

Computers and Electronics in Agriculture

Using Model-checking for precision spraying

--Manuscript Draft--

Manuscript Number:	COMPAG-D-23-01124
Article Type:	VSI:Fruits and veggies robot
Keywords:	Precision spraying; Model-checking; Cost-Optimal Reachability Analysis; Formal verification; Controllersynthesis
Corresponding Author:	Rim SADDEM FRANCE
First Author:	Rim Saddem-yagoubi
Order of Authors:	Rim Saddem-yagoubi Anice Cheraiet Karen Godary-Dejean Didier Crestani Olivier Naud
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Suggested Reviewers:	Laurent PIETRAC laurent.pietrac@sigma-clermont.fr It was in rapporteur in Rim SADDEM thesis Christine largouet christine.largouet@agrocampus-ouest.fr Dionysis Bochtis d.bochtis@certh.gr Claus Grøn Sørensen claus.soerensen@ece.au.dk Sanjit A. Seshia Seshia sseshia@eecs.berkeley.edu Robert Gardner raj.khosla@colostate.edu Professor of Precision Agriculture

COVER LETTER

Subject: SUBMISSION OF NEW MANUSCRIPT FOR EVALUATION

I am enclosing herewith a manuscript entitled "[Using Model-checking for precision spraying](#)", for possible evaluation, submitted to the special issue entitled "Intelligent and Autonomous Systems for Field Operations in Fruit and Vegetable Production" from *Computers and Electronics in Agriculture*. I received an invitation for Prof. Dr. Liangliang YANG, Guest Editor, to contribute to this special issue.

With the submission of this manuscript, I pledge that the above mentioned manuscript has not been published elsewhere, nor been accepted for publication elsewhere nor is under editorial review for publication elsewhere.

The type of submitted manuscript is an original research paper. This paper refers to previously published research ¹. Yet, its writing and contents are new, with new extensive explanations on modelling, new assessment based on full-scale field data, and a key algorithmic feature required to solve real-world agricultural problems with model-checking: a decomposition method.

Abstract:

One major challenge for agriculture is the sustainable use of pesticides. Once a treatment is deemed necessary, reducing overall sprayed quantities while ensuring required protection to each plant is a major direction for precision agriculture technologies in crop protection. In this paper, a new planning method for Variable Rate Application (VRA) called AMPS (Automata Modelling for Precision Spraying) is presented. It was designed to allow optimising sprayed crop protection products based on canopy density data and recommendations on appropriate spraying commands depending on this data. The new method considers constraints on the sprayer actuators (behaviour, dynamics), and use formal methods (model checking and CORA - Cost Optimal Reachability Analysis algorithm) to find the guaranteed optimised value for spraying a field. As formal methods are well known to have issues with regards to combinatorics, a decomposition methodology is proposed, that uses the specific spatialised characteristic of crops to simplify the modelling and analysis steps. The AMPS methodology is applied to a grapevine case using LiDAR data for characterising vegetation density. The conclusion presents the advances and limitations of this work and suggests ways to improve. Other applications of model-checking in agriculture are also suggested.

Detail of the author with his/her contribution in this paper is as under:

Name of the author and e-mail ID	Types of contribution
Rim SADDEM (rim.saddem@univ-amu.fr)	Design of the research, modelling, algorithmics, writing, numerical experiments and assessment of AMPS method
Anice Cheraiet (anice.cheraiet@inrae.fr)	writing, analysis of LiDAR data and assessment of AMPS method

¹ R. Saddem-Yagoubi, O. Naud, P. Cazenave, K. Godary-Dejean, D. Crestani, Precision spraying: from map to sprayer control using model-checking, Journal of Agricultural Informatics 8 (3)(2017) 1–10.

Olivier Naud (Olivier.naud@inrae.fr)	writing, supervision of the research, assessment of AMPS method, contribution to algorithmics
Didier Crestani (crestani@lirmm.fr)	writing, supervision of the research
Karen Dejean (godary@lirmm.fr)	writing, supervision of the research, supervision of modelling and model-checking

Highlights

- AMPS is a new planning method for Variable Rate Application
- AMPS optimises quantities and ensures required protection to each plant
- AMPS is based on formal methods to guarantee optimal and safe spraying
- AMPS was designed to use terrestrial LiDAR as input information
- AMPS may be adapted to various crop sensors and sprayers
- A decomposition methodology based on specific spatialised characteristic of crops

Using Model-checking for precision spraying

Rim Saddem-Yagoubi^a, Anice Cheraiet^c, Karen Godary-Dejean^b, Didier Crestani^b, Olivier Naud^c

^aLIS, Aix-Marseille University, CNRS , 52 Av. Escadrille Normandie Niemen, Marseille, 13397, FRANCE

^bLIRMM UMR 5506 CNRS, Univ Montpellier, 161 rue Ada, Montpellier, 34392, FRANCE

^cITAP, Univ Montpellier, INRAE, Institut Agro, Montpellier, France,

Abstract

One major challenge for agriculture is the sustainable use of pesticides. Once a treatment is deemed necessary, reducing overall sprayed quantities while ensuring required protection to each plant is a major direction for precision agriculture technologies in crop protection. In this paper, a new planning method for Variable Rate Application (VRA) called AMPS (Automata Modelling for Precision Spraying) is presented. It was designed to allow optimising sprayed crop protection products based on canopy density data and recommendations on appropriate spraying commands depending on this data. The new method considers constraints on the sprayer actuators (behaviour, dynamics), and use formal methods (model checking and CORA - Cost Optimal Reachability Analysis algorithm) to find the guaranteed optimised value for spraying a field. As formal methods are well known to have issues with regards to combinatorics, a decomposition methodology is proposed, that uses the specific spatialised characteristic of crops to simplify the modelling and analysis steps. The AMPS methodology is applied to a grapevine case using LiDAR data for characterising vegetation density. The conclusion presents the advances and limitations of this work and suggests ways to improve. Other applications of model-checking in agriculture are also suggested.

Keywords:

Precision spraying, Model-checking, Cost-Optimal Reachability Analysis, Formal verification, Controller synthesis, UPPAAL-CORA, Optimisation

1. Introduction

The current challenge for agriculture is to improve the quality and quantity of products while preserving the human health and the environment. One of the ways to meet this challenge is to use Precision Agriculture technologies. Precision agriculture has for origin the development of localisation and sensing technologies by which site specific management can be implemented in the field, in order to optimise a given criterion, e.g. economical or environmental benefit [1]. Most recent technologies like multi-spectral imagery and laser scanning, whether airborne or from the ground, allow the acquisition of crop data with a high spatial resolution [2], [3]. On both arable and perennial crops, sensors can be used to quantify and map the dimensional and density characteristics of vegetation ([4]). This spatial information is an opportunity for automation specialists to develop innovative and efficient methods for accurate site specific agricultural action using Variable Rate Application (VRA, [5]) Technologies (VRT). VRT enable optimisation of inputs (fertilisers, amendments, water,

pesticides, etc) with regard to outputs (yield, quality of the product, quality of the environment, profits, etc).

Over the last two decades, VRA as applied to spraying of crop protection products has received growing attention from scientists and seen the production of commercial systems for various crops. This is the case for orchards and vineyards[6].

VRA as of today is mainly enacted according to two alternative application principles. The first principle can be called *real-time* or *on-the-go* VRA. According to this principle, a measurement is done on the crop or on the soil and the rate of application of the agricultural input is modified in real-time according to a set of calculations. Most often, the measurement is a single measurement and the output of the control is also a single one: the rate of application of the agricultural input. Usually, no feedback needs to be implemented on variable rate control. This is because, thinking time on a discrete scale, the action of the machinery at $t + 1$ is not made on the same location as where the action at t was made. Thus, in control science terminology, real-time VRA is

43 most often single-input single-output open loop control.
44 The second principle is VRA according to a recom-
45 mendation or prescription map. In this case, the recom-
46 mendation map is prepared according to geo-localised
47 information previously acquired. Usually, a map is cal-
48 culated according to local variations of a given agro-
49 nomic attribute. So-called "decision rules" are applied.
50 Most often, the quantitative decision rules are based on
51 a linear model. The farmer may have access to parame-
52 ters to tune the recommendation map and to editing fea-
53 tures to override values on the map. Considering high
54 resolution site specific action, one key element is often
55 missing: the behaviour and precision of actuators. This
56 has been recognised in works such as [7] in which the
57 influence of spatial footprint of machinery and of un-
58 certainty of actual output with regard to prescribed set-
59 point are highlighted. One key point is the time of reac-
60 tion, which influences spatial precision along the ma-
61 chine track [8], depending on machine speed. Thus,
62 reaction time and machine behaviour may hinder the
63 proper application of a recommendation map that would
64 be solely based on characteristics of the vegetation. This
65 is why one may think about an alternative approach to
66 recommendation maps: maps with predefined and geo-
67 referenced control set-points (here: spraying configura-
68 tions and flow rates). Such set-points may be defined
69 by an expert according to rules about vegetation and
70 constraints of the sprayer. A control theory can be used
71 to manage these control set-points for automated de-
72 vices using numerical control. For example, the model-
73 checking. The purpose of model-checking here is to
74 verify that a desired state of a system can be reached,
75 and it can provide a sequence of set-points allowing to
76 reach this desired state. Furthermore, using Cost Opti-
77 mal Reachability Analysis (CORA), a sequence that is
78 optimised according to a given cost can be provided.

79 In this paper, the possibility to use model-checking
80 and CORA to compute an optimised control sequence
81 for sprayers in a vineyard is investigated.

82 More specifically, considering the control dynam-
83 ics of a sprayer and the possibility to acquire LiDAR
84 data that characterise the vegetation before spraying,
85 a precision agriculture oriented method that computes
86 an optimal spray command sequence is proposed. The
87 proposed method includes a decomposition technique
88 to leverage the combinatorial explosion issues that
89 are commonly encountered when performing model-
90 checking. An assessment of this method based on Li-
91 DAR data acquired in vineyards in the south of France
92 is provided.

93 This paper builds on previously published research
94 [9] with new extensive explanations on modelling, new

95 assessment based on full-scale field data, and a key al-
96 gorithmic feature required to solve real-world agricul-
97 tural problems with model-checking: a decomposition
98 method. The outline of the paper is as follows. Sec-
99 tion 2 describes the study context. Section 3 details the
100 Automata Modelling for Precision Spraying (AMPS)
101 method. Section 4 is devoted to the decomposition
102 method. In Section 5, experimental results are described
103 and discussed before concluding.

2. Background and study context

104 A short background on model-checking and tooling
105 for cost optimal reachability analysis is provided in the
106 beginning of this section. Details of the precision spray-
107 ing problem to solve are then given. The proposed gen-
108 eral methodology, named AMPS, is described in the fol-
109 lowing section.

110 2.1. Model-checking

111 The Model-Checking (MC) was introduced in the
112 early 1980s [10], [11]. It provides formal verification
113 methods to ensure that the model of a system con-
114 forms to its specifications. It is usually used to anal-
115 yse communications protocols [12] or industrial appli-
116 cations [13], [14], [15].

118 2.1.1. Model-checking phases

119 The model-checking process is based on 3 phases,
120 namely modelling, specification and verification.

121 **The formal modelling phase.**

122 This phase consists in the formal modelling of the sys-
123 tem behaviour. It is mainly based on state machines.
124 States are an abstraction of the status of the system,
125 while the transitions represent events making the system
126 switch from one state to another. For timed systems,
127 temporal constraints can be added to the model. The
128 most popular formalisms for timed systems modelling
129 are Timed Automata (TA) [16] and Time Petri nets [17].

130 **The specification phase.**

131 The specification phase consists in describing the ex-
132 pected system specification using properties. These
133 properties are expressed in logical languages such as
134 LTL (Linear Temporal Logic) or CTL (Computation
135 Tree Logic) [18]. The properties defined for model
136 checking [18] are classically: invariants, safety, absence
137 of deadlock, liveness, state (un)reachability.

138 **The verification phase.**
 139 The verification phase consists in determining if the
 140 model satisfies the specified properties using a model-
 141 checking algorithm. First, the state graph containing
 142 all the possible reachable states is constructed. Then,
 143 this state space is explored, checking the satisfaction
 144 of the properties. Model checkers can record a diag-
 145 nostic trace of the verification process along an exe-
 146 cution path, from the initial state until the property is
 147 (un)satisfied. Tools for model-checking can be classi-
 148 fied in four categories: code analysis model-checkers,
 149 probabilistic model-checkers, ordinary model-checkers
 150 and timed model-checkers. A large and detailed com-
 151 parison of the performance of many formal verifica-
 152 tion environments in checking a safety property has been
 153 made in [19] and has shown that UppAAL is a refer-
 154 ence tool.
 155 UppAAL¹ is a tool chain designed to validate sys-
 156 tems modelled as networks of timed automata. It ex-
 157 tends the TA formalism by adding integer variables,
 158 structured data types, user defined functions, and syn-
 159 chronisation channels [20]. The model checker of Up-
 160 pAAL allows to verify properties on the model of a sys-
 161 tem, analysing its state space. TA and UppAAL have al-
 162 ready been used in the agricultural and ecosystem man-
 163 agement domains (e.g. in [21], [22]).
 164 Concurrently with the model-checking verification
 165 phase, an optimisation process can be carried out using
 166 Cost Optimal Reachability Analysis.
 167 **2.1.2. Model Checking and Cost Optimal Reachability**
 168 **Analysis (CORA)**
 169

170 The notion of optimal cost is often used in schedul-
 171 ing and planning problems. Usually, constraints pro-
 172 gramming or linear programming approaches are used
 173 to solve such problems. The AMETIST project [23]
 174 proposed in 2006 addresses these issues using model
 175 checking and proves the practical applicability of model
 176 checking tools. However, basic MC algorithms do not
 177 include the ability to find an execution path that verifies
 178 at the same time a property and its optimality accord-
 179 ing to a cost criterion chosen by a user. A variant of
 180 UppAAL called UppAAL-CORA [24] [25] can provide
 181 a Cost Optimal Reachability Analysis. It addresses the
 182 problem of finding the minimum cost to reach a goal
 183 state. It has been successfully used for solving var-
 184 ious scheduling and routing problems ([24] including
 185 precision spraying [9] or harvest optimisation problems
 186 ([26], [27])).
 187

188 The CORA algorithm is based on the branch and
 189 bound concept. Depending on the chosen branching
 190 strategy, it may explore the entire state space to find,
 191 among the set of attainable paths, an optimal cost path.
 192 The idea of the branching strategy "*Minimum Cost or-
 193 der*" for reachability properties is to guide the explo-
 194 ration of the state space such that promising sets of
 195 states are visited first [28]. For a given state, a partial
 196 cost is evaluated. Then globally, the state having the
 197 lowest partial cost is explored first. If the obtained state
 198 achieves the goal of reachability, then the path found is
 199 optimal. The so-called Remaining feature can be used
 200 to reduce the number of explored spaces and guide the
 201 exploration process [24].
 202 Since properties verification using model checking is
 203 based on state-space analysis, its main limitation con-
 204 cerns combinatorial explosion.
 205

2.1.3. Limit of Model Checking: The state space explo- sion problem

State space explosion is a problem usually encountered during the verification phase of real systems. Its principal cause is the large size and the complexity of the model of the system to be verified. As MC enumerates exhaustively all the possible reachable states of a system, and stores them to verify properties, the combinatorial explosion affects both the time and space complexity of the verification algorithm. To deal with this problem, various techniques such as the reduction of the state space, the optimisation of modelling, or the limitation of the state space explored during the verification step, have been proposed

The most popular techniques for the reduction of state space are: 1) the binary decision diagram which provides a symbolic representation of states allowing a more compact representation of the state space [29]; 2) the partial order methods which consist in eliminating as much as possible unnecessary interleaving between parallel processes when constructing the state space ([30], [31]); and 3) the symmetry exploitation which is based on the exploitation of the structural symmetries of the system to build a reduced state space [32].

For the optimisation of modelling, the choice of abstractions and simplifications influences greatly the size of the state space. However, the simplified models must guarantee the correctness of the verification of the properties. This requires expertise in the semantics of the modelling language, of the modelling process as well as in the underlying verification technique.

So-called on-the-fly algorithms allow to verify some properties without building the entire state space, reducing the time and the memory used during the verification

¹<https://uppaal.org/>

238 process. This reduction is only effective for properties
 239 which do not require to explore the whole state space
 240 (like reachability ones). These algorithms are also useful
 241 to detect property violation (invariant, safety) since
 242 the first state that does not satisfy the property stops the
 243 verification process.

244 This sub-section summarised the basics of model
 245 checking and of the CORA techniques. Combinatorial
 246 explosion issues were pointed out as well as solutions to
 247 address them. The next section presents, in the context
 248 of precision agriculture, the Precision Spraying problem
 249 on which Model Checking, optimisation cost analysis
 250 and combinatorial explosion limitation methods are applied on.
 251

252 2.2. Detailed definition of the Precision Spraying Problem

253 The spraying problem definition includes the spraying hardware involved, the constraints that need to be defined to guarantee local quality of spraying, and the objective for optimisation.

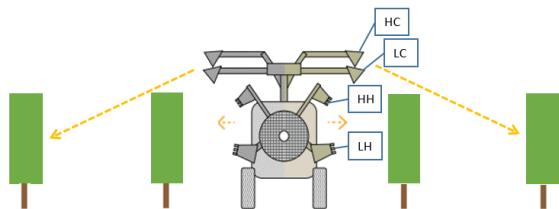
258 2.2.1. Sprayer description

259 In this section, a brief overview on different types
 260 of existing sprayers available for widely-spaced (wide
 261 inter-rows) vines is given. The hypothetical digitally
 262 controlled sprayer considered for the study is then presented.
 263

264 Presentation of a classic pneumatic sprayer.

265 There are several types of sprayers that can be mounted
 266 on or trailed by a tractor: first treatment booms (having
 267 nozzles and no air assistance), airblast sprayers (noz-
 268 zles mounted around a fan that generates the "airblast"
 269 that carries the droplet to canopy), pneumatic arches and
 270 pneumatic face to face sprayers, face to face sprayers
 271 with nozzles and air-assistance that can be turned off at
 272 early growth stages. Face to face sprayers can have re-
 273 covery panels that recycle the spray that is not deposited
 274 in the canopy. In pneumatic sprayers, the air is used
 275 both to break the liquid into droplets and to carry the
 276 droplets obtained into the canopy. In figure 1 presented
 277 an example of a pneumatic arch type sprayer.

278 This sprayer has 4 spraying devices: a low hand (LH),
 279 a high hand (HH), a high cannon (HC) and a low cannon
 280 (LC). A "hand" is a spraying device comprising 2 or 3
 281 nozzles, which will operate at the same time. When the
 282 sprayer is used, the hands spray on one side of the rows
 283 of vines adjacent to the sprayer. Cannons spray on dis-
 284 tant rows of vines and can be arranged in various ways.
 285 In the following, to simplify the modelling and descrip-
 286 tions, only the hands of the sprayer will be considered.
 287



288 Figure 1: Schematic representation in back view of a 4-handed, 4-
 289 cannon pneumatic arch with a low hand (LH), a high hand (HH), a
 290 high cannon (HC) and a low cannon (LC)

292 Hypothetical automated sprayer description.

293 In general, pneumatic sprayers on the market do not
 294 have automatic mechanisms to independently close or
 295 open the spraying spouts in real time. The on-off
 296 switching of spouts is done manually.

297 In the example given in figure 1, for example, both
 298 hands are typically used at the same time when vege-
 299 tation is high enough. However, the automation of the
 300 control of individual spraying elements is essential for
 301 precision spraying. There are published examples of au-
 302 tomated prototypes such as [5], [33].

303 To provide an example for the precision spraying
 304 methodology proposed in this paper, a hypothetical
 305 sprayer that can switch on/off each of its hands inde-
 306 pendently is proposed. In order to provide a mean to reduce
 307 the volume sprayed when vegetation is high but of a low
 308 foliage density, it is supposed that a third Central Hand,
 309 named CH, is added to the original Low Hand (LH) and
 310 High Hand (HH) (Figure 1). CH is supposed designed
 311 and set to that it can cover approximately the same crop
 312 height as LH and HH used together. Spraying with the
 313 CH alone provides only half the volume that combined
 314 LH and HH provide. Indeed, each hand is supposed to
 315 have the same flow rate, which is half the nominal flow
 316 rate (the nominal flow means a full dose of the product).

317 The vertical position of each hand on the sprayer, its
 318 inclination, as well as its lateral distance from the vege-
 319 tation define the height of vegetation it covers. One
 320 important aspect in the hypothetical sprayer considered
 321 is that opening and closing each hand takes some time.

322 In this article, for the sake of simplicity and generic-
 323 ity, we will call each "hand" of sprayer a "nozzle", even
 324 if a "hand" actually comprises several spray sources op-
 325 erating simultaneously. Generally speaking, the prin-
 326 ciple proposed here is that redundant nozzles can be used
 327 to provide both adequate spray targeting as well as the
 328 optimal management of the dose to be applied. This

principle can be applied to many types of sprayers. By redundant nozzles, it is meant that sprays of these nozzles may overlap in the height portion of the vegetation they cover.

2.2.2. Precision Spraying Problem and constraints: A comprehensive definition

The Precision Spraying Problem consists in verifying the aptitude of an agricultural sprayer to respect the constraints of the task while, at the same time, providing an optimal sequence of sprayer commands.

Spraying constraints can be classified into two categories: 1) Sprayer Constraints (SC) related to the dynamics of the agricultural machine, and 2) Agronomic Constraints (AC) which are related to requirements on precision spraying behaviour.

In the context of the study, Sprayer Constraints are the speed of the sprayer (1.4 m/s), the number of nozzles (3), the orientation of the nozzles, the opening time of the nozzles (0.2 s) and the closing time of the nozzles (0.2 s). Agronomic Constraints are about spraying enough and with adequate vegetation targeting to protect each plant from disease. In this paper, AC rely on a Precision Spraying Mapping that stipulates which nozzles to use according to vegetation profile. This mapping is defined in section 3. Because it takes time to open and close valves, one rule is added to AC: when a new set point is required for the set of nozzles, the required nozzles should always be opened before closing the ones to shut down. The agro-environmental objective is to minimise the total quantity of plant protection products sprayed in a field while respecting SC and AC.

More precisely, given a grapevine crop organised in rows, the objective of the Precision Spraying Problem (PSP) is to find a sequence of sprayer commands that sprays the entire crop while respecting all spraying constraints (SC and AC) and minimising the total quantity of sprayed product.

To resolve PSP, a method called Automata Modelling for Precision Spraying (AMPS) has been designed. It is described in the next section.

3. The AMPS methodology

This section presents the AMPS method for precision spraying.

3.1. General description of AMPS

The AMPS method takes 2D ground-based LiDAR data of the canopy as input. It then computes, for a given sprayer with individual control of nozzles, a command

sequence optimised for a cost criterion while ensuring a sufficient protection on each vine plant. The flow rate and the response time for opening or closing the nozzles are parameters taken into account in the modelling as they will affect the choice of the most appropriate command for the sprayer.

AMPS is based on 3 steps, represented in figure 2:

Step 1: Define a static correspondence function between the vegetation density and the spray commands. This function, called "Precision Spraying Mapping" (PSM), maps each possible vegetation state to two spray commands: the most suitable command C_{best} , and an alternative acceptable command C_{alt} . These two commands guarantee sufficient protection for each vine plant. This step is based on human expertise about spraying and crop protection. The PSM may be tailored according to a grower's expertise and attitude towards its crop management. As the AMPS method is modular, steps 2 and 3 are not dependent on the PSM that is chosen.

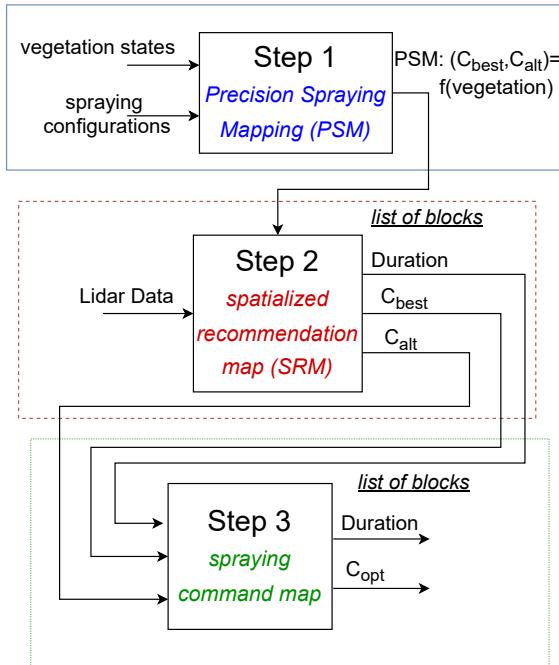


Figure 2: AMPS Method

Step 2: Apply a data processing algorithm to raw LiDAR data from scans of vine rows. This algorithm produces for each row a Spatialised Recommendation Map (SRM). First, the algorithm uses aggre-

gation and filtering rules to form blocks of vegetation which have a uniform vegetation density. The length of each block can vary from one block to another, with a minimum length that is consistent with nozzles response times. The algorithm uses the PSM function to assign to each vegetation block of the targeted vine the appropriate spray commands (C_{best} and C_{alt}).

Step 3: It is the core of AMPS methodology. Based on formal methods (model checking with CORA), it produces a spraying command map, with, for each identified vegetation block, its treatment time and the selected spray command (named C_{opt}). The SRM obtained in step 2 is input data of the PTA_AMPS model presented in section 3.4.1. PTA_AMPS models the set of the spraying operation and the dynamics of the sprayer. This model is used to compute the optimal command sequence to spray a row with a minimum quantity of product.

In the following, each step of the AMPS methodology is detailed and illustrated on a vineyard case study.

3.2. Step 1: The Precision Spraying Mapping

In order to build the Precision Spraying Mapping (PSM), step 1 takes as input the different possible states of vegetation and the different possible commands of the sprayer. As an output, it generates a set of spray commands that are compatible with each possible state of vegetation. In this work, two alternative commands are considered, one being considered as the best.

3.2.1. Vegetation characterisation

A state of vegetation is described by a set of qualitative values which characterises its spatial density. Each vegetation block is considered homogeneous in its characteristics, which are defined according to its height.

Each vegetation block is divided into 3 horizontal sections depending on the height. The very low area, which mainly consists of trunk and weeds or grass, is not considered for spraying. Then we consider a "Low" (L) and a "Middle" (M) sections, and finally the "High" (H) section for the higher canopy. The total height (T) is also considered as a section, such that $T=L+M+H$. In our example, the thresholds to separate the height sections will be defined in section 5.

Thus, a vegetation state is represented as a quadruplet T-L-M-H of density values. 3 qualitative density values are considered: 0, 1, 2, which respectively represent absence of vegetation, low vegetation density, and high vegetation density.

The values of vegetation density are obtained from raw 2D LiDAR data according to thresholds that will be described in section 5. The number of LiDAR beam interceptions in each section within a block is supposed to be representative of foliage quantity and canopy porosity. Considering the 4 sections (T, H, M, L) and 3 values for each of these, 81 vegetation states could be enumerated. Yet, because of consistency between total section T and other sections, and because of actual vine behaviour in the field, there are much less combinations observable in practice.

Also, specific blocks without any vegetation are considered: the "missing vegetation" blocks. The decision to consider a block as "missing vegetation" is taken with regard to the M section ($T-H-M-L = xx0x$). Indeed, statistics show that if M is empty, it means that the vine plant has not grown.

3.2.2. Correspondence between vegetation states and spray commands

The PSM function maps spray commands to each value of the quadruplet T-H-M-L of the field under study. In this study, the PSM function was produced using expertise based on the test of real sprayers on an artificial vineyard bench [34].

7 spray commands were considered. Their name is based on the nozzles used for spraying:

- 3 commands with one nozzle (LH , CH , HH), with therefore a debit of 50% of the nominal flow.
- 3 commands with two nozzles ($LH\&CH$, $LH\&HH$, $CH\&HH$), i.e. the nominal flow.
- a command with all nozzles off, noted –.

HH covers section H and a good part of M section, CH covers H, M and L with a reduced dosage if it is used alone, and LH covers well section L and a good part of M section.

Two spraying commands: C_{best} and C_{alt} are mapped to each possible vegetation state. C_{best} sprays the best dose (neither too high nor too low) at the best place and therefore corresponds to the most appropriate command. The alternative command C_{alt} sprays a local dose guaranteeing a protection of the vine, but which can use more spraying product and can be less adequately targeted than C_{best} . When no satisfactory alternative can be defined, then $C_{alt}=C_{best}$.

The Table 1 shows the mapping of C_{best} and C_{alt} for a selection of several vegetation states of our field under study. Supplementary material of the paper provides the whole mapping used in this study.

T-H-M-L	C_{best}	C_{alt}
xx0x	—	—
1010	LH	HH
1011	LH	CH
1022	LH&CH	LH&CH
1110	HH	CH
1111	CH	CH
1210	HH	CH&HH
2012	LH	LH&CH
2122	LH&CH	LH&HH
2222	LH&HH	LH&HH

Table 1: Excerpt of PSM function

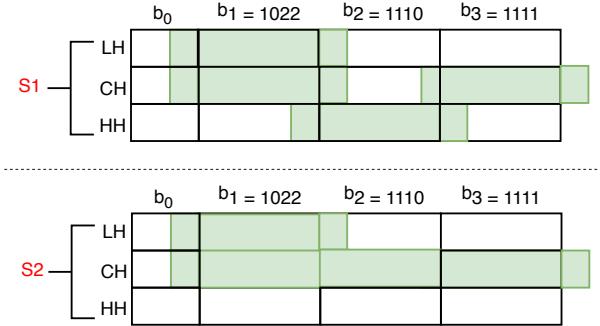


Figure 3: Interest of the alternative spray commands

492 3.2.3. Interest of alternative spray commands

493 The need to map two commands to each vegetation
 494 block instead of just C_{best} results from the response time
 495 of the nozzles. Choosing a unique local and ideal spray
 496 command for each block may not provide the optimal
 497 spraying on the whole field due to transition times in
 498 opening and closing nozzles. Indeed, to avoid insuffi-
 499 cient spraying, when spray command is changed, any
 500 nozzle to be set ON needs to be activated before the be-
 501 ginning of the blocks, and any nozzle to be set OFF is
 502 deactivated after the end. In addition, during the closing
 503 and opening phase of a nozzle, the flow of this nozzle is
 504 not zero. So, changing too frequently a spray command
 505 can lead to an unnecessary overexposure of the vege-
 506 tation to pesticides. This effect of nozzles dynamics is
 507 precisely why a computing framework is needed for a
 508 better control design. It is important to outline that in
 509 this application of model-checking with optimisation,
 510 spraying enough product on each vine plant is a con-
 511 straint for production safety (vine production point of
 512 view) and that quantities sprayed overall on the whole
 513 vine plot should be optimised (environmental and eco-
 514 nomical point of view).

515 Let's consider for example, as in figure 3, a row of
 516 vines composed of 3 blocks b_1 , b_2 and b_3 with respec-
 517 tive vegetation states 1–0–2–2, 1–1–1–0 and 1–1–1–1.
 518 According to the Table 1 (green boxes), only 2 se-
 519 quences of commands are possible: the best one $S1 =$
 520 $(LH\&CH, HH, CH)$, and $S2 = (LH\&CH, CH, CH)$
 521 which uses the command C_{alt} for the block b_2 . But the
 522 change of command for b_2 in $S1$ involves more closing
 523 and opening of the nozzles than in $S2$. Let's compute

524 the Product Consumed (PC) for each sequences:

$$\begin{aligned} PC_{S1} &= Open(LH) + Open(CH) \\ &+ Q_1(LH) + Q_1(CH) + \textbf{Open}(HH) \\ &+ Close(LH) + \textbf{Close}(CH) + Q_2(HH) \\ &+ \textbf{Open}(CH) + \textbf{Close}(HH) \\ &+ Q_3(CH) + Close(CH) \end{aligned}$$

$$\begin{aligned} PC_{S2} &= Open(LH) + Open(CH) \\ &+ Q_1(LH) + Q_1(CH) \\ &+ Close(LH) + Q_2(CH) \\ &+ Q_3(CH) + Close(CH) \end{aligned}$$

525 with:

- $Open(X)$: the amount of product sprayed when opening the nozzle $X \in \{LH, CH, HH\}$. It is in fact independent of the nozzle considered, but this notation facilitates the understanding.
- $Close(X)$: the same for closing the nozzle X .
- $Q_i(X)$: quantity of product sprayed during the block b_i by the nozzle X .

533 Assuming that all nozzles have the same flow ($Q_i(X)$ is
 534 the same $\forall X$), it follows that $Q_2(CH) < Open(HH) +$
 535 $Close(CH) + Q_2(HH) + Open(CH) + Close(HH)$ and
 536 consequently $PC_{S2} < PC_{S1}$. This proves that the use of
 537 an alternative command instead of the preferred one can
 538 reduce the cost of a spraying sequence.

539 In conclusion, for step 1, PSM is a static mapping
 540 function that assigns to each vegetation state two possi-
 541 ble spraying commands. In step 2, a recommendation
 542 map will be established, i.e. a link between the vege-
 543 tation at each location in the field and the appropriate
 544 commands.

545 3.3. Step 2: Definition of the spatialised recommenda- 586
 546 tion map 587

547 The step 2 consists in the processing of real LiDAR 588
 548 data to obtain a list of vegetation blocks for a row, us- 589
 549 ing the PSM function of step 1. At the end, each block 590
 550 will be characterised by its commands C_{best} and C_{alt} 591
 551 and by its duration (the time required to spray in this 592
 552 block). Each block should be long enough to guarantee 593
 553 the opening and closing of the nozzles at the right time, 594
 554 but short enough to effectively discriminate the vegeta- 595
 555 tion density. Thus the data processing algorithm of step 596
 556 2 is designed to finely adapt the duration and the number 597
 557 of blocks in a row.

558 3.3.1. Initial LiDAR data processing 598

559 The LiDAR data is first analysed by slices of reduced 599
 560 width (10 cm) in order to detect with good spatial accu- 600
 561 racy the absence or presence of vegetation.

562 For each vegetation slice, and for each horizontal sec- 601
 563 tion within a slice (T, H, M and L), the number of Li- 602
 564 DAR beam interceptions is counted, then converted into 603
 565 a qualitative value on {0, 1, 2}. This makes it possible 604
 566 to obtain a vegetation state coded in the form T-H-M- 605
 567 L for each slice, while respecting the selected thresh- 606
 568 olds. Therefore, it is now possible to establish a first 607
 569 specialised recommendation map (SRM) for these slices 608
 570 using the PSM function, as shown in table 2.

block number	vegetation state	C_{best}	C_{alt}
block 1	1011	LH	CH
block 2	1001 → 1011	-	-
block 3	1011	LH	CH
block 4	1021	LH	CH

609 Table 2: Example of the building of the SRM 630

611 But it is not possible with our hypothetical automated 612 sprayer to change nozzles for each slide. Indeed, at 613 a speed of 1.4 m/s (about 5 km/h), 10 cm represents 614 only a duration of 0.07s. Yet, as explained seen in sec- 615
 616 tion 2.2.2, the opening or closing time of the nozzles 617 requires 0.2 s. Thus, slices must be grouped into blocks 618 having a minimal length of 50 cm.

619 Therefore, a block identification algorithm based on 620 filtering and aggregation rules was established.

621 3.3.2. Aggregation and filtering of blocks

622 1. Homogenisation of similar slices:

623 In order to benefit from the similarity of neigh- 619
 624 bouring slices, the first Rule for Aggregation 620
 625 and Filtering (named *RAF1*) is applied for each 621
 626 slice and each horizontal section in the slice. 621

RAF1: Let s_{i-1} , s_i and s_{i+1} be 3 successive 599
 600 slices, X denotes a horizontal section ($X \in$ 601
 602 {H, M, L}) and $vegState(X, i)$ denotes the vegeta- 603
 604 tion state in the horizontal section X for the slice s_i .

$$(vegState(X,i - 1) = vegState(X,i + 1)) \\ \Rightarrow vegState(X,i) \leftarrow vegState(X,i + 1)$$

For example, in table 2, as the block 2 has two sim- 599
 600 ilar neighbours for the section M , then its vegeta- 601
 602 tion state becomes 1011.

Then, from vegetation state and using PSM func- 599
 600 tion, C_{best} and C_{alt} commands are computed. 601
 602 *RAF2* is, then, applied for each slice and each com- 603
 604 mand (C_{best} and C_{alt} commands).

RAF2: Let $Cmd[i]$ denotes the command for the 601
 602 block s_i ($cmd \in \{C_{best}, C_{alt}\}$)

$$(Cmd[i - 1] = Cmd[i + 1]) \\ \Rightarrow Cmd[i] \leftarrow Cmd[i + 1]$$

603 *RAF2* is defined for the homogenisation of com- 604
 605 mands. For example, in table 2, this rule makes the 606
 607 C_{best} command of the block 2 become LH and the 608
 609 C_{alt} command of the block 2 become CH .

610 2. Identification and aggregation of the "missing 611 vegetation" blocks:

The objective is then to separate the vegetation 612 blocks from the missing vegetation blocks, for 613 which the spraying command must close all the 614 nozzles. Now, if there is a block between two miss- 615
 616 ing vegetation blocks and that the command for 617 this block uses only one nozzle (meaning this is 618 block has low density) then this block can be con- 619
 620 sidered a missing vegetation block (*RAF3*).

RAF3: Let $C_{best}[i]$ the command C_{best} for the 619
 620 block s_i , similarly for C_{alt} and $merge(s_i, \dots, s_n)$ a 621
 622 function that merge the blocks s_i to s_n in s_i :

$$(C_{best}[i - 1] = -) \wedge (C_{best}[i + 1] = -) \wedge \\ (C_{best}[i] \in \{LH, HH, CH\}) \\ \Rightarrow C_{best}[i] \leftarrow - \wedge C_{alt}[i] \leftarrow - \wedge merge(i - 1, i, i + 1)$$

623 3. Aggregation of similar slices: At this point, 624
 625 the location of the missing vegetation blocks has 626
 627 been accurately detected. Now, the contiguous

622 slices having the same command can be grouped 657
 623 (RAF4).
 624

625 **RAF4:** Let $C_{best}[i]$ the command C_{best} for the 658
 626 block s_i , similarly for C_{alt} and $merge(i_1, \dots, i_n)$ as 659
 627 defined before:
 660

$$[(C_{best}[i] = C_{best}[i+1]) \wedge (C_{alt}[i] = C_{alt}[i+1])] \\ \Rightarrow merge(i, i + 1)$$

628 **4. Aggregation of narrow isolated slices:** At this 665
 629 point, the most similar vegetation blocks were ag- 666
 630 gregated. In the case where too small blocks re- 667
 631 main, *RAF5* consists in associating the remaining 668
 632 small blocks (size < 50 cm) with its larger neigh- 669
 633 bouring block at the condition that this block is not 670
 634 a missing vegetation block.
 635

636 **RAF5:** Let $sizeBlock[i]$ the size of block s_i , func- 673
 637 tion $max(i, j)$ (resp. $min(i, j)$) returns the number 674
 638 of the block with the bigger (resp. lower) size and 675
 639 $merge(i, j)$ as defined below:
 640

$$(sizeBlock[i] < resolution) \wedge \\ (C_{best}[max(i - 1, i + 1)] != -) \\ \Rightarrow merge(i, max(i - 1, i + 1))$$

$$(sizeBlock[i] < resolution) \wedge \\ (C_{best}[max(i - 1, i + 1)] = -) \Rightarrow \\ merge(max(i, min(i - 1, i + 1)), min(i, min(i - 1, i + 1)))$$

641 Please note that iteration of *RAF5* needs to be per- 690
 642 formed adequately in order to avoid that, starting 691
 643 from the first blocks, blocks would much often 692
 644 grow according to the left-hand side. Once s_i and 693
 s_{i+1} have been merged, the algorithm has to ad- 694
 645 dress next the blocks that were identified s_{i+2} and 695
 s_{i+3} before the merging.
 696

646 To conclude, RAF rules of AMPS methodology, al- 697
 647 low to extract a list of vegetation blocks from a raw Li- 698
 648 DAR data using the PSM function. The blocks were 699
 649 grouped depending on their vegetation density, and 700
 650 missing vegetation blocks were detected and precisely 701
 651 located. By considering a fixed sprayer speed through- 702
 652 out the row, the block lengths are converted into spray- 703
 653 ing durations. The computed spatialised recom- 704
 654 mendation map (SRM) which associates to each identified 705
 655 block, its duration and its C_{best} and C_{alt} commands will 706
 656 be used in the model presented in the next section to 707
 657 compute the optimal command sequence.
 658

3.4. Step 3: Definition of the spraying command map

659 The step 3 of AMPS, based on the model-checking 660 process, allows to compute and verify an optimal 661 spraying command map. At the first step, a formal 662 model for the Precision Spraying Problem (PSP), called 663 *PTA_PSP* and based on a network of Priced Timed Au- 664 tomata [24], was designed. The SRM obtained in step 665 2 is an input data of this model. The model represents 666 the *possible* behaviours of the automated sprayer. Spec- 667 ifications on *expected* spraying behaviour are then ex- 668 pressed in CTL temporal logic with reference to the 669 model. During the verification phase, these properties 670 are checked on the model, including the specific prop- 671 erty that computes the optimal command sequence.
 672

The model-checking process was implemented using 673 the Uppaal-CORA tool.

3.4.1. Modelling the Precision Spraying Problem

674 The *PTA_PSP* model is schematized in figure 4. It is 675 composed of 7 Priced Timed Automata with the follow- 676 ing functions:
 677

- 678 • Row start automaton (SA): manages the 679 starting of spray in the row,
- 680 • Movement automaton (MA): manages the move- 681 ments of the sprayer inside the row from block to 682 block,
- 683 • Anticipation automaton (AA): selects the 684 spraying command for the next vegetation block,
- 685 • Control nozzles automaton (CA): manages 686 the opening and closing of each nozzle according 687 to the chosen spraying command,
- 688 • Nozzles automata (NA_i): represent the 689 behaviour of each nozzle (3 nozzles represented by 690 3 automata).

Input data. As shown figure 2, the input of the mod- 691 els is SRM (i.e. for each block a C_{best} and C_{alt} com- 692 mand and a duration of spraying). Each command is 693 defined by the sets of nozzles that must be respectiv- 694 ely opened and closed. These input data are represented 695 in the dashed magenta nodes on figure 4. They are de- 696 fined in the model as command static data, implemented 697 as global constants available for each automaton.

Global variables. The global structure of our model 698 is based on several global variable shared by all the 699 automata. In particular, `currentBlock` is an integer 700 representing the index of the vegetation block that the 701 sprayer is currently spraying, while `nextBlock` is an 702

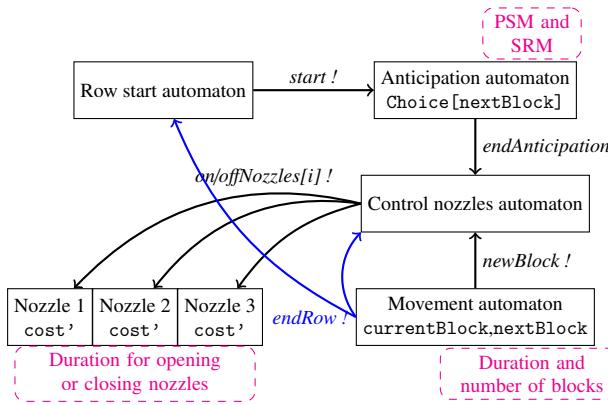


Figure 4: Scheme of our model: automata synchronisation, input data and main global variables

703 integer representing the index of the next vegetation
 704 block, necessary to anticipate the opening of the noz-
 705 zles. Also, the spraying command chosen by the antici-
 706 pation automaton is stored in a table $\text{Choice}[]$ which
 707 records the optimal command for each of the blocks.

708 **Synchronization between automata.** Automata can be
 709 synchronized through two types of channels: Binary
 710 channels (a transmitter and a single receiver) and Multi-
 711 ple channels (a transmitter and many or zero receivers).
 712 For example, in the model *PTA_PSP* and as shown fig-
 713 ure 4, *newBlock* is a binary channel sent at the end of
 714 each block. There are also two tables of binary chan-
 715 nels *onNozzle* and *offNozzle*. *endRow* (to indicate
 716 the end of the row) and *endAnticipation* (to indicate
 717 that a command has been selected for the next block)
 718 are multiple channels.

719 **Modelling of the cost.** The quantity of sprayed prod-
 720 uct is modeled for each nozzle in the nozzles automata,
 721 using the cost rate function cost' . This function rep-
 722 resents in UppAAL-CORA the flow of product sprayed
 723 at any time by the nozzle considered. The higher the
 724 flow, the higher the cost will be at the end. In UppAAL-
 725 CORA, this cost rate is an integer. The following con-
 726 ventions were used. When a nozzle is closed, then
 727 $\text{cost}'=0$. When a nozzle is fully opened (has normal
 728 flow) then $\text{cost}'=2$. During transitions for opening or
 729 closing a nozzle, the flow is neither zero nor maximum.
 730 These transitions are represented by a flow rate reduced
 731 by half ($\text{cost}'=1$).

732 3.4.2. Verifying properties and computing the (optimal) 733 Command Sequence

734 Specifications on the expected spraying behaviour of
 735 the Precision Spraying problem are described and for-

736 malised using UppAAL's syntax requirement specifica-
 737 tion language² (inspired from CTL temporal logic).

738 The property used to obtain the *optimal command*
 739 sequence with the lowest cost is:

740 "Is there a command sequence that allows the sprayer to
 741 reach the end of the row (while applying the command
 742 constraints specified in the model)?" This property is
 743 translated in temporal logic *PP1* by:

744 **PP1:** $E \Leftrightarrow \text{currentBlock} == \text{nb_block-1}$ and
 745 SA.end ,

746 with *SA* is the Row start automaton, *end* is a state in
 747 *SA* which denotes that the sprayer reaches the end of
 748 the row and all nozzles are off, *nb_block* is the number
 749 of blocks forming the row and *currentBlock* is the block
 750 currently sprayed.

751 The resulting command sequence can be a mixture of
 752 C_{best} and C_{alt} commands. It is possible to impose the
 753 use of only C_{best} or C_{alt} command.

754 UppAAL-CORA checks the properties and provide
 755 a trace with the lowest cost. As in the model the cost
 756 function calculates the total amount of product sprayed,
 757 the cost calculated in the optimal command is the min-
 758 imum quantity of product necessary to spray the row
 759 while ensuring sufficient protection.

760 The model checking with the CORA function thus al-
 761 lows to obtain an accurate command optimising the cost
 762 criteria (here, the quantity of spraying product) while
 763 guaranteeing the correct behaviour of the sprayer. But
 764 the model checking strength can be its weakness: the
 765 enumeration of all the possible cases which guaranty the
 766 verification results also implies an intrinsic complexity.
 767 For this reason, the use of model checking on real and
 768 complex application cases is known to be difficult [35].
 769 In a case such like solved here, vine rows can contain
 770 many blocks (over 100 blocks) and for each block two
 771 commands are possible. Therefore, the complexity of
 772 deciding between these two commands for each block
 773 of a row is exponential to the number of blocks.

774 To overcome the combinatorial explosion problem
 775 that may result from this, a decomposition methodology
 776 based on the spatial characteristic of the precision agri-
 777 culture problem at hand was developed. It is described
 778 in the next section.

779 4. Decomposition methodology

780 The overall idea of the proposed decomposition
 781 methodology is to break down the system and/or the

782 ²<https://docs.uppaal.org/language-reference/requirements-specification/>

782 verification into sub-parts that can be solved indepen- 831
783 dently regarding the properties to be validated over the 832
784 whole system. 833

785 The hard part of the model checking decomposition 834
786 is to find how to decompose while preserving a consis- 835
787 tent expression of "local" properties with regards to the 836
788 "global" ones. While the decomposition criteria pro- 837
789 vided here are specific to the Precision Spraying Prob- 838
790 lem, the intent is to propose a generic decomposition 839
791 method that can be used for decision support in other 840
792 agricultural domains or beyond. 841

793 The decomposition of a model checking problem 842
794 should consist in three phases: the decomposition of 843
795 the model (modelling decomposition), the decomposi- 844
796 tion of the verification process (verification decompo- 845
797 sition) and the analysis of the decomposition (decom- 846
798 position analysis). Modelling decomposition partitions 847
799 the model into n sub-models. 2 sub-models may have 848
800 an overlap zone in common and this will be detailed in 849
801 section 4.1. 850

802 The decomposition of verification is about decom- 851
803 posing the resolution of the property to be checked on 852
804 the global model into the resolution of properties on the 853
805 sub-models. The decomposition analysis is about prov- 854
806 ing that this verification of the properties on the sub- 855
807 models guaranties the verification of the initial property 856
808 on the global model. 857

809 The outline of the section follows the 3 above- 858
810 mentioned phases. 859

811 4.1. Modelling Decomposition 860

812 The modelling decomposition consists in decompos- 861
813 ing the model into n parts. One or several criteria for 862
814 decomposition need to be found out in order to proceed 863
815 to this. 864

816 **Decomposition criterion.** The intrinsic spatial char- 865
817 acteristics of the agricultural applications provide guid- 866
818 ance for decomposing. The geometrical structure of 867
819 most of the agricultural fields is a useful element for de- 868
820 composition. In the Precision Spraying problem, con- 869
821 sidering that each row is sprayed independently, step 870
822 3 of AMPS methodology can be applied separately to 871
823 each row. The decomposition of a model including n 872
824 rows to n models including each a unique row is thus 873
825 straightforward. On the practical side, the model pre- 874
826 sented in 3.4 was designed for one row, with a set of 875
827 data for each row of the studied field. Steps 1 and 2 of 876
828 AMPS are better applied at a larger scale (field or vine- 877
829 yard) in order to have consistent crop protection of the 878
830 vineyard. 879

Other characteristics may be used to find a decomposition criterion, depending on the application cases. The idea is to find an agricultural characteristic that imposes a fixed and known value in the verification process. This value will be the pivot of the decomposition strategy for verification. In the Precision Spraying case, where an optimal spraying command sequence is searched, the optimal command sequence before the pivot should be independent of the optimal command sequence after it. From this idea, two criteria were identified for the Precision Spraying problem in order to decompose the verification of a row. The first one relates to blocks with missing vegetation. The command to be applied in this case is to close all the nozzles. This criterion is close to the spatial decomposition of the different rows, as the nozzles are closed between two rows, with the significant difference that sub-systems overlap on missing vegetation blocks. The impact of overlapping will be explained hereafter.

A criterion that is more complex to handle can be extracted considering the PSM function. The presence of a block where $C_{best} = C_{alt}$ in a row represents a case where the command to apply is known a priori. These blocks allow to break the dependency between the sequence of commands before and after them, which is the basic need for the decomposition process. The MC decomposition based on the criterion $C_{best} = C_{alt}$ is the most complex with regards to the three phases of decomposition and is detailed in the following.

Forming row parts. A row part is a subset of successive blocks of a row. The row parts are defined so that there is an overlapping block that belongs to two successive parts. The case considered here is the case where an overlapping block has the property that $C_{best} = C_{alt}$. Such block will be called hereafter a "same command block".

Thus, a row R is decomposed into n parts $\{P_1, \dots, P_n\}$. Each P_i is a set of blocks which begins with a block where $C_{best} = C_{alt}$ or with the first block of the row, and which ends with a block where $C_{best} = C_{alt}$ or with the last block of the row.

The figure 5 illustrates, by an example, the formation of the row parts.

The hypothetical example row R is formed of 5 blocks. The block $\{b_3\}$ is a same command block ($C_{best} = C_{alt}$). The part P_A is made up of blocks b_1, b_2 and b_3 . The part P_B starts from block b_3 included and contains also b_4 and b_5 . b_3 is the overlapping block.

Generating sub-models. Using the *PTA_PSP* model for UPPAAL-CORA, the generation of the sub-models for each row part consists only in editing the

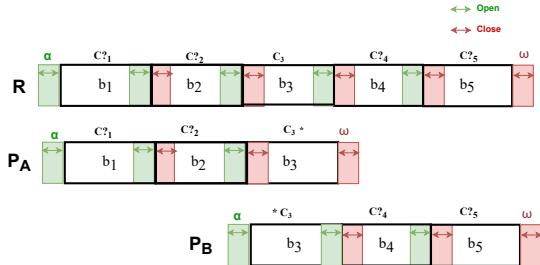


Figure 5: Decomposition of row R in two parts

input data of the model. No change is needed in the description of the automata. The global constants describing commands are updated with information related to the corresponding row part: the value of the number of blocks forming the row is replaced with the value of the number of blocks forming the part (constant `nb_block`); and all the tables storing the information of these blocks will be updated with only the concerned blocks. It is worth noting that, as the configuration of the models is based on text files, the modelling decomposition is automated. It is also important to have in mind that, because the model of a part of a row is a model of a row with a reduced number of blocks, some parts have a "virtual row ending" (part P_A in figure 5) and some have a "virtual row beginning" (parts P_B in same figure). Real beginnings and endings of rows have the characteristic that all the nozzles should be off before and after spraying the row. Technically, in the model of a part of a row, this constraint is also applied to its virtual beginning and its virtual ending. The consequences of this for calculating the optimal sequence and the optimal cost for a whole row from the optimal sequences and optimal costs for the parts are analysed in section 4.3.

4.2. Verification Decomposition

The verification decomposition decomposes the resolution of the property to be checked on the global model into the resolution of properties on the sub-models.

Let us recall that the property allowing to obtain the optimal command sequence applied on all the rows is the property PP1 described in the section 3.4.2. The verification process on the sub-models is based on the same property, but with the modifications of the models previously mentioned.

The decomposition of the verification consists in verifying this property on each row part. It is important to note that in the model of a part, `nb_block` becomes the number of blocks forming the part and

$S_{\text{StartRowAut.end}}$ is reached when the sprayer finishes spraying all the blocks of the part.

Checking the property PP1 on the sub-model allows to calculate the Optimal Sequence to be applied on the part and to calculate its Optimal Cost. The complete optimal sequence can be calculated from the concatenation of the optimal sequences of the parts, and the global optimal cost can be calculated from the sum of the optimal costs of the parts. Rules for concatenation and cost rectification terms respectively required in these operations when overlapping occurs in decomposition (see figure ??) will be explicated hereafter.

4.3. Decomposition Analysis

The decomposition analysis is about proving that the verification of the properties on the sub-models allows the verification of the initial property on the global model. Let us consider a row, or row part such as in figure 5, which can be described by equation 1:

$$S_R = \emptyset \triangleright C?_1 \triangleright C?_2 \triangleright C_3 \triangleright C?_4 \triangleright C?_5 \triangleright \emptyset \quad (1)$$

In equation 1, \emptyset means that all nozzles are off. $C?_i$ denotes a choice to make for block b_i and C_i is the command for block b_i when it has a unique possibility. The decomposition can be made here using block b_3 as overlapping block. Sequences S_A and S_B for the resulting parts P_A and P_B can be written:

$$S_A = \emptyset \triangleright C?_1 \triangleright C?_2 \triangleright C_3 * \triangleright \emptyset \quad (2)$$

$$S_B = \emptyset \triangleright *C_3 \triangleright C?_4 \triangleright C?_5 \triangleright \emptyset \quad (3)$$

The symbol $*$ either on the left or on the right of C_3 denotes that overlapping occurs here. The concatenation law for parts having an overlapping is given in equation 4. It can easily be shown that when applying this concatenation law to S_A and S_B , then $S_R = S_A \triangleright S_B$.

$$C * \triangleright \emptyset \triangleright \emptyset \triangleright * C = C \quad (4)$$

Now, as written in equation 5, the rectification terms for calculating the cost of S_R from the costs obtained for S_A and S_B once solved by CORA algorithm can be formulated. Considering that the cost for C_3 has been counted once in S_A with C_3* and once again in S_B with $*C_3$ then the cost $Q_3(C_3)$ of this command should be retrieved from the sum of costs of parts. Considering also that there was no actual closing and re-opening of nozzles for C_3 between C_3* and $*C_3$, the formulation of the cost correction term is provided in equation 6. This reasoning applies to any decomposition of a row in n parts by simple recursion of cutting a part in two.

960 The calculation of optimal cost of a row from optimal
961 sequences on n row parts is thus demonstrated.

$$c(S_A \triangleright S_B) = c(S_A) + c(S_B) + corr(S_A \triangleright S_B) \quad (5)$$

$$corr(S_A \triangleright S_B) = -Q_3(C_3) - close(C_3) - open(C_3) \quad (6)$$

963 In this section, it was shown how to proceed to
964 model-checking decomposition. In section 6, the
965 decomposition methodology will be applied on a real vine
966 plot. The next section details the data acquisition sys-
967 tem and presents the vineyard on which our precision
968 spraying approach will be tested.

969 5. LiDAR field data

970 5.1. 2D LiDAR information of canopy structure

971 A Sick LMS100 (SICK AG, Düsseldorf, Germany)
972 2D LiDAR sensor was used in the study. The LMS100
973 is a fully-automatic divergent laser scanner based on
974 time-of-flight (TOF) measurement with a typical error
975 of ± 30 mm, a selectable angular resolution set to 0.5° ,
976 a maximum scan angle of 270° and a maximum range
977 of 20 m. With these settings, there were 541 distances
978 recorded for each complete laser rotation, which is here-
979 after referred to as a “scan”, and scans were obtained
980 at 50 Hz. The LMS100 laser emission wavelength is
981 905 nm (near infrared) and it is Class one eye-safe.
982 The LMS100 and data logging system were mounted on
983 a purposely-built stainless-steel mast fixed behind the
984 tractor operating the sprayer, according to a previously
985 described procedure [36]. The LMS100 sensor height
986 ranged from 1.1 m above ground level. The tractor was
987 driven along the vineyard rows at a constant forward
988 travel speed of 5 km/h, with a typical error of ± 0.21
989 km/h. This sensing system was coupled to a Real Time
990 Kinematic (RTK) GNSS receiver (Teria GSM correc-
991 tion, Vitry-sur-Seine, France) to identify the start and
992 end point of the sampling units. Once the starting point
993 was set, scans were aggregated using a fixed forward
994 distance based on the constant tractor speed to gener-
995 ate a 3D point cloud reconstruction of the vine environ-
996 ment. The sprayer replicated commercial operations,
997 i.e. the tractor only traversed every second row so that
998 the canopy was only scanned from one side. This dif-
999 fers from most previous research activities with LiDAR
1000 sensors, but was deliberately done to approximate com-
1001 mercial conditions. Full details of the system set-up are
1002 given in [36].

5.2. Field data

1003 A vine estate with one block, "Aglae" (*Vitis vinifera*
1004 L. cv Marselan), was chosen for the study in 2019. Lo-
1005 cated in Grabels, close to Montpellier (Hérault, France),
1006 the Mas Piquet Estate is characteristic as a vineyard
1007 from the south of France, both in terms of grape vari-
1008 eties and training systems. The rows were northeast-
1009 southwest oriented. Vines were trellised in 2.5 m rows
1010 with a 1.0 m vine spacing within rows using a cordon
1011 Royat system that comprised a cordon wire and at least
1012 one trellising wire. 2D LiDAR acquisitions were carried
1013 out on the date 2019/07/31 during the season. This date
1014 corresponds to the beginning of veraison (81) in BBCH
1015 scale growth stages [37].

1016 From the data obtained, we were able to study the dy-
1017 namics at an intra-plot scale of canopy height and width.
1018 The height and width of the vegetation increased almost
1019 linearly from the flowering stage to the bunch closure
1020 stage. At the scale of the whole plot, the vegetation
1021 height was between 0.85 m and 1.64 m, and a vegeta-
1022 tion thickness of between 0.39 m and 0.95 m. Trim-
1023 ming, combined with increasing water stress over sum-
1024 mer, tends to stagnate any further growth.

1025 In order to define vegetation states and as explained
1026 in section 3.2.1, some thresholds need to be set. The
1027 thresholds to separate the height sections were respec-
1028 tively set to 0.3, 0.7 and 1.1 m and the maximum vine
1029 height was set to 1.7 m. The discrimination threshold
1030 between 1 and 2 was chosen as the median of the num-
1031 ber of LiDAR beams interceptions in the considered
1032 horizontal section and for the whole field. The thresh-
1033 olds for abstract value 0 were chosen specifically for
1034 each horizontal section: below 5 LiDAR intercep-
1035 tions for a 10 cm wide scan slice for H section, below 34%
1036 of the median for M section and below 10% of the median
1037 for L section. It is important to note that such thresh-
1038 olds depend on the BBCH scale growth stages, and they
1039 were defined for all rows forming the plot.

1040 In the following, the AMPS method and the decom-
1041 position methodology will be implemented on the study
1042 plot.

6. RESULTS & DISCUSSION

1043 In this section, we will apply the AMPS method for
1044 real vine LiDAR data. The optimal command sequence,
1045 taking into account sprayer dynamics, will be compared
1046 to classical spraying without automation.

1047 The AMPS step 1 consists on defining the precision
1048 spraying mapping, which maps each vegetation state to
1049 two spray commands C_{best} and C_{alt} . We have already to
1050

1052 provide this map in Section 3.2 (cf. Table 1). Now, we 1078
 1053 proceed to apply step 2.

1054 *6.1. Computation of blocks and spatialized recommen-
 1055 dation map*

1056 The AMPS step 2 consists in the processing of the Li-
 1057 DAR data to obtain C_{best} , C_{alt} and the duration of each
 1058 vegetation block for the studied plot. The sprayer is sup-
 1059 posed to move at 1.4 m/s . The length of a block is ex-
 1060 pressed as a function of the time needed to spray it. The
 1061 tables 3, 4 and 5 provide for an analysis of the step 2 of
 1062 the algorithm and are explained and commented in the
 1063 sequel.

1064 In the table 3, the column "Row" provides an iden-
 1065 tifier to each row, this ID is a value between 1 and
 1066 5. The column "D" represents the duration of time (in
 1067 s) needed to spray the row in seconds (s). The col-
 1068 umn "NB" gives the number of blocks forming the row,
 1069 the column "M" provides the number of blocks with
 1070 a missing vegetation and the column "NS" gives the
 1071 number of blocks where the command C_{best} is equal
 1072 to the command C_{alt} . The column " D_{max} " (in s) pro-
 1073 vides the higher duration of a block in the row, the col-
 1074 umn " ND_{min} " provides the number of blocks having
 1075 the smaller duration of 0.4 s in the row and the column
 1076 " NL " provides the number of blocks having a duration
 1077 longer than 1 s in the row.

Row	D (s)	NB	M	NS	D_{max} (s)	ND_{min}	NL
1	40,1	58	1	24	1,7	16	9
2	65,2	84	2	44	2,1	21	23
3	67,9	89	5	43	4,6	21	15
4	71,2	82	5	42	3,6	18	26
5	70,5	90	0	41	5,3	27	19

Table 3: Row decomposition

In all rows, the number of "same command" blocks represent around 50% of the number of blocks forming the row. This has two consequence for this particular field and date: the optimisation has an effect on approximately half of the blocks of row, and there are many blocks that can be chosen to support model decomposition for calculating optimal spraying sequences.

Veg.states (THML)	R1	R2	R3	R4	R5
'x x 0 x '	X	X	X	X	X
'1 0 1 0 '				X	
'1 0 1 1 '	X	X	X	X	X
'1 0 1 2 '	X	X	X	X	X
'1 0 2 1 '	X	X		X	
'1 0 2 2 '	X	X	X	X	X
'1 1 1 0 '	X	X	X	X	X
'1 1 1 1 '	X	X	X	X	X
'1 1 1 2 '	X	X	X	X	X
'1 1 2 0 '	X		X		
'1 1 2 1 '	X	X	X	X	X
'1 1 2 2 '	X	X	X	X	X
'1 2 1 0 '	X	X	X	X	X
'1 2 1 1 '	X	X	X	X	X
'1 2 1 2 '	X	X	X	X	X
'1 2 2 0 '	X	X	X	X	
'1 2 2 1 '	X	X	X	X	X
'2 0 1 2 '	X				
'2 0 2 1 '	X				X
'2 0 2 2 '	X		X		X
'2 1 1 2 '	X	X	X	X	X
'2 1 2 0 '					X
'2 1 2 1 '	X	X	X	X	X
'2 1 2 2 '	X	X	X	X	X
'2 2 1 0 '			X	X	
'2 2 1 1 '	X	X	X	X	X
'2 2 1 2 '	X	X	X	X	X
'2 2 2 0 '	X			X	
'2 2 2 1 '	X	X	X	X	X
'2 2 2 2 '	X	X	X	X	X

Table 4: Vegetation states distribution in row

The table 4 describes for each row the vegetation states encountered before and after applying step 2. Before step 2, states are related to vegetation slices (thin blocks) and after it, states are related to vegetation blocks of various sizes. Some states are deleted and others are added due to the aggregation rules implemented in step 2. Deleted states (resp. added states) are represented with cross (X) in a red color (resp. blue color).

1093 Black cross means that the vegetation state is encountered
 1094 before and after applying step 2.

1095 It can be seen that some vegetation states are present in
 1096 all rows such as (T-H-M-L) = (1-1-1-1). The vegetation
 1097 state (T-H-M-L) = (1-1-2-0) is added in the row 1 after
 1098 applying *RAF1* and some states are present in some
 1099 rows and deleted after applying *RAF1* such as (T-H-M-
 1100 L) = (1-0-1-1) present in the rows 1, 2 and 3 and deleted
 1101 in rows 4 and 5. This is due to the minimum size of the
 1102 block. Many states that are present in slices are deleted
 1103 when applying step2. Only one state is added and in
 1104 only one row.

1105 In table 5 are analysed the frequencies of potential
 1106 commands for blocks, before choice between C_{best} and
 1107 C_{alt} that is made at step 3. For each row and for each alterna-
 1108 tive C_{best} (row C_b) or C_{alt} (row C_a), the frequency
 1109 of each spray command is provided, as a percentage of
 1110 the number of blocks in the row and as a percentage of
 1111 the duration in the row. Let us recall that from the pre-
 1112 cision sprayer mapping defined in step 1 of AMPS (cf.
 1113 section 3.2), 7 spray commands were considered. Their
 1114 names are here abbreviated: – (all nozzles off), L (LH),
 1115 C (CH), H (HH), $L\&H$ ($LH\&HH$), $L\&C$ ($LH\&CH$),
 1116 and $C\&H$ ($CH\&HH$). The frequency for number of
 1117 blocks is defined as N/T where N is the number of
 1118 blocks having this command and T is the number of
 1119 blocks in the row. The frequency for duration is de-
 1120 fined as D/R where D is the sum of the durations of the
 1121 blocks having this command and R is the duration for
 1122 spraying the whole row.

1123 The frequencies for number of blocks and durations
 1124 are consistent. In 4 of the 5 rows, the most frequent
 1125 preferred command is the usual $LH\&HH$ which corre-
 1126 sponds to dense vegetation. CH is also a very frequent
 1127 preferred command in these rows, which allows to re-
 1128 duce the overall consumption of phytosanitary products
 1129 when C_{best} is chosen at step 3. The first row has lower
 1130 vigour and the most frequent preferred command in this
 1131 row is CH . CH corresponds to spraying the whole veg-
 1132 etation height when lower density is present. The com-
 1133 mands LH and HH are less frequent but useful. The
 1134 command HH does not appear in any row and any con-
 1135 trol sequence. This was expected. Indeed, from the pre-
 1136 cision spraying mapping defined in AMPS step 1, the
 1137 command HH appears, for the C_{alt} control sequences, in
 1138 the vegetation state (T-H-M-L) = (1-0-1-0) and for the
 1139 C_{best} control sequences, in the vegetation states (T-H-M-
 1140 L) = (1-1-1-0) and (T-H-M-L) = (1-2-1-0) (cf. yellow
 1141 rows in the Table 4). The vegetation states in yellow
 1142 cells are deleted after applying the step 2 of AMPS due
 1143 to the aggregation rules. Therefore, the command HH
 1144 does not appear.

Row	Cmd	% nb blocs						% duration							
		–	L	C	H	$L\&H$	$L\&C$	$C\&H$	–	L	C	H	$L\&H$	$L\&C$	$C\&H$
$R1$	C_b	1.7	17.2	43.1	0	15.5	5.2	17.2	2	17.2	48.6	0	13.7	4.5	14
$R1$	C_a	1.7	1.7	29.3	0	62.1	1.7	3.4	2	2.2	35.7	0	56.4	1.2	2.5
$R2$	C_b	2.4	6.0	26.2	0	35.7	16.7	13.1	2.3	5.7	28.4	0	39.1	14.3	10.3
$R2$	C_a	2.4	0	15.5	0	56.0	14.3	11.9	2.3	0	16.9	0	58.9	11.0	10.9
$R3$	C_b	5.6	11.2	22.5	0	33.7	6.7	20.2	10.8	9.6	21.5	0	32.8	5.6	19.7
$R3$	C_a	5.6	0	16.9	0	56.2	13.5	7.9	10.8	0	16.3	0	55.8	11.0	6.0
$R4$	C_b	6.1	9.8	24.4	0	36.6	11.0	12.2	11.2	11.2	23.9	0	36.7	9.3	8.7
$R4$	C_a	6.1	0	15.9	0	57.3	13.4	7.3	11.2	0	15.3	0	56.0	11.4	6.0
$R5$	C_b	0	6.7	25.6	0	34.4	11.1	22.2	0	5.4	23.5	0	40.3	12.5	18.3
$R5$	C_a	0	0	16.7	0	62.2	13.3	7.8	0	0	15.2	0	67.4	11.1	6.4

Table 5: Analysis of block commands

The following subsection will deal with the calculation of the optimal command sequence.

6.2. Computation of spraying command map using decomposition analysis

Let us recall that the optimal command sequence is obtained by verifying property PP1 on the *PTA_PSP*

1151 model using the UppAAL-CORA tool.

1152 It was not possible to find the optimal command se-
 1153 quence for any row without using the decomposition
 1154 method, due to the combinatorial explosion problem,
 1155 which typically occurs 2 to 3 minutes after the start of
 1156 the verification. Two reasons explain this combina-
 1157 torial explosion: the first is related to the intrinsic com-
 1158 plexity of model-checking. Indeed, by simplifying, if
 1159 we consider only the complexity for one row which is
 1160 composed, at least, of 58 blocks and for each block in
 1161 this row two commands are possible, which makes a
 1162 complexity of at least 2^{58} . To find the best cost, the
 1163 model checking process generates a significant part of
 1164 the whole tree and it explodes. The second reason is
 1165 related to a technical limitation of the UppAal-CORA
 1166 model-checking tool. Indeed, the available binary of
 1167 UPPAAL-CORA was built only for a 32-bit architec-
 1168 ture, which limits the memory usage to 4 GB of RAM.
 1169 Computing the optimal command sequence using more
 1170 than 4 GB of memory was therefore technically not pos-
 1171 sible.

1172 To overcome the combinatorial explosion in order to
 1173 be able to compute the optimal command sequence, the
 1174 decomposition methodology was applied.

1175 6.2.1. Modelling Decomposition

1176 Let us recall that the modelling decomposition con-
 1177 sists on decomposing the row into n row parts and then, ¹²⁰¹
 1178 generates the sub-model associated to each part. The ¹²⁰²
 1179 decomposition criterion here is $C_{best} = C_{alt}$. From Ta- ¹²⁰³
 1180 ble 3 and in all rows, the number of blocks having the ¹²⁰⁴
 1181 same commands (column NS) represents around 50% ¹²⁰⁵
 1182 of the number of blocks forming the row (column NB). ¹²⁰⁶
 1183 Therefore, applying the decomposition criterion $C_{best} = ¹²⁰⁷$
 1184 C_{alt} each time it happens in the sequence would produce ¹²⁰⁸
 1185 many row parts of 2 blocks and would unnecessarily ¹²⁰⁹
 1186 complicate the validation process. Thus, the decompo- ¹²¹⁰
 1187 sition process was arranged so that parts would have a ¹²¹¹
 1188 minimum length of 25 blocks. This value was deter- ¹²¹²
 1189 mined from expertise after calculation trials. ¹²¹³

1190 In the table 6, the column "Row" is the identifier ¹²¹⁴
 1191 of each row. The column "NB" gives the Number of ¹²¹⁵
 1192 Blocks forming the row, the column "NP" provides the ¹²¹⁶
 1193 Number of Parts, the column "PL" gives the Part Limits, ¹²¹⁷
 1194 and the column "NB.P" provides the Number of Blocks ¹²¹⁸
 1195 in each Part. ¹²¹⁹

1196 It can be noted that, in general, the number of blocks ¹²²⁰
 1197 forming parts is between 26 and 30 blocks. The last part ¹²²¹
 1198 of each row has a small size (between 7 and 13 blocks) ¹²²²
 1199 because it is formed by the rest of blocks forming the ¹²²³
 1200 row. ¹²²⁴

R	NB	NP	PL	NB.P
1	58	3	$b_0_b_{26}, b_{25}_b_{51}, b_{50}_b_{59}$	26, 26, 8
2	84	4	$b_0_b_{26}, b_{25}_b_{52}, b_{51}_b_{77}, b_{76}_b_{85}$	26, 27, 26, 8
3	89	4	$b_0_b_{27}, b_{26}_b_{52}, b_{51}_b_{81}, b_{80}_b_{90}$	27, 26, 30, 9
4	82	4	$b_0_b_{26}, b_{25}_b_{51}, b_{50}_b_{76}, b_{75}_b_{83}$	26, 26, 26, 7
5	90	4	$b_0_b_{27}, b_{26}_b_{53}, b_{52}_b_{78}, b_{77}_b_{91}$	27, 27, 26, 13

Table 6: Row decomposition

6.2.2. Spray savings

In this section, the spray savings are analysed for each of the five rows.

In the table 7, the column "Row" is the identifier of each row. The column "NB" gives the Number of Blocks forming the row. The column "Classical cost" gives the cost while using the classical spray configuration $LH\&HH$ for the entire row. The column "Best cost" gives the cost while using the best spray configuration C_{best} thanks to the two first steps of AMPS. The column "Optimal cost" gives the cost while using the third step of the AMPS method, which computes the optimal spray configuration (a mixture of the C_{best} and C_{alt} commands).

The optimal cost is the lowest in the Table 7. It provides a saving of 2% to 4 % with reference to a sequence choosing always C_{best} (best cost) and a saving of 10% to 28 % with reference to classical spraying (constant $LH\&HH$, which requires no automation). The saving between best cost and optimal cost is small in this example. This is due to the number of blocks having the same commands which represents around 50% of the number of blocks forming the row.

Besides performances of the approach on the specific

Row	NB	Classical cost	Best cost	Optimal cost
1	58	1604	1192	1148
2	84	2608	2344	2244
3	89	2716	2226	2156
4	82	2848	2220	2176
5	90	2820	2596	2548

Table 7: Comparative spraying configurations

example provided, the interest of the AMPS method is its genericity (the same model can be used for the verification of several properties) and its capacity to manage complexity (dealing with the combinatorial explosion problem using the decomposition methodology).

7. Conclusion

This paper dealt, in the context of the phytosanitary treatment of vineyards, with the issue of discrete control sequences for variable rate application in precision agriculture. The objective was to handle the dynamics of sprayer nozzles dynamic so that two objectives can be simultaneously achieved: getting sufficient protection on each plant and reducing overall the use of the phytosanitary products in the field. Based on model checking and Cost Optimal Reachability Analysis, this paper proposed a complete method to address this objective in which accuracy, optimality and complexity issues are handled.

The proposed Automata Modelling for Precision Spraying (AMPS) method is decomposed in 3 main steps. The preliminary phase catches the human expertise and defines the links between the best (C_{best}), the alternative appropriate (C_{alt}) sprayer commands and the vegetation density to obtain an accurate and acceptable protection. Step 2 performs aggregation of raw LiDAR data to obtain manageable density characteristics of vine rows as a sequence of vegetation blocks to which can attached possible commands for nozzles, with a preferred and an alternative command for each block. Finally, from Priced Timed Automata modelling that represent the sprayer movement inside a row and the functioning of nozzles, step 3 uses model checking and the UppAAL-CORA tool to compute the optimal and accurate sequence to spray a row with a minimal quantity of phytosanitary product.

In addition, to address real vineyard applications and deal with the problem of combinatorial explosion of the state-space, a decomposition method of the model-checking analysis was proposed.

The limitations of this research may be analysed in order to identify further research needs:

- Genericity: the paper was written with an example of possible spraying technology. It can be easily extended to actual and various sprayer types of today and of the future. The control method proposed here allows to handle sets of nozzles which would have overlapping sprays, in order to precisely target the vegetation to protect.
- Ergonomic design of decision-support: it is clear that the tooling used in this paper is not fit for a direct use by farmers. The AMPS method was implemented in a software tool that can automatically generate an optimal spraying command from LiDAR Data using the current model of an imaginary sprayer. A flexible and adaptable human-machine interface should now be developed to facilitate the dialogue with the end-user and for modelling various sprayers. An alternative to the development of a customisable tool would be that a manufacturer of a variable rate sprayer would model it and propose a decision system based on field data.
- Consideration of new spraying criterion: 2 criteria were considered in this paper: the accuracy and the optimality of the command. The quality of spraying is implicitly represented in the paper by C_{best} and C_{alt} configurations. Quality could be quantified and be the subject of optimisation.
- MC analysis performance: the paper is based on UppAAL-CORA tool. There are alternatives to UppAAL for modelling timed systems and temporal issues. Yet, available tools for performing CORA analysis are limited. Implementing CORA features in other model-checkers would allow to compare performances and select tooling that best minimises computation time and/or the amount of the required hardware memory.

Other questions concerning precision agriculture could be treated using model checking.

Furthermore, model checking can also be useful to optimize the control of an agricultural robot or a multi-robot team, or to ensure their safety or security.

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66–70.

1440 **Appendix A. Detailed description of PTA_PSP** 1474
 1441 **model**

1442 In this annex, we proposed a detailed description of
 1443 each automaton that is part of the model *PTA_PSP*. Let
 1444 us recall that *PTA_PSP* model is composed of 7 Priced
 1445 Timed Automata:

- Row start automaton (SA): manages the starting of spray in the row,
- Movement automaton (MA): manages the movements of the sprayer inside the row from block to block,
- Anticipation automaton (AA): selects the spraying command for the next vegetation block,
- Control nozzles automaton (CA): manages the opening and closing of each nozzle according to the chosen spraying command,
- Nozzles automata (NA_i): represent the behaviour of each nozzle (3 nozzles represented by 3 automata).

1459 **Appendix A.1. Row start automaton (SA)**

1460 This automaton, represented in the figure A.6, manages the startup phase. It sends a command event
 1461 "start0" to the *anticipation automaton* to select a
 1462 command for the first block. When selection is
 1463 finished, it receives from the *anticipation automaton*, a "finishAnticipation" event. Then, it sends
 1464 "start1" event to the *nozzle control automaton* to
 1465 activate the nozzles for the first block. It waits
 1466 *max_temp_open_Nozzle* the time required for nozzles
 1467 to be opened. It sends to the *movement automaton* a
 1468 "new_block" event to start spraying at the first block.
 1469 When spraying is finished it receives an "endRow"
 1470 event. When all nozzles are closed (*allClose == true*),
 1471 it passes to the state *end*.

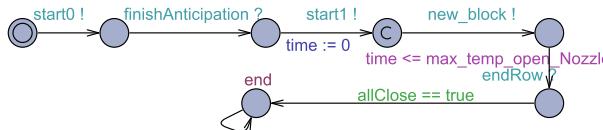


Figure A.6: Row Start automaton

1474 **Appendix A.2. Anticipation automaton.**

1475 This automaton, represented in the figure A.7, makes
 1476 it possible to select a command for the following block.
 1477 The two possible commands for each vegetation block
 1478 are C_{best} and C_{alt} which are stored respectively in $CBest$
 1479 and $CAlt$. The *anticipation automaton* first receives the
 1480 signal "start0" from the *Row Start automaton*. Then,
 1481 if the value of the variable *Choice* is -1 (choice not
 1482 predefined) then it chooses an order from $CBest$ and
 1483 $CAlt$, stores its choice in the variable *Choice* and calls
 1484 the function *updateNextNozzle*. If *Choice* is prede-
 1485 fined, then this choice is followed. Finally, the *an-
 1486 ticipation automaton* sends, in broadcast, the event
 1487 "finishAnticipation" and updates the variable *anticipe*
 1488 to false so as not to loop indefinitely.

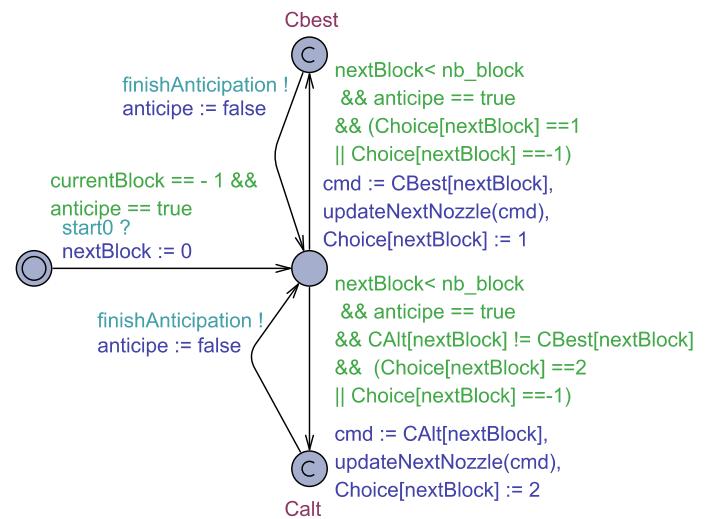


Figure A.7: Anticipation automaton

1489 **Appendix A.3. Movement automaton.**

1490 This automaton, represented on the figure A.8, al-
 1491 lowes to represent the movement of the sprayer. The time
 1492 required to spray a vegetation block is computed in step
 1493 2, based on the length of the block and the speed of the
 1494 sprayer. This information is stored in the *tempo_block*
 1495 variable. At the start, the sprayer is in the "Init"
 1496 state. When it receives the start event "new_block",
 1497 it goes to the state *block*. The state *block* has an
 1498 invariant $t_block \leq tempo_block[currentBlock]$, the
 1499 sprayer remain in this state for the duration of this
 1500 block. The state *block* has also a guard $t_block ==$
 1501 $tempo_block[currentBlock]$ on its outgoing transitions,
 1502 the automaton signals the end of a block by sending in

1503 broadcast the event "new_block" and the end of a row by
 1504 sending in broadcast the event "endRow" (it then returns
 to the state *Init*).

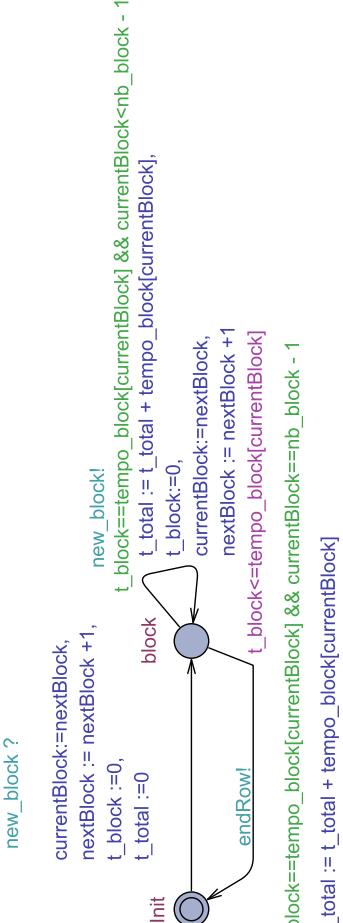


Figure A.8: Movement automaton

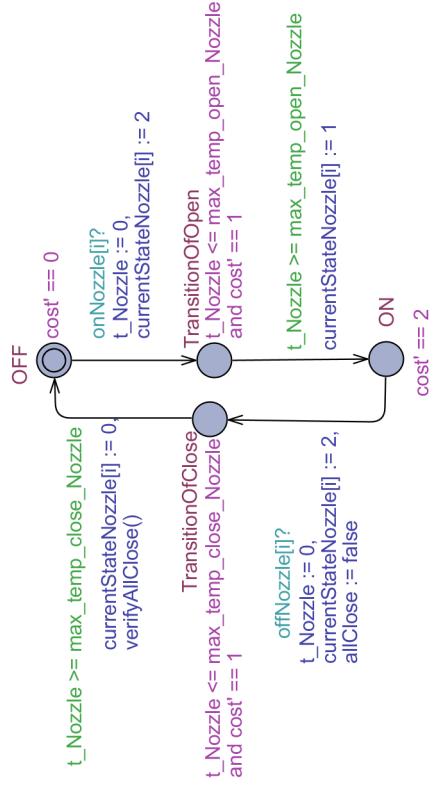


Figure A.9: Nozzles automata

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nal "finishAnticipation" from *the Anticipation automaton*, it calls the function *control()* which determines the nozzles to be opened or closed for the next block. To secure the quantity of sprayed product in each block, the nozzles selected for opening are opened 0.2s before the start of the block (the value 0.2 is stored in the constant *max_temp_open_Nozzle*). Conversely, those which must be closed will not be completely closed until 0.2s after the block change (the value 0.2 is stored in the constant *max_temp_close_Nozzle*). To open a nozzle i, the *nozzle control automaton* sends, *max_temp_open_Nozzle* before the end of the current block, the event *onNozzle[i]* (see guard *t_block <= tempo_block[currentBlock] - max_temp_open_Nozzle*), and to close the nozzle i, it sends the event *offNozzle[i]*, after having received the synchronization event *new_block* from *the movement automaton*. As soon as the commands on the nozzles are effective, then the variable *anticipe* is set to *True* to allow anticipation for the next block.

1506 Appendix A.4. Nozzles automata.

1507 These automata represent the behavior of each nozzle
 1508 (figure A.9). Each of these automata has four states:
 1509 *OFF* (initial state), *ON*, *TransitionOfOpen* (opening)
 1510 and *TransitionOfClose* (closing). It receives the
 1511 signals "*onNozzle*" and "*offNozzle*" to pass from a
 1512 state to another. The nozzles response time, for open-
 1513 ing or closing, is supposed to be a fixed and known
 1514 (*max_temp_open_Nozzle*, *max_temp_close_Nozzle*). It
 1515 is set at 0.2s in our example.

1516 Appendix A.5. Control Nozzles automaton.

1517 The role of this automaton, described in figure A.10,
 1518 is to control the nozzles. When it receives the sig-

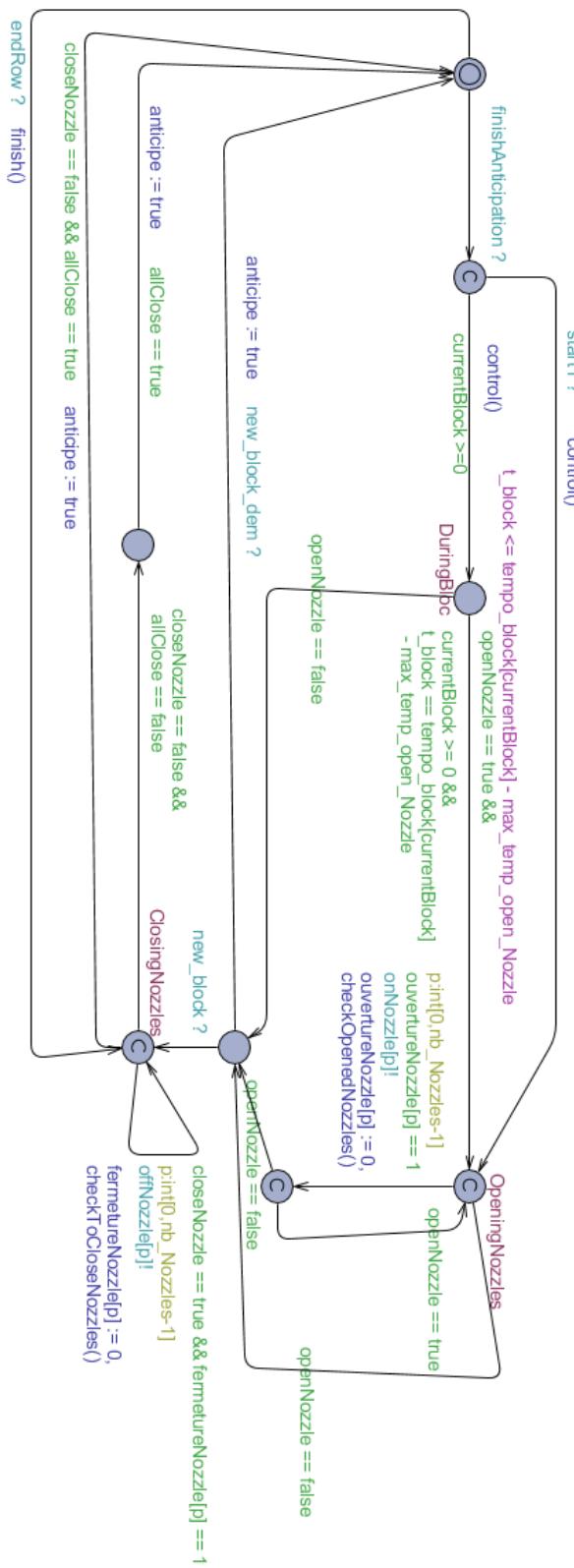


Figure A.10: Control Nozzles automaton

1539 **Appendix B. Details on decomposition analysis**

1540 The decomposition analysis is about proving that the
 1541 verification of the properties on the sub-models allows
 1542 the verification of the initial property on the global
 1543 model.

1544 The idea of the proof will be illustrated on a row com-
 1545 posed of 5 blocks, named b_1 to b_5 , as shown in fig-
 1546 ure B.11. The duration of each block is greater than
 1547 the sum of the opening and closing times of the nozzles,
 1548 which is a necessary assumption given in the step 2 of
 1549 AMPS. The row is divided into 2 parts: P_A groups to-
 1550 gether the first three blocks, and P_B includes the blocks
 1551 b_3 to b_5 . b_3 is the overlapping block and so is included
 1552 in both P_A and P_B . The decomposition criterion is such
 1553 that $C_{best} = C_{alt}$. Thus, on the block b_3 for which over-
 1554 lapping occurs, the command is known.

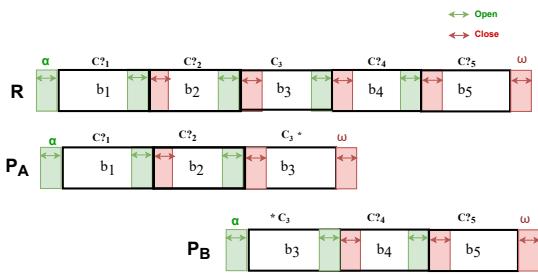


Figure B.11: Illustration of the decomposition to support proof

1555 For the example row R depicted in figure B.11, a se-
 1556 quence S_R for the whole row can be written:

$$S_R = C?_1 \triangleright C?_2 \triangleright C_3 \triangleright C?_4 \triangleright C?_5 \quad (B.1)$$

1557 where C_i is the command for block b_i when it is
 1558 unique (as for the overlapping block b_3) and where $C?_i$
 1559 denotes a choice to make for block b_i .

1560 In order to take into account that, before each row,
 1561 and at the end of each row, all nozzles should be closed,
 1562 equation B.1 rewrites, with \emptyset meaning all nozzles off:
 1591

$$S_R = \emptyset \triangleright C?_1 \triangleright C?_2 \triangleright C_3 \triangleright C?_4 \triangleright C?_5 \triangleright \emptyset \quad (B.2)$$

1563 Sequences S_A and S_B for parts P_A and P_B can be writ-
 1564 ten:

$$S_A = \emptyset \triangleright C?_1 \triangleright C?_2 \triangleright C_3 \triangleright \emptyset \quad (B.3)$$

$$S_B = \emptyset \triangleright *C_3 \triangleright C?_4 \triangleright C?_5 \triangleright \emptyset \quad (B.4)$$

1565 The symbol $*$ either on the left or on the right of C_3
 1566 denotes that overlapping occurs here.

1567 Details on the costs (product consumed) need now to
 1568 be given. A rule was enunciated in section 2.2.2 which
 1569 can be rephrased in the following way. When changing
 1570 from one block to another, opening the nozzles needed
 1571 in the new block and which were closed before has to be
 1572 anticipated in the end of the previous block. Conversely,
 1573 the nozzles no longer needed in the new block will be
 1574 closed at the beginning of the new block. The conse-
 1575 quences of this rule were explained in figure 3 and sec-
 1576 tion 3.2.3. The costs for opening a nozzle X ($Open(X)$),
 1577 using a nozzle X on a bloc b_i ($Q_i(X)$), and closing a noz-
 1578 zle X ($Close(X)$) were also introduced in section 3.2.3.

1579 Let now C_i be a command used for a block b_i which
 1580 can be defined as a set of opened nozzles. This set C_i is
 1581 any subset of $\Omega = \{LH, CH, HH\}$ with a cardinal infe-
 1582 rior or equal to 2, including the null set \emptyset (for missing
 1583 vegetation blocks and outside rows).

1584 The cost $Q_i(C_i)$ of using the nozzles of command C_i
 1585 during block b_i can be written:

$$Q_i(C_i) = \sum_{X \in C_i} Q_i(X) \quad (B.5)$$

1586 The cost $c(C_i, C_j)$ of changing from one command C_i
 1587 to a command C_j in the next block may be decomposed
 1588 in:

$$\begin{aligned} c(C_i, C_j) &= open(C_i, C_j) + close(C_i, C_j) \\ open(C_i, C_j) &= \sum_{X \in C_j \setminus C_i \cap C_j} Open(X) \\ close(C_i, C_j) &= \sum_{X \in C_i \setminus C_i \cap C_j} Close(X) \end{aligned}$$

1589 Costs of sequences can now be calculated. The cost
 1590 $c(S)$ of a sequence $S = C_{i-1} \triangleright C_i \triangleright C_{i+1}$ is the following:

$$c(S) = Q_{i-1}(C_{i-1}) + c(C_{i-1}, C_i) + Q_i(C_i) + c(C_i, C_{i+1}) + Q_{i+1}(C_{i+1}) \quad (B.6)$$

1591 The costs for the start ($\alpha = \emptyset \triangleright C$) and the end ($\omega = C \triangleright \emptyset$) of a part or of a row are:

$$c(\alpha) = open(C) + Q(C) \quad (B.7)$$

$$c(\omega) = Q(C) + close(C) \quad (B.8)$$

1593 The concatenation law for parts having an overlap-
 1594 ping and the rectification terms for costs of concatenated
 1595 parts can now be formulated. Considering the example
 1596 of figure B.11 and the sequences provided in equations
 1597 B.2, B.3 and B.4, it follows that:

$$S_R = S_A \triangleright S_B \Rightarrow C_3 * \triangleright \emptyset \triangleright \emptyset \triangleright * C_3 = C_3 \quad (B.9)$$

1598 1599 1600 1601 1602 Concatenation rule for row parts. Considering two row parts overlapping on a block for which command C is known a priori (because $C_{best} = C_{alt}$), the concatenation rule for handling the overlapping block is the one of equation B.10

$$C * \triangleright \emptyset \triangleright \emptyset \triangleright * C = C \quad (B.10)$$

1603 1604 1605 1606 1607 Considering that there is overlapping at block b_3 for which command should not be counted twice, and that termination *oslash* of part S_A and beginning *oslash* of part S_A are virtual, the concatenation rule stipulated in equation B.10 is easily understood.

1608 1609 1610 1611 1612 In order to prove that the concatenation of two optimal sequences found for the parts provided by decomposition of this example is an optimal sequence for the whole row, it is required that no term should be changed in the concatenated sequence for it to be optimal, and it is required to be able to calculate the optimal cost for the whole sequence from the optimal costs of the parts. 1613 Considering the first point, and considering two overlapping sequences such as S_A and S_B from our example. In an optimal choice for $C?_1$ and $C?_2$ within S_A , these choices only depend on the value of C_3 which is known. The same applies to choices for $C?_1$ and $C?_2$ within S_R . Thus, the optimal choices for $C?_1$ and $C?_2$ made in solving S_A are still valid for S_R . With similar reasoning, it follows that optimal choices for $C?_4$ and $C?_5$ made when solving S_B are still valid for S_R . Thus, provided that the concatenation rule stipulated in equation B.10 is applied, the optimal sequence for S_R can be calculated from its S_A and S_B parts. This reasoning extends straightforwardly to calculating the optimal sequence for a vine row using n row parts. Considering the second point, cost calculation, it can be done from the costs calculated for the parts.

$$\begin{aligned} c(S_A) &= open(C?_1) + Q_1(C?_1) + c(C?_1, C?_2) + Q_2(C?_2) + c(C?_2, C_3) \\ &\quad + Q_3(C_3) + close(C_3) \end{aligned} \quad (B.11)$$

$$\begin{aligned} c(S_B) &= open(C_3) + Q_3(C_3) + c(C_3, C?_4) + Q_4(C?_4) + c(C?_4, C?_5) \\ &\quad + +Q_5(C?_5) + close(C_5) \end{aligned} \quad (B.12)$$

1631 1632 1633 1634 The cost $c(S_R) = c(S_A \triangleright S_B)$ can be calculated from the S_R in a similar manner as in equations B.11 and B.12. Defining $corr(S_A \triangleright S_B)$ by equation B.13, this term can be easily calculated from equation B.14

$$c(S_R) = c(S_A \triangleright S_B) = c(S_A) + c(S_B) + corr(S_A \triangleright S_B) \quad (B.13)$$

$$corr(S_A \triangleright S_B) = -Q_3(C_3) - close(C_3) - open(C_3) \quad (B.14)$$

This cost correction easily extends to cost correction for the calculation of optimal cost of a row from optimal sequences on n row parts.

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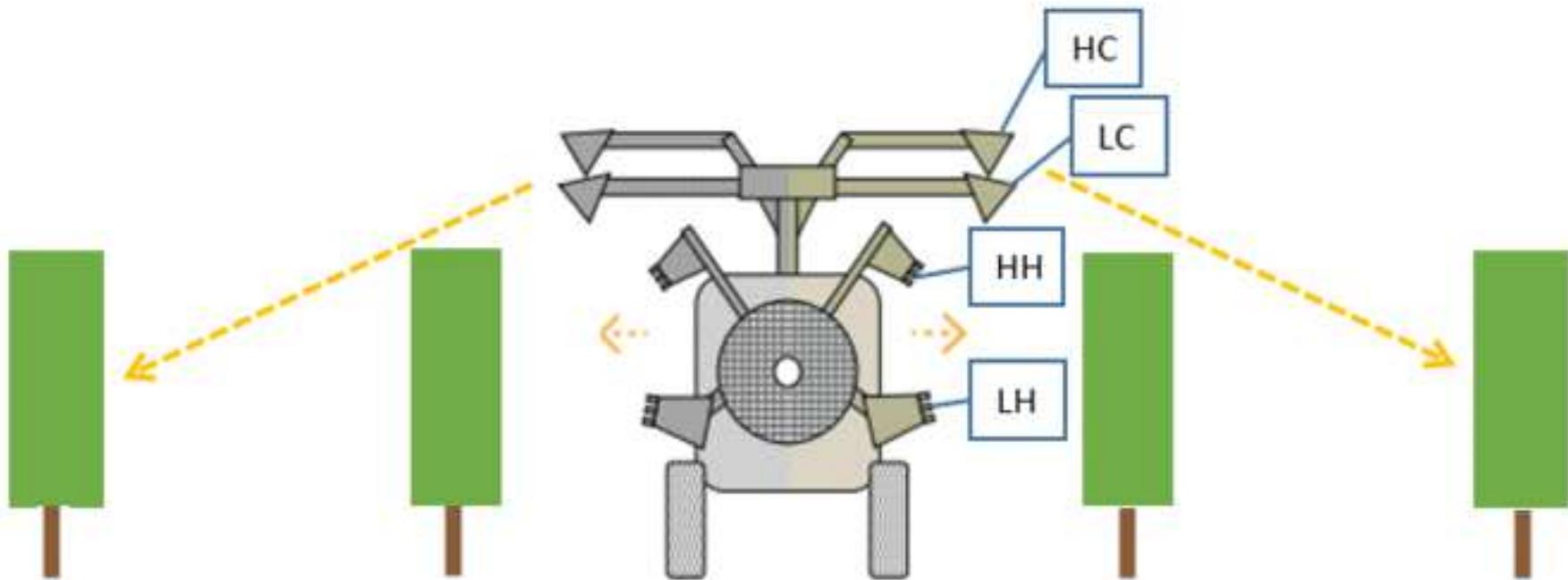
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vegetation states

spraying
configurations

Step 1

*Precision Spraying
Mapping (PSM)*

PSM: $(C_{best}, C_{alt}) = f(\text{vegetation})$

Lidar Data

Step 2

*spatialized
recommendation
map (SRM)*

list of blocks

Duration

C_{best}

C_{alt}

list of blocks

Duration

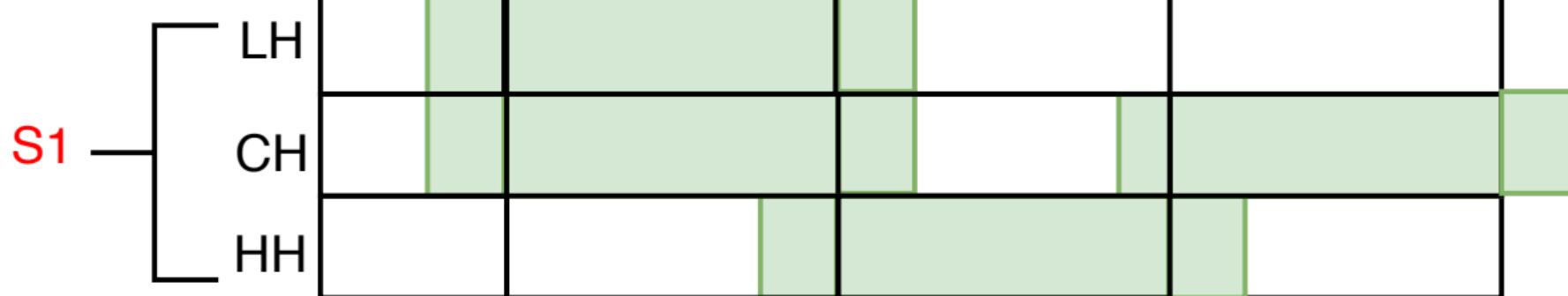
C_{opt}

Step 3

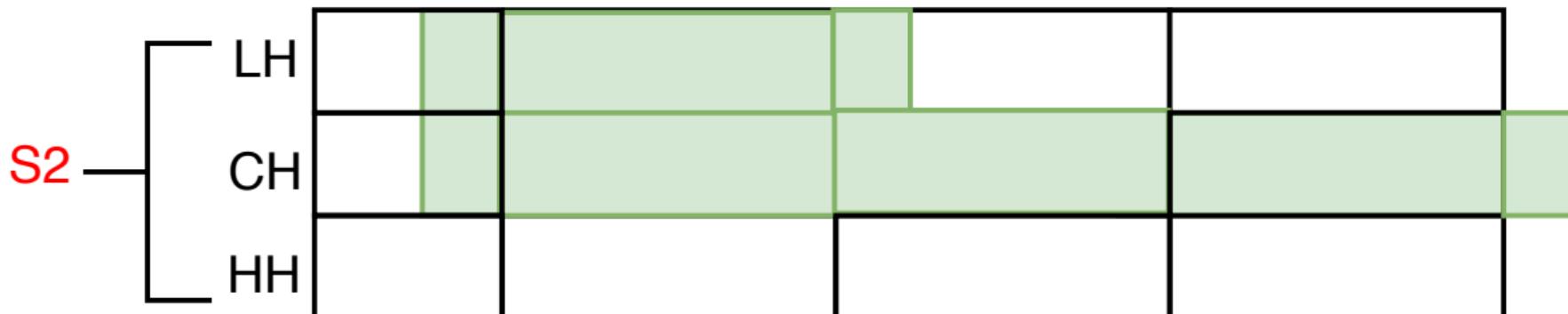
*spraying
command map*

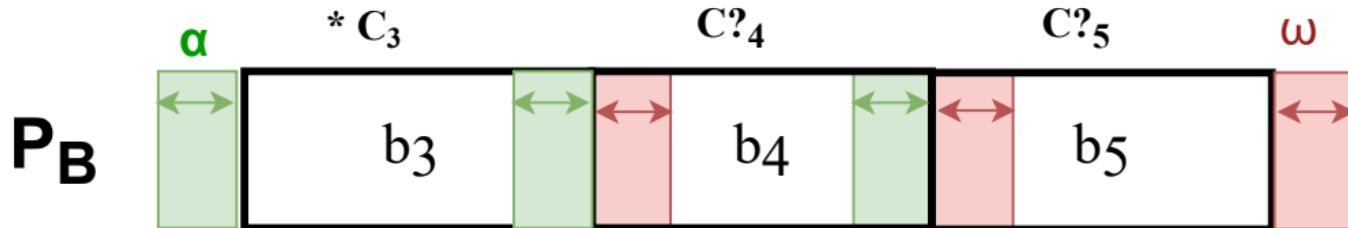
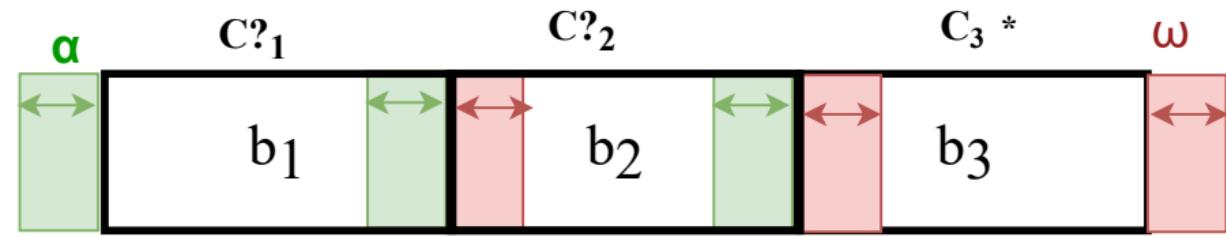
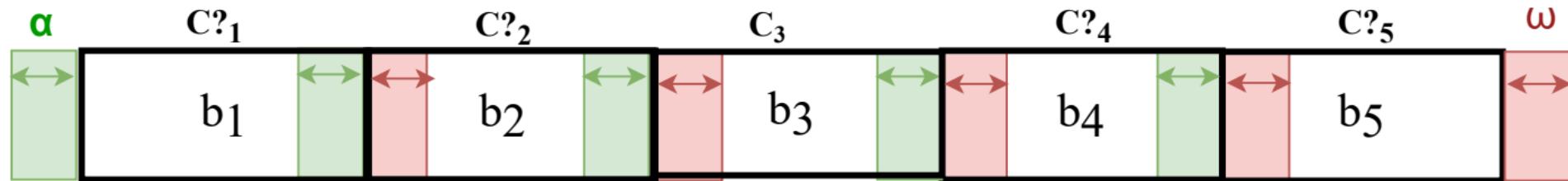
Interest of the alternative spray commands b_0 , $b_1 = 1022$, $b_2 = 1110$, $b_3 = 1111$

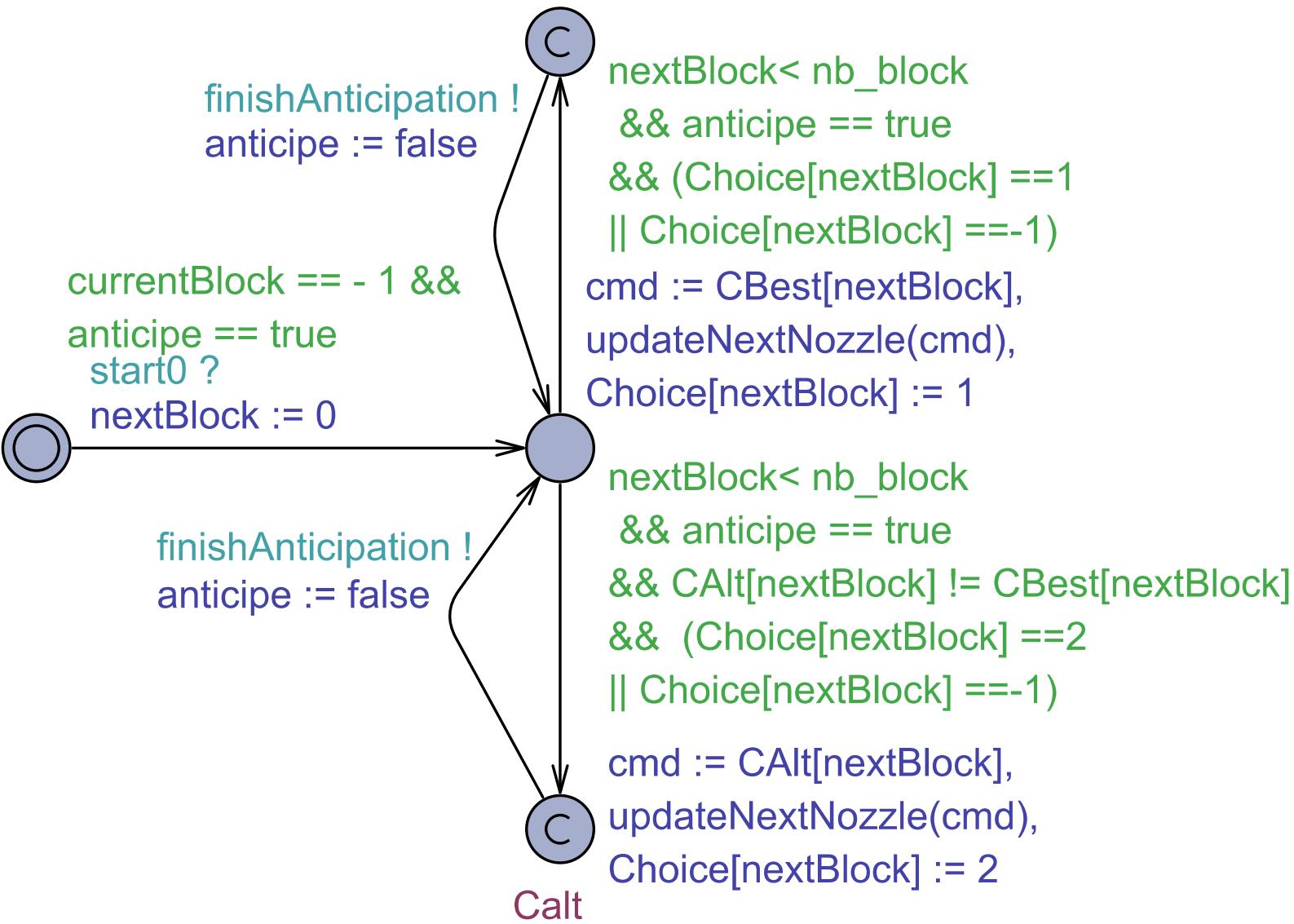
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b_0 , $b_1 = 1022$, $b_2 = 1110$, $b_3 = 1111$

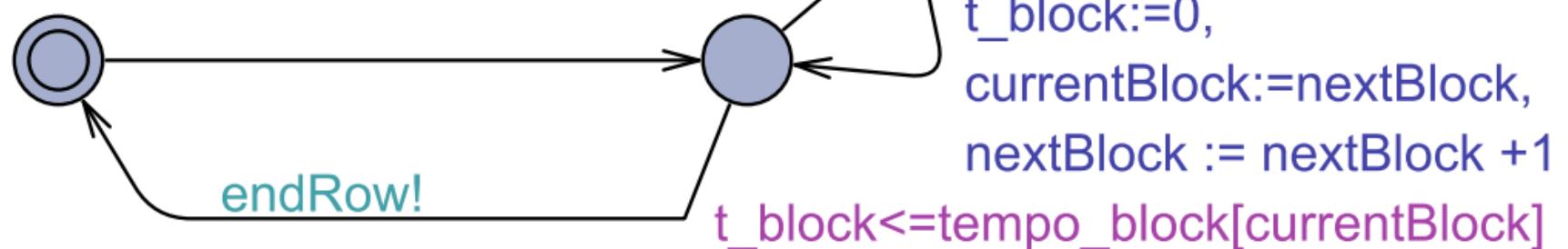


 Close




```
currentBlock:=nextBlock,  
nextBlock := nextBlock +1,  
t_block :=0,  
t_total :=0
```

Init

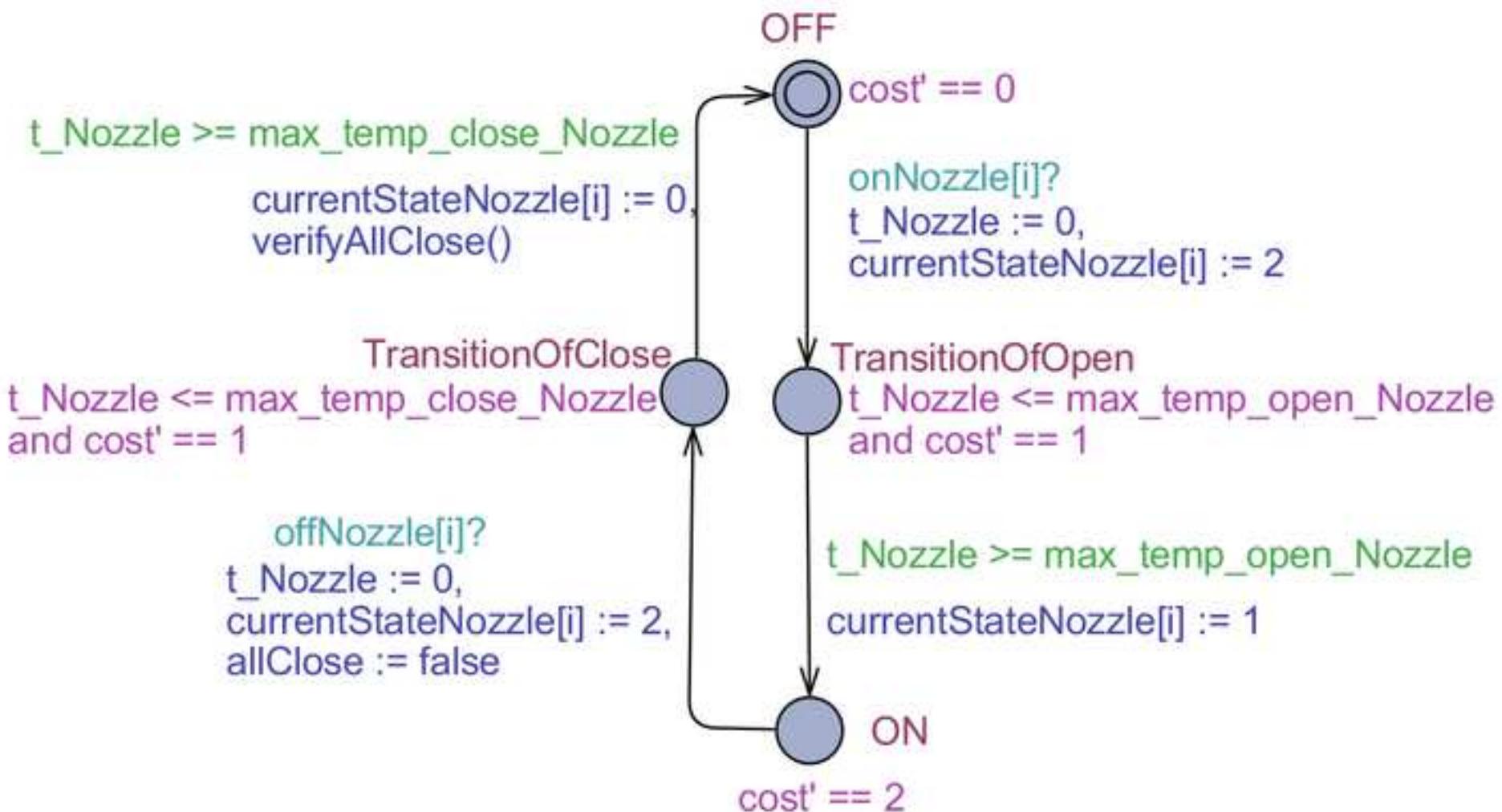


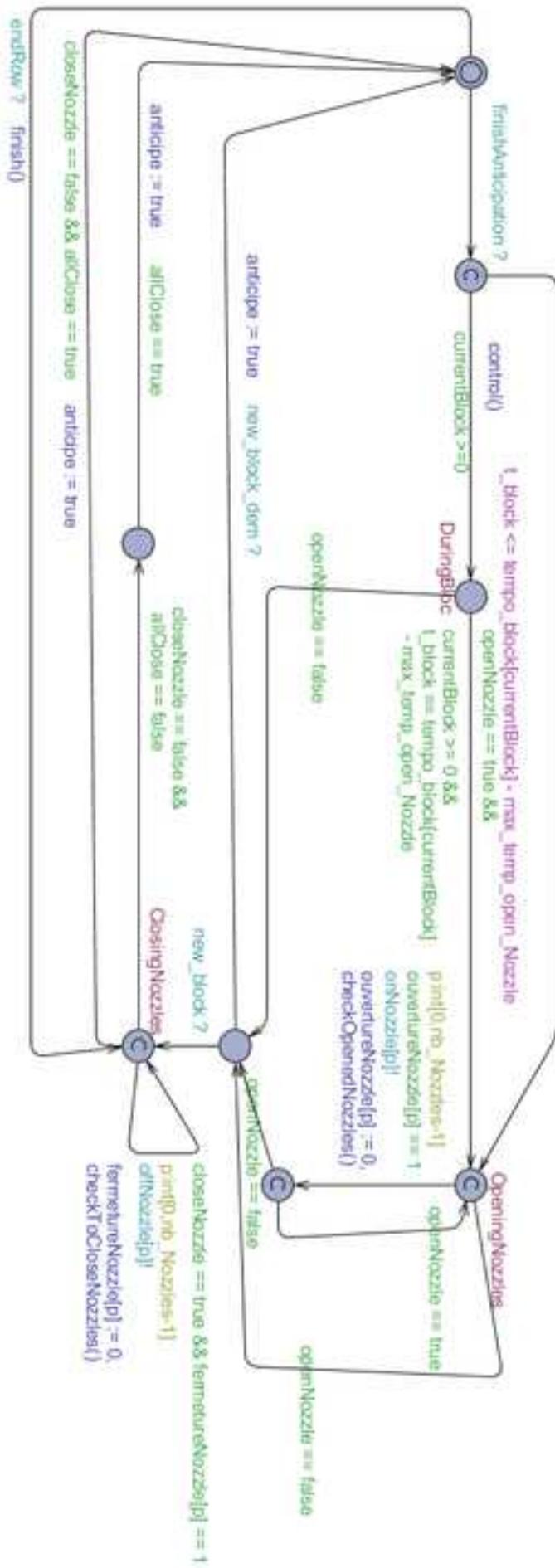
```
t_block==tempo_block[currentBlock] && currentBlock<nb_block - 1  
t_total := t_total + tempo_block[currentBlock],  
t_block:=0,
```

```
currentBlock:=nextBlock,  
nextBlock := nextBlock +1
```

```
t_block==tempo_block[currentBlock] && currentBlock==nb_block - 1
```

```
t_total := t_total + tempo_block[currentBlock]
```





Declaration of interests

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

The authors declare the following financial interests/personal relationships which may be considered as potential competing interests: