

# Drell-Yan cross section in TMD factorisation

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## 1 Structure of the observables

Let us start from Eq. (2.6) of Ref. [1], that is the fully differential cross section for lepton-pair production in the region in which the TMD factorisation applies, *i.e.*  $q_T \ll Q$ . After some minor manipulations, it reads:

$$\frac{d\sigma}{dQdydq_T} = \frac{16\pi\alpha^2 q_T}{9Q^3} H(Q, \mu) \sum_q C_q(Q) \int \frac{d^2\mathbf{b}}{4\pi} e^{i\mathbf{b}\cdot\mathbf{q}_T} \bar{F}_q(x_1, \mathbf{b}; \mu, \zeta) \bar{F}_{\bar{q}}(x_2, \mathbf{b}; \mu, \zeta), \quad (1)$$

where  $Q$ ,  $y$ , and  $q_T$  are the invariant mass, the rapidity, and the transverse momentum of the lepton pair, respectively, while  $\alpha$  is the electromagnetic coupling,  $H$  is the appropriate QCD hard factor

that can be perturbatively computed, and  $C_q$  are the effective electroweak charges. In addition, the variables  $x_1$  and  $x_2$  are functions of  $Q$  and  $y$  and are given by:

$$x_{1,2} = \frac{Q}{\sqrt{s}} e^{\pm y}, \quad (2)$$

being  $\sqrt{s}$  the centre-of-mass energy of the collision. In Eq. (1) we are using the short-hand notation:

$$\overline{F}_q(x, \mathbf{b}; \mu, \zeta) \equiv x F_q(x, \mathbf{b}; \mu, \zeta), \quad (3)$$

that is convenient for the implementation. The scales  $\mu$  and  $\zeta$  are introduced as a consequence of the removal of UV and rapidity divergences in the definition of the TMDs. Despite these scales are arbitrary scales, they are typically chosen  $\mu = \sqrt{\zeta} = Q$ . Therefore, for all practical purposes their presence is fictitious.

The computation-intensive part of Eq.(1) has the form of the integral:

$$I_{ij}(x_1, x_2, q_T; \mu, \zeta) = \int \frac{d^2 \mathbf{b}}{4\pi} e^{i \mathbf{b} \cdot \mathbf{q}_T} \overline{F}_i(x_1, \mathbf{b}; \mu, \zeta) \overline{F}_j(x_2, \mathbf{b}; \mu, \zeta). \quad (4)$$

where  $\overline{F}_{i(j)}$  are combinations of evolved TMD PDFs. At this stage, for convenience,  $i$  and  $j$  do not coincide with  $q$  and  $\bar{q}$  but they are linked through a simple linear transformation. The integral over the bidimensional impact parameter  $\mathbf{b}$  has to be taken. However,  $\overline{F}_{i(j)}$  only depend on the absolute value of  $\mathbf{b}$ , therefore Eq. (4) can be written as:

$$I_{ij}(x_1, x_2, q_T; \mu, \zeta) = \frac{1}{2} \int_0^\infty db b J_0(b q_T) \overline{F}_i(x_1, b; \mu, \zeta) \overline{F}_j(x_2, b; \mu, \zeta). \quad (5)$$

where  $J_0$  is the zero-th order Bessel function of the first kind whose integral representation is:

$$J_0(x) = \frac{1}{2\pi} \int_0^{2\pi} d\theta e^{ix \cos(\theta)}. \quad (6)$$

The evolved quark TMD PDF  $\overline{F}_i$  at the final scales  $\mu$  and  $\zeta$  is obtained by multiplying the same distribution at the initial scales  $\mu_0$  and  $\zeta_0$  by a single evolution factor  $R_q$ <sup>(1)</sup>. that is:

$$\overline{F}_i(x, b; \mu, \zeta) = R_q(\mu_0, \zeta_0 \rightarrow \mu, \zeta; b) \overline{F}_i(x, b; \mu_0, \zeta_0). \quad (7)$$

The initial scale TMD PDFs at small values  $b$  can be written as:

$$\overline{F}_i(x, b; \mu_0, \zeta_0) = \sum_{j=g, q(\bar{q})} x \int_x^1 \frac{dy}{y} C_{ij}(y; \mu_0, \zeta_0) f_j\left(\frac{x}{y}, \mu_0\right), \quad (8)$$

where  $f_j$  are the collinear PDFs (including the gluon) and  $C_{ij}$  are the so-called matching functions that are perturbatively computable and are currently known to NNLO, *i.e.*  $\mathcal{O}(\alpha_s^2)$ . If we define:

$$\overline{f}_i(x, \mu_0) = x f_i(x, \mu_0), \quad (9)$$

Eq. (8) can be written as:

$$\overline{F}_i(x, b; \mu_0, \zeta_0) = \sum_{j=g, q(\bar{q})} \int_x^1 dy C_{ij}(y; \mu_0, \zeta_0) \overline{f}_i\left(\frac{x}{y}, \mu_0\right). \quad (10)$$

Putting Eqs. (7) and (10), one finds:

$$\overline{F}_i(x, b; \mu, \zeta) = R_q(\mu_0, \zeta_0 \rightarrow \mu, \zeta; b) \sum_{j=g, q(\bar{q})} \int_x^1 dy C_{ij}(y; \mu_0, \zeta_0) \overline{f}_i\left(\frac{x}{y}, \mu_0\right). \quad (11)$$

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<sup>1</sup>Note that in Eq. (1) the gluon TMD PDF  $\overline{F}_g$  is not involved. If also the gluon TMD PDF was involved, it would evolve by means of a different evolution factor  $R_g$ .

Matching and evolution are affected by non-perturbative effects that become relevant at large  $b$ . In order to account for such effects, one usually introduces a phenomenological function  $f_{\text{NP}}$ . In the traditional approach (CSS [2]), the  $b$ -space TMDs get a multiplicative correction that does not depend on the flavour. In addition, the perturbative content of the TMDs is smoothly damped away at large  $b$  by introducing the so-called  $b_*$ -prescription:

$$\bar{F}_i(x, b; \mu, \zeta) \rightarrow \bar{F}_i(x, b_*(b); \mu, \zeta) f_{\text{NP}}(x, b, \zeta), \quad (12)$$

where  $b_* \equiv b_*(b)$  is a monotonic function of the impact parameter  $b$  such that:

$$\lim_{b \rightarrow 0} b_*(b) = b_{\min} \quad \text{and} \quad \lim_{b \rightarrow \infty} b_*(b) = b_{\max}, \quad (13)$$

being  $b_{\min}$  and  $b_{\max}$  constant values both in the perturbative region. Including the non-perturbative function, Eq. (5) becomes:

$$\begin{aligned} I_{ij}(x_1, x_2, q_T; \mu, \zeta) &= \int_0^\infty db J_0(b q_T) \left[ \frac{b}{2} \bar{F}_i(x_1, b_*(b); \mu, \zeta) \bar{F}_j(x_2, b_*(b); \mu, \zeta) f_{\text{NP}}(x_1, b, \zeta) f_{\text{NP}}(x_2, b, \zeta) \right] \\ &= \frac{1}{q_T} \int_0^\infty d\bar{b} J_0(\bar{b}) \left[ \frac{\bar{b}}{2 q_T} \bar{F}_i(x_1, b_* \left( \frac{\bar{b}}{q_T} \right); \mu, \zeta) \bar{F}_j(x_2, b_* \left( \frac{\bar{b}}{q_T} \right); \mu, \zeta) f_{\text{NP}} \left( x_1, \frac{\bar{b}}{q_T}, \zeta \right) f_{\text{NP}} \left( x_2, \frac{\bar{b}}{q_T}, \zeta \right) \right]. \end{aligned} \quad (14)$$

Eq. (14) is a Hankel tranform and can be efficiently computed using the so-called Ogata quadrature [3]. Effectively, the computation of the integral in Eq. (4) is achieved through a weighted sum:

$$\begin{aligned} I_{ij}(x_1, x_2, q_T; \mu, \zeta) &\simeq \frac{1}{q_T} \sum_{n=1}^N \frac{w_n^{(0)} z_n^{(0)}}{2 q_T} \bar{F}_i \left( x_1, b_* \left( \frac{z_n^{(0)}}{q_T} \right); \mu, \zeta \right) \bar{F}_j \left( x_2, b_* \left( \frac{z_n^{(0)}}{q_T} \right); \mu, \zeta \right) \\ &\times f_{\text{NP}} \left( x_1, \frac{z_n^{(0)}}{q_T}, \zeta \right) f_{\text{NP}} \left( x_2, \frac{z_n^{(0)}}{q_T}, \zeta \right), \end{aligned} \quad (15)$$

where the unscaled coordinates  $z_n^{(0)}$  and the weights  $w_n^{(0)}$  can be precomputed in terms of the zero's of the Bessel function  $J_0$  and one single parameter (see Ref. [3] for more details, specifically Eqs. (5.1) and (5.2) or Appendix A for the relevant formula to compute the unscaled coordinates and the weights)<sup>2</sup>. Based on the (empirically verified) assumption that the absolute value of each term in the sum in the r.h.s. of Eq. (15) is smaller than that of the preceding one, the truncation number  $N$  is chosen dynamically in such a way that the  $(N+1)$ -th term is smaller in absolute value than a user-defined cutoff relatively to the sum of the preceding  $N$  terms.

Eq. (15) factors out the non-perturbative part of the calculation represented by  $f_{\text{NP}}$  from the perturbative content. This is done on purpose to devise a method in which the perturbative content is precomputed and numerically convoluted with the non-perturbative functions *a posteriori*. This is convenient in view of a fit of the function  $f_{\text{NP}}$ .

As customary in QCD, the most convenient basis for the matching in Eq. (8) is the so-called “evolution” basis (*i.e.*  $\Sigma$ ,  $V$ ,  $T_3$ ,  $V_3$ , etc.). In fact, in this basis the operator matrix  $C_{ij}$  is almost diagonal with the only exception of crossing terms that couple the gluon and the singlet  $\Sigma$  distributions. As a consequence, this is the most convenient basis for the computation of  $I_{ij}$ . On the other hand, TMDs in Eq. (1) appear in the so-called “physical” basis (*i.e.*  $d$ ,  $\bar{d}$ ,  $u$ ,  $\bar{u}$ , etc.). Therefore, we need to rotate  $F_{i(j)}$  from the evolution basis, over which the indices  $i$  and  $j$  run, to the physical basis. This is done by means of an appropriate constant matrix  $T$ , so that:

$$\bar{F}_q(x_1, b; \mu, \zeta) = \sum_i T_{qi} F_i(x_1, b; \mu, \zeta), \quad (16)$$

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<sup>2</sup>The superscript 0 in  $z_n^{(0)}$  and  $w_n^{(0)}$  indicates that here we are performing a Hankel tranform that involves the Bessel function of degree zero  $J_0$ . This is useful in view of the next section in which the integration over  $q_T$  will give rise to a similar Hankel transform with  $J_0$  replaced by  $J_1$ . Also in that case the Ogata quadrature algorithm can be applied but coordinates and weights will be different.

and similarly for  $\bar{F}_{\bar{q}}$ . Putting all pieces together, one can conveniently write the cross section in Eq. (1) as:

$$\frac{d\sigma}{dQdydq_T} \simeq \sum_{n=1}^N w_n^{(0)} \frac{z_n^{(0)}}{q_T} S \left( x_1, x_2, \frac{z_n^{(0)}}{q_T}; \mu, \zeta \right) f_{\text{NP}} \left( x_1, \frac{z_n^{(0)}}{q_T}, \zeta \right) f_{\text{NP}} \left( x_2, \frac{z_n^{(0)}}{q_T}, \zeta \right), \quad (17)$$

with:

$$S(x_1, x_2, b; \mu, \zeta) = \frac{8\pi\alpha^2}{9Q^3} H(Q, \mu) \sum_q C_q(Q) [\bar{F}_q(x_1, b_*(b); \mu, \zeta)] [\bar{F}_{\bar{q}}(x_2, b_*(b); \mu, \zeta)]. \quad (18)$$

Eq. (17) allows one to precompute the weights  $S$  in such a way that the differential cross section in Eq. (1) can be computed as a simple weighted sum of the non-perturbative contribution. A misleading aspect of Eq. (18) is the fact that  $S$  has five arguments. In actual facts,  $S$  only depends on three independent variables. The reason is that  $\mu$  and  $\zeta$  are usually taken to be proportional to  $Q$  by a constant factor. In addition  $x_1$  and  $x_2$  depend on  $Q$  and  $y$  through Eq. (2). Therefore, the full dependence on the kinematics of the final state of Eq. (1) can be specified by  $Q$ ,  $y$  and  $q_T$ .

## 2 Integrating over the final-state kinematic variables

Despite Eq. (17) provides a powerful tool for a fast computation of cross sections, it is often not sufficient to allow for a direct comparison to experimental data. The reason is that experimental measurements of differential distributions are usually delivered as integrated over finite regions of the final-state kinematic phase space. In other words, experiments measure quantities like:

$$\tilde{\sigma} = \int_{Q_{\min}}^{Q_{\max}} dQ \int_{y_{\min}}^{y_{\max}} dy \int_{q_{T,\min}}^{q_{T,\max}} dq_T \left[ \frac{d\sigma}{dQdydq_T} \right]. \quad (19)$$

As a consequence, in order to guarantee performance, we need to include the integrations above in the precomputed factors.

### 2.1 Integrating over $q_T$

The integration over bins in  $q_T$  can be carried out analytically exploiting the following property of Bessel's function:

$$\frac{d}{dx} [x^m J_m(x)] = x^m J_{m-1}(x), \quad (20)$$

that leads to:

$$\int dx x J_0(x) = x J_1(x) \quad \Rightarrow \quad \int_{x_1}^{x_2} dx x J_0(x) = x_2 J_1(x_2) - x_1 J_1(x_1). \quad (21)$$

To see it, we observe that the differential cross section in Eq. (1) has the following structure:

$$\frac{d\sigma}{dQdydq_T} \propto \int_0^\infty db q_T J_0(bq_T) \dots \quad (22)$$

where the ellipses indicate terms that do not depend on  $q_T$ . Therefore, using Eq. (21) we find:

$$\begin{aligned} \int_{q_{T,\min}}^{q_{T,\max}} dq_T \left[ \frac{d\sigma}{dQdydq_T} \right] &\propto \int_0^\infty db \int_{q_{T,\min}}^{q_{T,\max}} dq_T q_T J_0(bq_T) \dots = \\ &\int_0^\infty \frac{db}{b^2} \int_{bq_{T,\min}}^{bq_{T,\max}} dx x J_0(x) \dots = \int_0^\infty \frac{db}{b} [q_{T,\max} J_1(bq_{T,\max}) - q_{T,\min} J_1(bq_{T,\min})] \dots \end{aligned} \quad (23)$$

Therefore, defining:

$$K(q_T) \equiv \int dq_T \left[ \frac{d\sigma}{dQ dy dq_T} \right] \quad (24)$$

as the indefinite integral over  $q_T$  of the cross section in Eq. (1), we have that:

$$\int_{q_{T,\min}}^{q_{T,\max}} dq_T \left[ \frac{d\sigma}{dQ dy dq_T} \right] = K(Q, y, q_{T,\max}) - K(Q, y, q_{T,\min}), \quad (25)$$

with:

$$\begin{aligned} K(Q, y, q_T) &= \frac{8\pi\alpha^2 q_T}{9Q^3} H(Q, \mu) \\ &\times \int_0^\infty db J_1(bq_T) \sum_q C_q(Q) \bar{F}_q(x_1, b; \mu, \zeta) \bar{F}_{\bar{q}}(x_2, b; \mu, \zeta) f_{\text{NP}}(x_1, b, \zeta) f_{\text{NP}}(x_2, b, \zeta), \end{aligned} \quad (26)$$

that can be computed using the Ogata quadrature as:

$$K(Q, y, q_T) \simeq \sum_{n=1}^N w_n^{(1)} S \left( x_1, x_2, \frac{z_n^{(1)}}{q_T}; \mu, \zeta \right) f_{\text{NP}} \left( x_1, \frac{z_n^{(1)}}{q_T}, \zeta \right) f_{\text{NP}} \left( x_2, \frac{z_n^{(1)}}{q_T}, \zeta \right), \quad (27)$$

with  $S$  defined in Eq. (18). The unscaled coordinates  $z_n^{(1)}$  and the weights  $w_n^{(1)}$  can again be precomputed and stored in terms of the zero's of the Bessel function  $J_1$ . Eq. (25) reduces the integration in  $q_T$  to a calculation completely analogous to the unintegrated cross section. This is particularly convenient because it avoids the computation a numerical integration.

### 2.1.1 Kinematic cuts

In the presence of kinematic cuts, such as those on the final-state leptons in Drell-Yan, the analytic integration over  $q_T$  discussed above cannot be performed. The reason is that the implementation of these cuts effectively introduces a  $q_T$ -dependent function  $\mathcal{P}^{(3)}$  in the integral:

$$\frac{d\sigma}{dQ dy dq_T} \propto \int_0^\infty db q_T J_0(bq_T) \mathcal{P}(q_T) \dots, \quad (28)$$

that prevents the direct use of Eq. (21). Since  $\mathcal{P}$  is a slowly-varying function of  $q_T$  over the typical bin size, we can approximate the integral over the bins in  $q_T$  as:

$$\begin{aligned} \int_{q_{T,\min}}^{q_{T,\max}} dq_T q_T J_0(bq_T) \mathcal{P}(q_T) &\simeq \mathcal{P} \left( \frac{q_{T,\max} + q_{T,\min}}{2} \right) \int_{q_{T,\min}}^{q_{T,\max}} dq_T q_T J_0(bq_T) \\ &= \mathcal{P} \left( \frac{q_{T,\max} + q_{T,\min}}{2} \right) \frac{1}{b} [q_{T,\max} J_1(bq_{T,\max}) - q_{T,\min} J_1(bq_{T,\min})]. \end{aligned} \quad (29)$$

Unfortunately, this structure is inconvenient because it mixes different bin bounds and prevents a recursive computation. However, we can try to go further and, assuming that the bin width is small enough, we can expand  $\mathcal{P}$  in the following ways:

$$\begin{aligned} \mathcal{P} \left( \frac{q_{T,\max} + q_{T,\min}}{2} \right) &= \mathcal{P}(q_{T,\min} + \Delta q_T) = \mathcal{P}(q_{T,\min}) + \mathcal{P}'(q_{T,\min}) \Delta q_T + \mathcal{O}(\Delta q_T^2), \\ \mathcal{P} \left( \frac{q_{T,\max} + q_{T,\min}}{2} \right) &= \mathcal{P}(q_{T,\max} - \Delta q_T) = \mathcal{P}(q_{T,\max}) - \mathcal{P}'(q_{T,\max}) \Delta q_T + \mathcal{O}(\Delta q_T^2), \end{aligned} \quad (30)$$

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<sup>3</sup>In fact,  $\mathcal{P}$  also depends on the invariant mass  $Q$  and the rapidity  $y$  of the lepton pair that also need to be integrated over.

with:

$$\Delta q_T = \frac{q_{T,\max} - q_{T,\min}}{2}. \quad (31)$$

Therefore:

$$\begin{aligned} b \int_{q_{T,\min}}^{q_{T,\max}} dq_T q_T J_0(bq_T) \mathcal{P}(q_T) &\simeq q_{T,\max} J_1(bq_{T,\max}) [\mathcal{P}(q_{T,\max}) - \mathcal{P}'(q_{T,\max}) \Delta q_T] \\ &- q_{T,\min} J_1(bq_{T,\min}) [\mathcal{P}(q_{T,\min}) + \mathcal{P}'(q_{T,\min}) \Delta q_T]. \end{aligned} \quad (32)$$

The advantage of this formula as compared to Eq. (29) is that each single term depends on one single bin-bound in  $q_T$  rather than on a combination of two consecutive bounds. Therefore, in the presence of kinematic cuts, the actual form of the primitive function  $K$  defined in Eq. (25) and given explicitly in Eq. (26) is:

$$\begin{aligned} K(Q, y, q_T) &= \frac{8\pi\alpha^2 q_T}{9Q^3} H(Q, \mu) [\mathcal{P}(Q, y, q_T) \pm \mathcal{P}'(Q, y, q_T) \Delta q_T] \\ &\times \int_0^\infty db J_1(bq_T) \sum_q C_q(Q) \bar{F}_q(x_1, b; \mu, \zeta) \bar{F}_{\bar{q}}(x_2, b; \mu, \zeta) f_{\text{NP}}(x_1, b, \zeta) f_{\text{NP}}(x_2, b, \zeta), \end{aligned} \quad (33)$$

where I have explicitly reinstated the dependence of the function  $\mathcal{P}$  and its derivative with respect to  $q_T$ ,  $\mathcal{P}'$ , on  $Q$  and  $y$ . In the square bracket in Eq. (33), the minus sign applies when  $q_T$  is the upper bound of the bin and the plus sign when it is the lower bound (see Eq. (32)). As discussed below, when integrating over bins in  $Q$  and  $y$ , one should also integrate the functions  $\mathcal{P}$  and  $\mathcal{P}'$ . However, we will argue that, in the interpolation procedure discussed below, these functions can be extracted from the integrals in  $Q$  and  $y$  in a proper manner in such a way to avoid computing the expensive function  $\mathcal{P}$  many times and, moreover, simplify enormously the structure of the resulting interpolation tables.

## 2.2 On the position of the peak of the $q_T$ distribution

It is interesting at this point to take a short detour to discuss the position of the peak on the distribution in  $q_T$  of the cross section in Eq. (1). The peak can be located by setting the derivative in  $q_T$  of the cross section equal to zero. To do so, we use another property of Bessel's functions:

$$\frac{dJ_0(x)}{dx} = -J_1(x). \quad (34)$$

Using this relation, it is easy to see that:

$$\begin{aligned} 0 &= \frac{d}{dq_T} \left[ \frac{d\sigma}{dQ dy dq_T} \right] = \\ &\frac{8\pi\alpha^2}{9Q^3} H(Q, \mu) \int_0^\infty db b [J_0(bq_T) - bq_T J_1(bq_T)] \sum_q C_q(Q) \bar{F}_q(x_1, b_*(b); \mu, \zeta) \bar{F}_{\bar{q}}(x_2, b_*(b); \mu, \zeta) \\ &\times f_{\text{NP}}(x_1, b, \zeta) f_{\text{NP}}(x_2, b, \zeta), \end{aligned} \quad (35)$$

that is equivalent to require that:

$$\int_0^\infty db b [J_0(bq_T) - bq_T J_1(bq_T)] \sum_q C_q(Q) \bar{F}_q(x_1, b_*(b); \mu, \zeta) \bar{F}_{\bar{q}}(x_2, b_*(b); \mu, \zeta) f_{\text{NP}}(x_1, b, \zeta) f_{\text{NP}}(x_2, b, \zeta) = 0. \quad (36)$$

The integral above can be solved numerically using the technique discussed above and the value of  $q_T$  that satisfies this equation represents the position of the peak of the  $q_T$  distribution.

### 2.3 Integrating over $Q$ and $y$

As a final step, we need to perform the integrals over  $Q$  and  $y$  defined in Eq. (19). To compute these integrals we can only rely on numerical methods. Having reduced the integration in  $q_T$  to the difference of the two terms in the r.h.s. of Eq. (25)<sup>(4)</sup>, we can concentrate on integrating the function  $K$  over  $Q$  and  $y$  for a fixed value of  $q_T$ :

$$\tilde{K}(q_T) = \int_{Q_{\min}}^{Q_{\max}} dQ \int_{y_{\min}}^{y_{\max}} dy K(Q, y, q_T), \quad (37)$$

such that:

$$\tilde{\sigma} = \tilde{K}(q_{T,\max}) - \tilde{K}(q_{T,\min}). \quad (38)$$

To this purpose, it is convenient to make explicit the dependence of  $x_1$  and  $x_2$  on  $Q$  and  $y$  using Eq. (2). In addition, for the sake of simplicity we will identify the scales  $\mu$  and  $\sqrt{\zeta}$  with  $Q$  (possible scale variations can be easily reinstated at a later stage) and thus drop one of the arguments from the TMD distributions  $\bar{F}$  and from the hard factor  $H$ . This yields:

$$\begin{aligned} \tilde{K}(q_T) &= \frac{8\pi q_T}{9} \int_0^\infty db J_1(bq_T) \int_{Q_{\min}}^{Q_{\max}} dQ \int_{e^{y_{\min}}}^{e^{y_{\max}}} \frac{d\xi}{\xi} \\ &\times \frac{1}{Q^3} \alpha^2(Q) H(Q) \sum_q C_q(Q) \bar{F}_q \left( \frac{Q}{\sqrt{s}} \xi, b_*(b); Q \right) \bar{F}_{\bar{q}} \left( \frac{Q}{\sqrt{s}} \frac{1}{\xi}, b_*(b); Q \right) \\ &\times f_{\text{NP}} \left( \frac{Q}{\sqrt{s}} \xi, b; Q \right) f_{\text{NP}} \left( \frac{Q}{\sqrt{s}} \frac{1}{\xi}, b; Q \right), \end{aligned} \quad (39)$$

where we have performed the change of variable  $e^y = \xi$ . Now we define one grid in  $\xi$ ,  $\{\xi_\alpha\}$  with  $\alpha = 0, \dots, N_\xi$ , and one grid in  $Q$ ,  $\{Q_\tau\}$  with  $\tau = 0, \dots, N_Q$ , each of which with a set of interpolating functions  $\mathcal{I}$  associated. In addition, the grids are such that:  $\xi_0 = e^{y_{\min}}$  and  $\xi_{N_\xi} = e^{y_{\max}}$ , and  $Q_0 = Q_{\min}$  and  $Q_{N_Q} = Q_{\max}$ . More details on the interpolation procedure are presented in Appendix B. This allows us to interpolate the pair of functions  $f_{\text{NP}}$  in Eq. (39) for generic values of  $\xi$  and  $Q$  as:

$$f_{\text{NP}} \left( \frac{Q}{\sqrt{s}} \xi, b; Q \right) f_{\text{NP}} \left( \frac{Q}{\sqrt{s}} \frac{1}{\xi}, b; Q \right) \simeq \sum_{\alpha=0}^{N_\xi} \sum_{\tau=0}^{N_Q} \mathcal{I}_\alpha(\xi) \mathcal{I}_\tau(Q) f_{\text{NP}} \left( \frac{Q_\tau}{\sqrt{s}} \xi_\alpha, b; Q_\tau \right) f_{\text{NP}} \left( \frac{Q_\tau}{\sqrt{s}} \frac{1}{\xi_\alpha}, b; Q_\tau \right). \quad (40)$$

Plugging the equation above into Eq. (39) we obtain:

$$\begin{aligned} \tilde{K}(q_T) &\simeq \frac{8\pi q_T}{9} \int_0^\infty db J_1(bq_T) \sum_{\tau=0}^{N_Q} \sum_{\alpha=0}^{N_\xi} \left[ \int_{Q_{\min}}^{Q_{\max}} dQ \mathcal{I}_\tau(Q) \frac{1}{Q^3} \alpha^2(Q) H(Q) \right. \\ &\times \left. \int_{e^{y_{\min}}}^{e^{y_{\max}}} d\xi \mathcal{I}_\alpha(\xi) \frac{1}{\xi} \sum_q C_q(Q) \bar{F}_q \left( \frac{Q}{\sqrt{s}} \xi, b_*(b); Q \right) \bar{F}_{\bar{q}} \left( \frac{Q}{\sqrt{s}} \frac{1}{\xi}, b_*(b); Q \right) \right] \\ &\times f_{\text{NP}} \left( \frac{Q_\tau}{\sqrt{s}} \xi_\alpha, b; Q_\tau \right) f_{\text{NP}} \left( \frac{Q_\tau}{\sqrt{s}} \frac{1}{\xi_\alpha}, b; Q_\tau \right). \end{aligned} \quad (41)$$

<sup>4</sup>For the moment we ignore the complication introduced by the presence of cuts on the final state discussed in Sect. 2.1.1. We will come back on this issue at the end of the section.

Finally, the integration over  $b$  can be performed using the Ogata quadrature as discussed above, so that:

$$\begin{aligned}\tilde{K}(q_T) &\simeq \sum_{n=1}^N \sum_{\tau=0}^{N_Q} \sum_{\alpha=0}^{N_\xi} \left[ \frac{8\pi}{9} w_n^{(1)} \int_{Q_{\min}}^{Q_{\max}} dQ \mathcal{I}_\tau(Q) \frac{1}{Q^3} \alpha^2(Q) H(Q) \right. \\ &\times \int_{e^{y_{\min}}}^{e^{y_{\max}}} d\xi \mathcal{I}_\alpha(\xi) \frac{1}{\xi} \sum_q C_q(Q) \bar{F}_q \left( \frac{Q}{\sqrt{s}} \xi, b_* \left( \frac{z_n}{q_T} \right); Q \right) \bar{F}_{\bar{q}} \left( \frac{Q}{\sqrt{s}} \frac{1}{\xi}, b_* \left( \frac{z_n}{q_T} \right); Q \right) \Big] \\ &\times f_{\text{NP}} \left( \frac{Q_\tau}{\sqrt{s}} \xi_\alpha, \frac{z_n}{q_T}; Q_\tau \right) f_{\text{NP}} \left( \frac{Q_\tau}{\sqrt{s}} \frac{1}{\xi_\alpha}, \frac{z_n}{q_T}; Q_\tau \right).\end{aligned}\quad (42)$$

In conclusion, if we define:

$$\begin{aligned}W_{n\tau\alpha}(q_T) &\equiv w_n^{(1)} \frac{8\pi}{9} \int_{Q_{\min}}^{Q_{\max}} dQ \mathcal{I}_\tau(Q) \frac{\alpha^2(Q)}{Q^3} H(Q) \\ &\times \int_{e^{y_{\min}}}^{e^{y_{\max}}} d\xi \mathcal{I}_\alpha(\xi) \frac{1}{\xi} \sum_q C_q(Q) \bar{F}_q \left( \frac{Q}{\sqrt{s}} \xi, b_* \left( \frac{z_n}{q_T} \right); Q \right) \bar{F}_{\bar{q}} \left( \frac{Q}{\sqrt{s}} \frac{1}{\xi}, b_* \left( \frac{z_n}{q_T} \right); Q \right),\end{aligned}\quad (43)$$

the quantity  $\tilde{K}(q_T)$  can be computed as:

$$\tilde{K}(q_T) \simeq \sum_{n=1}^N \sum_{\tau=0}^{N_Q} \sum_{\alpha=0}^{N_\xi} W_{n\tau\alpha}(q_T) f_{\text{NP}} \left( \frac{Q_\tau}{\sqrt{s}} \xi_\alpha, \frac{z_n}{q_T}; Q_\tau \right) f_{\text{NP}} \left( \frac{Q_\tau}{\sqrt{s}} \frac{1}{\xi_\alpha}, \frac{z_n}{q_T}; Q_\tau \right). \quad (44)$$

The advantage of Eq. (44) is that the weights  $W_{n\tau\alpha}$ , that clearly depend on  $q_T$  but also on the intervals  $[Q_{\min} : Q_{\max}]$  and  $[y_{\min} : y_{\max}]$ , can be precomputed once and for all for each of the experimental points included in a fit and used to determine the function  $f_{\text{NP}}$ . This provides a fast tool for the computation of predictions that makes the extraction of the non-perturbative part of the TMDs much easier.

It is now time to discuss how the weights defined in Eq. (43) are affected by the presence of cuts as discussed in Sect. 2.1.1. In principle, the function between square brackets in Eq. (33) should be inside the integrals in Eq. (43) and integrated over the variable  $Q$  and  $\xi = e^y$ . However, this turns out to be numerically problematic because the phase-space-reduction function  $\mathcal{P}$  is expensive to compute. On top of this, the fact that the factor between square brackets in Eq. (33) depends on whether  $q_T$  is a lower or an upper integration bound would lead to a duplication of the weights to compute. In order to simplify the computation, we assume that the function  $\mathcal{P}$  and its derivative  $\mathcal{P}'$  are slowly varying functions of  $Q$  and  $y$  over the typical grid interval of the grids in  $Q$  and  $\xi$ . In addition, the interpolating functions  $\mathcal{I}_\tau(Q)$  and  $\mathcal{I}_\alpha(\xi)$  are strongly peaked at  $Q_\tau$  and  $\xi_\alpha$ , respectively. These considerations allow us to avoid integrating explicitly  $\mathcal{P}$  and  $\mathcal{P}'$  over  $Q$  and  $\xi$  and to replace the weights in Eq. (43) with:

$$W_{n\tau\alpha}(q_T) \rightarrow [\mathcal{P}(Q_\tau, \ln(\xi_\alpha), q_T) \pm \mathcal{P}'(Q_\tau, \ln(\xi_\alpha), q_T) \Delta q_T] W_{n\tau\alpha}(q_T). \quad (45)$$

At the end of the day, the only additional information required to implement cuts on the final state is the value of the phase-space-reduction function  $\mathcal{P}$  and its derivative  $\mathcal{P}'$  on all points of the bidimensional grid in  $Q$  and  $\xi$  for all  $q_T$  bin bounds. Eq. (45) will then allow one to use the weights computed over the full phase space. We will check the accuracy of this procedure by comparing it to the explicit integration.



## 2.4 Cross section differential in $x_F$

In some cases, the Drell-Yan differential cross section may be presented as differential in the invariant mass of the lepton pair  $Q$  and, instead of the rapidity  $y$ , of the Feynman variable  $x_F$  defined as:

$$x_F = \frac{Q}{\sqrt{s}} (e^y - e^{-y}) = \frac{2Q}{\sqrt{s}} \sinh y = x_1 - x_2, \quad (46)$$

so that:

$$\frac{dx_F}{dy} = \frac{2Q}{\sqrt{s}} \cosh y = x_1 + x_2. \quad (47)$$

Therefore:

$$\frac{d\sigma}{dQ dx_F dq_T} = \frac{dy}{dx_F} \frac{d\sigma}{dQ dy dq_T} = \frac{\sqrt{s}}{2Q \cosh y} \frac{d\sigma}{dQ dy dq_T} = \frac{1}{x_1 + x_2} \frac{d\sigma}{dQ dy dq_T} \quad (48)$$

with:

$$y(x_F, Q) = \sinh^{-1} \left( \frac{x_F \sqrt{s}}{2Q} \right) = \ln \left[ \frac{\sqrt{s}}{2Q} \left( x_F + \sqrt{x_F^2 + \frac{4Q^2}{s}} \right) \right], \quad (49)$$

so that:

$$x_1 = \frac{1}{2} \left( x_F + \sqrt{x_F^2 + \frac{4Q^2}{s}} \right) \quad \text{and} \quad x_2 = \frac{Q^2}{sx_1}. \quad (50)$$

Therefore, we can compute the integral:

$$\tilde{I}(q_T) = \int_{Q_{\min}}^{Q_{\max}} dQ \int_{x_{F,\min}}^{x_{F,\max}} dx_F I(Q, x_F, q_T), \quad (51)$$

where  $I$  is the primitive in  $q_T$  of the cross section differential in  $x_F$ :

$$I(Q, x_F, q_T) = \int dq_T \left[ \frac{d\sigma}{dQ dx_F dq_T} \right], \quad (52)$$

following the same steps of Sect. 2.3. This leads to:

$$\tilde{I}(q_T) \simeq \sum_{n=1}^N \sum_{\tau=0}^{N_Q} \sum_{\alpha=0}^{N_x} \bar{W}_{n\tau\alpha}(q_T) f_{\text{NP}} \left( x_{1,\alpha\tau}, \frac{z_n}{q_T}; Q_\tau \right) f_{\text{NP}} \left( x_{2,\alpha\tau}, \frac{z_n}{q_T}; Q_\tau \right), \quad (53)$$

with:

$$\begin{aligned} \bar{W}_{n\tau\alpha}(q_T) &\equiv w_n^{(1)} \frac{8\pi}{9} \int_{Q_{\min}}^{Q_{\max}} dQ \mathcal{I}_\tau(Q) \frac{1}{Q^3} \alpha^2(Q) H(Q) \\ &\times \int_{x_{F,\min}}^{x_{F,\max}} dx_F \mathcal{I}_\alpha(x_F) \frac{1}{x_1 + x_2} \sum_q C_q(Q) \bar{F}_q \left( x_1, b_* \left( \frac{z_n}{q_T} \right); Q \right) \bar{F}_{\bar{q}} \left( x_2, b_* \left( \frac{z_n}{q_T} \right); Q \right), \end{aligned} \quad (54)$$

where  $x_1$  and  $x_2$  are functions of  $x_F$  and  $Q$  through Eq. (50). In addition, we have defined a grid in  $x_F$ ,  $\{x_{F,\alpha}\}$  with  $\alpha = 0, \dots, N_x$ , that allowed us to define  $x_{1(2),\alpha\tau} \equiv x_{1(2)}(x_{F,\alpha}, Q_\tau)$ .

## 2.5 Flavour dependence

It may be advantageous to introduce a flavour dependence of the non-perturbative contributions to TMDs. This can be easily done by observing that the tensor  $W_{n\tau\alpha}$  defined in Eq. (43) can be decomposed as<sup>5</sup>:

$$W_{n\tau\alpha}(q_T) = \sum_q W_{n\tau\alpha}^{(q)}(q_T), \quad (55)$$

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<sup>5</sup>The same procedure applies to the tensor  $\bar{W}_{n\tau\alpha}$  defined in Eq. (54).

with:

$$\begin{aligned}
W_{n\tau\alpha}^{(q)}(q_T) &\equiv w_n^{(1)} \frac{8\pi}{9} \int_{Q_{\min}}^{Q_{\max}} dQ \mathcal{I}_\tau(Q) \frac{\alpha^2(Q)}{Q^3} H(Q) C_q(Q) \\
&\times \int_{e^{y_{\min}}}^{e^{y_{\max}}} d\xi \mathcal{I}_\alpha(\xi) \frac{1}{\xi} \bar{F}_q \left( \frac{Q}{\sqrt{s}} \xi, b_* \left( \frac{z_n}{q_T} \right); Q \right) \bar{F}_{\bar{q}} \left( \frac{Q}{\sqrt{s}} \frac{1}{\xi}, b_* \left( \frac{z_n}{q_T} \right); Q \right).
\end{aligned} \tag{56}$$

This allows for an independent parameterisation of the non-perturbative contribution such that Eq. (44) can be written as:

$$\tilde{K}(q_T) \simeq \sum_q \sum_{n=1}^N \sum_{\tau=0}^{N_Q} \sum_{\alpha=0}^{N_\xi} W_{n\tau\alpha}^{(q)}(q_T) f_{\text{NP}}^{(q)} \left( \frac{Q_\tau}{\sqrt{s}} \xi_\alpha, \frac{z_n}{q_T}; Q_\tau \right) f_{\text{NP}}^{(q)} \left( \frac{Q_\tau}{\sqrt{s}} \frac{1}{\xi_\alpha}, \frac{z_n}{q_T}; Q_\tau \right), \tag{57}$$

where  $f_{\text{NP}}^{(q)}$  parametrises the non-perturbative component of the TMD with flavour  $q$ .

## 2.6 Gradient with respect to the free parameters

A very appealing implication of the computation of cross section in terms of precomputed table as in Eqs. (44) and (57) is the fact that it exposes the free parameters of the non-perturbative functions. To be more specific, the non-perturbative function  $f_{\text{NP}}$ , on top of being a function of  $x$ ,  $b$ , and  $\zeta$ , depends parameterically on a set of  $N_p$  parameters  $\{\theta_k\}$ ,  $k = 1, \dots, N_p$ , that are typically determined by fits to data, in other words:

$$f_{\text{NP}} \equiv f_{\text{NP}}(x, b, \zeta; \{\theta_k\}). \tag{58}$$

Now, when performing a fit, it is very useful to be able to compute the derivative of the figure of merit (usually the  $\chi^2$ ) with respect to the parameters to be determined. In turn, this immediately implies being able to compute the derivative of the observables. Referring to Eq. (44), the relevant quantity is:

$$\frac{d\tilde{K}}{d\theta_k} = \sum_{n=1}^N \sum_{\tau=0}^{N_Q} \sum_{\alpha=0}^{N_\xi} W_{n\tau\alpha}(q_T) \left[ \frac{df_{\text{NP}}^{(1)}}{d\theta_k} f_{\text{NP}}^{(2)} + f_{\text{NP}}^{(1)} \frac{df_{\text{NP}}^{(2)}}{d\theta_k} \right], \tag{59}$$

where  $f_{\text{NP}}^{(1)}$  and  $f_{\text{NP}}^{(2)}$  refer to the non-perturbative function  $f_{\text{NP}}$  computed in  $x_1$  and  $x_2$ , respectively. It is thus clear that the derivatives w.r.t. the free parameters penetrates the observable. Since in most cases the derivative of  $f_{\text{NP}}$  can be computed analytically, this allows one to compute the gradient of the figure of merit analytically. This potentially makes any fit much simpler.

## 2.7 Narrow-width approximation

A possible alternative to the numerical integration in  $Q$  when the integration region includes the  $Z$ -peak region is the so-called narrow-width approximation (NWA). In the NWA one assumes that the width of the  $Z$  boson,  $\Gamma_Z$ , is much smaller than its mass,  $M_Z$ . This way one can approximate the peaked behaviour of the couplings  $C_q(Q)$  around  $Q = M_Z$  with a  $\delta$ -function, *i.e.*  $C_q(Q) \sim \delta(Q^2 - M_Z^2)$ . Therefore, the integration over  $Q$  can be done analytically. The exact structure of the electroweak couplings is the following:

$$C_q(Q) = e_q^2 - 2e_q V_q V_e \chi_1(Q) + (V_e^2 + A_e^2)(V_q^2 + A_q^2) \chi_2(Q), \tag{60}$$

with:

$$\begin{aligned}
\chi_1(Q) &= \frac{1}{4 \sin^2 \theta_W \cos^2 \theta_W} \frac{Q^2(Q^2 - M_Z^2)}{(Q^2 - M_Z^2)^2 + M_Z^2 \Gamma_Z^2}, \\
\chi_2(Q) &= \frac{1}{16 \sin^4 \theta_W \cos^4 \theta_W} \frac{Q^4}{(Q^2 - M_Z^2)^2 + M_Z^2 \Gamma_Z^2}.
\end{aligned} \tag{61}$$

In the limit  $\Gamma_Z/M_Z \rightarrow 0$ , the leading contribution to the coupling in Eq. (60) comes from the region  $Q \simeq M_Z$  and is that proportional to  $\chi_2$ :

$$C_q(Q) \simeq (V_e^2 + A_e^2)(V_q^2 + A_q^2)\chi_2(Q), \quad Q \simeq M_Z. \quad (62)$$

In addition, in this limit one can show that:

$$\frac{1}{(Q^2 - M_Z^2)^2 + M_Z^2 \Gamma_Z^2} \rightarrow \frac{\pi}{M_Z \Gamma_Z} \delta(Q^2 - M_Z^2) = \frac{\pi}{2M_Z^2 \Gamma_Z} \delta(Q - M_Z). \quad (63)$$

Therefore, considering that:

$$\Gamma_Z = \frac{\alpha M_Z}{\sin^2 \theta_W \cos^2 \theta_W}, \quad (64)$$

the electroweak couplings in the NWA have the following form:

$$C_q(Q) \simeq \frac{\pi M_Z (V_e^2 + A_e^2)(V_q^2 + A_q^2)}{32\alpha \sin^2 \theta_W \cos^2 \theta_W} \delta(Q - M_Z) = \tilde{C}_q(Q) \delta(Q - M_Z). \quad (65)$$

Therefore, using Eq. (65) the integral of the cross section over  $Q$  under the condition that  $Q_{\min} < M_Z < Q_{\max}$  has the consequence of adjusting the couplings and of setting  $Q = M_Z$  in the computation. This yields:

$$\int_{Q_{\min}}^{Q_{\max}} dQ \frac{d\sigma}{dQ dy dq_T} = \frac{16\pi\alpha^2 q_T}{9M_Z^3} H(M_Z, M_Z) \sum_q \tilde{C}_q(M_Z) I_{q\bar{q}}(x_1, x_2, q_T; M_Z, M_Z^2), \quad (66)$$

where we are also assuming that  $\mu = \sqrt{\zeta} = M_Z$ . As a final step, one may want to let the  $Z$  boson decay into leptons. At leading order in the EW sector and assuming an equal decay rate for electrons, muons, and tauons, this can be done by multiplying the cross section above by three times the branching ratio for the  $Z$  decaying into any pair of leptons,  $3\text{Br}(Z \rightarrow \ell^+ \ell^-)$ .

## A Ogata quadrature

In this section we limit ourselves to write the formulas for the computation of the unscaled coordinates  $z_n^{(\nu)}$  and weights  $w_n^{(\nu)}$  required to compute the following integral:

$$I_\nu(q_T) = \int_0^\infty db J_\nu(bq_T) f(b) = \frac{1}{q_T} \int_0^\infty d\bar{b} J_\nu(\bar{b}) f\left(\frac{\bar{b}}{q_T}\right) \simeq \frac{1}{q_T} \sum_{n=1}^\infty w_n^{(\nu)} f\left(\frac{z_n^{(\nu)}}{q_T}\right) \quad \nu = 0, 1, \dots, \quad (67)$$

using the Ogata-quadrature algorithm. More details can be found in Ref. [3]. There relevant formulas are:

$$z_n^{(\nu)} = \frac{\pi}{h} \psi\left(\frac{h\xi_{\nu n}}{\pi}\right), \quad (68)$$

$$w_n^{(\nu)} = \pi \frac{Y_\nu(\xi_{\nu n})}{J_{\nu+1}(\xi_{\nu n})} J_\nu(z_n^{(\nu)}) \psi'\left(\frac{h\xi_{\nu n}}{\pi}\right).$$

where:

- $h$  is a free parameter of the algorithm that has to be typically small (we choose  $h = 10^{-3}$ ),
- $\xi_{\nu n}$  are the zero's of  $J_\nu$ , i.e.  $J_\nu(\xi_{\nu n}) = 0 \quad \forall n$ ,
- $J_\nu$  and  $Y_\nu$  are the Bessel functions of first and second kind, respectively, of degree  $\nu$ ,
- $\psi$  is the following function:

$$\psi(t) = t \tanh\left(\frac{\pi}{2} \sinh t\right) \quad (69)$$

and its derivative:

$$\psi'(t) = \frac{\pi t \cosh t + \sinh(\pi \sinh t)}{1 + \cosh(\pi \sinh t)}. \quad (70)$$

## B Lagrange interpolation

Just for the record, it is useful to derive a general expression for the Lagrange interpolating functions  $\mathcal{I}$  introduced in Eq. (40) and used to interpolate the non-perturbative functions  $f_{\text{NP}}$ . More, importantly, we need to understand how these functions behave upon integration.

Suppose one wants to interpolate the test function  $g$  in the point  $x$  using a set of Lagrange polynomials of degree  $k$ . This requires a subset of  $k+1$  consecutive points on an interpolation grid, say  $\{x_\alpha, \dots, x_{\alpha+k}\}$ . The relative position between the point  $x$  and the subset of points used for the interpolation is arbitrary. It is convenient to choose the subset of points such that  $x_\alpha < x \leq x_{\alpha+k}$ .<sup>6</sup> However, the ambiguity remains because there are  $k$  possible choices according to whether  $x_\alpha < x \leq x_{\alpha+1}$ , or  $x_{\alpha+1} < x \leq x_{\alpha+2}$ , and so on.

In order to determine the exact form of the interpolation functions  $\mathcal{I}$ , let us see how to derive eq. (40). Using the standard Lagrange interpolation procedure, we can approximate the function  $g$  in  $x$  as:

$$g(x) = \sum_{i=0}^k \ell_i^{(k)}(x) g(x_{\alpha+i}), \quad (71)$$

where  $\ell_i^{(k)}$  is the  $i$ -th Lagrange polynomial of degree  $k$  which can be written as:

$$\ell_i^{(k)}(x) = \prod_{m=0, m \neq i}^k \frac{x - x_{\alpha+m}}{x_{\alpha+i} - x_{\alpha+m}}. \quad (72)$$

---

<sup>6</sup>In fact, it is not even necessary to impose the constraint  $x_\alpha < x \leq x_{\alpha+k}$ . In case this relation is not fulfilled one usually refers to *extrapolation* rather than *interpolation*. If not necessary, this option is typically not convenient because it may lead to a substantial deterioration in the accuracy with which  $g(x)$  is determined.

We now assume that:

$$x_\alpha < x \leq x_{\alpha+1}, \quad (73)$$

Eq. (71) becomes:

$$g(x) = \theta(x - x_\alpha)\theta(x_{\alpha+1} - x) \sum_{i=0}^k g(x_{\alpha+i}) \prod_{m=0, m \neq i}^k \frac{x - x_{\alpha+m}}{x_{\alpha+i} - x_{\alpha+m}}. \quad (74)$$

In order to make Eq. (74) valid for all values of  $\alpha$ , one just has to sum over all  $N_x$  intervals of the *global* interpolation grid  $\{x_0, \dots, x_{N_x}\}$ , that is:

$$g(x) = \sum_{\alpha=0}^{N_x-1} \theta(x - x_\alpha)\theta(x_{\alpha+1} - x) \sum_{i=0}^k g(x_{\alpha+i}) \prod_{m=0, m \neq i}^k \frac{x - x_{\alpha+m}}{x_{\alpha+i} - x_{\alpha+m}}, \quad (75)$$

Defining  $\beta = \alpha + i$ , we can rearrange the equation above as:

$$g(x) = \sum_{\beta=0}^{N_x+k-1} \mathcal{I}_\beta^{(k)}(x) g(x_\beta), \quad (76)$$

that leads us to the definition of the interpolating functions:

$$\mathcal{I}_\beta^{(k)}(x) = \sum_{i=0, i \leq \beta}^k \theta(x - x_{\beta-i})\theta(x_{\beta-i+1} - x) \prod_{m=0, m \neq i}^k \frac{x - x_{\beta-i+m}}{x_\beta - x_{\beta-i+m}}, \quad (77)$$

where the condition  $i \leq \beta$  comes from the condition  $\alpha \geq 0$ . It is important to observe that the sum in Eq. (76) extends up to the  $(N_x + k - 1)$ -th node. Therefore, the original grid needs to be extended by  $k - 1$  nodes. However, the range of validity of the interpolation remains that defined by the original grid, *i.e.*  $x_0 \leq x \leq x_{N_x}$ .

When implementing this interpolation procedure, it is convenient to realise that, typically, only a small number of terms in the sum in Eq. (76) is different from zero. For any give value of  $x$ , it is possible to determine the values of the index  $\beta$  for which the interpolating functions  $\mathcal{I}_\beta^{(k)}$  are different from zero, reducing (often dramatically) the amount of sums required to carry out an interpolation. The range of  $\beta$  is easily determined by observing that in Eq. (74) the summation extends on the nodes between  $x_\alpha$  and  $x_{\alpha+k}$ . But since  $\beta$  is defined like  $\alpha + i$  this exactly defines the range in  $\beta$ :

$$\alpha(x) \leq \beta \leq \alpha(x) + k, \quad (78)$$

where the function  $\alpha(x)$  is implicitly defined through Eq. (73). Therefore, Eq. (76) becomes:

$$g(x) = \sum_{\beta=\alpha(x)}^{\alpha(x)+k} \mathcal{I}_\beta^{(k)}(x) g(x_\beta), \quad (79)$$

Finally, we notice that sometimes it may be required to integrate the interpolating functions. In this case, it is very useful to use the fact that the interpolation function  $\mathcal{I}_\beta^{(k)}(x)$  is different from zero only over a limited interval, specifically:

$$\mathcal{I}_\beta^{(k)}(x) \neq 0 \quad \Leftrightarrow \quad x_{\beta-k} < x < x_{\beta+1}. \quad (80)$$

This allows one to optimise the integration restricting the integration region only to where the interpolating functions is different from zero.

## B.1 Generalised interpolation

In the rest of this document we will stick to the assumption in Eq. (73). However, before going further, it is interesting to generalise Eq. (73) to:

$$x_{\alpha+t} < x \leq x_{\alpha+t+1} \quad \text{with} \quad t = 0, \dots, k-1, \quad (81)$$

such that the interpolation formula becomes:

$$g(x) = \sum_{\alpha=-t}^{N_x-t-1} \theta(x - x_{\alpha+t}) \theta(x_{\alpha+t+1} - x) \sum_{i=0}^k g(x_{\alpha+i}) \prod_{m=0, m \neq i}^k \frac{x - x_{\alpha+m}}{x_{\alpha+i} - x_{\alpha+m}}, \quad (82)$$

that can be rearranged as:

$$g(x) = \sum_{\beta=-t}^{N_x+k-t-1} \mathcal{I}_{\beta,t}^{(k)}(x) g(x_{\beta}), \quad (83)$$

with:

$$\mathcal{I}_{\beta,t}^{(k)}(x) = \sum_{i=0, i \leq \beta}^k \theta(x - x_{\beta-i+t}) \theta(x_{\beta-i+t+1} - x) \prod_{m=0, m \neq i}^k \frac{x - x_{\beta-i+m}}{x_{\beta} - x_{\beta-i+m}}, \quad (84)$$

being the “generalised” interpolation functions. We observe that the support region of  $\mathcal{I}_{\beta,t}^{(k)}$  is:

$$\mathcal{I}_{\beta,t}^{(k)}(x) \neq 0 \quad \Leftrightarrow \quad x_{\beta+t-k} < x < x_{\beta+t+1}, \quad (85)$$

that generalises Eq. (80). The generalised interpolation functions can be used to avoid interpolating over some particular grid nodes. This turns out to be useful when interpolating non-smooth functions or with discontinuities, such as PDFs or FFs as functions of the factorisation scales in correspondence of the heavy-quark thresholds. More specifically, one can choose  $t$  dynamically in such a way that  $\beta+t$  in Eq. (84) never corresponds to the heavy-quark thresholds node. This mechanism is implemented in APFEL as follows. The interpolation grid is chosen to have two nodes in correspondence of the threshold  $x_T$ , but slightly displaced up and down by an “infinitesimal” amount  $\epsilon$  to keep them separate, that is:

$$\{x_0, \dots, x_{\alpha_t-1}, x_{\alpha_t}, \dots, x_{N_x}\} \quad \text{with} \quad x_{\alpha_t-1} = x_T - \epsilon \quad \text{and} \quad x_{\alpha_t} = x_T + \epsilon. \quad (86)$$

The aim is then to avoid interpolating over the nodes  $x_{\alpha_t-1}$  and  $x_{\alpha_t}$ . By default we assume  $t = 0$  in Eq. (84) so that we automatically reduce to Eq. (77). In this situation, we are assuming Eq. (73) where effectively the index  $\alpha$  is determined dynamically according to the values of  $x$ . Therefore, we can effectively write:

$$x_{\alpha(x)} < x \leq x_{\alpha(x)+1}, \quad (87)$$

which implicitly defines the function  $\alpha(x)$ . Eq. (74) then requires summing over the  $k+1$  nodes of the grid  $\{x_{\alpha(x)}, \dots, x_{\alpha(x)+k}\}$ . However, when the point  $x$  approaches  $x_T$  from below, the range  $\{x_{\alpha(x)}, \dots, x_{\alpha(x)+k}\}$  may end up enclosing both nodes  $x_{\alpha_t-1}$  and  $x_{\alpha_t}$ . To avoid this, we promote the index  $t$  in Eq. (81) to a function of  $x$  defined through the inequalities:

$$\begin{cases} x < x_T, \\ x_{\alpha_t-2} < x_{\alpha(x)-t(x)+k} \leq x_{\alpha_t-1}, \end{cases} \quad (88)$$

that translate into:

$$\begin{cases} \alpha(x) \leq \alpha_t - 2, \\ \alpha_t - 2 < \alpha(x) - t(x) + k \leq \alpha_t - 1. \end{cases} \quad (89)$$

Being all integers and imposing the unnecessary but convenient constraint  $t(x) \geq 0$ , we find the final expression:

$$t(x) = \max[\min[\alpha(x), \alpha_t - 2] - \alpha_t + k + 1, 0], \quad (90)$$

that also obeys:

$$0 \leq t(x) \leq k-1, \quad (91)$$

as required. In addition, as in Eq. (79), the summation over  $\beta$  in Eq. (83) can be restricted to a range of  $k+1$  nodes as:

$$g(x) = \sum_{\beta=\alpha(x)-t(x)}^{\alpha(x)-t(x)+k} \mathcal{I}_{\beta,t}^{(k)}(x) g(x_\beta). \quad (92)$$

## B.2 Bi-dimensional interpolation

Now suppose we want to compute the following integral:

$$I_1 = \int_{x_0}^{x_{N_x}} dx g(x) f(x), \quad (93)$$

where  $f$  is a smooth function. Using Eqs. (76) and (80) we have that:

$$I_1 = \sum_{\beta=0}^{N_x+k-1} W_\beta g(x_\beta), \quad (94)$$

with:

$$W_\beta = \int_{x_{\max(0,\beta-k)}}^{x_{\min(N_x,\beta+1)}} dx \mathcal{I}_\beta^{(k)}(x) f(x). \quad (95)$$

The equation above can be easily generalised to a bidimensional integral as:

$$I_2 = \int_{x_0}^{x_{N_x}} dx \int_{y_0}^{y_{N_y}} dy g(x, y) f(x, y) = \sum_{\alpha=0}^{N_x+k-1} \sum_{\beta=0}^{N_y+l-1} W_{\alpha\beta} g(x_\alpha, y_\beta), \quad (96)$$

with:

$$W_{\alpha\beta} = \int_{x_{\max(0,\alpha-k)}}^{x_{\min(N_x,\alpha+1)}} dx \int_{y_{\max(0,\beta-k)}}^{y_{\min(N_y,\beta+1)}} dy \mathcal{I}_\alpha^{(k)}(x) \mathcal{I}_\beta^{(l)}(y) f(x, y). \quad (97)$$

This formalism nicely applies to the integral in  $Q$  and  $\xi = e^y$  discussed above in Eq. (43). In view of a numerical implementation, it is worth noticing that the functions  $\mathcal{I}$  are piecewise. In particular, while these functions are continuous in correspondence of the nodes of the grid, their first derivative is not. As a consequence, the result of the numerical integrals in Eqs. (95) and (97) may be inaccurate. To overcome this problem, it is sufficient to split the integrals in sub-integrals over the intervals delimited by two consecutive nodes. Using Eq. (80), it is easy to see that, for an interpolation of degree  $k$ , one needs to do  $k+1$  integrals over the intervals included between the  $(\beta-k)$ -th and the  $(\beta+1)$ -th node.

## B.3 Derivative and integral of an interpolated function

The simple form of the Lagrange polynomials allows, in some cases, for the analytic handling of operations such as derivation and integration of the interpolated functions. In this section we discuss how derivation and integration can be carried out analytically exploiting the properties of the Lagrange polynomials.

We start from Eq. (71) and the main observation is that the interpolating functions  $\ell_i^{(k)}$  are solutions of the following differential-equation system:

$$\begin{cases} \frac{d\ell_i^{(k)}}{dx} = \left( \sum_{\substack{n=0 \\ n \neq i}}^k \frac{1}{x - x_{\alpha+n}} \right) \ell_i^{(k)}(x) \\ \ell_i^{(k)}(x_{\alpha+i}) = 1 \end{cases}, \quad (98)$$

whose solution is Eq. (72). This allows us to compute the derivative of the test function  $g$  in Eq. (79) only knowing its values on the grid points as:

$$\frac{dg}{dx} = \sum_{\beta=\alpha(x)}^{\alpha(x)+k} \mathcal{D}_{\beta}^{(k)}(x)g(x_{\beta}), \quad (99)$$

where:

$$\mathcal{D}_{\beta}^{(k)}(x) = \sum_{i=0}^{\min(k,\beta)} \theta(x - x_{\beta-i})\theta(x_{\beta-i+1} - x) \left( \sum_{\substack{n=0 \\ n \neq i}}^k \frac{1}{x_{\beta} - x_{\beta-i+n}} \prod_{\substack{m=0 \\ m \neq i, n}}^k \frac{x - x_{\beta-i+m}}{x_{\beta} - x_{\beta-i+m}} \right). \quad (100)$$

Eq. (98) can also be used to compute integrals of the function  $g$ . In particular, we want to compute the integral:

$$I(a, b) = \int_a^b dy g(y). \quad (101)$$

Using Eq. (79), we find that:

$$I(a, b) = \int_a^b dy \sum_{\beta=\alpha(y)}^{\alpha(y)+k} \mathcal{I}_{\beta}^{(k)}(y)g(x_{\beta}) = \int_a^b dy \left[ \mathcal{I}_{\alpha(y)}^{(k)}(y)g(x_{\alpha(y)}) + \cdots + \mathcal{I}_{\alpha(y)+k}^{(k)}(y)g(x_{\alpha(y)+k}) \right]. \quad (102)$$

The dependence on the integration variable  $y$  of the index  $\alpha$  complicates the solution of this integral. It is easy to derive a close form for the function  $\alpha(y)$ :

$$\alpha(y) = -1 + \sum_{\beta=0}^{N_x} \theta(y - x_{\beta}), \quad (103)$$

that (obviously) means that  $\alpha(y)$  is constant on the separate intervals  $[x_0 : x_1]$ ,  $[x_1 : x_2]$ , and so on. This allows us to break the integral above as follows:

$$\int_a^b dy \sum_{\beta=\alpha(y)}^{\alpha(y)+k} \mathcal{I}_{\beta}^{(k)}(y)g(x_{\beta}) = \left[ \int_a^{x_{\alpha(a)+1}} + \sum_{\gamma=\alpha(a)+1}^{\alpha(b)-1} \int_{x_{\gamma}}^{x_{\gamma+1}} + \int_{x_{\alpha(b)}}^b \right] dy \sum_{\beta=\alpha(y)}^{\alpha(y)+k} \mathcal{I}_{\beta}^{(k)}(y)g(x_{\beta}), \quad (104)$$

such that in each single integral the integrand has a constant value of  $\alpha$ . The three terms above can be separately rearranged as:

$$\sum_{\beta=\alpha(a)}^{\alpha(a)+k} g(x_{\beta}) \int_a^{x_{\alpha(a)+1}} dy \mathcal{I}_{\beta}^{(k)}(y), \quad (105)$$

$$\sum_{\gamma=\alpha(a)+1}^{\alpha(b)-1} \sum_{\beta=\gamma}^{\gamma+k} g(x_{\beta}) \int_{x_{\gamma}}^{x_{\gamma+1}} dy \mathcal{I}_{\beta}^{(k)}(y), \quad (106)$$

$$\sum_{\beta=\alpha(b)}^{\alpha(b)+k} g(x_{\beta}) \int_{x_{\alpha(b)}}^b dy \mathcal{I}_{\beta}^{(k)}(y), \quad (107)$$

where we have also used the fact that  $\alpha(x_{\gamma}) = \gamma$ . Notice that this we managed to obtain direct integrations of the interpolating functions  $\mathcal{I}_{\beta}^{(k)}$ . Now we note that the three terms above span the range of nodes  $\beta \in [\alpha(a) : \alpha(b) + k]$ . Therefore, the integral in Eq. (101) can be written as:

$$I(a, b) = \sum_{\beta=\alpha(a)}^{\alpha(b)+k} \mathcal{G}_{\beta}^{(k)}(a, b)g(x_{\beta}), \quad (108)$$



with:

$$\begin{aligned}
\mathcal{G}_\beta^{(k)}(a, b) &= \int_{\max(a, x_{\beta-k})}^{\min(b, x_{\beta+1})} dy \mathcal{I}_\beta^{(k)}(y) \\
&= \sum_{i=0}^{\min(k, \beta)} \int_{\max(a, x_{\beta-k})}^{\min(b, x_{\beta+1})} dy \theta(y - x_{\beta-i}) \theta(x_{\beta-i+1} - y) \prod_{\substack{m=0 \\ m \neq i}}^k \frac{y - x_{\beta-i+m}}{x_\beta - x_{\beta-i+m}}.
\end{aligned} \tag{109}$$

Now, assuming that  $a \leq b$ , we can write the integral above as:

$$\int_{\max(a, x_{\beta-k})}^{\min(b, x_{\beta+1})} dy \theta(y - x_{\beta-i}) \theta(x_{\beta-i+1} - y) \cdots = \theta(b - x_{\beta-i}) \theta(x_{\beta-i+1} - a) \int_{\max(a, x_{\beta-i})}^{\min(b, x_{\beta-i+1})} dy \dots, \tag{110}$$

so that:

$$\mathcal{G}_\beta^{(k)}(a, b) = \sum_{i=0}^{\min(k, \beta)} \theta(b - x_{\beta-i}) \theta(x_{\beta-i+1} - a) \prod_{\substack{m=0 \\ m \neq i}}^k \frac{1}{x_\beta - x_{\beta-i+m}} \int_{\max(a, x_{\beta-i})}^{\min(b, x_{\beta-i+1})} dy \prod_{\substack{m=0 \\ m \neq i}}^k (y - x_{\beta-i+m}). \tag{111}$$

It is easy to see that:

$$\prod_{\substack{m=0 \\ m \neq i}}^k (y - x_{\beta-i+m}) = \sum_{n=0}^k (-1)^n p_\beta^{(k)}(n) y^{k-n}, \tag{112}$$

such that:

$$\begin{aligned}
\mathcal{G}_\beta^{(k)}(a, b) &= \sum_{i=0}^{\min(k, \beta)} \theta(b - x_{\beta-i}) \theta(x_{\beta-i+1} - a) \\
&\times \left[ \prod_{\substack{m=0 \\ m \neq i}}^k \frac{1}{x_\beta - x_{\beta-i+m}} \right] \sum_{n=0}^k \frac{(-1)^n p_\beta^{(k)}(n)}{k - n + 1} \left( \bar{b}^{k-n+1} - \bar{a}^{k-n+1} \right).
\end{aligned} \tag{113}$$

with  $\bar{a} = \max(a, x_{\beta-i})$  and  $\bar{b} = \min(b, x_{\beta-i+1})$ . What is left to do is to determine the coefficients  $p_\beta^{(k)}$ . For convenience, let us define the set  $\{r_1, \dots, r_k\} = \{x_{\beta-i}, \dots, x_{\beta-1}, x_{\beta+1}, \dots, x_{\beta-i+k}\}$ .<sup>7</sup> The coefficients  $p_\beta^{(k)}$  defined in Eq. (112) can be expressed as:

$$p_\beta^{(k)}(n) = \sum_{i_1=1}^k r_{i_1} \sum_{i_2=i_1+1}^k r_{i_2} \cdots \sum_{i_n=i_{n-1}+1}^k r_{i_n}. \tag{114}$$

In order to obtain a convenient algorithm to compute the coefficients  $p_\beta^{(k)}$ , we define the vectorial function:

$$\mathbf{f}^{(k)}(\mathbf{r}, \mathbf{a}) \quad \text{with components} \quad f_j^{(k)}(\mathbf{r}, \mathbf{a}) = \sum_{i=j+1}^k r_i a_i. \tag{115}$$

It is important to notice that while  $\mathbf{r}$  is a  $k$ -dimensional vector with index running between 1 and  $k$ ,  $\mathbf{a}$  and  $\mathbf{f}^{(k)}$  are in principle infinite-dimensional vectors with index running between  $-\infty$  and  $+\infty$ . However, given the definition of its components in Eq. (114), it turns out that  $f_j^{(k)} = 0$  for  $j \geq k$ . The

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<sup>7</sup>From the definition of the set  $\{r_1, \dots, r_k\}$ , it becomes clear that the subscript  $\beta$  of the coefficients  $p_\beta^{(k)}$  refers to the fact that this coefficients are computed on a vector of  $k$  nodes where the node  $x_\beta$  has been removed.

same applies to  $\mathbf{a}$  because, as we will see below, it has to be identified with some  $\mathbf{f}^{(k)}$ . The function  $\mathbf{f}^{(k)}$  can now be used to define the vector  $\mathbf{P}^{(k)}(n)$  recursively. The relevant recursive relation is:

$$\mathbf{P}^{(k)}(n+1) = \mathbf{f}^{(k)}(\mathbf{r}, \mathbf{P}^{(k)}(n)) \quad \text{with} \quad \mathbf{P}^{(k)}(0) = \mathbf{1}. \quad (116)$$

Finally, the coefficient  $p_\beta^{(k)}(n)$  is the zero-th component of the vector  $\mathbf{P}^{(k)}(n)$ , i.e.  $p_\beta^{(k)}(n) \equiv P_0^{(k)}(n)$ .

Now, we turn to derive derivation and integration formulas for the generalised interpolation formula in Eq. (117). The derivative is as simple as in the  $t = 0$  case, that is:

$$\frac{dg}{dx} = \sum_{\beta=\alpha(x)-t(x)}^{\alpha(x)-t(x)+k} \mathcal{D}_{\beta,t}^{(k)}(x) g(x_\beta), \quad (117)$$

with:

$$\mathcal{D}_{\beta,t}^{(k)}(x) = \sum_{i=0}^{\min(k,\beta)} \theta(x - x_{\beta-i+t(x)}) \theta(x_{\beta-i+t(x)+1} - x) \left( \sum_{\substack{n=0 \\ m \neq i}}^k \frac{1}{x_\beta - x_{\beta-i+n}} \prod_{\substack{m=0 \\ m \neq i, n}}^k \frac{x - x_{\beta-i+m}}{x_\beta - x_{\beta-i+m}} \right). \quad (118)$$

Due to the presence of the function  $t(x)$ , defined in Eq. (90), the integration procedure is more involved. We want to compute:

$$\begin{aligned} I(a, b) &= \int_a^b dy \sum_{\beta=\alpha(y)-t(y)}^{\alpha(y)-t(y)+k} \mathcal{I}_{\beta,t}^{(k)}(y) g(x_\beta) \\ &= \left[ \int_a^{x_{\alpha(a)+1}} + \sum_{\gamma=\alpha(a)+1}^{\alpha(b)} \int_{x_\gamma}^{x_{\gamma+1}} - \int_b^{x_{\alpha(b)+1}} \right] dy \sum_{\beta=\alpha(y)-t(y)}^{\alpha(y)-t(y)+k} \mathcal{I}_{\beta,t}^{(k)}(y) g(x_\beta). \end{aligned} \quad (119)$$

As in the case of  $t = 0$ , each of the integrals above has a constant value of  $\alpha(y)$  and  $t(y)$  so that sum over  $\beta$  and integral sign can be exchanged:

$$\begin{aligned} I(a, b) &= \sum_{\beta=\alpha(a)-t(a)}^{\alpha(a)-t(a)+k} g(x_\beta) \int_a^{x_{\alpha(a)+1}} dy \mathcal{I}_{\beta,t}^{(k)}(y) \\ &+ \sum_{\gamma=\alpha(a)+1}^{\alpha(b)} \sum_{\beta=\gamma-t_\gamma}^{\gamma-t_\gamma+k} g(x_\beta) \int_{x_\gamma}^{x_{\gamma+1}} dy \mathcal{I}_{\beta,t}^{(k)}(y) \\ &- \sum_{\beta=\alpha(b)-t(b)}^{\alpha(b)-t(b)+k} g(x_\beta) \int_b^{x_{\alpha(b)+1}} dy \mathcal{I}_{\beta,t}^{(k)}(y), \end{aligned} \quad (120)$$

with:

$$t_\gamma = t(x_\gamma) = \max[\min[\gamma, \alpha_t - 2] - \alpha_t + k + 1, 0]. \quad (121)$$

It turns out to be very complicated to write the expression in Eq. (120) in a more compact form, such as that in Eq. (108). Therefore, we implement Eq. (120) as it is. The one thing left to do is to solve the integrals. This is done by using the general formula:

$$\begin{aligned} \int_{\ell_1}^{\ell_2} dy \mathcal{I}_{\beta,t}^{(k)}(y) &= \sum_{i=0}^{\min(k,\beta)} \theta(\ell_2 - x_{\beta-i+t_\ell}) \theta(x_{\beta-i+t_\ell+1} - \ell_1) \\ &\times \left[ \prod_{\substack{m=0 \\ m \neq i}}^k \frac{1}{x_\beta - x_{\beta-i+m}} \right] \sum_{n=0}^k \frac{(-1)^n p_\beta^{(k)}(n)}{k - n + 1} \left( \bar{\ell}_2^{k-n+1} - \bar{\ell}_1^{k-n+1} \right), \end{aligned} \quad (122)$$

with  $t(\ell_1) = t(\ell_2) = t_\ell$ , and  $\bar{\ell}_1 = \max(\ell_1, x_{\beta-i+t_\ell})$  and  $\bar{\ell}_2 = \min(\ell_2, x_{\beta-i+t_\ell+1})$ .

## C Cuts on the final-state leptons

In this section we derive explicitly the phase-space reduction factor  $\mathcal{P}$  introduced in Sect. 2.1.1. This factor is defined as:

$$\mathcal{P}(Q, y, q_T) = \mathcal{P}(q) = \frac{\int_{\text{fid. reg.}} d^4 p_1 d^4 p_2 \delta(p_1^2) \delta(p_2^2) \theta(p_{1,0}) \theta(p_{2,0}) \delta^{(4)}(p_1 + p_2 - q) g_{\mu\nu} L^{\mu\nu}(p_1, p_2)}{\int d^4 p_1 d^4 p_2 \delta(p_1^2) \delta(p_2^2) \theta(p_{1,0}) \theta(p_{2,0}) \delta^{(4)}(p_1 + p_2 - q) g_{\mu\nu} L^{\mu\nu}(p_1, p_2)}, \quad (123)$$

where  $p_1$  and  $p_2$  are the four-momenta of the outgoing leptons and  $L^{\mu\nu}$  is the leptonic tensor that, assuming massless leptons, reads:

$$L^{\mu\nu}(p_1, p_2) = 4(p_1^\mu p_2^\nu + p_2^\mu p_1^\nu - g^{\mu\nu} p_1 p_2), \quad (124)$$

so that:

$$g_{\mu\nu} L^{\mu\nu}(p_1, p_2) = -8(p_1 p_2) = -4(p_1 + p_2)^2. \quad (125)$$

In the last step we have used the on-shell-ness of the leptons ( $p_1^2 = p_2^2 = 0$ ). The integral in the denominator of Eq. (123) is restricted to some *fiducial region*. Finally, we find:

$$\mathcal{P}(q) = \frac{\int_{\text{fid. reg.}} d^4 p_1 d^4 p_2 \delta(p_1^2) \delta(p_2^2) \theta(p_{1,0}) \theta(p_{2,0}) \delta^{(4)}(p_1 + p_2 - q) (p_1 + p_2)^2}{\int d^4 p_1 d^4 p_2 \delta(p_1^2) \delta(p_2^2) \theta(p_{1,0}) \theta(p_{2,0}) \delta^{(4)}(p_1 + p_2 - q) (p_1 + p_2)^2}. \quad (126)$$

The effect of integrating over the fiducial region can be implemented by defining a generalised  $\theta$ -function,  $\Phi(p_1, p_2)$ , that is equal to one inside the fiducial region and zero outside. This allows one to integrate also the numerator of Eq. (126) over the full phase-space of the two outgoing leptons:

$$\mathcal{P}(q) = \frac{\int d^4 p_1 d^4 p_2 \delta(p_1^2) \delta(p_2^2) \theta(p_{1,0}) \theta(p_{2,0}) \delta^{(4)}(p_1 + p_2 - q) \Phi(p_1, p_2) (p_1 + p_2)^2}{\int d^4 p_1 d^4 p_2 \delta(p_1^2) \delta(p_2^2) \theta(p_{1,0}) \theta(p_{2,0}) \delta^{(4)}(p_1 + p_2 - q) (p_1 + p_2)^2}. \quad (127)$$

Now we can integrate over one of the outgoing momenta, say  $p_2$ , exploiting the momentum-conservation  $\delta$ -function both in the numerator and in the denominator. Specifically, the numerator of Eq. (127) gives:

$$\int d^4 p_1 d^4 p_2 \delta(p_1^2) \delta(p_2^2) \theta(p_{1,0}) \theta(p_{2,0}) \delta^{(4)}(p_1 + p_2 - q) \Phi(p_1, p_2) (p_1 + p_2)^2 = \quad (128)$$

$$Q^2 \int d^4 p_1 \delta(p_1^2) \delta((q - p_1)^2) \theta(p_{1,0}) \theta(q_0 - p_{1,0}) \Phi(p_1, q - p_1),$$

and likewise in the denominator setting  $\Phi(p_1, p_2) = 1$ . Finally, renaming  $p_1 = p$ , the phase-space reduction factor reads:

$$\mathcal{P}(q) = \frac{\int d^4 p \delta(p^2) \delta((q - p)^2) \theta(p_0) \theta(q_0 - p_0) \Phi(p, q - p)}{\int d^4 p \delta(p^2) \delta((q - p)^2) \theta(p_0) \theta(q_0 - p_0)}. \quad (129)$$

The  $\delta$ -functions can now be used to constrain two of the four components of the momentum  $p$ . The first,  $\delta(p_0^2)$ , is usually used to set the first component of  $p$ , the energy, to the on-shell value. Since the leptons are assumed to be massless, this produces:

$$\int d^4 p \delta(p^2) \theta(p_0) = \int d^4 p \delta(E^2 - |\mathbf{p}|^2) \theta(E) = \int \frac{dE d^3 \mathbf{p}}{2|\mathbf{p}|} \delta(E - |\mathbf{p}|) = \int \frac{d^3 \mathbf{p}}{2|\mathbf{p}|}. \quad (130)$$

Of course, the four-momentum  $p$  appearing in the rest of the integrand has to be set on shell ( $E = |\mathbf{p}|$ ). Now we express the three-dimensional measure  $d^3\mathbf{p}$  in spherical coordinates as:

$$d^3\mathbf{p} = |\mathbf{p}|^2 d|\mathbf{p}| d(\cos\theta) d\phi. \quad (131)$$

Then we make a change of variable from  $(|\mathbf{p}|, \cos\theta)$  to  $(|\mathbf{p}_T|, \eta)$ : the second set of variables are exactly those on which kinematic cuts are imposed. We do so by knowing that:

$$\begin{cases} |\mathbf{p}| = |\mathbf{p}_T| \cosh \eta, \\ \cos\theta = \tanh \eta. \end{cases} \quad (132)$$

This leads to:

$$\int \frac{d^3\mathbf{p}}{2|\mathbf{p}|} = \frac{1}{2} \int |\mathbf{p}| d|\mathbf{p}| d(\cos\theta) d\phi = \frac{1}{2} \int |\mathbf{p}_T| d|\mathbf{p}_T| d\eta d\phi = \frac{1}{2} \int d^2\mathbf{p}_T d\eta. \quad (133)$$

Now we consider the second  $\delta$ -function:

$$\frac{1}{2} \int d^2\mathbf{p}_T d\eta \delta((q-p)^2) \theta(q_0 - p_0) = \frac{1}{2} \int_{-\infty}^{\infty} d\eta \int_0^{2\pi} d\phi \int_0^{\infty} |\mathbf{p}_T| d|\mathbf{p}_T| \delta(Q^2 - 2p \cdot q) \theta(q_0 - p_0), \quad (134)$$

being  $q^2 = Q^2$  and  $p^2 = 0$ . It is convenient to express the four-vector  $q$  in terms of  $Q$ ,  $y$ , and  $\mathbf{q}_T$ :

$$q = (M \cosh y, \mathbf{q}_T, M \sinh y). \quad (135)$$

with  $M = \sqrt{Q^2 + |\mathbf{q}_T|^2}$ . While:

$$p = (|\mathbf{p}_T| \cosh \eta, \mathbf{p}_T, |\mathbf{p}_T| \sinh \eta), \quad (136)$$

so that:

$$p \cdot q = |\mathbf{p}_T| M (\cosh \eta \cosh y - \sinh \eta \sinh y) - \mathbf{p}_T \cdot \mathbf{q}_T = |\mathbf{p}_T| M \cosh(\eta - y) - \mathbf{p}_T \cdot \mathbf{q}_T. \quad (137)$$

We can now assume that the two-dimensional vector  $\mathbf{q}_T$  is aligned with the  $x$  axis so that  $\mathbf{p}_T \cdot \mathbf{q}_T = |\mathbf{p}_T| |\mathbf{q}_T| \cos \phi$ <sup>(8)</sup>. Therefore, the argument of the  $\delta$ -function in Eq. (134) becomes:

$$f(|\mathbf{p}_T|, \eta, \phi) = Q^2 - 2|\mathbf{p}_T| [M \cosh(\eta - y) - |\mathbf{q}_T| \cos \phi]. \quad (138)$$

and that of the  $\vartheta$ -function  $M \cosh y - |\mathbf{p}_T| \cosh \eta$ . It thus appears convenient to integrate Eq. (134) over  $|\mathbf{p}_T|$  first:

$$\frac{1}{2} \int_0^{\infty} |\mathbf{p}_T| d|\mathbf{p}_T| \delta(Q^2 - 2p \cdot q) \theta(q_0 - p_0) = \frac{\bar{p}_T^2}{2Q^2} \vartheta(M \cosh y - \bar{p}_T \cosh \eta) = \frac{\bar{p}_T^2}{2Q^2}, \quad (139)$$

with<sup>(9)</sup>:

$$\bar{p}_T(\cos \phi) = \frac{Q^2}{2[M \cosh(\eta - y) - |\mathbf{q}_T| \cos \phi]} = \frac{Q^2}{2|\mathbf{q}_T| \left[ \frac{M \cosh(\eta - y)}{|\mathbf{q}_T|} - \cos \phi \right]}. \quad (140)$$

Now we turn to consider the integral in  $d\phi$ . To this end, the following relations are useful:

$$\int_0^{2\pi} d\phi f(\cos \phi) = \int_{-1}^1 \frac{dx}{\sqrt{1-x^2}} [f(x) + f(-x)]. \quad (141)$$

and:

$$\int \frac{dx}{(a \pm x)^2 \sqrt{1-x^2}} = \frac{\sqrt{1-x^2}}{(a^2-1)(x \pm a)} \pm \frac{a}{(a^2-1)^{3/2}} \tan^{-1} \left( \frac{1 \pm ax}{\sqrt{a^2-1} \sqrt{1-x^2}} \right). \quad (142)$$

<sup>(8)</sup>In the general case in which  $\mathbf{q}_T$  forms an angle  $\beta$  with the  $x$  axis, the scalar product would result in  $|\mathbf{p}_T| |\mathbf{q}_T| \cos(\phi - \beta)$ . However, the angle  $\beta$  could always be reabsorbed in a redefinition of the integration angle  $\phi$  in Eq. (134).

<sup>(9)</sup>Notice that the  $\vartheta$ -function has no effect. I have verified it numerically but I cannot see it analytically.

The last integral is such that:

$$\int_{-1}^1 \frac{dx}{(a \pm x)^2 \sqrt{1-x^2}} = \frac{\pi a}{(a^2 - 1)^{3/2}}. \quad (143)$$

We now use Eqs. (141)-(143) to compute:

$$\begin{aligned} & \frac{1}{2Q^2} \int_0^{2\pi} d\phi [\bar{p}_T(\cos \phi)]^2 = \frac{Q^2}{4|\mathbf{q}_T|^2} \int_0^{2\pi} \frac{d\phi}{\left[ \frac{M \cosh(\eta-y)}{|\mathbf{q}_T|} - \cos \phi \right]^2} \\ &= \frac{Q^2}{8|\mathbf{q}_T|^2} \int_{-1}^1 \frac{dx}{\sqrt{1-x^2}} \left[ \frac{1}{\left( \frac{M \cosh(\eta-y)}{|\mathbf{q}_T|} - x \right)^2} + \frac{1}{\left( \frac{M \cosh(\eta-y)}{|\mathbf{q}_T|} + x \right)^2} \right] \\ &= \frac{Q^2}{8} \left\{ \frac{|\mathbf{q}_T|^2 x \sqrt{1-x^2}}{(M^2 \cosh^2(\eta-y) - |\mathbf{q}_T|^2)(x^2 |\mathbf{q}_T|^2 - M^2 \cosh^2(\eta-y))} \right. \\ &\quad - \frac{M \cosh(\eta-y)}{(M^2 \cosh^2(\eta-y) - |\mathbf{q}_T|^2)^{3/2}} \left[ \tan^{-1} \left( \frac{|\mathbf{q}_T| - x M \cosh(\eta-y)}{\sqrt{(M^2 \cosh^2(\eta-y) - |\mathbf{q}_T|^2) \sqrt{1-x^2}}} \right) \right. \\ &\quad \left. \left. - \tan^{-1} \left( \frac{|\mathbf{q}_T| + x M \cosh(\eta-y)}{\sqrt{(M^2 \cosh^2(\eta-y) - |\mathbf{q}_T|^2) \sqrt{1-x^2}}} \right) \right] \right\}_{-1}^1 \\ &= \frac{\pi Q^2 M \cosh(\eta-y)}{4(M^2 \cosh^2(\eta-y) - |\mathbf{q}_T|^2)^{3/2}} \end{aligned} \quad (144)$$

We can go further and solve also the integral in  $\eta$ :

$$\begin{aligned} & \int d^4 p \delta(p^2) \delta((q-p)^2) \theta(p_0) \theta(q_0 - p_0) = \int_{-\infty}^{\infty} d\eta \frac{\pi Q^2 M \cosh(\eta-y)}{4(M^2 \cosh^2(\eta-y) - |\mathbf{q}_T|^2)^{3/2}} = \\ & \frac{\pi}{4} \frac{Q^2}{M^2} \int_{-\infty}^{\infty} \frac{d(\sinh \eta)}{\left( \sinh^2(\eta-y) + \frac{Q^2}{M^2} \right)^{3/2}} = \frac{\pi}{4} \frac{Q^2}{M^2} \left[ \frac{M^2}{Q^2} \frac{\sinh \eta}{\sqrt{\sinh^2 \eta + \frac{Q^2}{M^2}}} \right]_{-\infty}^{\infty} = \frac{\pi}{2}. \end{aligned} \quad (145)$$

Remarkably, this result gives us the denominator of Eq. (129). We now need to compute the numerator by inserting the appropriate function  $\Phi$ . In our case, the kinematic cuts are identical for the outgoing leptons and read:

$$\eta_{\min} < \eta_{1(2)} < \eta_{\max} \quad \text{and} \quad |\mathbf{p}_{T,1(2)}| > p_{T,\min}. \quad (146)$$

Therefore, the function  $\Phi$  factorises into two identical functions as:

$$\Phi(p_1, p_2) = \Theta(p_1) \Theta(p_2), \quad (147)$$

with:

$$\Theta(p) = \vartheta(\eta - \eta_{\min}) \vartheta(\eta_{\max} - \eta) \vartheta(|\mathbf{p}_T| - p_{T,\min}). \quad (148)$$

Regerring to Eq. (129), and considering that:

$$q - p = (M \cosh y - |\mathbf{p}_T| \cosh \eta, \mathbf{q}_T - \mathbf{p}_T, M \sinh y - |\mathbf{p}_T| \sinh \eta). \quad (149)$$

we thus have:

$$\begin{aligned}
\Phi(p, q-p) &= \Theta(p)\Theta(q-p) = \\
&\vartheta(\eta - \eta_{\min})\vartheta(\eta_{\max} - \eta) \times \\
&\vartheta(|\mathbf{p}_T| - p_{T,\min}) \times \\
&\vartheta\left(\frac{1}{2} \ln\left(\frac{M \cosh y - |\mathbf{p}_T| \cosh \eta + M \sinh y - |\mathbf{p}_T| \sinh \eta}{M \cosh y - |\mathbf{p}_T| \cosh \eta - M \sinh y + |\mathbf{p}_T| \sinh \eta}\right) - \eta_{\min}\right) \times \\
&\vartheta\left(\eta_{\max} - \frac{1}{2} \ln\left(\frac{M \cosh y - |\mathbf{p}_T| \cosh \eta + M \sinh y - |\mathbf{p}_T| \sinh \eta}{M \cosh y - |\mathbf{p}_T| \cosh \eta - M \sinh y + |\mathbf{p}_T| \sinh \eta}\right)\right) \times \\
&\vartheta(|\mathbf{q}_T - \mathbf{p}_T| - p_{T,\min}) = \\
1) : &\quad \vartheta(\eta - \eta_{\min}) \times \vartheta(\eta_{\max} - \eta) \times \\
2) : &\quad \vartheta(\bar{p}_T - p_{T,\min}) \times \\
3) : &\quad \vartheta\left(\frac{1}{2} \ln\left(\frac{Me^y - \bar{p}_T e^\eta}{Me^{-y} - \bar{p}_T e^{-\eta}}\right) - \eta_{\min}\right) \times \vartheta\left(\eta_{\max} - \frac{1}{2} \ln\left(\frac{Me^y - \bar{p}_T e^\eta}{Me^{-y} - \bar{p}_T e^{-\eta}}\right)\right) \times \\
4) : &\quad \vartheta(\sqrt{|\mathbf{q}_T|^2 + \bar{p}_T^2 - 2|\mathbf{q}_T|\bar{p}_T \cos \phi} - p_{T,\min}),
\end{aligned} \tag{150}$$

where in the last step we have replaced  $|\mathbf{p}_T|$  with  $\bar{p}_T$  defined Eq. (140). Now the question is identifying the integration domain defined by  $\Phi(p, q-p)$  on the  $(\eta, \cos \phi)$ -plane. Since the  $\theta$ -functions in Eq. (129) will be used inside a double nested integral over  $x = \cos \phi$  first and  $\eta$  second, it is convenient to rewrite the function  $\Phi(p, q-p)$  in Eq. (150) as follows:

$$\begin{aligned}
\Phi(p, q-p) &= \vartheta(\eta - \eta_{\min}) \times \vartheta(\eta_{\max} - \eta) \\
&\times \vartheta(x - f^{(2)}(\eta, p_{T,\min})) \\
&\times \vartheta(f^{(3)}(\eta, \eta_{\min}) - x) \times \vartheta(f^{(3)}(\eta, \eta_{\max}) - x) \\
&\times \vartheta(f^{(4)}(\eta, p_{T,\min}) - x),
\end{aligned} \tag{151}$$

with:

$$\begin{aligned}
f^{(2)}(\eta, p_{T,\text{cut}}) &= \frac{2Mp_{T,\min} \cosh(\eta - y) - Q^2}{2p_{T,\text{cut}}|\mathbf{q}_T|}, \\
f^{(3)}(\eta, \eta_{\text{cut}}) &= \frac{M \cosh(\eta - y)}{|\mathbf{q}_T|} - \frac{Q^2 (\sinh(\eta - y) \coth(y - \eta_{\text{cut}}) + \cosh(\eta - y))}{2|\mathbf{q}_T|M}, \\
f^{(4)}(\eta, p_{T,\text{cut}}) &= \frac{M \cosh(\eta - y)(Q^2 - 2p_{T,\text{cut}}^2 + 2|\mathbf{q}_T|^2) - Q^2 \sqrt{M^2 \sinh^2(\eta - y) + p_{T,\min}^2}}{2|\mathbf{q}_T| (M^2 - p_{T,\min}^2)}.
\end{aligned} \tag{152}$$

Considering that  $1 \leq \cos \phi \leq 1$ , the integration domain is limited to this region. Therefore, Eq. (151)



Figure 1: The red area indicates the integration domain of the numerator in of the phase-space reduction factor Eq. (129) for  $p_{T,\min} = 20$  GeV and  $-\eta_{\min} = \eta_{\max} = 2.4$  at  $Q = 91$  GeV,  $|\mathbf{q}_T| = 10$  GeV and  $y = 1$ .

can be written in an even more convenient way as:

$$\begin{aligned}
\Phi(p, q - p) &= \vartheta(\eta - \eta_{\min})\vartheta(\eta_{\max} - \eta) \\
&\times \vartheta(x - \max[f^{(2)}(\eta, p_{T,\min}), -1]) \\
&\times \vartheta(\min[f^{(3)}(\eta, \eta_{\min}), f^{(3)}(\eta, \eta_{\max}), f^{(4)}(\eta, p_{T,\min}), 1] - x)
\end{aligned} \tag{153}$$

such that a double integral over  $\eta$  and  $x$  would read:

$$\int_{-\infty}^{\infty} d\eta \int_{-1}^1 dx \Phi(p, q - p) \dots = \int_{\eta_{\min}}^{\eta_{\max}} d\eta \vartheta(x_2(\eta) - x_1(\eta)) \int_{x_1(\eta)}^{x_2(\eta)} dx \dots \tag{154}$$

with:

$$x_1(\eta) = \max[f^{(2)}(\eta, p_{T,\min}), -1] \tag{155}$$

and:

$$x_2(\eta) = \min[f^{(3)}(\eta, \eta_{\min}), f^{(3)}(\eta, \eta_{\max}), f^{(4)}(\eta, p_{T,\min}), 1]. \tag{156}$$

As an example, Fig. 1 shows the integration domain of the numerator in of the phase-space reduction factor Eq. (129) for  $p_{T,\min} = 20$  GeV and  $-\eta_{\min} = \eta_{\max} = 2.4$  at  $Q = 91$  GeV,  $|\mathbf{q}_T| = 10$  GeV and  $y = 1$ . The gray band corresponds to the region  $1 \leq \cos \phi \leq 1$ . The  $\theta$ -function 1) in Eq. (150) limits the region to the vertical strip defined by  $\eta_{\min} < \eta < \eta_{\max}$  (black vertical lines), the  $\theta$ -function 2) gives the red lines, the  $\theta$ -functions 3) the blue lines, and the  $\theta$ -function 4) the green lines.

Gathering all pieces, the final expression for the phase-space reduction factor reads:

$$\mathcal{P}(Q, y, q_T) = \int_{\eta_{\min}}^{\eta_{\max}} d\eta \vartheta(x_2(\eta) - x_1(\eta)) [F(x_2(\eta), \eta) - F(x_1(\eta), \eta)] \tag{157}$$

with:

$$\begin{aligned}
F(x, \eta) = & \frac{1}{4\pi} \frac{Q^2}{E_q^2 - q_T^2} \left\{ \frac{q_T^2 x \sqrt{1-x^2}}{x^2 q_T^2 - E_q^2} \right. \\
& \left. - \frac{E_q}{\sqrt{E_q^2 - q_T^2}} \left[ \tan^{-1} \left( \frac{q_T - x E_q}{\sqrt{E_q^2 - q_T^2} \sqrt{1-x^2}} \right) - \tan^{-1} \left( \frac{q_T + x E_q}{\sqrt{E_q^2 - q_T^2} \sqrt{1-x^2}} \right) \right] \right\}
\end{aligned} \tag{158}$$

where we have defined  $E_q = M \cosh(\eta - y)$  and  $q_T = |\mathbf{q}_T|$ .

Let us consider the case  $y = q_T = 0$ . For simplicity, we also take  $\eta_{\min} = -\eta_{\max}$ . In these conditions, Eq. (158) reduces to:

$$F(x, \eta) = \frac{1}{4\pi} \frac{1}{\cosh^2(\eta)} \left[ \tan^{-1} \left( \frac{x}{\sqrt{1-x^2}} \right) - \tan^{-1} \left( -\frac{x}{\sqrt{1-x^2}} \right) \right]. \tag{159}$$

As evident from Eq. (152), for  $q_T = 0$  all functions  $f^{(2)}$ ,  $f^{(3)}$ , and  $f^{(4)}$  diverge. The relevant question, though, is whether they go to plus or minus infinity depending on the value of  $Q$ . Of course,  $q_T$  will tend to zero positively so we find:

$$\begin{aligned}
f^{(2)}(\eta, p_{T,\min}) & \rightarrow \infty \times \text{sign}[2p_{T,\min} \cosh(\eta) - Q], \\
f^{(3)}(\eta, \eta_{\min} = -\eta_{\max}) & \rightarrow +\infty \\
f^{(3)}(\eta, \eta_{\max}) & \rightarrow -\infty, \\
f^{(4)}(\eta, p_{T,\min}) & \rightarrow \infty \times \text{sign} \left[ \frac{\cosh(\eta)(Q^2 - 2p_{T,\min}^2) - Q\sqrt{Q^2 \sinh^2(\eta) + p_{T,\min}^2}}{Q^2 - p_{T,\min}^2} \right],
\end{aligned} \tag{160}$$

Therefore,  $f^{(3)}$  never actually contributes. In addition, for the  $\theta$ -function in Eq. (157) to be different from zero, we need  $f^{(2)}(\eta) \rightarrow -\infty$  and  $f^{(3)}(\eta) \rightarrow \infty$ . These both translate into  $Q \geq 2p_{T,\min} \cosh(\eta)$ . This inequality is satisfied only if  $Q \geq 2p_{T,\min}$  for:

$$-\bar{\eta} \leq \eta \leq \bar{\eta} \quad \text{with} \quad \bar{\eta} = \cosh^{-1} \left( \frac{Q}{2p_{T,\min}} \right). \tag{161}$$

Therefore, the phase-space reduction factor eventually becomes:

$$\begin{aligned}
\mathcal{P}(Q, 0, 0) &= \frac{1}{2} \vartheta(Q - 2p_{T,\min}) \int_{-\eta_{\max}}^{\eta_{\max}} \frac{d\eta}{\cosh^2 \eta} \vartheta(\eta + \bar{\eta}) \vartheta(\bar{\eta} - \eta) \\
&= \vartheta(Q - 2p_{T,\min}) \tanh(\max[\eta_{\max}, \bar{\eta}]).
\end{aligned} \tag{162}$$

This result can be written more explicitly as:

$$\mathcal{P}(Q, 0, 0) = \begin{cases} 0 & Q < 2p_{T,\min}, \\ \tanh(\bar{\eta}) = \left( 1 + \frac{2p_{T,\min}}{Q} \right) \sqrt{1 - \frac{4p_{T,\min}}{Q + 2p_{T,\min}}} & 2p_{T,\min} \leq Q < 2p_{T,\min} \cosh \eta_{\max}, \\ \tanh(\eta_{\max}) & Q \geq 2p_{T,\min} \cosh \eta_{\max}. \end{cases} \tag{163}$$

This differs from Eq. (24) of Ref. [1]. Despite the three different regions coincide, the behavior of the phase-space reduction factor for all regions but for  $Q < 2p_{T,\min}$  is different. In favour of our result there is the fact that  $\mathcal{P}(Q, 0, 0)$  in Eq. (163) is continuous at  $Q = 2p_{T,\min} \cosh \eta_{\max}$  while that of Ref. [1] is not. In addition, when setting  $p_{T,\min} = 0$  and  $\eta_{\max} = \infty$ , *i.e.* no cuts, our result tends to



$\mathcal{P}(Q, 0, 0) = \tanh(\infty) = 1$ , as it should. While the result in Eq. (24) of Ref. [1] actually diverges in this limit.

The integrand of Eq. (157), due to the behaviour of  $x_1$  and  $x_2$  as functions of  $\eta$ , a piecewise function. Therefore, its numerical integration is problematic in that quadrature algorithms assume the integrand be continuous over the integration range. The solution is to identify the discontinuity points and integrate the function separately over the resulting ranges. However, the complexity of the integration region (*e.g.* see Fig. 1) makes the analytical identification of the discontinuity points very hard to achieve.

### C.1 Contracting the leptonic tensor with $g_{\perp}^{\mu\nu}$

The calculation done in the previous section holds when contracting the leptonic tensor  $L_{\mu\nu}$  with the metric tensor  $g^{\mu\nu}$  associated with the Lorentz structure of the hadronic tensor. However, at small values of  $|\mathbf{q}_T|$ , the leading-power Lorentz structure that one needs to multiply the leptonic tensor for is:

$$g_{\perp}^{\mu\nu} = g^{\mu\nu} + z^{\mu}z^{\nu} - t^{\mu}t^{\nu} \quad (164)$$

where the vectors  $z^{\mu}$  and  $t^{\mu}$  in the Collins-Soper (CS) frame are defined as:

$$\begin{aligned} z^{\mu} &= (\sinh y, \mathbf{0}, \cosh y), \\ t^{\mu} &= \frac{q^{\mu}}{Q}, \end{aligned} \quad (165)$$

and they are such that  $z^2 = -1$ ,  $t^2 = 1$  and  $zq = 0$ . if we use the on-shell-ness of  $p_1$  and  $p_2$  ( $p_1^2 = p_2^2 = 0$ ) and the momentum conservation ( $p \equiv p_1$ ,  $p_2 = q - p$ ), we find that  $t^{\mu}t^{\nu}L_{\mu\nu} = 0$  and the quantity above reduces to:

$$L_{\perp} = g_{\perp}^{\mu\nu}L_{\mu\nu} = 4 \left[ \frac{1}{2}q^2 + 2(zp)^2 \right] = 2Q^2 \left[ 1 + 4\sinh^2(y - \eta) \frac{|\mathbf{p}_T|^2}{Q^2} \right]. \quad (166)$$

Therefore, we need to introduce this factor in both the numerator and the denominator of Eq. (129). Following the same steps of the previous section, up to a factor  $2Q^2$ , this leads us to replace the integral in Eq. (139) with<sup>(10)</sup>:

$$\frac{1}{2} \int_0^{\infty} |\mathbf{p}_T| \left[ 1 + 4\sinh^2(y - \eta) \frac{|\mathbf{p}_T|^2}{Q^2} \right] d|\mathbf{p}_T| \delta(Q^2 - 2p \cdot q) = \frac{2\bar{p}_T^2}{Q^2} + 2\sinh^2(y - \eta) \frac{\bar{p}_T^4}{Q^4}. \quad (167)$$

We can still use Eq. (142) for the first term in the r.h.s. of the equation above. For the second, instead we need to use:

$$\begin{aligned} \int \frac{dx}{(a \pm x)^4 \sqrt{1 - x^2}} &= \frac{\sqrt{1 - x^2} [(11a^2 + 4)x^2 \pm 3a(9a^2 + 1)x + (18a^4 - 5a^2 + 2)]}{6(a^2 - 1)^3(x \pm a)^3} \\ &\pm \frac{a(2a^2 + 3)}{2(a^2 - 1)^{7/2}} \tan^{-1} \left( \frac{1 \pm ax}{\sqrt{a^2 - 1}\sqrt{1 - x^2}} \right), \end{aligned} \quad (168)$$

that is such that:

$$\int_{-1}^1 \frac{dx}{(a \pm x)^4 \sqrt{1 - x^2}} = \frac{\pi a(2a^2 + 3)}{2(a^2 - 1)^{7/2}}. \quad (169)$$

In our particular case, the integrand we are considering is the second term in the r.h.s. term of Eq. (167):

$$\begin{aligned} \frac{2\sinh^2(y - \eta)}{Q^4} \int_{-1}^1 d(\cos \phi) \bar{p}_T^4(\cos \phi) &= \\ \frac{Q^4}{8q_T^4} \sinh^2(y - \eta) \int_{-1}^1 \frac{dx}{\sqrt{1 - x^2}} \left[ \frac{1}{(a + x)^4} + \frac{1}{(a - x)^4} \right] &= \frac{\pi Q^4}{8q_T^4} \sinh^2(y - \eta) \frac{a(2a^2 + 3)}{(a^2 - 1)^{7/2}}. \end{aligned} \quad (170)$$

<sup>10</sup>We removed the  $\theta$ -function as we know it does not have any effect.

with:

$$a = \frac{M}{q_T} \cosh(y - \eta). \quad (171)$$

Now we need to integrate Eq. (170) over  $\eta$ :

$$\frac{\pi Q^4}{8q_T^4} \int_{-\infty}^{\infty} d\eta \sinh^2(y - \eta) \frac{a(2a^2 + 3)}{(a^2 - 1)^{7/2}}. \quad (172)$$

If we make the following change of variable in the integral above:

$$z = \frac{M}{q_T} \sinh(y - \eta) \quad (173)$$

such that:

$$a^2 = z^2 + \frac{M^2}{q_T^2} \quad \text{and} \quad dz = -ad\eta, \quad (174)$$

the integral above becomes:

$$\frac{\pi Q^4}{4M^2 q_T^2} \int_{-\infty}^{\infty} dz \frac{z^2 \left( z^2 + \frac{M^2}{q_T^2} + \frac{3}{2} \right)}{\left( z^2 + \frac{M^2}{q_T^2} - 1 \right)^{7/2}} = \frac{\pi}{6}. \quad (175)$$

Putting this result together with Eq. (145) and taking into account the factor  $2Q^2$  in Eq. (166), we find that:

$$\int d^4 p \delta(p^2) \delta((q - p)^2) \theta(p_0) \theta(q_0 - p_0) L_{\perp} = \frac{4\pi}{3} Q^2. \quad (176)$$

This result agrees with Eq. (2.38) of Ref. [1], up to a factor four. This provides the denominator of the phase-space-reduction factor  $\mathcal{P}$ . The structure of  $\mathcal{P}$  will be exactly like that in Eq. (157), the only thing we need to do is to identify the correct function  $F(x, \eta)$ . To this end, we need to make the following replacement for the function  $F$  given in Eq. (158) with:

$$F(x, \eta) \rightarrow \bar{F}(x, \eta) = \frac{3}{4} F(x, \eta) + \frac{1}{4} G(x, \eta), \quad (177)$$

where:

$$\begin{aligned} G(x, \eta) &= \frac{1}{16\pi} \sinh^2(y - \eta) \frac{Q^4}{(E_q^2 - q_T^2)^3} \left\{ \sqrt{1 - x^2} q_T \right. \\ &\times \left[ \frac{(11E_q^2 q_T^2 + 4q_T^4)x^2 + 3E_q q_T (9E_q^2 + q_T^2)x + (18E_q^4 - 5E_q^2 q_T^2 + 2q_T^4)}{(xq_T + E_q)^3} \right. \\ &+ \left. \frac{(11E_q^2 q_T^2 + 4q_T^4)x^2 - 3E_q q_T (9E_q^2 + q_T^2)x + (18E_q^4 - 5E_q^2 q_T^2 + 2q_T^4)}{(xq_T - E_q)^3} \right] \\ &- \left. \frac{6E_q (2E_q^2 + 3q_T^2)}{\sqrt{E_q^2 - q_T^2}} \left[ \tan^{-1} \left( \frac{q_T - xE_q}{\sqrt{E_q^2 - q_T^2} \sqrt{1 - x^2}} \right) - \tan^{-1} \left( \frac{q_T + xE_q}{\sqrt{E_q^2 - q_T^2} \sqrt{1 - x^2}} \right) \right] \right\}. \end{aligned} \quad (178)$$

Finally, combining the functions  $F$  and  $G$  given in Eqs. (158) and (178), respectively, according to Eq. (177) to obtain  $\bar{F}$ , and replacing  $F$  with  $\bar{F}$  in Eq. (157) gives the phase-space-reduction factor  $\mathcal{P}(Q, y, q_T)$  when the leptonic tensor  $L_{\mu\nu}$  is contracted with the transverse metrics  $g_{\perp}^{\mu\nu}$ .



Figure 2: Same as Fig. 1 for the asymmetric rapidity cut  $2 < \eta < 4.5$  at  $y = 3$ .

As a final check, it is interesting to compute  $\mathcal{P}$  when  $y = q_T = 0$ , again assuming  $\eta_{\min} = -\eta_{\max}$ . In this limit  $F$  reduces to the expression in Eq. (159), while  $G$  becomes:

$$G(x, \eta) = \frac{3}{4\pi} \frac{\sinh^2(\eta)}{\cosh^4(\eta)} \left\{ \left[ \tan^{-1} \left( \frac{x}{\sqrt{1-x^2}} \right) - \tan^{-1} \left( -\frac{x}{\sqrt{1-x^2}} \right) \right] \right\}, \quad (179)$$

such that:

$$\begin{aligned} \mathcal{P}(Q, 0, 0) &= \frac{3}{8} \vartheta(Q - 2p_{T,\min}) \int_{-\eta_{\max}}^{\eta_{\max}} d\eta \left[ \frac{\cosh^2(\eta) + \sinh^2(\eta)}{\cosh^4(\eta)} \right] \vartheta(\eta + \bar{\eta}) \vartheta(\bar{\eta} - \eta) \\ &= \vartheta(Q - 2p_{T,\min}) \tanh(\max[\eta_{\max}, \bar{\eta}]) \left[ 1 - \frac{1}{4 \cosh^2(\max[\eta_{\max}, \bar{\eta}])} \right], \end{aligned} \quad (180)$$

with  $\bar{\eta}$  defined in Eq. (161). The relation above can be written more explicitly as:

$$\mathcal{P}(Q, 0, 0) = \begin{cases} 0 & Q < 2p_{T,\min}, \\ \tanh(\bar{\eta}) \left[ 1 - \frac{1}{4 \cosh^2(\bar{\eta})} \right] = \left( 1 - \frac{p_{T,\min}^2}{Q^2} \right) \sqrt{1 - \frac{4p_{T,\min}^2}{Q^2}} & 2p_{T,\min} \leq Q < 2p_{T,\min} \cosh \eta_{\max}, \\ \tanh(\eta_{\max}) \left[ 1 - \frac{1}{4 \cosh^2(\eta_{\max})} \right] & Q \geq 2p_{T,\min} \cosh \eta_{\max}. \end{cases} \quad (181)$$

The reason why we kept  $\eta_{\min} \neq -\eta_{\max}$  is that in some cases it may be required to implement an asymmetric cut,  $\eta_{\min} < \eta < \eta_{\max}$ . This is the case, for example, of the LHCb experiment that delivers data only in the forward region ( $2 < \eta < 4.5$ ). As an example, Fig. 2 shows the integration domain of the phase-space reduction factor Eq. (129) for  $p_{T,\min} = 20$  GeV and  $2 < \eta < 4.5$  at  $Q = 91$  GeV,  $|\mathbf{q}_T| = 10$  GeV and  $y = 3$ .

## C.2 Parity-violating contribution

In the presence of cuts on the final-state leptons and for invariant masses around the  $Z$  mass, parity-violating effects arise. As we will show below, these effects integrate to zero when removing the

leptonic cuts. This contribution stems from interference of the antisymmetric contributions to the lepton tensor, proportional to  $p_1^\mu p_2^\nu \epsilon_{\mu\nu\rho\sigma}$ , and the hadronic tensor, proportional to  $\epsilon_\perp^{\mu\nu}$  defined as:

$$\epsilon_\perp^{\mu\nu} \equiv \epsilon^{\mu\nu\rho\sigma} t_\rho z_\sigma, \quad (182)$$

where  $t^\mu$  and  $z^\mu$  are given in Eq. (165). Therefore, the contribution we are after results from the contraction of the following Lorentz structures:

$$L_{\text{PV}} \equiv p_1^\mu p_2^\nu \epsilon_{\mu\nu\rho\sigma} \epsilon_\perp^{\rho\sigma}. \quad (183)$$

After some manipulation, one finds:

$$\begin{aligned} L_{\text{PV}} &= p_1^\mu p_2^\nu \epsilon_{\mu\nu\rho\sigma} \epsilon^{\rho\sigma\alpha\beta} t_\alpha z_\beta = -2p_1^\mu p_2^\nu \delta_\mu^\alpha \delta_\nu^\beta t_\alpha z_\beta \\ &= -2(p_1 t)(p_2 z) = -2(pt)[(qz) - (pz)] = 2(pt)(pz) \\ &= \frac{2|\mathbf{p}_T|^2}{Q} \sinh(y - \eta) [M \cosh(y - \eta) - |\mathbf{q}_T| \cos \phi], \end{aligned} \quad (184)$$

where I have defined  $p_1 \equiv p$  and used the equalities  $p_2 = q - p$ , and  $zq = 0$ . To compute the third line I have used the explicit parameterisation of  $q$  and  $p$  given in Eqs. (135) and (136), respectively. The presence of  $\sinh(y - \eta)$  in Eq. (184) is such that integrating over the full range in the lepton rapidity  $\eta$  nullifies this contribution:

$$\int_{-\infty}^{\infty} d\eta L_{\text{PV}} = 0. \quad (185)$$

Therefore, it turns out that, for observables inclusive in the lepton phase space, the parity violating term does not give any contribution. Conversely, the presence of cuts on the final-state leptons may prevent Eq. (185) from being satisfied leaving a residual contribution. In order to quantify this effect, we take the same steps performed in the previous sections to integrate  $L_{\text{PV}}$  over the fiducial region. As above, we start integrating over the full range in  $|\mathbf{p}_T|$  using the on-shell-ness  $\delta$ -function:

$$\begin{aligned} \int_0^\infty d|\mathbf{p}_T| |\mathbf{p}_T| L_{\text{PV}} &= \frac{\sinh(y - \eta)}{Q} [M \cosh(y - \eta) - |\mathbf{q}_T| \cos \phi] \int_0^\infty d|\mathbf{p}_T| |\mathbf{p}_T|^3 \delta(Q^2 - 2pq) \\ &= \frac{\bar{p}_T^4}{Q^3} \sinh(y - \eta) [M \cosh(y - \eta) - |\mathbf{q}_T| \cos \phi], \end{aligned} \quad (186)$$

with  $\bar{p}_T$  defined in Eq. (140). Now we compute the indefinite integral over  $\cos \phi$ . To do so, we need to use Eq. (141) along with the equality:

$$\int \frac{dx}{(a \pm x)^3 \sqrt{1 - x^2}} = \frac{\sqrt{1 - x^2} [3ax \pm (4a^2 - 1)]}{2(a^2 - 1)^2 (x \pm a)^2} \pm \frac{(2a^2 + 1)}{2(a^2 - 1)^{5/2}} \tan^{-1} \left( \frac{1 \pm ax}{\sqrt{a^2 - 1} \sqrt{1 - x^2}} \right). \quad (187)$$

This allows us to compute the integral<sup>(11)</sup>:

$$\begin{aligned}
H(x, \eta) &= \left( \frac{4\pi Q^2}{3} \right)^{-1} \frac{\sinh(y - \eta)}{Q^3} \left[ M \cosh(y - \eta) \int d(\cos \phi) \bar{p}_T^4(\cos \phi) - |\mathbf{q}_T| \int d(\cos \phi) \cos \phi \bar{p}_T^4(\cos \phi) \right] \\
&= \frac{3Q^3 \sinh(y - \eta)}{64\pi |\mathbf{q}_T|^4} \left[ M \cosh(y - \eta) \int \frac{d(\cos \phi)}{(a - \cos \phi)^4} - |\mathbf{q}_T| \int \frac{\cos \phi d(\cos \phi)}{(a - \cos \phi)^4} \right] \\
&= \frac{3Q^3 \sinh(y - \eta)}{64\pi q_T^3} \int \frac{dx}{\sqrt{1 - x^2}} \left[ \frac{1}{(a - x)^3} + \frac{1}{(a + x)^3} \right] \\
&= \frac{3Q^3 \sinh(y - \eta)}{128\pi q_T^3} \left\{ \frac{\sqrt{1 - x^2}}{(a^2 - 1)^2} \left[ \frac{3ax - (4a^2 - 1)}{(x - a)^2} + \frac{3ax + (4a^2 - 1)}{(x + a)^2} \right] \right. \\
&\quad \left. - \frac{(2a^2 + 1)}{(a^2 - 1)^{5/2}} \left[ \tan^{-1} \left( \frac{1 - ax}{\sqrt{a^2 - 1} \sqrt{1 - x^2}} \right) - \tan^{-1} \left( \frac{1 + ax}{\sqrt{a^2 - 1} \sqrt{1 - x^2}} \right) \right] \right\}
\end{aligned} \tag{188}$$

with  $E_q = M \cosh(\eta - y)$ ,  $q_T = |\mathbf{q}_T|$ , and:

$$a = \frac{E_q}{q_T}, \tag{189}$$

so that:

$$\begin{aligned}
H(x, \eta) &= \frac{3Q^3 \sinh(y - \eta)}{128\pi (E_q^2 - q_T^2)^2} \left\{ \sqrt{1 - x^2} q_T \left[ \frac{3E_q q_T x - (4E_q^2 - q_T^2)}{(x q_T - E_q)^2} + \frac{3E_q q_T x + (4E_q^2 - q_T^2)}{(q_T x + E_q)^2} \right] \right. \\
&\quad \left. - \frac{(2E_q^2 + q_T^2)}{\sqrt{E_q^2 - q_T^2}} \left[ \tan^{-1} \left( \frac{q_T - x E_q}{\sqrt{E_q^2 - q_T^2} \sqrt{1 - x^2}} \right) - \tan^{-1} \left( \frac{q_T + x E_q}{\sqrt{E_q^2 - q_T^2} \sqrt{1 - x^2}} \right) \right] \right\}.
\end{aligned} \tag{190}$$

Finally, using the definition of  $H$  in Eq. (190), one can perform the integral over the fiducial phase space as discussed above in Eq. (157):

$$\mathcal{P}_{\text{PV}}(Q, y, q_T) = \int_{\eta_{\min}}^{\eta_{\max}} d\eta \vartheta(x_2(\eta) - x_1(\eta)) [H(x_2(\eta), \eta) - H(x_1(\eta), \eta)]. \tag{191}$$

This allows one to estimate the impact of the parity-violating contribution to the phase-space reduction factor.

In order to quantify numerically the impact of Eq. (191), Fig. 3 displays the size  $\mathcal{P}_{\text{PV}}$  relative to the parity-conserving phase-space reduction factor as a function of  $y$  for three different values of  $q_T$  at  $Q = M_Z$  and for the following lepton cuts:  $p_{T,\ell} > 20$  GeV and  $-2.4 < \eta_\ell < 2.4$ . It turns out that the size of  $\mathcal{P}_{\text{PV}}$  relative to  $\mathcal{P}$  is never larger than  $2 \times 10^{-6}$ . In addition, the rapid oscillations with  $y$  contribute to suppress even more the integral over realistic bins in  $y$ . One can thus conclude that, for realistic kinematic configurations, the impact of parity violating effects is completely negligible.

We finally notice that also following contraction enters the game in the presence of cuts on the leptonic final state:

$$L_\phi = (z^\mu t^\nu + z^\nu t^\mu) L_{\mu\nu}. \tag{192}$$

We find that:

$$L_\phi = 8(zp) [Q - 2(tp)]. \tag{193}$$

---

<sup>11</sup>The factor  $\left( \frac{4\pi Q^2}{3} \right)^{-1}$  in Eq. (188) corresponds to the full phase-space in integral of  $L_\perp$  in Eq. (176) that provides the natural normalisation.

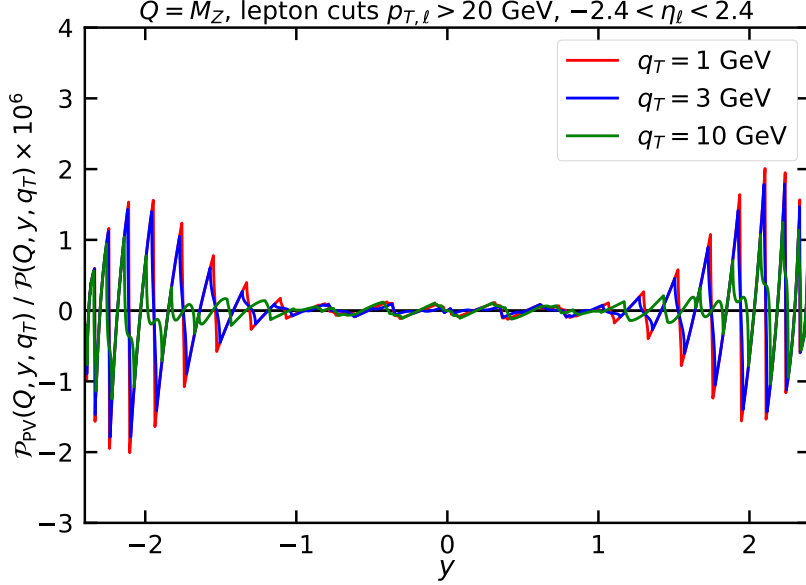


Figure 3: Ratio between the parity-violating phase-space reduction factor  $\mathcal{P}_{\text{PV}}$  in Eq. (191) and the respective parity-conserving factor as a function of the  $Z$  rapidity  $y$  at  $Q = M_Z$  and for three different values of  $q_T$ , with lepton cuts equal to  $p_{T,\ell} > 20$  GeV and  $-2.4 < \eta_\ell < 2.4$ .

Using Eqs. (136) and (165), we have that:

$$(zp) = p_T(\cosh \eta \sinh y - \sinh \eta \cosh y) = p_T \sinh(y - \eta), \quad (194)$$

and:

$$(tp) = \frac{1}{Q} [Mp_T \cosh(y - \eta) - \mathbf{q}_T \cdot \mathbf{p}_T] = \frac{p_T}{Q} [M \cosh(y - \eta) - q_T \cos \phi]. \quad (195)$$

Therefore:

$$L_\phi = 16 \frac{p_T^2}{Q} \sinh(y - \eta) \left[ \frac{Q^2}{2p_T} - M \cosh(y - \eta) + q_T \cos \phi \right] = 16 \left[ \frac{1}{2} p_T Q \sinh(y - \eta) - L_{\text{PV}} \right]. \quad (196)$$

Due to the presence of the overall factor  $\sinh(y - \eta)$ , also this contribution is expected to be subdominant.

## D Differential cross section in the leptonic variables

The calculation of the phase-space reduction factor carried out in the previous section can be used to express the Drell-Yan cross section in Eq. (1) as differential in the kinematic variables of the single leptons. Loosely speaking, this amounts to removing the integral sign in the numerator in Eq. (123) but taking into account kinematic constraints. Using the transverse metric tensor  $g_\perp^{\mu\nu}$ , one finds:

$$d\mathcal{P} = \frac{d^4 p_1 d^4 p_2 \delta(p_1^2) \delta(p_2^2) \theta(p_{1,0}) \theta(p_{2,0}) \delta^{(4)}(p_1 + p_2 - q) L_\perp(p_1, p_2)}{\int d^4 p_1 d^4 p_2 \delta(p_1^2) \delta(p_2^2) \theta(p_{1,0}) \theta(p_{2,0}) \delta^{(4)}(p_1 + p_2 - q) L_\perp(p_1, p_2)}, \quad (197)$$

From Eq. (176), we know the value of the denominator. In the numerator, we can make use of the momentum-conservation and one of the on-shell-ness  $\delta$ -functions. Using the r.h.s. of Eq. (167), but

integrating over  $\phi$  rather than  $|\mathbf{p}_T|$ , leads to:

$$\frac{d\mathcal{P}}{d|\mathbf{p}_T|d\eta} = \frac{3|\mathbf{p}_T|}{4\pi} \left[ 1 + 4 \sinh^2(y - \eta) \frac{|\mathbf{p}_T|^2}{Q^2} \right] \int_0^{2\pi} d\phi \delta(Q^2 - 2|\mathbf{p}_T| [M \cosh(\eta - y) - |\mathbf{q}_T| \cos \phi]), \quad (198)$$

where we have used Eqs. (130)-(134) and Eq. (138). Finally, to perform the integral over  $\phi$  we use Eq. (141) to get:

$$\frac{d\mathcal{P}}{d|\mathbf{p}_T|d\eta} = \frac{3|\mathbf{p}_T|}{2\pi Q^2} \frac{Q^2 + 4|\mathbf{p}_T|^2 \sinh^2(\eta - y)}{\sqrt{4|\mathbf{p}_T|^2 |\mathbf{q}_T|^2 - (2|\mathbf{p}_T| M \cosh(\eta - y) - Q^2)^2}}. \quad (199)$$

Getting rid of the absolute value of the transverse vectors, this allows one to get the Drell-Yan cross section differential in the leptonic variables  $|\mathbf{p}_T|$  and  $\eta$ :

$$\frac{d\sigma}{dQ dy dq_T d\eta dp_T} = \left[ \frac{3p_T^2}{\pi Q^2 M} \frac{\left( \frac{Q^2}{4p_T^2} - 1 \right) + \cosh^2(\eta - y)}{\sqrt{\frac{q_T^2}{M^2} - \left( \cosh(\eta - y) - \frac{Q^2}{2p_T M} \right)^2}} \right] \frac{d\sigma}{dQ dy dq_T}. \quad (200)$$

Due to the square root in the denominator, for fixed values of  $Q$ ,  $q_T$ , and  $y$ , the expression above is defined for values of  $p_T$  and  $\eta$  such that:

$$\frac{Q^2}{2p_T M} - \frac{q_T}{M} < \cosh(\eta - y) < \frac{Q^2}{2p_T M} + \frac{q_T}{M}. \quad (201)$$

In order to focus on the  $p_T$  dependence of the cross section, one may want to integrate of the lepton rapidity  $\eta$ . Using the analogous of Eq. (141) for  $\cosh(\eta)$ :

$$\int_{-\infty}^{\infty} d\eta f(\cosh \eta) = \int_1^{\infty} \frac{dx}{\sqrt{x^2 - 1}} [f(x) + f(-x)], \quad (202)$$

and taking into account the constraint in Eq. (201), one finds:

$$\begin{aligned} \frac{d\sigma}{dQ dy dq_T dp_T} &= \frac{d\sigma}{dQ dy dq_T} \times \\ &\frac{3p_T}{2\pi Q^2} \int_{-\frac{q_T}{M}}^{\frac{q_T}{M}} \frac{dy}{\sqrt{\frac{q_T^2}{M^2} - y^2}} \left( \frac{\left( \frac{Q^2}{4p_T^2} - 1 \right) + \left( y + \frac{Q^2}{2p_T M} \right)^2}{\sqrt{\left( y + \frac{Q^2}{2p_T M} \right)^2 - 1}} + \frac{\left( \frac{Q^2}{4p_T^2} - 1 \right) + \left( y - \frac{Q^2}{2p_T M} \right)^2}{\sqrt{\left( y - \frac{Q^2}{2p_T M} \right)^2 - 1}} \right). \end{aligned} \quad (203)$$

For fixed values of  $Q$ ,  $q_T$ , and  $y$ , the integral above can be solved numerically and plotted as a function of  $p_T$ . The result is shown in Fig. 4.

## E Convolution in transverse-momentum space

The “transverse-momentum” version of Eq. (1) reads:

$$\begin{aligned} \frac{d\sigma}{dQ dy dq_T} &= \frac{16\pi\alpha^2 q_T}{9Q^3} H(Q, \mu) \sum_q C_q(Q) \\ &\times \int d^2\mathbf{k}_{T,1} d^2\mathbf{k}_{T,2} \bar{F}_q(x_1, \mathbf{k}_{T,1}; \mu, \zeta) \bar{F}_{\bar{q}}(x_2, \mathbf{k}_{T,2}; \mu, \zeta) \delta^{(2)}(\mathbf{q}_T - \mathbf{k}_{T,1} - \mathbf{k}_{T,2}), \end{aligned} \quad (204)$$

where, with abuse of notation, we used the same symbol for the distributions  $F$  both in  $k_T$  and  $b_T$  space. We can make use of the  $\delta$ -function to reduce the expression above to:

$$\frac{d\sigma}{dQ dy dq_T} = \frac{16\pi\alpha^2 q_T}{9Q^3} H(Q, \mu) \sum_q C_q(Q) \int d^2\mathbf{k}_T \bar{F}_q(x_1, \mathbf{k}_T; \mu, \zeta) \bar{F}_{\bar{q}}(x_2, \mathbf{q}_T - \mathbf{k}_T; \mu, \zeta). \quad (205)$$

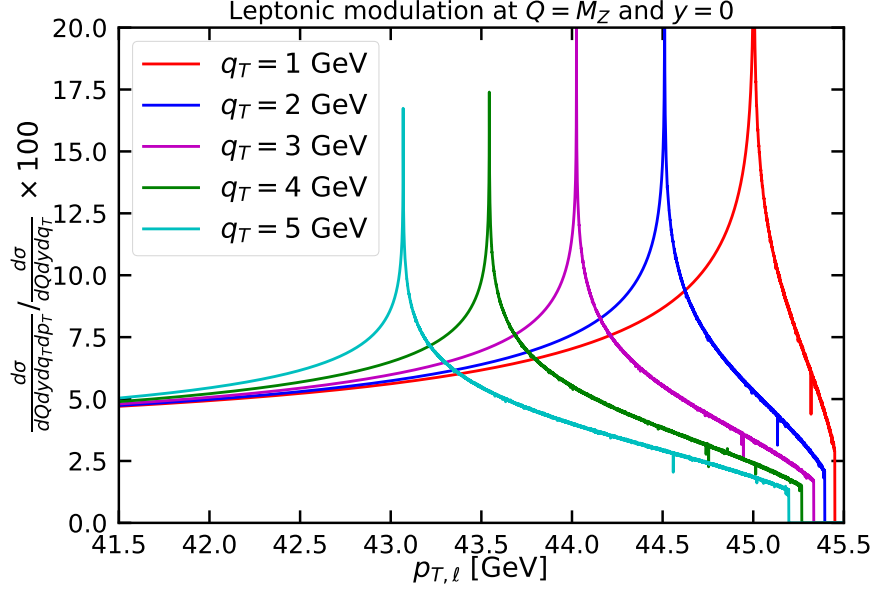


Figure 4: Behaviour of the second line of Eq. (203) at  $Q = M_Z$  and  $y = 0$  as a function of the lepton transverse momentum  $p_{T,\ell}$ .

Since the distributions  $F$  only depend on the absolute value of their argument (be it  $k_T$  or  $b_T$ ), the expression above can be further reduced to:

$$\begin{aligned} \frac{d\sigma}{dQ dy dq_T} &= \frac{16\pi\alpha^2 q_T}{9Q^3} H(Q, \mu) \sum_q C_q(Q) \\ &\times \int_0^\infty dk_T k_T \int_0^{2\pi} d\theta \bar{F}_q(x_1, k_T; \mu, \zeta) \bar{F}_{\bar{q}}(x_2, \sqrt{q_T^2 + k_T^2 - 2q_T k_T \cos \theta}; \mu, \zeta), \end{aligned} \quad (206)$$

where, without loss of generality, we are assuming that the vector  $\mathbf{q}_T$  is directed along the  $x$  axis. Knowing the functions  $F$  in  $k_T$  space, the formula above can be implemented numerically.

## F The $A_0$ coefficient

Using Eq. (5) of Ref. [6], the azimuthal angle  $\theta$  of the (negative) lepton in the Collins-Soper frame can be related to the momenta on the vector boson and of one of the leptons in the laboratory frame as:

$$\cos \theta(\eta, p_T) = \text{sign}(y) \frac{2p_T}{Q} \sinh(y - \eta). \quad (207)$$

This can be related to the coefficient  $A_0$  as [7]:

$$A_0 = 4 - 10 \langle \cos^2 \theta \rangle, \quad (208)$$

where:

$$\langle \cos^2 \theta \rangle \equiv \left[ \int dp_T d\eta \frac{d\sigma}{dQ dy dq_T d\eta dp_T} \right]^{-1} \int dp_T d\eta [\cos \theta(\eta, p_T)]^2 \frac{d\sigma}{dQ dy dq_T d\eta dp_T}. \quad (209)$$

If the integration in both numerator and denominator in the r.h.s. of the quantity above is performed over the full phase space, the result at small  $q_T$  is:

$$\langle \cos^2 \theta \rangle = \int dp_T d\eta [\cos \theta(\eta, p_T)]^2 \frac{d\mathcal{P}}{dp_T d\eta} \quad (210)$$



with the element of phase space  $d\mathcal{P}$  is given in Eq. (199). Therefore, the “QCD dynamics” totally cancels in the ration and one is left with a relatively interesting kinematic factor.

## G Implementing the $\phi^*$ distribution

A physical observable that is particularly useful to probe the intrinsic transverse dynamics of hadrons is the so-called  $\phi^*$  distribution in Drell-Yan production, defined as [4]:

$$\phi^* = \tan\left(\frac{\pi - \Delta\phi}{2}\right) \sin\theta^* = \tan\left(\frac{\pi - \Delta\phi}{2}\right) \sqrt{1 - \tanh^2\left(\frac{\Delta\eta}{2}\right)}, \quad (211)$$

where  $\Delta\phi = \phi_1 - \phi_2$  and  $\Delta\eta = \eta_1 - \eta_2$  are the separation in azimuthal angle and pseudo-rapidity of the two outgoing leptons. The reason why  $\phi^*$  is interesting is that experimental measurements of this quantity reach an extremely high accuracy. It is therefore useful to express the Drell-Yan cross section differential in  $q_T$  into a cross section differential in  $\phi^*$ . This is achieved through the chain rule:

$$\frac{d\sigma}{dQdydq_Td\eta dp_T} = \frac{d\phi^*}{dq_T} \frac{d\sigma}{dQdyd\phi^*d\eta dp_T}. \quad (212)$$

Of course, this requires the knowledge of  $\phi^*$  as a function of  $q_T$  which is what we will work out in the following. The starting point is the four-momentum conservation  $q = p_1 + p_2$ . Taking the absolute value of this relation and using the parameterisations in Eq. (135) for  $q$  and in Eq. (136) for both  $p_1$  and  $p_2$  immediately gives:

$$\cosh\Delta\eta = 1 + \frac{Q^2}{2p_{T1}p_{T2}}. \quad (213)$$

In addition, equating the absolute values of the transverse component ( $|\mathbf{q}_T|^2 = |\mathbf{p}_{T1} + \mathbf{p}_{T2}|^2$ ) leads to:

$$\cos\Delta\phi = \frac{p_{T1}^2 + p_{T2}^2 - q_T^2}{2p_{T1}p_{T2}}. \quad (214)$$

Using Eq. (213) one has:

$$\tanh\left(\frac{\Delta\eta}{2}\right) = \sqrt{\frac{\cosh\Delta\eta - 1}{\cosh\Delta\eta + 1}} = \sqrt{\frac{Q^2}{Q^2 + 4p_{T1}p_{T2}}}, \quad (215)$$

so that:

$$\sin\theta^* = \sqrt{1 - \tanh^2\left(\frac{\Delta\eta}{2}\right)} = \sqrt{\frac{4p_{T1}p_{T2}}{Q^2 + 4p_{T1}p_{T2}}}. \quad (216)$$

On the other hand, using Eq. (214) one finds:

$$\tan\left(\frac{\pi - \Delta\phi}{2}\right) = \sqrt{\frac{1 - \cos(\pi - \Delta\phi)}{1 + \cos(\pi - \Delta\phi)}} = \sqrt{\frac{1 + \cos\Delta\phi}{1 - \cos\Delta\phi}} = \sqrt{\frac{p_{T1}^2 + p_{T2}^2 - q_T^2 + 2p_{T1}p_{T2}}{p_{T1}^2 + p_{T2}^2 - q_T^2 - 2p_{T1}p_{T2}}}. \quad (217)$$

Now let us define  $p_{T1} = p_T$  and  $\eta = \eta_1$  and trade  $p_{T2}$  for  $\cosh(y - \eta)$  using the relation:

$$p_{T2}^2 = M^2 + p_T^2 - 2p_TM \cosh(y - \eta) \quad (218)$$

with  $M = \sqrt{Q^2 + q_T^2}$ . This gives:

$$\sin\theta^* = \sqrt{\frac{4p_T\sqrt{M^2 + p_T^2 - 2p_TM \cosh(y - \eta)}}{Q^2 + 4p_T\sqrt{M^2 + p_T^2 - 2p_TM \cosh(y - \eta)}}}. \quad (219)$$

and:

$$\tan\left(\frac{\pi - \Delta\phi}{2}\right) = \sqrt{\frac{Q^2 + 2p_T \left[ p_T - M \cosh(y - \eta) + \sqrt{M^2 + p_T^2 - 2p_TM \cosh(y - \eta)} \right]}{Q^2 + 2p_T \left[ p_T - M \cosh(y - \eta) - \sqrt{M^2 + p_T^2 - 2p_TM \cosh(y - \eta)} \right]}}. \quad (220)$$

Gathering all pieces together finally gives:

$$\begin{aligned}\phi^* &= \sqrt{\frac{Q^2 + 2p_T \left[ p_T - M \cosh(y - \eta) + \sqrt{M^2 + p_T^2 - 2p_T M \cosh(y - \eta)} \right]}{Q^2 + 2p_T \left[ p_T - M \cosh(y - \eta) - \sqrt{M^2 + p_T^2 - 2p_T M \cosh(y - \eta)} \right]}} \\ &\times \sqrt{\frac{4p_T \sqrt{M^2 + p_T^2 - 2p_T M \cosh(y - \eta)}}{Q^2 + 4p_T \sqrt{M^2 + p_T^2 - 2p_T M \cosh(y - \eta)}}}.\end{aligned}\quad (221)$$

One can show that the boost required to go from the laboratory frame, in which the vectors  $q$  and  $p$  are given by Eqs. (135) and (136), respectively, with  $p_T$  given by Eq. (140), to the Collins-Soper frame, in which:

$$q = Q(1, 0, 0, 0) \quad \text{and} \quad p = \frac{Q}{2}(1, \sin \theta \cos \phi, \sin \theta \sin \phi, \cos \theta), \quad (222)$$

is given by:

$$\Lambda_{\text{Lab} \rightarrow \text{CS}} = \begin{pmatrix} \frac{M}{Q} \cosh y & -\frac{q_T}{Q} & 0 & -\frac{M}{Q} \sinh y \\ -\frac{q_T}{Q} \cosh y & \frac{M}{Q} & 0 & \frac{q_T}{Q} \sinh y \\ 0 & 0 & 1 & 0 \\ -\sinh y & 0 & 0 & \cosh y \end{pmatrix}, \quad (223)$$

with  $M = \sqrt{Q^2 + q_T^2}$ . Likewise, the boost to go from the Collins-Soper to the laboratory frame is the inverse of the above transformation and reads:

$$\Lambda_{\text{CS} \rightarrow \text{Lab}} = \Lambda_{\text{Lab} \rightarrow \text{CS}}^{-1} = \begin{pmatrix} \frac{M}{Q} \cosh y & \frac{q_T}{Q} \cosh y & 0 & \sinh y \\ \frac{q_T}{Q} & \frac{M}{Q} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ \frac{M}{Q} \sinh y & \frac{q_T}{Q} \sinh y & 0 & \cosh y \end{pmatrix}. \quad (224)$$

Notice that rotating the vector in Eq. (136) using the transformation in Eq. (223) and equating the  $z$  component to that of the vector  $p$  in Eq. (222) immediately gives Eq. (207). This immediately allows one to write:

$$\sin \theta = \frac{\sqrt{Q^2 - 4p_T \sinh^2(\eta - y)}}{Q} \quad (225)$$

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