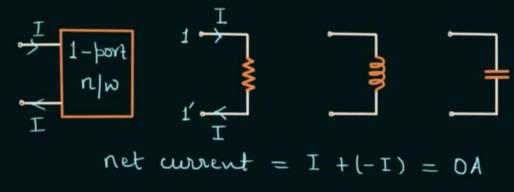
# Introduction to Two-Port Networks

2 7

**Port:** Pair of terminals through which a current may enter or leave the network.

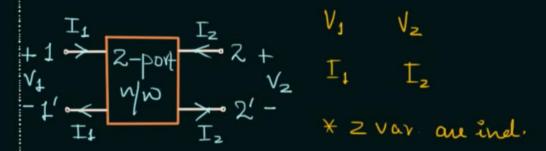
1-Port N/W: Two terminal devices such as R, L and C forms 1-port network.



>> Current entering from one terminal must leave from the other terminal.

the black box may also contain the dependent sources but never contain an

2-Port N/W: Two-port networks have two separate ports.



- >> Black box should consist only linear (bidirectional) and passive elements.
- >> Black box may contain energy storing elements. Land C
- >>> Black box may also contain dependent sources, but never contain an independent source.

# Z Parameters (or) Impedance Parameters (or) Spen ckt. porometer

$$I_1$$
 and  $I_2 \rightarrow ind$ .

$$V_1$$
 and  $V_2 \rightarrow dep$ .

$$\begin{pmatrix} V_1 \\ V_2 \end{pmatrix} = \pm \begin{pmatrix} I_1 \\ I_2 \end{pmatrix}$$

$$\begin{array}{c} I_1 \text{ and } I_2 \rightarrow \text{ind.} \\ V_1 \text{ and } V_2 \rightarrow \text{dep.} \end{array} \begin{pmatrix} V_1 \\ V_2 \end{pmatrix} = \begin{pmatrix} I_1 \\ I_2 \end{pmatrix} \text{ current } I_1 \\ \text{[I]} \text{ wat.} + \bullet \rightarrow \bullet \\ \text{[I]} \text{ V}_1 \end{array}$$

$$V_1 = Z_{11} I_1 + Z_{12} I_2 - I$$

$$V_{1} = Z_{11}I_{1} + Z_{12}I_{2} - 1$$

$$V_{2} = Z_{21}I_{1} + Z_{22}I_{2} - 2$$

$$\begin{bmatrix} V_{1} \\ V_{2} \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} \begin{bmatrix} I_{1} \\ I_{2} \end{bmatrix} \Rightarrow [V] = [Z][I]$$

Voltage mat. Impedance matrix 
$$V_1 - Z_{11}I_1 - Z_{12}I_2 = 0$$

$$V_2 - Z_{21}I_1 - Z_{22}I_2 = 0$$

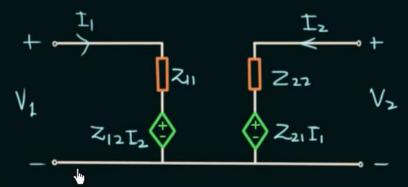
$$V_1 - Z_{11}I_1 - Z_{12}I_2 = 0$$
  
 $V_2 - Z_{21}I_1 - Z_{22}I_2 = 0$ 

$$Z_{11} = \frac{\sqrt{1}}{I_L} \Big|_{I_2 = 0}$$

 $Z_{11} = \frac{V_1}{I_1} |_{I_1=0}$  Open circuit driving pt. i/p imp.

$$Z_{21} = \frac{\sqrt{2}}{I_1} \Big|_{I_2 = 0}$$

 $Z_{21} = \frac{\sqrt{z}}{|I_1|} |I_{2}=0$  Open circuit forward tr. imp. (H.w.) - NESCACATENT=0 Open circuit rev. tr. imp.  $Z_{22}=?$ 



# Z-Parameters (Solved Problem 1)

Question: Find the Z-parameters of the below given two-port network.



$$\begin{bmatrix} \mathbf{Z} \end{bmatrix} = \begin{bmatrix} \mathbf{Z}_{11} & \mathbf{Z}_{12} \\ \mathbf{Z}_{21} & \mathbf{Z}_{22} \end{bmatrix}$$

$$\begin{bmatrix} z \end{bmatrix} = \begin{bmatrix} 6 & 4 \\ 4 & 10 \end{bmatrix}$$
 ans

Solution:

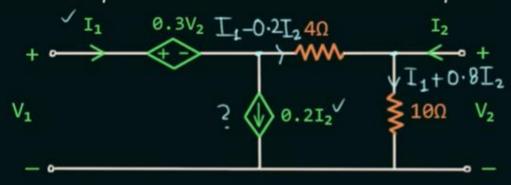
$$+V_1-2I_1-4(I_1+I_2)=0$$

$$+\sqrt{2}-6I_2-4(I_1+I_2)=0$$



# Z-Parameters (Solved Problem 2)

Question: The Z-parameter matrix of the two-port network as shown below is



$$\begin{bmatrix} Z \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix}$$

$$\begin{aligned} +V_{1} - 0.3V_{2} - 4(I_{1} - 0.2I_{2}) - \\ & 10(I_{1} + 0.8I_{2}) = 0 \\ V_{1} - 0.3\tilde{V}_{2} - 14I_{1} - 7.2I_{2} = 0 - \textcircled{1} \\ V_{1} - 0.3(10I_{1} + 8I_{2}) - 14I_{1} - 7.2I_{2} = 0 \\ V_{1} = 17I_{1} + 9.6I_{2} - \textcircled{3} \\ V_{1} = Z_{11}I_{1} + Z_{12}I_{2} \end{aligned}$$

$$+V_{2} - 10(I_{1} + 0.8I_{2}) = 0$$

$$V_{2} = 10I_{1} + 8I_{2} - 2$$

$$V_{2} = Z_{21}I_{1} + Z_{22}I_{2}$$



#### <u>Y-Parameters</u> (or) <u>Admittance Parameters</u>

$$V_{1} \text{ and } V_{2} \rightarrow \text{ind.}$$

$$I_{1} \text{ and } I_{2} \rightarrow \text{dep.}$$

$$I_{1} \text{ and } I_{2} \rightarrow \text{dep.}$$

$$I_{1} = Y_{11} V_{1} + Y_{12} V_{2} - \bigcirc$$

$$I_{2} = Y_{21} V_{1} + Y_{22} V_{2} - \bigcirc$$

$$I_{3} = Y_{21} V_{1} + Y_{22} V_{2} - \bigcirc$$

$$I_{4} = Y_{11} V_{1} + Y_{12} V_{2} - \bigcirc$$

$$I_{5} = Y_{11} V_{1} + Y_{22} V_{2} - \bigcirc$$

$$I_{7} = Y_{11} V_{1} + Y_{22} V_{2} - \bigcirc$$

$$I_{1} = X_{11} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{2} = X_{21} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{3} = X_{21} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{4} = X_{11} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{5} = X_{11} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{7} = X_{11} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{1} = X_{11} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{2} = X_{21} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{3} = X_{21} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{4} = X_{11} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{5} = X_{11} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{7} = X_{11} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{7} = X_{11} V_{1} + X_{22} V_{2} - \bigcirc$$

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$$I_{7} = X_{11} V_{1} + X_{22} V_{2} - \bigcirc$$

$$I_{7} = X_{11} V_{1} + X_{12} V_{2} - \bigcirc$$

$$I_{7} = X_{11} V_{1} + X_{12} V_{2} - \bigcirc$$

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$$I_{7} = X_{11} V_{1} + X_{12} V_{2} - \bigcirc$$

$$I_{7} = X_{11} V_{1} + X_{12} V_{2} - \bigcirc$$

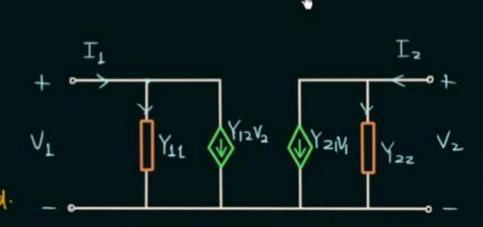
$$I_{7} = X_{11$$

$$Y_{11} = \frac{I_1}{V_1} \Big|_{V_2 = 0}$$
 Short Ckt. Driving Pt.  $V_1$  ad.

$$Y_{21} = \frac{I_2}{V_1} \Big|_{V_2=0}$$
 Short Ckt. for. tr. ad.

$$Y_{12} = \frac{I_1}{V_2} \Big|_{V_1 = 0}$$
 Short Ckt. Yev. tr. ad.

$$V_{22} = \frac{I_2}{V_2} |_{V_1 = 0}$$
 Short ckt. driving pt. 9/p ad.



### √ Y-Parameters to Z-Parameters Conversion

$$\checkmark$$
 [V] = [Z][I] and [I] = [Y][V]  $\Rightarrow$   $\checkmark$ [V] = [Y]<sup>-1</sup>[I]

$$[z] = [Y]^{-1}$$

$$\begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}^{-1}$$

$$= \frac{\text{adj}(Y)}{|Y|}$$

$$= \frac{|Y|}{|Y|}$$

$$= \frac{1}{|Y|} \begin{bmatrix} (-1)^{1/2} Y_{22} - Y_{21} \\ -Y_{12} & Y_{11} \end{bmatrix}_{2 \times 2}$$

$$\begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}^{-1} \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} = \frac{1}{|Y|} \begin{bmatrix} Y_{22} & -Y_{12} \\ -Y_{21} & Y_{11} \end{bmatrix}$$

$$Y_{11} \times Y_{22} - Y_{21} \times Y_{12}$$

$$J_{2} = -\frac{\gamma_{12}}{|\gamma|} \qquad Z_{22} = \frac{\gamma_{11}}{|\gamma|}$$

### Z-Parameters to Y-Parameters Conversion

$$\begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}_{2\chi^{2}} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix}_{2\chi^{2}}^{-1} \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} = \frac{1}{|Z|} \begin{bmatrix} Z_{22} & -Z_{12} \\ -Z_{21} & Z_{11} \end{bmatrix}^{T} \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} = \frac{1}{|Z|} \begin{bmatrix} Z_{22} & -Z_{12} \\ -Z_{21} & Z_{11} \end{bmatrix}^{T} \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} = \frac{1}{|Z|} \begin{bmatrix} Z_{22} & -Z_{21} \\ -Z_{12} & Z_{11} \end{bmatrix}^{T} \begin{bmatrix} Y_{12} & -\frac{Z_{12}}{|Z|} & Y_{22} & \frac{Z_{11}}{|Z|} \end{bmatrix}^{T} \begin{bmatrix} Y_{12} & -\frac{Z_{12}}{|Z|} & Y_{22} & \frac{Z_{11}}{|Z|} \end{bmatrix}^{T}$$

# <u>h-Parameters</u> (or) <u>Hybrid Parameters</u>

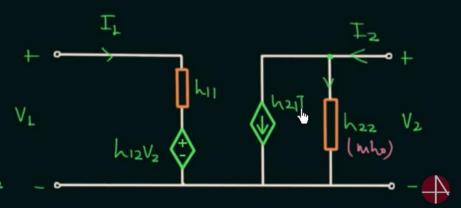
$$h_{11} = \frac{V_1}{I_1}|_{V_2=0}$$
 Short Okt. driving pt.  $\frac{1}{2}$ p imp.

\* 
$$h_{11} = \frac{1}{I_1/V_1|_{V_2=0}} \Rightarrow h_{11} = \frac{1}{1/Y_{11}}$$

$$h_{21} = \frac{I_2}{I_1} \Big|_{V_2 = 0}$$
 Short Ckt. for when gain

$$h_{12} = \frac{V_1}{V_2} \Big|_{I_1=0}$$
 Open Okt. rev. voltage gain.  $V_L$ 

$$h_{22} = \frac{I_2}{V_2/I_2} | I_1 = 0$$
NESO ACADE/N2/  $I_1 = 0$  (H.W.)  $* h_{22} = \frac{1}{V_2/I_2} | I_1 = 0$ 



#### h-Parameters to Z-Parameters Conversion

$$V_{1} = h_{11}^{\prime} I_{L} + h_{12}^{\prime} V_{2} - 0$$

$$I_{2} = h_{21}^{\prime} I_{1} + h_{22}^{\prime} V_{2} - 0$$

$$-h_{21}I_{1} + I_{2} = h_{22}V_{2}$$

$$V_{2} = -\frac{h_{21}}{h_{22}}I_{1} + \frac{1}{h_{22}}I_{2} - \boxed{0}$$

$$V_{1} = h_{11}I_{1} + h_{12}\left[\frac{-h_{21}}{h_{22}}I_{1} + \frac{1}{h_{22}}I_{2}\right]$$

$$V_{2} = h_{11}I_{1} + h_{12}\left[\frac{-h_{21}}{h_{22}}I_{1} + \frac{1}{h_{22}}I_{2}\right]$$

$$V_{L} = h_{11}I_{1} - \frac{h_{21}h_{12}}{h_{22}}I_{L} + \frac{h_{12}}{h_{22}}I_{2}$$

$$V_1 = Z_{11}I_1 + Z_{12}I_2 - 0$$

$$V_2 = Z_{21}I_1 + Z_{22}I_2 - 0$$

$$V_{1} = \left[ h_{11} - \frac{h_{21}h_{12}}{h_{22}} \right] I_{1} + \frac{h_{12}}{h_{22}} I_{2}$$

$$\frac{h_{11}h_{22} - h_{21}h_{12}}{h_{22}} = \frac{|H|}{h_{22}}$$

$$V_1 = \frac{1H1}{h_{22}}I_1 + \frac{h_{12}}{h_{22}}I_2 - (V)$$

$$Z_{11} = \frac{1H1}{h_{22}}$$
  $Z_{12} = \frac{h_{12}}{h_{22}}$   $Z \to h$   $Z_{11} = \frac{|Z|}{|Z|_{22}}$ 

$$Z_{12} = \frac{h_{12}}{h_{22}}$$

$$Z_{21} = -\frac{h_{21}}{h_{22}}$$

$$Z_{21} = -\frac{h_{21}}{h_{22}}$$
  $Z_{22} = \frac{1}{h_{22}}$   $h_{12} = \frac{Z_{12}}{Z_{22}}$   $h_{21} = -\frac{Z_{21}}{Z_{22}}$ 

h=2 = 1/2=2

#### h-Parameters to Y-Parameters Conversion

$$V_{1} = h_{11}I_{1} + h_{12}V_{2} - 0$$

$$I_{2} = h_{21}I_{1} + h_{22}V_{2} - 0$$

$$V_{1} - h_{12}V_{2} = h_{11}I_{1}$$

$$\Rightarrow I_{L} = \frac{1}{h_{11}}V_{1} - \frac{h_{12}}{h_{11}}V_{2} - 0$$

$$I_{1} \rightarrow 1 - I_{2} = h_{21} \left[ \frac{1}{h_{11}} V_{1} - \frac{h_{12}}{h_{11}} V_{2} \right] + h_{22} V_{2}$$

$$I_{2} = \frac{h_{21}}{h_{11}} V_{1} - \frac{h_{21} h_{12}}{h_{11}} V_{2} + h_{22} V_{2}$$

$$I_{1} = Y_{11}V_{1} + Y_{12}V_{2} - II$$

$$I_{2} = Y_{21}V_{1} + Y_{22}V_{2} - II$$

$$I_{2} = \frac{h_{21}}{h_{11}}V_{1} + \left[\begin{array}{c} h_{22} - \frac{h_{21}h_{12}}{h_{11}} \end{array}\right]V_{2}$$

$$\frac{h_{11}h_{22} - h_{21}h_{12}}{h_{11}} = \frac{|H|}{h_{11}}$$

$$I_{2} = \frac{h_{21}}{h_{11}}V_{1} + \frac{|H|}{h_{11}}V_{2} - II$$

$$Y_{11} = \frac{1}{h_{11}} \quad Y_{12} = -\frac{h_{12}}{h_{11}} \quad Y \rightarrow h$$

$$Y_{21} = \frac{h_{21}}{h_{11}} \quad Y_{22} = \frac{|H|}{h_{11}} \quad h_{12} = -Y_{12}/Y_{11}$$

$$h_{21} = Y_{21}/Y_{11}$$

$$h_{22} = |Y_{11}/Y_{11}|$$

# √9-Parameters (or) Inverse Hybrid Parameters

$$V_1$$
 and  $I_2 \rightarrow ind$ 

$$I_1$$
 and  $V_2 \rightarrow dep$ .

$$V_1$$
 and  $I_2 \rightarrow ind$ .  
 $I_1$  and  $V_2 \rightarrow dep$ .
$$\begin{pmatrix} I_1 \\ V_2 \end{pmatrix} = f \begin{pmatrix} V_1 \\ \overline{I}_2 \end{pmatrix}$$

$$I_1 = g_{11} v_1 + g_{12} I_2 \stackrel{KCL}{\longrightarrow} 0$$

$$\begin{split} & I_1 \quad \text{and} \quad V_2 \rightarrow \text{dep.} \\ & I_1 = \underbrace{g_{11}}_{V_1} V_1 + \underbrace{g_{12}}_{I_2} \underbrace{I_2}_{I_2} \underbrace{KCL}_{I_1} \\ & V_2 = \underbrace{g_{21}}_{V_1} V_1 + \underbrace{g_{22}}_{I_2} \underbrace{I_2}_{I_2} \underbrace{KVL}_{I_1} \underbrace{I_2}_{I_2} \\ \end{split}$$

$$\begin{array}{c|c}
 & I_1 \\
 & \downarrow \\
 & \downarrow$$

$$g_{11} = \frac{\Gamma_1}{V_1}\Big|_{\Gamma_2 = 0}$$

 $g_{11} = \frac{\Gamma_1}{V_1}\Big|_{\Gamma_2=0}$  Open clet. dr. þt. i/p ad.

$$g_{11} = \frac{1}{V_{1}/L_{1}} \Rightarrow g_{11} = \frac{1}{Z_{11}}$$

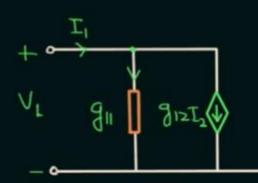
$$g_{21} = \frac{V_2}{V_1} |_{I_2 = 0}$$

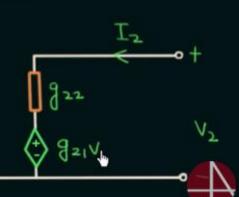
 $g_{21} = \frac{V_2}{V_1} \Big|_{I_2=0}$  Open clet. for. vol. gain

$$g_{12} = \frac{I_1}{I_2} \Big|_{V_1 = 0}$$

 $g_{12} = \frac{L_1}{T_2} \Big|_{V_1=0}$  Short Ckt. Lev. Cur. gain

$$g_{22} = \frac{V_z}{I_z} |_{V_1=0}$$
 Short ckt. dr. pt. 0/2  
\*  $g_{22} = \frac{1}{I_z/V_z}|_{V_1=0} \Rightarrow g_{22} = \frac{1}{V_{22}}$ 





[A]

$$g_{11} = \frac{\Gamma_1}{V_1} \Big|_{\Gamma_2 = 0}$$

 $g_{11} = \frac{\Gamma_1}{V_1} \Big|_{\Gamma_2=0}$  Open clet. dr. pt. i/p ad.

$$\star g_{11} = \frac{1}{V_{1}/I_{1}} \Rightarrow g_{11} = \frac{1}{Z_{11}}$$

$$g_{21} = \frac{V_2}{V_1} \Big|_{I_2=0}$$
 Open clet. for. vol. gain

$$g_{12} = \frac{I_1}{I_2} \Big|_{V_1 = 0}$$

 $\rightarrow$  [A] = [&][B]

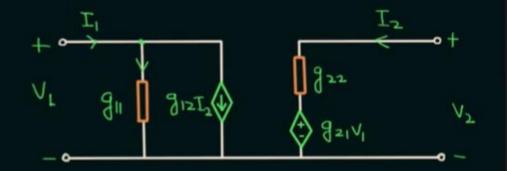
 $g_{12} = \frac{L_1}{T_2} \Big|_{V_1 = D}$  Short Ckt. Nev. au gain

$$[A] = [G][B]$$

$$\Rightarrow [G] = [H]^{-1}$$

$$[B] = [H][A] \Rightarrow [A] = [H]^{-1}[B] \Rightarrow [H] = [G]^{-1}$$

$$g_{22} = \frac{V_2}{I_2} |_{V_1=0}$$
 Short det. dr. pt. 0/2  
\*  $g_{22} = \frac{1}{I_2/V_2} |_{V_1=0} \Rightarrow g_{22} = \frac{1}{Y_{22}}$ 



$$h \rightarrow g : g_{11} = h_{22}/IHI$$
  $g_{12} = -h_{12}/IHI$ 
 $g_{21} = -h_{22}/IHI$   $g_{22} = h_{11}/IHI$ 

$$g \rightarrow h : h_{11} = \frac{922}{161} \cdot h_{12} = -\frac{912}{161} \cdot h_{22} = \frac{912}{161} \cdot h_{22} = \frac{912}{161} \cdot h_{23} =$$

# VZ-Parameters to g-Parameters Conversion

$$V_{1} = Z_{11} \overline{I}_{1} + Z_{12} \overline{I}_{2} - 0$$

$$V_{2} = Z_{21} \overline{I}_{1} + Z_{22} \overline{I}_{2} - 0$$

$$V_{3} = Z_{21} \overline{I}_{1} + Z_{22} \overline{I}_{2} - 0$$

$$V_{4} = Z_{21} \overline{I}_{1} + Z_{22} \overline{I}_{2} - 0$$

$$V_{5} = Z_{21} \overline{I}_{1} + Z_{22} \overline{I}_{2} - 0$$

$$V_{7} - Z_{12} \overline{I}_{2} = Z_{11} \overline{I}_{1}$$

$$\Rightarrow \overline{I}_{1} = \frac{1}{Z_{11}} V_{1} - \frac{Z_{12}}{Z_{11}} \overline{I}_{2} - 0$$

$$V_{2} = \frac{Z_{21}}{Z_{11}} V_{1} + \frac{|Z|}{|Z|} \overline{I}_{2} - 0$$

$$V_{5} = Z_{5} \overline{I}_{1} = 0$$

$$V_{7} = Z_{5} \overline{I}_{1} = 0$$

$$V_{8} = Z_{11} \overline{I}_{1} - \overline{I}_{11} = 0$$

$$V_{8} = Z_{11} \overline{I}_{1} - \overline{I}_{11} = 0$$

$$V_{8} = Z_{11} \overline{I}_{1} - \overline{I}_{11} = 0$$

$$V_{11} = \overline{I}_{11} - \overline{I}_{11} = 0$$

$$V_{2} = \overline{I}_{21} \overline{I}_{11} - \overline{I}_{21} = 0$$

$$V_{3} = \overline{I}_{11} = \overline{I}_{11} - \overline{I}_{12} = 0$$

$$V_{5} = \overline{I}_{11} = \overline{I}_{11} - \overline{I}_{12} = 0$$

$$V_{7} = \overline{I}_{11} = \overline{I}_{11} - \overline{I}_{12} = 0$$

$$V_{8} = \overline{I}_{11} = \overline{I}_{11} - \overline{I}_{12} = 0$$

$$V_{11} = \overline{I}_{11} - \overline{I}_{12} = 0$$

$$V_{11} = \overline{I}_{12} - \overline{I}_{12} = \overline{I}_{12} = 0$$

$$V_{11} = \overline{I}_{12} - \overline{I}_{12} = \overline{I}_{12} = 0$$

$$V_{11} = \overline{I}_{12} - \overline{I}_{12} = \overline{I}_{12} = 0$$

$$V_{11} = \overline{I}_{12} - \overline{I}_{12} = \overline{I}_{12} = 0$$

$$V_{11} = \overline{I}_{12} - \overline{I}_{12} = \overline{I}_{12} = \overline{I}_{12} = 0$$

$$V_{11} = \overline{I}_{12} - \overline{I}_{12} = \overline{I}_{12} = \overline{I}_{12} = 0$$

$$V_{11} = \overline{I}_{12} - \overline{I}_{12} = \overline{I}_{12} = \overline{I}_{12} = 0$$

$$\overline{I}_{11} = \overline{I}_{12} - \overline{I}_{12} = \overline{I}_{12} = \overline{I}_{12} = 0$$

$$\overline{I}_{11} = \overline{I}_{12} - \overline{I}_{12} = \overline{I}_{12} = \overline{I}_{12} = 0$$

$$\overline{I}_{11} = \overline{I}_{12} - \overline{I}_{12} = \overline$$



### ABCD-Parameters (or) Transmission Parameters

>> Also known as T-Parameters, Cascade Parameters and Chain Parameters.

$$V_s = V_1$$
,  $I_s = I_1$ ,  $V_r = V_2$ ,  $I_r = -\tilde{I}_2$ 

$$V_r$$
 and  $I_r \rightarrow ind$ .

$$I_s = CV_r + DI_r$$

$$V_1 = AV_2 + B(-I_2)$$
 ——①

$$I_L = CV_2 + D(-I_2) - 0$$

$$\binom{I^{2}}{\sqrt{2}} = f\binom{I^{A}}{\sqrt{A}}$$

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$

I.T.P.

(01) abcd par.

$$V_s = AV_r + BI_r$$

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix} \quad A = \frac{V_1}{V_2} \Big|_{I_2 = 0} \quad \text{Open ckt. Tev. vol. gain}$$

$$C = \frac{I_1}{V_2} \Big|_{I_2=0}$$
 Open clet. They. tr.

$$B = \frac{V_1}{-I_2} \Big|_{V_2=0} \text{ Short Ckt yev. tr.}$$

$$D = \frac{I_1}{-I_2} \Big|_{V_2 = 0}$$

D = II Short act yeur Short act yeur

# ✓ ABCD-Parameters to Z-Parameters Conversion

$$V_{1} = AV_{2} - BI_{2} - 0$$

$$I_{1} = CV_{2} - DI_{2} - 0$$

$$I_1 + DI_2 = CV_2$$

$$\Rightarrow$$
  $V_2 = \frac{1}{6}I_1 + \frac{D}{6}I_2 - 0$ 

$$V_{L} = A \left[ \frac{1}{C} I_{L} + \frac{D}{C} I_{2} \right] - B I_{2}$$

$$V_L = \frac{A}{C}I_1 + \frac{AD}{C}I_2 - BI_2$$

$$V_{L} = \frac{A}{C}I_{L} + \left[\frac{AD}{C} - B\right]I_{2}$$

$$V_{1} = Z_{11} \check{I}_{1} + Z_{12} \check{I}_{2} - 0$$

$$V_{2} = Z_{21} \check{I}_{1} + Z_{22} \check{I}_{2} - 0$$

$$\frac{AD}{C} - B = \frac{AD - BC}{C} = \frac{|T|}{C}$$

$$V_1 = \frac{A}{c}I_1 + \frac{|T|}{c}I_2 - W$$

$$Z_{II} = \frac{A}{c}$$

$$Z_{21}=\frac{1}{c}$$

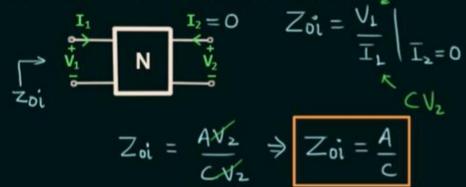
$$A = \frac{Z_{11}}{Z_{21}}$$

$$B = \frac{|Z|}{|Z|}$$

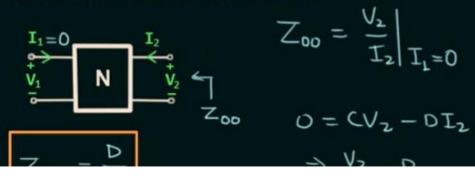
# Open Circuit & Short Circuit Impedances (in terms of ABCD-Parameters)

$$V_1 = AV_2 - BI_2 - 0$$

1) Open Circuit i/p Impedance: AV2

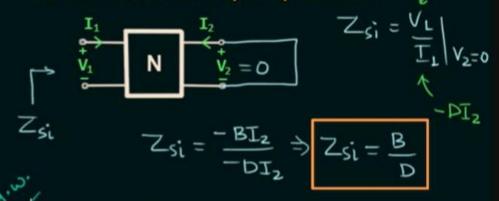


2) Open Circuit o/p Impedance:



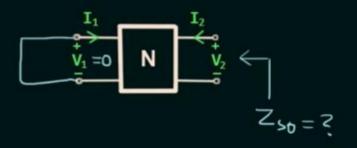
$$V_1 = AV_2 - BI_2 - 0$$
  $I_1 = CV_2 - DI_2 - 0$ 

3) Short Circuit i/p Impedance:



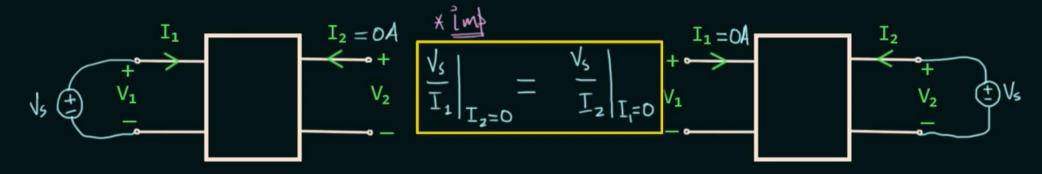
-BI

4) Short Circuit o/p Impedance:



## Concept of Symmetry in Two-Port Networks

>> A two-port network is said to be symmetrical if the ratio of excitation to response remains the same at both the ports independently w.r.t. the defined circuit conditions such as open circuit or short circuit.



Note: For small independent networks we can identify the symmetry using the mirror image





# Condition for Symmetry in Two-Port Networks

>> Condition for Symmetry:

$$\frac{V_s}{I_1}\Big|_{I_2=0} = \frac{V_s}{I_2}\Big|_{I_1=0}$$

 $Z_{11} = \frac{Y_{22}}{|Y|}$   $\Rightarrow \frac{Y_{22}}{|Y|} = \frac{Y_{11}}{|Y|} \Rightarrow Y_{11} = Y_{22}$   $Z_{22} = \frac{Y_{11}}{|Y|}$ 

>> In terms of Z-Parameters:

$$V_1 = Z_{11}I_1 + Z_{12}I_2 - 0$$

$$V_1 = V_s$$
 and  $I_2 = 0$ 

$$V_5 = Z_{11}I_1 \Rightarrow \frac{V_5}{I_1}|_{I_2=0} = Z_{11}$$

$$V_2 = V_5$$
 and  $I_1 = 0$ 

$$Z_{11} = Z_{22}$$

$$Z_{22} = \frac{|G|}{g_{11}}$$

$$\Rightarrow \ln \text{ terms}$$

$$V_5 = Z_{22}I_2 \Rightarrow \frac{V_5}{I_2}|_{I_1=0} = Z_{21}$$

>> In terms of h-Parameters:

>> In terms of Y-Parameters:

$$Z_{11} = \underbrace{|H|}_{h_{22}} \Rightarrow \underbrace{\frac{|H|}{h_{22}}} = \frac{1}{h_{22}} \Rightarrow |H| = 1$$

$$Z_{22} = \frac{1}{h_{22}}$$

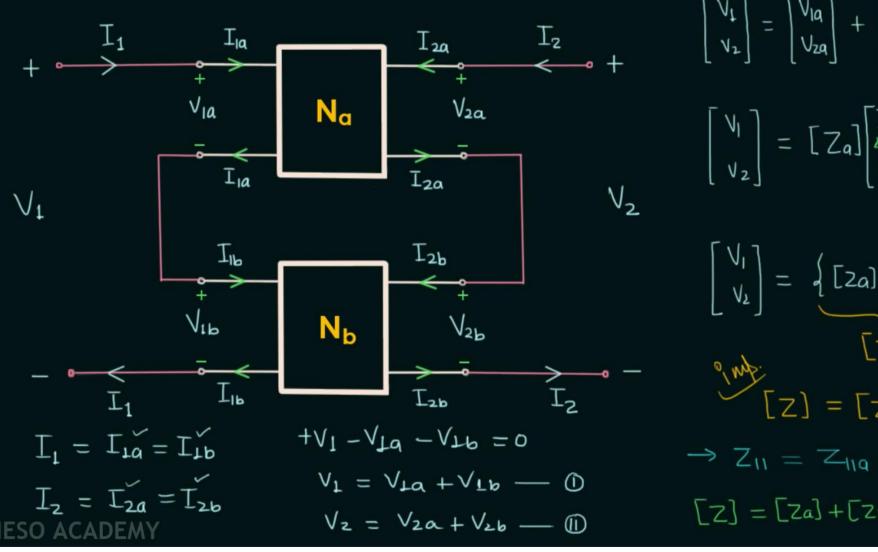
>> In terms of g-Parameters:

$$Z_{11} = \frac{1}{9} \frac{1}{911}$$
  $\Rightarrow \frac{1}{911} = \frac{|G_1|}{911} \Rightarrow |G_1| = 1$ 
 $Z_{22} = \frac{|G_1|}{911} \Rightarrow \frac{1}{911} = \frac{|G_2|}{911} \Rightarrow |G_1| = 1$ 

>> In terms of ABCD-Parameters:

$$Z_{II} = A/c$$
  $Z_{ZZ} = P/c$   $\Rightarrow \frac{A}{C} = \frac{D}{C} \Rightarrow A = D$ 

### Series-Series Interconnection



$$\begin{bmatrix} V_{1} \\ V_{2} \end{bmatrix} = \begin{bmatrix} V_{10} \\ V_{20} \end{bmatrix} + \begin{bmatrix} V_{10} \\ V_{20} \end{bmatrix}$$

$$\begin{bmatrix} V_{1} \\ V_{2} \end{bmatrix} = \begin{bmatrix} Z_{0} \end{bmatrix} \begin{bmatrix} I_{10} \\ I_{20} \\ I_{2} \end{bmatrix} + \begin{bmatrix} Z_{0} \end{bmatrix} \begin{bmatrix} I_{10} \\ I_{20} \\ I_{2} \end{bmatrix}$$

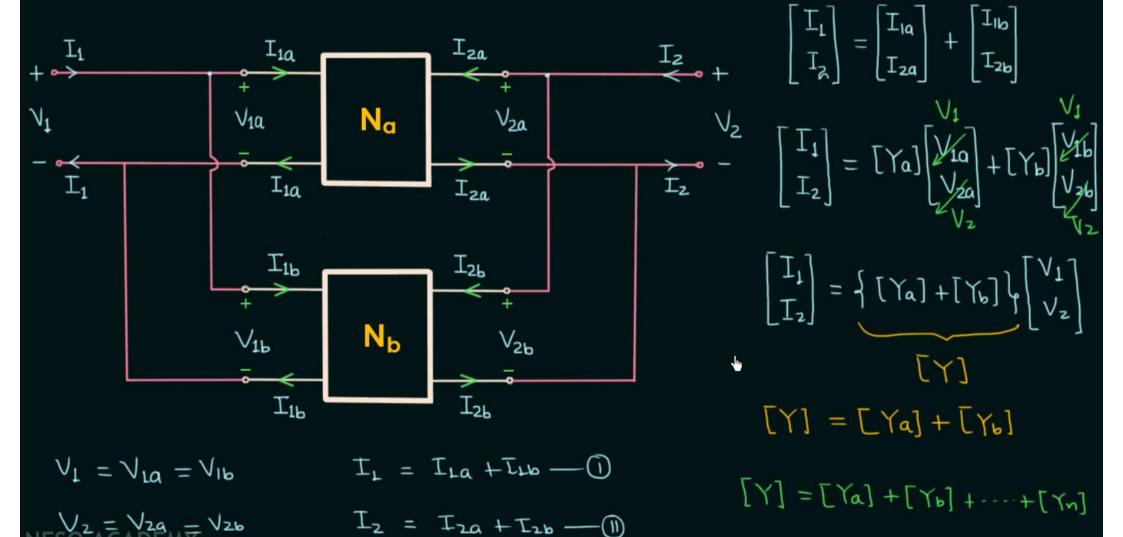
$$\begin{bmatrix} V_{1} \\ V_{2} \end{bmatrix} = \begin{bmatrix} Z_{0} \end{bmatrix} + \begin{bmatrix} Z_{0} \end{bmatrix} + \begin{bmatrix} Z_{0} \end{bmatrix} \begin{bmatrix} I_{1} \\ I_{2} \end{bmatrix}$$

$$\begin{bmatrix} Z \end{bmatrix} = \begin{bmatrix} Z_{0} \end{bmatrix} + \begin{bmatrix} Z_{0} \end{bmatrix} + \begin{bmatrix} Z_{0} \end{bmatrix}$$

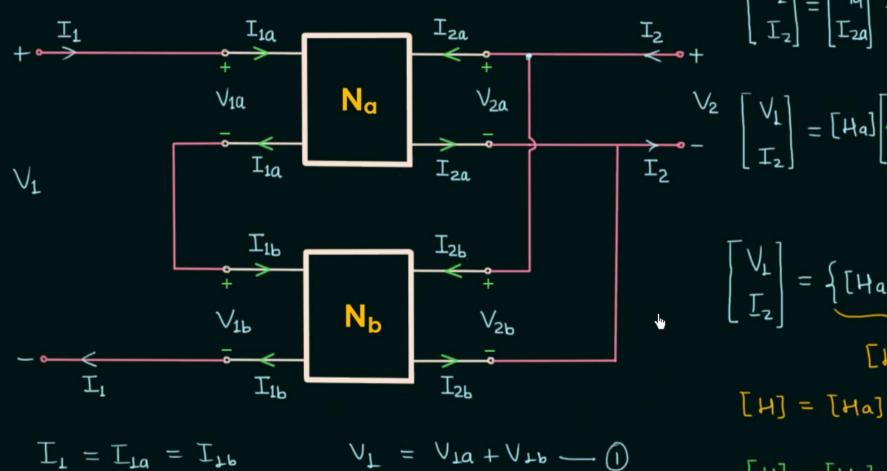
$$\Rightarrow Z_{11} = Z_{110} + Z_{110}$$

$$\begin{bmatrix} Z \end{bmatrix} = \begin{bmatrix} Z_{0} \end{bmatrix} + \begin{bmatrix} Z_{0} \end{bmatrix} + \cdots + \begin{bmatrix} Z_{0} \end{bmatrix}$$

## Parallel-Parallel Interconnection



### Series-Parallel Interconnection



 $I_z = I_{za} + I_{zb} - 0$ 

Vz = Vza = Vzb

$$I_{2} = \begin{bmatrix} V_{1} \\ I_{2} \end{bmatrix} = \begin{bmatrix} V_{1} \\ I_{2b} \end{bmatrix} + \begin{bmatrix} V_{1b} \\ I_{2b} \end{bmatrix}$$

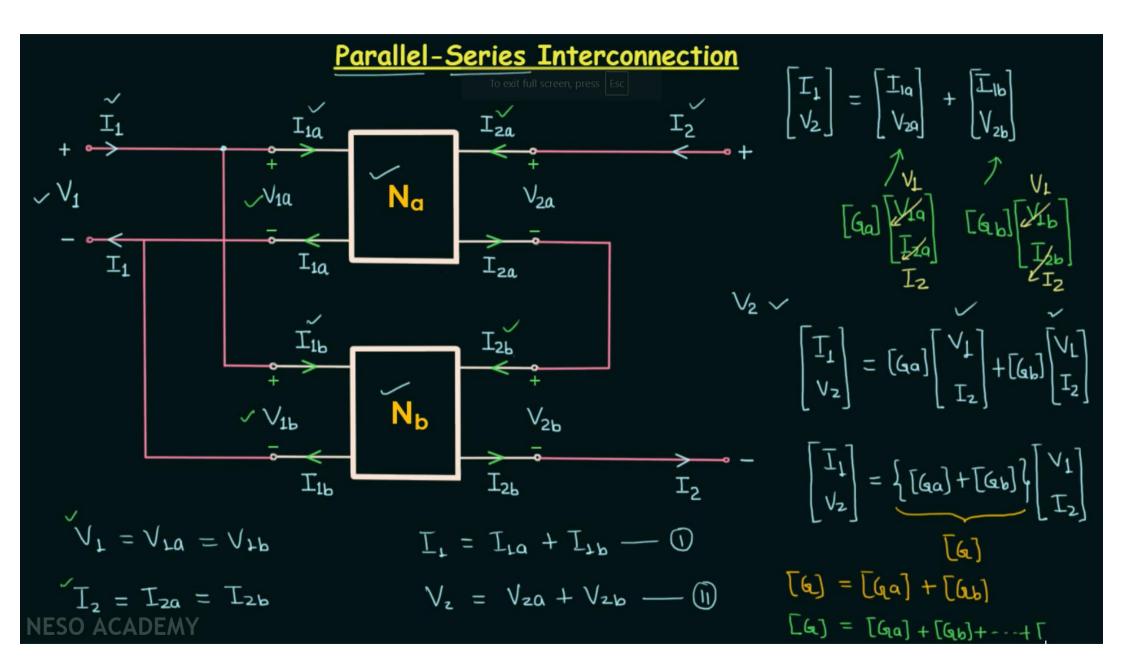
$$V_{2} = \begin{bmatrix} V_{1} \\ I_{2} \end{bmatrix} = \begin{bmatrix} H_{1} \end{bmatrix} \begin{bmatrix} I_{1a} \\ V_{2a} \end{bmatrix} + \begin{bmatrix} H_{1b} \end{bmatrix} \begin{bmatrix} I_{1b} \\ V_{2b} \end{bmatrix}$$

$$V_{2} = \begin{bmatrix} V_{1} \\ I_{2} \end{bmatrix} = \begin{bmatrix} H_{1a} \\ I_{2b} \end{bmatrix} + \begin{bmatrix} H_{1b} \\ I_{2b} \end{bmatrix} \begin{bmatrix} I_{1b} \\ I_{2b} \end{bmatrix}$$

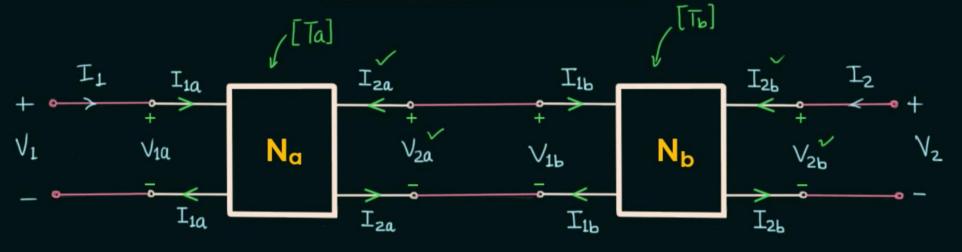
$$I_{1a} = I_{1a} + I_{1b}$$

$$I_{1b} = I_{1b} + I_{1b} = I_{1b}$$

$$I_{1b} = I_{1b} + I_{1b} = I_{1b} = I_{1b} + I_{1b} = I_{1$$







$$V_L = V_{LQ}$$
,  $I_L = I_{LQ}$ ,  $V_{2Q} = V_{Lb}$ ,  $I_{2Q} = -I_{Lb}$ ,  $V_{2b} = V_2$  and  $I_{2b} = I_2$ 

$$\begin{bmatrix} V_{1} \\ I_{1} \end{bmatrix} = \begin{bmatrix} V_{10} \\ I_{10} \end{bmatrix}$$

$$\begin{bmatrix} V_{1} \\ I_{1} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \begin{bmatrix} V_{20} \\ -I_{20} \end{bmatrix}$$
SO ACADEMY

$$\begin{bmatrix} V_{1} \\ I_{1} \end{bmatrix} = \begin{bmatrix} T_{a} \end{bmatrix} \begin{bmatrix} V_{1b} \\ I_{1b} \end{bmatrix}$$

$$\begin{bmatrix} V_{1} \\ I_{1} \end{bmatrix} = \begin{bmatrix} T_{a} \end{bmatrix} \begin{bmatrix} T_{b} \end{bmatrix} \begin{bmatrix} V_{2b} \\ -I_{2b} \end{bmatrix}$$

$$\uparrow \qquad \qquad -I_{2}$$

$$\begin{bmatrix} V_{1} \\ I_{1} \end{bmatrix} = \begin{bmatrix} V_{10} \\ I_{10} \end{bmatrix} \qquad \begin{bmatrix} V_{1} \\ I_{1} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \begin{bmatrix} V_{1b} \\ I_{1b} \end{bmatrix} \qquad \begin{bmatrix} V_{1} \\ I_{1} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \times \begin{bmatrix} V_{2} \\ I_{2} \end{bmatrix}$$

$$\begin{bmatrix} V_{1} \\ I_{1} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \begin{bmatrix} V_{1b} \\ I_{1b} \end{bmatrix} \qquad \begin{bmatrix} V_{1} \\ I_{1} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \times \begin{bmatrix} T_{0} \end{bmatrix} \times \begin{bmatrix} T_{0} \\ I_{2b} \end{bmatrix} \qquad \begin{bmatrix} T_{0} \\ I_{1b} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \times \begin{bmatrix} T_{0} \\ I_{1b} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \times \begin{bmatrix} T_{0} \\ I_{1b} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \times \begin{bmatrix} T_{0} \\ I_{2b} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \times \begin{bmatrix} T_{0} \\ I_{2b} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \times \begin{bmatrix} T_{0} \\ I_{2b} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \times \begin{bmatrix} T_{0} \\ I_{2b} \end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \times \begin{bmatrix} T_{0} \\ I_{2b} 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\end{bmatrix} = \begin{bmatrix} T_{0} \end{bmatrix} \times \begin{bmatrix} T_{0} \end{bmatrix}$$

### Bartlett's Bisection Theorem

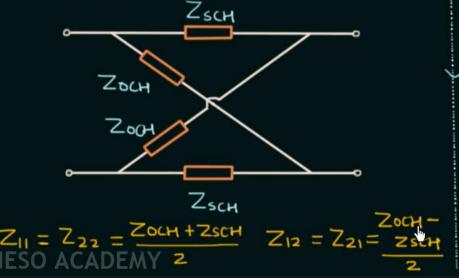
Z-bar.

>> Albert Charles Bartlett

lattice N/w? Shunt el.?

- >> Applicable to symmetrical two-port networks
- >> Basic symmetrical lattice

**Step 3:** Construct basic symmetrical lattice using Zoch & Zsch.



Step 1: Separate the n/w into two equal parts.



Step 2: Bisect and find out Zoch & Zsch.

