HOMER calculates clearness index](#).

For assistance in finding monthly solar data, see [Finding data to run HOMER](#)

See also

[How HOMER calculates clearness index](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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3.15 Generating Synthetic Wind Data



Generating Synthetic Wind Data

When you have no access to measured wind speed data, you can create time series wind speed data using HOMER's synthetic wind speed synthesis algorithm. This algorithm requires you to enter a few parameters, from which it generates artificial but statistically reasonable time series data. The algorithm produces data that mimic the characteristics of real wind speed data, including strong and sustained gusts, long lulls between windy periods, and seasonal and diurnal patterns.

Tip: When you import measured wind speed data, it can have any time step down to one minute. Similarly, when you generate synthetic wind data, it can have any time step down to one minute.

Parameters

To generate synthetic wind speed data, go to the Wind Resources Inputs window and choose Enter monthly averages. You must enter the twelve monthly average wind speeds, as well as the following four parameters:

| Parameter | Description |
|---|--|
| Weibull k | Reflects the breadth of the distribution of wind speeds over the year. |
| 1-hour autocorrelation factor | Reflects how strongly the wind speed in one time step tends to depend on the wind speed in the previous time step. |
| Diurnal pattern strength | Reflects how strongly the wind speed depends on the time of day. |
| Hour of peak wind speed | The hour of day that tends to be windiest on average. |

One can estimate the value of each of these parameters without detailed knowledge of the wind data in a particular location. The articles on each of the parameters give guidance for doing so.

Algorithm

HOMER follows a five-step process to synthesize one year of time series wind speed data:

Step 1

In the first step of the algorithm, HOMER generates a sequence of autocorrelated numbers, one for each time step of the year, using the first-order autoregressive model:

$$z_t = a \cdot z_{t-1} + f(t)$$

where:

z_t = the value in time step i

z_{t-1} = the value in time step i-1

a = the autoregressive parameter

$f(t)$ = a 'white noise' function that returns a random number drawn from a normal distribution with mean of zero and a standard deviation of 1

HOMER sets the autoregressive parameter equal to the one-time-step autocorrelation coefficient:

$$a = r_1$$

But on the Wind Resource Inputs window you enter the *one-hour autocorrelation coefficient*, which is different from the one-time-step autocorrelation coefficient if the time step is not 60 minutes.

To calculate the one-time-step autocorrelation coefficient from the one-hour autocorrelation factor, HOMER assumes logarithmic decay in the autocorrelation function, in which case the following equation gives the autocorrelation parameter for a lag of k time steps:

$$r_k = r_1^k$$

Solving that for r_1 gives:

$$r_1 = \exp\left[\frac{\ln(r_k)}{k}\right]$$

The one-hour autocorrelation factor is r_k where k is the number of time steps that fit in one hour, meaning:

$$k = \frac{60}{t}$$

Where t is the time step in minutes.

This first step of the algorithm produces a series of numbers that conform to a normal distribution with a mean of zero and a standard deviation of 1.

Step 2

In the second step of the algorithm, HOMER creates a full year of data by piecing together the desired average diurnal wind speed profile, repeated every day. Because the average wind speed varies by month, the average diurnal wind speed profile scales to a different value each month, but within each month the diurnal pattern simply repeats over and over.

Step 3

In the third step, HOMER performs a probability transformation on the sequence of numbers generated in Step 2 so that it conforms to the same normal distribution as the sequence generated in Step 1.

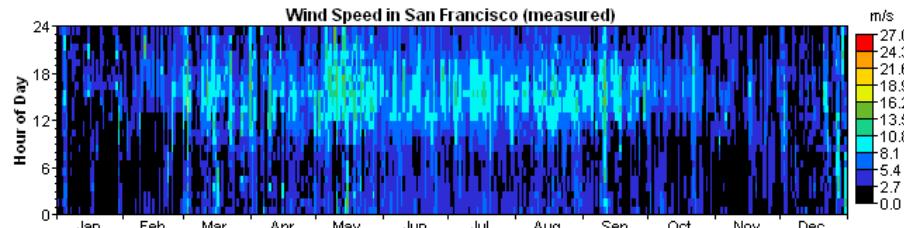
Step 4

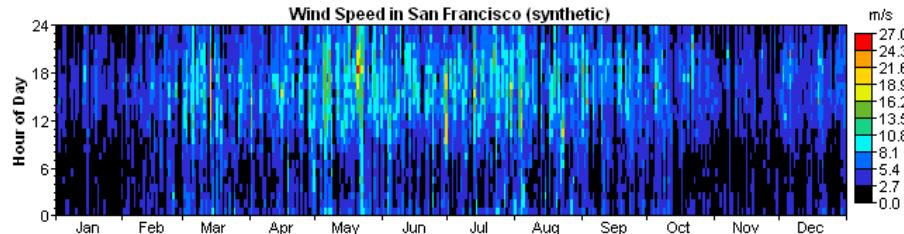
In the fourth step, HOMER adds the sequence generated in Step 3 to the sequence generated in Step 1. The resulting sequence conforms to a normal distribution, but exhibits the desired degree of autocorrelation.

Step 5

In the fifth and final step, HOMER performs a probability transformation on the sequence generated in Step 4 to make it conform to the desired Weibull distribution.

The two [DMaps](#) below demonstrate the results of the synthetic wind data generation algorithm. The first shows the measured wind speed data for San Francisco, California from the TMY2 data set. The second shows the synthetic wind speed data that HOMER generated from the monthly average wind speeds and the four wind data parameters measured from the real data:





For assistance in finding wind data, see [Finding data to run HOMER](#)

See also

[Generating synthetic solar data](#)

[Generating synthetic load data](#)

[Finding data to run HOMER](#)

[Probability transformation](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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3.16 Unit Conversions



Unit Conversions

If we are missing a factor you need, please let us know by writing to support@homerenergy.com. A good online unit conversion website is www.onlineconversion.com.

Energy

- 1 kWh = 3,600,000 J
- 1 kWh = 3.6 MJ
- 1 kWh = 3,412.14 Btu
- 1 kWh = 0.0341296 therm [US]

Length

- 1 m = 1000 mm
- 1 m = 3.28084 ft
- 1 ft = 0.3048 m

Speed

- 1 m/s = 3.6 km/hr
- 1 m/s = 2.23694 mph
- 1 m/s = 1.94385 knot
- 1 mph = 0.44704 m/s
- 1 knot = 0.514444 m/s

Volume

- 1 m³ = 1000 L
- 1 ft³ = 0.0283168 m³
- 1 gallon [US, liquid] = 3.78541 L
- 1 barrel [US, petroleum] = 158.987 L

Flow Rate

- $1 \text{ m}^3/\text{s} = 1000 \text{ L/s}$
- $1 \text{ ft}^3/\text{min}$ [or cfm] = 0.4719475 L/s
- $1 \text{ ft}^3/\text{s}$ [or cfs] = 28.316847 L/s
- 1 gallon/min [US] = 0.0630902 L/s

Weight/Mass

- $1 \text{ kg} = 1000 \text{ g}$
- 1 t [tonne] = $1,000 \text{ kg}$
- $1 \text{ kg} = 2.20462 \text{ lb}$
- $1 \text{ lb} = 0.453592 \text{ kg}$
- 1 ton [short] = 907.185 kg
- 1 ton [long] = $1,016.05 \text{ kg}$

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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4. Finding data to run HOMER



Finding Data to Run HOMER

One of the biggest challenges in using a model like HOMER is finding the numbers to put into it. This page is meant to help you find the information you need. If you know of any other helpful sources, **please let us know** so we can add them. Note that NREL cannot guarantee the accuracy of any data from external sources, and does not endorse any manufacturer or retailer.

Electric Load Data

The only source of hourly load data that we're aware of is the DG Marketplace, which you can visit at www.dgmarketplace.com. This website sells typical residential, commercial, and industrial load data for locations across the US.

Geography

To find your latitude and longitude, check maps.google.com. For help with Google Maps, see this Google Support article about latitude and longitude: [Latitude and longitude coordinates](#).

To find your time zone, check www.worldtimezone.com.

Solar Radiation Data

HOMER will accept solar radiation data as monthly averages or as a time series. Time series solar radiation data is most commonly available with an hourly time step, but HOMER can accept any time step down to one minute. One of the best sources of solar radiation data is the TMY2 and TMY3 data sets provided for free by the US National Renewable Energy Laboratory. You can import TMY2 and TMY3 files directly into HOMER's Solar Resource Inputs window.

- NREL provides TMY2 data at: http://rredc.nrel.gov/solar/old_data/nsrdb/1961-1990/tmy2/.
- And TMY3 data at: http://rredc.nrel.gov/solar/old_data/nsrdb/1991-2005/tmy3/.
- NASA's Surface Solar Energy Data Set provides monthly average solar radiation data for everywhere on earth at <http://eosweb.larc.nasa.gov/sse/>. This help file contains a [table of monthly solar data](#) for selected worldwide locations.
- The US Renewable Resource Data Center provides US data and maps at www.nrel.gov/rredc/solar_resource.html.
- The World Radiation Data Center provides worldwide solar data at <http://wrdc-mgo.nrel.gov>. Note that data from this website need a lot of processing to be useful in HOMER.
- GeoModel Solar has many solar data sets available at various resolutions: <http://solargis.info>.

Wind Speed Data

It can be difficult to obtain measured wind speed data. Proper measurement of wind speed is expensive and time consuming, and average wind speeds can vary markedly over short distances because of terrain effects. For these reasons, it is often necessary to [synthesize](#) wind data from estimated monthly average wind speeds.

Many countries have published wind atlases:

- Wind maps for many US states are available at apps2.eere.energy.gov/wind/windexchange/windmaps/.

- The Canadian Wind Atlas is available at www.windatlas.ca.
- The Brazilian Wind Atlas is available at www.cresesb.cepel.br/publicacoes/index.php?task=livro&cid=1.

A number of other websites provide wind speed data:

- The US Renewable Resource Data Center provides information on wind data at http://www.nrel.gov/rredc/wind_resource.html.
- The website www.weatherbase.com provides monthly average wind speed data for many cities around the world.
- The [Windustry](http://www.windustry.com/resources/windmaps.htm) website maintains a list of US wind data resources at www.windustry.com/resources/windmaps.htm.
- The US National Climatic Data Center provides monthly average wind speed data for many US cities at <http://www1.ncdc.noaa.gov/pub/data/ccd-data/wndspd12.txt>. To convert from mph to m/s, divide by 2.23694.
- The Technical University of Denmark maintains a database of wind characteristics at www.winddata.com.

Renewable Power System Components

Several retailers sell components for renewable power systems. The website www.ecobusinesslinks.com maintains a list of renewable power retailers around the world. A few have very helpful websites providing cost and performance data for PV panels, wind turbines, hydro turbines, batteries, converters, and other system components. Check out:

- The Alternative Energy Store at www.altenergystore.com
- SolarEnergy.com at www.solarenergy.com
- The Solar Biz at www.thesolarbiz.com
- The Energy Development Co-operative at www.unlimited-power.co.uk

Other sources of cost and performance data for renewable power system components include:

- The Renewable Energy Technology Characterizations, a detailed report on the performance and costs of solar, wind, and biomass power systems, available at http://www1.eere.energy.gov/pba/pdfs/entire_document.pdf. This report includes predictions of future performance and costs out to the year 2030.
- SolarBuzz, which provides price data for PV modules, inverters, batteries, and charge controllers at www.solarbuzz.com.
- The EPA provides a prices and references for renewable technologies at <http://www.epa.gov/cleanenergy/energy-resources/renewabledatabase.html>.

Generators

- A very useful document covering the technology, emissions, and costs of natural gas-fired reciprocating generators, microturbines, fuel cells, and Stirling engines is the Gas-Fired Distributed Energy Resource Technology Characterizations, available at <http://www.nrel.gov/docs/fy04osti/34783.pdf>.

PV

- PV WATTS v.1 is a simple and useful tool for estimating a PV derating factor. <http://rredc.nrel.gov/solar/calculators/pvwatts/version1/derate.cgi>.

Emissions

- This help file contains a [table of US grid emissions factors](#).

The US Environmental Protection Agency provides emissions coefficients for CO₂, SO₂, and NO_x for US locations at their Power Profiler website at http://oaspub.epa.gov/powpro/ept_pack.charts.

The EPA's [eGRID](#) website contains even more emissions data, including state-by-state average emissions factors for all the pollutants that HOMER models.

- Additional data is available The EPA document Emissions Factors, Global Warming Potentials, Unit Conversions, Emissions, and Related Facts, November 1999, at www.epa.gov/appdstar/pdf/brochure.pdf.

Policies and Incentives

- For information on current net metering policies across the United States, see the US Department of Energy web page on the topic at www.eere.energy.gov/greenpower/markets/netmetering.shtml
- For a list of renewable energy incentives across the United States, see the Database of State Incentives for Renewable Energy at www.dsireusa.org.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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4.1 US Grid Emissions Factors



US Grid Emissions Factors

The following table contains the *average* emissions factors for the year 2000 for each US state. Source: [eGRID](#).

| State | Average grid emissions factors | | |
|----------------------|--------------------------------|--------------------------|--------------------------|
| | CO ₂ g/kWh | SO ₂ g/kWh | NO _x g/kWh |
| Alabama | 656 | 3.76 | 1.38 |
| Alaska | 586 | 0.61 | 2.21 |
| Arizona | 533 | 0.74 | 1.06 |
| Arkansas | 659 | 1.57 | 1.10 |
| California | 287 | 0.08 | 0.26 |
| Colorado | 913 | 1.85 | 1.59 |
| Connecticut | 335 | 1.02 | 0.62 |
| Delaware | 894 | 5.93 | 1.59 |
| District of Columbia | 1205 | 6.18 | 2.36 |
| Florida | 644 | 2.74 | 1.53 |
| Georgia | 641 | 3.87 | 1.43 |
| Hawaii | 779 | 2.08 | 2.38 |
| Idaho | 42 | 0.04 | 0.07 |
| Illinois | 503 | 2.24 | 1.23 |
| Indiana | 977 | 6.01 | 2.37 |
| Iowa | 894 | 3.13 | 1.84 |
| Kansas | 848 | 2.36 | 1.93 |
| Kentucky | 1011 | 5.70 | 2.41 |
| Louisiana | 629 | 1.60 | 1.15 |
| Maine | 297 | 0.96 | 0.65 |
| Maryland | 623 | 4.58 | 1.58 |
| Massachusetts | 587 | 2.53 | 0.91 |
| Michigan | 710 | 3.20 | 1.52 |
| Minnesota | 744 | 2.26 | 1.78 |
| Mississippi | 597 | 3.20 | 1.55 |
| Missouri | 898 | 2.79 | 1.96 |
| Montana | 662 | 0.79 | 1.29 |
| Nebraska | 702 | 1.95 | 1.42 |
| Nevada | 704 | 1.35 | 1.34 |
| New Hampshire | 321 | 3.12 | 0.64 |
| New Jersey | 332 | 0.96 | 0.62 |
| New Mexico | 969 | 1.83 | 2.32 |
| New York | 444 | 1.88 | 0.66 |
| North Carolina | 586 | 3.45 | 1.33 |
| North Dakota | 1086 | 4.41 | 2.27 |
| Ohio | 836 | 7.50 | 2.33 |
| Oklahoma | 833 | 1.57 | 1.66 |
| Oregon | 149 | 0.26 | 0.25 |
| Pennsylvania | 560 | 4.32 | 1.23 |
| Rhode Island | 454 | 0.09 | 0.24 |
| South Carolina | 405 | 2.00 | 0.89 |
| South Dakota | 378 | 1.25 | 1.61 |
| Tennessee | 621 | 3.96 | 1.51 |
| Texas | 666 | 1.38 | 1.05 |
| Utah | 950 | 0.71 | 2.01 |
| Vermont | 26 | 0.02 | 0.14 |
| Virginia | 559 | 2.64 | 1.17 |
| Washington | 130 | 0.72 | 0.25 |
| West Virginia | 920 | 5.84 | 2.62 |
| Wisconsin | 799 | 3.01 | 1.70 |
| Wyoming | 1044 | 1.69 | 1.84 |
| US average | 632 | 2.74 | 1.34 |

The following table contains the average *marginal* CO₂ emissions factors for grid electricity in the US in the year 2000. Source: EPA document "Emissions Factors, Global Warming Potentials, Unit Conversions, Emissions, and Related Facts, November 1999"

| EPA | Marginal CO ₂ emissions |
|-----|---------------------------------------|
|-----|---------------------------------------|

| region | States within region | factor g/kWh |
|-------------------|--------------------------------|-----------------|
| Region 1 | MA, CT, ME, NH, RI, VT | 783 |
| Region 2 | NY, NJ | 762 |
| Region 3 | PA, VA, MD, WV, DC, DE | 951 |
| Region 4 | FL, NC, GA, TN, AL, SC, KY, MS | 1005 |
| Region 5 | OH, IL, MI, IN, WI, MN | 902 |
| Region 6 | TX, LA, OK, AR, NM | 538 |
| Region 7 | MO, IA, KS, NE | 637 |
| Region 8 | CO, UT, MT, WY, ND, SD | 564 |
| Region 9 | CA, AZ, NV | 562 |
| Region 10 | WA, OR, ID | 545 |
| US average | | 744 |

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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4.2 Published Solar Data



Published Solar Data

The following tables show the monthly average [clearness index](#) for various locations around the world. The data for U.S. sites were calculated from the TMY2 data set. Data for all other locations were taken from [Duffie & Beckmann](#).

Africa

| Location | Latitude | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|------------------------|----------|------|------|------|------|------|------|------|------|------|------|------|------|
| Luanda, Angola | S8.8 | 0.52 | 0.53 | 0.52 | 0.53 | 0.55 | 0.49 | 0.42 | 0.38 | 0.43 | 0.47 | 0.52 | 0.50 |
| Cairo, Egypt | N30.0 | 0.56 | 0.60 | 0.61 | 0.63 | 0.66 | 0.68 | 0.67 | 0.66 | 0.66 | 0.65 | 0.59 | 0.56 |
| Addis Ababa, Ethiopia | N9.0 | 0.59 | 0.60 | 0.57 | 0.54 | 0.52 | 0.45 | 0.37 | 0.38 | 0.46 | 0.61 | 0.68 | 0.64 |
| Nairobi, Kenya | S1.3 | 0.63 | 0.62 | 0.59 | 0.52 | 0.49 | 0.46 | 0.39 | 0.40 | 0.51 | 0.54 | 0.52 | 0.61 |
| Casablanca, Morocco | N33.6 | 0.51 | 0.54 | 0.56 | 0.58 | 0.58 | 0.59 | 0.61 | 0.61 | 0.61 | 0.56 | 0.54 | 0.48 |
| Benin City, Nigeria | N6.1 | 0.46 | 0.47 | 0.46 | 0.46 | 0.47 | 0.43 | 0.36 | 0.34 | 0.37 | 0.44 | 0.51 | 0.48 |
| Dakar, Senegal | N14.7 | 0.62 | 0.67 | 0.68 | 0.67 | 0.65 | 0.60 | 0.53 | 0.50 | 0.52 | 0.60 | 0.60 | 0.59 |
| Pretoria, South Africa | S25.8 | 0.55 | 0.56 | 0.57 | 0.57 | 0.65 | 0.67 | 0.69 | 0.67 | 0.63 | 0.57 | 0.57 | 0.57 |
| El Fasher, Sudan | N13.6 | 0.68 | 0.70 | 0.70 | 0.68 | 0.67 | 0.64 | 0.61 | 0.61 | 0.64 | 0.67 | 0.70 | 0.70 |
| Sidi-Dou-Said, Tunisia | N6.9 | 0.51 | 0.51 | 0.55 | 0.55 | 0.60 | 0.63 | 0.66 | 0.64 | 0.61 | 0.59 | 0.58 | 0.53 |
| Entebbe, Uganda | N0.1 | 0.50 | 0.48 | 0.48 | 0.47 | 0.47 | 0.48 | 0.46 | 0.46 | 0.48 | 0.48 | 0.48 | 0.49 |

Asia

| Location | Latitude | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|------------------------|----------|------|------|------|------|------|------|------|------|------|------|------|------|
| Madras, India | N13.0 | 0.60 | 0.66 | 0.66 | 0.65 | 0.59 | 0.53 | 0.52 | 0.53 | 0.54 | 0.49 | 0.50 | 0.48 |
| New Delhi, India | N28.6 | 0.51 | 0.52 | 0.50 | 0.54 | 0.53 | 0.46 | 0.45 | 0.44 | 0.53 | 0.55 | 0.54 | 0.51 |
| Akita, Japan | N39.7 | 0.30 | 0.35 | 0.41 | 0.42 | 0.43 | 0.41 | 0.43 | 0.44 | 0.43 | 0.44 | 0.33 | 0.27 |
| Kagoshima, Japan | N31.6 | 0.42 | 0.40 | 0.41 | 0.39 | 0.38 | 0.36 | 0.42 | 0.47 | 0.42 | 0.46 | 0.44 | 0.43 |
| Shimizu, Japan | N32.7 | 0.48 | 0.45 | 0.46 | 0.41 | 0.41 | 0.38 | 0.47 | 0.49 | 0.44 | 0.46 | 0.48 | 0.49 |
| Kuala Lumpur, Malaysia | N3.1 | 0.51 | 0.52 | 0.52 | 0.50 | 0.50 | 0.48 | 0.49 | 0.48 | 0.46 | 0.50 | 0.44 | 0.49 |
| Karachi, Pakistan | N24.8 | 0.67 | 0.66 | 0.63 | 0.61 | 0.60 | 0.58 | 0.50 | 0.49 | 0.60 | 0.66 | 0.68 | 0.67 |
| Lahore, Pakistan | N31.5 | 0.49 | 0.55 | 0.58 | 0.56 | 0.57 | 0.54 | 0.49 | 0.50 | 0.56 | 0.58 | 0.57 | 0.53 |
| Singapore, Singapore | N1.0 | 0.47 | 0.47 | 0.47 | 0.45 | 0.44 | 0.45 | 0.45 | 0.44 | 0.44 | 0.42 | 0.39 | 0.41 |
| Colombo, Sri Lanka | N6.9 | 0.35 | 0.49 | 0.53 | 0.52 | 0.49 | 0.47 | 0.44 | 0.43 | 0.43 | 0.45 | 0.35 | 0.52 |

Bangkok, Thailand

N13.7 0.55 0.52 0.54 0.51 0.47 0.45 0.42 0.42 0.42 0.48 0.56 0.56

Canada

| Location | Latitude | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|---------------------|----------|------|------|------|------|------|------|------|------|------|------|------|------|
| Beaverlodge, AB | N55.2 | 0.48 | 0.55 | 0.62 | 0.59 | 0.53 | 0.54 | 0.54 | 0.53 | 0.49 | 0.48 | 0.47 | 0.44 |
| Edmonton, AB | N53.6 | 0.54 | 0.57 | 0.61 | 0.58 | 0.55 | 0.54 | 0.59 | 0.55 | 0.55 | 0.54 | 0.51 | 0.49 |
| Suffield, AB | N50.3 | 0.55 | 0.59 | 0.62 | 0.57 | 0.56 | 0.57 | 0.62 | 0.60 | 0.57 | 0.56 | 0.35 | 0.49 |
| Cape St. James, BC | N51.9 | 0.34 | 0.39 | 0.44 | 0.47 | 0.51 | 0.49 | 0.48 | 0.50 | 0.49 | 0.42 | 0.36 | 0.31 |
| Fort Nelson, BC | N58.8 | 0.43 | 0.50 | 0.56 | 0.58 | 0.52 | 0.50 | 0.50 | 0.50 | 0.48 | 0.46 | 0.39 | 0.38 |
| Nanaimo, BC | N49.2 | 0.31 | 0.39 | 0.46 | 0.50 | 0.54 | 0.53 | 0.59 | 0.57 | 0.52 | 0.45 | 0.34 | 0.28 |
| Port Hardy, BC | N50.7 | 0.33 | 0.38 | 0.40 | 0.43 | 0.46 | 0.46 | 0.48 | 0.45 | 0.43 | 0.38 | 0.31 | 0.28 |
| Prince George, BC | N53.9 | 0.40 | 0.43 | 0.50 | 0.53 | 0.48 | 0.52 | 0.53 | 0.52 | 0.47 | 0.42 | 0.38 | 0.32 |
| Sandspit, BC | N53.3 | 0.33 | 0.39 | 0.45 | 0.46 | 0.48 | 0.44 | 0.43 | 0.46 | 0.44 | 0.39 | 0.35 | 0.30 |
| Summerland, BC | N49.6 | 0.37 | 0.44 | 0.51 | 0.53 | 0.54 | 0.54 | 0.59 | 0.57 | 0.56 | 0.49 | 0.36 | 0.31 |
| Vancouver, BC | N49.3 | 0.31 | 0.37 | 0.44 | 0.48 | 0.52 | 0.52 | 0.57 | 0.54 | 0.51 | 0.43 | 0.33 | 0.28 |
| Churchill, MB | N58.8 | 0.56 | 0.63 | 0.70 | 0.67 | 0.54 | 0.53 | 0.52 | 0.49 | 0.41 | 0.36 | 0.45 | 0.51 |
| The Pas, MB | N54.0 | 0.51 | 0.58 | 0.62 | 0.61 | 0.55 | 0.52 | 0.52 | 0.50 | 0.46 | 0.42 | 0.41 | 0.45 |
| Winnipeg, MB | N49.9 | 0.57 | 0.62 | 0.62 | 0.56 | 0.54 | 0.55 | 0.57 | 0.55 | 0.52 | 0.48 | 0.44 | 0.49 |
| Fredericton, NB | N45.9 | 0.47 | 0.52 | 0.50 | 0.47 | 0.46 | 0.48 | 0.49 | 0.49 | 0.48 | 0.44 | 0.39 | 0.41 |
| St. John's West, NF | N47.5 | 0.39 | 0.44 | 0.44 | 0.42 | 0.43 | 0.47 | 0.50 | 0.45 | 0.45 | 0.37 | 0.35 | 0.33 |
| Halifax Citadel, NS | N44.7 | 0.41 | 0.46 | 0.48 | 0.44 | 0.44 | 0.48 | 0.47 | 0.35 | 0.35 | 0.45 | 0.39 | 0.35 |
| Kentville, NS | N45.1 | 0.41 | 0.48 | 0.50 | 0.46 | 0.48 | 0.51 | 0.51 | 0.52 | 0.51 | 0.46 | 0.38 | 0.35 |
| Sable Island, NS | N43.9 | 0.33 | 0.38 | 0.45 | 0.46 | 0.49 | 0.49 | 0.51 | 0.50 | 0.50 | 0.43 | 0.35 | 0.31 |
| Inuvik, NT | N68.3 | 0.70 | 0.55 | 0.63 | 0.65 | 0.58 | 0.53 | 0.49 | 0.43 | 0.40 | 0.41 | 0.56 | 0.00 |
| Mould Bay, NT | N76.2 | 0.00 | 0.00 | 0.58 | 0.66 | 0.63 | 0.52 | 0.43 | 0.37 | 0.43 | 0.52 | 0.00 | 0.00 |
| Norman Wells, NT | N65.3 | 0.43 | 0.52 | 0.61 | 0.61 | 0.56 | 0.56 | 0.53 | 0.35 | 0.46 | 0.37 | 0.44 | 0.60 |
| Sachs Harbour, NT | N72.0 | 0.00 | 0.64 | 0.68 | 0.67 | 0.61 | 0.53 | 0.51 | 0.43 | 0.40 | 0.45 | 0.00 | 0.00 |
| Alert, NU | N82.5 | 0.00 | 0.00 | 0.60 | 0.61 | 0.61 | 0.55 | 0.46 | 0.41 | 0.48 | 0.00 | 0.00 | 0.00 |
| Baker Lake, NU | N64.3 | 0.53 | 0.58 | 0.72 | 0.69 | 0.62 | 0.53 | 0.51 | 0.47 | 0.42 | 0.43 | 0.53 | 0.56 |
| Cambridge Bay, NU | N69.1 | 0.00 | 0.58 | 0.66 | 0.68 | 0.62 | 0.55 | 0.48 | 0.43 | 0.40 | 0.53 | 0.73 | 0.00 |
| Coral Harbour, NU | N64.2 | 0.51 | 0.61 | 0.68 | 0.70 | 0.65 | 0.56 | 0.47 | 0.47 | 0.44 | 0.48 | 0.52 | 0.60 |
| Eureka, NU | N80.0 | 0.00 | 0.00 | 0.59 | 0.61 | 0.63 | 0.56 | 0.46 | 0.40 | 0.46 | 0.00 | 0.00 | 0.00 |
| Hall Beach, NU | N68.8 | 0.00 | 0.60 | 0.66 | 0.69 | 0.62 | 0.57 | 0.49 | 0.47 | 0.39 | 0.48 | 0.69 | 0.00 |
| Iqaluit, NU | N63.8 | 0.50 | 0.58 | 0.63 | 0.68 | 0.59 | 0.48 | 0.43 | 0.43 | 0.40 | 0.39 | 0.44 | 0.53 |
| Isachsen, NU | N78.8 | 0.00 | 0.00 | 0.59 | 0.61 | 0.61 | 0.53 | 0.42 | 0.35 | 0.43 | 0.59 | 0.00 | 0.00 |
| Resolute, NU | N74.7 | 0.00 | 0.79 | 0.66 | 0.70 | 0.64 | 0.58 | 0.47 | 0.42 | 0.43 | 0.54 | 0.00 | 0.00 |
| Big Trout Lake, ON | N53.8 | 0.57 | 0.63 | 0.64 | 0.63 | 0.53 | 0.47 | 0.51 | 0.46 | 0.41 | 0.39 | 0.41 | 0.50 |
| Guelph, ON | N43.5 | 0.46 | 0.55 | 0.52 | 0.49 | 0.51 | 0.54 | 0.54 | 0.53 | 0.49 | 0.45 | 0.34 | 0.39 |
| Kapuskasing, ON | N49.4 | 0.48 | 0.57 | 0.61 | 0.54 | 0.51 | 0.56 | 0.52 | 0.47 | 0.46 | 0.40 | 0.38 | 0.45 |
| Moosonee, ON | N51.3 | 0.50 | 0.59 | 0.58 | 0.54 | 0.47 | 0.48 | 0.47 | 0.45 | 0.42 | 0.37 | 0.35 | 0.44 |
| Ottawa, ON | N45.5 | 0.48 | 0.54 | 0.55 | 0.51 | 0.51 | 0.53 | 0.51 | 0.48 | 0.44 | 0.36 | 0.41 | 0.41 |
| Toronto, ON | N43.7 | 0.40 | 0.45 | 0.47 | 0.48 | 0.35 | 0.53 | 0.54 | 0.52 | 0.49 | 0.45 | 0.34 | 0.34 |
| Charlottetown, PE | N46.3 | 0.47 | 0.53 | 0.52 | 0.48 | 0.48 | 0.35 | 0.35 | 0.47 | 0.41 | 0.39 | 0.38 | 0.38 |
| Fort Chimo, PQ | N58.1 | 0.52 | 0.58 | 0.67 | 0.65 | 0.48 | 0.45 | 0.42 | 0.43 | 0.42 | 0.37 | 0.41 | 0.44 |
| Inoucdjouac, PQ | N58.5 | 0.57 | 0.64 | 0.73 | 0.70 | 0.55 | 0.51 | 0.46 | 0.44 | 0.45 | 0.36 | 0.33 | 0.45 |
| Montreal, PQ | N45.5 | 0.45 | 0.51 | 0.35 | 0.48 | 0.49 | 0.49 | 0.52 | 0.49 | 0.49 | 0.41 | 0.35 | 0.38 |
| Nitchequon, PQ | N53.2 | 0.52 | 0.62 | 0.63 | 0.62 | 0.52 | 0.46 | 0.43 | 0.43 | 0.39 | 0.35 | 0.39 | 0.46 |
| Normandin, PQ | N48.8 | 0.52 | 0.60 | 0.62 | 0.56 | 0.49 | 0.49 | 0.48 | 0.49 | 0.44 | 0.38 | 0.39 | 0.47 |
| Sept-Iles, PQ | N50.2 | 0.48 | 0.56 | 0.53 | 0.47 | 0.48 | 0.50 | 0.46 | 0.50 | 0.46 | 0.43 | 0.40 | 0.42 |
| Bad Lake, SK | N51.3 | 0.60 | 0.62 | 0.64 | 0.58 | 0.57 | 0.57 | 0.59 | 0.57 | 0.56 | 0.56 | 0.52 | 0.51 |
| Swift Current, SK | N50.3 | 0.57 | 0.60 | 0.63 | 0.57 | 0.56 | 0.56 | 0.61 | 0.59 | 0.56 | 0.56 | 0.52 | 0.51 |
| Whitehorse, YT | N60.7 | 0.42 | 0.35 | 0.56 | 0.58 | 0.54 | 0.51 | 0.48 | 0.49 | 0.45 | 0.42 | 0.39 | 0.37 |

Europe

| Location | Latitude | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----------------------|----------|------|------|------|------|------|------|------|------|------|------|------|------|
| Brussels, Belgium | N35.8 | 0.27 | 0.32 | 0.36 | 0.40 | 0.43 | 0.43 | 0.42 | 0.43 | 0.43 | 0.38 | 0.30 | 0.24 |
| Copenhagen, Denmark | N55.8 | 0.25 | 0.34 | 0.44 | 0.48 | 0.48 | 0.53 | 0.48 | 0.49 | 0.45 | 0.39 | 0.32 | 0.28 |
| Nice, France | N43.7 | 0.48 | 0.48 | 0.55 | 0.57 | 0.56 | 0.58 | 0.63 | 0.59 | 0.58 | 0.57 | 0.35 | 0.51 |
| Stuttgart, Germany | N48.8 | 0.35 | 0.39 | 0.42 | 0.46 | 0.46 | 0.47 | 0.49 | 0.47 | 0.35 | 0.45 | 0.35 | 0.32 |
| London, Great Britian | N51.5 | 0.24 | 0.29 | 0.34 | 0.35 | 0.39 | 0.43 | 0.40 | 0.39 | 0.39 | 0.35 | 0.31 | 0.25 |
| Athens, Greece | N38.0 | 0.40 | 0.43 | 0.48 | 0.51 | 0.57 | 0.59 | 0.61 | 0.60 | 0.57 | 0.52 | 0.46 | 0.40 |

| | | | | | | | | | | | | | |
|------------------------|-------|------|------|------|------|------|------|------|------|------|------|------|------|
| Rome, Italy | N41.9 | 0.43 | 0.47 | 0.51 | 0.53 | 0.55 | 0.57 | 0.61 | 0.61 | 0.58 | 0.55 | 0.48 | 0.43 |
| Vlissigen, Netherlands | N51.5 | 0.30 | 0.36 | 0.41 | 0.44 | 0.46 | 0.48 | 0.45 | 0.46 | 0.45 | 0.41 | 0.33 | 0.29 |
| Lisbon, Portugal | N38.7 | 0.45 | 0.35 | 0.55 | 0.57 | 0.60 | 0.62 | 0.67 | 0.68 | 0.62 | 0.57 | 0.52 | 0.53 |
| Warsaw, Poland | N52.3 | 0.25 | 0.26 | 0.39 | 0.39 | 0.43 | 0.47 | 0.46 | 0.49 | 0.42 | 0.33 | 0.24 | 0.21 |
| Cluj, Romania | N46.8 | 0.43 | 0.45 | 0.35 | 0.48 | 0.52 | 0.53 | 0.55 | 0.54 | 0.52 | 0.48 | 0.38 | 0.33 |
| Moscow, Russia | N55.8 | 0.39 | 0.44 | 0.46 | 0.44 | 0.48 | 0.35 | 0.46 | 0.46 | 0.41 | 0.32 | 0.26 | 0.26 |
| St. Petersburg, Russia | N60.0 | 0.34 | 0.40 | 0.44 | 0.44 | 0.51 | 0.51 | 0.49 | 0.46 | 0.41 | 0.33 | 0.26 | 0.26 |
| Almeria, Spain | N36.8 | 0.57 | 0.56 | 0.53 | 0.56 | 0.60 | 0.62 | 0.66 | 0.64 | 0.61 | 0.60 | 0.57 | 0.58 |
| Zurich, Switzerland | N47.5 | 0.28 | 0.36 | 0.41 | 0.44 | 0.47 | 0.47 | 0.52 | 0.47 | 0.48 | 0.39 | 0.30 | 0.26 |
| Kiev, Ukraine | N35.4 | 0.38 | 0.41 | 0.42 | 0.45 | 0.49 | 0.53 | 0.35 | 0.35 | 0.35 | 0.42 | 0.29 | 0.28 |
| Odessa, Ukraine | N46.5 | 0.31 | 0.32 | 0.38 | 0.44 | 0.35 | 0.53 | 0.53 | 0.54 | 0.52 | 0.45 | 0.30 | 0.27 |

Latin America

| Location | Latitude | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-------------------------|----------|------|------|------|------|------|------|------|------|------|------|------|------|
| San Juan, Puerto Rico | N18.4 | 0.54 | 0.56 | 0.58 | 0.57 | 0.53 | 0.53 | 0.55 | 0.55 | 0.53 | 0.53 | 0.54 | 0.53 |
| Ciudad Univ., Mexico | N19.4 | 0.60 | 0.59 | 0.61 | 0.58 | 0.51 | 0.35 | 0.47 | 0.46 | 0.44 | 0.51 | 0.56 | 0.60 |
| Buenos Aires, Argentina | S34.6 | 0.58 | 0.59 | 0.57 | 0.54 | 0.51 | 0.46 | 0.48 | 0.52 | 0.51 | 0.52 | 0.57 | 0.56 |
| Valparaiso, Chile | S33.0 | 0.51 | 0.46 | 0.44 | 0.38 | 0.33 | 0.31 | 0.34 | 0.40 | 0.41 | 0.42 | 0.46 | 0.48 |
| Izobamba, Ecuador | S0.4 | 0.42 | 0.39 | 0.39 | 0.37 | 0.43 | 0.44 | 0.45 | 0.45 | 0.43 | 0.40 | 0.41 | 0.42 |
| Huancayo, Peru | S12.1 | 0.66 | 0.61 | 0.63 | 0.69 | 0.74 | 0.80 | 0.78 | 0.76 | 0.72 | 0.70 | 0.70 | 0.65 |
| Caracas, Venezuela | N10.5 | 0.46 | 0.47 | 0.46 | 0.43 | 0.42 | 0.43 | 0.45 | 0.45 | 0.45 | 0.43 | 0.44 | 0.44 |
| Maracaibo, Venezuela | N10.6 | 0.49 | 0.35 | 0.48 | 0.43 | 0.41 | 0.45 | 0.47 | 0.46 | 0.45 | 0.43 | 0.43 | 0.47 |

Middle East

| Location | Latitude | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-------------------|----------|------|------|------|------|------|------|------|------|------|------|------|------|
| Bet Dagan, Israel | N32.0 | 0.53 | 0.57 | 0.58 | 0.62 | 0.66 | 0.69 | 0.69 | 0.69 | 0.67 | 0.63 | 0.58 | 0.51 |

Pacific

| Location | Latitude | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|--------------------------|----------|------|------|------|------|------|------|------|------|------|------|------|------|
| Aspendale, Australia | S38.0 | 0.57 | 0.57 | 0.54 | 0.48 | 0.45 | 0.46 | 0.47 | 0.46 | 0.48 | 0.35 | 0.53 | 0.55 |
| Darwin, Australia | S12.4 | 0.44 | 0.47 | 0.49 | 0.61 | 0.64 | 0.71 | 0.73 | 0.70 | 0.66 | 0.60 | 0.62 | 0.49 |
| Perth, Australia | S31.9 | 0.58 | 0.61 | 0.58 | 0.53 | 0.52 | 0.35 | 0.55 | 0.57 | 0.59 | 0.58 | 0.56 | 0.59 |
| Nandi, Fiji | S17.8 | 0.47 | 0.48 | 0.47 | 0.49 | 0.51 | 0.52 | 0.52 | 0.53 | 0.52 | 0.51 | 0.51 | 0.51 |
| Wellington, New Zealand | S41.3 | 0.52 | 0.52 | 0.48 | 0.46 | 0.42 | 0.42 | 0.41 | 0.42 | 0.46 | 0.49 | 0.51 | 0.35 |
| Quezon City, Phillipines | N14.6 | 0.47 | 0.35 | 0.52 | 0.54 | 0.49 | 0.46 | 0.41 | 0.37 | 0.42 | 0.42 | 0.45 | 0.45 |
| Koror Island | N7.3 | 0.48 | 0.35 | 0.35 | 0.51 | 0.48 | 0.46 | 0.45 | 0.45 | 0.47 | 0.48 | 0.49 | 0.47 |
| Kwajalein Island | N8.7 | 0.55 | 0.57 | 0.55 | 0.52 | 0.35 | 0.35 | 0.35 | 0.51 | 0.49 | 0.49 | 0.35 | 0.52 |
| Wake Island | N19.3 | 0.56 | 0.58 | 0.59 | 0.58 | 0.59 | 0.59 | 0.56 | 0.56 | 0.55 | 0.56 | 0.58 | 0.57 |

United States

| Location | Latitude | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----------------|----------|------|------|------|------|------|------|------|------|------|------|------|------|
| Anchorage, AK | N61.2 | 0.38 | 0.47 | 0.49 | 0.46 | 0.47 | 0.45 | 0.44 | 0.41 | 0.43 | 0.37 | 0.42 | 0.36 |
| Annette, AK | N55.0 | 0.39 | 0.38 | 0.41 | 0.44 | 0.46 | 0.45 | 0.43 | 0.49 | 0.45 | 0.38 | 0.36 | 0.35 |
| Barrow, AK | N71.3 | 0.51 | 0.41 | 0.58 | 0.57 | 0.48 | 0.42 | 0.41 | 0.36 | 0.32 | 0.40 | 0.60 | 0.00 |
| Bethel, AK | N60.8 | 0.44 | 0.51 | 0.57 | 0.52 | 0.43 | 0.43 | 0.38 | 0.38 | 0.43 | 0.37 | 0.44 | 0.42 |
| Bettles, AK | N66.9 | 0.48 | 0.51 | 0.57 | 0.61 | 0.55 | 0.48 | 0.47 | 0.47 | 0.42 | 0.44 | 0.47 | 1.41 |
| Big Delta, AK | N64.0 | 0.45 | 0.49 | 0.55 | 0.55 | 0.51 | 0.48 | 0.48 | 0.47 | 0.49 | 0.46 | 0.48 | 0.48 |
| Cold Bay, AK | N55.2 | 0.37 | 0.40 | 0.41 | 0.38 | 0.33 | 0.34 | 0.33 | 0.33 | 0.32 | 0.36 | 0.36 | 0.34 |
| Fairbanks, AK | N64.8 | 0.43 | 0.52 | 0.58 | 0.60 | 0.50 | 0.49 | 0.48 | 0.47 | 0.45 | 0.47 | 0.50 | 0.43 |
| Gulkana, AK | N62.1 | 0.44 | 0.53 | 0.58 | 0.57 | 0.49 | 0.49 | 0.50 | 0.47 | 0.47 | 0.45 | 0.47 | 0.43 |
| King Salmon, AK | N58.7 | 0.40 | 0.46 | 0.48 | 0.47 | 0.44 | 0.41 | 0.40 | 0.38 | 0.41 | 0.43 | 0.41 | 0.38 |
| Kodiak, AK | N57.8 | 0.42 | 0.46 | 0.44 | 0.46 | 0.44 | 0.40 | 0.41 | 0.42 | 0.42 | 0.44 | 0.43 | 0.36 |
| Kotzebue, AK | N66.9 | 0.46 | 0.50 | 0.58 | 0.61 | 0.53 | 0.47 | 0.45 | 0.39 | 0.44 | 0.46 | 0.53 | 1.01 |
| Mcgrath, AK | N63.0 | 0.45 | 0.52 | 0.61 | 0.59 | 0.49 | 0.45 | 0.44 | 0.42 | 0.41 | 0.43 | 0.44 | 0.46 |
| Nome, AK | N64.5 | 0.43 | 0.52 | 0.59 | 0.63 | 0.51 | 0.47 | 0.42 | 0.42 | 0.44 | 0.46 | 0.42 | 0.50 |
| St Paul Is., AK | N57.1 | 0.34 | 0.39 | 0.43 | 0.45 | 0.39 | 0.35 | 0.34 | 0.33 | 0.36 | 0.38 | 0.35 | 0.34 |
| Talkeetna, AK | N62.3 | 0.42 | 0.50 | 0.54 | 0.58 | 0.49 | 0.44 | 0.43 | 0.43 | 0.43 | 0.39 | 0.45 | 0.48 |
| Yakutat, AK | N59.5 | 0.42 | 0.47 | 0.50 | 0.47 | 0.41 | 0.39 | 0.37 | 0.41 | 0.38 | 0.42 | 0.40 | 0.39 |

| | | | | | | | | | | | | | |
|----------------------|-------|------|------|------|------|------|------|------|------|------|------|------|------|
| Birmingham, AL | N33.6 | 0.48 | 0.50 | 0.54 | 0.56 | 0.53 | 0.54 | 0.53 | 0.55 | 0.55 | 0.56 | 0.51 | 0.47 |
| Huntsville, AL | N34.6 | 0.45 | 0.51 | 0.50 | 0.53 | 0.53 | 0.55 | 0.56 | 0.56 | 0.54 | 0.59 | 0.50 | 0.45 |
| Mobile, AL | N30.7 | 0.47 | 0.51 | 0.52 | 0.53 | 0.52 | 0.51 | 0.49 | 0.50 | 0.50 | 0.57 | 0.49 | 0.50 |
| Montgomery, AL | N32.3 | 0.48 | 0.52 | 0.54 | 0.57 | 0.56 | 0.54 | 0.54 | 0.56 | 0.56 | 0.57 | 0.52 | 0.49 |
| Fort Smith, AR | N35.3 | 0.52 | 0.55 | 0.54 | 0.55 | 0.56 | 0.58 | 0.57 | 0.59 | 0.54 | 0.56 | 0.55 | 0.49 |
| Little Rock, AR | N34.7 | 0.48 | 0.50 | 0.54 | 0.55 | 0.56 | 0.56 | 0.57 | 0.59 | 0.55 | 0.57 | 0.47 | 0.47 |
| Flagstaff, AZ | N35.1 | 0.61 | 0.64 | 0.63 | 0.62 | 0.63 | 0.66 | 0.58 | 0.53 | 0.64 | 0.65 | 0.63 | 0.61 |
| Phoenix, AZ | N33.4 | 0.61 | 0.65 | 0.66 | 0.72 | 0.73 | 0.72 | 0.69 | 0.69 | 0.70 | 0.70 | 0.65 | 0.59 |
| Prescott, AZ | N34.6 | 0.61 | 0.61 | 0.60 | 0.65 | 0.69 | 0.71 | 0.62 | 0.63 | 0.64 | 0.68 | 0.64 | 0.60 |
| Tucson, AZ | N32.1 | 0.64 | 0.64 | 0.68 | 0.71 | 0.71 | 0.71 | 0.63 | 0.66 | 0.69 | 0.69 | 0.67 | 0.63 |
| Arcata, CA | N41.0 | 0.45 | 0.46 | 0.49 | 0.53 | 0.52 | 0.50 | 0.53 | 0.50 | 0.53 | 0.50 | 0.51 | 0.48 |
| Bakersfield, CA | N35.4 | 0.47 | 0.54 | 0.57 | 0.62 | 0.65 | 0.72 | 0.71 | 0.70 | 0.68 | 0.66 | 0.57 | 0.46 |
| Daggett, CA | N34.9 | 0.65 | 0.65 | 0.70 | 0.74 | 0.72 | 0.74 | 0.72 | 0.71 | 0.72 | 0.70 | 0.66 | 0.63 |
| Fresno, CA | N36.8 | 0.44 | 0.54 | 0.60 | 0.65 | 0.68 | 0.70 | 0.72 | 0.72 | 0.68 | 0.66 | 0.56 | 0.43 |
| Long Beach, CA | N33.8 | 0.54 | 0.56 | 0.56 | 0.59 | 0.59 | 0.59 | 0.64 | 0.65 | 0.61 | 0.59 | 0.58 | 0.54 |
| Los Angeles, CA | N33.9 | 0.55 | 0.59 | 0.57 | 0.60 | 0.59 | 0.59 | 0.62 | 0.64 | 0.58 | 0.59 | 0.58 | 0.56 |
| Sacramento, CA | N38.5 | 0.42 | 0.51 | 0.55 | 0.61 | 0.65 | 0.68 | 0.70 | 0.70 | 0.69 | 0.62 | 0.49 | 0.43 |
| San Diego, CA | N32.7 | 0.57 | 0.58 | 0.59 | 0.63 | 0.57 | 0.58 | 0.61 | 0.64 | 0.60 | 0.62 | 0.60 | 0.57 |
| San Francisco, CA | N37.6 | 0.48 | 0.53 | 0.53 | 0.58 | 0.61 | 0.62 | 0.67 | 0.64 | 0.65 | 0.59 | 0.50 | 0.46 |
| Santa Maria, CA | N34.9 | 0.56 | 0.58 | 0.59 | 0.63 | 0.65 | 0.62 | 0.66 | 0.66 | 0.63 | 0.62 | 0.59 | 0.60 |
| Alamosa, CO | N37.5 | 0.65 | 0.64 | 0.65 | 0.68 | 0.64 | 0.67 | 0.63 | 0.64 | 0.65 | 0.69 | 0.66 | 0.64 |
| Boulder, CO | N40.0 | 0.57 | 0.55 | 0.61 | 0.59 | 0.58 | 0.59 | 0.58 | 0.60 | 0.62 | 0.62 | 0.58 | 0.58 |
| Colorado Springs, CO | N38.8 | 0.58 | 0.58 | 0.59 | 0.59 | 0.57 | 0.60 | 0.58 | 0.60 | 0.62 | 0.65 | 0.62 | 0.57 |
| Eagle, CO | N39.6 | 0.56 | 0.56 | 0.56 | 0.59 | 0.60 | 0.63 | 0.61 | 0.62 | 0.62 | 0.63 | 0.57 | 0.54 |
| Grand Junction, CO | N39.1 | 0.58 | 0.60 | 0.59 | 0.61 | 0.64 | 0.67 | 0.65 | 0.65 | 0.66 | 0.64 | 0.60 | 0.56 |
| Pueblo, CO | N38.3 | 0.58 | 0.61 | 0.60 | 0.60 | 0.62 | 0.65 | 0.64 | 0.63 | 0.63 | 0.69 | 0.63 | 0.60 |
| Bridgeport, CT | N41.2 | 0.46 | 0.50 | 0.47 | 0.51 | 0.50 | 0.51 | 0.51 | 0.51 | 0.50 | 0.51 | 0.45 | 0.44 |
| Hartford, CT | N41.9 | 0.49 | 0.51 | 0.49 | 0.50 | 0.48 | 0.51 | 0.51 | 0.51 | 0.50 | 0.48 | 0.44 | 0.45 |
| Wilmington, DE | N39.7 | 0.48 | 0.53 | 0.51 | 0.51 | 0.51 | 0.55 | 0.54 | 0.55 | 0.52 | 0.54 | 0.48 | 0.43 |
| Daytona Beach, FL | N29.2 | 0.50 | 0.54 | 0.57 | 0.59 | 0.58 | 0.55 | 0.56 | 0.54 | 0.55 | 0.52 | 0.54 | 0.52 |
| Jacksonville, FL | N30.5 | 0.51 | 0.49 | 0.54 | 0.58 | 0.56 | 0.53 | 0.53 | 0.52 | 0.51 | 0.52 | 0.53 | 0.48 |
| Key West, FL | N24.6 | 0.55 | 0.59 | 0.58 | 0.62 | 0.57 | 0.55 | 0.55 | 0.55 | 0.54 | 0.55 | 0.55 | 0.54 |
| Miami, FL | N25.8 | 0.53 | 0.57 | 0.56 | 0.59 | 0.55 | 0.51 | 0.54 | 0.54 | 0.52 | 0.54 | 0.52 | 0.54 |
| Tallahassee, FL | N30.4 | 0.51 | 0.54 | 0.51 | 0.58 | 0.59 | 0.55 | 0.51 | 0.53 | 0.54 | 0.57 | 0.54 | 0.47 |
| Tampa, FL | N28.0 | 0.52 | 0.55 | 0.57 | 0.62 | 0.57 | 0.54 | 0.53 | 0.55 | 0.52 | 0.56 | 0.55 | 0.51 |
| West Palm Beach, FL | N26.7 | 0.53 | 0.53 | 0.55 | 0.55 | 0.53 | 0.50 | 0.52 | 0.53 | 0.52 | 0.53 | 0.53 | 0.51 |
| Athens, GA | N34.0 | 0.48 | 0.53 | 0.55 | 0.56 | 0.55 | 0.55 | 0.55 | 0.54 | 0.54 | 0.60 | 0.53 | 0.50 |
| Atlanta, GA | N33.6 | 0.49 | 0.52 | 0.53 | 0.60 | 0.57 | 0.56 | 0.56 | 0.56 | 0.53 | 0.60 | 0.54 | 0.49 |
| Augusta, GA | N33.4 | 0.48 | 0.53 | 0.52 | 0.57 | 0.53 | 0.54 | 0.55 | 0.55 | 0.54 | 0.55 | 0.53 | 0.51 |
| Columbus, GA | N32.5 | 0.48 | 0.55 | 0.53 | 0.57 | 0.56 | 0.53 | 0.54 | 0.55 | 0.55 | 0.57 | 0.52 | 0.47 |
| Macon, GA | N32.7 | 0.46 | 0.53 | 0.55 | 0.56 | 0.56 | 0.53 | 0.54 | 0.54 | 0.51 | 0.58 | 0.55 | 0.48 |
| Savannah, GA | N32.1 | 0.48 | 0.54 | 0.57 | 0.57 | 0.56 | 0.54 | 0.56 | 0.53 | 0.52 | 0.56 | 0.54 | 0.50 |
| Hilo, HI | N19.7 | 0.49 | 0.52 | 0.48 | 0.46 | 0.47 | 0.52 | 0.48 | 0.51 | 0.51 | 0.48 | 0.48 | 0.50 |
| Honolulu, HI | N21.3 | 0.54 | 0.57 | 0.57 | 0.56 | 0.59 | 0.60 | 0.60 | 0.61 | 0.62 | 0.58 | 0.56 | 0.55 |
| Kahului, HI | N20.9 | 0.56 | 0.56 | 0.57 | 0.55 | 0.57 | 0.61 | 0.61 | 0.63 | 0.63 | 0.61 | 0.55 | 0.56 |
| Lihue, HI | N22.0 | 0.53 | 0.53 | 0.50 | 0.52 | 0.52 | 0.56 | 0.54 | 0.56 | 0.58 | 0.55 | 0.50 | 0.51 |
| Des Moines, IA | N41.5 | 0.51 | 0.54 | 0.51 | 0.52 | 0.53 | 0.57 | 0.59 | 0.56 | 0.55 | 0.53 | 0.47 | 0.48 |
| Mason City, IA | N43.1 | 0.53 | 0.55 | 0.50 | 0.50 | 0.54 | 0.55 | 0.56 | 0.58 | 0.54 | 0.56 | 0.47 | 0.49 |
| Sioux City, IA | N42.4 | 0.54 | 0.53 | 0.53 | 0.53 | 0.55 | 0.57 | 0.58 | 0.57 | 0.54 | 0.54 | 0.50 | 0.47 |
| Waterloo, IA | N42.5 | 0.48 | 0.50 | 0.52 | 0.50 | 0.53 | 0.54 | 0.55 | 0.54 | 0.55 | 0.55 | 0.45 | 0.48 |
| Boise, ID | N43.6 | 0.46 | 0.51 | 0.54 | 0.56 | 0.59 | 0.62 | 0.68 | 0.67 | 0.65 | 0.62 | 0.51 | 0.46 |
| Pocatello, ID | N42.9 | 0.46 | 0.48 | 0.54 | 0.55 | 0.58 | 0.60 | 0.66 | 0.66 | 0.62 | 0.62 | 0.47 | 0.43 |
| Chicago, IL | N41.8 | 0.45 | 0.49 | 0.48 | 0.51 | 0.54 | 0.54 | 0.57 | 0.52 | 0.52 | 0.51 | 0.43 | 0.40 |
| Moline, IL | N41.5 | 0.46 | 0.50 | 0.47 | 0.50 | 0.51 | 0.55 | 0.54 | 0.56 | 0.54 | 0.55 | 0.48 | 0.43 |
| Peoria, IL | N40.7 | 0.48 | 0.52 | 0.48 | 0.51 | 0.54 | 0.56 | 0.57 | 0.55 | 0.55 | 0.55 | 0.48 | 0.44 |
| Rockford, IL | N42.2 | 0.49 | 0.52 | 0.51 | 0.50 | 0.52 | 0.54 | 0.55 | 0.53 | 0.54 | 0.52 | 0.43 | 0.41 |
| Springfield, IL | N39.8 | 0.50 | 0.53 | 0.50 | 0.54 | 0.54 | 0.57 | 0.58 | 0.56 | 0.54 | 0.56 | 0.47 | 0.45 |
| Evansville, IN | N38.0 | 0.46 | 0.47 | 0.49 | 0.51 | 0.53 | 0.56 | 0.55 | 0.56 | 0.53 | 0.55 | 0.47 | 0.43 |
| Fort Wayne, IN | N41.0 | 0.44 | 0.46 | 0.48 | 0.50 | 0.53 | 0.56 | 0.54 | 0.53 | 0.49 | 0.41 | 0.38 | |
| Indianapolis, IN | N39.7 | 0.47 | 0.51 | 0.49 | 0.51 | 0.55 | 0.56 | 0.57 | 0.55 | 0.54 | 0.45 | 0.41 | |
| South Bend, IN | N41.7 | 0.43 | 0.46 | 0.46 | 0.49 | 0.52 | 0.53 | 0.53 | 0.54 | 0.52 | 0.50 | 0.41 | 0.38 |
| Dodge City, KS | N37.8 | 0.60 | 0.62 | 0.61 | 0.60 | 0.56 | 0.62 | 0.64 | 0.64 | 0.60 | 0.64 | 0.58 | 0.59 |

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|-------------------------|-------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Goodland, KS | N39.4 | 0.58 | 0.57 | 0.60 | 0.59 | 0.55 | 0.63 | 0.63 | 0.62 | 0.62 | 0.64 | 0.58 | 0.59 | |
| Topeka, KS | N39.1 | 0.52 | 0.53 | 0.54 | 0.51 | 0.52 | 0.56 | 0.56 | 0.57 | 0.57 | 0.56 | 0.54 | 0.52 | 0.49 |
| Wichita, KS | N37.6 | 0.55 | 0.56 | 0.55 | 0.56 | 0.55 | 0.58 | 0.61 | 0.61 | 0.57 | 0.59 | 0.55 | 0.51 | |
| Covington, KY | N39.1 | 0.44 | 0.46 | 0.49 | 0.50 | 0.53 | 0.54 | 0.53 | 0.56 | 0.53 | 0.55 | 0.43 | 0.37 | |
| Lexington, KY | N38.0 | 0.46 | 0.47 | 0.48 | 0.51 | 0.53 | 0.56 | 0.53 | 0.53 | 0.51 | 0.53 | 0.47 | 0.41 | |
| Louisville, KY | N38.2 | 0.44 | 0.48 | 0.51 | 0.52 | 0.53 | 0.56 | 0.54 | 0.54 | 0.54 | 0.55 | 0.47 | 0.45 | |
| Baton Rouge, LA | N30.5 | 0.47 | 0.48 | 0.51 | 0.53 | 0.54 | 0.53 | 0.51 | 0.54 | 0.51 | 0.60 | 0.52 | 0.48 | |
| Lake Charles, LA | N30.1 | 0.47 | 0.52 | 0.52 | 0.51 | 0.55 | 0.56 | 0.54 | 0.54 | 0.54 | 0.58 | 0.54 | 0.47 | |
| New Orleans, LA | N30.0 | 0.44 | 0.53 | 0.52 | 0.54 | 0.55 | 0.55 | 0.53 | 0.52 | 0.52 | 0.57 | 0.53 | 0.48 | |
| Shreveport, LA | N32.5 | 0.47 | 0.51 | 0.51 | 0.53 | 0.53 | 0.56 | 0.57 | 0.58 | 0.55 | 0.59 | 0.49 | 0.49 | |
| Boston, MA | N42.4 | 0.48 | 0.53 | 0.52 | 0.49 | 0.51 | 0.52 | 0.54 | 0.55 | 0.53 | 0.54 | 0.46 | 0.46 | |
| Worchester, MA | N42.3 | 0.48 | 0.54 | 0.52 | 0.49 | 0.51 | 0.51 | 0.54 | 0.52 | 0.52 | 0.51 | 0.47 | 0.45 | |
| Baltimore, MD | N39.2 | 0.47 | 0.52 | 0.51 | 0.51 | 0.50 | 0.54 | 0.54 | 0.52 | 0.51 | 0.55 | 0.48 | 0.43 | |
| Caribou, ME | N46.9 | 0.56 | 0.57 | 0.57 | 0.56 | 0.48 | 0.50 | 0.49 | 0.50 | 0.48 | 0.47 | 0.44 | 0.50 | |
| Portland, ME | N43.6 | 0.52 | 0.59 | 0.56 | 0.52 | 0.51 | 0.52 | 0.55 | 0.54 | 0.54 | 0.52 | 0.47 | 0.47 | |
| Alpena, MI | N45.1 | 0.46 | 0.52 | 0.54 | 0.52 | 0.51 | 0.53 | 0.55 | 0.50 | 0.48 | 0.44 | 0.41 | 0.42 | |
| Detroit, MI | N42.4 | 0.44 | 0.47 | 0.46 | 0.48 | 0.53 | 0.53 | 0.52 | 0.54 | 0.53 | 0.48 | 0.41 | 0.40 | |
| Flint, MI | N43.0 | 0.43 | 0.50 | 0.48 | 0.50 | 0.53 | 0.53 | 0.53 | 0.52 | 0.51 | 0.47 | 0.41 | 0.36 | |
| Grand Rapids, MI | N42.9 | 0.45 | 0.48 | 0.48 | 0.51 | 0.53 | 0.55 | 0.56 | 0.54 | 0.50 | 0.47 | 0.40 | 0.40 | |
| Houghton, MI | N47.2 | 0.48 | 0.54 | 0.54 | 0.55 | 0.50 | 0.53 | 0.53 | 0.52 | 0.50 | 0.43 | 0.41 | 0.45 | |
| Lansing, MI | N42.8 | 0.44 | 0.48 | 0.48 | 0.50 | 0.52 | 0.53 | 0.56 | 0.53 | 0.53 | 0.49 | 0.43 | 0.38 | |
| Muskegon, MI | N43.2 | 0.42 | 0.51 | 0.49 | 0.52 | 0.57 | 0.58 | 0.56 | 0.55 | 0.52 | 0.47 | 0.40 | 0.38 | |
| Sault Ste. Marie, MI | N46.5 | 0.51 | 0.56 | 0.60 | 0.50 | 0.53 | 0.53 | 0.52 | 0.52 | 0.46 | 0.44 | 0.41 | 0.45 | |
| Traverse City, MI | N44.7 | 0.44 | 0.51 | 0.54 | 0.53 | 0.53 | 0.54 | 0.54 | 0.52 | 0.49 | 0.43 | 0.40 | 0.39 | |
| Duluth, MN | N46.8 | 0.54 | 0.55 | 0.59 | 0.50 | 0.52 | 0.53 | 0.52 | 0.53 | 0.50 | 0.50 | 0.44 | 0.48 | |
| International Falls, MN | N48.6 | 0.51 | 0.59 | 0.59 | 0.54 | 0.51 | 0.52 | 0.54 | 0.53 | 0.47 | 0.46 | 0.43 | 0.46 | |
| Minneapolis, MN | N44.9 | 0.55 | 0.59 | 0.54 | 0.49 | 0.55 | 0.56 | 0.57 | 0.56 | 0.55 | 0.52 | 0.47 | 0.48 | |
| Rochester, MN | N43.9 | 0.51 | 0.57 | 0.52 | 0.51 | 0.50 | 0.54 | 0.56 | 0.55 | 0.52 | 0.48 | 0.45 | 0.47 | |
| Saint Cloud, MN | N45.5 | 0.53 | 0.61 | 0.59 | 0.52 | 0.53 | 0.54 | 0.55 | 0.55 | 0.52 | 0.52 | 0.49 | 0.46 | |
| Columbia, MO | N38.8 | 0.50 | 0.55 | 0.53 | 0.56 | 0.54 | 0.58 | 0.57 | 0.59 | 0.56 | 0.58 | 0.48 | 0.46 | |
| Kansas City, MO | N39.3 | 0.51 | 0.50 | 0.53 | 0.54 | 0.55 | 0.56 | 0.58 | 0.58 | 0.55 | 0.56 | 0.49 | 0.48 | |
| Springfield, MO | N37.2 | 0.51 | 0.50 | 0.54 | 0.54 | 0.54 | 0.56 | 0.57 | 0.58 | 0.55 | 0.55 | 0.50 | 0.46 | |
| St. Louis, MO | N38.8 | 0.49 | 0.51 | 0.53 | 0.52 | 0.54 | 0.56 | 0.57 | 0.53 | 0.54 | 0.54 | 0.49 | 0.45 | |
| Jackson, MS | N32.3 | 0.46 | 0.51 | 0.52 | 0.55 | 0.57 | 0.57 | 0.54 | 0.54 | 0.53 | 0.58 | 0.52 | 0.48 | |
| Meridian, MS | N32.3 | 0.46 | 0.54 | 0.51 | 0.55 | 0.54 | 0.54 | 0.55 | 0.53 | 0.52 | 0.57 | 0.52 | 0.50 | |
| Billings, MT | N45.8 | 0.50 | 0.54 | 0.56 | 0.53 | 0.56 | 0.57 | 0.63 | 0.61 | 0.61 | 0.57 | 0.54 | 0.50 | |
| Cut Bank, MT | N48.6 | 0.51 | 0.56 | 0.56 | 0.53 | 0.55 | 0.57 | 0.64 | 0.60 | 0.58 | 0.59 | 0.52 | 0.49 | |
| Glasgow, MT | N48.2 | 0.51 | 0.56 | 0.58 | 0.52 | 0.55 | 0.56 | 0.61 | 0.60 | 0.55 | 0.55 | 0.49 | 0.51 | |
| Great Falls, MT | N47.5 | 0.47 | 0.53 | 0.55 | 0.54 | 0.53 | 0.60 | 0.62 | 0.61 | 0.62 | 0.55 | 0.51 | 0.48 | |
| Helena, MT | N46.6 | 0.46 | 0.49 | 0.56 | 0.50 | 0.53 | 0.55 | 0.64 | 0.60 | 0.58 | 0.55 | 0.49 | 0.45 | |
| Kalispell, MT | N48.3 | 0.47 | 0.48 | 0.47 | 0.48 | 0.52 | 0.55 | 0.60 | 0.61 | 0.55 | 0.52 | 0.41 | 0.40 | |
| Lewistown, MT | N47.0 | 0.50 | 0.51 | 0.53 | 0.50 | 0.53 | 0.57 | 0.61 | 0.60 | 0.58 | 0.57 | 0.49 | 0.46 | |
| Miles City, MT | N46.4 | 0.53 | 0.55 | 0.55 | 0.51 | 0.56 | 0.58 | 0.63 | 0.63 | 0.59 | 0.57 | 0.51 | 0.50 | |
| Missoula, MT | N46.9 | 0.43 | 0.47 | 0.46 | 0.50 | 0.51 | 0.56 | 0.65 | 0.61 | 0.59 | 0.52 | 0.42 | 0.39 | |
| Asheville, NC | N35.4 | 0.50 | 0.50 | 0.53 | 0.53 | 0.52 | 0.54 | 0.52 | 0.52 | 0.50 | 0.56 | 0.52 | 0.48 | |
| Cape Hatteras, NC | N35.3 | 0.50 | 0.48 | 0.53 | 0.56 | 0.57 | 0.56 | 0.55 | 0.55 | 0.55 | 0.56 | 0.53 | 0.48 | |
| Charlotte, NC | N35.2 | 0.52 | 0.51 | 0.54 | 0.57 | 0.55 | 0.55 | 0.53 | 0.54 | 0.53 | 0.57 | 0.52 | 0.50 | |
| Greensboro, NC | N36.1 | 0.52 | 0.51 | 0.55 | 0.55 | 0.54 | 0.56 | 0.54 | 0.54 | 0.54 | 0.56 | 0.52 | 0.47 | |
| Raleigh, NC | N35.9 | 0.49 | 0.53 | 0.56 | 0.56 | 0.53 | 0.55 | 0.53 | 0.54 | 0.55 | 0.58 | 0.55 | 0.48 | |
| Wilmington, NC | N34.3 | 0.50 | 0.51 | 0.56 | 0.58 | 0.53 | 0.55 | 0.52 | 0.52 | 0.53 | 0.54 | 0.54 | 0.50 | |
| Bismarck, ND | N46.8 | 0.56 | 0.60 | 0.60 | 0.56 | 0.56 | 0.57 | 0.60 | 0.59 | 0.57 | 0.55 | 0.49 | 0.53 | |
| Fargo, ND | N46.9 | 0.54 | 0.60 | 0.54 | 0.53 | 0.54 | 0.55 | 0.56 | 0.56 | 0.53 | 0.51 | 0.48 | 0.48 | |
| Minot, ND | N48.3 | 0.54 | 0.60 | 0.54 | 0.54 | 0.55 | 0.55 | 0.57 | 0.58 | 0.57 | 0.56 | 0.50 | 0.50 | |
| Grand Island, NE | N41.0 | 0.55 | 0.56 | 0.56 | 0.57 | 0.55 | 0.59 | 0.60 | 0.60 | 0.58 | 0.60 | 0.56 | 0.53 | |
| Norfolk, NE | N42.0 | 0.55 | 0.53 | 0.57 | 0.53 | 0.56 | 0.60 | 0.60 | 0.58 | 0.55 | 0.58 | 0.52 | 0.50 | |
| North Platte, NE | N41.1 | 0.55 | 0.56 | 0.56 | 0.56 | 0.57 | 0.60 | 0.61 | 0.60 | 0.59 | 0.61 | 0.55 | 0.54 | |
| Omaha, NE | N41.4 | 0.53 | 0.57 | 0.53 | 0.52 | 0.56 | 0.59 | 0.57 | 0.57 | 0.58 | 0.54 | 0.47 | 0.48 | |
| Scottsbluff, NE | N41.9 | 0.56 | 0.55 | 0.57 | 0.57 | 0.57 | 0.61 | 0.62 | 0.61 | 0.61 | 0.60 | 0.55 | 0.55 | |
| Concord, NH | N43.2 | 0.53 | 0.55 | 0.53 | 0.52 | 0.52 | 0.53 | 0.53 | 0.54 | 0.52 | 0.49 | 0.47 | 0.47 | |
| Atlantic City, NJ | N39.5 | 0.48 | 0.50 | 0.51 | 0.51 | 0.52 | 0.53 | 0.53 | 0.54 | 0.53 | 0.48 | 0.46 | | |
| Newark, NJ | N40.7 | 0.47 | 0.49 | 0.49 | 0.48 | 0.51 | 0.51 | 0.50 | 0.51 | 0.52 | 0.52 | 0.45 | 0.44 | |
| Albuquerque, NM | N35.0 | 0.62 | 0.65 | 0.65 | 0.69 | 0.71 | 0.70 | 0.69 | 0.67 | 0.66 | 0.69 | 0.66 | 0.63 | |
| Tucumcari, NM | N35.2 | 0.61 | 0.61 | 0.62 | 0.64 | 0.63 | 0.68 | 0.64 | 0.63 | 0.61 | 0.65 | 0.62 | 0.61 | |

| | | | | | | | | | | | | | |
|--------------------|-------|------|------|------|------|------|------|------|------|------|------|------|------|
| Elko, NV | N40.8 | 0.52 | 0.52 | 0.53 | 0.53 | 0.59 | 0.62 | 0.64 | 0.66 | 0.67 | 0.63 | 0.52 | 0.52 |
| Ely, NV | N39.3 | 0.61 | 0.58 | 0.62 | 0.59 | 0.61 | 0.66 | 0.67 | 0.64 | 0.69 | 0.68 | 0.59 | 0.60 |
| Las Vegas, NV | N36.1 | 0.62 | 0.65 | 0.66 | 0.70 | 0.72 | 0.72 | 0.72 | 0.70 | 0.72 | 0.70 | 0.67 | 0.62 |
| Reno, NV | N39.5 | 0.52 | 0.56 | 0.61 | 0.63 | 0.61 | 0.66 | 0.70 | 0.70 | 0.72 | 0.66 | 0.60 | 0.55 |
| Tonopah, NV | N38.1 | 0.56 | 0.60 | 0.61 | 0.64 | 0.63 | 0.69 | 0.70 | 0.69 | 0.70 | 0.69 | 0.62 | 0.58 |
| Winnemucca, NV | N40.9 | 0.52 | 0.53 | 0.57 | 0.58 | 0.58 | 0.63 | 0.67 | 0.67 | 0.68 | 0.63 | 0.54 | 0.51 |
| Albany, NY | N42.8 | 0.47 | 0.53 | 0.48 | 0.50 | 0.53 | 0.51 | 0.54 | 0.54 | 0.52 | 0.50 | 0.40 | 0.42 |
| Binghamton, NY | N42.2 | 0.45 | 0.50 | 0.48 | 0.48 | 0.49 | 0.50 | 0.51 | 0.48 | 0.49 | 0.42 | 0.41 | |
| Buffalo, NY | N42.9 | 0.41 | 0.45 | 0.49 | 0.49 | 0.52 | 0.52 | 0.53 | 0.52 | 0.47 | 0.46 | 0.37 | 0.38 |
| Massena, NY | N44.9 | 0.49 | 0.54 | 0.54 | 0.51 | 0.49 | 0.54 | 0.54 | 0.52 | 0.49 | 0.47 | 0.42 | 0.44 |
| New York City, NY | N40.8 | 0.45 | 0.51 | 0.50 | 0.52 | 0.51 | 0.54 | 0.54 | 0.54 | 0.53 | 0.53 | 0.43 | 0.45 |
| Rochester, NY | N43.1 | 0.42 | 0.49 | 0.47 | 0.49 | 0.50 | 0.55 | 0.53 | 0.52 | 0.52 | 0.46 | 0.39 | 0.39 |
| Syracuse, NY | N43.1 | 0.47 | 0.47 | 0.49 | 0.50 | 0.53 | 0.52 | 0.55 | 0.53 | 0.52 | 0.48 | 0.39 | 0.43 |
| Akron, OH | N40.9 | 0.40 | 0.45 | 0.46 | 0.47 | 0.52 | 0.52 | 0.53 | 0.53 | 0.54 | 0.50 | 0.40 | 0.38 |
| Cleveland, OH | N41.4 | 0.41 | 0.45 | 0.46 | 0.49 | 0.53 | 0.53 | 0.53 | 0.53 | 0.52 | 0.49 | 0.37 | 0.35 |
| Columbus, OH | N40.0 | 0.43 | 0.43 | 0.45 | 0.50 | 0.49 | 0.53 | 0.51 | 0.54 | 0.52 | 0.53 | 0.41 | 0.38 |
| Dayton, OH | N39.9 | 0.44 | 0.45 | 0.45 | 0.51 | 0.51 | 0.53 | 0.52 | 0.55 | 0.52 | 0.55 | 0.43 | 0.40 |
| Mansfield, OH | N40.8 | 0.39 | 0.46 | 0.47 | 0.46 | 0.51 | 0.53 | 0.54 | 0.52 | 0.52 | 0.49 | 0.42 | 0.38 |
| Toledo, OH | N41.6 | 0.44 | 0.48 | 0.47 | 0.52 | 0.55 | 0.54 | 0.56 | 0.56 | 0.53 | 0.48 | 0.42 | 0.40 |
| Youngstown, OH | N41.3 | 0.38 | 0.43 | 0.47 | 0.47 | 0.48 | 0.50 | 0.51 | 0.51 | 0.46 | 0.47 | 0.37 | 0.37 |
| Oklahoma City, OK | N35.4 | 0.54 | 0.56 | 0.56 | 0.58 | 0.55 | 0.58 | 0.60 | 0.61 | 0.58 | 0.60 | 0.55 | 0.56 |
| Tulsa, OK | N36.2 | 0.51 | 0.52 | 0.55 | 0.57 | 0.54 | 0.56 | 0.59 | 0.58 | 0.52 | 0.59 | 0.51 | 0.50 |
| Astoria, OR | N46.1 | 0.35 | 0.40 | 0.41 | 0.42 | 0.45 | 0.47 | 0.49 | 0.48 | 0.51 | 0.48 | 0.39 | 0.39 |
| Burns, OR | N43.6 | 0.50 | 0.51 | 0.52 | 0.55 | 0.58 | 0.61 | 0.65 | 0.65 | 0.64 | 0.60 | 0.46 | 0.45 |
| Eugene, OR | N44.1 | 0.39 | 0.39 | 0.45 | 0.45 | 0.51 | 0.54 | 0.61 | 0.62 | 0.57 | 0.50 | 0.38 | 0.33 |
| Medford, OR | N42.4 | 0.40 | 0.45 | 0.55 | 0.54 | 0.60 | 0.62 | 0.70 | 0.68 | 0.64 | 0.57 | 0.40 | 0.38 |
| North Bend, OR | N43.4 | 0.43 | 0.48 | 0.50 | 0.54 | 0.55 | 0.59 | 0.56 | 0.56 | 0.52 | 0.45 | 0.41 | |
| Pendleton, OR | N45.7 | 0.42 | 0.46 | 0.52 | 0.55 | 0.57 | 0.60 | 0.66 | 0.65 | 0.64 | 0.56 | 0.45 | 0.42 |
| Portland, OR | N45.6 | 0.40 | 0.40 | 0.45 | 0.45 | 0.51 | 0.51 | 0.58 | 0.54 | 0.52 | 0.48 | 0.38 | 0.33 |
| Redmond, OR | N44.3 | 0.46 | 0.49 | 0.53 | 0.58 | 0.58 | 0.63 | 0.68 | 0.68 | 0.68 | 0.60 | 0.52 | 0.47 |
| Salem, OR | N44.9 | 0.33 | 0.40 | 0.47 | 0.47 | 0.51 | 0.54 | 0.60 | 0.60 | 0.59 | 0.49 | 0.39 | 0.39 |
| Allentown, PA | N40.6 | 0.46 | 0.49 | 0.50 | 0.52 | 0.50 | 0.50 | 0.53 | 0.51 | 0.51 | 0.51 | 0.43 | 0.43 |
| Bradford, PA | N41.8 | 0.45 | 0.48 | 0.50 | 0.49 | 0.49 | 0.52 | 0.53 | 0.50 | 0.49 | 0.48 | 0.42 | 0.42 |
| Erie, PA | N42.1 | 0.40 | 0.46 | 0.47 | 0.50 | 0.53 | 0.53 | 0.55 | 0.54 | 0.53 | 0.49 | 0.36 | 0.39 |
| Harrisburg, PA | N40.2 | 0.47 | 0.50 | 0.49 | 0.52 | 0.51 | 0.54 | 0.54 | 0.52 | 0.52 | 0.44 | 0.42 | |
| Philadelphia, PA | N39.9 | 0.45 | 0.50 | 0.50 | 0.50 | 0.50 | 0.52 | 0.53 | 0.55 | 0.52 | 0.53 | 0.47 | 0.42 |
| Pittsburgh, PA | N40.5 | 0.41 | 0.46 | 0.47 | 0.49 | 0.50 | 0.52 | 0.51 | 0.53 | 0.49 | 0.50 | 0.42 | 0.36 |
| Wilkes-Barre, PA | N41.3 | 0.43 | 0.46 | 0.45 | 0.49 | 0.52 | 0.51 | 0.52 | 0.51 | 0.50 | 0.49 | 0.39 | 0.40 |
| Williamsport, PA | N41.3 | 0.46 | 0.46 | 0.49 | 0.46 | 0.50 | 0.51 | 0.52 | 0.51 | 0.49 | 0.46 | 0.40 | 0.41 |
| Guam, PI | N13.6 | 0.55 | 0.52 | 0.57 | 0.55 | 0.55 | 0.53 | 0.49 | 0.47 | 0.48 | 0.51 | 0.51 | 0.53 |
| San Juan, PR | N18.4 | 0.56 | 0.57 | 0.59 | 0.57 | 0.54 | 0.56 | 0.57 | 0.56 | 0.57 | 0.55 | 0.53 | 0.53 |
| Providence, RI | N41.7 | 0.48 | 0.52 | 0.52 | 0.52 | 0.51 | 0.53 | 0.56 | 0.55 | 0.50 | 0.52 | 0.47 | 0.45 |
| Charleston, SC | N32.9 | 0.54 | 0.51 | 0.57 | 0.59 | 0.56 | 0.52 | 0.55 | 0.52 | 0.50 | 0.59 | 0.56 | 0.48 |
| Columbia, SC | N34.0 | 0.48 | 0.51 | 0.51 | 0.58 | 0.54 | 0.56 | 0.55 | 0.52 | 0.53 | 0.61 | 0.55 | 0.49 |
| Greenville, SC | N34.9 | 0.49 | 0.53 | 0.55 | 0.58 | 0.53 | 0.54 | 0.54 | 0.56 | 0.55 | 0.57 | 0.51 | 0.50 |
| Huron, SD | N44.4 | 0.54 | 0.56 | 0.56 | 0.54 | 0.54 | 0.55 | 0.60 | 0.60 | 0.57 | 0.56 | 0.51 | 0.48 |
| Pierre, SD | N44.4 | 0.56 | 0.54 | 0.56 | 0.56 | 0.56 | 0.60 | 0.61 | 0.59 | 0.60 | 0.59 | 0.52 | 0.49 |
| Rapid City, SD | N44.0 | 0.55 | 0.56 | 0.57 | 0.55 | 0.55 | 0.59 | 0.61 | 0.61 | 0.59 | 0.61 | 0.56 | 0.53 |
| Sioux Falls, SD | N43.6 | 0.51 | 0.53 | 0.52 | 0.53 | 0.54 | 0.57 | 0.60 | 0.58 | 0.56 | 0.56 | 0.48 | 0.47 |
| Bristol, TN | N36.5 | 0.42 | 0.47 | 0.48 | 0.52 | 0.52 | 0.51 | 0.50 | 0.52 | 0.52 | 0.56 | 0.45 | 0.45 |
| Chattanooga, TN | N35.0 | 0.48 | 0.46 | 0.50 | 0.54 | 0.54 | 0.52 | 0.54 | 0.51 | 0.57 | 0.46 | | |
| Knoxville, TN | N35.8 | 0.44 | 0.48 | 0.51 | 0.52 | 0.51 | 0.54 | 0.53 | 0.52 | 0.51 | 0.55 | 0.48 | 0.46 |
| Memphis, TN | N35.0 | 0.50 | 0.52 | 0.55 | 0.56 | 0.56 | 0.58 | 0.59 | 0.60 | 0.53 | 0.60 | 0.51 | 0.48 |
| Nashville, TN | N36.1 | 0.48 | 0.52 | 0.54 | 0.54 | 0.57 | 0.57 | 0.55 | 0.54 | 0.57 | 0.48 | 0.45 | |
| Abilene, TX | N32.4 | 0.57 | 0.59 | 0.60 | 0.62 | 0.59 | 0.61 | 0.62 | 0.60 | 0.57 | 0.64 | 0.61 | 0.57 |
| Amarillo, TX | N35.2 | 0.57 | 0.61 | 0.61 | 0.62 | 0.60 | 0.64 | 0.63 | 0.60 | 0.60 | 0.67 | 0.56 | 0.59 |
| Austin, TX | N30.3 | 0.52 | 0.55 | 0.55 | 0.53 | 0.53 | 0.58 | 0.60 | 0.60 | 0.57 | 0.60 | 0.55 | 0.50 |
| Brownsville, TX | N25.9 | 0.46 | 0.47 | 0.50 | 0.51 | 0.54 | 0.57 | 0.59 | 0.56 | 0.53 | 0.59 | 0.50 | 0.43 |
| Corpus Christi, TX | N27.8 | 0.46 | 0.48 | 0.48 | 0.48 | 0.50 | 0.54 | 0.56 | 0.56 | 0.54 | 0.53 | 0.50 | 0.46 |
| El Paso, TX | N31.8 | 0.62 | 0.64 | 0.68 | 0.70 | 0.70 | 0.72 | 0.67 | 0.64 | 0.67 | 0.70 | 0.65 | 0.64 |
| Fort Worth, TX | N32.8 | 0.53 | 0.53 | 0.56 | 0.57 | 0.58 | 0.61 | 0.62 | 0.61 | 0.58 | 0.59 | 0.54 | 0.53 |
| Houston, TX | N30.0 | 0.46 | 0.47 | 0.49 | 0.48 | 0.51 | 0.54 | 0.52 | 0.53 | 0.53 | 0.56 | 0.52 | 0.44 |
| Lubbock, TX | N33.6 | 0.57 | 0.59 | 0.63 | 0.61 | 0.62 | 0.63 | 0.59 | 0.59 | 0.58 | 0.65 | 0.62 | 0.59 |

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|--------------------|-------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lufkin, TX | N31.2 | 0.48 | 0.50 | 0.51 | 0.53 | 0.55 | 0.56 | 0.56 | 0.57 | 0.56 | 0.58 | 0.54 | 0.48 |
| Midland, TX | N31.9 | 0.60 | 0.62 | 0.66 | 0.64 | 0.62 | 0.62 | 0.65 | 0.62 | 0.60 | 0.65 | 0.62 | 0.59 |
| Port Arthur, TX | N29.9 | 0.46 | 0.50 | 0.51 | 0.51 | 0.53 | 0.58 | 0.53 | 0.55 | 0.54 | 0.58 | 0.49 | 0.47 |
| San Angelo, TX | N31.4 | 0.57 | 0.58 | 0.59 | 0.58 | 0.57 | 0.60 | 0.61 | 0.61 | 0.59 | 0.62 | 0.56 | 0.56 |
| San Antonio, TX | N29.5 | 0.51 | 0.54 | 0.55 | 0.53 | 0.54 | 0.58 | 0.63 | 0.61 | 0.58 | 0.60 | 0.56 | 0.51 |
| Victoria, TX | N28.9 | 0.47 | 0.50 | 0.49 | 0.49 | 0.52 | 0.54 | 0.57 | 0.56 | 0.56 | 0.56 | 0.54 | 0.48 |
| Waco, TX | N31.6 | 0.51 | 0.57 | 0.54 | 0.51 | 0.54 | 0.60 | 0.63 | 0.59 | 0.58 | 0.61 | 0.57 | 0.53 |
| Wichita Falls, TX | N34.0 | 0.55 | 0.57 | 0.58 | 0.58 | 0.57 | 0.61 | 0.62 | 0.60 | 0.60 | 0.60 | 0.57 | 0.55 |
| Cedar City, UT | N37.7 | 0.58 | 0.59 | 0.60 | 0.63 | 0.63 | 0.69 | 0.65 | 0.64 | 0.65 | 0.68 | 0.59 | 0.56 |
| Salt Lake City, UT | N40.8 | 0.49 | 0.54 | 0.54 | 0.55 | 0.62 | 0.63 | 0.66 | 0.67 | 0.64 | 0.62 | 0.54 | 0.45 |
| Lynchburg, VA | N37.3 | 0.50 | 0.54 | 0.57 | 0.55 | 0.54 | 0.56 | 0.57 | 0.55 | 0.55 | 0.55 | 0.53 | 0.49 |
| Norfolk, VA | N36.9 | 0.50 | 0.52 | 0.49 | 0.53 | 0.51 | 0.55 | 0.52 | 0.54 | 0.51 | 0.55 | 0.51 | 0.46 |
| Richmond, VA | N37.5 | 0.52 | 0.51 | 0.52 | 0.52 | 0.52 | 0.53 | 0.54 | 0.52 | 0.54 | 0.52 | 0.50 | 0.49 |
| Roanoke, VA | N37.3 | 0.50 | 0.51 | 0.51 | 0.53 | 0.54 | 0.54 | 0.53 | 0.53 | 0.53 | 0.55 | 0.51 | 0.47 |
| Sterling, VA | N39.0 | 0.49 | 0.51 | 0.51 | 0.52 | 0.51 | 0.54 | 0.53 | 0.52 | 0.53 | 0.54 | 0.48 | 0.42 |
| Burlington, VT | N44.5 | 0.50 | 0.54 | 0.52 | 0.51 | 0.53 | 0.52 | 0.53 | 0.54 | 0.51 | 0.48 | 0.42 | 0.42 |
| Olympia, WA | N47.0 | 0.32 | 0.39 | 0.44 | 0.41 | 0.46 | 0.50 | 0.54 | 0.54 | 0.51 | 0.43 | 0.36 | 0.34 |
| Quillayute, WA | N48.0 | 0.32 | 0.36 | 0.38 | 0.42 | 0.46 | 0.45 | 0.48 | 0.46 | 0.48 | 0.46 | 0.36 | 0.37 |
| Seattle, WA | N47.5 | 0.31 | 0.37 | 0.44 | 0.45 | 0.51 | 0.52 | 0.56 | 0.52 | 0.52 | 0.41 | 0.35 | 0.29 |
| Spokane, WA | N47.6 | 0.49 | 0.44 | 0.47 | 0.51 | 0.53 | 0.53 | 0.65 | 0.63 | 0.58 | 0.55 | 0.41 | 0.43 |
| Yakima, WA | N46.6 | 0.42 | 0.50 | 0.54 | 0.53 | 0.58 | 0.61 | 0.65 | 0.63 | 0.63 | 0.58 | 0.44 | 0.43 |
| Eau Claire, WI | N44.9 | 0.50 | 0.59 | 0.56 | 0.49 | 0.53 | 0.54 | 0.54 | 0.53 | 0.50 | 0.49 | 0.42 | 0.43 |
| Green Bay, WI | N44.5 | 0.49 | 0.52 | 0.52 | 0.52 | 0.53 | 0.53 | 0.56 | 0.50 | 0.49 | 0.50 | 0.42 | 0.46 |
| La Crosse, WI | N43.9 | 0.55 | 0.55 | 0.53 | 0.50 | 0.54 | 0.53 | 0.57 | 0.53 | 0.50 | 0.53 | 0.44 | 0.43 |
| Madison, WI | N43.1 | 0.48 | 0.54 | 0.50 | 0.48 | 0.54 | 0.55 | 0.56 | 0.57 | 0.51 | 0.51 | 0.44 | 0.49 |
| Milwaukee, WI | N43.0 | 0.51 | 0.51 | 0.48 | 0.51 | 0.54 | 0.57 | 0.54 | 0.55 | 0.54 | 0.51 | 0.45 | 0.44 |
| Charleston, WV | N38.4 | 0.44 | 0.44 | 0.48 | 0.51 | 0.50 | 0.50 | 0.52 | 0.52 | 0.51 | 0.52 | 0.45 | 0.39 |
| Elkins, WV | N38.9 | 0.44 | 0.45 | 0.45 | 0.48 | 0.49 | 0.49 | 0.49 | 0.49 | 0.48 | 0.50 | 0.43 | 0.39 |
| Huntington, WV | N38.4 | 0.46 | 0.45 | 0.49 | 0.49 | 0.50 | 0.52 | 0.51 | 0.51 | 0.52 | 0.52 | 0.47 | 0.42 |
| Casper, WY | N42.9 | 0.55 | 0.55 | 0.56 | 0.57 | 0.57 | 0.61 | 0.61 | 0.65 | 0.62 | 0.61 | 0.54 | 0.51 |
| Cheyenne, WY | N41.1 | 0.54 | 0.56 | 0.58 | 0.57 | 0.56 | 0.60 | 0.58 | 0.59 | 0.62 | 0.60 | 0.57 | 0.53 |
| Lander, WY | N42.8 | 0.57 | 0.62 | 0.61 | 0.59 | 0.59 | 0.63 | 0.63 | 0.62 | 0.66 | 0.63 | 0.59 | 0.58 |
| Rock Springs, WY | N41.6 | 0.53 | 0.56 | 0.58 | 0.60 | 0.60 | 0.62 | 0.64 | 0.65 | 0.65 | 0.64 | 0.54 | 0.52 |
| Sheridan, WY | N44.8 | 0.55 | 0.55 | 0.56 | 0.55 | 0.52 | 0.58 | 0.60 | 0.62 | 0.61 | 0.58 | 0.54 | 0.53 |

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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4.3 Wind Data Histograms

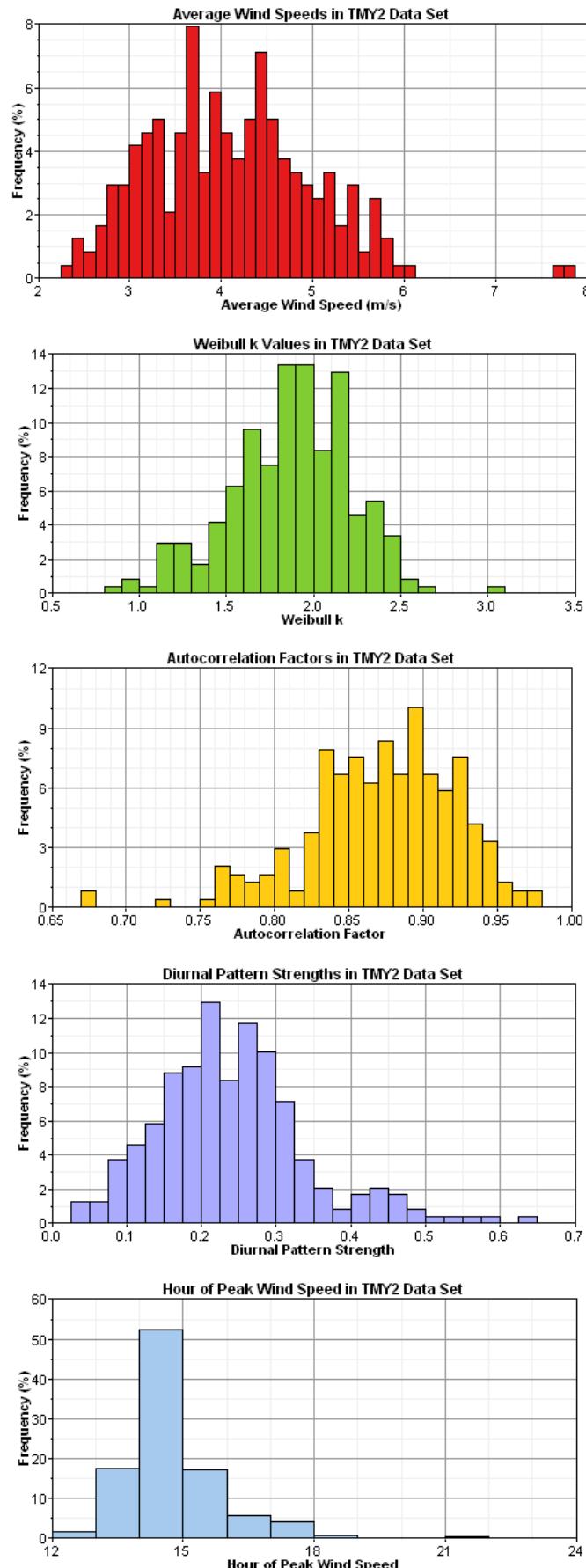


Wind Data Histograms

The following five wind data parameters were measured for the 239 weather stations in the U.S. National Solar Radiation Data Base:

- annual average wind speed
- [Weibull k value](#)
- [autocorrelation factor](#)
- [diurnal pattern strength](#)
- [hour of peak wind speed](#)

The numerical results are displayed in the [table of measured parameters](#). The histograms below show the distribution of each of these parameters:



For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

4.4 Wind Data Parameters



Wind Data Parameters

The following table contains the following parameters for each of the 239 stations in the US National Solar Radiation Data Base:

- annual average wind speed, v_{ave} [m/s]
- [Weibull k value](#), k
- [one-hour autocorrelation factor](#), r_1
- [diurnal pattern strength](#), d
- [hour of peak wind speed](#), f

You can also look at [histograms](#) of these parameters.

Important: The stations that make these measurements are not typically located so as to maximize the wind resource. So this data is likely to be conservative in terms of wind speed, since in siting a wind turbine you would normally seek out a ridgeline or other topographic feature to maximize average wind speeds. Also, this data is compiled from TMY (Typical Meteorological Year) data, which is chosen as "typical" largely on the basis of solar data, not wind data. So these data do not necessarily represent a typical year of wind speeds.

| City | State | v_{ave} | k | r_1 | d | f |
|-----------------|-------|-----------|-------|-------|-------|-----|
| Anchorage | AK | 3.277 | 1.681 | 0.769 | 0.125 | 17 |
| Annette | AK | 4.206 | 1.650 | 0.973 | 0.132 | 13 |
| Barrow | AK | 5.482 | 2.234 | 0.948 | 0.036 | 15 |
| Bethel | AK | 5.659 | 2.166 | 0.950 | 0.059 | 16 |
| Bettles | AK | 3.148 | 1.689 | 0.873 | 0.112 | 14 |
| Big Delta | AK | 4.069 | 1.297 | 0.966 | 0.091 | 17 |
| Cold Bay | AK | 7.661 | 2.019 | 0.913 | 0.075 | 15 |
| Fairbanks | AK | 2.506 | 1.289 | 0.787 | 0.160 | 17 |
| Gulkana | AK | 2.651 | 0.809 | 0.934 | 0.183 | 16 |
| King Salmon | AK | 4.882 | 1.874 | 0.932 | 0.143 | 16 |
| Kodiak | AK | 4.652 | 1.468 | 0.895 | 0.082 | 15 |
| Kotzebue | AK | 6.005 | 1.833 | 0.934 | 0.030 | 14 |
| McGrath | AK | 2.482 | 1.428 | 0.894 | 0.202 | 16 |
| Nome | AK | 4.774 | 1.621 | 0.920 | 0.117 | 15 |
| St. Paul Island | AK | 7.802 | 2.084 | 0.966 | 0.052 | 14 |
| Talkeetna | AK | 2.465 | 1.030 | 0.876 | 0.268 | 15 |
| Yakutat | AK | 2.964 | 1.359 | 0.945 | 0.218 | 14 |
| Birmingham | AL | 3.163 | 1.521 | 0.831 | 0.345 | 13 |
| Huntsville | AL | 3.626 | 1.619 | 0.838 | 0.276 | 13 |
| Mobile | AL | 3.684 | 1.852 | 0.849 | 0.268 | 13 |
| Montgomery | AL | 3.023 | 1.658 | 0.794 | 0.338 | 13 |
| Fort Smith | AR | 3.235 | 1.845 | 0.901 | 0.307 | 14 |
| Little Rock | AR | 3.435 | 1.887 | 0.807 | 0.284 | 14 |
| Flagstaff | AZ | 3.238 | 1.537 | 0.922 | 0.447 | 14 |
| Phoenix | AZ | 2.984 | 2.016 | 0.727 | 0.148 | 14 |
| Prescott | AZ | 3.734 | 1.927 | 0.847 | 0.272 | 15 |
| Tucson | AZ | 3.935 | 2.127 | 0.858 | 0.160 | 15 |
| Arcata | CA | 3.051 | 1.366 | 0.911 | 0.424 | 14 |
| Bakersfield | CA | 2.852 | 1.750 | 0.830 | 0.267 | 16 |
| Dagget | CA | 4.901 | 1.750 | 0.933 | 0.028 | 21 |
| Fresno | CA | 2.986 | 1.880 | 0.867 | 0.194 | 17 |
| Long Beach | CA | 2.702 | 1.595 | 0.850 | 0.549 | 15 |
| Los Angeles | CA | 3.575 | 1.961 | 0.676 | 0.469 | 15 |
| Sacramento | CA | 3.251 | 1.413 | 0.894 | 0.276 | 15 |
| San Diego | CA | 3.224 | 1.983 | 0.798 | 0.412 | 14 |
| San Francisco | CA | 4.530 | 1.689 | 0.876 | 0.405 | 17 |
| Santa Maria | CA | 3.356 | 1.271 | 0.871 | 0.632 | 15 |
| Alamosa | CO | 3.746 | 1.502 | 0.900 | 0.336 | 17 |
| Boulder/Denver | CO | 3.639 | 1.849 | 0.678 | 0.208 | 16 |

| | | | | | | |
|------------------|----|-------|-------|-------|-------|----|
| Colorado Springs | CO | 4.356 | 1.890 | 0.831 | 0.185 | 15 |
| Eagle | CO | 2.712 | 0.944 | 0.836 | 0.579 | 16 |
| Grand Junction | CO | 3.560 | 1.784 | 0.823 | 0.086 | 14 |
| Pueblo | CO | 4.097 | 1.678 | 0.842 | 0.311 | 16 |
| Bridgeport | CT | 5.423 | 2.336 | 0.880 | 0.173 | 14 |
| Hartford | CT | 3.831 | 1.878 | 0.882 | 0.275 | 14 |
| Wilmington | DE | 4.134 | 1.977 | 0.899 | 0.252 | 14 |
| Daytona Beach | FL | 3.811 | 1.795 | 0.895 | 0.416 | 14 |
| Jacksonville | FL | 3.283 | 1.555 | 0.775 | 0.463 | 14 |
| Key West | FL | 5.089 | 2.506 | 0.942 | 0.069 | 13 |
| Miami | FL | 4.337 | 2.214 | 0.803 | 0.292 | 14 |
| Tallahassee | FL | 2.901 | 1.432 | 0.841 | 0.460 | 14 |
| Tampa | FL | 3.579 | 2.147 | 0.762 | 0.336 | 14 |
| West Palm Beach | FL | 4.391 | 1.984 | 0.926 | 0.297 | 14 |
| Athens | GA | 3.314 | 2.002 | 0.920 | 0.209 | 14 |
| Atlanta | GA | 3.947 | 2.152 | 0.808 | 0.170 | 14 |
| Augusta | GA | 3.158 | 1.587 | 0.860 | 0.338 | 14 |
| Columbus | GA | 2.950 | 1.604 | 0.889 | 0.346 | 14 |
| Macon | GA | 3.287 | 1.689 | 0.780 | 0.307 | 14 |
| Savannah | GA | 3.565 | 1.969 | 0.918 | 0.324 | 14 |
| Hilo | HI | 3.142 | 2.263 | 0.839 | 0.260 | 14 |
| Honolulu | HI | 4.950 | 2.433 | 0.822 | 0.306 | 15 |
| Kahului | HI | 5.712 | 2.305 | 0.880 | 0.374 | 15 |
| Lihue | HI | 5.503 | 3.024 | 0.951 | 0.086 | 15 |
| Des Moines | IA | 4.696 | 1.999 | 0.922 | 0.216 | 13 |
| Mason City | IA | 5.079 | 2.052 | 0.898 | 0.210 | 13 |
| Sioux City | IA | 4.885 | 2.030 | 0.894 | 0.208 | 14 |
| Waterloo | IA | 4.763 | 1.904 | 0.897 | 0.235 | 13 |
| Boise | ID | 3.810 | 1.845 | 0.779 | 0.201 | 15 |
| Pocatello | ID | 4.728 | 1.731 | 0.881 | 0.192 | 15 |
| Chicago | IL | 4.620 | 2.152 | 0.847 | 0.195 | 14 |
| Moline | IL | 4.619 | 1.896 | 0.905 | 0.260 | 13 |
| Peoria | IL | 4.379 | 2.124 | 0.859 | 0.224 | 13 |
| Rockford | IL | 4.665 | 2.137 | 0.903 | 0.234 | 13 |
| Springfield | IL | 4.804 | 2.178 | 0.909 | 0.159 | 13 |
| Evansville | IN | 3.525 | 1.492 | 0.858 | 0.327 | 13 |
| Fort Wayne | IN | 4.468 | 2.115 | 0.899 | 0.200 | 14 |
| Indianapolis | IN | 4.063 | 1.966 | 0.890 | 0.209 | 14 |
| South Bend | IN | 4.503 | 2.084 | 0.894 | 0.225 | 14 |
| Dodge City | KS | 5.790 | 2.404 | 0.847 | 0.130 | 13 |
| Goodland | KS | 5.831 | 2.396 | 0.855 | 0.084 | 13 |
| Topeka | KS | 4.392 | 1.843 | 0.847 | 0.249 | 14 |
| Wichita | KS | 5.214 | 2.205 | 0.909 | 0.175 | 14 |
| Covington | KY | 3.950 | 2.076 | 0.856 | 0.207 | 14 |
| Lexington | KY | 3.942 | 2.277 | 0.929 | 0.180 | 13 |
| Louisville | KY | 3.672 | 1.876 | 0.831 | 0.268 | 15 |
| Baton Rouge | LA | 3.239 | 1.647 | 0.872 | 0.311 | 14 |
| Lake Charles | LA | 3.775 | 1.973 | 0.832 | 0.286 | 14 |
| New Orleans | LA | 3.582 | 1.828 | 0.864 | 0.258 | 13 |
| Shreveport | LA | 3.464 | 1.746 | 0.841 | 0.279 | 14 |
| Boston | MA | 5.430 | 2.401 | 0.838 | 0.126 | 14 |
| Worcester | MA | 4.319 | 1.944 | 0.903 | 0.087 | 13 |
| Baltimore | MD | 4.108 | 1.995 | 0.842 | 0.264 | 14 |
| Caribou | ME | 4.593 | 1.769 | 0.909 | 0.172 | 14 |
| Portland | ME | 3.904 | 1.908 | 0.856 | 0.295 | 14 |
| Alpena | MI | 3.693 | 1.943 | 0.897 | 0.289 | 14 |
| Detroit | MI | 4.507 | 2.123 | 0.848 | 0.243 | 14 |
| Flint | MI | 4.378 | 2.027 | 0.886 | 0.212 | 14 |
| Grand Rapids | MI | 4.454 | 2.199 | 0.892 | 0.215 | 14 |
| Houghton | MI | 4.060 | 2.338 | 0.909 | 0.161 | 15 |
| Lansing | MI | 4.344 | 1.855 | 0.933 | 0.223 | 14 |
| Muskegon | MI | 4.888 | 2.104 | 0.931 | 0.190 | 14 |

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|----------------------|----|-------|-------|-------|-------|----|
| Sault Ste. Marie | MI | 3.806 | 1.987 | 0.862 | 0.244 | 15 |
| Traverse City | MI | 3.993 | 1.818 | 0.868 | 0.241 | 14 |
| Duluth | MN | 4.701 | 2.205 | 0.924 | 0.156 | 14 |
| International Falls | MN | 4.019 | 1.977 | 0.871 | 0.221 | 13 |
| Minneapolis/St. Paul | MN | 4.624 | 2.016 | 0.897 | 0.223 | 14 |
| Rochester | MN | 5.789 | 2.441 | 0.926 | 0.130 | 12 |
| St. Cloud | MN | 3.661 | 1.730 | 0.942 | 0.274 | 14 |
| Columbia | MO | 4.439 | 2.322 | 0.874 | 0.157 | 13 |
| Kansas City | MO | 4.482 | 2.527 | 0.842 | 0.166 | 14 |
| Springfield | MO | 4.506 | 2.284 | 0.858 | 0.190 | 12 |
| St. Louis | MO | 4.401 | 2.094 | 0.857 | 0.172 | 14 |
| Jackson | MS | 3.322 | 1.607 | 0.857 | 0.324 | 13 |
| Meridian | MS | 2.769 | 1.247 | 0.825 | 0.434 | 13 |
| Billings | MT | 5.155 | 2.324 | 0.885 | 0.079 | 14 |
| Cut Bank | MT | 5.672 | 1.761 | 0.946 | 0.225 | 15 |
| Glasgow | MT | 4.802 | 2.059 | 0.933 | 0.130 | 14 |
| Great Falls | MT | 5.513 | 1.898 | 0.906 | 0.156 | 14 |
| Helena | MT | 3.527 | 1.537 | 0.876 | 0.281 | 16 |
| Kalispell | MT | 2.828 | 1.139 | 0.905 | 0.255 | 14 |
| Lewistown | MT | 4.245 | 1.745 | 0.917 | 0.149 | 14 |
| Miles City | MT | 4.624 | 2.040 | 0.836 | 0.102 | 14 |
| Missoula | MT | 3.023 | 1.296 | 0.831 | 0.327 | 17 |
| Asheville | NC | 3.480 | 1.308 | 0.854 | 0.313 | 14 |
| Cape Hatteras | NC | 5.157 | 2.419 | 0.954 | 0.100 | 14 |
| Charlotte | NC | 3.139 | 1.825 | 0.791 | 0.291 | 14 |
| Greensboro | NC | 3.116 | 1.861 | 0.823 | 0.287 | 13 |
| Raleigh/Durham | NC | 3.503 | 2.005 | 0.816 | 0.245 | 14 |
| Wilmington | NC | 3.670 | 1.822 | 0.904 | 0.309 | 14 |
| Bismarck | ND | 4.420 | 1.608 | 0.875 | 0.308 | 14 |
| Fargo | ND | 5.377 | 2.026 | 0.927 | 0.158 | 14 |
| Minot | ND | 5.489 | 2.310 | 0.879 | 0.138 | 14 |
| Grand Island | NE | 5.336 | 2.246 | 0.910 | 0.175 | 14 |
| Norfolk | NE | 5.455 | 1.710 | 0.924 | 0.229 | 14 |
| North Platte | NE | 4.651 | 1.692 | 0.862 | 0.264 | 15 |
| Omaha | NE | 4.493 | 1.838 | 0.922 | 0.176 | 13 |
| Scottsbluff | NE | 4.663 | 1.820 | 0.813 | 0.235 | 14 |
| Concord | NH | 2.865 | 1.149 | 0.838 | 0.441 | 14 |
| Atlantic City | NJ | 4.420 | 1.935 | 0.948 | 0.262 | 14 |
| Newark | NJ | 4.624 | 2.345 | 0.809 | 0.157 | 15 |
| Albuquerque | NM | 4.009 | 1.723 | 0.789 | 0.255 | 17 |
| Tucumcari | NM | 4.335 | 1.907 | 0.911 | 0.208 | 14 |
| Elko | NV | 2.700 | 1.195 | 0.827 | 0.470 | 15 |
| Ely | NV | 4.374 | 1.963 | 0.879 | 0.078 | 13 |
| Las Vegas | NV | 4.063 | 1.809 | 0.854 | 0.139 | 18 |
| Reno | NV | 2.839 | 1.124 | 0.856 | 0.555 | 17 |
| Tonopah | NV | 4.317 | 1.804 | 0.826 | 0.167 | 15 |
| Winnemucca | NV | 3.630 | 1.833 | 0.851 | 0.245 | 15 |
| Albany | NY | 3.958 | 1.567 | 0.856 | 0.259 | 14 |
| Binghamton | NY | 4.509 | 2.357 | 0.891 | 0.155 | 14 |
| Buffalo | NY | 5.135 | 2.152 | 0.889 | 0.181 | 14 |
| Massena | NY | 3.632 | 1.520 | 0.885 | 0.267 | 13 |
| NYC (Central Park) | NY | 5.185 | 2.676 | 0.933 | 0.130 | 15 |
| Rochester | NY | 4.377 | 1.983 | 0.916 | 0.183 | 14 |
| Syracuse | NY | 4.100 | 1.903 | 0.877 | 0.202 | 14 |
| Akron/Canton | OH | 4.173 | 2.179 | 0.890 | 0.210 | 13 |
| Cleveland | OH | 4.506 | 2.186 | 0.842 | 0.191 | 14 |
| Columbus | OH | 3.728 | 1.898 | 0.847 | 0.288 | 14 |
| Dayton | OH | 4.311 | 2.106 | 0.847 | 0.185 | 14 |
| Mansfield | OH | 4.786 | 2.342 | 0.930 | 0.159 | 13 |
| Toledo | OH | 4.150 | 1.914 | 0.898 | 0.266 | 14 |
| Youngstown | OH | 4.407 | 2.312 | 0.893 | 0.178 | 14 |
| Oklahoma City | OK | 5.352 | 2.253 | 0.937 | 0.183 | 13 |

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|----------------|----|-------|-------|-------|-------|----|
| Tulsa | OK | 4.811 | 2.173 | 0.902 | 0.222 | 14 |
| Astoria | OR | 3.987 | 1.876 | 0.916 | 0.254 | 15 |
| Burns | OR | 3.213 | 1.652 | 0.946 | 0.240 | 15 |
| Eugene | OR | 3.366 | 1.904 | 0.890 | 0.273 | 14 |
| Medford | OR | 2.255 | 1.262 | 0.765 | 0.484 | 16 |
| North Bend | OR | 4.276 | 1.768 | 0.911 | 0.322 | 15 |
| Pendleton | OR | 3.826 | 1.749 | 0.885 | 0.125 | 16 |
| Portland | OR | 3.580 | 1.560 | 0.872 | 0.230 | 16 |
| Redmond/Bend | OR | 3.640 | 1.913 | 0.835 | 0.295 | 15 |
| Salem | OR | 3.127 | 1.387 | 0.897 | 0.291 | 14 |
| Allentown | PA | 4.143 | 1.684 | 0.884 | 0.289 | 14 |
| Bradford | PA | 3.660 | 1.765 | 0.921 | 0.260 | 14 |
| Erie | PA | 5.141 | 2.216 | 0.910 | 0.104 | 12 |
| Harrisburg | PA | 3.353 | 1.513 | 0.845 | 0.278 | 14 |
| Philadelphia | PA | 4.307 | 2.190 | 0.831 | 0.203 | 14 |
| Pittsburgh | PA | 3.922 | 1.760 | 0.850 | 0.284 | 14 |
| Wilkes-Barre | PA | 3.641 | 2.146 | 0.836 | 0.222 | 14 |
| Williamsport | PA | 3.442 | 1.295 | 0.870 | 0.297 | 14 |
| Guam | PI | 4.205 | 2.189 | 0.973 | 0.307 | 13 |
| San Juan | PR | 3.823 | 1.788 | 0.869 | 0.504 | 15 |
| Providence | RI | 4.702 | 2.157 | 0.881 | 0.257 | 14 |
| Charleston | SC | 3.892 | 2.069 | 0.821 | 0.318 | 14 |
| Columbia | SC | 3.035 | 1.555 | 0.773 | 0.382 | 14 |
| Greenville | SC | 2.982 | 1.810 | 0.896 | 0.277 | 13 |
| Huron | SD | 4.842 | 1.956 | 0.918 | 0.202 | 14 |
| Pierre | SD | 5.102 | 1.884 | 0.920 | 0.194 | 14 |
| Rapid City | SD | 5.342 | 1.677 | 0.928 | 0.231 | 13 |
| Sioux Falls | SD | 5.023 | 2.021 | 0.927 | 0.217 | 14 |
| Bristol | TN | 2.397 | 1.174 | 0.833 | 0.437 | 15 |
| Chattanooga | TN | 2.507 | 1.108 | 0.801 | 0.493 | 15 |
| Knoxville | TN | 3.023 | 1.545 | 0.845 | 0.262 | 15 |
| Memphis | TN | 3.998 | 1.903 | 0.887 | 0.229 | 13 |
| Nashville | TN | 3.642 | 1.902 | 0.803 | 0.250 | 14 |
| Abilene | TX | 5.205 | 2.418 | 0.915 | 0.119 | 14 |
| Amarillo | TX | 5.929 | 2.411 | 0.878 | 0.129 | 14 |
| Austin | TX | 4.062 | 1.895 | 0.835 | 0.238 | 14 |
| Brownsville | TX | 5.266 | 2.130 | 0.924 | 0.361 | 14 |
| Corpus Christi | TX | 5.377 | 2.197 | 0.918 | 0.303 | 15 |
| El Paso | TX | 3.534 | 1.612 | 0.798 | 0.241 | 16 |
| Fort Worth | TX | 4.433 | 1.984 | 0.909 | 0.191 | 14 |
| Houston | TX | 3.777 | 2.112 | 0.775 | 0.321 | 14 |
| Lubbock | TX | 5.196 | 2.164 | 0.890 | 0.184 | 15 |
| Lufkin | TX | 3.068 | 1.515 | 0.854 | 0.395 | 14 |
| Midland/Odessa | TX | 5.050 | 2.184 | 0.832 | 0.225 | 14 |
| Port Arthur | TX | 4.367 | 2.176 | 0.885 | 0.261 | 14 |
| San Angelo | TX | 4.638 | 2.150 | 0.863 | 0.199 | 14 |
| San Antonio | TX | 4.200 | 2.332 | 0.864 | 0.202 | 15 |
| Victoria | TX | 4.487 | 2.158 | 0.929 | 0.308 | 14 |
| Waco | TX | 4.842 | 2.323 | 0.906 | 0.138 | 14 |
| Wichita Falls | TX | 5.675 | 2.414 | 0.944 | 0.164 | 14 |
| Cedar City | UT | 3.554 | 1.179 | 0.861 | 0.439 | 16 |
| Salt Lake City | UT | 3.968 | 1.667 | 0.762 | 0.119 | 13 |
| Lynchburg | VA | 3.061 | 1.454 | 0.867 | 0.359 | 14 |
| Norfolk | VA | 4.883 | 2.207 | 0.862 | 0.183 | 13 |
| Richmond | VA | 3.653 | 2.110 | 0.897 | 0.227 | 14 |
| Roanoke | VA | 3.630 | 1.662 | 0.859 | 0.265 | 15 |
| Sterling | VA | 3.490 | 1.694 | 0.821 | 0.291 | 14 |
| Burlington | VT | 4.064 | 2.004 | 0.806 | 0.204 | 13 |
| Olympia | WA | 3.060 | 1.441 | 0.883 | 0.303 | 14 |
| Quillayute | WA | 2.787 | 1.559 | 0.871 | 0.372 | 14 |
| Seattle | WA | 3.897 | 2.108 | 0.760 | 0.121 | 15 |
| Spokane | WA | 4.333 | 1.934 | 0.875 | 0.122 | 12 |

| | | | | | | |
|--------------|----|-------|-------|-------|-------|----|
| Yakima | WA | 3.296 | 1.725 | 0.870 | 0.139 | 18 |
| Eau Claire | WI | 3.974 | 1.888 | 0.872 | 0.275 | 14 |
| Green Bay | WI | 4.438 | 1.999 | 0.918 | 0.232 | 13 |
| La Crosse | WI | 3.706 | 1.645 | 0.887 | 0.199 | 14 |
| Madison | WI | 4.223 | 1.860 | 0.892 | 0.260 | 13 |
| Milwaukee | WI | 4.944 | 2.087 | 0.868 | 0.194 | 13 |
| Charleston | WV | 2.764 | 1.433 | 0.860 | 0.326 | 14 |
| Elkins | WV | 2.932 | 0.971 | 0.906 | 0.370 | 14 |
| Huntington | WV | 3.101 | 1.917 | 0.822 | 0.241 | 14 |
| Casper | WY | 5.652 | 2.075 | 0.929 | 0.216 | 13 |
| Cheyenne | WY | 5.735 | 1.996 | 0.868 | 0.173 | 13 |
| Lander | WY | 3.363 | 1.459 | 0.759 | 0.255 | 17 |
| Rock Springs | WY | 5.097 | 1.629 | 0.874 | 0.280 | 15 |
| Sheridan | WY | 3.367 | 1.494 | 0.833 | 0.265 | 14 |

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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4.5 References



References

This page lists sources of information on the algorithms used within HOMER and sources you can use to develop the inputs you need to run HOMER.

Solar Power

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Search Space Optimization

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- Le Digabel S (2011) Algorithm 909:NOMAD: Nonlinear optimization with the MADS algorithm, *ACM Transactions on Mathematical Software*, **37(4)** 44:1-44:15.

See also

[Recommended reading](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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4.6 Recommended Reading

Recommended Reading



This page lists sources of information that you might find helpful in learning about micropower systems. None of this information is essential to running HOMER.

Renewable and Micropower Systems

- Masters G (2004) [Renewable and Efficient Electric Power Systems](#), Wiley-IEEE Press, ISBN: 0471280607
- Borbely AM, Kreider JF, (2001) [Distributed Generation: The Power Paradigm for the New Millennium](#), CRC Press, ISBN: 0849300746

Solar Resource

- Chapters 1 and 2 of Duffie JA, Beckman WA (1991) [Solar Engineering of Thermal Processes](#) 2nd edition, Wiley, New York, NY, ISBN: 0471510564

Wind Resource

- An excellent and multilingual source of information on the wind resource, wind turbine technology, economics and more is [www.windpower.org](#), the Danish Wind Industry Association's website.
- Chapter 2 of Manwell JF, McGowan JG, Rogers AL (2002) [Wind Energy Explained](#), Wiley, New York, NY, ISBN: 0471499722

Biomass Resource

- McKendry P (2002a) Energy production from biomass (part 1): overview of biomass, *Bioresource Technology*, **83**, 37-46

Biomass Power

- McKendry P (2002b) Energy production from biomass (part 2): conversion technologies, *Bioresource Technology*, **83**, 47-54

Hydro Power

- For a helpful introduction to small hydro, see Paish O (2002) Small hydro power: technology and current status, *Renewable and Sustainable Energy Reviews*, **6**, 537-556
- For a useful website on all things microhydro, see [www.microhydropower.net](#).
- Some useful calculation tools are available at the website of VA Tech Hydro, [www.compact-hydro.com](#).

See also

[References](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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5. License Management



License Management

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See also

[Renewing your HOMER license](#)

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6. Glossary

6.1 English-Spanish Glossary



English-Spanish Glossary

This glossary includes words and terms that are part of the HOMER user interface with their equivalents in Spanish. The words appear in alphabetical order, based on the English spelling.

To see a definition, click on a letter below to go to the section of the glossary for that letter.

[A](#) [B](#) [C](#) [D](#) [E](#) [F](#) [G](#) [H](#) [I](#) [J](#) [K](#) [L](#) [M](#) [N](#) [O](#) [P](#) [Q](#) [R](#) [S](#) [T](#) [U](#) [V](#) [W](#) [X](#) [Y](#) [Z](#)

| English | Spanish |
|---|---|
| Agregar/Eliminar | |
| A | |
| Abbreviation | Abreviación |
| AC | CA |
| Add noise | Agregar ruido |
| Add/Remove | |
| Advanced parameters | Parámetros avanzados |
| Allow multiple generators to operate simultaneously | Permite múltiples generadores para operar simultáneamente |
| Allow systems with generator capacity less than peak load | Permite sistemas con generadores de capacidad inferior a picos de demanda |
| Allow systems with multiple generators | Permite sistemas con múltiples generadores |
| Annual electric energy production | Producción anual de energía eléctrica |
| Annual electric loads | Cargas eléctricas anuales |
| Annual fuel consumption | Consumo anual de combustible |
| Annual peak | Pico anual |
| Annual peak load | Carga anual pico |
| Annual real interest rate | Tasa de interés real anual |
| Apply setpoint SOC | Aplica punto de ajuste EDC (Estado De Carga) |
| As percent of load | Como porcentaje de la carga |
| As percent of renewable output | Como porcentaje de producción renovable |
| Author | Autor |
| Autocorrelation factor | Factor de auto corrección |
| Automatically check for updates on startup | Revisa automáticamente para actualizarse al inicio |
| Available biomass | Biomasa disponible |
| Average electrical efficiency | Eficiencia eléctrica promedio |

| | |
|-------------------------------------|---|
| Average electrical output | Producción eléctrica promedio |
| Average Hydrogen Load | Carga promedio de hidrógeno |
| Average price | Precio promedio |
| Average total efficiency | Promedio de eficiencia total |
| Azimuth | Azimut |
| B | |
| Baseline data | Datos base |
| Batt. (battery) | Batería |
| Batt. cap. mult. | Multiplicador del costo inversión de la batería |
| Batt. capital cost Multiplier | Multiplicador del costo inversión de la batería |
| Batt. O&M mult. | Multiplicador del costo operación y mantenimiento de la batería |
| Batt. O&M cost multiplier | Multiplicador del costo operación y mantenimiento de la batería |
| Batt. repl. mult. | Multiplicador del costo reemplazo batería |
| Batt. replacement cost multiplier | Multiplicador del costo reemplazo de la batería |
| Battery | Batería |
| Battery capital cost multiplier | Multiplicador del costo inversión de la batería |
| Battery O&M cost multiplier | Multiplicador del costo operación y mantenimiento de la batería |
| Battery replacement cost multiplier | Multiplicador del costo reemplazo de la batería |
| Bio. gas. ratio | Razón de biogás |
| Bio. GR | Razón de biogás |
| Biogas | Biogás |
| Biogas LHV | Valor calórico mas bajo de biogás (VCB) |
| Biogas lower heating value | Valor calórico mas bajo de biogás |
| Biomass carbon content | Contenido de carbón biomasa |
| Biomass data scaled average | Promedio escalado de datos de biomasa |
| Biomass gasification ratio | Razón de gasificación de la biomasa |
| Biomass price | Precio de la biomasa |
| Biomass resource | Recurso de biomasa |
| Biomass resource price | Precio del recurso biomasa |
| Boiler | Calentador |
| Boiler cap. | Capacidad de la caldera |
| Boiler capacity | Capacidad de la caldera |
| Boiler eff. | Eficiencia de la caldera |
| Boiler efficiency | Eficiencia de la caldera |
| c | |
| Calculate | Calcular |
| Calculated parameters | Parámetros calculados |
| Cancel | Cancelar |
| Capacity curve | Curva de capacidad |
| Capacity ratio | Razón de capacidad |
| Capacity relative to inverter | Capacidad relativa al inversor |
| Capacity shortage | Falta de capacidad |
| Capital | Capital |
| Carbon content | Contenido de carbón |
| Carbon emissions | Emisiones de carbón |
| Clear | Borrar |
| Clearness index | Índice de claridad |
| COE (cost of energy) | CE (costo de la energía) |
| Cofire inputs | Datos del combustible alterno |

| | |
|---------------------------------------|---|
| Cofire with biogas | Combustible con biogás |
| Component | Componente |
| Constraints | Consideraciones |
| Consumption limit | Límite de consumo |
| Conv. (converter) | Convertidor |
| Conv. cap. mult. | Multiplicador del costo inversión del convertidor |
| Conv. O&M mult. | Multiplicador del costo operación y mantenimiento del convertidor |
| Conv. repl. mult. | Multiplicador del costo reemplazo del convertidor |
| Converter | Convertidor |
| Converter capital cost multiplier | Multiplicador del costo inversión del convertidor |
| Converter capital multiplier | Multiplicador del costo inversión del convertidor |
| Converter O&M cost multiplier | Multiplicador del costo operación y mantenimiento del convertidor |
| Converter O&M multiplier | Multiplicador del costo operación y mantenimiento del convertidor |
| Converter replacement cost multiplier | Multiplicador del costo reemplazo del convertidor |
| Converter replacement multiplier | Multiplicador del costo reemplazo del convertidor |
| Cost curve | Curva de costo |
| Costs | Costos |
| Current | Corriente |
| Cycle charging | Ciclos de carga |
| Cycles to failure | Ciclos de falla |
| D | |
| Daily noise | Ruido diario |
| Daily radiation | Radiación diaria |
| Day type | Tipo de día |
| DC | CD |
| Default author | Autor por definición |
| Def. load min. | Carga Mínima diferida |
| Def. load peak | Carga Pico diferida |
| Def. load storage | Capacidad de almacenamiento diferida |
| Deferrable load | Cargas diferidas |
| Deferrable load min. | Carga mínima diferida |
| Deferrable load minimum | Carga mínima diferida |
| Deferrable load peak | Carga pico diferida |
| Deferrable load served | Cargas diferidas servidas |
| Deferrable load storage capacity | Capacidad de almacenamiento diferida |
| Degrees | Grados |
| Delete | Eliminar |
| Demand | Demanda |
| Demand rate | Razón de demanda |
| Density | Densidad |
| Depth of discharge | Profundidad de descarga |
| Derating factor | Factor de reducción |
| Design flow rate | Razón de flujo de diseño |
| Details | Detalles |
| Dispatch strategy | Estrategia de despacho |
| Diurnal pattern strength | Patrón diurno de intensidad |
| Document | Documento |
| E | |

| | |
|--|--|
| Economics | Económicos |
| Efficiency curve | Curva de eficiencia |
| Efficiency inputs | Datos de eficiencia |
| Elec. (electrolyzer) | Elec. (fluído electrolítico) |
| Elec. cap. mult. | Multiplicador del costo inversión del electrolizador |
| Elec. eff. | Eficiencia electrolizador |
| Elec. min. | Mínimo electrolizador |
| Elec. min. load | Carga mínima electrolizador |
| Elec. O&M mult. | Multiplicador del costo operación y mantenimiento del electrolizador |
| Elec. repl. mult. | Multiplicador del costo reemplazo del electrolizador |
| Electrolyzer | Fluido electrolítico |
| Electrolyzer capital cost multiplier | Multiplicador del costo de inversión del electrolizador |
| Electrolyzer capital multiplier | Multiplicador del costo de inversión del electrolizador |
| Electrolyzer eff. | Eficiencia electrolítica |
| Electrolyzer efficiency | Eficiencia electrolítica |
| Electrolyzer life | Vida del electrolito |
| Electrolyzer lifetime | Tiempo de vida del electrolito |
| Electrolyzer load served | Cargas cubiertas por el electrolizador |
| Electrolyzer minimum load ratio | Razón carga mínima del electrolizador |
| Electrolyzer O&M cost multiplier | Multiplicador del costo operación y mantenimiento del electrolizador |
| Electrolyzer O&M multiplier | Multiplicador del costo operación y mantenimiento del electrolizador |
| Electrolyzer replacement cost multiplier | Multiplicador del costo reemplazo del electrolizador |
| Electrolyzer replacement multiplier | Multiplicador del costo reemplazo del electrolizador |
| Equipment to consider | Equipo a considerar |
| Excess electricity | Excedente de electricidad |
| Excess electricity can serve thermal load | Excedente de electricidad puede servir a cargas térmicas |
| Export | Exportar |
| F | |
| File version | Versión del archivo |
| Fixed (variables) | Fijo (variables) |
| Fixed cap. cost | Costo de inversión fijo |
| Fixed O&M cost | Costo de operación y mantenimiento fijo |
| Fuel curve | Curva de combustible |
| G | |
| Generator | Generador |
| Generator control | Control del generador |
| Generator fuel curve intercept coefficient | Coeficiente de intercepción de la curva de combustible del generador |
| Generator fuel curve slope | Pendiente de la curva de combustible del generador |
| Generator heat recovery ratio | Razón de recuperación de calor generador |
| Generator lifetime | Tiempo de vida generador |
| Generator minimum fossil fraction | Fracción combustible mínimo generador |
| Generator minimum load | Carga mínima generador |
| Generator substitution ratio | Razón de sustitución generador |
| Generator type | Tipo de generador |

| | |
|--------------------------------|--|
| Global solar | Radiación solar global |
| Graphic | Grafica |
| Grid | Red |
| Grid cap. | Capacidad de la red |
| Grid capital cost | Costo de la red |
| Grid demand rate | Razón de demanda de la red |
| Grid extension cost | Costo extensión de la red |
| Grid extension capital cost | Costo por extensión de la red |
| Grid extension O&M Cost | Costo por operación y mantenimiento de extensión de la red |
| Grid extension power price | Precio de la energía por extensión de la red |
| Grid interconnection charge | Cargo por interconexión con la Red |
| Grid O&M | Costo por operación y mantenimiento de la red |
| Grid O&M cost | Costo por operación y mantenimiento de la red |
| Grid power | Capacidad de la red |
| Grid power price | Precio de la energía de la red |
| Grid power price | Precio de la energía de la red |
| Grid sellback rate | Razón de repago de la red |
| Grid standby charge | Cargo por tiempo de espera de la red |
| Grid-connected system | Sistema conectado a la red |
| Grnd. ref. | Reflexión de tierra |
| Ground reflectance | Reflexión de tierra |
| H | |
| H2 Load | Carga hidrogeno |
| H2 tank capital multiplier | Multiplicador del costo inversión del tanque de hidrogeno |
| H2 tank life | Tiempo de vida del tanque de hidrogeno |
| H2 tank O&M multiplier | Multiplicador del costo de operación y mantenimiento del tanque de hidrogeno |
| H2 tank replacement multiplier | Multiplicador de reemplazo del tanque de Hidrogeno |
| Help | Ayuda |
| Hour of peak wind speed | Hora de velocidad de viento pico |
| Hourly data | Datos horarios |
| Hourly load | Carga horaria |
| Hourly noise | Ruido horario |
| Hours of operations | Horas de operación |
| HT cap. mult. | Multiplicador del costo inversión del tanque de hidrogeno |
| HT O&M mult. | Multiplicador del costo de operación y mantenimiento del tanque de hidrogeno |
| HT repl. mult. | Multiplicador del costo de reemplazo del tanque de Hidrogeno |
| Hydro | Hidroeléctrica |
| Hydro capital | Costo de la hidroeléctrica |
| Hydro capital Cost | Costo de la hidroeléctrica |
| Hydro data scaled Average | Promedio de datos escalados de hidro |
| Hydro design Flow Rate | Tasa de flujo de diseño de la hidro |
| Hydro eff. | Eficiencia de la Hidro |
| Hydro head | Carga (Salto) de la hidro |
| Hydro head loss | Perdida de carga de la hidro |
| Hydro life | Vida de la hidro |
| Hydro lifetime | Tiempo de vida de la hidro |
| Hydro maximum flow ratio | Tasa de flujo máximo de la hidro |
| Hydro minimum flow ratio | Tasa de flujo mínimo de la hidro |
| Hydro O&M | operación y mantenimiento de la hidro |

| | |
|---|--|
| Hydro O&M cost | Costo de operación y mantenimiento de la hidro |
| Hydro repl. | Reemplazo de la hidro |
| Hydro replacement | Reemplazo de la hidro |
| Hydro replacement cost | Costo del reemplazo de la hidro |
| Hydro resource | Recurso hidráulico |
| Hydro turbine efficiency | Eficiencia de la turbina hidro |
| Hydrogen load | Carga de hidrógeno |
| Hydrogen tank capital cost multiplier | Multiplicador del costo inversión del tanque del hidrógeno |
| Hydrogen tank lifetime | Tiempo de vida del tanque de hidrógeno |
| Hydrogen tank O&M cost multiplier | Multiplicador del costo de operación y mantenimiento del tanque de hidrógeno |
| Hydrogen tank replacement cost multiplier | Multiplicador del costo de reemplazo del tanque de hidrógeno |
| Hydrogen consumption | Consumo de hidrógeno |
| I | |
| Import file | Importar archivo |
| Intake pipe | Tubo de admisión |
| Intercept | Interceptar |
| Interconn. charge | Cargo por interconexión |
| Interconnection charge | Cargo por interconexión |
| Interest rate | Tasa de interés |
| Inverter | Inversor |
| Inverter eff. | Eficiencia del inversor |
| Inverter efficiency | Eficiencia del inversor |
| Inverter life | Vida del inversor |
| Inverter lifetime | Tiempo de vida del inversor |
| J | |
| K | |
| L | |
| Label | Etiqueta |
| Latitude | Latitud |
| Legend | Leyenda |
| LHV of biogas | Valor calórico bajo del biogás |
| Lifetime | Tiempo de vida |
| Lifetime curve | Curva de tiempo de vida |
| Lifetime throughput | Rendimiento en el tiempo de vida |
| Limit consumption to | Límite de consumo para |
| Link with | Enlace con |
| Load | Carga |
| Load factor | Factor de carga |
| Load following | Seguimiento de la carga |
| Load profile | Perfil de carga |
| Load type | Tipo de carga |
| Longitude | Longitud |
| Lower heating value | Valor calórico bajo |
| M | |
| Manufacturer | Fabricante |
| Max. annual capacity shortage | Máxima falta de capacidad anual |
| Max. cap. shortage | Máxima falta de capacidad |
| Max. flow ratio | Tasa de flujo máximo |

| | |
|-------------------------------------|---------------------------------------|
| Max. grid demand | Demanda máxima de la red |
| Max. grid sale | Venta máxima de la red |
| Maximum annual capacity shortage | Máxima falta de capacidad anual |
| Maximum capacity | Capacidad máxima |
| Maximum electrical output | Producción eléctrica máxima |
| Maximum grid demand | Demanda máxima de la red |
| Maximum grid power sale | Venta máxima de la red |
| Minimum battery life | Vida mínima de la batería |
| Minimum electrical output | Producción eléctrica mínima |
| Minimum renewable fraction | Fracción renovable mínima |
| Minutes | Minutos |
| Min. batt. life | Vida mínima de la batería |
| Min. battery life | Vida mínima de la batería |
| Min. flow ratio | Tasa mínima de flujo |
| Min. ren. fraction | Fracción renovable mínima |
| Min. RF | Fracción renovable mínima |
| Month | Mes |
| Monthly average electric production | Producción eléctrica promedio mensual |
| N | |
| Net generation calculated yearly | Generación calculada neta anual |
| Net generation calculated monthly | Generación calculada neta mensual |
| Net metering | Medición neta |
| New | Nuevo |
| New window | Ventana nueva |
| Nominal capacity | Capacidad nominal |
| Nominal power | Potencia nominal |
| Nominal voltage | Voltaje nominal |
| North | Norte |
| Notes | Notas |
| Number of starts | Numero de arranques |
| O | |
| OK | OK |
| Operating reserve | Reserva operativa |
| Operating reserve hourly load | Carga horaria reserva operativa |
| Operating reserve peak load | Carga pico reserva operativa |
| Operating reserve solar | Reserva operativa solar |
| Operating reserve wind | Reserva operativa eólica |
| Operational life | Vida Operacional |
| Optimal system type | Tipo de sistema optimo |
| Optimization results | Resultados de la optimización |
| OR hourly load | Carga horaria reserva operativa |
| OR peak load | Carga pico reserva operativa |
| OR solar | Reserva operativa solar |
| OR wind | Reserva operativa eólica |
| Other | Otro |
| Overall rankings list size | Lista general clasificada por tamaño |
| P | |

| | |
|---------------------------------|---|
| Pipe head loss | Perdida de carga en tubería |
| Plot | Graficar |
| Power price | Precio de la energía |
| Preferences | Preferencias |
| Price | Precio |
| Primary | Primaria |
| Primary load | Carga primaria |
| Primary load served | Carga primaria servida |
| Progress | Progreso |
| Project lifetime | Tiempo de vida del proyecto |
| Properties | Propiedades |
| PV | FV |
| PV cap. mult. | Multiplicador del costo inversión del FV |
| PV capital cost multiplier | Multiplicador del costo inversión del FV |
| PV capital multiplier | Multiplicador del costo inversión del FV |
| PV O&M cost multiplier | Multiplicador del costo de operación y mantenimiento del FV |
| PV O&M mult. | Multiplicador del costo de operación y mantenimiento del FV |
| PV O&M multiplier | Multiplicador del costo de operación y mantenimiento del FV |
| PV repl. mult. | Multiplicador del costo de remplazo del FV |
| PV replacement cost multiplier | Multiplicador del costo de reemplazo del FV |
| PV replacement multiplier | Multiplicador del costo de reemplazo del FV |
| Q | |
| Quantity | Cantidad |
| R | |
| Rate constant | Razón constante |
| Rectifier | Rectificador |
| Rectifier cap. | Capacidad del Rectificador |
| Rectifier eff. | Eficiencia del rectificador |
| Rectifier efficiency | Eficiencia del rectificador |
| Rectifier rel. cap. | Capacidad relativa del rectificador |
| Relative rectifier capacity | Capacidad relativa del rectificador |
| Reload last project on startup | Recarga del ultimo proyecto al inicio |
| Ren. frac. (renewable fraction) | Fracción renovable |
| Renewable fraction | Fracción renovable |
| Replacement | Reemplazar |
| Resources | Recursos |
| S | |
| Scaled average | Promedio escalado |
| Scaled data for simulation | Datos escalados para simulación |
| Scaled peak | Pico escalado |
| Search space | Busca espacio - mas opciones |
| Search space usage | Uso de búsqueda de espacio |
| Sellback | Retorno por venta |
| Sellback Rate | Tasa de retorno por venta |
| Sensitivities | Sensibilidad |
| Sensitivity results | Resultados sensibles |
| Sensitivity variables | Variables sensibles |
| Setpoint SOC | Punto de ajuste de estado de carga |
| Setpoint state of charge | Punto de ajuste de estado de carga |
| Simulation results | Resultados de la simulación |

| | |
|------------------------------------|---|
| Simulations | Simulaciones |
| Size | Tamaño |
| Sizes to consider | Tamaño a considerar |
| Slope | Pendiente |
| Solar Data Scaled Average | Promedio escalado de datos solares |
| Solar power output | Producción de energía solar |
| Solar resource | Recurso solar |
| South | Sur |
| Specific fuel consumption | Consumo de combustible específico |
| Standby Charge | Carga en modo de espera |
| Stand-alone system | Sistema autónomo |
| Status | Estatus |
| Stored hydrogen | Hidrógeno almacenado |
| Stream Flow | Flujo de vapor |
| Suggested value | Valor sugerido |
| Superimposed | Superpuesto |
| Synthesize data | Dato generado |
| Synthesized | Sintetizado |
| System architecture | Arquitectura del sistema |
| System fixed capital cost | Costo inversión fijo del sistema |
| System fixed O&M cost | Costo de operación y mantenimiento fijo del sistema |
| T | |
| Tabular | Tabular |
| Thermal load | Carga térmica |
| Total load served | Total de la carga servida (satisficha) |
| Total NPC (total net present cost) | CNP total (costo neto presente total) |
| Total production | Producción total |
| Tracking system | Sistema de seguimiento |
| U | |
| Units | Unidades |
| Unmet load | Carga insatisficha |
| Unmet load cost | Costo carga no satisficha |
| Utility rate structure | Estructura tarifaria de la energía |
| V | |
| Values | Valores |
| Variable | Variable |
| Variables to plot | Variables para graficas |
| W | |
| Warnings | Advertencia |
| Weekday | Día de la semana |
| Weekend | Fin de semana |
| Weibull k | K Weibull |
| Wind data scaled average | Promedio escalado de velocidad de viento |
| Wind power output | Producción de energía eólica |
| Wind resource | Recurso eólico |
| Wind speed | Velocidad de viento |
| Wind turbine | Turbina eólica |
| X | |
| Y | |

Translations by: Arturo Romero Paredes, Ignacio Cruz Cruz

For more information

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6.2 Absolute State of Charge



Absolute State of Charge

The absolute state of charge is the total amount of energy currently contained in the battery bank, measured in kWh. When the batteries are fully charged, the absolute state of charge is equal to the maximum capacity of the battery bank.

State of charge is often abbreviated as SOC.

See also

[Relative state of charge](#)

For more information

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6.3 AC Primary Load Served



AC Primary Load Served

Type: Output Variable

Units: kWh/yr

Symbol: $E_{\text{prim}, \text{AC}}$

The AC primary load served is the total amount of energy that went towards serving the AC primary load(s) during the year.

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6.4 Altitude



Altitude

Type: Input Variable

Units: m

Symbol: z

The altitude is the elevation above mean sea level. Altitude affects air density, which in turn affects wind turbine output. HOMER therefore considers the altitude when calculating the output of the wind turbine.

According to the ideal gas law, air density is given by the following equation:

$$\rho = \frac{P}{RT}$$

where:

r = air density [kg/m³]

P = pressure [Pa]

R = gas constant [287 J/kgK]

T = temperature [K]

The quantity that HOMER uses is the *air density ratio*, which is the actual air density divided by the air density under standard conditions (sea level, 15 degrees Celsius). When calculating the output of the wind turbine at the specified altitude, HOMER multiplies the power output obtained from the wind turbine power curve by the air density ratio. Using the ideal gas law, the air density ratio can be expressed as follows:

$$\frac{\rho}{\rho_0} = \frac{P}{P_0} \left(\frac{T_0}{T} \right)$$

where:

P₀ = standard pressure [101,325 Pa]

T₀ = standard temperature [288.16 K]

Altitude affects both pressure and temperature. The US Standard Atmosphere uses the simplifying assumption that, up to an altitude of 11,000m, temperature decreases linearly with altitude according to the following equation:

$$T = T_0 - Bz$$

where:

B = lapse rate [0.00650 K/m]

z = altitude [m]

Using the assumption that temperature decreases linearly with altitude, the air pressure can be shown to depend on the altitude according to the following equation:

$$P = P_0 \left(1 - \frac{Bz}{T_0} \right)^{g/RB}$$

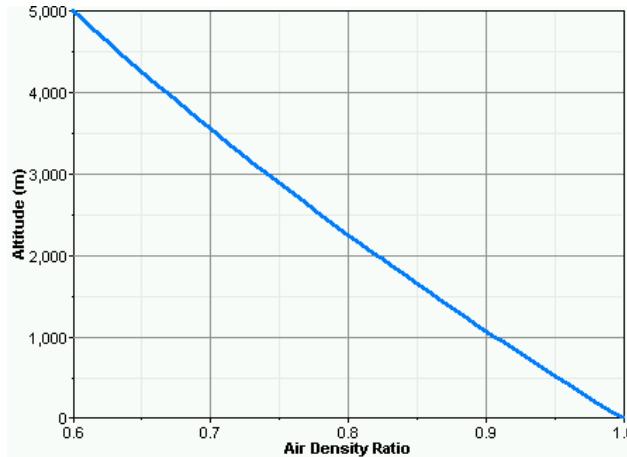
where:

g = gravitational acceleration [9.81 m/s²]

By substituting these equations for P and T into the equation defining the air density ratio, we get the following equation for the air density ratio:

$$\frac{\rho}{\rho_0} = \left(1 - \frac{Bz}{T_0} \right)^{g/RB} \left(\frac{T_0}{T_0 - Bz} \right)$$

On the right hand side of the above equation, only z, the altitude, is not constant. So with the assumptions we have used, the air density ratio is a function of altitude alone. We can use this equation to produce a graph of air density ratio versus altitude, as shown below:



The graph shows that at an altitude of 2000m, the air density ratio is about 0.82, meaning that air at that altitude is 82% as dense as air at standard temperature and pressure.

See also:

[Calculating the output of a wind turbine](#)

For more information

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6.5 Anemometer Height



Anemometer Height

Type: Input Variable

Units: m

Symbol: z_{anem}

The anemometer height is the height above ground at which the wind speed data are measured. Wind speeds tend to increase with height above ground, so if the wind turbine hub height is not the same as the anemometer height, HOMER adjusts the wind speed data accordingly. A common anemometer height for meteorological measurements is 10m. Anemometers installed specifically to determine wind power potential are often placed higher than 10m, since wind turbine towers are typically between 25m and 100m in height. The closer the anemometer is placed to the eventual hub height of the wind turbine, the more accurately it measures the wind resource to which the wind turbine will be exposed.

For details on how HOMER calculates the wind speed at the hub height of the wind turbine, see [Wind shear inputs](#).

See also:

[Wind shear inputs](#)

[Wind turbine hub height](#)

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6.6 Annualized Cost

Annualized Cost

The annualized cost of a component is the cost that, if it were to occur equally in every year of the project lifetime, would give the same net present cost as the actual cash flow sequence associated with that component.

HOMER calculates annualized cost by first calculating the net present cost, then multiplying it by the capital recovery factor, as in the following equation:

$$C_{ann} = CRF(i, R_{proj}) \cdot C_{NPC}$$

where:

C_{NPC} = the [net present cost](#) [\$]

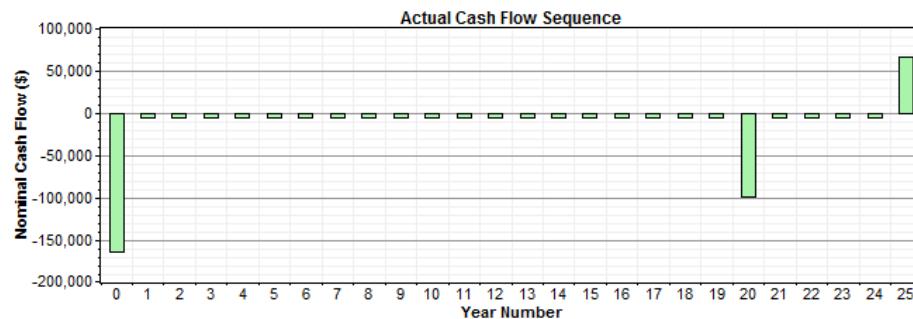
i = the [annual real interest rate](#) [%]

R_{proj} = the [project lifetime](#) [yr]

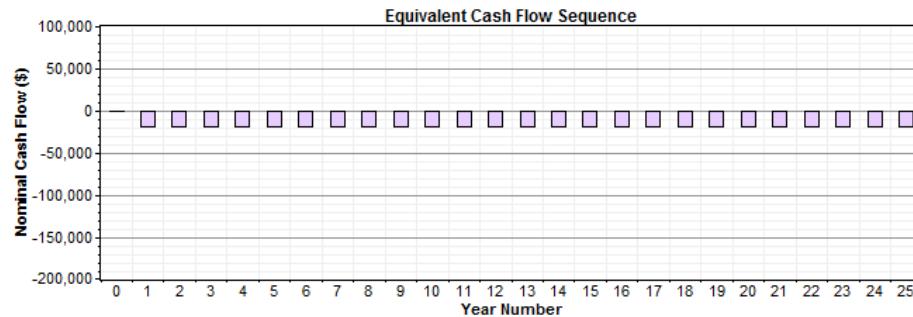
$CRF()$ = a function returning the [capital recovery factor](#)

Example: A wind turbine has an initial capital cost of \$165,000, a replacement cost of \$95,000, a lifetime of 20 years, and an operation and maintenance (O&M) cost of \$5,000/yr. What is its annualized cost over a 25-year project lifetime at an annual real interest rate of 6%?

The actual cash flow sequence associated with this wind turbine appears in the graph below. This graph shows the large capital expense in year zero, the small O&M cost that appears in every year, the large replacement cost that occurs after 20 years, and the salvage value that occurs at the end of the project:



We want to calculate an equivalent cash flow sequence, meaning one that gives the same net present cost, in which a single cost occurs in every year of the project. That single cost is the annualized cost, and the equivalent cash flow sequence would look like the one that appears below:



To calculate the net present cost of the wind turbine, we create a cash flow table as shown below. For each year, we calculate the discount factor, the nominal cash flow, and discounted cash flow, which is equal to the nominal cash flow multiplied by the discount factor. The sum of the discounted cash flows is the net present cost of the wind turbine over the project lifetime: \$241,938. We multiply this by the capital recovery factor, which for 25 years and 6% is equal to 0.0782, giving an annualized cost of \$18,926/yr.

Tip: For a complete description of the process of creating a cash flow table, please see the article on the [Cash Flow Details Table](#).

| Year | Discount Factor | Actual Cash Flows | |
|------|-----------------|-------------------|------------|
| | | Nominal | Discounted |
| 0 | 1.000 | -165,000 | -165,000 |
| 1 | 0.943 | -5,000 | -4,717 |
| 2 | 0.890 | -5,000 | -4,450 |
| 3 | 0.840 | -5,000 | -4,198 |
| 4 | 0.792 | -5,000 | -3,960 |
| 5 | 0.747 | -5,000 | -3,736 |
| 6 | 0.705 | -5,000 | -3,525 |
| 7 | 0.665 | -5,000 | -3,325 |
| 8 | 0.627 | -5,000 | -3,137 |
| 9 | 0.592 | -5,000 | -2,959 |

| | | | |
|-------|-------|----------|----------|
| 10 | 0.558 | -5,000 | -2,792 |
| 11 | 0.527 | -5,000 | -2,634 |
| 12 | 0.497 | -5,000 | -2,485 |
| 13 | 0.469 | -5,000 | -2,344 |
| 14 | 0.442 | -5,000 | -2,212 |
| 15 | 0.417 | -5,000 | -2,086 |
| 16 | 0.394 | -5,000 | -1,968 |
| 17 | 0.371 | -5,000 | -1,857 |
| 18 | 0.350 | -5,000 | -1,752 |
| 19 | 0.331 | -5,000 | -1,653 |
| 20 | 0.312 | -100,000 | -31,181 |
| 21 | 0.294 | -5,000 | -1,471 |
| 22 | 0.278 | -5,000 | -1,388 |
| 23 | 0.262 | -5,000 | -1,309 |
| 24 | 0.247 | -5,000 | -1,235 |
| 25 | 0.233 | 66,250 | 15,436 |
| Total | | | -241,938 |

To check our work, we can create a cash flow table for this equivalent cash flow sequence, and verify that it gives the same net present cost. The table below shows that the equivalent cash flow does indeed lead to the correct net present cost.

| Year | Discount Factor | Equivalent Cash Flows | |
|-------|-----------------|-----------------------|------------|
| | | Nominal | Discounted |
| 0 | 1.000 | 0 | 0 |
| 1 | 0.943 | -18,926 | -17,855 |
| 2 | 0.890 | -18,926 | -16,844 |
| 3 | 0.840 | -18,926 | -15,891 |
| 4 | 0.792 | -18,926 | -14,991 |
| 5 | 0.747 | -18,926 | -14,143 |
| 6 | 0.705 | -18,926 | -13,342 |
| 7 | 0.665 | -18,926 | -12,587 |
| 8 | 0.627 | -18,926 | -11,874 |
| 9 | 0.592 | -18,926 | -11,202 |
| 10 | 0.558 | -18,926 | -10,568 |
| 11 | 0.527 | -18,926 | -9,970 |
| 12 | 0.497 | -18,926 | -9,406 |
| 13 | 0.469 | -18,926 | -8,873 |
| 14 | 0.442 | -18,926 | -8,371 |
| 15 | 0.417 | -18,926 | -7,897 |
| 16 | 0.394 | -18,926 | -7,450 |
| 17 | 0.371 | -18,926 | -7,028 |
| 18 | 0.350 | -18,926 | -6,631 |
| 19 | 0.331 | -18,926 | -6,255 |
| 20 | 0.312 | -18,926 | -5,901 |
| 21 | 0.294 | -18,926 | -5,567 |
| 22 | 0.278 | -18,926 | -5,252 |
| 23 | 0.262 | -18,926 | -4,955 |
| 24 | 0.247 | -18,926 | -4,674 |
| 25 | 0.233 | -18,926 | -4,410 |
| Total | | | -241,937 |

The annualized cost serves as a useful metric for comparing the costs of different components because it measures their relative contribution to the total net present cost. It allows for a fair cost comparison between components with low capital and high operating costs (such as diesel generators) and those with high capital and low operating costs (such as PV arrays or wind turbines).

The annualized costs of each system component and of the system as a whole appear on the Cost Summary tab of the Simulation Results window.

See also

[Net present cost](#)

[Discount recovery factor](#)

[Capital recovery factor](#)

[Cash Flow Details table](#)

[Cost Summary tab](#)

[Total annualized cost](#)

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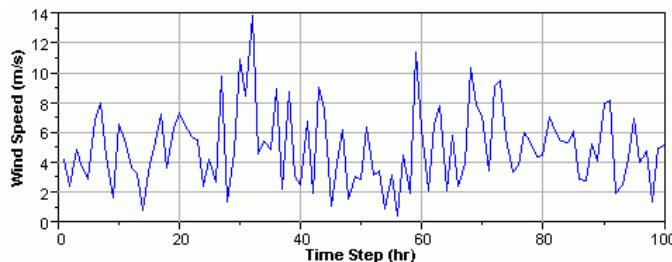
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6.7 Autocorrelation

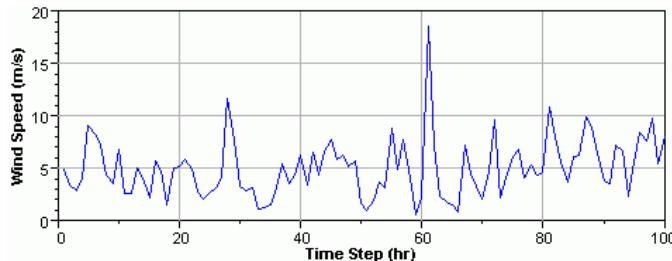


Autocorrelation

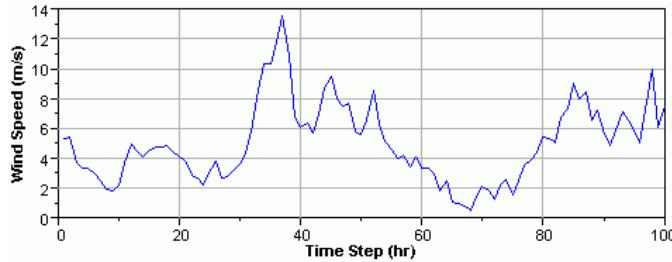
Wind speed time series data typically exhibit autocorrelation, which can be defined as the degree of dependence on preceding values. The effect of autocorrelation is demonstrated in Figure 1. In the absence of autocorrelation, each data point is completely independent of the previous values and the data points jump up and down at random, as in part a) of Figure 1. In a strongly autocorrelated time series, the value in any one time step is strongly influenced by the values in previous time steps, so long periods of high or low values emerge, as in part c) of Figure 1. Note that each data set in Figure 1 has the same average and the same Weibull k value. The degree of autocorrelation is the only distinction between the data sets.



a) Synthetic wind speed time series with no autocorrelation ($r_1 = 0.0$)



b) Synthetic wind speed time series with moderate autocorrelation ($r_1 = 0.5$)



c) Synthetic wind speed time series with strong autocorrelation ($r_1 = 0.96$)

Figure 1: The effect of autocorrelation. All three time series have a mean wind speed of 5 m/s and a Weibull k value of 2.

We know from experience that the wind exhibits autocorrelation. If the wind is blowing strongly at 10 a.m., it is quite likely that it will still be blowing strongly at 11 a.m. But the autocorrelation characteristics of the wind vary from place to place. Before we can explore this any further, we need to learn some fundamentals of autocorrelation.

For a time series $z_1, z_2, z_3, \dots, z_n$, we can define an autocorrelation coefficient r_k as follows:

$$r_k = \frac{\sum_{i=1}^{n-k} (z_i - \bar{z})(z_{i+k} - \bar{z})}{\sum_{i=1}^n (z_i - \bar{z})^2}$$

The value r_k is the autocorrelation between any two time series values separated by a "lag" of k time units. For a particular time series, we can measure r_k for

several values of k . The resulting function is known as the autocorrelation function. By definition, $r_0 = 1$.

The autocorrelation function of the wind data measured at Kotzebue, Alaska is shown in Figure 2. This simple autocorrelation function shows that wind speeds at Kotzebue are strongly autocorrelated at short lags and less strongly autocorrelated at longer lags, which is intuitive.

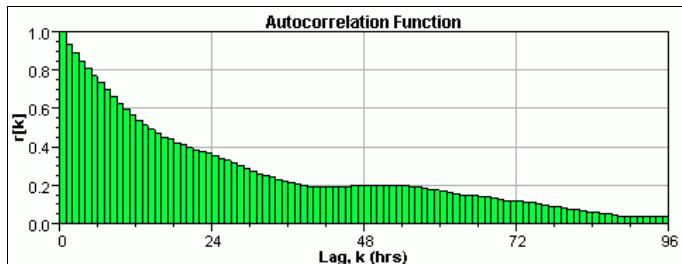


Figure 2: Autocorrelation function for the hourly wind speed data measured at Kotzebue, Alaska.

Kotzebue, however, is an unusual case because there is almost no daily pattern to its wind. A much more common example of a wind speed autocorrelation function is that of San Diego, California, which is shown in Figure 3. The wind speeds at San Diego show a distinct daily pattern, with the afternoons being on average much windier than the mornings. This recurring pattern in the wind speed causes the autocorrelation function to oscillate on a 24 hour period. Since it is usually windy at 3 p.m., the wind speed at 3 p.m. today is strongly autocorrelated with the wind speed at 3 p.m. yesterday, and therefore with the wind speed at 3 p.m. two days ago, etc.

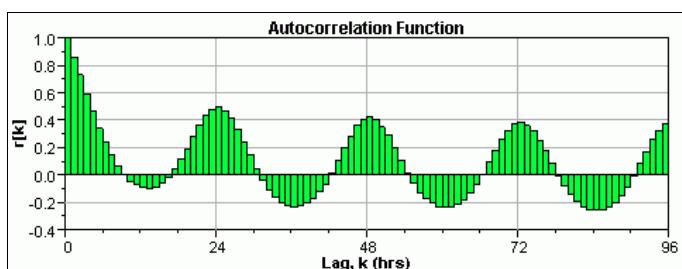


Figure 3: Autocorrelation function for the hourly wind speed data measured at San Diego, California.

HOMER describes the autocorrelation characteristics of wind data with a single number, the autocorrelation factor.

See also

[Autocorrelation factor](#)

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6.8 Available Head



Available Head

Type: Input Variable

Units: m

Symbol: h

The total available vertical drop between the intake and the turbine. Friction losses in the pipeline between the intake and the turbine make the effective head somewhat less than the available head.

HOMER uses the available head to calculate the nominal hydro power and the effective head. It uses the effective head to calculate the power output of the hydro turbine.

See also

[Effective head](#)

[Nominal hydro power](#)[Calculating hydro power output](#)

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6.9 Battery Bank Autonomy



Battery Bank Autonomy

Type: Output Variable

Units: hr

Symbol: A_{batt}

The battery bank autonomy is the ratio of the battery bank size to the electric load. HOMER calculates the battery bank autonomy using the following equation:

$$A_{batt} = \frac{N_{batt} V_{nom} Q_{nom} \left(1 - \frac{q_{min}}{100}\right) (24 h/d)}{L_{prim,ave} (1000 Wh/kWh)}$$

where:

- N_{batt} = number of batteries in the battery bank
- V_{nom} = nominal voltage of a single battery [V]
- Q_{nom} = nominal capacity of a single battery [Ah]
- q_{min} = minimum state of charge of the battery bank [%]
- $L_{prim,ave}$ = average primary load [kWh/d]

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6.10 Battery Bank Life



Battery Bank Life

Type: Output Variable

Units: years

Symbol: R_{batt}

In HOMER, two independent factors may limit the lifetime of the battery bank: the lifetime throughput and the battery float life. In other words, batteries can die either from use or from old age. When you create a new battery, you can choose whether the battery lifetime is limited by time, throughput, or both.

HOMER calculates the battery bank life using the following equation:

$$R_{batt} = \begin{cases} \frac{N_{batt} \cdot Q_{lifetime}}{Q_{thrpt}} & \text{if limited by throughput} \\ R_{batt,f} & \text{if limited by time} \\ \text{MIN}\left(\frac{N_{batt} \cdot Q_{lifetime}}{Q_{thrpt}}, R_{batt,f}\right) & \text{if limited by throughput and time} \end{cases}$$

where:

R_{batt} = battery bank life [yr]

N_{batt} = number of batteries in the battery bank

$Q_{lifetime}$ = [lifetime throughput](#) of a single battery [kWh]

Q_{thrpt} = [annual battery throughput](#) [kWh/yr]

$R_{batt,f}$ = [battery float life](#) [yr]

See also

[Create New Battery window](#)

[Battery lifetime throughput](#)

[Battery float life](#)

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6.11 Battery Charge Efficiency



Battery Charge Efficiency

HOMER assumes the battery charge efficiency is equal to the square root of the battery round trip efficiency, hence:

$$\eta_{batt,c} = \sqrt{\eta_{batt,rt}}$$

where:

$\eta_{batt,c}$ = battery charge efficiency, and

$\eta_{batt,rt}$ = [battery round trip efficiency](#).

See also

[Battery discharge efficiency](#)

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6.12 Battery Discharge Efficiency



Battery Discharge Efficiency

HOMER assumes the battery discharge efficiency is equal to the square root of the battery round trip efficiency, hence:

$$\eta_{batt,d} = \sqrt{\eta_{batt,rt}}$$

where:

$\eta_{batt,d}$ = battery discharge efficiency, and

$\eta_{batt,rt}$ = [battery round trip efficiency](#).

See also

[Battery charge efficiency](#)

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6.13 Battery Energy Cost



Battery Energy Cost

Type: Intermediate Variable

Units: \$/kWh

Symbol: $c_{be,n}$

In any time step, the battery energy cost is the average cost of the energy that the system has put into the battery bank up until that time step. HOMER uses the following equation to calculate the battery energy cost in each time step:

$$c_{be,n} = \frac{\sum_{i=1}^{n-1} C_{cc,i}}{\sum_{i=1}^{n-1} E_{cc,i}}$$

[\$]

where:

$c_{be,n}$ = the battery energy cost in time step n [\$/kWh]

$C_{cc,i}$ = the cost of cycle charging the battery in time step i

$E_{bc,i}$ = the amount of energy that went into the battery bank in time step i [kWh]

The battery energy cost reflects the average cost that the system has incurred for *deliberately* charging the battery bank. The "cost of cycle charging," which appears in the numerator of the above equation, is the extra cost incurred by the system specifically for charging the battery. Excess electricity that charges the battery bank in some time step represents no such cost. But if the generator produced more power than required to serve the load, and it did so specifically to charge the battery, then that act of charging the battery bank does cause the system to incur extra cost. The same is true if the system purchases extra grid power expressly to charge the battery. Such events occur routinely under the cycle charging strategy.

In any time step in which a generator or the grid cycle charges the battery, HOMER calculates the cycle charge cost by taking the actual cost of operating the system in that time step and subtracting the cost that would have occurred in that time step had the system not charged the battery.

The battery energy cost will always be zero under the load following dispatch strategy, because under load following the system never pays to charge the battery bank, it only uses excess electricity to charge the battery bank.

The battery bank's marginal cost of generation is equal to the sum of the battery wear cost and the battery energy cost.

See also

[Battery wear cost](#)

[Cycle charging strategy](#)

[Load following strategy](#)

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6.14 Battery Float Life



Battery Float Life

Type: Input Variable

Units: yr

Symbol: $R_{batt,f}$

The float life of the battery is the length of time that the battery will last before it needs replacement. When you create a battery you can choose whether to limit its life by time, by throughput, or by both. The float life does not apply if you have chosen to limit the battery lifetime by throughput only.

HOMER uses the float life to calculate the [battery bank life](#).

See also

[Battery lifetime throughput](#)

[Battery bank life](#)

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6.15 Battery Maximum Charge Rate



Battery Maximum Charge Rate

Type: Input Variable

Units: A/Ah of unfilled capacity

Symbol: a_c

The maximum charge rate variable imposes a limit on the rate at which the system can charge the battery bank. That limit is directly proportional to the amount of "unfilled capacity" in the battery, where the unfilled capacity is defined as the battery's maximum capacity minus its current absolute state of charge.

For example, consider a battery whose maximum capacity is 350 Ah and whose maximum charge rate is 0.4 A/Ah. If at some point in time the battery's absolute state of charge is 310 Ah, then it has 40 Ah of unfilled capacity, so the highest charge current it could accept would be $40 \text{ Ah} * 0.4 \text{ A/Ah} = 16 \text{ A}$. If at some other point in time its state of charge was 335 Ah, then the highest charge current it could accept would be only 6 A. So the allowable charge current decreases with increasing state of charge.

Another variable, the maximum charge current, imposes an upper limit on the allowable charge current, regardless of the state of charge. If our example battery were empty, the maximum charge rate variable would imply that it could accept a charge current of as high as $350 \text{ Ah} * 0.4 \text{ A/Ah} = 140 \text{ A}$. But a current that high might be very damaging to the battery. If you set the maximum charge current variable to 25 A, then HOMER ensures that the charge current never exceeds 25 A, no matter what the state of charge.

Notes:

1. The [kinetic battery model](#) imposes a separate limit on the rate of charge.
2. This discussion relates to a single battery. To find the maximum battery charge power, HOMER calculates the product of the maximum charge current times the nominal voltage times the number of batteries in the battery bank.

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6.16 Battery Minimum State Of Charge



Battery Minimum State Of Charge

Type: Input Variable

Units: %

Symbol: q_{min}

The [relative state of charge](#) below which the battery bank is never drawn - specified as a percentage of the total capacity. Most rechargeable batteries are not meant to be fully discharged. In fact, fully discharging some batteries can permanently damage them. The minimum state of charge is typically set to 30-50% in order to avoid damaging the battery bank by excessive discharge.

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6.17 Battery Roundtrip Efficiency



Battery Roundtrip Efficiency

Type: Input Variable

Units: %

Symbol: $h_{batt,rt}$

The round trip DC-to-storage-to-DC energetic efficiency of the battery bank, or the fraction of energy put into the battery that can be retrieved. Typically this is about 80%. HOMER assumes the battery charge efficiency and the battery discharge efficiency are both equal to the square root of the roundtrip efficiency.

See also

[Battery charge efficiency](#)

[Battery discharge efficiency](#)

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6.18 Battery Throughput



Battery Throughput

Type: Output Variable

Units: kWh/yr

Symbol: Q_{thrt}

The battery throughput is the amount of energy that cycles through the battery bank in one year. Throughput is defined as the change in energy level of the battery bank, measured after charging losses and before discharging losses. This value is used to calculate the [life of the battery bank](#).

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6.19 Battery Wear Cost



Battery Wear Cost

Type: Intermediate Variable

Units: \$/kWh

Symbol: c_{bw}

The battery wear cost is the cost of cycling energy through the battery bank. If the battery properties indicate that the battery life is limited by throughput, then HOMER assumes the battery bank will require replacement once its total throughput equals its lifetime throughput. Each kWh of throughput therefore brings the battery bank that much closer to needing replacement. HOMER calculates the battery wear cost using the following equation:

$$c_{bw} = \frac{C_{rep,batt}}{N_{batt} \cdot Q_{\text{lifetime}} \cdot \sqrt{\eta_r}}$$

where:

$C_{rep,batt}$ = replacement cost of the battery bank [\$]

N_{batt} = the number of batteries in the battery bank

Q_{lifetime} = the [lifetime throughput](#) of a single battery [kWh]

η_r = [battery roundtrip efficiency](#) [fractional]

The battery bank's marginal cost of generation is equal to the sum of the battery wear cost and the battery energy cost.

See also

[Battery energy cost](#)

[Cycle charging strategy](#)

[Load following strategy](#)

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6.20 Biogas (PRO)

Biogas



In HOMER, the term *biogas* refers to gasified biomass. Biomass feedstock (such as wood waste, agricultural residue, or energy crops) can be gasified by thermo-chemical or biological processes, and the product may be called one of several different names, including synthesis gas, syngas, producer gas, and wood gas.

Whatever the feedstock and the means of gasification, the major constituent gases of biogas are typically carbon monoxide, hydrogen, and carbon dioxide, plus a significant amount of nitrogen (about 50% by weight) if thermal gasification is performed in the presence of air. Minor constituent gases include methane and water vapor.

Biogas typically has a low heating value compared with fossil fuels, particularly if it contains a large amount of nitrogen, which is noncombustible. But it has several advantages over solid biomass, including cleaner combustion, higher efficiency, and better control.

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6.21 Biomass Carbon Content (PRO)



Biomass Carbon Content P

Type: Input Variable

Units: %

Symbol: k_{bio}

The amount of carbon contained in the biomass feedstock, expressed as a mass-based percentage. HOMER uses this value to calculate the emissions of CO₂, CO, and unburned hydrocarbons.

Tip: if you want HOMER to calculate the system's *gross* carbon emissions, then you should enter the gross carbon content of the biomass feedstock, which is typically on the order of 50%. On the other hand, if you want HOMER to calculate the system's *net* carbon emissions, then you should enter the net carbon content of the feedstock, which is typically near zero. The net value takes into account the fact that the carbon in the biomass feedstock was originally absorbed from the atmosphere, and consuming that feedstock as fuel simply puts that carbon back into the atmosphere. The net effect on the atmosphere is near zero if the feedstock is harvested in a sustainable manner, meaning that the rate of consumption of biomass feedstock does not exceed the biosphere's ability to regenerate that feedstock.

A precise estimate of the net carbon content of a biomass feedstock will take into account the carbon emissions associated with the harvesting and processing of the feedstock. It may also account for avoided methane emissions related to the natural decomposition of the feedstock that would have occurred were it not for the consumption of that feedstock to produce energy.

See also:

[How HOMER calculates emissions](#)

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6.22 Biomass Gasification Ratio (PRO)



Biomass Gasification Ratio P

Type: Input Variable
Units: kg gas / kg biomass
Symbol: f_{gas}

The ratio of [biogas](#) generated to biomass feedstock consumed in the gasifier. HOMER assumes this value is constant.

For more information, see the article [Operation of a Cofired Generator](#).

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6.23 Biomass Resource Cost (PRO)



Biomass Resource Cost P

Type: Input Variable
Units: \$/t
Symbol: c_{bio}

The cost per tonne (1000 kg) of biomass feedstock.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

[HOMER online](#) contains the latest information on model updates, as well as sample files, resource data, and contact information.

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6.24 Biomass Substitution Ratio (PRO)



Biomass Substitution Ratio P

Type: Input Variable
Units: none
Symbol: z_{gas}

The ratio with which the [biogas](#) replaces fossil fuel in a cofired generator. If 8 kg/hr of biogas is required to replace 1 kg/hr of fossil fuel to maintain output power, the substitution ratio is 8. This ratio is assumed to be constant, independent of fuel mixture or output power.

If the fossil fuel burned by the generator is gaseous, the substitution ratio will be roughly equal to the ratio of the lower heating values of the fossil fuel and biogas. For example, if the cofired generator runs on a mixture of propane and biogas and the LHV of the biogas is one-third that of propane, the substitution ratio will likely be approximately 3.

For liquid fossil fuels, the substitution ratio is typically somewhat higher than the LHV ratio because the generator does not operate as efficiently on the mixture of biogas and liquid fuel as it would on liquid fuel alone.

For more information, see the article [Operation of a Cofired Generator](#).

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

6.25 Boiler Marginal Cost (PRO)



Boiler Marginal Cost

Type: Intermediate Variable

Units: \$/kWh

Symbol: c_{boiler}

The marginal cost of thermal energy from the boiler. HOMER uses this value when calculating the [levelized cost of energy](#). HOMER calculates the boiler marginal cost with the following equation:

$$c_{boiler} = \frac{3.6 \cdot (c_{fuel} + c_{boiler,emissions})}{\eta_{boiler} \cdot LHV_{fuel}}$$

where:

c_{fuel} = cost of fuel [\$/kg of fuel]

$c_{boiler,emissions}$ = cost penalty associated with emissions from the boiler [\$/kg of fuel]

η_{boiler} = boiler efficiency [unitless]

LHV_{fuel} = the lower heating value of the boiler fuel [MJ/kg]

The factor of 3.6 in the above equation arises because 1 kWh = 3.6 MJ.

Note: The fuel cost in the above equation is per kg, not per L or m³. For fuels denominated in volumetric units, HOMER calculates the cost per kg using the fuel density.

HOMER calculates the cost penalty associated with boiler emissions using the following equation:

$$c_{boiler,emissions} = \frac{c_{CO_2}\gamma_{CO_2} + c_{CO}\gamma_{CO} + c_{UHC}\gamma_{UHC} + c_{PM}\gamma_{PM} + c_{SO_2}\gamma_{SO_2} + c_{NO_x}\gamma_{NO_x}}{1000}$$

where:

c_{CO_2} = penalty for emissions of CO₂ [\$/t]

c_{CO} = penalty for emissions of CO [\$/t]

c_{UHC} = penalty for emissions of unburned hydrocarbons (UHC) [\$/t]

c_{PM} = penalty for emissions of particulate matter (PM) [\$/t]

c_{SO_2} = penalty for emissions of SO₂ [\$/t]

c_{NO_x} = penalty for emissions of NO_x [\$/t]

γ_{CO_2} = boiler's carbon dioxide emissions coefficient [kg CO₂ / kg fuel]

γ_{CO} = boiler's carbon monoxide emissions coefficient [kg CO / kg fuel]

γ_{UHC} = boiler's unburned hydrocarbons emissions coefficient [kg UHC / kg fuel]

γ_{PM} = boiler's particulate matter emissions coefficient [kg PM / kg fuel]

γ_{SO_2} = boiler's SO₂ emissions coefficient [kg SO₂ / kg fuel]

γ_{NO_x} = boiler's NO_x emissions coefficient [kg NO_x / kg fuel]

HOMER calculates the CO₂ emissions coefficient using the following equation:

$$\gamma_{CO_2} = \frac{44}{12} \left[f_{C,fuel}(1 - \gamma_{UHC}) - \left(\frac{12}{28} \right) \gamma_{CO} \right]$$

where:

$f_{C,fuel}$ = the carbon content of the fuel [unitless]

γ_{CO} = boiler's carbon monoxide emissions coefficient [kg CO / kg fuel]

γ_{UHC} = boiler's unburned hydrocarbons emissions coefficient [kg UHC / kg fuel]

Note that the factors of 44/12 and 12/28 in the above equation arise because the molecular weights of C, CO, and CO₂ are equal to 12, 28, and 44 respectively.

HOMER calculates the SO₂ emissions coefficient using the following equation:

$$\gamma_{SO_2} = 2 f_{S,fuel} (1 - \gamma_{UHC} - x_{PM})$$

where:

$f_{S,fuel}$ = the sulfur content of the fuel [unitless]

γ_{UHC} = boiler's unburned hydrocarbons emissions coefficient [kg UHC / kg fuel]

x_{PM} = the proportion of fuel sulfur converted to particulate matter [unitless]

Note that the factor of 2 in the above equation arises because the molecular weight of SO₂ (64) is twice that of S (32).

See also:

[Levelized cost of energy](#)

For more information

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6.26 Breakeven Grid Extension Distance (PRO)



Breakeven Grid Extension Distance

Type: Output Variable

Units: km

Symbol: D_{grid}

The distance from the grid which makes the net present cost of extending the grid equal to the net present cost of the stand-alone system. Farther away from the grid, the stand-alone system is optimal. Nearer to the grid, grid extension is optimal.

HOMER calculates the breakeven grid extension distance using the following equation:

$$D_{grid} = \frac{C_{NPC} \cdot CRF(i, R_{proj}) - c_{power} \cdot E_{demand}}{c_{cap} \cdot CRF(i, R_{proj}) + c_{om}}$$

where:

C_{NPC} = [total net present cost](#) of the stand-alone power system [\$]

CRF() = [capital recovery factor](#)

i = [interest rate](#) [%]

R_{proj} = [project lifetime](#) [yr]

E_{demand} = total annual electrical demand (primary plus deferrable) [kWh/yr]

c_{power} = cost of power from the grid [\$/kWh]

c_{cap} = capital cost of grid extension [\$/km]

c_{om} = O&M cost of grid extension [\$/yr/km]

For more information

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6.27 Capacity Shortage



Capacity Shortage

An capacity shortage is a shortfall that occurs between the [required operating capacity](#) and the actual amount of operating capacity the system can provide. HOMER keeps track of such shortages and calculates the total amount that occurs over the year.

For example, consider a simple system consisting of a 50 kW AC generator serving an AC load:

- If the load is 30 kW and the required operating reserve is 15 kW, the required operating capacity is 45 kW and the actual operating capacity is 50 kW, so there is no capacity shortage. The generator would operate at 30 kW to meet the load, and the 20 kW of operating reserve it provides would satisfy the requirement.
- If the load is 40 kW and the required operating reserve is 12 kW, the required operating capacity is 52 kW and the actual operating capacity is 50 kW, so the capacity shortage is 2 kW. The generator provides only 10 kW of operating reserve in this situation, not enough to satisfy the requirement.
- If the load is 55 kW and the required operating reserve is 0 kW, the required operating capacity is 55 kW and the actual operating capacity is 50 kW, so the capacity shortage is 5 kW (and the unmet load is also 5 kW).
- If the load is 55 kW and the required operating reserve is 20 kW, the required operating capacity is 75 kW and the actual operating capacity is 50 kW, so the capacity shortage is 25 kW (and the unmet load is 5 kW).

See also:

[Required operating reserve](#)

[Maximum annual capacity shortage](#)

[Total capacity shortage](#)

[Capacity shortage fraction](#)

For more information

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6.28 Capacity Shortage Fraction



Capacity Shortage Fraction

Type: Output Variable

Units: none

Symbol: f_{cs}

The capacity shortage fraction is equal to the total capacity shortage divided by the total electrical demand. HOMER considers a system feasible (or acceptable) only if the capacity shortage fraction is less than or equal to the [maximum annual capacity shortage](#). HOMER uses the following equation to calculate the capacity shortage fraction:

$$f_{cs} = \frac{E_{cs}}{E_{demand}}$$

where:

E_{cs} = [total capacity shortage](#) [kWh/yr]

E_{demand} = total electrical demand (primary and deferrable load) [kWh/yr]

For more information

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6.29 Capacity Shortage Penalty



Capacity Shortage Penalty

Type: Input Variable

Units: \$/kWh

Symbol: c_{cs}

The capacity shortage penalty is a cost penalty that HOMER applies to the system for any [capacity shortage](#) that occurs during the year. HOMER uses this value to calculate the [other O&M cost](#).

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6.30 Capital Recovery Factor



Capital Recovery Factor

The capital recovery factor is a ratio used to calculate the [present value](#) of an annuity (a series of equal annual cash flows). The equation for the capital recovery factor is:

$$CRF(i, N) = \frac{i(1+i)^N}{(1+i)^N - 1}$$

where:

i = [real interest rate](#)

N = number of years

Example: for i = 7% and N = 5 years, the capital recovery factor is equal to 0.2439. A \$1000 loan at 7% interest could therefore be paid back with 5 annual payments of \$243.90. The [present value](#) of the five annual payments of \$243.90 is \$1000.

See also

[Sinking fund factor](#)

For more information

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6.31 How HOMER Calculates the PV Cell Temperature



How HOMER Calculates the PV Cell Temperature

The PV cell temperature is the temperature of the surface of the PV array. During the night it is the same as the ambient temperature, but in full sun the cell

temperature can exceed the ambient temperature by 30°C or more.

If in the PV Array inputs window you choose to consider the effect of temperature on the PV array, then HOMER will calculate the cell temperature in each time step, and use that in calculating the power output of the PV array. This article describes how HOMER calculates the cell temperature from the ambient temperature and the radiation striking the array.

We start by defining an energy balance for the PV array, using the following equation from [Duffie and Beckman \(1991\)](#):

$$\tau\alpha G_T = \eta_c G_T + U_L (T_c - T_a)$$

where:

τ is the [solar transmittance](#) of any cover over the PV array [%]

α is the [solar absorptance](#) of the PV array [%]

G_T is the solar radiation striking the PV array [kW/m²]

η_c is the electrical conversion efficiency of the PV array [%]

U_L is the coefficient of heat transfer to the surroundings [kW/m²°C]

T_c is the PV cell temperature [°C]

T_a is the ambient temperature [°C]

The above equation states that a balance exists between, on one hand, the solar energy absorbed by the PV array, and on the other hand, the electrical output plus the heat transfer to the surroundings. We can solve that equation for cell temperature to yield:

$$T_c = T_a + G_T \left(\frac{\tau\alpha}{U_L} \right) \left(1 - \frac{\eta_c}{\tau\alpha} \right)$$

It is difficult to measure the value of $(\tau\alpha / U_L)$ directly, so instead manufacturers report the nominal operating cell temperature (NOCT), which is defined as the cell temperature that results at an incident radiation of 0.8 kW/m², an ambient temperature of 20°C, and no load operation (meaning $\eta_c = 0$). We can substitute these values into the above equation and solve it for $\tau\alpha/U_L$ to yield the following equation:

$$\frac{\tau\alpha}{U_L} = \frac{T_{c,NOCT} - T_{a,NOCT}}{G_{T,NOCT}}$$

where:

$T_{c,NOCT}$ is the [nominal operating cell temperature](#) [°C]

$T_{a,NOCT}$ is the ambient temperature at which the NOCT is defined [20°C]

$G_{T,NOCT}$ is the solar radiation at which the NOCT is defined [0.8 kW/m²]

If we assume that $\tau\alpha/U_L$ is constant, we can substitute this equation into the cell temperature equation to yield:

$$T_c = T_a + G_T \left(\frac{T_{c,NOCT} - T_{a,NOCT}}{G_{T,NOCT}} \right) \left(1 - \frac{\eta_c}{\tau\alpha} \right)$$

HOMER assumes a value of 0.9 for $\tau\alpha$ in the above equation, as [Duffie and Beckman \(1991\)](#) suggest. Since the term $\eta_c/\tau\alpha$ is small compared to unity, this assumption does not introduce significant error.

HOMER assumes that the PV array always operates at its maximum power point, as it would if it were controlled by a maximum power point tracker. That means HOMER assumes the cell efficiency is always equal to the maximum power point efficiency:

$$\eta_c = \eta_{mp}$$

where:

η_{mp} is the efficiency of the PV array at its maximum power point [%]

So in the equation for cell temperature we can replace η_c with η_{mp} to yield:

$$T_c = T_a + (T_{c,NOCT} - T_{a,NOCT}) \left(\frac{G_T}{G_{T,NOCT}} \right) \left(1 - \frac{\eta_{mp}}{\tau\alpha} \right)$$

But η_{mp} depends on the cell temperature T_c . HOMER assumes that the efficiency varies linearly with temperature according to the following equation:

$$\eta_{mp} = \eta_{mp,STC} \left[1 + \alpha_p (T_c - T_{c,STC}) \right]$$

where:

$\eta_{mp,STC}$ is the [maximum power point efficiency under standard test conditions](#) [%]

α_p is the [temperature coefficient of power](#) [%/°C]

$T_{c,STC}$ is the cell temperature under [standard test conditions](#) [25°C]

The temperature coefficient of power is normally negative, meaning that the efficiency of the PV array decreases with increasing cell temperature.

We can substitute this efficiency equation into the preceding cell temperature equation and solve for cell temperature to yield:

$$T_c = \frac{T_a + (T_{c,NOCT} - T_{a,NOCT}) \left(\frac{G_T}{G_{T,NOCT}} \right) \left[1 - \frac{\eta_{mp,STC}(1 - \alpha_P T_{c,STC})}{\tau\alpha} \right]}{1 + (T_{c,NOCT} - T_{a,NOCT}) \left(\frac{G_T}{G_{T,NOCT}} \right) \left(\frac{\alpha_P \eta_{mp,STC}}{\tau\alpha} \right)}$$

The temperatures in the above equation must be in Kelvin. HOMER uses this equation to calculate the cell temperature in each time step.

See also

[PV Inputs window](#)

[Standard test conditions](#)

[Nominal operating cell temperature](#)

[How HOMER calculates the radiation incident on the PV array](#)

[How HOMER calculates the PV array power output](#)

[Can HOMER model a maximum power point tracker?](#)

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6.32 Clearness Index



Clearness Index

The clearness index is a measure of the clearness of the atmosphere. It is the fraction of the solar radiation that is transmitted through the atmosphere to strike the surface of the Earth. It is a dimensionless number between 0 and 1, defined as the surface radiation divided by the extraterrestrial radiation. The clearness index has a high value under clear, sunny conditions, and a low value under cloudy conditions.

The clearness index can be defined on an instantaneous, hourly, or monthly basis. The clearness index values in HOMER's Solar Resource Inputs window are monthly average values. The symbol for the monthly average clearness index is K_t .

Typical values of K_t range from 0.25 (a very cloudy month, such as an average December in London) to 0.75 (a very sunny month, such as an average June in Phoenix).

The [table of solar data](#) contains monthly average clearness indices for numerous locations around the world.

See also

[How HOMER calculates clearness index](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.33 CO Emissions Penalty (PRO)



CO Emissions Penalty

Type: Input Variable

Units: \$/t

Symbol: c_{CO}

Use the CO emissions penalty to penalize systems for their production of carbon monoxide. HOMER uses this input value when calculating the [Other O&M cost](#).

For more information

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6.34 CO₂ Emissions Penalty



CO₂ Emissions Penalty

Type: Input Variable

Units: \$/t

Symbol: c_{CO_2}

Use the CO₂ emissions penalty to penalize systems for their production of carbon dioxide. HOMER uses this input value when calculating the [Other O&M cost](#).

For more information

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6.35 Component



Component

In HOMER, the term "component" refers to any part of the system that generates, stores or transfers electric or thermal energy, and whose size or quantity is an optimization variable.

Photovoltaic panels, diesel generators and wind turbines are examples of components. Less obvious are things like converters, electrolyzers and the utility grid.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.36 Component Library

Component Library

The component library is a collection of properties of batteries, flywheels, wind turbines, and fuels. Wherever you need to select a type of battery, flywheel, wind turbine, or fuel, HOMER uses the component library to generate a list of available types. In the example shown below, taken from the Wind Turbine Inputs window, HOMER is displaying a list of the wind turbine types contained in the component library.

| Description | Value |
|--------------|--------------|
| Abbreviation | G10 |
| Manufacturer | |
| Name | Generic 10kW |
| Notes | |
| Url | |
| Website | |

| Parameter | Value |
|-------------------------------|-------------------------------------|
| AC | <input checked="" type="checkbox"/> |
| Availability Losses | 0 |
| Capacity | 10 |
| Consider Maintenance Schedule | <input type="checkbox"/> |
| Consider Temperature Effect | <input type="checkbox"/> |
| Curtailment Losses | n |

You can add and remove items from the component library using the New and Delete buttons on the battery, flywheel, wind turbine, generator, and boiler windows.

Note that the component library contains performance data, but no cost data.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.37 Cycle Charging Strategy

Cycle Charging Strategy

The cycle charging strategy is a [dispatch strategy](#) whereby whenever a generator needs to operate to serve the primary load, it operates at full output power. Surplus electrical production goes toward the lower-priority objectives such as, in order of decreasing priority: serving the [deferrable load](#), charging the battery bank, and serving the electrolyzer.

Note: A generator will not produce surplus power just to dump it as [excess electricity](#). There must be some use for its surplus power for HOMER to operate it above the level needed to serve the primary load.

When using the cycle charging strategy, HOMER dispatches the controllable power sources (generators, battery bank, grid) each time step of the simulation in a two-step process. First, HOMER selects the optimal combination of power sources to serve the primary and thermal load according to the [load-following strategy](#). Then HOMER ramps up the output of each generator in that optimal combination to its rated capacity, or as close as possible without causing [excess electricity](#).

If a [setpoint state of charge](#) is applied to the cycle charging strategy, then when the battery state of charge is below the setpoint and the battery was not discharging in the previous time step, HOMER will avoid discharging the battery in this time step. A generator will likely be called upon to serve the primary load and produce excess electricity to charge the battery bank. So once the system starts charging the battery bank it continues to do so until it reaches the setpoint state of charge.

See also

[Load following strategy](#)

[Setpoint state of charge](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.38 DC Primary Load Served



DC Primary Load Served

Type: Output Variable

Units: kWh/yr

Symbol: E_{prim} , DC

The DC primary load served is the total amount of energy that went towards serving the DC primary load(s) during the year.

For more information

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6.39 Decision Variable



Decision Variable

A decision variable is a variable whose optimal value is determined during the course of the optimization process. An example is the size of the PV array. If you are using [SearchSizer](#), HOMER will automatically determine the optimal values for your PV array size. If you are specifying your own [Search Space](#), HOMER considers each different PV array size you specify and finds the value that results in the least net present cost.

The decision variables in HOMER are:

- the size of the PV array
- the number of wind turbines
- the size of the hydro system
- the size of each generator
- the number of batteries
- the size of the converter
- the size of the electrolyzer
- the size of the hydrogen storage tank
- the dispatch strategy
- the maximum grid demand

Decision variables are also known as *optimization variables*.

For more information

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6.40 Deferrable Load Served (PRO)



Deferrable Load Served P

Type: Output Variable

Units: kWh/yr

Symbol: E_{def}

The deferrable load served is the total amount of energy that went towards serving the deferrable load during the year.

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6.41 Deltaplot



Deltaplot

The deltaplot shows the frequency of changes in any variable over some length of time. Choose the variable from the drop-down box, and choose the length of time using the slider control.

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6.42 Design Flow Rate (PRO)



Design Flow Rate P

Type: Input Variable

Units: L/s

Symbol: \dot{Q}_{design}

The design flow rate is the flow rate for which the hydro turbine is designed. This is also typically the flow rate at which the turbine operates at its maximum efficiency, although HOMER assumes the turbine efficiency is constant.

HOMER uses the design flow rate to calculate the [hydro turbine flow rate](#) and the [nominal hydro power](#).

See also

[Minimum flow rate](#)

[Maximum flow rate](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.43 Discount Factor



Discount Factor

The discount factor is a ratio used to calculate the present value of a cash flow that occurs in any year of the project lifetime. HOMER calculates the discount factor using the following equation:

$$f_d = \frac{1}{(1+i)^N}$$

where:

i = [real interest rate](#) [%]

N = number of years

Example: for i = 5% and N = 12 years, the discount factor equals 0.557. That means a \$1000 nominal cash flow in year 12 has a present value of \$557. In other words, a \$1000 cash flow in year 12 is equivalent to a \$557 cash flow in year zero. This is a demonstration of the time value of money: a dollar now is worth more than a dollar twelve years in the future.

See also

[Present value](#)

For more information

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6.44 Dispatch Strategy



Dispatch Strategy

A *dispatch strategy* is a set of rules used to control the operation of the generator(s) and the battery bank whenever there is insufficient renewable energy to supply the load. See [Barley and Winn, 1996](#) for a complete discussion of hybrid system dispatch strategies.

See also

[System Control Inputs](#)

For more information

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6.45 Diurnal Pattern Strength



Diurnal Pattern Strength

Type: Input Variable

Units: none

Symbol: d

Typical Range: 0.0 - 0.4

The diurnal pattern strength is a number between 0 and 1 that reflects how strongly the wind speed tends to depend on the time of day. When you generate synthetic wind speed data, HOMER assumes a sinusoidal diurnal pattern, with the diurnal pattern strength defined as the ratio of the amplitude to the mean.

The following equation describes the average diurnal profile of the synthesized wind speed data:

$$U_i = \bar{U} \left\{ 1 + \delta \cos \left[\left(\frac{2\pi}{24} \right) (i - \phi) \right] \right\} \quad \text{for } i = 1, 2, \dots, 24$$

where:

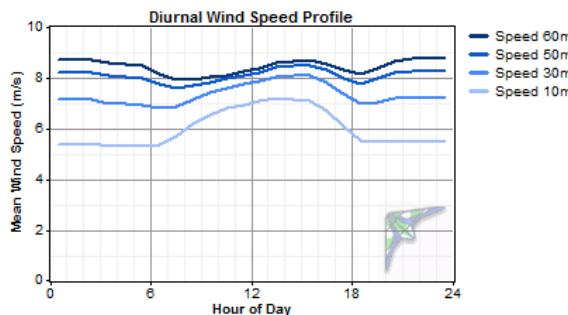
U_i = the mean wind speed in hour i [m/s]

\bar{U} = the overall mean wind speed [m/s]

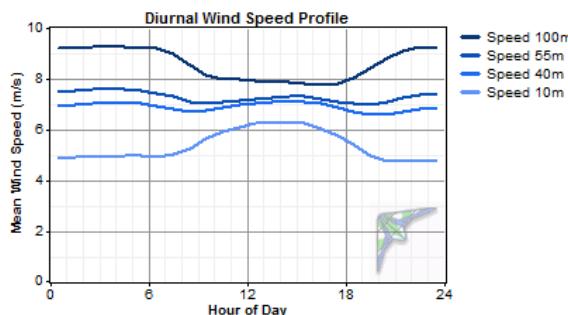
d = diurnal pattern strength (a number between 0 and 1)

f = [hour of peak windspeed](#) (an integer between 1 and 24)

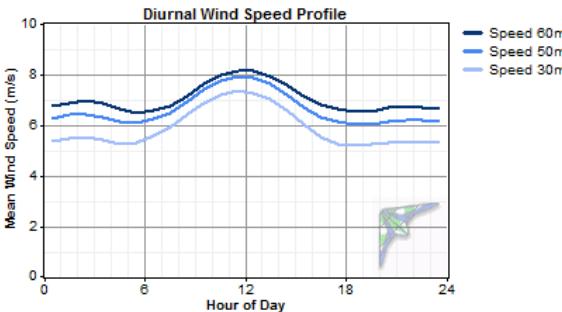
Note that the character of the diurnal pattern tends to vary significantly with height above ground. The following graph shows a typical example, where at 10m above ground the wind speed tends to peak in the afternoon, whereas at 60m above ground, the wind speed tends to peak overnight. This graph shows data measured at a site in the Midwest region of the US:



This pattern can be very pronounced, such as in the following graph, which shows mean diurnal profiles at heights from 10m to 100m above ground, at a location in the Great Plains region of the US. In this example, the diurnal pattern at 100m is almost the mirror image of that at 10m above ground:

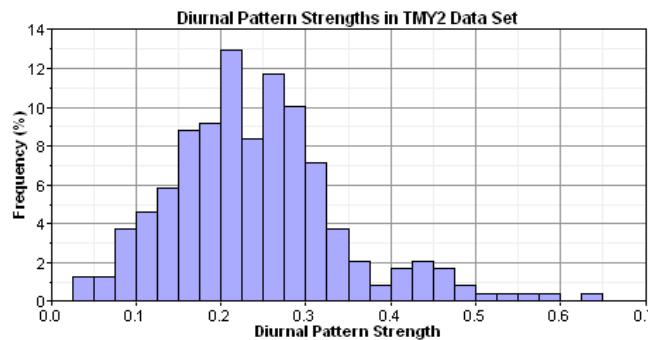


In other cases, the diurnal pattern changes much less with height above ground, such as in the following graph:



Since HOMER will use the wind speeds to estimate wind turbine power output, you want the wind speed data to reflect, as closely as possible, the conditions at the hub height of the wind turbine. So consider the height above ground when you specify the diurnal pattern strength and the hour of peak wind speed.

To measure the diurnal pattern strength from time series wind speed data, one can calculate the average diurnal profile and perform a curve fit operation to find the best-fit value of the hour of peak wind speed and the diurnal pattern strength. We performed that process for the 239 weather stations in the U.S. National Solar Radiation Data Base, which record wind speeds at 10m above ground. The histogram below shows the distribution of the diurnal pattern strength values that we measured. The measured values themselves appear in the [table of measured wind parameters](#).



For more information

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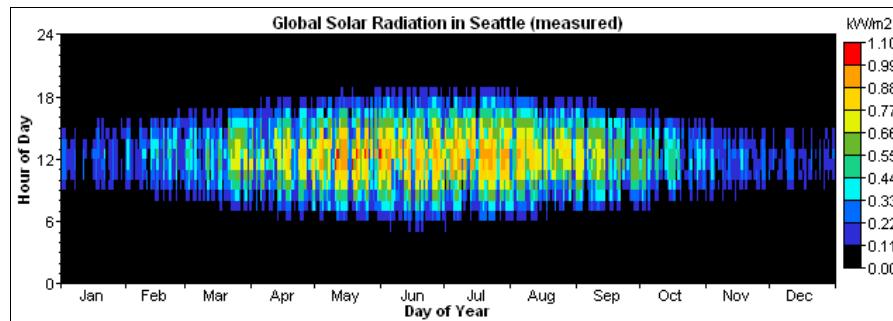
[\[TOP\]](#)

6.46 DMap



DMap

A DMap (data map) is a type of graph showing one year of time series data. With time of day on one axis and day of the year on the other, each time steps of the year is represented by a rectangle which is colored according to the data value for that hour. The DMap format often allows you to see daily and seasonal patterns more easily than you could with a simple time series plot. An example of a DMap appears below:



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6.47 Effective Head (PRO)



Effective Head

Type: Intermediate Variable

Units: m

Symbol: h_{net}

One can model the friction pressure loss in the pipeline between the intake and the turbine as a loss in head. The effective head is the actual vertical drop minus this head loss. HOMER calculates the effective head (or net head) using the following equation:

$$h_{\text{net}} = h \cdot (1 - f_h)$$

where:

h = [available head](#) [m]

f_h = [pipe head loss](#) [%]

HOMER uses the effective head to calculate the power output of the hydro turbine in each time step.

See also

[Available head](#)

[Calculating hydro power output](#)

For more information

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6.48 Electrolyzer Efficiency (PRO)



Electrolyzer Efficiency

Type: Input Variable

Units: %

Symbol: $h_{\text{electrolyzer}}$

The efficiency with which the electrolyzer converts electricity into hydrogen. This is equal to the energy content (based on higher heating value) of the hydrogen produced divided by the amount of electricity consumed.

Example: The higher heating value of hydrogen is 142 MJ/kg, which is equal to 39.4 kWh/kg. So an electrolyzer that consumes 50 kWh of electricity to produce one kilogram of hydrogen has an efficiency of 39.4 kWh/kg divided by 50 kWh/kg, which is 79%.

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6.49 Excess Electricity



Excess Electricity

Excess electricity is surplus electrical energy that must be dumped (or curtailed) because it cannot be used to serve a load or charge the batteries. Excess electricity occurs when there is a surplus of power being produced (either by a renewable source or by the generator when its minimum output exceeds the load) and the batteries are unable to absorb it all.

A resistive heater (often called an electric boiler) can convert excess electricity into thermal energy that can meet the thermal load. You can model such a situation by going to the [System Control Inputs](#) window and checking the checkbox labeled Allow excess electricity to serve thermal load.

If it cannot be put to use, excess electricity may need to be dissipated in a *dump load*, which is usually a simple resistive heater or a bank of light bulbs. In some cases, excess energy represents energy that could be curtailed rather than dissipated.

HOMER tabulates the excess electricity experienced by the system in each time step. You can see the time series and the annual total in the [Simulation Results](#) window, which appears when you double click on a system in the Optimization Results tab of HOMER's main window.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.50 Excess Electricity Fraction



Excess Electricity Fraction

Type: Output Variable

Units: none

Symbol: f_{excess}

The excess electricity fraction is the ratio of [total excess electricity](#) to the [total electrical production](#). HOMER calculates this value at the end of each simulation using the following equation:

$$f_{\text{excess}} = \frac{E_{\text{excess}}}{E_{\text{prod}}}$$

where:

E_{excess} = [total excess electricity](#) [kWh/yr]

E_{prod} = [total electrical production](#) [kWh/yr]

See also

[Total excess energy](#)

For more information

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6.51 Feasible and Infeasible Systems



Feasible and Infeasible Systems

A feasible system is one that satisfies the constraints. An infeasible system is one that does not satisfy the constraints.

HOMER discards infeasible systems and does not display them in the optimization results or sensitivity results.

See also:

[The definition of a system](#)

[Optimization results](#)

[Sensitivity results](#)

[Constraints](#)

For more information

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6.52 Flow Rate Available To Hydro Turbine (PRO)



Flow Rate Available To Hydro Turbine

Type: Intermediate Variable

Units: m³/s

Symbol: $\dot{Q}_{available}$

The flow rate available to the hydro turbine is the maximum flow rate that could be diverted into the hydro turbine. In each time step, HOMER calculates the available flow rate using the following equation:

$$\dot{Q}_{available} = \dot{Q}_{stream} - \dot{Q}_{residual}$$

where:

\dot{Q}_{stream} = the total stream flow [m³/s]

$\dot{Q}_{residual}$ = [residual flow](#) [m³/s]

HOMER uses the available stream flow to calculate the actual stream flow through the hydro turbine in each time step.

See also

[Hydro turbine flow rate](#)

[Calculating the hydro power output](#)

For more information

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6.53 Fossil Fraction (PRO)



Fossil Fraction

A cofired generator can operate on a mixture of fossil fuel and [biogas](#). The *fossil fraction* (x_{fossil}) is the ratio of fossil fuel used by the generator in dual-fuel mode to that required to produce the same output power in pure fossil mode. With compression-ignition (diesel) engines, it is necessary to maintain a minimum fossil fraction to ensure proper ignition.

For a more complete explanation of the fossil fraction and the operation of a cofired generator, please see the article [Operation of a Cofired Generator](#).

See also

[Minimum fossil fraction](#)

[Operation of a cofired generator](#)

For more information

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6.54 Fuel Carbon Content



Fuel Carbon Content

Type: Input Variable

Units: % (by mass)

Symbol: k_{fuel}

The carbon content of the fuel as a percent of its mass. This value is used to calculate the annual emissions of carbon dioxide, carbon monoxide, and unburned hydrocarbons resulting from the consumption of this fuel in a generator, boiler, or reformer.

See also:

[How HOMER calculates emissions](#)

[CO2 emissions penalty](#)

[CO emissions penalty](#)

[Grid emissions factors](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.55 Fuel Price



Fuel Price

Type: Input Variable
Units: \$/L
Symbol: c_{fuel}

The price of fuel in dollars per liter. It is very common to do a sensitivity analysis on this variable for two reasons: it is difficult to accurately predict the future fuel price, and the optimal architecture of the power system can vary widely depending on the fuel price.

This input is used to calculate the [generator fuel cost](#).

For more information

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6.56 Fuel Sulfur Content



Fuel Sulfur Content

Type: Input Variable
Units: % (by mass)

The sulfur content of the fuel as a percent of its mass. This value is used to calculate the annual emissions of particulate matter and sulfur dioxide resulting from the consumption of this fuel in a generator, boiler, or reformer.

See also:

[How HOMER calculates emissions](#)

[SO₂ emissions penalty](#)

[PM emissions penalty](#)

[Grid emissions factors](#)

For more information

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6.57 Future Value



Future Value

The future value is defined as the equivalent value at some designated future date of a sequence of cash flows, taking into account the time value of money.

See also

[Interest rate](#)

[Sinking fund factor](#)

[Present value](#)

For more information

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6.58 Generator



Generator

In HOMER, a "generator" is a device that consumes fuel to produce electric (and sometimes thermal) energy. Generators can be dispatched, meaning the system can turn them on as necessary. Microturbines and fuel cells are generators, as are diesel- and gasoline-fueled reciprocating engine generators.

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6.59 Generator Average Electrical Efficiency



Generator Average Electrical Efficiency

Type: Output Variable

Units: %

Symbol: η_{gen}

This is the average electrical efficiency of the generator over the year, defined as the electrical energy out divided by fuel energy in. HOMER uses the following equation to calculate the average electrical efficiency:

$$\eta_{gen} = \frac{3.6 \cdot E_{gen}}{m_{fuel} \cdot LHV_{fuel}}$$

where:

E_{gen} = the generator's total annual electrical production [kWh/yr]

m_{fuel} = the generator's total annual fuel consumption [kg/yr]

LHV_{fuel} = the lower heating value of the fuel [MJ/kg]

The factor of 3.6 in the above equation arises because 1 kWh = 3.6 MJ.

See also:

[Generator average total efficiency](#)

For more information

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6.60 Generator Average Total Efficiency



Generator Average Total Efficiency

Type: Output Variable

Units: %

Symbol: $h_{gen,tot}$

This is the average total efficiency of the generator over the year, defined as the electrical plus thermal energy out divided by fuel energy in. HOMER uses the following equation to calculate the average total efficiency:

$$\eta_{gen,tot} = \frac{3.6 \cdot (E_{gen} + H_{gen})}{m_{fuel} \cdot LHV_{fuel}}$$

where:

E_{gen} = the generator's total annual electrical production [kWh/yr]

H_{gen} = the generator's total annual thermal production [kWh/yr]

m_{fuel} = the generator's total annual fuel consumption [kg/yr]

LHV_{fuel} = the lower heating value of the fuel [MJ/kg]

The factor of 3.6 in the above equation arises because 1 kWh = 3.6 MJ.

See also:

[Generator average efficiency](#)

For more information

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6.61 Generator Carbon Monoxide Emissions Factor



Generator Carbon Monoxide Emissions Factor

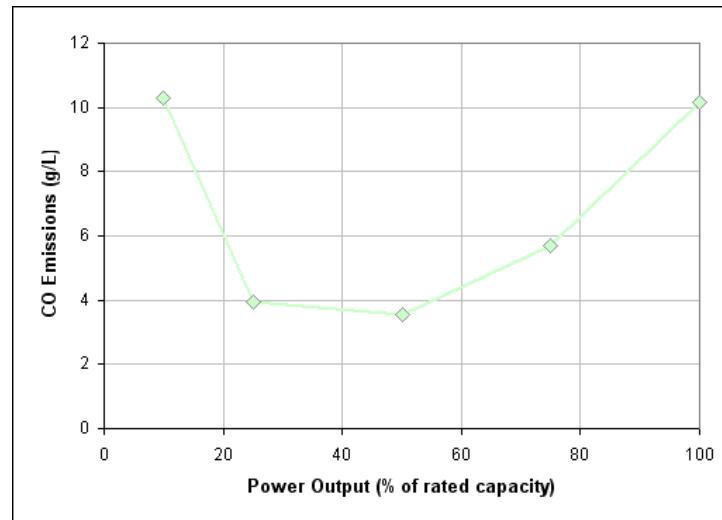
Type: Input Variable

Units: grams per unit fuel (fuel units can be L, m³, or kg)

Symbol: $f_{gen,CO}$

The amount of carbon monoxide emitted per unit fuel consumed by the generator. Because carbon monoxide is a product of incomplete combustion, the quantity produced will depend on the fuel, engine design, and operating conditions, including the power output of the generator. But HOMER makes a simplifying assumption that this factor is constant.

The following graph shows the value of the carbon monoxide emissions factor for diesel generators in the size range 50 kW - 450 kW. The source of these data is an internal NREL report by Erin Kassoy entitled "Modeling diesel exhaust emissions in diesel retrofits". The default value for the generator CO emissions factor is equal to the average value between 50% and 100% load.



HOMER uses this value to calculate the emissions of carbon monoxide and carbon dioxide. For details, see the article on [How HOMER calculates emissions](#).

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6.62 Generator Derating Factor (PRO)



Generator Derating Factor P

Type: Input Variable

Units: %

Symbol: t

The maximum output of a cofired generator operating at the [minimum fossil fraction](#), as a percentage of its rated output. For example, say a 20 kW diesel generator is modified to run on a mixture of diesel fuel and [biogas](#), with a minimum diesel of 20%. If the output of the engine is limited to 15 kW when operating at 20% diesel fraction, the derating factor would be 15 kW divided by 20 kW, or 75%.

Note that HOMER assumes a cofired generator can produce up to 100% of its rated output, provided the fossil fraction is high enough. In the above example, the generator could produce up to 20 kW, but the diesel fraction would have to exceed 20% for any output power above 15 kW.

For a more complete explanation of a cofired generator, please see [Operation of a Cofired Generator](#).

For more information

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6.63 Generator Fuel Cost



Generator Fuel Cost

Type: Output Variable

Units: \$/yr

Symbol: $C_{fuel,gen}$

The annual cost of fueling the generator. HOMER calculates this value by multiplying the fuel price by the amount of fuel used by the generator in one year.

If the generator burns [biogas](#), either as its primary fuel or cofired with another fuel, HOMER includes the biomass cost in the generator fuel cost. The biomass cost is equal to the amount of biomass *feedstock* consumed over a year multiplied by the price of biomass.

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6.64 Generator Fuel Curve Intercept Coefficient



Generator Fuel Curve Intercept Coefficient

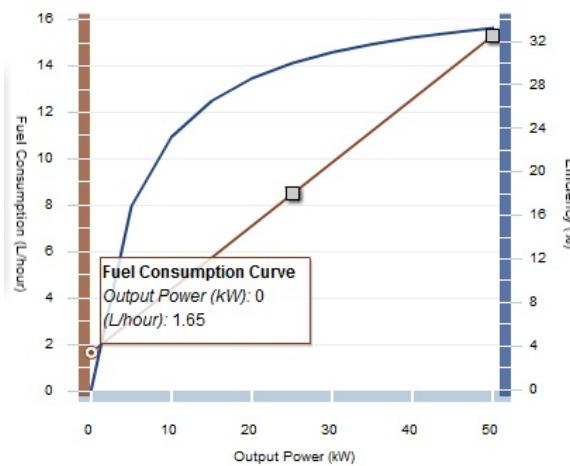
Type: Input Variable

Units: fuel units/hr/kW_{rated}

Symbol: F_0

The fuel curve intercept coefficient is the no-load fuel consumption of the generator divided by its rated capacity. If you were to plot a straight line of fuel consumption versus the power output of the generator, the y-intercept of that line divided by the generator size is equal to the fuel curve intercept coefficient.

For example, if a 50 kW generator consumes 8.48 L/hr at 25 kW output and 15.3 L/hr at rated output, the slope of the fuel curve would be $(15.3 - 8.48)/(50 - 25) = 0.273 \text{ L/hr/kW}_{\text{output}}$. So the y-intercept would be $8.48 - (0.273 \cdot 25) = 1.655 \text{ L/hr}$. Dividing by 50 kW (the size of the generator) gives the fuel curve intercept coefficient of $0.033 \text{ L/hr/kW}_{\text{rated}}$. This fuel curve is plotted below:



The [Fuel Curve Calculator](#) helps calculate the fuel curve slope and intercept coefficient.

If the generator is running in a particular time step, HOMER calculates the fuel consumption rate for that time step using the following equation:

$$F = F_0 \cdot Y_{gen} + F_1 \cdot P_{gen}$$

where:

F = fuel consumption rate [L/hr]

F_0 = generator fuel curve intercept coefficient [L/hr/kW_{rated}]

F_1 = [generator fuel curve slope](#) [L/hr/kW_{output}]

Y_{gen} = rated capacity of the generator [kW]

P_{gen} = output of the generator in this time step [kW]

If the generator is not running in a particular time step, then the fuel consumption for that time step is zero.

See also

[Fuel curve slope](#)

For more information

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6.65 Generator Fuel Curve Slope



Generator Fuel Curve Slope

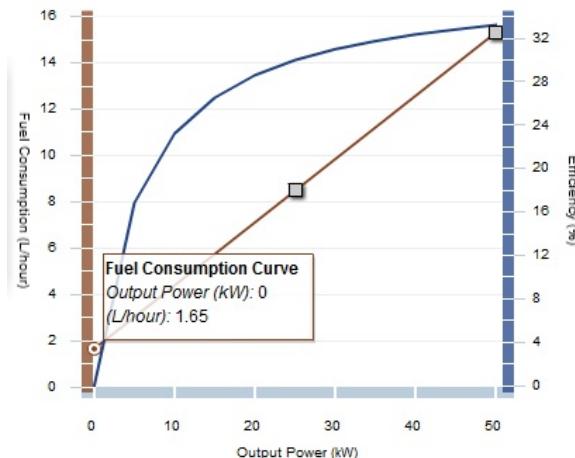
Type: Input Variable

Units: fuel units/hr/kW

Symbol: F_1

The fuel curve slope is the marginal fuel consumption of the generator, in units of fuel per hour per kW of output, or equivalently, units of fuel per kWh. If you were to plot a straight line of fuel consumption versus the power output of the generator, the slope of that line is the fuel curve slope.

For example, if a 50 kW generator consumes 8.48 L/hr at 25 kW output and 15.3 L/hr at rated output, the slope of the fuel curve would be $(15.3-8.48)/(50-25) = 0.273 \text{ L/hr/kW}_{\text{output}}$. This fuel curve is plotted below:



The [Fuel Curve Calculator](#) helps calculate the fuel curve slope and intercept coefficient.

If the generator is running in a particular time step, HOMER calculates the fuel consumption rate for that time step using the following equation:

$$F = F_0 \cdot Y_{gen} + F_1 \cdot P_{gen}$$

where:

F = fuel consumption rate this time step [L/hr]

F_0 = [generator fuel curve intercept coefficient](#) [L/hr/kW_{rated}]

F_1 = generator fuel curve slope [L/hr/kW_{output}]

Y_{gen} = rated capacity of the generator [kW]

P_{gen} = output of the generator in this time step [kW]

If the generator is not running in a particular time step, then the fuel consumption for that time step is zero.

See also

[Fuel curve intercept coefficient](#)

For more information

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6.66 Generator Heat Recovery Ratio (PRO)



Generator Heat Recovery Ratio P

Type: Input Variable

Units: %

Symbol: f_{hr}

This input is relevant only for cogeneration systems, also called combined-heat-and-power systems or CHP systems. Such systems serve both electric and thermal loads, with waste heat recovered from the generator meeting some or all of the thermal load. If you do not want to model a cogeneration system, leave this input at zero.

HOMER assumes that the generator converts all of the energy of the fuel into electricity and heat. The generator's fuel curve specifies how much electricity it produces for a given fuel input, and HOMER simply assumes the remaining fuel energy is converted to heat. The heat recovery ratio is the percentage of that heat that can be recovered to serve the thermal load.

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6.67 Generator Hourly Replacement Cost



Generator Hourly Replacement Cost

Type: Intermediate Variable

Units: \$/hr

Symbol: $C_{rep,gen}$

The generator lifetime is specified in number of operating hours. So the hourly replacement cost of each generator can be calculated according to the following equation:

$$C_{rep,gen} = \frac{C_{rep,gen}}{R_{gen,h}}$$

where:

$C_{rep,gen}$ = generator [replacement cost](#)

$R_{gen,h}$ = [generator lifetime](#)

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6.68 Generator Lifetime



Generator Lifetime

Type: Input Variable

Units: hr

Symbol: $R_{gen,h}$

Unlike the lifetime inputs for most other components, the generator lifetime is specified not in years but in hours of operation. This is because the lifetime of a generator depends strongly on the hours of operation, but not very strongly on its age.

It is not always easy to obtain lifetime data for a particular generator, as it can depend on operating conditions, maintenance frequency, fuel quality, and other factors. But it is possible to estimate longevity based on the engine type. Reciprocating internal combustion engines are the most common engine type. Of these, compression-ignition (diesel) engines tend to last several times longer than spark-ignition engines (gasoline, propane, or natural gas) engines. For longevity, low speed (1800 RPM) is superior to high speed (3600 RPM), liquid cooling is superior to air cooling, and pressurized oil lubrication is superior to splash lubrication. The following table serves as a rough guideline for estimating the lifetime of certain types of generators.

| Generator Type | Size Range (kW) | Estimated Lifetime (hrs) |
|--|-----------------|--------------------------|
| High speed (3600 RPM) air-cooled gasoline, natural gas, or propane generator | 1-10 | 250 - 1,000 |
| High speed (3600 RPM) air-cooled diesel | 4 - 20 | 6,000 - 10,000 |
| Low speed (1800 RPM) liquid-cooled natural gas or propane generator | 15 - 50 | 6,000 - 10,000 |
| Prime power liquid-cooled diesel | 7 - 10,000 | 20,000 - 80,000 |
| Natural gas microturbine | 25 - 500 | 50,000 - 80,000 |

Because its lifetime is specified in operating hours, the more frequently the generator operates, the shorter its lifetime in years. This affects the economics of the system because more frequent replacements leads to higher annualized cost. HOMER takes this into consideration when deciding whether to operate a generator or to use an alternative dispatchable source such as a battery, the grid, or another generator.

Once it has simulated a system, HOMER calculates the generator's expected lifetime in years and reports it as the [generator operational life](#) on the [Simulation Results](#) window.

For more information

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6.69 Generator Minimum Fossil Fraction (PRO)



Generator Minimum Fossil Fraction

Type: Input Variable

Units: %**Symbol:** x_{fossil}

The minimum allowable [fossil fraction](#) for a cofired generator operating on a mixture of fossil fuel and biogas. Diesel engines require a certain minimum amount of diesel fuel to ensure proper ignition. Spark-ignition engines may not have any such requirement, and may be able to operate on pure [biogas](#).

For more information

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6.70 Generator Minimum Percent Load



Generator Minimum Percent Load

Type: Input Variable**Units:** %**Symbol:** $f_{gen,min}$

The minimum allowable load on the generator, as a percentage of its rated capacity. Specifying a minimum load will not prevent the generator from being shut off, it will simply prevent it from operating at too low a load. This input exists because some manufacturers recommend that their generators not be run below a certain load.

As an example, say this number is set to 30%. If the required power from the generator is 40% of its capacity, it will run at 40%. If the required power is 15%, it will run at 30%, with the excess power either serving the deferrable load, charging the batteries, or being dumped. If no power is required from the generator, it will be shut off.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.71 Generator Nitrogen Oxides Emissions Factor

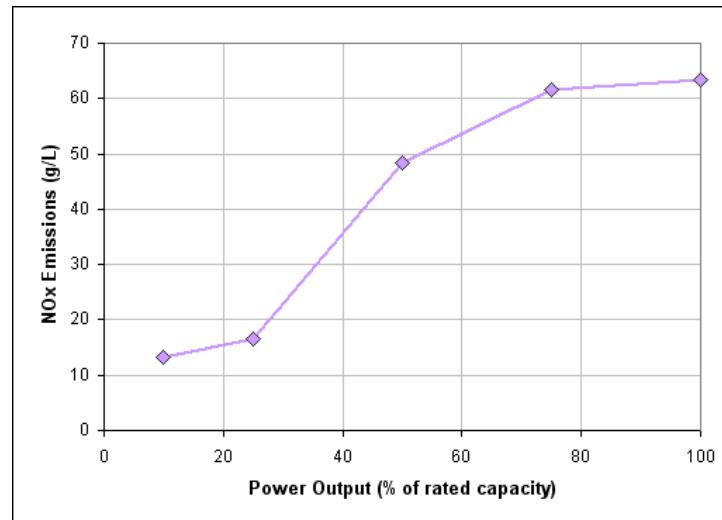


Generator Nitrogen Oxides Emissions Factor

Type: Input Variable**Units:** grams per unit fuel (fuel units can be L, m³, or kg)**Symbol:** $f_{gen,NOx}$

The amount of nitrogen oxides emitted per unit fuel consumed by the generator. The actual quantity of this pollutant produced by the generator will depend on engine design and operating conditions, principally the power output of the generator. But HOMER makes a simplifying assumption that this factor is constant.

The following graph shows the value of the nitrogen oxides emissions factor for diesel generators in the size range 50 kW - 450 kW. The source of these data is an unpublished NREL report by Erin Kassoy entitled "Modeling diesel exhaust emissions in diesel retrofits". HOMER's default value for the generator's nitrogen oxides emissions factor is equal to the average value between 50% and 100% load.



HOMER uses this value to calculate the emissions of nitrogen oxides. For details, see the article on [How HOMER calculates emissions](#).

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6.72 Generator Operational Life



Generator Operational Life

Type: Output Variable

Units: yr

Symbol: R_{gen}

In HOMER, the lifetime of generators is specified in terms of operating hours. The number of years that a generator will last is therefore an output variable, which HOMER calculates according to the following equation:

$$R_{gen} = \frac{R_{gen,h}}{N_{gen}}$$

where:

$R_{gen,h}$ = [generator lifetime](#) [hr]

N_{gen} = the number of hours the generator operates during one year [hr/yr]

For example, if the generator has a lifetime of 20,000 operating hours and HOMER determines that it will operate 4300 hours per year, then its expected lifetime in years would be 20,000 hours / 4300 hours per year = 4.65 years

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6.73 Generator Particulate Matter Emissions Factor

Generator Particulate Matter Emissions Factor

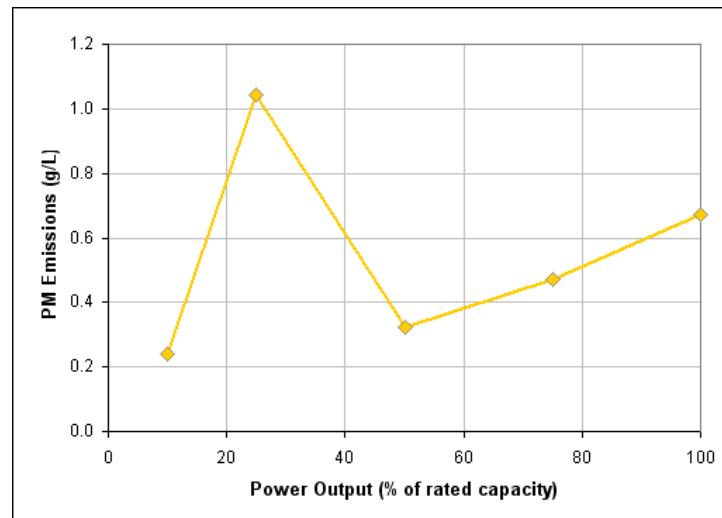
Type: Input Variable

Units: grams per unit fuel (fuel units can be L, m³, or kg)

Symbol: $f_{gen,PM}$

The amount of particulate matter (smoke, soot, and liquid droplets) emitted per unit fuel consumed by the generator. The actual quantity of this pollutant produced by the generator will depend on the fuel, engine design, and operating conditions, including the power output of the generator. But HOMER makes a simplifying assumption that this factor is constant.

The following graph shows the value of the particulate matter emissions factor for diesel generators in the size range 50 kW - 450 kW. The source of these data is an internal NREL report by Erin Kassoy entitled "Modeling diesel exhaust emissions in diesel retrofits". HOMER's default value for the generator's particulate matter emissions factor is equal to the average value between 50% and 100% load.



HOMER uses this value to calculate the emissions of particulate matter. For details, see the article on [How HOMER calculates emissions](#).

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6.74 Generator Proportion of Sulfur Emited as Particulate Matter

Generator Proportion of Sulfur Emited as Particulate Matter

Type: Input Variable

Units: %

Symbol: x_{PM}

The fraction of the sulfur in the fuel that gets emitted as particulate matter. HOMER assumes that the rest gets emitted as sulfur dioxide. This value is 2.2% for diesel generators, according to the EPA document EPA420-P-02-016, dated November 2002, entitled "Exhaust and Crankcase Emission Factors for Nonroad Engine Modeling -- Compression-Ignition".

HOMER uses this value to calculate the emissions of sulfur dioxide. Note that HOMER does not use this value to calculate emissions of particulate matter. For that, it uses the [particulate matter emissions factor](#). For details, see the article on [How HOMER calculates emissions](#).

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6.75 Generator Unburned Hydrocarbons Emissions Factor



Generator Unburned Hydrocarbons Emissions Factor

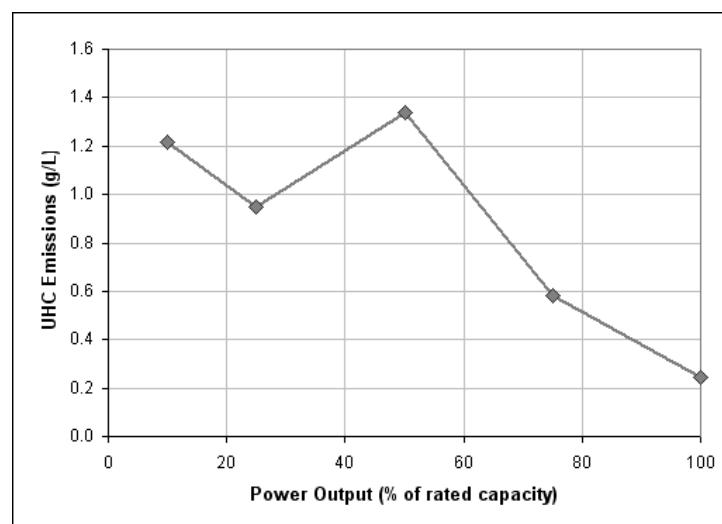
Type: Input Variable

Units: grams per unit fuel (fuel units can be L, m³, or kg)

Symbol: $f_{gen,UHC}$

The amount of unburned hydrocarbons emitted per unit fuel consumed by the generator. The actual quantity of this pollutant produced by the generator will depend on the fuel, engine design, and operating conditions, including the power output of the generator. But HOMER makes a simplifying assumption that this factor is constant.

The following graph shows the value of the unburned hydrocarbons emissions factor for diesel generators in the size range 50 kW - 450 kW. The source of these data is an internal NREL report by Erin Kassoy entitled "Modeling diesel exhaust emissions in diesel retrofits". The default value for the generator's unburned hydrocarbon emissions factor is equal to the average value between 50% and 100% load.



HOMER uses this value to calculate the emissions of unburned hydrocarbons and carbon dioxide. For details, see the article on [How HOMER calculates emissions](#).

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6.76 Grid Costs



Grid Costs

Since the grid is unlike any other component, HOMER calculates the costs associated with the grid in a unique way. This article explains how HOMER calculates each of the grid cost outputs.

Grid capital cost

If the system is connected to the grid and contains some other power producing device (such as a microturbine, a fuel cell, a PV array, or a wind turbine), the grid capital cost is equal to the interconnection charge. Otherwise, the grid capital cost is zero.

Grid replacement cost

The replacement cost of the grid is always zero.

Grid O&M cost

The grid O&M cost is equal to the annual cost of buying electricity from the grid (energy cost plus demand cost) minus any income from the sale of electricity to the grid. For grid-connected systems that contain some other power producing device (such as a microturbine, a fuel cell, a PV array, or a wind turbine), the grid O&M cost also includes the standby charge.

See also

[Interconnection charge](#)

[Standby charge](#)

[Capital recovery factor](#)

[Project lifetime](#)

For more information

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6.77 Grid Interconnection Charge (PRO)



Grid Interconnection Charge P

Type: Input Variable

Units: \$

Symbol: $C_{\text{grid,int}}$

The interconnection charge is a one-time fee charged by the utility for allowing a power system to be connected to the grid. HOMER does not apply this fee to grid-only systems, but rather to grid-connected systems that include some other generation source. For such systems, the interconnection charge is added to the [grid capital cost](#).

See also:

[Standby charge](#)

[Grid capital cost](#)

For more information

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6.78 Grid Standby Charge (PRO)



Grid Standby Charge

Type: Input Variable

Units: \$/yr

Symbol: $C_{\text{grid,standby}}$

The standby charge is an annual fee charged by the utility for providing backup grid power for a grid-connected power system. HOMER does not apply this fee to grid-only systems, but rather to grid-connected systems that include some other generation source (like a microturbine, a fuel cell, or a PV array). For such systems, the standby charge is added to the [grid O&M cost](#).

See also:

[Interconnection charge](#)

[Grid O&M cost](#)

For more information

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6.79 Ground Reflectance



Ground Reflectance

Type: Input Variable

Units: %

Symbol: r_g

The ground reflectance (also called albedo) is the fraction of solar radiation incident on the ground that is reflected. A typical value for grass-covered areas is 20%. Snow-covered areas may have a reflectance as high as 70%. This value is used in calculating the radiation incident on the tilted PV panels, but it has only a modest effect.

See also:

[PV Inputs window](#)

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6.80 Hydrocarbons Emissions Penalty (PRO)



Hydrocarbons Emissions Penalty

Type: Input Variable**Units:** \$/t**Symbol:** c_{HC}

Use the HC emissions penalty to penalize systems for their production of unburned hydrocarbons. HOMER uses this input value when calculating the [Other O&M cost](#).

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6.81 Hour of Peak Windspeed

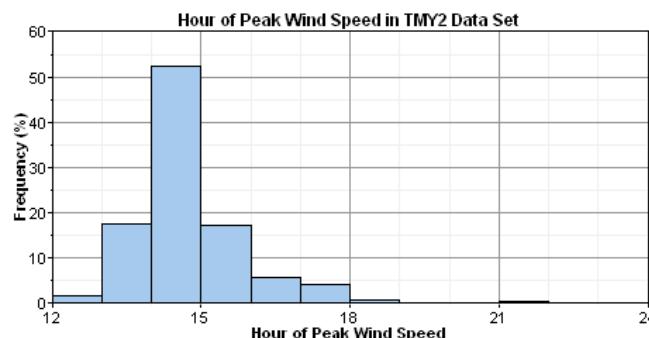


Hour of Peak Windspeed

Type: Input Variable**Units:** none**Symbol:** f**Typical Range:** 14 - 16

The hour of peak windspeed is the hour of the day that tends to be the windiest, on average. The article on diurnal pattern strength describes how HOMER calculates this value.

We calculated the hour of peak wind speed for each of the 239 weather stations in the TMY2 data set. The histogram below shows the resulting distribution. You can see the measured values themselves in the [table of measured wind parameters](#).



See also

[Diurnal pattern strength](#)

[Autocorrelation factor](#)

[Weibull k](#)

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6.82 Hydro Turbine Efficiency (PRO)



Hydro Turbine Efficiency

Type: Input Variable

Units: %

Symbol: h_{hyd}

The efficiency with which the hydro turbine converts the mechanical power of the water into electrical power. HOMER uses this value to calculate the nominal hydro power and the actual output power of hydro turbine in each time step.

See also

[Nominal hydro power](#)

[Calculating hydro power output](#)

For more information

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6.83 Hydro Turbine Flow Rate (PRO)



Hydro Turbine Flow Rate

Type: Intermediate Variable

Units: m³/s

Symbol: $\dot{Q}_{turbine}$

The hydro turbine flow rate is the amount of water flowing through the hydro turbine. HOMER calculates this value in each time step using the following equation:

$$\dot{Q}_{turbine} = \begin{cases} 0 & \text{if } \dot{Q}_{available} < \dot{Q}_{min} \\ \dot{Q}_{available} & \text{if } \dot{Q}_{min} \leq \dot{Q}_{available} \leq \dot{Q}_{max} \\ \dot{Q}_{max} & \text{if } \dot{Q}_{available} > \dot{Q}_{max} \end{cases}$$

where:

$\dot{Q}_{available}$ = the [flow rate available to the hydro turbine](#) [m³/s]

\dot{Q}_{min} = [minimum flow rate of the hydro turbine](#) [m³/s]

\dot{Q}_{max} = [maximum flow rate of the hydro turbine](#) [m³/s]

Note: As this equation shows, HOMER assumes that unless the available stream exceeds the turbine's minimum flow rate, the turbine flow rate is zero, meaning the turbine does not operate and hence produces no power. If HOMER reports that your hydro turbine is not producing any power, this is probably the reason.

HOMER uses the hydro turbine flow rate to calculate the hydro power output in each time step.

See also

[Calculating the hydro power output](#)

For more information

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6.84 Hydrogen Tank Autonomy (PRO)



Hydrogen Tank Autonomy P

Type: Output Variable

Units: hr

Symbol: A_{htank}

The hydrogen tank autonomy is the ratio of the energy capacity of the hydrogen tank to the electric load. HOMER calculates the hydrogen tank autonomy using the following equation:

$$A_{htank} = \frac{Y_{htank} \text{LHV}_{H_2} (24 \text{ h/d})}{L_{prim,ave} (3.6 \text{ MJ/kWh})}$$

where:

Y_{htank} = capacity of the hydrogen tank [kg]

LHV_{H_2} = energy content (lower heating value) of hydrogen [120 MJ/kg]

$L_{prim,ave}$ = average primary load [kWh/d]

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6.85 Initial Capital Cost



Initial Capital Cost

The initial capital cost of a component is the total installed cost of that component at the beginning of the project.

Tip: To see initial capital costs and all other costs that occur over the lifetime of the project, see the [Cash Flow Details Table](#).

See also

[Replacement cost](#)

[Cash Flow Details table](#)

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6.86 Interest Rate



Interest Rate

Type: Input Variable**Units:** %**Symbol:** i

The interest rate that one enters for HOMER's input is the annual real interest rate (also called the *real interest rate* or just *interest rate*). It is the discount rate used to convert between one-time costs and annualized costs. HOMER uses the interest rate to calculate discount factors and to calculate annualized costs from net present costs.

You enter the interest rate in the Economic Inputs window.

To calculate the annual real interest rate from the nominal interest rate, use the following equation:

$$i = \frac{i' - f}{1 + f}$$

where:

i = real interest rate

i' = nominal interest rate (the rate at which you could borrow money)

f = annual inflation rate

For example, if the nominal interest rate is 8% and the inflation rate is 3.5%, the annual real interest rate is 4.35%.

By defining the interest rate in this way, **inflation** is factored out of the economic analysis. All costs therefore become *real costs*, meaning that they are defined in terms of constant dollars. The assumption is that the rate of inflation is the same for all costs.

See also

[Economic Inputs window](#)

[Annualized cost](#)

[Net present cost](#)

[Salvage value](#)

[Interest rate](#)

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6.87 Levelized Cost of Energy



Levelized Cost of Energy

Type: Output Variable**Units:** \$/kWh**Symbol:** COE

HOMER defines the levelized cost of energy (COE) as the average cost per kWh of useful electrical energy produced by the system. To calculate the COE, HOMER divides the annualized cost of producing electricity (the total annualized cost minus the cost of serving the thermal load) by the total electric load served, using the following equation:

$$COE = \frac{C_{ann,tot} - c_{boiler} H_{served}}{E_{served}}$$

where:

$C_{ann,tot}$ = [total annualized cost](#) of the system [\$/yr]

c_{boiler} = [boiler marginal cost](#) [\$/kWh]

H_{served} = [total thermal load served](#) [kWh/yr]

E_{served} = [total electrical load served](#) [kWh/yr]

The second term in the numerator is the portion of the annualized cost that results from serving the thermal load. In systems that do not serve a thermal load ($H_{\text{thermal}}=0$) this term will equal zero.

The COE is a convenient metric with which to compare systems, but HOMER does not rank systems based on COE. For an explanation, please refer to [Why does HOMER rank systems by total NPC?](#)

See also

[Annualized cost](#)

[Total annualized cost](#)

[Why does HOMER rank systems by total NPC?](#)

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6.88 Lifetime Throughput



Lifetime Throughput

Type: Input Variable

Units: kWh

Symbol: Q_{lifetime}

If the battery properties indicate that the battery life is limited by throughput, HOMER assumes that the battery will require replacement after a fixed amount of energy cycles through the battery, regardless of the depth of the individual charge-discharge cycles. HOMER uses this *lifetime battery throughput* to calculate the [life of the battery bank](#) and the [battery wear cost](#).

See also

[Battery float life](#)

[Create New Battery window](#)

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6.89 Load Factor



Load Factor

The load factor is a dimensionless number equal to the average load divided by the peak load.

Example: If the average load is 66 kWh/d (or 2.75 kW) and the peak load is 10.5 kW, the load factor is $2.75 \text{ kW} / 10.5 \text{ kW} = 0.26$.

For more information

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6.90 Load Following Strategy



Load Following Strategy

The load following strategy is a [dispatch strategy](#) whereby whenever a generator operates, it produces only enough power to meet the primary load. Lower-priority objectives such as charging the battery bank or serving the [deferrable load](#) are left to the renewable power sources.

Under the load following strategy, HOMER dispatches the system's controllable power sources (generators, grid, battery bank) so as to serve the primary load and the thermal load at the least total cost each time step, while satisfying the [operating reserve requirement](#). The total cost includes the cost of fuel, operation and maintenance, and replacement. To accomplish this, HOMER calculates the fixed and marginal cost of each dispatchable power source:

- A generator's fixed cost is equal to its hourly operation and maintenance cost plus its [hourly replacement cost](#) plus the cost of its no-load fuel consumption. Its marginal cost is equal to its fuel curve slope times the fuel price. If waste heat can be recovered from the generator **and** the waste heat is needed to serve the thermal load, the generator's marginal cost is reduced by the value of the thermal energy it produces (which is equal to the marginal cost of thermal energy from the [boiler](#)). If a cost is assigned to carbon emissions, the generator's marginal cost is increased accordingly.
- The battery bank's fixed cost is zero and its marginal cost is equal to the [battery wear cost](#).
- The grid's fixed cost is zero and its marginal cost is equal to the grid power price. If a cost is assigned to carbon emissions, the grid's marginal cost is increased accordingly.

Once it characterizes each dispatchable source in this way, HOMER searches for the combination of generation sources that satisfies the primary load, required operating reserve, and thermal load at least cost.

See also

[Cycle charging strategy](#)

For more information

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6.91 Maximum Annual Capacity Shortage



Maximum Annual Capacity Shortage

Type: Input Variable

Units: %

The maximum annual capacity shortage is the maximum allowable value of the [capacity shortage fraction](#), which is the [total capacity shortage](#) divided by the total electric load. HOMER considers infeasible (or unacceptable) any system with a higher value of the capacity shortage fraction.

Allowing some capacity shortage can change the results dramatically in some cases. This might happen if there were a very high peak for a very short time. If the maximum annual capacity shortage is set to zero, HOMER will size the system to meet even this very high peak load. This could mean that the system has to include large, expensive equipment that is not fully used most of the time. If you allow a small amount of capacity shortage, HOMER could choose to install smaller, less expensive equipment that would be able to supply all but that peak load.

Note: If you set each of the four operating reserve inputs to zero, the capacity shortage fraction will be equal to the unmet load fraction.

See also:

[Required operating reserve](#)

[Total capacity shortage](#)

[Capacity shortage fraction](#)

[Unmet load fraction](#)

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6.92 Maximum Battery Capacity



Maximum Battery Capacity

The maximum capacity (or theoretical capacity) of a battery is the total amount of energy it contains when fully charged. It is not possible to extract all this energy at any finite discharge current (it would take an infinite amount of time to extract it all), so battery sizes are not typically given in terms of maximum capacity. HOMER calculates the maximum capacity for use in the [kinetic battery model](#).

See also

[Nominal Capacity](#)

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6.93 Maximum Flow Rate (PRO)



Maximum Flow Rate

Type: Intermediate Variable

Units: m³/s

Symbol: \dot{Q}_{max}

The maximum flow rate is the maximum allowable flow rate through the hydro turbine. HOMER calculates the maximum flow rate of the hydro turbine using the following equation:

$$\dot{Q}_{max} = w_{max} \cdot \dot{Q}_{design}$$

where:

w_{max} = the hydro turbine's [maximum flow ratio](#) [%]

\dot{Q}_{design} = the hydro turbine's [design flow rate](#) [m³/s]

HOMER uses this value to calculate the hydro turbine flow rate in each time step.

See also

[Minimum flow rate](#)

[Hydro turbine flow rate](#)

[Calculating the hydro power output](#)

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6.94 Maximum Flow Ratio (PRO)



Maximum Flow Ratio

Type: Input Variable

Units: %

Symbol: w_{max}

The maximum acceptable flow rate through the hydro turbine, expressed as a percentage of the turbine's design flow rate. HOMER uses this input to calculate the maximum flow rate through the hydro turbine, and hence the actual flow rate through the hydro turbine.

See also

[Design flow rate](#)

[Maximum flow rate](#)

[Hydro turbine flow rate](#)

[Minimum flow ratio](#)

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6.95 Purchase Capacity



Purchase Capacity

Type: Input Variable

Units: kW

Symbol: T_{grid}

The purchase capacity is the maximum amount of power that can be drawn from the grid at any time. It is a [decision variable](#) because of the effect of demand charges. HOMER does not explicitly consider the demand rate in its time-step-by-time-step decisions as to how to control the power system; the demand charge is simply calculated at the end of each annual simulation. As a result, HOMER will not turn on a generator simply to save demand charges. But it will turn on a generator whenever the load exceeds the maximum grid demand.

If the demand rate is zero, you need only specify a single value for the maximum grid demand. Normally, the true capacity of the grid is much higher than the system peak load, and the maximum grid demand can be set to any value higher than the system peak load. In the rare case that the grid is unable to meet the system peak load, the maximum grid demand should be set to the actual capacity of the grid.

If the demand rate is not zero, specify a value equal to or greater than the peak load, plus at least one value smaller than the peak load. HOMER will find the optimal value.

The maximum grid demand appears in a table on the [Grid Inputs](#) window:

| Purchase Capacity (kW) |
|------------------------|
| 300 |
| 350 |
| 400 |
| 450 |
| 500 |

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

6.96 Minimum Flow Rate (PRO)



Minimum Flow Rate

Type: Intermediate Variable

Units: m³/s

Symbol: \dot{Q}_{min}

The minimum flow rate is the minimum allowable flow rate through the hydro turbine. HOMER assumes that the hydro turbine can operate only if the available stream flow is equal to or exceeds this minimum value. HOMER calculates the minimum flow rate of the hydro turbine using the following equation:

$$\dot{Q}_{min} = w_{min} \cdot \dot{Q}_{design}$$

where:

w_{min} = the hydro turbine's [minimum flow ratio](#) [%]

\dot{Q}_{design} = the hydro turbine's [design flow rate](#) [m³/s]

HOMER uses this value to calculate the hydro turbine flow rate in each time step.

See also

[Maximum flow rate](#)

[Hydro turbine flow rate](#)

[Calculating the hydro power output](#)

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6.97 Minimum Flow Ratio (PRO)



Minimum Flow Ratio

Type: Input Variable

Units: %

Symbol: w_{min}

The minimum acceptable flow rate through the hydro turbine, expressed as a percentage of the turbine's design flow rate. HOMER uses this input to calculate the minimum flow rate through the hydro turbine, and hence the actual flow rate through the hydro turbine.

See also

[Design flow rate](#)

[Minimum flow rate](#)

[Hydro turbine flow rate](#)

[Maximum flow ratio](#)

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6.98 Net Present Cost



Net Present Cost

The net present cost (or life-cycle cost) of a component is the present value of all the costs of installing and operating that component over the project lifetime, minus the present value of all the revenues that it earns over the project lifetime. HOMER calculates the net present cost of each component of the system, and of the system as a whole.

Tip: To calculate net present costs, HOMER performs a cash flow analysis. You can see the resulting table of nominal and discounted cash flows in the [Cash Flow Details Table](#).

Example: A diesel generator has an initial capital cost of \$96,000, a replacement cost of \$48,000, and a lifetime of 3.52 years. Its cost of operation and maintenance (O&M) is \$2,471/yr, and its fuel cost is \$34,969/yr. What is the net present cost of this generator over a 25-year project lifetime at an annual real interest rate of 6%?

To perform this calculation, HOMER produces a cash flow table such as the one that appears below. Except for the salvage value that occurs at the end of the 25th year, all of these cash flows are costs, so they appear as negative numbers in the table.

The first column shows the time at which each cash flow occurs, in years since the start of the project. The capital cost occurs at the start of the project, meaning year zero. The annual O&M and fuel costs occur at the end of each year, and the replacement costs happen every 3.52 years.

The second column, highlighted in yellow, contains the discount factor. The columns highlighted in green contain the nominal cash flows, and the columns highlighted in purple contain the same cash flow discounted to year zero. HOMER calculates the discounted costs by multiplying the nominal costs by the discount factor.

The bottom row below the purple discounted cash flow columns contains the net present value of each category of cash flow, as well as the total net present value, shown in red, with a value of -\$725,240. The net present value and the net present cost differ only in sign, so the net present cost of this generator over the 25-year project lifetime is \$725,240.

HOMER does a similar analysis for each component of the system, and for the system as a whole.

| Year | Discount | Nominal Cash Flows | | | | | Discounted Cash Flows | | | | | | | |
|-------|----------|--------------------|---------|-------------|---------|--------|-----------------------|---------|---------|-------------|---------|--------|---------|---------|
| | | Factor | Capital | Replacement | Salvage | O&M | Fuel | Total | Capital | Replacement | Salvage | O&M | Fuel | Total |
| 0 | 1.000 | | -96,000 | | | | | -96,000 | -96,000 | | | | -96,000 | |
| 1 | 0.943 | | | | | -2,471 | -34,969 | -37,441 | | | | -2,331 | -32,990 | -35,321 |
| 2 | 0.890 | | | | | -2,471 | -34,969 | -37,441 | | | | -2,200 | -31,123 | -33,322 |
| 3 | 0.840 | | | | | -2,471 | -34,969 | -37,441 | | | | -2,075 | -29,361 | -31,436 |
| 3.52 | 0.815 | | -48,000 | | | | | -48,000 | | -39,098 | | | | -39,098 |
| 4 | 0.792 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,958 | -27,699 | -29,657 |
| 5 | 0.747 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,847 | -26,131 | -27,978 |
| 6 | 0.705 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,742 | -24,652 | -26,394 |
| 7 | 0.665 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,644 | -23,257 | -24,900 |
| 7.04 | 0.663 | | -48,000 | | | | | -48,000 | | -31,847 | | | | -31,847 |
| 8 | 0.627 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,551 | -21,940 | -23,491 |
| 9 | 0.592 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,463 | -20,698 | -22,161 |
| 10 | 0.558 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,380 | -19,527 | -20,907 |
| 10.56 | 0.540 | | -48,000 | | | | | -48,000 | | -25,941 | | | | -25,941 |
| 11 | 0.527 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,302 | -18,421 | -19,723 |
| 12 | 0.497 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,228 | -17,379 | -18,607 |
| 13 | 0.469 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,159 | -16,395 | -17,554 |
| 14 | 0.442 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,093 | -15,467 | -16,560 |
| 14.08 | 0.440 | | -48,000 | | | | | -48,000 | | -21,130 | | | | -21,130 |
| 15 | 0.417 | | | | | -2,471 | -34,969 | -37,441 | | | | -1,031 | -14,592 | -15,623 |
| 16 | 0.394 | | | | | -2,471 | -34,969 | -37,441 | | | | -973 | -13,766 | -14,738 |
| 17 | 0.371 | | | | | -2,471 | -34,969 | -37,441 | | | | -918 | -12,986 | -13,904 |
| 17.60 | 0.359 | | -48,000 | | | | | -48,000 | | -17,212 | | | | -17,212 |
| 18 | 0.350 | | | | | -2,471 | -34,969 | -37,441 | | | | -866 | -12,251 | -13,117 |

| | | | | | | | | | | | | | |
|-------|-------|---------|----------|---------|---------|----------|------------|---------|----------|--------|---------|----------|----------|
| 19 | 0.331 | | -2,471 | -34,969 | -37,441 | | -817 | -11,558 | -12,375 | | | | |
| 20 | 0.312 | | -2,471 | -34,969 | -37,441 | | -771 | -10,904 | -11,674 | | | | |
| 21 | 0.294 | | -2,471 | -34,969 | -37,441 | | -727 | -10,286 | -11,013 | | | | |
| 21.12 | 0.292 | -48,000 | | | -48,000 | -14,020 | | | -14,020 | | | | |
| 22 | 0.278 | | -2,471 | -34,969 | -37,441 | | -686 | -9,704 | -10,390 | | | | |
| 23 | 0.262 | | -2,471 | -34,969 | -37,441 | | -647 | -9,155 | -9,802 | | | | |
| 24 | 0.247 | | -2,471 | -34,969 | -37,441 | | -610 | -8,637 | -9,247 | | | | |
| 24.64 | 0.238 | -48,000 | | | -48,000 | -11,420 | | | -11,420 | | | | |
| 25 | 0.233 | | 43,120 | -2,471 | -34,969 | 5,679 | 10,047 | -576 | -8,148 | 1,323 | | | |
| Total | | -96,000 | -336,000 | 43,120 | -61,784 | -874,234 | -1,324,899 | -96,000 | -160,668 | 10,047 | -31,593 | -447,026 | -725,239 |

Note that HOMER uses the discount factor to account not for inflation, but for the time value of money. Inflation is factored out of the analysis by the use of the real interest rate instead of the nominal interest rate. All costs in the table above are in year-zero dollars. This explains why the fuel and O&M costs remain the same for each year of the project lifetime.

But even when we factor inflation out of the analysis, the time value of money dictates that a future cash flow is worth less than a present cash flow of the same amount. The discount factor accounts for this effect; its value decreases with increasing number of years from the start of the project.

See also

[Total net present cost](#)

[Annualized cost](#)

[Present value](#)

[Future value](#)

[Salvage value](#)

[Project lifetime](#)

[Interest rate](#)

[Discount factor](#)

[Cash Flow Details table](#)

For more information

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6.99 Nominal Battery Capacity



Nominal Battery Capacity

The nominal capacity (or rated capacity) of a battery is the amount of energy that could be withdrawn from it at a particular constant current, starting from a fully charged state. The current used to rate batteries varies from one manufacturer to another, but it is typically either the 10-hour, 20-hour, or 100-hour rate. The 10-hour rate (C_{10}) is the current that causes the battery to be drained after 10 hours.

See also

[Maximum battery capacity](#)

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6.100 Nominal Hydro Power (PRO)



Nominal Hydro Power

Type: Output Variable

Units: kW

Symbol: $P_{hyd,nom}$

The nominal power of the hydro system. This would be the power produced by the hydro turbine given the available head and a stream flow equal to the design flow rate of the hydro turbine. The calculation of the nominal hydro power includes the [efficiency](#) of the hydro turbine, but not the [pipe head loss](#).

Note: HOMER uses this value only to identify the size of the hydro system, to allow easy comparison to the sizes of other components of the power system.

HOMER calculates the nominal hydro power using the following equation:

$$P_{hyd,nom} = \frac{\eta_{hyd} \cdot \rho_{water} \cdot g \cdot h \cdot \dot{Q}_{design}}{1000 \text{ W/kW}}$$

where:

$P_{hyd,nom}$ = nominal power output of the hydro turbine [kW]

η_{hyd} = [hydro turbine efficiency](#) [%]

ρ_{water} = density of water [1000 kg/m³]

g = acceleration due to gravity [9.81 m/s²]

h = [available head](#) [m]

\dot{Q}_{design} = the [design flow rate](#) of the hydro turbine [m³/s]

See also

[Calculating hydro power output](#)

For more information

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6.101 Nonrenewable Electrical Production



Nonrenewable Electrical Production

Type: Intermediate Variable

Units: kWh/yr

Symbol: E_{nonren}

The nonrenewable electrical production is the total amount of electrical energy produced annually by the nonrenewable components of the power system. HOMER uses the following equation to calculate the nonrenewable electrical production:

$$E_{nonren} = E_{prod} - E_{ren}$$

where:

E_{prod} = [total electrical production](#) [kWh]

E_{ren} = [renewable electrical production](#) [kWh]

HOMER uses this variable to calculate the renewable fraction.

See also

[Renewable fraction](#)

[Renewable thermal production](#)

[Total electrical production](#)

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6.102 Nonrenewable Thermal Production (PRO)



Nonrenewable Thermal Production P

Type: Intermediate Variable

Units: kWh/yr

Symbol: H_{nonren}

The nonrenewable thermal production is the total amount of thermal energy produced annually by non-renewable thermal energy sources. HOMER uses the following equation to calculate the nonrenewable thermal production:

$$H_{nonren} = H_{prod} - H_{ren}$$

where:

H_{prod} = [total thermal production](#) [kWh]

H_{ren} = [renewable thermal production](#) [kWh]

HOMER uses this value to calculate the renewable fraction.

See also

[Renewable fraction](#)

[Renewable electrical production](#)

[Total thermal production](#)

For more information

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6.103 NOx Emissions Penalty (PRO)



NO_x Emissions Penalty P

Type: Input Variable

Units: \$/t**Symbol:** c_{NO_x}

Use the NO_x emissions penalty to penalize systems for their production of nitrogen oxides. HOMER uses this input value when calculating the [Other O&M cost](#).

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6.104 O&M (Operation and Maintenance) Cost



O&M (Operation and Maintenance) Cost

The O&M cost of a component is the cost associated with operating and maintaining that component. The total O&M cost of the system is the sum of the O&M costs of each system component.

For most components, you enter the O&M cost as an annual amount. In the case of the generator, you enter the O&M cost as an hourly value, and HOMER multiplies that by the operating hours per year to calculate the annual O&M cost.

The grid O&M cost is the annual cost of buying power from the grid minus any revenue earned from selling power to the grid.

HOMER classifies miscellaneous annual costs, such as the system fixed O&M cost, and penalties such as emissions penalties and the capacity shortage penalty, as other O&M cost.

HOMER displays the O&M costs on the Cost Summary and Cash Flow tabs of the Simulation Results window.

See also

[Grid costs](#)

[Other O&M cost](#)

[System fixed O&M cost](#)

[Capacity shortage penalty](#)

[Emissions inputs](#)

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6.105 One-Hour Autocorrelation Factor



One-Hour Autocorrelation Factor

Type: Input Variable

Units: none

Symbol: r_1

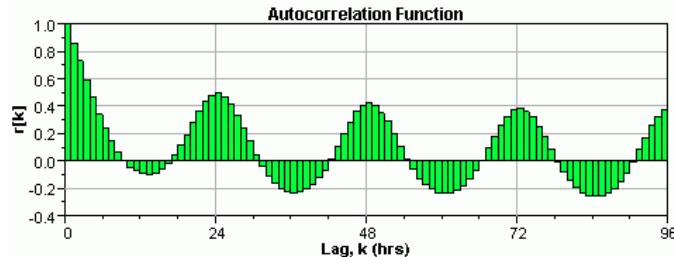
Typical Range: 0.80 - 0.95

The autocorrelation factor reflects how strongly the wind speed in one time step depends on the wind speeds in previous time steps. A high autocorrelation factor indicates that the wind speed tends to depend strongly on the wind speed in the previous time step. Lower values indicate that the wind speed tends to fluctuate in a more random fashion from one time step to the next. Among other factors, local topography can influence this parameter. Autocorrelation factors tend to be

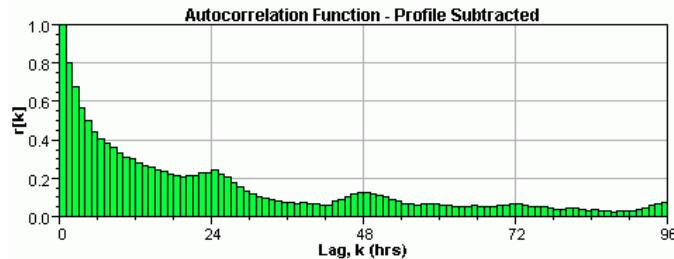
lower (0.70 - 0.80) in areas of complex topography and higher (0.90 - 0.97) in areas of more uniform topography.

To define the autocorrelation factor we first need to look at the typical autocorrelation characteristics of measured wind speed data.

As explained in the discussion of [autocorrelation](#), the daily patterns in the wind data tend to complicate its autocorrelation function. The graph below shows the autocorrelation function for the hourly wind speed data measured at San Diego, California:



To simplify the autocorrelation characteristics of wind data, we can factor out the diurnal pattern. HOMER does this by calculating the average diurnal profile, and then subtracting that profile from the wind speed data. For example, if the diurnal profile showed an average wind speed of 3.2 m/s at 1 a.m., then HOMER would subtract 3.2 m/s from all 365 values of wind speed at 1 a.m. It does the same for all 24 hours of the day, resulting in a time series that has an average of 0 m/s and no daily pattern. The autocorrelation function of this new time series typically displays almost no oscillation. The graph below shows the autocorrelation function for the San Diego data after subtracting out the diurnal profile:

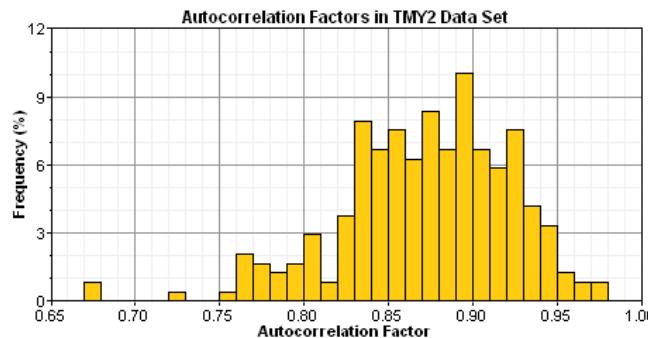


The autocorrelation function shown above dies down roughly in damped exponential fashion, so that to a good approximation,

$$r_k = r_1^k$$

We can therefore describe the degree of correlation with a single parameter. In HOMER we call this the *one-hour autocorrelation factor*, which is r_k where k is the number of time steps in one hour. If the time step is 60 minutes, the one-hour autocorrelation factor is r_1 . If the time step is 20 minutes, the one-hour autocorrelation factor is r_3 . If the time step is 10 minutes, the one-hour autocorrelation factor is r_6 .

To help HOMER users estimate the one-hour autocorrelation factor in the absence of measured data, we calculated the autocorrelation factor for each of the 239 weather stations in the TMY2 data set. The histogram below shows the resulting distribution. You can see the measured values themselves in the table of TMY2 wind parameters.



The complexity of local topography has a significant effect on the autocorrelation factor. Areas surrounded by a variety of different types of topography tend to have low (0.70 - 0.80) autocorrelation factors. For example, the stations with the lowest autocorrelation factors in the [table of measured wind parameters](#) are Los Angeles CA, Denver CO, Phoenix AZ, Lander WY, Seattle WA, and Salt Lake City UT. Each of these cities is surrounded by complex topography: mountains or hills on one side, and plains or open water on another. In such surroundings, shifts in wind direction can result in the wind having a very different character. So there is less persistence of wind speeds, and therefore lower autocorrelation [[Brett and Tuller, 1991](#)].

Areas surrounded by more uniform topography tend to have high (0.90 - 0.97) autocorrelation factors. The stations with the highest autocorrelation factors in the [table of measured wind parameters](#) include Cut Bank MT, St. Paul Island AK, and the island of Guam. Each of these sites is surrounded by relatively featureless topography: either plains or open water.

Note: the autocorrelation factor is independent of the Weibull k value. Whereas the Weibull k value reflects the breadth of the annual distribution of wind speeds, the autocorrelation factor reflects how randomly the wind speeds vary from hour to hour. The data contained in the table of measured wind parameters shows no correlation between these two parameters.

See also

[Autocorrelation](#)

[Generating synthetic wind data](#)

[Weibull k value](#)[Diurnal pattern strength](#)[Hour of peak wind speed](#)[TMY2 wind parameters](#)

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6.106 Operating Capacity



Operating Capacity

The operating capacity is the total amount of electrical generation capacity that is operating (and ready to produce electricity) at any one time. It is therefore the maximum amount of electrical load that the system could serve at a moment's notice.

To ensure reliable supply, the operating capacity should be greater than the electric load. The difference between the operating capacity and the electric load is the [operating reserve](#). As it simulates the power system, HOMER attempts to keep the operating reserve equal to or greater than the [required operating reserve](#).

In HOMER, both dispatchable power sources (generators, grid, battery bank) and renewable power sources (wind, solar, hydro) provide operating capacity. The operating capacity of a dispatchable source is equal to the maximum amount of power it could produce at a moment's notice. For example:

- A generator that is not currently operating provides no operating capacity because it cannot be counted on to provide power at a moment's notice. It must first be started, allowed to warm up, and synchronized.
- A 50 kW generator that is operating provides 50 kW of operating capacity, regardless of the actual amount of power it is producing at any time.
- The operating capacity provided by the grid is equal to the [maximum grid demand](#).
- The operating capacity provided by the battery bank is equal to the maximum amount of power it could discharge at a particular time. It therefore depends on the battery bank's state of charge and its recent charge and discharge history. For more information please see the article on the [kinetic battery model](#).

The operating capacity provided by a non-dispatchable renewable source (like a PV array or a wind turbine) is equal to the amount of power the source is currently producing, not the maximum amount of power it could produce. Since a renewable power source cannot be controlled like a dispatchable source can, its maximum capacity is not relevant in this context. So a wind turbine with a rated capacity of 50 kW that is only producing 13 kW provides only 13 kW of operating capacity.

HOMER keeps track of operating capacity and operating reserve separately for the AC and DC buses. For more information please see [operating reserve](#).

For more information

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6.107 Operating Cost



Operating Cost

Type: Output Variable

Units: \$/yr

Symbol: $C_{\text{oper,tot}}$

The operating cost is the annualized value of all costs and revenues other than initial capital costs. HOMER uses the following equation to calculate the operating cost:

$$C_{operating} = C_{ann,tot} - C_{ann,cap}$$

where:

$C_{ann,tot}$ is the [total annualized cost](#) [\$/yr]

$C_{ann,cap}$ is the total annualized capital cost [\$/yr]

The total annualized capital cost is equal to the total initial capital cost multiplied by the capital recovery factor.

HOMER displays the operating cost in the optimization results list, and at the top of the Simulation Results window. You can see the total annualized cost and the total annualized capital cost by going to the Cost Summary tab of the Simulation Results window and choosing to display annualized costs.

See also

[Total annualized cost](#)

[Simulation Results window](#)

[Cost Summary tab](#)

[Cash Flow Details Window](#)

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6.108 Operating Reserve



Operating Reserve

Operating reserve is surplus operating capacity that can instantly respond to a sudden increase in the electric load or a sudden decrease in the renewable power output. Operating reserve provides a safety margin that helps ensure reliable electricity supply despite variability in the electric load and the renewable power supply.

Tip: "Spinning reserve" is a more common term that means exactly the same thing as operating reserve. We call it operating reserve simply because batteries, fuel cells, and the grid can provide it, but they don't spin.

Power systems must always provide some amount of operating reserve because the electric load tends to jump around randomly. Without operating reserve, the load would sometimes exceed the operating capacity of the system and the lights would go out. Systems that include wind and solar power sources require additional operating reserve to guard against random decreases in the renewable power supply.

The operating reserve is equal to the [operating capacity](#) minus the electric load. HOMER keeps track of the operating capacity (and hence operating reserve) separately for the AC and DC buses. It accounts for the efficiency and the capacity of the converter when operating reserve on one bus is needed to cover load on the other bus. For example, consider a diesel-battery-inverter system serving an AC load. If the battery is discharging 2 kW but is capable of discharging 10 kW, it is providing 8 kW of DC operating reserve. If the inverter efficiency is 90% and the inverter capacity is not a limiting factor, that 8 kW of DC operating reserve corresponds to 7.2 kW of AC operating reserve. In other words, the battery bank could supply the AC load even if the load suddenly increased by as much as 7.2 kW. But the inverter capacity can be a limiting factor. If the inverter capacity (the maximum amount of AC power it can provide) is 5 kW, then the battery bank provides only 3.2 kW of AC operating reserve, since the inverter is providing 1.8 kW of AC power to serve the load and therefore has 3.2 kW of excess capacity.

When simulating systems, HOMER attempts to keep the operating reserve equal to or greater than the [required operating reserve](#). That may necessitate operating a generator that is not needed to meet the average load (or a larger generator than is needed to meet the average load) just to satisfy the operating reserve requirement.

See also

[Required operating reserve](#)

[Maximum annual capacity shortage](#)

[Total capacity shortage](#)

[Capacity shortage fraction](#)

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6.109 Other Capital Cost



Other Capital Cost

Type: Output Variable

Units: \$

Symbol: $C_{cap,other}$

HOMER uses the 'other capital cost' to account for the system fixed capital cost and, if any primary load efficiency measures are in effect for the current system configuration, the capital cost associated with those efficiency measures.

The 'other capital cost' appears in the Cash Flow Details Table.

HOMER uses the following equation to calculate the other capital cost:

$$C_{cap,other} = C_{cap,fixed} + C_{eff,1} + C_{eff,2}$$

where:

$C_{cap,fixed}$ = [system fixed capital cost](#) [\$]

$C_{eff,1}$ = cost of efficiency measures (if any) for primary load 1 [\$]

$C_{eff,2}$ = cost of efficiency measures (if any) for primary load 2 [\$]

See also

[System fixed capital cost](#)

[Other O&M cost](#)

[Cash Flow Details table](#)

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6.110 Other O&M Cost



Other O&M Cost

Type: Output Variable

Units: \$/yr

Symbol: $C_{om,other}$

The other O&M cost is the sum of:

- the system fixed O&M cost
- the penalty for capacity shortage
- the penalties for emissions of pollutants

HOMER uses the following equation to calculate the other O&M cost:

$$C_{om,other} = C_{om,fixed} + C_{cs} + C_{emissions}$$

where:

$C_{om, fixed}$ = [system fixed O&M cost](#) [\$/yr]

C_{cs} = the penalty for capacity shortage [\$/yr]

$C_{emissions}$ = the penalty for emissions [\$/yr]

HOMER uses the following equation to calculate the penalty for capacity shortage:

$$C_{cs} = c_{cs} \cdot E_{cs}$$

where:

c_{cs} = [capacity shortage penalty](#) [\$/kWh]

E_{cs} = [total capacity shortage](#) [kWh/yr]

HOMER uses the following equation to calculate the penalty for emissions:

$$C_{emissions} = \frac{c_{CO_2} M_{CO_2} + c_{CO} M_{CO} + c_{UHC} M_{UHC} + c_{PM} M_{PM} + c_{SO_2} M_{SO_2} + c_{NO_x} M_{NO_x}}{1000}$$

where:

c_{CO_2} = penalty for emissions of CO₂ [\$/t]

c_{CO} = penalty for emissions of CO [\$/t]

c_{UHC} = penalty for emissions of unburned hydrocarbons (UHC) [\$/t]

c_{PM} = penalty for emissions of particulate matter (PM) [\$/t]

c_{SO_2} = penalty for emissions of SO₂ [\$/t]

c_{NO_x} = penalty for emissions of NO_x [\$/t]

M_{CO_2} = annual emissions of CO₂ [kg/yr]

M_{CO} = annual emissions of CO [kg/yr]

M_{UHC} = annual emissions of unburned hydrocarbons (UHC) [kg/yr]

M_{PM} = annual emissions of particulate matter (PM) [kg/yr]

M_{SO_2} = annual emissions of SO₂ [kg/yr]

M_{NO_x} = annual emissions of NO_x [kg/yr]

You can specify the penalties for each pollutant on the [Emissions Inputs](#) window. For information on how HOMER calculates emissions of each pollutant, please see the article on [how HOMER calculates emissions](#).

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6.111 Pipe Head Loss (PRO)



Pipe Head Loss

Type: Input Variable

Units: %

Symbol: f_h

The frictional loss in the hydro pipeline, expressed as a fraction of the [available head](#).

Water (like any viscous fluid) flowing through a pipe experiences a loss in pressure due to friction. We can express this pressure loss in terms of a loss of head, where head is the vertical drop through which the fluid flows. In HOMER, you specify the pipe head loss as a percentage of the available head.

Small high-head, low-flow hydro systems typically experience pipe head losses of between 10% and 20%. With low-head systems, pipe head losses are typically only a few percent.

For assistance in estimating the pipe head loss, click the button beside the head loss input to access the [Pipe Head Loss Calculator](#) window.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.112 PM Emissions Penalty (PRO)



PM Emissions Penalty

Type: Input Variable

Units: \$/t

Symbol: c_{PM}

Use the PM emissions penalty to penalize systems for their production of particulate. HOMER uses this input value when calculating the [Other O&M cost](#).

For more information

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6.113 Present Value



Present Value

The present value is the equivalent value at the present of a set of future cash flows, taking into account the time value of money.

For example, if the real interest rate is 6%, the present value of a \$1000 payment twelve years in the future is $\$1000 / ((1.06)^{12}) = \497 .

See also

[Interest rate](#)

[Capital recovery factor](#)

[Future value](#)

For more information

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6.114 Probability Transformation



Probability Transformation

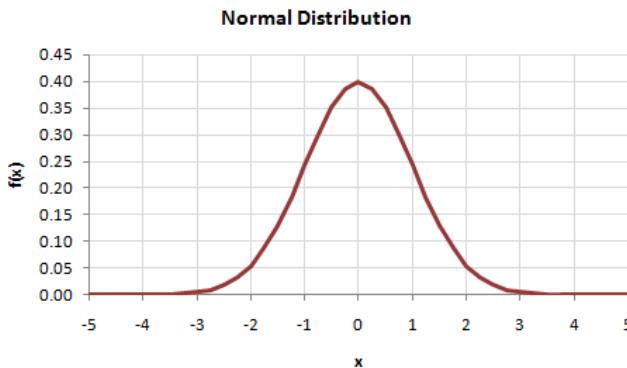
A probability transformation is a statistical procedure by which one modifies a set of numbers to conform to a desired probability distribution function.

To perform a probability transformation, HOMER first calculates the cumulative distribution function of the original set of data -- we will refer to this as the 'original CDF'. Then for each original data point, it performs the following steps:

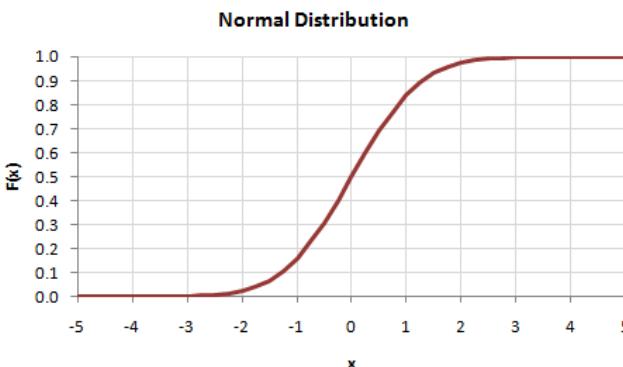
1. It refers to the original CDF to calculate the percentile value corresponding to that original data point
2. It refers to the desired CDF to calculate the transformed value corresponding to that same percentile value

Let's look at an example to illustrate this process. Imagine that we have a set of data that conform to a normal distribution, and we want to transform it so that it conforms to a Weibull distribution. (HOMER does exactly this when synthesizing wind speed data.)

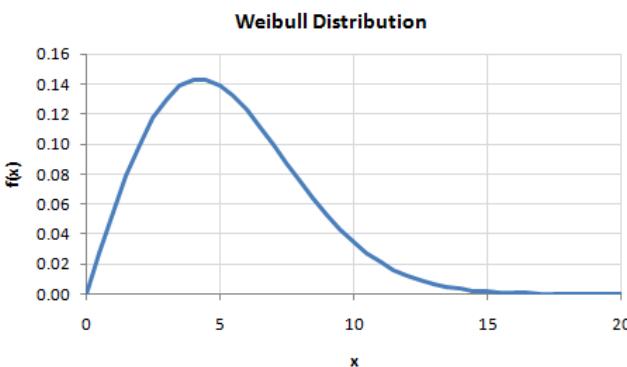
If our normally-distributed data had a mean of zero and a standard deviation of 1, its probability distribution function would look like so:



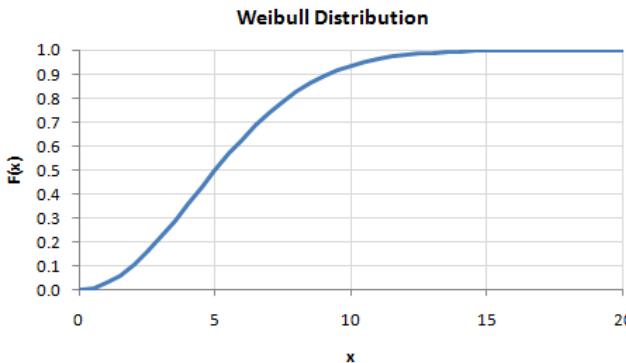
And its cumulative distribution function -- the original CDF -- would look like so:



Imagine that we wish to transform this data to fit a Weibull distribution with a mean value of 6 and a Weibull k value of 2. Our desired probability distribution function would therefore look like so:



And our desired cumulative distribution function -- the desired CDF -- would look like so:



To transform each value in the original data set, we would refer to the original CDF to find its corresponding y -value, then we would take that same y -value to the desired CDF and find its corresponding x -value.

An original value of zero, for example, corresponds to a CDF value of 0.5 on the original CDF. Looking at the desired CDF, we find that the value corresponding to a CDF value of 0.5 is approximately 5. That means that any zero value in the original data set gets transformed into a value of 5 in the transformed data set. Similarly, an original value of -1 would be transformed to value of approximately 2.5, and an original value of 1.5 would be transformed to a value of approximately 10.

This example looks at transforming data from a normal distribution to a Weibull distribution, but with this same probability transformation approach, we could transform from any distribution to any other distribution.

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6.115 Project Lifetime



Project Lifetime

Type: Input Variable

Units: yr

Symbol: R_{proj}

The project lifetime is the length of time over which the costs of the system occur. HOMER uses the project lifetime to calculate annualized costs from net present costs. HOMER assumes that salvage values occur at the end of the project lifetime.

You enter the project lifetime in the Economics Inputs window.

See also

[Economic Inputs window](#)

[Annualized cost](#)

[Net present cost](#)

[Salvage value](#)

[Interest rate](#)

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6.116 PV Azimuth



PV Azimuth

Type: Input Variable

Units: °

Symbol: g

The azimuth is the direction towards which the PV panels face. Due south is 0°, due east is -90°, due west is 90°, and due north is 180°. With fixed-azimuth systems, the panels are almost always oriented towards the equator (0° azimuth in the northern hemisphere, 180° azimuth in the southern hemisphere).

The azimuth is insignificant if the panels are mounted horizontally (zero slope). If you choose vertical-axis or two-axis tracking, HOMER does not let you enter the azimuth, but rather calculates it in each time step as the tracking system moves the PV array.

See also

[PV tracking system](#)

[PV slope](#)

[PV Inputs window](#)

For more information

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6.117 PV Derating Factor



PV Derating Factor

Type: Input Variable

Units: %

Symbol: f_{PV}

The PV derating factor is a scaling factor that HOMER applies to the PV array power output to account for reduced output in real-world operating conditions compared to the conditions under which the PV panel was rated.

Use the derating factor to account for such factors as soiling of the panels, wiring losses, shading, snow cover, aging, and so on. If you choose not to explicitly model the effect of temperature on the PV array, then you should also include temperature-related effects in the derating factor.

See also:

[Does HOMER account for the effect of temperature on the PV array?](#)

[Can HOMER model a maximum power point tracker?](#)

[How HOMER calculates the PV array power output](#)

[PV Inputs window](#)

For more information

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6.118 PV Efficiency at Standard Test Conditions (PRO)



PV Efficiency at Standard Test Conditions

Type: Input Variable

Units: %

Symbol: $h_{mp,STC}$

The efficiency with which the PV array converts sunlight into electricity at its maximum power point under standard test conditions. HOMER uses the efficiency to calculate the PV cell temperature.

PV manufacturers rarely report this efficiency in their product brochures, but one can calculate it for any PV module using the following equation:

$$\eta_{mp,STC} = \frac{Y_{PV}}{A_{PV} G_{T,STC}}$$

where:

$h_{mp,STC}$ is the efficiency of the PV module under standard test conditions [%]

Y_{PV} is the rated power output of the PV module under standard test conditions [kW]

A_{PV} is the surface area of the PV module [m^2]

$G_{T,STC}$ is the radiation at standard test conditions [$1\text{ kW}/m^2$]

In November 2007 we performed a non-exhaustive, non-scientific survey of the product brochures available for some of the commonly available PV modules. The following table contains the average values of the efficiency under standard test conditions for various types of PV modules in our survey.

| PV Module Type | Modules In Survey | Average Value of Efficiency at STC [%] |
|--|-------------------|--|
| Polycrystalline silicon | 10 | 13.0 |
| Monocrystalline silicon | 8 | 13.5 |
| Monocrystalline/amorphous silicon hybrid | 1 | 16.4 |
| Thin film amorphous silicon | 4 | 5.5 |
| Thin film CIS | 1 | 8.2 |

Tip: HOMER assumes the PV array always operates at its maximum power point, as it would if it were controlled by a maximum power point tracker.

See also:

[How HOMER calculates the PV cell temperature](#)

[Standard test conditions](#)

[PV Inputs window](#)

[Can HOMER model a maximum power point tracker?](#)

For more information

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6.119 PV Nominal Operating Cell Temperature (PRO)



PV Nominal Operating Cell Temperature

Type: Input Variable

Units: °C

Symbol: $T_{c,NOCT}$

The nominal operating cell temperature is the surface temperature that the PV array would reach if it were exposed to 0.8 kW/m^2 of solar radiation, an ambient temperature of 20°C , and a wind speed of 1 m/s . Sometimes called the "normal operating cell temperature" and frequently abbreviated NOCT, the nominal operating cell temperature provides a measure of how the PV cell temperature (the surface temperature of the PV array) varies with the ambient temperature and the solar radiation. HOMER uses the NOCT to calculate the PV cell temperature.

PV manufacturers typically report the nominal operating cell temperature as part of their product data. In our non-exhaustive survey of commercially-available PV modules in November 2007, about 60% of the product data sheets specified the NOCT, with the values varying over a narrow range from 45°C to 48°C .

See also:

[How HOMER calculates the PV cell temperature](#)

[PV Inputs window](#)

For more information

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6.120 PV Slope



PV Slope

Type: Input Variable

Units: °

Symbol: b

The slope is the angle at which the panels are mounted relative to the horizontal. A slope of 0° corresponds to horizontal, and 90° corresponds to vertical. With fixed-slope systems, a slope roughly equal to the latitude will typically maximize the annual PV energy production. The azimuth specifies the direction towards which the panels slope.

If you choose a horizontal-axis or two-axis tracking system, HOMER does not let you enter the slope, but rather calculates it in each time step.

See also

[PV tracking system](#)

[PV azimuth](#)

[PV Inputs window](#)

For more information

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6.121 PV Temperature Coefficient of Power (PRO)

PV Temperature Coefficient of Power

Type: Input Variable

Units: %/°C

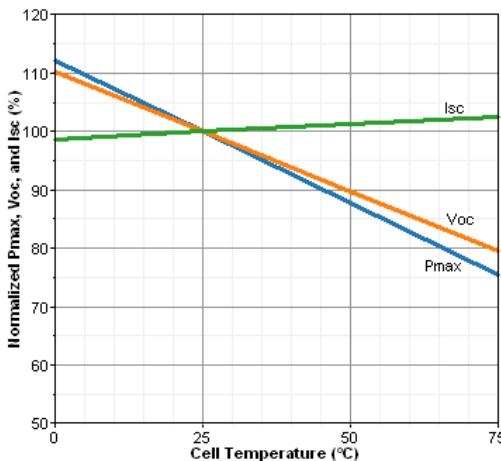
Symbol: α_p

The temperature coefficient of power indicates how strongly the PV array power output depends on the cell temperature, meaning the surface temperature of the PV array. It is a negative number because power output decreases with increasing cell temperature. Manufacturers of PV modules usually provide this coefficient in their product brochures, often labeled either as "temperature coefficient of power", "power temperature coefficient", or "max. power temperature coefficient".

In November 2007 we performed a non-exhaustive, non-scientific survey of the product brochures available for some of the commonly available PV modules. The following table contains the average values of the temperature coefficient of power for various types of PV modules in our survey.

| PV Module Type | Modules In Survey | Modules Reporting α_p | Average Value of α_p |
|--|-------------------|------------------------------|-----------------------------|
| | | | [%/°C] |
| Polycrystalline silicon | 10 | 7 | -0.48 |
| Monocrystalline silicon | 8 | 4 | -0.46 |
| Monocrystalline/amorphous silicon hybrid | 1 | 1 | -0.30 |
| Thin film amorphous silicon | 4 | 4 | -0.20 |
| Thin film CIS | 1 | 1 | -0.60 |

If the product brochure does not specify the value of the temperature coefficient of power, it may contain a graph showing the normalized performance versus cell temperature, like the sample shown below. In such a graph, the slope of the power line (labeled P_{max} in this sample) is the temperature coefficient of power. The normalized open-circuit voltage and short-circuit current also appear in this sample.



Some product brochures do not specify the temperature coefficient of power, but do specify the temperature coefficient of the open-circuit voltage. In that case, you can calculate the temperature coefficient of power using the approximation suggested by [Duffie and Beckman \(1991\)](#):

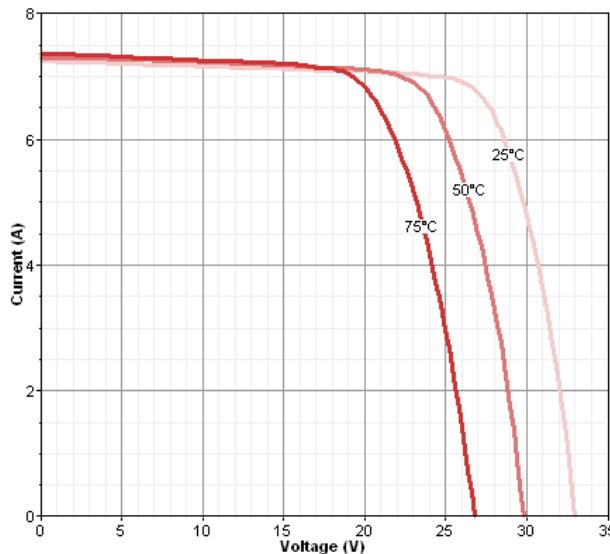
$$\alpha_p \approx \frac{\mu_{V_{oc}}}{V_{mp}}$$

where:

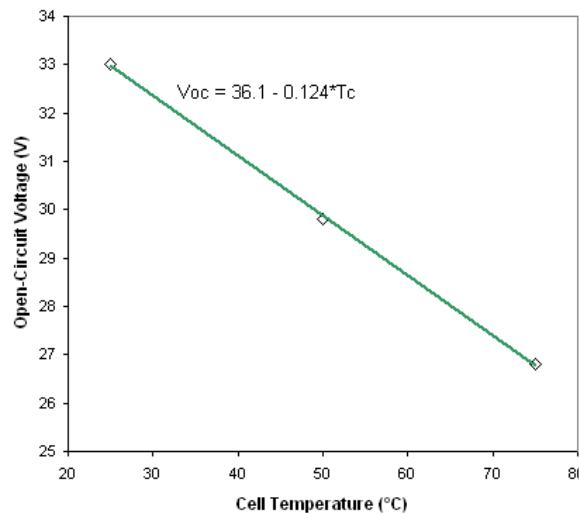
$\mu_{V_{oc}}$ is the temperature coefficient of the open-circuit voltage [V/°C]

V_{mp} is the voltage at the maximum power point under [standard test conditions](#) [V]

If the brochure does not specify the temperature coefficient of the open-circuit voltage but it contains a graph showing the IV curve at different cell temperatures, such as the sample shown below, you can use the graph to calculate the temperature coefficient of the open-circuit voltage.



To do so, plot the open-circuit voltage (the voltage at the bottom of the IV curve) versus cell temperature, and find the slope of that line, as shown below. The slope of that line is the temperature coefficient of the open-circuit voltage. In this example, the slope of the line is -0.124 V/°C.



See also:

[How HOMER calculates the PV cell temperature](#)

[How HOMER calculates the PV array power output](#)

[PV Inputs window](#)

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6.122 PV Tracking System (PRO)

PV Tracking System



Type: Input Variable

Units: none

Photovoltaic panels are typically mounted at a fixed orientation. They can, however, be made to "track" the sun in order to maximize the incident solar radiation. Tracking systems are classified according to the number of axes of rotation and the frequency with which the adjustments are made. HOMER can consider the following tracking systems:

- **No Tracking:** Panels are mounted at a fixed slope and azimuth. This is the simplest and most common case.
- **Horizontal Axis, monthly adjustment:** Rotation is about a horizontal east-west axis. The slope is adjusted on the first day of every month so that the sun's rays are perpendicular to the surface at noon of that day.
- **Horizontal Axis, weekly adjustment:** Rotation is about a horizontal east-west axis. The slope is adjusted on the first day of every week so that the sun's rays are perpendicular to the surface at noon of that day.
- **Horizontal Axis, daily adjustment:** Rotation is about a horizontal east-west axis. The slope is adjusted each day so that the sun's rays are perpendicular to the surface at noon.
- **Horizontal Axis, continuous adjustment:** Rotation is about a horizontal east-west axis. The slope is adjusted continually in order to minimize the angle of incidence.
- **Vertical Axis, continuous adjustment:** Rotation is about a vertical axis. The slope is fixed, but the azimuth is continually adjusted to minimize the angle of incidence.
- **Two Axis:** The panels are rotated about both horizontal and vertical axes so that the sun's rays are always perpendicular to the surface. This type of tracking system maximizes the power production of the PV panels, but it is the most expensive.

See also

[PV slope](#)

[PV azimuth](#)

[PV Inputs window](#)

For more information

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6.123 Reformer Efficiency (PRO)



Reformer Efficiency [P](#)

Type: Input Variable

Units: %

Symbol: h_{ref}

The efficiency with which the reformer converts the fuel to hydrogen. This is equal to the energy content (based on LHV) of the hydrogen out divided by the energy content (based on LHV) of the fuel in. HOMER uses this value to determine how much fuel the reformer uses to produce a certain amount of hydrogen.

For more information

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6.124 Relative State of Charge



Relative State of Charge

The relative state of charge is the ratio of the current [absolute state of charge](#) to the maximum capacity of the battery bank. When the batteries are fully charged, the relative state of charge is 100%. Wherever HOMER reports the amount of energy stored in the battery bank, it reports the relative state of charge.

State of charge is often abbreviated as SOC.

See also

[Absolute state of charge](#)

For more information

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6.125 Renewable Electrical Production



Renewable Electrical Production

Type: Intermediate Variable

Units: kWh/yr

Symbol: E_{ren}

The renewable electrical production is the total amount of electrical energy produced annually by the renewable components of the power system. It is the sum of the electrical energy produced by the PV array, the wind turbines, and the hydro system, plus that portion of the electrical energy produced by each generator which originates from biomass.

HOMER uses this variable to calculate the renewable fraction.

See also

[Renewable fraction](#)

[Renewable thermal production](#)

[Total electrical production](#)

For more information

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6.126 Renewable Fraction



Renewable Fraction

Type: Output Variable

Units: none

Symbol: f_{ren}

The renewable fraction is the fraction of the energy delivered to the load that originated from renewable power sources. HOMER calculates the renewable fraction using the following equation:

$$f_{ren} = 1 - \frac{E_{nonren} + H_{nonren}}{E_{served} + H_{served}}$$

where:

- E_{nonren} = [nonrenewable electrical production](#) [kWh/yr]
- $E_{grid,sales}$ = energy sold to the grid [kWh/yr] (included in E_{served})
- H_{nonren} = [nonrenewable thermal production](#) [kWh/yr]
- E_{served} = [total electrical load served](#) [kWh/yr]
- H_{served} = [total thermal load served](#) [kWh/yr]

HOMER abbreviates the renewable fraction as "Ren. Frac." in the sensitivity and optimization results tables.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.127 Renewable Penetration



Renewable Penetration

Type: Output Variable

Units: none

Symbol: p_{ren}

In every time step, HOMER calculates the renewable penetration using the following equation:

$$p_{ren} = \frac{P_{ren}}{L_{served}}$$

where:

P_{ren} = total renewable electrical power output in this time step [kW]

L_{served} = total electrical load served in this time step [kW]

On the [Electrical](#) tab of the Simulation Results window, HOMER reports the maximum value of renewable penetration that occurs during the year.

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.128 Renewable Thermal Production (PRO)



Renewable Thermal Production

Type: Intermediate Variable

Units: kWh/yr
Symbol: H_{ren}

The renewable thermal production is the total amount of thermal energy produced annually by renewable-fuelled generators. The renewable thermal output of each generator is equal to that portion of its total thermal output originating from biomass (as opposed to fossil fuel, if the generator is cofired).

HOMER uses this value to calculate the renewable fraction.

See also

[Renewable fraction](#)

[Renewable electrical production](#)

[Total thermal production](#)

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6.129 Replacement Cost



Replacement Cost

The replacement cost is the cost of replacing a component at the end of its lifetime. This may be different from the initial capital cost for several reasons:

- Not all of the component may require replacement at the end of its life. For example, the wind turbine nacelle may need replacement but the tower may not.
- The initial capital cost may be reduced or eliminated by a donor organization, but the replacement cost may not.
- You may want to account for the fixed costs (e.g. travel cost) of a visit to the site. At initial construction, these costs are shared by all components, but at replacement time they may not.
- You may want to account for a reduction over time in the purchase cost of a particular technology.

Important: the replacement cost is not meant to account for **inflation**. All costs in HOMER are *real costs*, defined in terms of constant dollars. For more information, please see that article on the interest rate.

Tip: To see when replacement costs occur and how they affect the total net present cost, see the [Cash Flow Details Table](#).

Replacement cost is abbreviated as Repl. in HOMER's cost input tables.

See also

[Initial capital cost](#)

[Interest rate](#)

[Cash Flow Details table](#)

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6.130 Required Operating Capacity



Required Operating Capacity

HOMER calculates the required operating capacity each time step by adding the [required operating reserve](#) to the electric load. When simulating the operation of a file:///C:/users/jonathan/documents/HOMER_help/HOMERManual_SourceCode_output/SingleHTML/HOMER.htm

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power system, HOMER attempts to keep the operating capacity equal to or greater than the required operating capacity. HOMER records any shortfall as a [capacity shortage](#).

See also

[Required operating reserve](#)

[Maximum annual capacity shortage](#)

[Total capacity shortage](#)

[Capacity shortage fraction](#)

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6.131 Required Operating Reserve



Required Operating Reserve

Required operating reserve is the minimum amount of [operating reserve](#) that the system must be capable of providing. HOMER calculates the required operating reserve for each time step based on the values that you enter on the [Constraints](#) window. Whenever possible, HOMER ensures that enough dispatchable capacity is available to keep the operating reserve equal to or greater than the required operating reserve. HOMER records any shortfall as a [capacity shortage](#).

Because operating reserve guards against increases in the load or decreases in the renewable power output, the required operating reserve is a function of both the load and the renewable power output (specifically, the solar and wind power output, since the hydro power output typically experiences little short-term variability). The amount of required operating reserve therefore typically changes from one time step to the next. In each time step, HOMER calculates the required operating reserve on the AC and DC buses using the following equations:

$$\begin{aligned} L_{res,AC} &= r_{load} \cdot L_{prim,AC} + r_{peakload} \cdot \hat{L}_{prim,AC} + r_{wind} \cdot P_{wind,AC} \\ L_{res,DC} &= r_{load} \cdot L_{prim,DC} + r_{peakload} \cdot \hat{L}_{prim,DC} + r_{wind} \cdot P_{wind,DC} + r_{solar} \cdot P_{PV} \end{aligned}$$

where:

$L_{res,AC}$ is the required operating reserve on the AC bus

$L_{res,DC}$ is the required operating reserve on the DC bus

r_{load} is the input 'operating reserve as a percent of load in the current time step'

$L_{prim,AC}$ is the average AC primary load in the current time step

$L_{prim,DC}$ is the average DC primary load in the current time step

$r_{peakload}$ is the input 'operating reserve as a percent of annual peak load'

$\hat{L}_{prim,AC}$ is the highest AC primary load experienced by the system during the year

$\hat{L}_{prim,DC}$ is the highest DC primary load experienced by the system during the year

r_{wind} is the input 'operating reserve as a percent of wind power output'

$P_{wind,AC}$ is the average AC wind power output in the current time step

$P_{wind,DC}$ is the average DC wind power output in the current time step

r_{solar} is the input 'operating reserve as a percent of solar power output'

P_{PV} is the average PV array output in the current time step

See also

[Maximum annual capacity shortage](#)

[Total capacity shortage](#)

[Capacity shortage fraction](#)

For more information

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6.132 Residual Flow (PRO)



Residual Flow P

Type: Input Variable

Units: L/s

Symbol: $Q_{residual}$

The residual flow is the quantity of water that must remain undisturbed in the waterway for ecological reasons, such as to support fish populations. It is the quantity of water that cannot be diverted to flow through the hydro turbine.

HOMER uses the residual flow to calculate the flow rate available to the hydro turbine.

See also

[Hydro Turbine Flow Rate](#)

For more information

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6.133 Resource



Resource

In HOMER, a "resource" is anything coming from outside the system that is used by a [component](#) to generate electric or thermal energy. Wind, solar radiation, and diesel fuel are examples of resources. Electrolyzed hydrogen is not, because it is produced by the system.

For more information

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6.134 Return On Investment



Return On Investment

Type: Intermediate Variable

Units: \$/kWh**Symbol:** c_{boiler}

The marginal cost of thermal energy from the boiler. HOMER uses this value when calculating the [levelized cost of energy](#). HOMER calculates the boiler marginal cost with the following equation:

$$c_{boiler} = \frac{3.6 \cdot (c_{fuel} + c_{boiler,emissions})}{\eta_{boiler} \cdot LHV_{fuel}}$$

where:

c_{fuel} = cost of fuel [\$/kg of fuel]

$c_{boiler,emissions}$ = cost penalty associated with emissions from the boiler [\$/kg of fuel]

η_{boiler} = boiler efficiency [unitless]

LHV_{fuel} = the lower heating value of the boiler fuel [MJ/kg]

The factor of 3.6 in the above equation arises because 1 kWh = 3.6 MJ.

Note: The fuel cost in the above equation is per kg, not per L or m³. For fuels denominated in volumetric units, HOMER calculates the cost per kg using the fuel density.

HOMER calculates the cost penalty associated with boiler emissions using the following equation:

$$c_{boiler,emissions} = \frac{c_{CO_2}\gamma_{CO_2} + c_{CO}\gamma_{CO} + c_{UHC}\gamma_{UHC} + c_{PM}\gamma_{PM} + c_{SO_2}\gamma_{SO_2} + c_{NO_x}\gamma_{NO_x}}{1000}$$

where:

c_{CO_2} = penalty for emissions of CO₂ [\$/t]

c_{CO} = penalty for emissions of CO [\$/t]

c_{UHC} = penalty for emissions of unburned hydrocarbons (UHC) [\$/t]

c_{PM} = penalty for emissions of particulate matter (PM) [\$/t]

c_{SO_2} = penalty for emissions of SO₂ [\$/t]

c_{NO_x} = penalty for emissions of NO_x [\$/t]

g_{CO_2} = boiler's carbon dioxide emissions coefficient [kg CO₂ / kg fuel]

g_{CO} = boiler's carbon monoxide emissions coefficient [kg CO / kg fuel]

g_{UHC} = boiler's unburned hydrocarbons emissions coefficient [kg UHC / kg fuel]

g_{PM} = boiler's particulate matter emissions coefficient [kg PM / kg fuel]

g_{SO_2} = boiler's SO₂ emissions coefficient [kg SO₂ / kg fuel]

g_{NO_x} = boiler's NO_x emissions coefficient [kg NO_x / kg fuel]

HOMER calculates the CO₂ emissions coefficient using the following equation:

$$\gamma_{CO_2} = \frac{44}{12} \left[f_{C,fuel}(1 - \gamma_{UHC}) - \left(\frac{12}{28} \right) \gamma_{CO} \right]$$

where:

$f_{C,fuel}$ = the carbon content of the fuel [unitless]

g_{CO} = boiler's carbon monoxide emissions coefficient [kg CO / kg fuel]

g_{UHC} = boiler's unburned hydrocarbons emissions coefficient [kg UHC / kg fuel]

Note that the factors of 44/12 and 12/28 in the above equation arise because the molecular weights of C, CO, and CO₂ are equal to 12, 28, and 44 respectively.

HOMER calculates the SO₂ emissions coefficient using the following equation:

$$\gamma_{SO_2} = 2 f_{S,fuel} (1 - \gamma_{UHC} - x_{PM})$$

where:

$f_{S,fuel}$ = the sulfur content of the fuel [unitless]

g_{UHC} = boiler's unburned hydrocarbons emissions coefficient [kg UHC / kg fuel]

x_{PM} = the proportion of fuel sulfur converted to particulate matter [unitless]

Note that the factor of 2 in the above equation arises because the molecular weight of SO₂ (64) is twice that of S (32).

See also:

[Levelized cost of energy](#)

For more information

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6.135 Salvage Value



Salvage Value

Salvage value is the value remaining in a component of the power system at the end of the project lifetime. HOMER assumes *linear depreciation* of components, meaning that the salvage value of a component is directly proportional to its remaining life. It also assumes that the salvage value depends on the replacement cost rather than the initial capital cost. HOMER calculates salvage value using the following equation:

$$S = C_{rep} \cdot \frac{R_{rem}}{R_{comp}}$$

R_{rem} , the remaining life of the component at the end of the project lifetime, is given by:

$$R_{rem} = R_{comp} - (R_{proj} - R_{rep})$$

R_{rep} , the replacement cost duration, is given by:

$$R_{rep} = R_{comp} \cdot \text{INT}\left(\frac{R_{proj}}{R_{comp}}\right)$$

other definitions:

C_{rep} = replacement cost [\$]

R_{comp} = component lifetime [yr]

R_{proj} = project lifetime [yr]

$\text{INT}()$ = a function that returns the integer amount of a real number. For example, $\text{INT}(6.843) = 6$

HOMER assumes that salvage value accrues at the end of the project lifetime.

Tip: You can see the salvage value and all other cash flows in the [Cash Flow Details Table](#).

Example 1: A wind turbine has a capital cost of \$1 million, a replacement cost of \$750,000, and a 25-year lifetime. At the end of a 20-year project lifetime, what is its salvage value? Solution: the replacement cost duration, R_{rep} , is zero, the remaining life, R_{rem} , is 5 years, so the salvage value is $\$750,000 * 5/25 = \$150,000$. Note that the capital cost does not affect the calculation of salvage value.

Example 2: A diesel generator has a capital cost of \$400,000, a replacement cost of \$350,000, and a lifetime of 7.85 years. At the end of a 30-year project lifetime, what is its salvage value? Solution: the replacement cost duration, R_{rep} , is 23.55 years, the remaining life, R_{rem} , is 6.45 years, so the salvage value is $\$350,000 * 6.45/7.85 = \$287,580$.

See also

[Project lifetime](#)

[Replacement cost](#)

[Cash Flow Details table](#)

For more information

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6.136 Search Space



Search Space

The Search Space is the set of [decision variable](#) values that HOMER searches to locate the optimal system. The Search Space is part of the [Design Values](#).

If you are using [SearchSizer](#), when you click Calculate, HOMER automatically finds the optimal decision variable values that represent the least-cost [system](#) for each [sensitivity case](#).

If you are specifying your own search space, you define the search space by specifying the sizes and quantities of the different system components in the [Search Space](#) for a particular [component](#) or in the Design Values window.

See also:

[How HOMER Determines the Search Space Values with SearchSizer](#)

[SearchSizer](#)

For more information

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6.137 Sensitivity Analysis



Sensitivity Analysis

You can perform a sensitivity analysis by entering multiple values for a particular input variable. HOMER repeats its optimization process for each value of that variable and lets you see how the results are affected. An input variable for which you have specified multiple values is called a [sensitivity variable](#), and you can define as many sensitivity variables as you want.

A sensitivity analysis can be referred to as *one-dimensional* if there is a single sensitivity variable. If there are two sensitivity variables, it is a *two-dimensional* sensitivity analysis, and so on. HOMER's most powerful graphical capabilities were developed to help examine the results of sensitivity analyses of two or more dimensions.

For more information, please see [Why would I want to do a sensitivity analysis?](#)

See also

[Sensitivity variable](#)

[Sensitivity case](#)

For more information

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6.138 Sensitivity Case



Sensitivity Case

A sensitivity case is a specific combination of [sensitivity variable](#) values. For example, say you have specified four values for the average annual wind speed (3 m/s, 4 m/s, 5 m/s, and 6 m/s) and three values for the fuel price (\$0.40/L, \$0.50/L, and \$0.60/L). Then you have specified twelve different sensitivity cases because there are twelve different combinations of sensitivity values. HOMER performs a separate optimization for each sensitivity case.

If there are no sensitivity variables, then there is only one sensitivity case.

For more information

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6.139 Sensitivity Variable



Sensitivity Variable

A sensitivity variable is an input variable for which multiple values have been specified. HOMER performs a separate optimization procedure for each specified value. For an explanation of why you would do this, please see [Why would I do a sensitivity analysis?](#)

It is easy to specify multiple values for an input variable. All variables for which multiple values can be specified have a sensitivity button beside them. The sensitivity button for the [Annual Real Interest Rate](#) can be seen below next to the input field:

To specify multiple values, click on the sensitivity button and enter any number of values on the [sensitivity values dialog box](#):

The values do not have to be evenly spaced, and you can enter them in any order you want. If there are other sensitivity variables, they will be listed in the dropdown box labeled "Link with". By selecting one of these variables, you can perform a [linked sensitivity](#).

When you click OK, the sensitivity button will display the number of values that have been specified for the Annual Real Interest Rate:

For capital, replacement and O&M cost variables, rather than performing a sensitivity analysis directly on these costs, there is a *multiplier variable* which scales these values. If, for example, you entered a PV Capital of \$1000/kW, then Capital Cost Multipliers of 3, 4, and 5 would correspond to effective PV Capital Costs of \$3000/kW, \$4000/kW, and \$5000/kW.

For variables specified in the component cost tables, the sensitivity concept is slightly different. Inputs like the initial capital cost are not defined by a single value, but by a column in the component cost table. There may be just one value in that column, but there may be more. For each such variable, there is a *multiplier variable* which is accessed by clicking on the sensitivity button below the appropriate table column. Pictured below is the wind turbine cost table and the sensitivity buttons for the initial capital cost, replacement cost, and O&M cost.

| Costs | | | |
|-----------|--------------|--------------|-------------|
| Size (kW) | Capital (\$) | Replace (\$) | O&M (\$/yr) |
| 1 | 5500 | 3000 | 80 |
| 2 | 10500 | 5700 | 120 |
| | | | |

Multiplier:

Because you can enter several values for these multiplier variables, they allow you to do a sensitivity on any column. The multiplier simply scales the whole column up or down. You can edit the first value in the sensitivity table for a multiplier variable. That's not the case with normal sensitivity values, where the first value in the sensitivity table is the value entered in the corresponding edit box.

HOMER designs an optimal hybrid system for each [sensitivity case](#).

For more information

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6.140 Setpoint State of Charge



Setpoint State of Charge

The setpoint state of charge is a parameter that can be applied to the [cycle charging strategy](#). If a setpoint state of charge is applied, once the system starts to charge the battery bank it will not stop until the battery bank reaches the setpoint state of charge.

The setpoint state of charge tends to reduce the amount of time the battery bank spends at a low state of charge. It also tends to reduce the number of generator starts and the number of battery charge-discharge cycles that occur throughout the year.

The setpoint state of charge appears on the [System Control Inputs](#) window.

See also

[Cycle charging strategy](#)

For more information

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6.141 Simulation Time Step



Simulation Time Step

The default simulation time step in HOMER is 1 hour (60 minutes).

HOMER Pro can simulate system operation with any time step from as long as several hours to as short as one minute. You specify the simulation time step on the [System Control Inputs tab](#).

The shorter the time step, the more time steps HOMER must simulate to cover one year, so the longer each simulation takes.

The simulation time step does not have to match the time step of any time series data you may have imported. For example, if you import 10-minute wind data and 60-minute load data, and you simulate on a 10-minute time step, HOMER will divide each 60-minute load value into six identical 10-minute values. If you simulate on a 60-minute time step, HOMER will aggregate six 10-minute wind speed values together into a single 60-minute value for each time step. Or you could choose to simulate using a 30-minute time step, in which case it would aggregate the wind values and disaggregate the load values.

For more information

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6.142 Sinking Fund Factor



Sinking Fund Factor

The sinking fund factor is a ratio used to calculate the [future value](#) of a series of equal annual cash flows. The equation for the sinking fund factor is:

$$\text{SFF}(i, N) = \frac{i}{(1 + i)^N - 1}$$

where:

i = [real interest rate](#)

N = number of years

Example: for i = 7% and N = 5 years, the sinking fund factor is equal to 0.1739. Therefore, five annual payments of \$173.90 earning 7% interest would be worth \$1000.00 at the end of the fifth year.

See also

[Capital recovery factor](#)

For more information

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6.143 SO₂ Emissions Penalty (PRO)



SO₂ Emissions Penalty P

Type: Input Variable

Units: \$/t

Symbol: c_{SO₂}

Use the SO₂ emissions penalty to penalize systems for their production of sulfur dioxide. HOMER uses this input value when calculating the [Other O&M cost](#).

For more information

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6.144 Solar Absorptance



Solar Absorptance

The solar absorptance of a surface is the fraction of the sun's radiation that the surface absorbs.

The solar absorptance is a factor in the calculation of the PV array temperature. But it is a relatively unimportant one, so rather than making you enter it, HOMER uses the assumption suggested by [Duffie and Beckman \(1991\)](#) that the product of the solar absorptance and the solar transmittance is 0.9 or 90%.

See also

[Solar transmittance](#)

[How HOMER calculates the PV cell temperature](#)

For more information

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6.145 Solar Transmittance



Solar Transmittance

The solar transmittance of a surface is the fraction of the sun's radiation that are transmitted through the surface.

The solar transmittance is a factor in the calculation of the PV array temperature. But it is a relatively unimportant one, so rather than making you enter it, HOMER uses the assumption suggested by [Duffie and Beckman \(1991\)](#) that the product of the solar absorptance and the solar transmittance is 0.9 or 90%.

See also

[Solar absorptance](#)

[How HOMER calculates the PV cell temperature](#)

For more information

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6.146 Specific Fuel Consumption



Specific Fuel Consumption

Type: Output Variable

Units: L/kWh, m³/kWh, or kg/kWh, depending on the units of the fuel

Symbol: F_{spec}

The specific fuel consumption is the average amount of fuel consumed by the generator per kWh of electricity it generates. HOMER calculates the specific fuel consumption using the following equation:

$$F_{spec} = \frac{F_{tot}}{E_{gen}}$$

where:

F_{tot} = total annual generator fuel consumption [L/yr, m³/yr, or kg/yr]

E_{gen} = total annual electrical production of the generator [kWh/yr]

For more information

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6.147 Standard Test Conditions



Standard Test Conditions

PV manufacturers rate the power output of their PV modules at standard test conditions (STC), meaning a radiation of 1 kW/m^2 , a cell temperature of 25°C , and no wind. Standard test conditions do not reflect typical operating conditions, since full-sun cell temperatures tend to be much higher than 25°C .

See also

[How HOMER calculates the PV cell temperature](#)

For more information

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6.148 Suggested Lifetime Throughput



Suggested Lifetime Throughput

HOMER calculates a suggested value of lifetime throughput for a battery based on the information entered in the lifetime curve. The suggested value is equal to the average value of the lifetime throughput values that fall within the allowable range of depth of discharge. (This allowable range is determined by the minimum state of charge -- if the minimum state of charge is 40%, then the battery will only experience depths of discharge between 0% and 60%.) You can accept the suggested value or modify it according to your judgement.

See also

[Battery lifetime throughput](#)

[Create New Battery window](#)

For more information

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6.149 System



System

In HOMER documentation, the word *system* refers to the combinations of technologies and components of a power generation system. The terms *system type* and *system configuration* have different meanings that are described below.

System type

A system type is a combination of technologies. For example, wind/diesel/battery describes a system type that includes wind turbines, diesel generators, and batteries.

System configuration

A system configuration is a combination of particular numbers and sizes of components. For example, a system with a generic 10 kW wind turbine, 15 kW diesel

generator, 32 batteries and a 6 kW inverter describes a configuration of the wind/diesel/battery system type. The same system type with 48 batteries is a different system configuration.

HOMER simulates system configurations. As it searches for the optimal system type, HOMER typically evaluates hundreds or thousands of system configurations. HOMER displays a list of system configurations in the [overall optimization results](#) table, and the most cost effective configuration of each system type in the [categorized optimization results](#) table.

A system configuration can also be defined by dispatch strategy. For example, a system consisting of a generic 10 kW wind turbine, 15 kW diesel, 32 batteries, and an inverter could have two configurations: one with a load following dispatch strategy, and another with a cycle charging dispatch strategy.

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6.150 System Fixed Capital Cost



System Fixed Capital Cost

Type: Input Variable

Units: \$

Symbol: $C_{cap,fixed}$

The system fixed capital cost is the capital cost that occurs at the start of the project regardless of the size or architecture of the power system.

The system fixed capital cost appears in the Cash Flow Details Table as 'other capital cost'. It adds to the total initial capital cost of the system, and therefore to the total net present cost. But since it affects the NPC of all system configurations in the search space by the same amount, it has no effect on the system rankings.

See also

[System fixed O&M cost](#)

[Cash Flow Details table](#)

[Total net present cost](#)

For more information

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6.151 System Fixed Operations and Maintenance (O&M) Cost



System Fixed O&M Cost

Type: Input Variable

Units: \$/yr

Symbol: $C_{om,fixed}$

The system fixed operation and maintenance (O&M) cost is the recurring annual cost that occurs regardless of the size or architecture of the power system.

The system fixed O&M cost appears in the Cash Flow Details Table as 'other O&M cost'. It affects the total net present cost of each system configuration equally, so it has no effect on the system rankings.

See also

[System fixed capital cost](#)[Cash Flow Details table](#)[Total net present cost](#)

For more information

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6.152 System Roundtrip Efficiency



System Roundtrip Efficiency

Type: Intermediate Variable

Units: none

Symbol: h

The system roundtrip efficiency is the overall efficiency of the system in converting AC energy to DC, putting that energy into storage in the battery bank, removing it from the battery bank, and converting it back to AC. HOMER calculates the system roundtrip efficiency using the following equation:

$$h = h_{\text{inv}} h_{\text{rt}} h_{\text{rect}}$$

where:

h_{inv} = inverter efficiency

h_{rt} = [battery roundtrip efficiency](#)

h_{rect} = rectifier efficiency

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6.153 Thermal Load Served (PRO)



Thermal Load Served

Type: Output Variable

Units: kWh/yr

Symbol: H_{served}

The thermal load served is the total amount of thermal energy that went towards serving the thermal load during the year.

For more information

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6.154 Total Annualized Cost



Total Annualized Cost

Type: Output Variable

Units: \$/year

Symbol: $C_{ann,tot}$

The total annualized cost is the annualized value of the total net present cost. HOMER calculates the total annualized cost using the following equation:

$$C_{ann,tot} = CRF(i, R_{proj}) \cdot C_{NPC,tot}$$

where:

$C_{NPC,tot}$ = the [total net present cost](#) [\$]

i = the [annual real interest rate](#) [%]

R_{proj} = the [project lifetime](#) [yr]

$CRF()$ = a function returning the [capital recovery factor](#)

HOMER uses the total annualized cost to calculate the leveled cost of energy.

See also

[Annualized cost definition](#)

[Total net present cost](#)

[Leveled cost of energy](#)

[Cash Flow Details table](#)

For more information

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6.155 Total Capacity Shortage



Total Capacity Shortage

Type: Output Variable

Units: kWh/yr

Symbol: E_{cs}

The total capacity shortage (or annual capacity shortage) is the total amount of [capacity shortage](#) that occurs throughout the year. At the end of the year, this value is used to calculate the [capacity shortage fraction](#).

Note that if each of the four operating reserve inputs (specified on the [Constraints](#) window) are set to zero, the total capacity shortage will be equal to the [total unmet load](#).

See also

[Required operating reserve](#)[Maximum annual capacity shortage](#)[Capacity shortage fraction](#)[Total unmet load](#)

For more information

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6.156 Total Electrical Load Served



Total Electrical Load Served

Type: Output Variable

Units: kWh/yr

Symbol: E_{served}

The total electrical load served is the total amount of energy that went towards serving the primary and deferrable loads during the year, plus the amount of energy sold to the grid. HOMER calculates the total electrical load served using the following equation:

$$E_{\text{served}} = E_{\text{served,ACprim}} + E_{\text{served,DCprim}} + E_{\text{served,def}} + E_{\text{grid,sales}}$$

where:

$E_{\text{served,primAC}}$ = [AC primary load served](#) [kWh/yr]

$E_{\text{served,primDC}}$ = [DC primary load served](#) [kWh/yr]

$E_{\text{served,def}}$ = [deferrable load served](#) [kWh/yr]

$E_{\text{grid,sales}}$ = energy sold to the grid [kWh/yr]

HOMER uses this value to calculate the renewable fraction and the levelized cost of energy.

See also

[Renewable fraction](#)

[Levelized cost of energy](#)

[Total thermal load served](#)

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6.157 Total Electrical Production



Total Electrical Production

Type: Output Variable**Units:** kWh/yr**Symbol:** E_{prod}

The total electrical production is the total amount of electrical energy produced by the power system in one year. It is the sum of the electrical energy produced by all components of the system.

See also

[Total thermal production](#)

[Renewable electrical production](#)

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6.158 Total Thermal Production (PRO)



Total Thermal Production P

Type: Output Variable**Units:** kWh/yr**Symbol:** H_{prod}

The total thermal production is the total amount of thermal energy produced by the power system in one year. It is the sum of the thermal energy produced by all components of the system.

See also

[Total electrical production](#)

[Renewable thermal production](#)

For more information

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6.159 Total Excess Electricity



Total Excess Electricity

Type: Output Variable**Units:** kWh/yr**Symbol:** E_{excess}

The total excess electricity is the total amount of [excess electricity](#) that occurs throughout the year.

See also

[Excess electricity fraction](#)

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6.160 Total Fuel Cost



Total Fuel Cost

Type: Output Variable

Units: \$/yr

Symbol: $C_{fuel,tot}$

The total fuel cost is the sum of the fuel costs of each generator and the boiler.

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6.161 Total Net Present Cost



Total Net Present Cost

Type: Output Variable

Units: \$

Symbol: C_{NPC}

The total net present cost (NPC) of a system is the present value of all the costs that it incurs over its lifetime, minus the present value of all the revenue that it earns over its lifetime. Costs include capital costs, replacement costs, O&M costs, fuel costs, emissions penalties, and the costs of buying power from the grid. Revenues include salvage value and grid sales revenue.

HOMER calculates the total NPC by summing up the total discounted cash flows in each year of the project lifetime. The total NPC appears in the bottom-right cell of the Cash Flow Details Table.

Tip: Look at the [Cash Flow Details Table](#) to see a precise itemization of the cash flows that contribute to the total net present cost.

The total NPC is HOMER's main economic output, the value by which it ranks all system configurations in the optimization results, and the basis from which it calculates the total annualized cost and the levelized cost of energy.

See also

[Cash Flow Details table](#)

[Net present cost definition](#)

[Total annualized cost](#)

[Levelized cost of energy](#)

[Why does HOMER rank systems by total NPC?](#)

For more information

The [HOMER Support Site](#) has a searchable knowledgebase and additional support options.

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6.162 Total Unmet Load



Total Unmet Load

Type: Output Variable

Units: kWh/yr

Symbol: E_{unmet}

The total unmet load is the total amount of [unmet load](#) that occurs throughout the year.

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6.163 Unmet Load



Unmet Load

Unmet load is electrical load that the power system is unable to serve. It occurs when the electrical demand exceeds the supply. For each [system](#), HOMER calculates the [total unmet load](#) that occurs over the year, as well as the [unmet load fraction](#). By default, HOMER considers infeasible any system that experiences unmet load, but you can change that by entering a non-zero value for the [maximum annual capacity shortage](#).

See also

[Capacity shortage](#)

[Unmet load fraction](#)

For more information

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6.164 Unmet Load Fraction



Unmet Load Fraction

Type: Output Variable
Units: none
Symbol: f_{unmet}

The unmet load fraction is the proportion of the total annual electrical load that went unserved because of insufficient generation. The equation for the unmet load fraction is given below:

$$f_{unmet} = \frac{E_{unmet}}{E_{demand}}$$

where:

E_{unmet} = [total unmet load](#) [kWh/yr]

E_{demand} = total annual electrical demand (primary plus deferrable) [kWh/yr]

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6.165 Weibull Distribution



The Weibull Distribution

The two-parameter Weibull distribution is often used to characterize wind regimes because it has been found to provide a good fit with measured wind data. The probability density function is given by the following equation:

$$f(v) = \frac{k}{c} \left(\frac{v}{c}\right)^{k-1} \cdot \exp\left[-\left(\frac{v}{c}\right)^k\right]$$

where:

v is the wind speed [m/s]

k is the Weibull shape factor [unitless]

c is the Weibull scale parameter [m/s]

The cumulative distribution function is given by the following equation:

$$F(v) = 1 - \exp\left[-\left(\frac{v}{c}\right)^k\right]$$

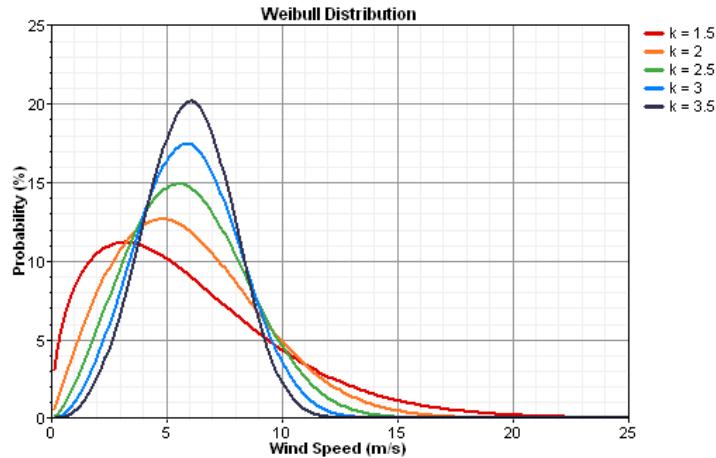
The following equation relates the two Weibull parameters and the average wind speed:

$$\bar{v} = c \Gamma\left(\frac{1}{k} + 1\right)$$

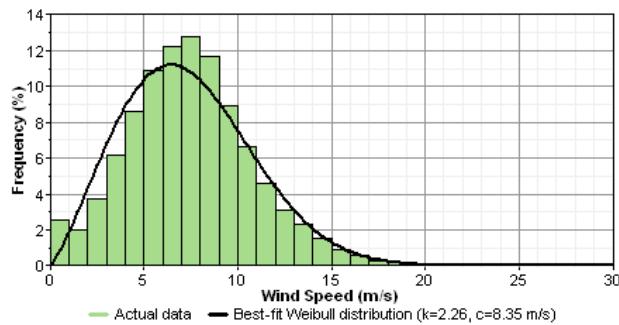
where:

G is the gamma function

One can describe a Weibull distribution by an average wind speed and a Weibull k value. The graph below shows five Weibull distributions, all with the same average wind speed of 6 m/s, but each with a different Weibull k value. As the graph shows, lower k values correspond to broader distributions.



To fit a Weibull distribution to measured wind data, HOMER uses the maximum likelihood method given by [Stevens and Smulders, 1979](#). The graph below shows a typical distribution of wind speeds and the best-fit Weibull distribution.



See also

[Weibull k value](#)

For more information

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6.166 Weibull k Value



Weibull k Value

Type: Input Variable

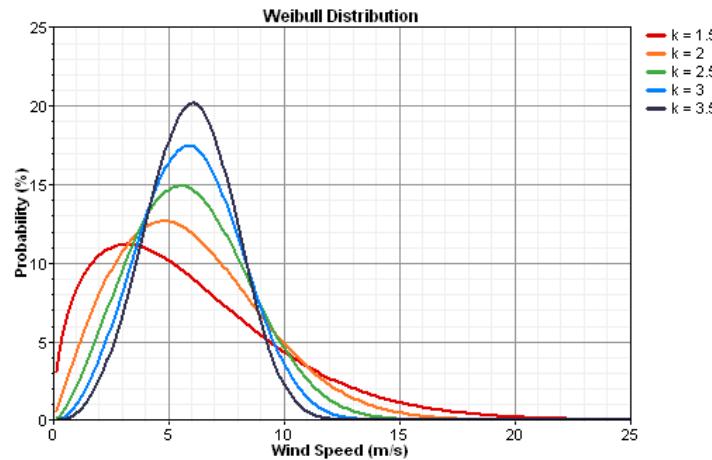
Units: none

Symbol: k

Typical Range: 1.5 - 2.5

The Weibull k value, or Weibull shape factor, is a parameter that reflects the breadth of a distribution of wind speeds. HOMER fits a Weibull distribution to the wind speed data, and the k value refers to the shape of that distribution.

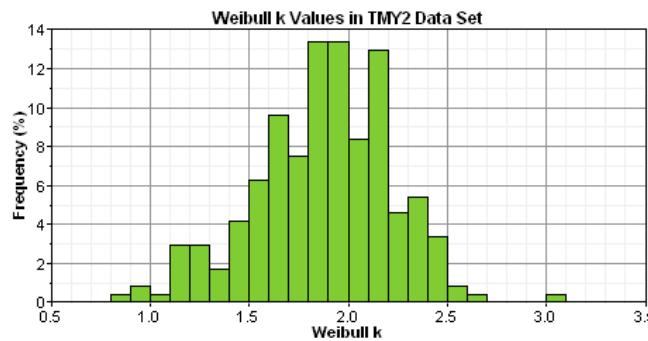
The graph below shows five Weibull distributions, all with the same average wind speed of 6 m/s, but each with a different Weibull k value. As the graph shows, lower k values correspond to broader distributions of wind speed, meaning that winds tend to vary over a large range of speeds. Higher k values correspond to narrower wind speed distributions, meaning that wind speeds tend to stay within a narrow range.



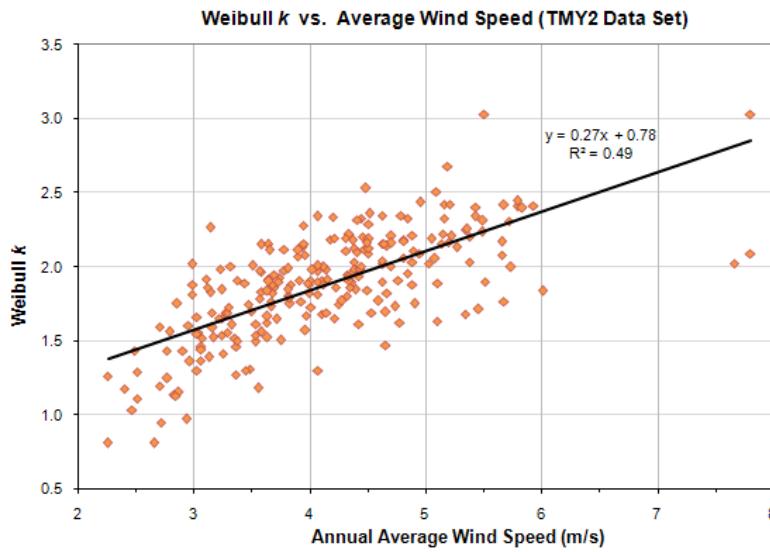
Lower k values correspond to broader wind speed distributions. So a very gusty location may have a Weibull k value as low as 1.5 or so, whereas a location characterized by very steady winds (like tropical trade wind environments) may have a k value as high as 3 or 4. When you synthesize wind speed data, HOMER uses a default Weibull k value of 2, which is typical of many wind regimes.

When fitting a Weibull distribution to measured wind data, HOMER uses the maximum likelihood method given by [Stevens and Smulders, 1979](#).

To help HOMER users estimate Weibull k values in the absence of measured data, we calculated the best-fit Weibull k value for each of the 239 weather stations in the TMY2 data set. The histogram below shows the resulting distribution of Weibull k values. The measured values themselves appear in the [table of measured wind parameters](#).



In the TMY2 data set, we observed a correlation between the Weibull k value and the average wind speed, with higher annual average wind speeds tending to correspond to lower Weibull k values. The graph below displays this correlation:



See also

[Weibull distribution](#)

[Autocorrelation factor](#)

[Diurnal pattern strength](#)

[Hour of peak wind speed](#)

[TMY2 wind parameters](#)

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6.167 Wind Turbine Hub Height



Wind Turbine Hub Height

Type: Input Variable

Units: m

Symbol: z_{hub}

The wind turbine hub height is the height above ground at which the rotor sits. Hub heights typically range between 25m (for smaller wind turbines, 50 kW or less) and 100m (for large, multi-megawatt wind turbines). Wind speeds tend to increase with height above ground, so if the hub height is not the same as the anemometer height, HOMER adjusts the wind speed data accordingly.

For details on how HOMER calculates the wind speed at the hub height of the wind turbine, see [Wind shear inputs](#).

See also:

[Wind shear inputs](#)

[Anemometer height](#)

For more information

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