

Multibody Dynamics B - Assignment 7

ME41055

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1 Statement of integrity

my homework is completely in accordance with
the Academic Integrity

Figure 1: My handwritten statement of integrity

2 Acknowledgements

I used [1] in making this assignment when finished I compared initial values with Prajish Kumar (4743873).

3 Setup overview

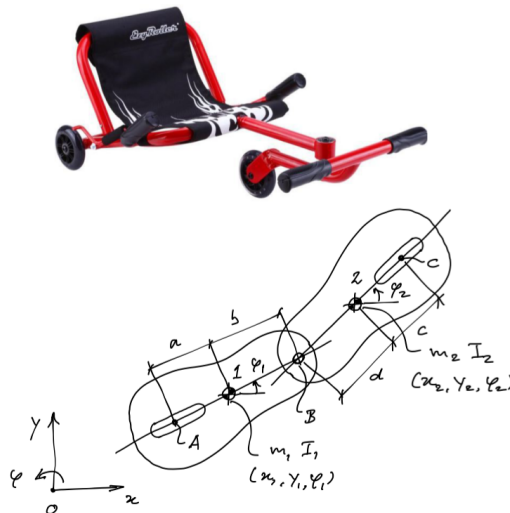


Figure 2: Quick return mechanism as depicted in assignment 7

4 Problem Statement

In this assignment we were asked to derive the motion of the EzyRoller Mechanism (see fig 2). This EzyRoller mechanism has the following parameters:

$$a = 0.5m \quad (1)$$

$$b = 0.5m \quad (2)$$

$$c = 0.125m \quad (3)$$

$$d = 0.125m \quad (4)$$

$$m1 = 1kg \quad (5)$$

$$m2 = 0kg \quad (6)$$

$$J1 = 0.1kgm^2 \quad (7)$$

$$J2 = 0kgm^2 \quad (8)$$

$$g = 9.81m/s^2 \quad (9)$$

$$(10)$$

Since the EOM were asked in the implicit form we will use the COM coordinates as the state. From this state the position of all the other points on the Ezyroller can be calculated.

$$x0 = [x_1 \ y_1 \ \phi_{i1} \ x_2 \ y_2 \ \phi_{i2}] \quad (11)$$

In the first part of the question there were no external forces or torques applied to the EzyRoller. We were asked to choose a set of initial states that comply with the given constraints. I choose the following initial states:

$$x0 = [x_1 \ y_1 \ \phi_{i1} \ x_2 \ y_2 \ \phi_{i2} \ \dot{x}_1 \ \dot{y}_1 \ \dot{\phi}_{i1} \ \dot{x}_2 \ \dot{y}_2 \ \dot{\phi}_{i2}] \quad (12)$$

$$x0 = [a \ 0 \ 0 \ a+b \ d \ \pi/2 \ 1 \ 0 \ 0 \ 0 \ 1 \ 0] \quad (13)$$

With these initial states the EOM can be derived in implicit form by putting the Newton-Euler equations (explained in CH1-CH2 [1]) and the constraint equations in one big matrix vector product. Following to get the state derivative this system of equations can then be solved by using Gaussian elimination. The full derivation will be explained below.

4.1 Equations of motion(EOM)

After applying the earlier explained procedure we get the following system of equations:

$$\begin{pmatrix} M_{ij} & C_{k,i} & S_{mi} \\ C_{k,j} & \mathbf{0} & \mathbf{0} \\ S_{mj} & \mathbf{0} & \mathbf{0} \end{pmatrix} \begin{pmatrix} \ddot{x}_j \\ \lambda_k \\ \lambda_m \end{pmatrix} = \begin{pmatrix} F_i \\ -C_{k,jl}\dot{x}_j\dot{x}_l \\ -S_{mj,l}\dot{x}_j\dot{x}_l \end{pmatrix},$$

Figure 3: Vector product of the EOM

In this $M_{i,j}$ depicts the mass matrix, $C_{k,j}$ the Jacobean of the holonomic constraints (position constraint) and $S_{k,j}$ the Jacobean of the non-holonomic constraints (velocity constraint). The right hand side of this system of equations contains the force vector F and the convective e terms. In our example the left hand size matrix A equal to:

$$A = \begin{pmatrix} m_1 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & -\sin(\varphi_1) & 0 \\ 0 & m_1 & 0 & 0 & 0 & 0 & 0 & 1 & \cos(\varphi_1) & 0 \\ 0 & 0 & J_1 & 0 & 0 & 0 & -b \sin(\varphi_1) & b \cos(\varphi_1) & -a & 0 \\ 0 & 0 & 0 & m_2 & 0 & 0 & -1 & 0 & 0 & -\sin(\varphi_2) \\ 0 & 0 & 0 & 0 & m_2 & 0 & 0 & -1 & 0 & \cos(\varphi_2) \\ 0 & 0 & 0 & 0 & 0 & J_2 & -d \sin(\varphi_2) & d \cos(\varphi_2) & 0 & -c \\ 1 & 0 & -b \sin(\varphi_1) & -1 & 0 & -d \sin(\varphi_2) & 0 & 0 & 0 & 0 \\ 0 & 1 & b \cos(\varphi_1) & 0 & -1 & d \cos(\varphi_2) & 0 & 0 & 0 & 0 \\ -\sin(\varphi_1) & \cos(\varphi_1) & -a & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -\sin(\varphi_2) & \cos(\varphi_2) & -c & 0 & 0 & 0 & 0 \end{pmatrix} \quad (14)$$

and B matrix is equal to:

$$B = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ b \cos(\varphi_1) \dot{\varphi}_1^2 + d \cos(\varphi_2) \dot{\varphi}_2^2 \\ b \sin(\varphi_1) \dot{\varphi}_1^2 + d \sin(\varphi_2) \dot{\varphi}_2^2 \\ \dot{\varphi}_1 (\dot{x}_1 \cos(\varphi_1) + \dot{y}_1 \sin(\varphi_1)) \\ \dot{\varphi}_2 (\dot{x}_2 \cos(\varphi_2) + \dot{y}_2 \sin(\varphi_2)) \end{pmatrix} \quad (15)$$

$$F = [0 \ 0 \ 0 \ 0 \ 0 \ 0] \quad (16)$$

4.1.1 holonomic constraints

The mechanism of this example had 2 holonomic constraints in point B. These are defined as follos:

$$C = \begin{pmatrix} x_1 + b \cos(\varphi_1) - x_2 + d \cos(\varphi_2) \\ y_1 + b \sin(\varphi_1) - y_2 + d \sin(\varphi_2) \end{pmatrix} \quad (17)$$

To add this constraints to the EOM we need to differentiate it two times to get them in terms of accelerations. The Jacobean and Hessian of these constraints were calculated by symbolic toolbox and is therefore not displayed.

4.1.2 non-holonomic constraints

The non-holonomic constraints for this mechanism can be found in the two wheels. These constraint ensure that there is no lateral movement of the wheels. The non-holonomic constraints in our can be derived by calculating the x and y velocity in point A and C. This is done with the relative velocity theorhem:

$$V_A = V_{COM1} + \omega \times r_{A/COM1} \quad (18)$$

After the velocity of point A and C are calculated we can use the dot product to project them onto the tangential and normal wheel components. By following setting the normal velocity component (The component pointing out of the wheel axle to 0 we get the following velocity constraints:

$$D = \begin{pmatrix} \dot{y}_1 \cos(\varphi_1) - a \dot{\varphi}_1 - \dot{x}_1 \sin(\varphi_1) \\ c \dot{\varphi}_2 + \dot{y}_2 \cos(\varphi_2) - \dot{x}_2 \sin(\varphi_2) \end{pmatrix} \quad (19)$$

To add these constraints to the EOM we only need to calculate the first derivative. The jacobian of the velocity constraint was calculated by symbolic toolbox and is therefore not displayed. They can however be found in the A matrix (equation 14).

4.2 Numerical integration method

To get the movement of EzyRoller in time we will use a 4th order Runge-Kuta integration method combined with a Gauß-Newton correction for position and speed. This correction is done to compensate for integration drift. In this correction we use the position constraints and the velocity constraints.

4.2.1 Runge-Kutta 4th order method (RK4)

The Runge-Kutta 4th order method has the following iteration scheme:

$$k_1 = f(t_n, y_n) \quad (20)$$

$$k_2 = f\left(t_n + \frac{h}{2}, y_n + \frac{h}{2}k_1\right) \quad (21)$$

$$k_3 = f\left(t_n + \frac{h}{2}, y_n + \frac{h}{2}k_2\right) \quad (22)$$

$$k_4 = f(t_n + h, y_n + hk_3) \quad (23)$$

$$y_{n+1} = y_n + \frac{h}{6}(k_1 + 2k_2 + 2k_3 + k_4) \quad (24)$$

Gauß-Newton corrections

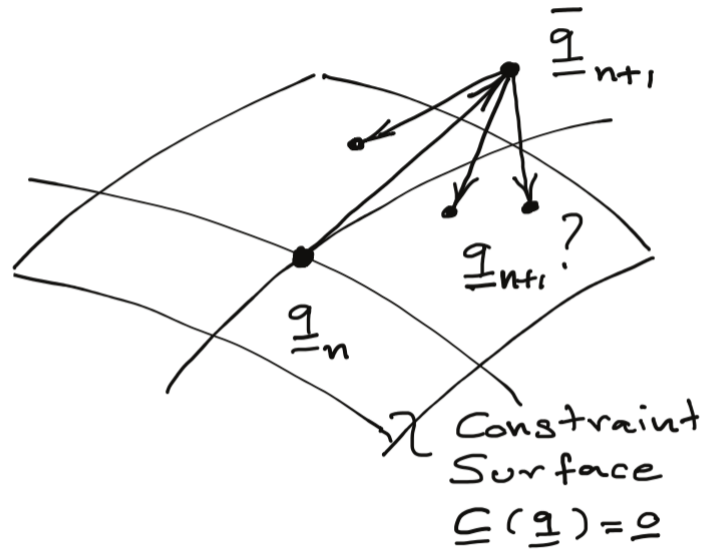


Figure 4: A depiction of the constraint surface and Gauß-Newton method as displayed in [1]. This picture was not modified in any sense

The Gauß-Newton we are using here is a non-linear least-square constraint optimization method. In our problem we have the following optimization problem:

$$\|\bar{q}_{n+1} - q_{n+1}\|_2 = \min_{q_{n+1}}, \quad \forall \quad \{q_{n+1} | C(q_{n+1}) = 0\} \quad (25)$$

In words what you are doing with the Gauss-Newton method is you look at the solution and see how much it deviates from the constraint surface. You then look for the point on the constraint surface that is closest to our original point. This point searching is what is done by the optimization (see 4). Above named non-linear constraint optimization problem is easily solved by an iterative method. The idea of this method is that you look at a small change around the current state q :

$$q_{n+1} = \bar{q}_{n+1} + \Delta q_{n+1} \quad (26)$$

When you fill this in in the original

$$\Delta q_{n+1} = 0, \quad \forall \quad \{\Delta q_{n+1} | C(\bar{q}_{n+1})\Delta q_{n+1} = 0\} \quad (27)$$

This leads to the following system of equations:

$$\begin{pmatrix} I & C^T \\ C & 0 \end{pmatrix} \begin{pmatrix} \Delta \\ \mu \end{pmatrix} = \begin{pmatrix} 0 \\ e \end{pmatrix} \quad (28)$$

In which:

$$-CC^T\mu = e \quad (29)$$

$$\mu = -(CC^T)^{-1}e \quad (30)$$

$$\Delta = C^T(CC^T)^{-1}e \quad (31)$$

In the end you obtain:

$$\Delta = C^+e \quad (32)$$

With this you can calculate a new q that is closer to the constraint surface as:

$$q_{new} = q_{old} + \Delta \quad (33)$$

Following you can recalculate the C and \dot{C} and start the process over again. In our example we repeat this process till or 10 function iterations are done or the constraints

are smaller than 10^{-12} . This procedure is applied to both the position and velocity of the quick return mechanism.

Position scheme explanation

For the position constraints since they are non-linear we will need to use the loop described above this was implemented in matlab as follows:

```

464 % Solve non-linear constraint least-square problem
465 while (max(abs(C)) > parms.tol) && (n_iter < parms.nmax)
466     x_tmp = x(1:6);
467     n_iter = n_iter + 1;
468     x_del = Cd*inv(Cd'*Cd)*-C.';
469     x(1:6) = x_tmp + x_del.';
470
471 % Recalculate constraint
472 [C,Cd,~,~] = constraint_calc(x,parms);
473 end

```

Figure 5: Matlab code doing the position correction

velocity

Since the velocity constraints are linear to compensate for the velocity drift we can do this more easily. The MATLAB code implementing this is shown below:

```

183 % Calculate the corresponding speeds
184 q_tmp_vel = q(4:6);
185 Dqd_n1 = -Cd*inv(Cd'*Cd)*Cd.'*q_tmp_vel.';
186 q(4:6) = q_tmp_vel + Dqd_n1.';
187

```

Figure 6: Matlab code doing the velocity correction

In these MATLAB scripts C depicts the position constraints, Cd the Jacobean of these constraints, D the velocity constraints and Dd the Jacobean of these velocity constraints. Sd is simply the matrix of both the holonomic and non-holonomic velocity constraints together.

5 Results

5.1 Non powered mechanism

First we were asked to implement a non-powered version of the Ezyroller. The full MATLAB code implementing the model can be found in appendix A. After this model was created I tested the model with three initial conditions.

$$x0 = \begin{bmatrix} a & 0 & 0 & a+b & d & \pi/2 & 1 & 0 & 0 & 0 & 1 & 0 \end{bmatrix} \quad (34)$$

$$x0 = \begin{bmatrix} a & 0 & 0 & a+b & d & 0 & 1 & 0 & 0 & 1 & 0 & 0 \end{bmatrix} \quad (35)$$

$$x0 = \begin{bmatrix} a & 0 & \pi/2 & a+b & d & \pi/2 & 0 & 1 & 0 & 0 & 1 & 0 \end{bmatrix} \quad (36)$$

While doing this I used intuition to see if the motion of the EzyRoller was the one expected. I did this by looking at the animation and the plot of the path. The path of the most interesting condition (equation 34) is shown in figure 7. From the figure we see that as we put a input x-velocity on the COM of the first body while the second body is under a angle of $\pi/2$ the first body will push the second body upwards. Further since the second body applies a reaction force on the first body the whole mechanism will go upwards. The other initial conditions also displayed expected behavior (the mechanism moves in a horizontal or vertical straight line). From the animation we can also see that our drift correction works correctly since the Mechanism doesn't fall apart.

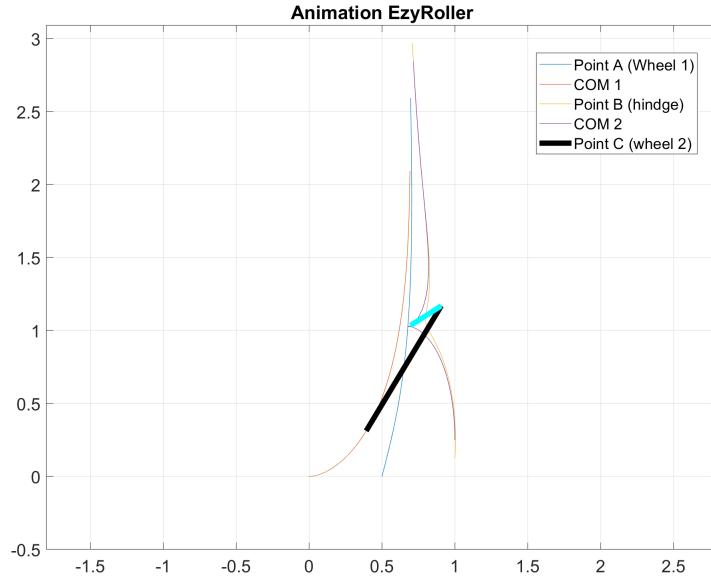


Figure 7: Path of the points on the EzyRoller

5.2 Powered mechanism

To get the powered mechanism we add the following torques to the force matrix F :

$$F = \begin{bmatrix} 0 & 0 & T1 & 0 & 0 & T2 \end{bmatrix} \quad (37)$$

In this $T1 = -M1 * \cos(\pi * t)$ and $T2 = M1 * \cos(\pi * t)$. The new B matrix now becomes:

$$B = \begin{pmatrix} 0 \\ 0 \\ -\frac{\cos(\pi t)}{10} \\ 0 \\ 0 \\ \frac{\cos(\pi t)}{10} \\ b \cos(\varphi_1) \dot{\phi}_1^2 + d \cos(\varphi_2) \dot{\phi}_2^2 \\ b \sin(\varphi_1) \dot{\phi}_1^2 + d \sin(\varphi_2) \dot{\phi}_2^2 \\ \dot{\phi}_1 (\dot{x}_1 \cos(\varphi_1) + \dot{y}_1 \sin(\varphi_1)) \\ \dot{\phi}_2 (\dot{x}_2 \cos(\varphi_2) + \dot{y}_2 \sin(\varphi_2)) \end{pmatrix} \quad (38)$$

Further we are instructed to use the following initial state.

$$x0 = [a \quad 0 \quad 0 \quad a+b \quad d \quad \pi \quad 0 \quad 0 \quad 0 \quad 0 \quad 0 \quad 0] \quad (39)$$

5.2.1 Path of the mechanism

In figure 8 the path of the mechanism is plotted. From this figure we can see that with input torques The EzyRoller follows a path that goes slightly upwards. As we have put segment 1 of the roller aligned with the horizontal and the second segment aligned with the vertical this path is to be expected. We can further notice that this path looks linear, however when we Zoom in (see figure 9)we see that it actually is comprised of small oscillations around this linear path.

5.2.2 Linear and angular velocities

In figure 11 the linear velocities of the COM's of the two segments are shown. From the figure we can see that the mechanism displays oscillatory behavior and that both the x and y velocities of the COM's are oscillating around the a given velocity magnitude ??.

In figure 12 the angular velocities are shown. We can see from the figure that both segments display oscillatory behavior and that the amplitude segment 2 is bigger than segment 1. This is probably due to the difference in segment parameters.

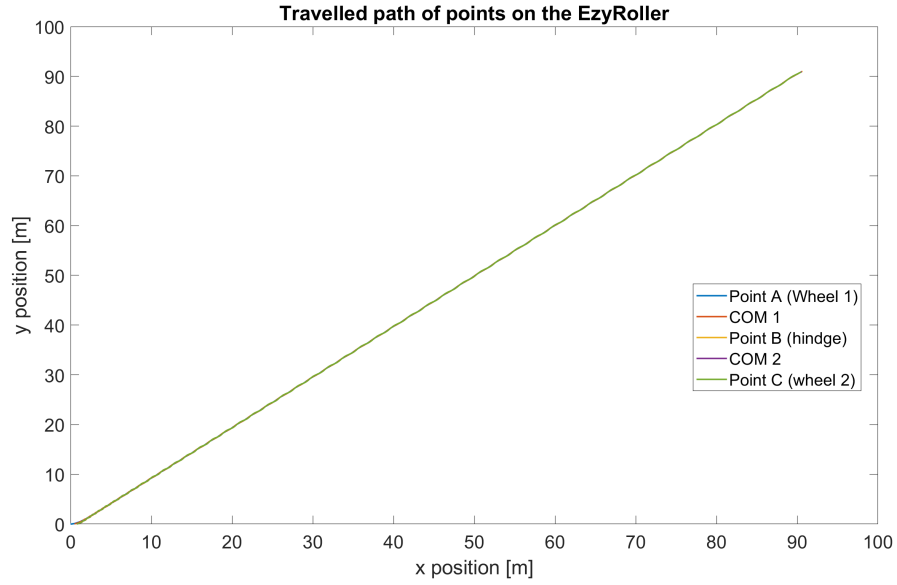


Figure 8: Path of the points on the EzzRoller

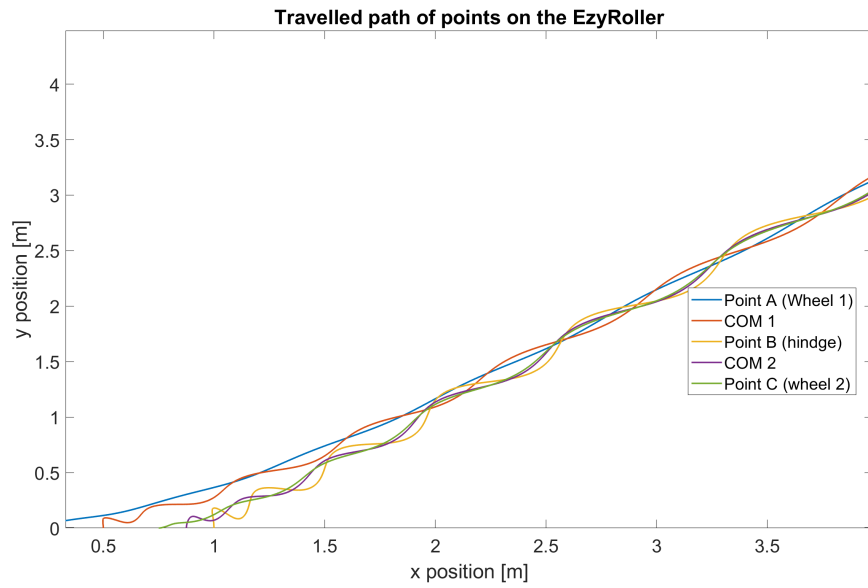


Figure 9: Path of the points on the EzzRoller Zoomed in

5.2.3 kinetic energy and Torque work

In figure 13 the kinetic energy and the work created by the torque are shown.

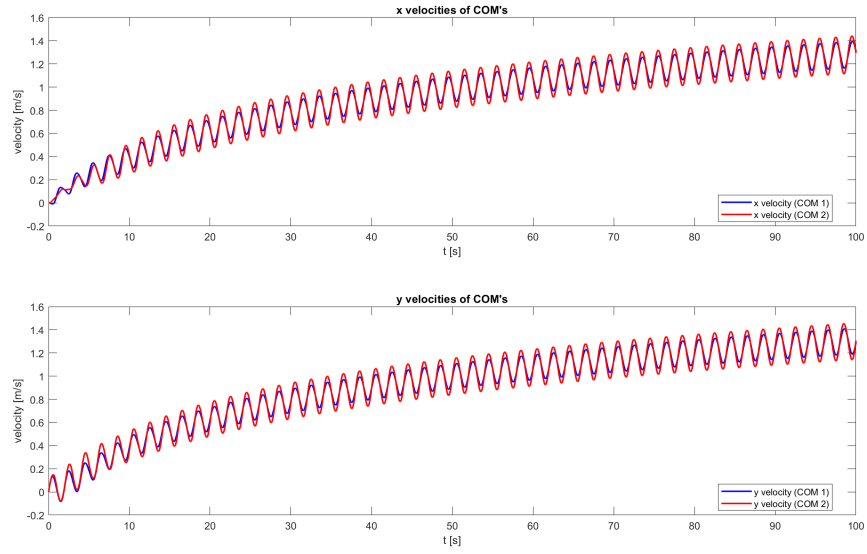


Figure 10: Linear velocities of EzzRoller

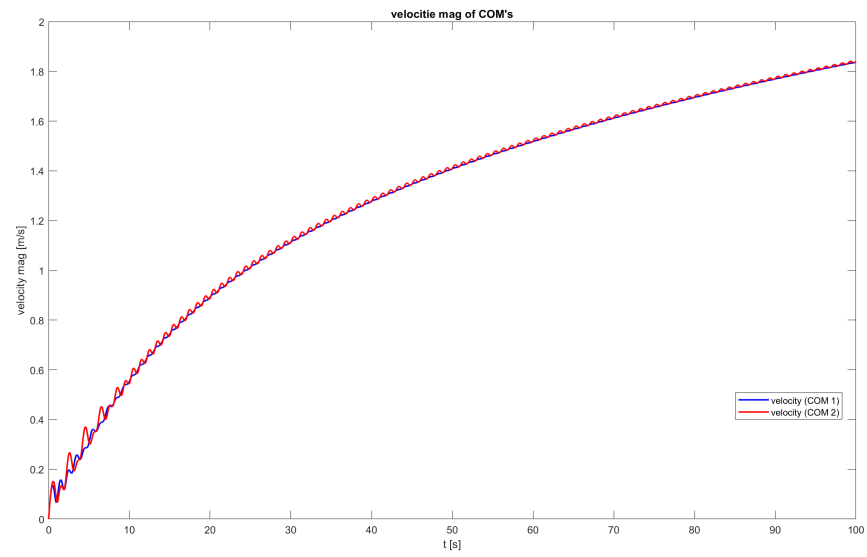


Figure 11: Magnitudes of Linear velocities of EzzRoller

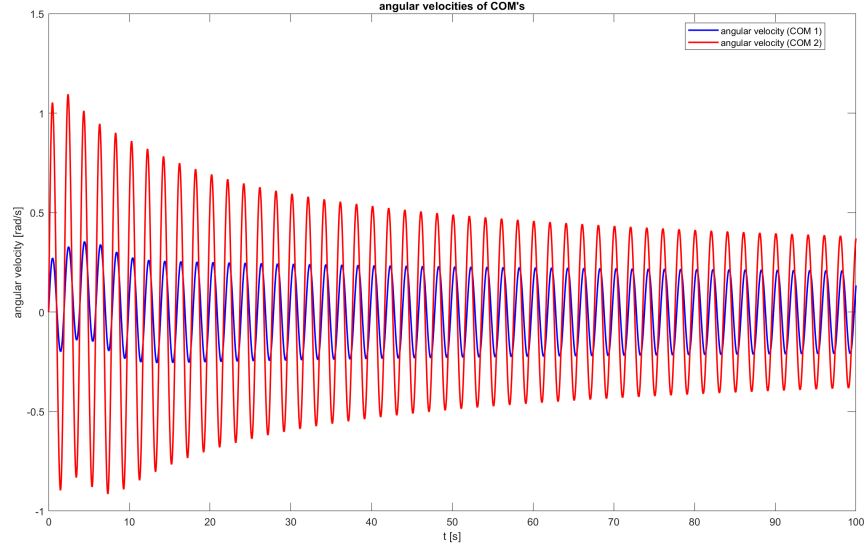


Figure 12: Angular velocities of EzzRoller

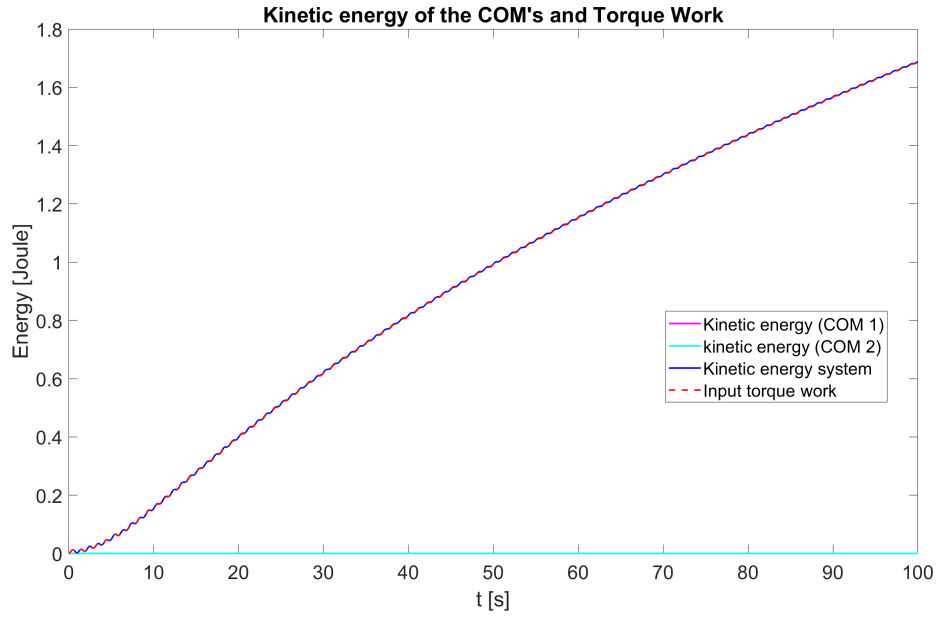


Figure 13: Kinetic energy of the system plotted together with the work supplied by the external torque.

6 Discussion

From the results above we see that the work done by the torque is equal to the kinetic energy. This is to be expected since due to the absence of other external forces there

is no potential or dissipate component. All the work done on the segment is therefore transformed into kinetic energy of the system. Further it might seem strange that body 2 has no kinetic energy but this is caused by the fact that the mass and inertia of body 2 were said to be zero.

Appendix A: Accompanying MAT LAB scripts

```
1 %% MBD_B: Assignment 8 - EzyRoller
2 % Rick Staa (4511328)
3 % Last edit: 29/05/2018
4
5 %% - - Pre processing operations --
6 clear all; close all; clc;
7 fprintf('--- A8 ---\n');
8 animate_bool = 0; % Set on 1 if you
   want to see an animation
9
10 %% Script settings
11 parms.accuracy_bool = 0; % If set to 1 A\b
   will be performed instead of inv(A)*B this is more
   accurate but slower
12 parms.question_bool = 1; % Set on 0 for
   the first part of the question and 1 for the second part
13
14 %% Model parameters
15 % Set up needed symbolic parameters
16 syms x1 y1 phi1 x2 y2 phi2 x1d y1d phi1d x2d y2d phi2d t
17
18 % State
19 parms.syms.x1 = x1;
20 parms.syms.y1 = y1;
21 parms.syms.phi1 = phi1;
22 parms.syms.x2 = x2;
23 parms.syms.y2 = y2;
24 parms.syms.phi2 = phi2;
25 parms.syms.t = t;
26
27 % State derivative
28 parms.syms.x1d = x1d;
29 parms.syms.y1d = y1d;
30 parms.syms.phi1d = phi1d;
31 parms.syms.x2d = x2d;
32 parms.syms.y2d = y2d;
33 parms.syms.phi2d = phi2d;
34
35 %% -- Set model/simulation parameters and initial states --
36 %% Intergration parameters
```

```

37 | sim_time          = 100;
                                     % Intergration time
38 | parms.h          = 1e-3;
                                     % Intergration step
    | size
39 | parms.tol        = 1e-12;
                                     % Intergration
    | constraint error tolerance
40 | parms.nmax       = 10;
                                     % Maximum number of
    | Gauss-Newton drift correction iterations
41 |
42 | %% Model Parameters
43 | % Lengths and distances
44 | parms.a          = 0.5;
                                     % Length wheel first
    | segment to COM segment 1
45 | parms.b          = 0.5;
                                     % Length COM to
    | revolute joint B
46 | parms.c          = 0.125;
                                     % Length revolute jonit
    | B to COM segment 2
47 | parms.d          = 0.125;
                                     % Length COM segment 2
    | to wheel 2
48 |
49 | % Masses and inertias
50 | parms.m1         = 1;
                                     % Body 1 weight [kg]
51 | parms.m2         = 0;
                                     % Body 2 weight [kg]
52 | parms.J1         = 0.1;
                                     % Moment of inertia
    | body 1 [kgm^2]
53 | parms.J2         = 0;
                                     % Moment of inertia
    | body 2 [kgm^2]
54 |
55 | % Create mass matrix (Segment 1 and 2)
56 | parms.M          = diag([parms.m1,parms.m1,parms.
    | J1,parms.m2,parms.m2,parms.J2]);
57 |

```

```

58 % Torque and force variables (See assignment)
59 parms.M0 = 0.1;
60 parms.omega = pi;
61
62 %% World parameters
63 % Gravity
64 parms.g = 9.81; % [parms.m/s^2]
65
66 if parms.question_bool == 0
67     %% states for Question 1
68     x1_0 = parms.a;
69     y1_0 = 0;
70     phi1_0 = 0;
71     x2_0 = parms.a+parms.b;
72     y2_0 = parms.d;
73     phi2_0 = pi/2;
74
75     % Phi1d
76     x1d_0 = 1;
77     y1d_0 = 0;
78     phi1d_0 = 0;
79     x2d_0 = 0;
80     y2d_0 = 1;
81     phi2d_0 = 0;
82
83     % Set forces
84     F = [0 0 0 0 0 0].'; % No torque applied
85     parms.F = F;
86     x0 = [x1_0 y1_0 phi1_0 x2_0 y2_0
87           phi2_0 x1d_0 y1d_0 phi1d_0 x2d_0 y2d_0 phi2d_0];
88 else
89     %% States Question 2
90     % In this the generalised coordinates x1_init and y1_init
91     % are assumed to be defined so that wheel 1 is in the origin.
92     phi1_0 = 0; % Angle of first
93     % body with horizontal
94     phi2_0 = pi; % Angle of second
95     % body with horizontal

```



```

93
94 % Calculate other dependent initial positions and angles
95 x1_0 = parms.a*cos(phi1_0);
96 y1_0 = parms.b*sin(phi1_0);
97 x2_0 = (parms.a+parms.b)*cos(
    phi1_0)+parms.d*cos(phi2_0);
98 y2_0 = (parms.a+parms.b)*sin(
    phi1_0)+parms.d*sin(phi2_0);
99
100 % Velocity initital states (Make sure that the are
    admissable)
101 % Phi1d
102 x1d_0 = 0;
103 y1d_0 = 0;
104 phi1d_0 = 0;
105 x2d_0 = 0;
106 y2d_0 = 0;
107 phi2d_0 = 0;
108
109 % Create full state for optimization
110 x0 = [x1_0 y1_0 phi1_0 x2_0 y2_0
    phi2_0 x1d_0 y1d_0 phi1d_0 x2d_0 y2d_0 phi2d_0];
111
112 % Set Forces and torques
113 % F=[F1_x,F1_y,M1,F2_x,F2_y,M2];
114 F = [0 0 -parms.M0*cos(parms.
    omega*t) 0 0 parms.M0*cos(parms.omega*t)].';
    % Torque applied
115
116 % Store F in function
117 parms.F = F;
118 end
119
120 %% -- Derive equation of motion --
121 %% Calculate EOM by means of Newton-Euler equations
122 EOM_calc(parms);
    %
    Calculate symbolic equations of motion and put in parms
    struct
123
124 %% -- Perform simulation --
125 %% Calculate movement by mean sof a Runge-Kuta 4th order
    intergration method

```

```

126 tic
127 [t,x] = RK4_custom(x0,sim_time,parms);
128 toc
129
130 %% -- Post Processing --
131 %% Calculate com velocities
132 % xd = diff(x)/parms.h;
133 xdd = state_deriv(x,parms);
134
135 %% Calculate position of point A B and C
136 [A,B,C] = point_calc(x,parms);
137
138 %% Calculate kinetic energy and torque wo[ekin] = ekin_calc(x
,parms);
139 [ekin] = ekin_calc(x,parms);
140 [tw] = tw_calc(x,parms);
141
142 %% -- ANIMATE --
143 if animate_bool == 1
144     % Adapted from A. Schwab's animation code
145
146     % Rename data
147     X1 = x(:,1); Y1 = x(:,2); P1 = x(:,3);
148     DX1 = x(:,7); DY1 = x(:,8); DP1 = x(:,9);
149     X2 = x(:,4); Y2 = x(:,5); P2 = x(:,6);
150     DX2 = x(:,10); DY2 = x(:,11); DP2 = x(:,12);
151
152     % Rename Points
153     XA = A(:,1); YA = A(:,2);
154     XB = B(:,1); YB = B(:,2);
155     XC = C(:,1); YC = C(:,2);
156
157     % Create figure
158     figure
159     plot(X1,Y1)
160     hold on
161     plot(XA,YA)
162     hold on
163     plot(X2,Y2)
164     hold on
165     plot(XC,YC)
166     grid on
167     set(gca,'fontsize',16)

```

```

168     title('Animation EzyRoller')
169     axis([min(X1)-parms.a max(X1)+parms.a min(Y1)-parms.a max
        (Y1)+parms.a]);
170     axis equal
171     l = plot([X1(1) XA(1)],[Y1(1) YA(1)]);
172     k = plot([X2(1) XC(1)],[Y2(1) YC(1)]);
173     j = plot([X1(1) XB(1)],[Y1(1) YB(1)]);
174     m = plot([XB(1) X2(1)],[YB(1) Y2(1)]);
175     set(l,'LineWidth',5);
176     set(l,'Color','K')
177     set(k,'LineWidth',5);
178     set(k,'Color','C')
179     set(j,'LineWidth',5);
180     set(j,'Color','K')
181     set(m,'LineWidth',5);
182     set(m,'Color','C')
183     nstep = length(t);
184     nskip = 10;
185     for istep = 2:nskip:nstep
186         set(l,'XData',[X1(istep) XA(istep)])
187         set(l,'YData',[Y1(istep) YA(istep)])
188         set(k,'XData',[X2(istep) XC(istep)])
189         set(k,'YData',[Y2(istep) YC(istep)])
190         set(j,'XData',[X1(istep) XB(istep)])
191         set(j,'YData',[Y1(istep) YB(istep)])
192         set(m,'XData',[XB(istep) X2(istep)])
193         set(m,'YData',[YB(istep) Y2(istep)])
194         drawnow
195         pause(1e-10)
196     end
197
198 end
199
200 %% - - Create plots - -
201 %% Plot path of points on the robot
202 figure;
203 plot(A(:,1),A(:,2),x(:,1),x(:,2),B(:,1),B(:,2),x(:,4),x(:,5),
        C(:,1),C(:,2),'linewidth',1.5);
204 set(gca,'fontsize',18);
205 title('Travelled path of points on the EzyRoller');
206 xlabel('x position [m]');
207 ylabel('y position [m]');

```

```

208 legend('Point A (Wheel 1)', 'COM 1', 'Point B (hidge)', 'COM 2'
        , 'Point C (wheel 2)', 'Location', 'Best');
209
210 %% Plot linear velocities COM's
211 figure;
212 subplot(2,1,1);
213 plot(t,x(:,7), 'b', t,x(:,10), 'r', 'Linewidth', 1.5);
214 title("x velocities of COM's");
215 xlabel('t [s]');
216 ylabel('velocity [m/s]');
217 legend('x velocity (COM 1)', 'x velocity (COM 2)', 'Location',
        'Best');
218 subplot(2,1,2);
219 plot(t,x(:,8), 'b', t,x(:,11), 'r', 'Linewidth', 1.5);
220 title("y velocities of COM's");
221 xlabel('t [s]');
222 ylabel('velocity [m/s]');
223 legend('y velocity (COM 1)', 'y velocity (COM 2)', 'Location',
        'Best');
224
225 %% Plot linear magnitude velocities COM's
226 % Calculate velocity magnitudes
227 v_com1 = sqrt(x(:,7).^2+x(:,8).^2);
228 v_com2 = sqrt(x(:,10).^2+x(:,11).^2);
229
230 % Plot figure
231 figure;
232 plot(t,v_com1, 'b', t,v_com2, 'r', 'Linewidth', 1.5);
233 title("velocity mag of COM's");
234 xlabel('t [s]');
235 ylabel('velocity mag [m/s]');
236 legend('velocity (COM 1)', 'velocity (COM 2)', 'Location', '
        Best');
237
238 %% Plot angular velocities
239 figure;
240 plot(t,x(:,9), 'b', t,x(:,12), 'r', 'Linewidth', 1.5);
241 title("angular velocities of COM's");
242 xlabel('t [s]');
243 ylabel('angular velocity [rad/s]');
244 legend('angular velocity (COM 1)', 'angular velocity (COM 2)',
        'Location', 'Best');
245

```

```

246 %% Plot linear and angular accelerations COM's
247 figure;
248 subplot(2,1,1);
249 plot(t,xdd(:,7),'b',t,xdd(:,10),'r','Linewidth',1.5);
250 title("x accelerations of COM's");
251 xlabel('t [s]');
252 ylabel('acceleration [m/s^2]');
253 legend('x acceleration (COM 1)','x celleration (COM 2)', '
      Location', 'Best');
254 subplot(2,1,2);
255 plot(t,xdd(:,8),'b',t,xdd(:,11),'r','Linewidth',1.5);
256 title("y accelerations of COM's");
257 xlabel('t [s]');
258 ylabel('Accelleration [m/s^2]');
259 legend('y acceleration (COM 1)','y acceleration (COM 2)', '
      Location', 'Best');
260
261 %% Plot angular accelerations-
262 figure;
263 plot(t,xdd(:,9),'b',t,xdd(:,12),'r','Linewidth',1.5);
264 title("Angular velocities of COM's");
265 xlabel('t [s]');
266 ylabel('Angular acceleration [rad/s^2]');
267 legend('Angular acceleration (COM 1)','Angular acceleration (
      COM 2)', 'Location', 'Best');
268
269 %% Plot reaction forces
270 figure;
271 plot(t,x(:,13:end),'Linewidth',1.5);
272 title("Reaction forces in the constraints");
273 xlabel('t [s]');
274 ylabel('Reaction Force [N]');
275 legend('X reaction force in joint B (FB_x)','Y reaction force
      in joint B (FB_y)','Wheel A friction force (no slip)', '
      Wheel C friction force (no slip)', 'Location', 'Best');
276
277 %% Plot kinetic energy
278 figure;
279 plot(t,ekin(:,1),'-b',t,ekin(:,2),'-r',t,ekin(:,3),'-g', '
      Linewidth',1.5)
280 set(gca,'fontsize',18);
281 title("Kinetic energy of the COM's");
282 xlabel('t [s]');

```

```

283 ylabel('Kinetic energy[Joule]');
284 legend('Kinetic energy (COM 1)','kinetic energy (COM 2)','
        Kinetic energy system','Location', 'Best');
285
286 %% Plot Kinetic energy plus torque energy
287 figure;
288 plot(t,ekin(:,1),'-m',t,ekin(:,2),'-c',t,ekin(:,3),'-b',t,tw,
        '--r','Linewidth',1.5)
289 set(gca,'fontsize',18);
290 title("Kinetic energy of the COM's and Torque Work");
291 xlabel('t [s]');
292 ylabel('Energy [Joule]');
293 legend('Kinetic energy (COM 1)','kinetic energy (COM 2)','
        Kinetic energy system','Input torque work','Location', '
        Best');
294
295 %% FUNCTIONS
296
297 %% Post processing functions
298 % These functions are used to calculate quantities that are
        not calculated
299 % during the simulation. This regards quantities which are
        not state
300 % variables
301
302 % Calculate second derivative
303 function [xdd] = state_deriv(x,parms)
304
305 % preallocate memory for xdd vector
306 xdd = zeros(size(x,1),12);
307
308 % Create time vector
309 time = 0:parms.h:((parms.h*size(x,1))-parms.h);
310
311 % Loop through states
312 for ii = 1:size(x,1)
313     % Set time
314     t = time(ii);
315
316     % Calculate xdd
317     x_now_tmp = x(ii,1:end-4);
318     x_now_input = num2cell([x(ii,[3 6 7:12]),t],1);
319     xdd_tmp = subs_xdd(x_now_input{:}).';

```

```

320     xdd(ii,:)      = [x_now_tmp(7:12),xdd_tmp(1:6)];
321 end
322 end
323
324 % Calculation points on EzyRoller
325 function [A,B,C] = point_calc(x,parms)
326
327 %% Calculate Point A, B, C out of the state
328 A_x      = x(:,1)-parms.a*cos(x(:,3));
329 A_y      = x(:,2)-parms.a*sin(x(:,3));
330 B_x      = x(:,1)+parms.b*cos(x(:,3));
331 B_y      = x(:,2)+parms.b*sin(x(:,3));
332 C_x      = x(:,4)+parms.c*cos(x(:,6));
333 C_y      = x(:,5)+parms.c*sin(x(:,6));
334
335 % Put them in their corresponding vector
336 A        = [A_x A_y];
337 B        = [B_x B_y];
338 C        = [C_x C_y];
339
340 end
341
342 % Calculate kinetic energy of COM's
343 function [ekin] = ekin_calc(x,parms)
344
345 % preallocate memory for ekin vector
346 ekin      = zeros(size(x,1),1);
347
348 % Loop through states
349 % State is x = [x1 y1 phi1 x2 y2 phi2 x1p y1p phi1p x2p y2p
    phi2p
350 for ii = 1:size(x,1)
351     ekin(ii,1) = 0.5*x(ii,7:9)*parms.M(1:3,1:3)*x(ii,7:9).';
352     ekin(ii,2) = 0.5*x(ii,10:12)*parms.M(4:6,4:6)*x(ii,10:12)
        .';
353     ekin(ii,3) = 0.5*x(ii,7:12)*parms.M*x(ii,7:12).';
354 end
355 end
356
357 % Calculate kinetic energy of COM's
358 function [tw] = tw_calc(x,parms)
359
360 % Calculate the applied torque for the whole movement

```

```

361 % preallocate memory for xdd vector
362 tw = zeros(size(x,1),1);
363
364 % Create time vector
365 time = 0:params.h:((params.h*size(x,1))-params.h);
366
367 % Create W vector
368 if params.question_bool == 0
369     for ii = (2:size(x,1))
370         tw(ii) = tw(ii-1) + sum(subs_F.'.*(x(ii,1:6)-x((
371             ii-1),1:6)));
372     end
373 else
374     for ii = (2:size(x,1))
375         tw(ii) = tw(ii-1) + sum((subs_F(time(ii))).'*(x(
376             ii,1:6)-x((ii-1),1:6)));
377     end
378 end
379
380 %% Runge-Kuta numerical intergration function
381 % This function calculates the motion of the system by means
382 % of a
383 % Runge-Kuta numerical intergration. This function takes as
384 % inputs the
385 % parameters of the system (params), the EOM of the system (
386 % params.EOM)
387 % and the initial state.
388 function [time,x] = RK4_custom(x0,sim_time,params)
389
390 % Initialise variables
391 time = (0:params.h:sim_time).';
392 % Create time array
393 x = zeros(length(time),16);
394 % Create empty state array
395 x(1,1:length(x0)) = x0;
396 % Put
397 % initial state in array
398
399 % Caculate the motion for the full simulation time by means
400 % of a
401 % Runge-Kutta4 method

```



```

394
395 % Perform intergration till end of set time
396 for ii = 1:(size(time,1)-1)
397
398     % Add time constant
399     t = time(ii);
400
401     % Perform RK 4
402     x_now_tmp          = x(ii,1:end-4);
403
404     % Create cell for subs function function
405     x_input             = num2cell([x(ii,[3 6 7:12])),t],1);
406                                     % Add
407     time to state
408     K1                  = [x_now_tmp(1,end-5:end),subs_xdd(
409         x_input{:}).'];
410                                     %
411     Calculate the second derivative at the start of the
412     step
413     x1_tmp              = x_now_tmp + (parms.h*0.5)*K1(1:end
414         -4);
415                                     %
416     Create cell for subs function function
417     x1_input            = num2cell([x1_tmp([3 6 7:12])),t],1);
418                                     % Add
419     time to state
420     K2                  = [x1_tmp(1,end-5:end),subs_xdd(
421         x1_input{:}).'];
422                                     %
423     Calculate the second derivative halfway the step
424     x2_tmp              = x_now_tmp + (parms.h*0.5)*K2(1:end
425         -4);
426                                     %
427     Refine value calculation with new found derivative
428     x2_input            = num2cell([x2_tmp([3 6 7:12])),t],1);
429                                     % Add
430     time to state
431     K3                  = [x2_tmp(1,end-5:end),subs_xdd(
432         x2_input{:}).'];
433                                     %
434     Calculate new derivative at the new refined location
435     x3_tmp              = x_now_tmp + (parms.h)*K3(1:end-4);
436                                     %
437     Calculate state at end step with refined derivative
438     x3_input            = num2cell([x3_tmp([3 6 7:12])),t],1);
439                                     % Add
440     time to state

```

```

413     K4 = [x3_tmp(1,end-5:end),subs_xdd(
        x3_input{:}).'];
        %
        Calculate last second derivative
414     x(ii,end-3:end) = (1/6)*(K1(end-3:end)+2*K2(end-3:end)
        )+2*K3(end-3:end)+K4(end-3:end));
        % Take
        weighted sum of K1, K2, K3
415     x(ii+1,1:end-4) = x_now_tmp + (parms.h/6)*(K1(1:end
        -4)+2*K2(1:end-4)+2*K3(1:end-4)+K4(1:end-4));
        %
        Perform euler intergration step

416
417     % Calculate last acceleration
418     if ii == (size(time,1)-1)
419         x_now_tmp = x(ii+1,1:end-4);

        % Create cell for subs function function
420         x_input = num2cell([x(ii+1,[3 6 7:12])),t
            ],1);

            % Add
            time to state

421         K1 = [x_now_tmp(1,end-5:end),
            subs_xdd(x_input{:}).'];

            % Calculate the
            second derivative at the start of the step
422         x1_tmp = x_now_tmp + (parms.h*0.5)*K1(1:
            end-4);
            % Create cell for subs function function
423         x1_input = num2cell([x1_tmp([3 6 7:12])),t
            ],1);

            % Add
            time to state

424         K2 = [x1_tmp(1,end-5:end),subs_xdd(
            x1_input{:}).'];

            % Calculate the
            second derivative halfway the step
425         x2_tmp = x_now_tmp + (parms.h*0.5)*K2(1:
            end-4);
            % Refine value calculation with new found
            derivative
426         x2_input = num2cell([x2_tmp([3 6 7:12])),t
            ],1);

            % Add
            time to state

```

```

427         K3 = [x2_tmp(1,end-5:end),subs_xdd(
            x2_input{:}).'];
            % Calculate new
            derivative at the new refined location
428         x3_tmp = x_now_tmp + (parms.h)*K3(1:end
            -4);
            %
            Calculate state at end step with refined derivative
429         x3_input = num2cell([x3_tmp([3 6 7:12]),t
            ],1);
            % Add
            time to state
430         K4 = [x3_tmp(1,end-5:end),subs_xdd(
            x3_input{:}).'];
            % Calculate last
            second derivative
431         x(ii+1,end-3:end) = (1/6)*(K1(end-3:end)+2*K2(end
            -3:end)+2*K3(end-3:end)+K4(end-3:end));
            % Take weighted sum of K1, K2, K3
432     end
433
434     % Correct for intergration drift
435     x_now_tmp = x(ii+1,:);
436     [x_new,~] = gauss_newton(x_now_tmp,parms);
437
438     % Update the constraint forces
439     x_new_input = num2cell([x(ii,[3 6 7:12]),t],1);
440     x_update = subs_xdd(x_new_input{:}).';
441
442     % Overwrite position coordinates
443     x(ii+1,:) = [x_new(1:end-4) x_update(end-3:end)];
444
445 end
446 end
447
448 %% Constraint calculation function
449 function [C,Cd,D,Dd] = constraint_calc(x,parms)
450
451 % Get needed angles out
452 x_now_tmp = num2cell(x,1);
453
454 %% Calculate position constraint
455 C = subs_C(x_now_tmp{1:6}).';

```

```

456
457 % Calculate constraint derivative
458 Cd          = subs_Cd(x_now_tmp{[3 6]}).';
459
460 %% Calculate velocity constraint
461 D           = subs_D(x_now_tmp{[3 6:12]}).';
462
463 % Calculate velocity constraint derivative
464 Dd          = subs_Dd(x_now_tmp{[3 6]}).';
465 end
466
467 %% Speed correct function
468 function [x,error] = gauss_newton(x,parms)
469
470 % Get rid of the drift by solving a non-linear least square
    problem by
471 % means of the Gaus-Newton method
472 % Calculate the two needed constraints
473 [C,Cd,~,~] = constraint_calc(x,parms);
474
475 %% Guass-Newton position constraint correction
476 n_iter      = 0;
    % Set iteration counter
    % Get position data out
477
478 % Solve non-linear constraint least-square problem
479 while (max(abs(C)) > parms.tol)&& (n_iter < parms.nmax)
480     x_tmp      = x(1:6);
481     n_iter     = n_iter + 1;
482     x_del      = Cd*inv(Cd.'*Cd)*-C.';
483     x(1:6)     = x_tmp+ x_del.';
484
485     % Recalculate constraint
486     [C,Cd,~,~] = constraint_calc(x,parms);
487 end
488
489 % % Calculate the corresponding speeds
490 % x_tmp_vel    = x(7:12);
491 % Dxd_n1      = -Cd*inv(Cd.'*Cd)*Cd.'*x_tmp_vel.';
492 % x(7:12)     = x_tmp_vel + Dxd_n1.';
493 %

```

```

494
495 %% Gaus-newton velocity constraint correction
496 n_iter          = 0;

    % Set iteration counter

    % Get position data out
497
498 % % Calculate the two needed constraints
499 % [~,~,D,Dd] = constraint_calc(x,parms);
500
501 % % Solve non-linear constraint least-square problem
502 % while (max(abs(D)) > parms.tol)&& (n_iter < parms.nmax)
503 %     x_tmp          = x(7:12);
504 %     n_iter = n_iter + 1;
505 %     x_del   = Dd*inv(Dd.*Dd)*-D.';
506 %     x(7:12) = x_tmp+ x_del.';
507 %
508 %     % Recalculate constraint
509 %     [~,~,D,Dd]          = constraint_calc(x,parms);
510 % end
511
512
513 % Calculate constraints
514 [~,Cd,D,Dd]          = constraint_calc(x,parms);
515 Sd                    = [Cd Dd];
516
517 % Calculate new velocities
518 x_tmp_vel             = x(7:12);
519 Dxd_n1                = -Sd*inv(Sd.*Sd)*Sd.*x_tmp_vel.';
520 x(7:12)                = x_tmp_vel + Dxd_n1.';
521
522 %% Recalculate error
523 [C,~,D,~]             = constraint_calc(x,parms);
524 C_error = C;
525 D_error = D;
526
527 % Store full error
528 error = [C_error D_error];
529 end
530
531 %% Calculate (symbolic) Equations of Motion four our setup
532 function EOM_calc(parms)

```

```

533
534 %% -- The code between this lines is done to obtain the latex
      formulas --
535 % % Create model parameters in symbolic form
536 % syms a b c d m1 m2 J1 J2 g;
537
538 % Overwrite with real values if you don't want the full
      symbolic expression
539 a          = parms.a;
540 b          = parms.b;
541 c          = parms.c;
542 d          = parms.d;
543 m1         = parms.m1;
544 m2         = parms.m2;
545 J1         = parms.J1;
546 J2         = parms.J2;
547 g          = parms.g;
548
549 %% -- The code between this lines is done to create the latex
      formulas --
550
551 % Unpack symbolic variables from parms
552 x1          = parms.syms.x1;
553 y1          = parms.syms.y1;
554 phi1        = parms.syms.phi1;
555 x2          = parms.syms.x2;
556 y2          = parms.syms.y2;
557 phi2        = parms.syms.phi2;
558 t           = parms.syms.t;
559
560 % Generalised state derivative
561 x1d          = parms.syms.x1d;
562 y1d          = parms.syms.y1d;
563 phi1d        = parms.syms.phi1d;
564 x2d          = parms.syms.x2d;
565 y2d          = parms.syms.y2d;
566 phi2d        = parms.syms.phi2d;
567
568 % Create generalized coordinate vectors
569 x            = [x1;y1;phi1;x2;y2;phi2];
570 xd           = [x1d;y1d;phi1d;x2d;y2d;phi2d];
571
572 % Calculate Position constraints

```

```

573 C = [x1+b*cos(phi1)-x2+d*cos(phi2); ...
574 y1+b*sin(phi1)-y2+d*sin(phi2)];
575
576 % Calculate Velocity constraints
577 v1 = [x1d y1d 0;x2d y2d 0].';
578 omega = [0 0 phi1d;0 0 phi2d].';
579 R_A_COM = [-a*cos(phi1) -a*sin(phi1) 0; c*cos(phi2) c
    *sin(phi2) 0].';
580 Va = v1 + cross(omega,R_A_COM);
581 eA = [-sin(phi1) cos(phi1) 0; -sin(phi2) cos(
    phi2) 0].';
582 D_x = simplify([Va(:,1).'*eA(:,1);Va(:,2).'*eA
    (:,2)]);
583
584 % Split constraint in matrix vector product
585 D = equationsToMatrix(D_x,[x1d y1d phi1d x2d
    y2d phi2d]);
586
587 % Compute the jacobian of the (non-)holonomic constraints
588 JC_x = simplify(jacobian(C,x.'));
589 JD_x = simplify(jacobian(D_x,xd.'));
590
591 % Calculate convective component
592 JC_xd = jacobian(JC_x*xd,x);
593 JD_xd = jacobian(D*xd,x);
594
595 % Create system of DAE
596 A = [parms.M JC_x.' D.'
    ; ...
597 JC_x zeros(size(JC_x,1),size(JC_x.',2)) zeros(size(D,1),
    size(D.',2)); ...
598 D zeros(size(D,1),size(JC_x.',2)) zeros(size(D,1),size(D
    .',2))];
599 B = [parms.F ;-JC_xd*xd;-JD_xd*xd];
600
601 % Calculate result expressed in generalized coordinates
602 if parms.accuracy_bool == 0
603     xdd = inv(A)*B; % Less accurate but in
        our case faster
604 else
605     xdd = A\B; % More accurate but it
        is slow
606 end

```

```

607
608 %% Convert to function handles
609 matlabFunction(simplify(xdd),'vars',[x1 y1 phi1 x2 y2 phi2], '
    vars',[phi1 phi2 x1d y1d phi1d x2d y2d phi2d t],'File','
    subs_xdd');
610
611 % Position constraint function handle
612 matlabFunction(simplify(C),'vars',[x1 y1 phi1 x2 y2 phi2], '
    File','subs_C');
613
614 % Position constraint derivative function handle
615 matlabFunction(simplify(JC_x),'File','subs_Cd');
616
617 % Velocity constraint function handle
618 matlabFunction(simplify(D_x),'vars',[phi1 phi2 x1d y1d phi1d
    x2d y2d phi2d],'File','subs_D');
619
620 % Velocity constraint derivative function handle
621 matlabFunction(simplify(JD_x),'File','subs_Dd');
622
623 % Force torque velocity handle
624 if parms.question_bool == 0
625     parms.F = sym(parms.F);
626     matlabFunction(parms.F,'File','subs_F');
627 else
628     matlabFunction(parms.F,'File','subs_F');
629 end
630
631 end

```


References

- [1] Arend L. Schwab. Reader: MultiBody Dynamics B. In *Multibody Dynamics*, chapter 3. TU Delft, Delft, The Netherlands, 2018.